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A REPORT ON SURVEY CAMP 2080

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Submitted to:-

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GROUP-01

Acknowledgements:

We would like to express our sincere appreciation to the **Department of Geomatics Engineering at Paschimanchal Campus** for providing us opportunity to submit our Report titled "A REPORT ON SURVEY CAMP-2080". We have thoroughly reviewed its contents and would like to acknowledge our hard work and dedication in compiling such a comprehensive document.

We are truly grateful to the Department of Geomatics Engineering, Paschimanchal Campus for providing us with the opportunity to apply our theoretical surveying expertise in a practical setting. This year's successful conduct of the survey camp, within the scheduled timeframe and in a pleasant environment, sets it apart from previous years. Such achievement was made possible by the persistent efforts of our Department.

The dedication and tireless contributions of our mentors, Er. Pradip Aryal, Er. Umesh Bhurtel, Er. Roshan Poudel, Er. Netra Bahadur Katuwal, Er. Saurav Gautam, and other teachers, deserve credit for the successful completion of the Survey camp. They guided us through every step, from initiation to conclusion, and provided assistance in overcoming various challenges encountered during the fieldwork. Additionally, we extend our appreciation to other teachers and colleagues for their continued support and cooperation throughout the survey camp on campus.

The topographical survey of the college premises, Road Alignment Survey, and Bridge Site Survey conducted in Kali Khola were carried out based on the parameters specified in the field book. While we made our best efforts to adhere to the criteria, it is possible that the report may contain some mistakes. Therefore, we welcome any feedback and recommendations we may have regarding the report, as they will greatly assist us in improving its accuracy and quality.

Once again, we express our sincere appreciation to the Department of Geomatics Engineering, Paschimanchal Campus for your remarkable work and dedication in completing this report. The knowledge and experience gained through the survey camp will undoubtedly contribute to our future endeavors in the field of Geomatics Engineering.

Thank you for your valuable contribution.

Abstract:

The Survey Camp 2080 organized by the **Department of Geomatics Engineering, IOE Paschimanchal Campus,** aimed to provide students from the 077-BGE Batch with an opportunity to enhance their theoretical and practical knowledge of Engineering Surveying in real field conditions. The camp was conducted at two locations: Kali-khola and its surroundings in Pokhara, as well as Paschimanchal Campus in Pokhara.

This Report consists of tabulated data, graphs and maps of the survey of the road along Kali Khola and the bridge of the same along with the traverse of the campus.

The students formed groups and carried out fieldwork, enabling them to actively participate in the planning and execution of field tasks. The primary goals were to create a topographical map and conduct a detailed survey of the road and bridge. The survey camp significantly contributed to building the students' confidence in conducting Engineering Surveys with accuracy and professionalism.

The report has been prepared using the recorded data and calculations from the survey camp. While efforts were made to ensure accuracy, we acknowledge that errors or mistakes may exist within the document. We kindly request readers to provide constructive feedback upon reviewing the report.

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Abbreviations:

- RL-Reduced Level
- BM-Bench Mark
- TBM- Temporary Benchmark
- TL-Tangent length
- TMB-Top Middle Bottom
- U/S-Upstream
- D/S-Downstream
- HCR-Horizontal Circle Reading
- VCR- Vertical Circle Reading
- WCB- Whole Circle Bearing
- W.T-Water Tank
- BS-Back Sight
- IS-Intermediate Sight
- FS-Fore Sight
- BC-Beginning of Curve
- MC-Middle of Curve
- EC-End of Curve
- RB-Reduced Bearing
- GL-Ground Level
- FL-Formation Level
- RBL-River Bed Level
- LFLR-Low Flood Level Right
- LFLL- Low Flood Level Right
- HFLR-High Flood Level Right
- HFLL- High Flood Level Left
- TT- Table Tennis Board
- OFF-Offset
- BC-Building Corner
- BTOL-Boys Toilet
- SH-Spot Height

CHAPTER-1

INTRODUCTION

Background

Surveying is the process of determining the relative positions of natural and manmade features on or beneath the Earth's surface. This information is presented graphically through plans or statistically through tables. Surveying involves measurements, computations, plan creation, and executing location determinations. Surveyors employ various tools such as total stations, retroreflectors, 3D scanners, robotic total stations, GPS receivers, drones, GIS, radios, handheld tablets, digital levels, and subsurface locators. They also utilize software designed specifically for surveying purposes.

Surveying has played a crucial role in the development of industries and the human environment throughout history. For Geomatics engineering students, surveying courses aim to teach the fundamental techniques of surveying. These techniques are essential in their professional practice for engineering tasks. The completion of all surveying courses, including a 10-day survey camp, is a requirement for Geomatics engineering students. The Department of Geomatics Engineering at Paschimanchal Campus coordinates this camp, which is designed to enhance students' proficiency in various surveying methods. Lecture classes also cover these techniques in detail.

This report provides a comprehensive overview of the work carried out by Group-1 during the survey camp. It is divided into six sections, each describing the functioning of different methods and techniques employed by the group. The report includes observations, computations, error correction methods, encountered challenges, solutions, and outcomes related to the group's work during the camp.

Objectives of Survey Camp:

The camp's major goal is to give a foundation in the practical implementation of various survey tasks that may be encountered in the future. It improves practical knowledge, allowing different jobs and projects to be implemented. On the other hand, it entails a perpetual sense of self-assurance. It directs us where to walk the path that leads to success

The main objectives of survey camp are as follows:

- a. To become familiar with potential fieldwork issues.
- b. To become familiar with proper instrument handling and operation.
- c. To learn about the spirit and value of teamwork.
- d. To accomplish a project on time and so understand the value of time.
- e. To collect required data in a methodical manner in the field.
 - To compute and manipulate observed data with the needed accuracy, and todisplay it in diagrammatic and tabular form so that others can understand it.
- f. To deal with errors and missing data from the field during office work.
- g. To prepare for the final report.

Classification of Surveying:

Survey may be classified on the different heading depending upon the uses or purposes of resulting map.

- > Based on nature of field
- o Land Survey: includes topographical, cadastral and city survey.
- Hydrographic Survey
- Astronomical Survey
- Based on object of survey
- Engineering Survey
- Military Survey
- Mine Survey
- Geological Survey
- Archaeological Survey
- Based on instruments used
- Chain survey
- Theodolite survey
- o Traverse survey
- Triangulation survey
- Tachometric survey
- Plane Table Survey
- Photogrammetric survey
- Aerial Survey

The type of survey we did in our survey camp was an engineering survey, which included the preparation of a topographic map and required both horizontal and vertical controls. We perform the odolite traverse survey for fixing control points, tachometric survey for detailing with total station alliance, and triangulation survey for establishing control points in bridge site survey, depending on the instrument employed.

Principles of surveying:

While surveying, we became careful about the different principles of surveying. We started with the first principle: Working from whole to part. As well as we performed the survey camp keeping in mind the principles: Location of point by measurement from two points of reference, Consistency in work, Independent Check, Accuracy required.

Accuracy and errors:

In any kind of survey, errors are inevitable. As precision is the degree to which the repeatedobservations under same condition shows the same result but accuracy is the level of perfection achieved via observation. It is the degree to which an observation is close to thetrue value. Precision instruments, precise processes, and good planning are all required foraccuracy.

The difference between two measured values of the same quantity is called a discrepancy; it is not an error.

We have different sources and types of error, in maximum cases we tried to avoid errors but there were some as follows:

> Sources of errors:

- o Instrumental error: E.g. a tape too short
- o Personal error: E.g. error while taking staff reading
- Natural error: errors due to different natural phenomenon such as temperature, refraction, etc.

> Types of errors:

Mistakes Systematic errors Accidental errors

In our survey, all the computations were made within permissible error limit. As mentioned earlier, the survey camp was divided into three major works:

- ✓ Topographical survey
- ✓ Road alignment survey
- ✓ Bridge Site survey

Major works carried out:

- ➤ Road Alignment in Kali Khola premises:
- Fixing the stations IP0, IP1....
- Computation of chainages for each beginning, middle and end of curves withthe help of theodolite for total length of about 1037.06 m.
- Cross-sectioning and then fly levelling for determination of reduced levels.
- Setting out of curve.
- Drawing plan, L-section and cross-section in suitable scale.
- ➤ Topographical Survey in Pashchimanchal Campus:
- Reconnaissance survey
- Fixing major stations and forming the major traverse covering the project area.
- Measuring distance by using tape along ranging method in both ways between the major stations and later with total station for greater accuracy.
- Two peg test (Test for Permanent adjustment of level)
- Transfer of R.L from BM to CP1 and to other stations with level machine.
- Detailing with T.S. along with preparation of rough sketches.
- Plotting & topographical map preparation.
- ➤ Bridge Site Survey:
- Reciprocal levelling.
- Triangulation to determine width of river.
- L-section of river.
- Preparing contour map of river.
- Cross-sectioning of the river and also determining high flood level.

Topographic Map Presentation:

Details:

- Scale for Plot of Major Traverse: 1:1000
- Scale for Plot of Detailing Topographic Map: 1:500
- Paper size: A1
- Contour interval: 1 m

Control Points Establishment:

At least 10 - 15 stations (Main control stations)

- Distance measurement by TS with precision less than 1:2000
- Vertical control by levelling.
- Fly Levelling ($\pm 25\sqrt{K}$ mm accuracy)
- Leg ratio: Major Traverse = 1:2

Road Alignment Survey:

- Chainage should be at least 1000 m & deflection angle not too low.
- Preparing plan of road in scale 1:500.
- Preparing L-section of road with scale 1:200 for vertical and 1:1000 for horizontal.
- Preparing cross-section graphs of road in scale 1:100 for vertical and 1:20 for horizontal.

Bridge Site Survey:

- Triangulation was done to determine length of bridge axis.
- Reciprocal levelling was done to determine R.L. of one of stations.
- Preparing contour map of river with contour interval 1 m.
- L-section of river.
- Cross-section graphs of river in ArcMap.

Survey Camp Area:



Figure 1: Paschimanchal Campus Area



Figure 2: Kali- Khola Area

Source: Google Earth

CHAPTER-2

TOPOGRAPHIC SURVEY

Introduction:

Topography is indeed a field of geoscience and planetary science that deals with the detailed study and description of the features and configuration of the Earth's surface. It encompasses various aspects, including relief (variations in elevation), natural features (such as mountains, rivers, and valleys), artificial features (such as buildings and roads), and even local history and culture.

Topographic surveying is the process of accurately determining the positions, both horizontally (plan) and vertically (elevation), of natural and artificial features in a particular area. The purpose of topographic surveying is to create a detailed representation of the terrain, which is typically done by creating a topographic map. This map uses conventional signs and symbols to depict the three-dimensional relationships of the land, showing both horizontal and vertical information.

Topographic maps are essential tools in various fields, including urban planning, engineering, geology, environmental studies, and military operations. They provide valuable information about the shape of the land, the location and characteristics of features, and the spatial relationships between different elements. By accurately representing the topography, these maps allow for better understanding, analysis, and decision-making related to land use, infrastructure development, resource management, and other related activities

Therefore, the fieldwork in a topographical surveying consists of three parts.

- i. Establishing both horizontal and vertical control.
- ii. Locating the contours.
- iii. Locating the details such as rivers, streams, lakes, canals, houses, and trees etc.

Objectives:

To prepare the topographic map of the given area with horizontal and vertical control at required degree accuracy.

Brief description of the area:

Topographic survey was carried out at Pashchimanchal Campus, Lamachaur, Pokhara. Themajor traverse was run covering a major portion of campus area while offset was run through the area where our detailing work was assigned. Our objective was to prepare a topographic map of the given area. Therefore, our major task was to prepare the topographic map of the area including Mechanical and Automobile Workshops, D/Civil Block, Auditorium hall, MSc Hostel, Cafeteria, Mechanical Workshops, Library, different parks, Roads Boundary wall and so on.

Norms (Technical specifications):

- Reconnaissance survey of the area to be surveyed: A closed traverse (major) was formed around the premises of the area by fixing or marking appropriate no. of stations. During the selection of traverse stations, the leg ratio i.e. the ratio of length of thelongest traverse leg to the length of the smallest leg should be less than or equal to 1:2 formajor traverse. References were taken for the major traverses.
- Two-way measurement of the traverse legs: Discrepancy (Accuracy of two-way measurement in the case of major traverse) is 1:1000. Two-way measurement means measurement of the traverse leg in the forward as well as in the backward direction.
- Determination of horizontal angles between stations: With the help of bearing of one of stations, horizontal angles between corresponding stations were determined.
- The difference between the mean angles as well as the difference in each angle observationshould be within 10'.
- Determination of RL of traverse stations by fly levelling from the given B.M: A two peg test was carried out to determine if the level required permanent adjustment. Balancing ofback sight and fore sight is necessary for the elimination of different types of errors including collimation error. The permissible error of fly levelling is ± 25√K mm, where Kis the distance of the levelling passed in kilometer.
- Adjustment of traverse or balancing the traverse: The permissible angular error or the angular mis-closure for the sum of interior angles of the traverse should be within $C\sqrt{N}$, where N denotes the no. of traverse leg or traverse stations and, C=10" for major traverse. For traverse the relative error of closure should be less than 1:1000.
- Detailing or the detail survey of the plot by Total Station: The details were extracted from
- T.S. Conventional symbols were used to denote the detailing along with the contours of 0.5m contour interval in the same scale.
- Plotting of the traverse stations by co-ordinate method: An appropriate scale was adopted, i.e.1:500 for the major traverse and 1:1000 for minor traverse and all the details like trees, buildings, parks, roads, etc. were represented with conventional symbols.

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Instruments used:

The following are the instruments used for topographic survey:

- Measuring tape
- Pegs
- Ranging rods
- Tripod stand
- Auto level
- Levelling Staff
- Total Station
- Clampers
- Reflectors (Target prisms with stands and levelling bubble provided)
- Hammer
- Marker pen
- Field books



Figure 3: Measuring Tape Figure 4: Ranging Rods

Figure 5: Tripod Stand



Figure 6: Level Machine





Figure 7: Levelling Staff

Figure 8: Pegs

Total Station:

A total station is an optical instrument commonly used in modern surveying. It combines the functionality of an electronic theodolite, an electronic distance meter (EDM), and software running on an external computer called a data collector. This instrument allows surveyors to determine both angles and distances from the total station to the points being surveyed.

To calculate the distance, the total station emits and receives multiple frequencies, determining the number of wavelengths to the target for each frequency. This allows for the determination of the distance between the total station and the target object.

Most total stations use a purpose-built glass Porro prism as the reflector for the EDM signal. These instruments can measure distances up to a few kilometers. However, some total stations are "reflectorless" and can measure distances to any reasonably light-colored object, typically up to a few hundred meters.

The typical EDM of a total station can measure distances with an accuracy of about 3 millimeters or 1/100th of a foot. In summary, the basic principle of a total station is based on

determining the time it takes for a light wave to travel a known distance and back, utilizing the velocity of light. With this information, distances, angles, and coordinates can be calculated, allowing for precise surveying and positioning.

The basic principle of Total Station is that the distance between any two points can be known once the time light wave takes to travel the distance and back and the velocity of light is known. Then the following relation, which is already programmed in total station's computer is used to calculate distance:

Distance = (Velocity * Time)/ 2

In this formula, time is total time taken by light wave from EDM to reach reflector and return.



Advantages of Total Station:

A total station is a modern-day surveying instrument that has several advantages like:

- a) Quick setup: Total stations are designed for easy and quick setup on a tripod, often aided by a laser plummet. This allows surveyors to start their work promptly, saving time and increasing efficiency
- b) On-board area computation: Total stations are equipped with software that can compute the area of a field or land directly within the instrument. This feature eliminates the need for manual calculations and speeds up the surveying process.
- c) Language support: Many total stations support multiple languages, allowing surveyors to operate the instrument in their preferred language. This feature enhances ease of use and ensures effective communication.
- d) Graphical view: Total stations provide a graphical view of the land and plots being surveyed. This visual representation helps surveyors better understand the terrain and make more informed decisions during the surveying process.
- e) Computerization of old maps: Total stations, when used in conjunction with appropriate software, can facilitate the computerization of old maps. This process involves capturing survey data from existing maps and integrating it with digital systems for improved accessibility and analysis.

These advantages collectively contribute to enhanced productivity, accuracy, and efficiency in surveying operations.

Disadvantages of Total Station:

- 1. The instrument is costlier than other conventional surveying instruments.
- 2. It might be troublesome for the surveyor to investigate and check the work when surveying.
- 3. Working with total station is not so easy, as more skilled surveyors are required toconduct a total station survey.

Methodology:

The methodology is based on the principles of surveying. They are as follows:

- 1. Working from whole to a part
- 2. Location of a point with respect to at least two control points
- 3. Independent check
- 4. Consistency in work
- 5. Required accuracy

The different methodologies were used in surveying to solve the problems arise in the field. These methodologies are as follows:

Reconnaissance (Recci):

Reconnaissance plays a crucial role in surveying as it involves the initial exploration and assessment of the survey area. It provides an overall understanding of the site and helps in

- detailed planning by making necessary observations and assessments. Here are the key points to consider during the reconnaissance phase:
- 1. Exploration and assessment: During reconnaissance, surveyors walk around the survey area to gather information about various aspects such as the total area, type of land, topography, vegetation, climate, geology, and inter-visibility conditions. This helps in gaining a comprehensive understanding of the site.
- 2. Fixing traverse stations: Based on the observations made during reconnaissance, the positions of traverse stations are planned. The adjacent stations should have clear line-of-sight visibility to ensure accurate measurements and efficient surveying.
- 3. Minimum number of stations: The aim is to include the least number of stations possible while maintaining the required accuracy. This helps in optimizing resources and reducing surveying time.
- 4. Traverse leg ratio: The ratio of the minimum traverse leg to the maximum traverse leg is an important consideration. For major traverses, this ratio should be less than 1:2, while for minor traverses, it should be less than 1:3. Maintaining these ratios ensures balanced measurements and accurate traversing.
- 5. Suitable station locations: Traverse stations should be positioned to provide a minimum level surface for setting up the surveying instrument. This helps in ensuring stability and accuracy during measurements.
- 6. Avoidance of difficult terrain: Steep slopes and badly broken ground should be avoided as much as possible during the selection of traverse stations. Such terrain can introduce difficulties in measurements and may affect the accuracy of the survey.
- 7. Atmospheric refraction considerations: The selection of stations should avoid placing the line of sight too close to the ground level. This minimizes the potential errors caused by atmospheric refraction, which can affect measurement accuracy. By taking these points into consideration and fixing the traverse stations accordingly, the reconnaissance phase is completed.

This preliminary step provides the necessary foundation for the subsequent surveying activities

Traversing:

Traversing is a type of surveying in which a number of connected survey lines form the framework of survey. It is also a method of control surveying. The survey consists of the measurement of angles between successive lines or bearings of each line and the length of each lines.

The directions and lengths of the lines are measured with the help of angle measuring instrument and length measuring instruments like Total Station (or Theodolite) and an Electronic Distance Measurement (EDM) system respectively. If the co-ordinates of the first station and the bearing of the first line are known, the co-ordinates of all successive points can be computed as follows:

X2 = X1 + Lcose

Y2 = Y1 + Lsine

Where, L=Length of traverse leg, Θ is the bearing of the line and (X1, Y1) is known coordinate.

Types of Travers

A. Closed Traverse:

A traverse is said to be closed when a complete circuit is made or when it begins and ends at points whose positions on plan are known. (Or) If the traverse formed by the lines closesat a station i.e. if they form a polygon or it starts and finishes at the points of known co- ordinates, then the traverse is called closed traverse. A traverse is said to be a closed loop traverse if it returns to the starting point, thereby forming a closed polygon. In addition, a traverse which begins and ends at the points whose position on the plan is known are referred as a closed linked traverse.

B. Open Traverse:

If the traverse ends elsewhere other than at the starting point or at some other point, then the traverse is termed as an open traverse. It consists of a series of lines expanding in the same direction. It is employed for surveying long narrow strips of country such as the path of highway, canal, pipeline, etc.

Major traverse:

The whole site which was to be surveyed was enclosed by a number of inter-connecting survey lines forming a closed circuit or a framework joining successive major control points. This was the required major traverse. The skeleton of lines joining those control points, which covers the whole entire area, is called major traverse. Work on major traverse must be precise. Therefore, two-set of readings should be taken for major traverse.

In the survey camp, two traverses - major and minor had to be established. The major traverse had12 control stations including two given common points. The control stations were named as M1, M2and so on along with CP1 & CP2 (the common points). The leg ratio of maximum traverse leg to minimum traverse leg was maintained 1:2. The discrepancy in length between the forward measurements and the backward measurements of all the traverse legs was within 1:1000.

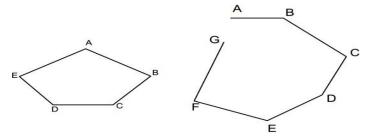


Figure 10: Closed Traverse and Open Traverse

Fixing of control points:

After the completion of reconnaissance of the area to be surveyed, the major traverse control points were fixed by driving pegs into the ground or by marking the points with marker including the group name and the station number. Some of the points needed to

bekept in the mind while fixing major traverse stations are as follows:

- Inter-visibility of the adjacent major traverse stations.
- Maintaining of the permissible leg ratio of 1:2.
- Measurement of traverse legs without any obstruction.
- Fixing of stations with reference points as well as a neat sketch.
- Fixing of stations driving wooden pegs and marking with marker.

Measurement of traverse legs:

Work on the major traverse should be precise. Thus, after appropriate selection and fixing of major traverse stations, two-way measurements of the traverse legs were carried out making use of EDM in the total station. The distances between the adjacent control points were accurately measured as far as possible for the accuracy of the whole traverse. The precision of the measurement should be within 1:1000.

Discrepancy and linear misclosure:

In order to measure the lengths of the sides of the traverse, two ways of taping (forward and backward) are done. In difficult areas where taping is not possible, other methods like the subtense bar are used. The difference in values obtained by forward and backward taping is called discrepancy. The reciprocal of the mean of the two measurements divided by the discrepancy is called precision. Both the discrepancy and the precision for each traverse leg should be within the given limits.

```
Mathematically,
Discrepancy = | Forward length - Backward length |
and,
Linear precision = 1 / (Mean length / Discrepancy)
```

Measurement of traverse angles:

The horizontal angles between the traverse stations were measured by the help of a knownbearing of a station. The difference in two angles and as well in each of the angular observation cannot exceed 1' as stated earlier.

Sum and the correction of the interior angles:

Permissible Angular Error for the closed traverse = $C\sqrt{N}$

```
Where, N = no. of traverse legs
```

C = 10'

For a closed traverse,

Sum of interior angles = $(2n - 4) \times 90^{\circ}$

Closing error = $(2n - 4) \times 90^{\circ}$ - \sum Observed sum of internal angles

If the angular error is within the permissible value of 10^{i} N, then the error in the sum of internal angles is equally distributed.

Computation of the co-ordinates:

After the computation of bearings and having the average lengths of all traverse legs, the positions or the co-ordinates of the major stations are calculated.

a) Consecutive co-ordinates:

The latitude of the survey line is defined as its coordinate length measured parallel to an assumed meridian. It is also termed as northing. The departure of the survey line is defined as its coordinate length measured perpendicular to an assumed meridian. It is also termed as easting.

Each station point is defined by its latitude and departure with respect to the origin.

Latitude of B = Latitude of $A + L*cos\theta$

Departure of B = Departure of A + $L*\sin\theta$

Where,

 θ = Bearing of the line AB

L = Length of the line AB

b) Independent co-ordinates

The latitude and departure of any line with respect to common origin of co-ordinates are called independent co-ordinates or total co-ordinates. The independent co-ordinates are calculated after the traverse is completely balanced. They are obtained by adding algebraically the latitudes and departures of the traverse legs between that station and origin.

Closing Error:

In closed traverse when plotting according to the field measurements, if the end point of the traverse will not coincide exactly with the starting point due to the error in the field measurements of the length and angles, then it is called closing error. In a closed loop algebraic sum of Latitude (ΣL) and of departure (ΣD) must be zero.

```
Mathematically,
```

```
Closing error (e) = \sqrt{[(\Delta L)^2 + (\Delta D)^2]} And
```

Direction,
$$\tan \theta = ((\Delta D)/(\Delta L))$$

The sign of ΔL and ΔD will thus define the quadrant in which the closing error lies. The relative error of closure (Accuracy ratio)

```
= Error of Closure / Perimeter of the traverse
```

$$= e / P$$

$$= 1 / (P/e)$$

Balancing the traverse:

The process of adjusting the consecutive co-ordinates by applying the correction to the latitudes & departures of each of the traverse legs such that their algebraic sum is equal tozero is called balancing the traverse or balancing the consecutive co-ordinates. A closed traverse can be balanced by any one of the following methods.

- 1. Bowditch's method
- 2. Transit rule
- 3. Graphical method
- 4. Axis method

a. Bowditch's Method:

The method is based on the assumption that errors in the linear measurement are proportional to \sqrt{L} and the errors in the angular measurements are inversely proportional to \sqrt{L} where L is the length of a line. The method is applicable when both the linear as wellas angular measurements are of equal precision.

The Bowditch rule is:

Correction to latitude (or departure) of any side =Total error in latitude or departure×Length of that side/perimeter of the traverse(lat= $\sum (Lat) \times L / \sum L_s$)

&(Dep= \sum Dep \times L/ \sum L_S)

Where,

 $Lat = Correction \ to \ latitude \ of \ any side$ $Dep = Correction \ to \ departure \ of \ any \ side$ $\Sigma(Lat) = Total \ error \ in \ latitude$ $L_S = Length \ of \ any \ side$

Levelling:

Levelling is defined as the branch of surveying which deals in finding the elevations of the given points with respect to a given or an assumed datum. It also deals with establishing the points at a given elevation with respect to a given or an assumed datum. It deals with the measurement in a vertical plane. It helps to provide the vertical controls in a topographic map. The elevations of the relevant points must be known so that complete topography of the area can be explored. Accurate determination of the elevations of different points alongthe certain alignment is a necessary part. Hence, it is a subject of prime importance to engineers and the project as a whole.

Types of levelling:

Two types of levelling are used in general Engineering practices, namely direct levelling (spirit levelling) and indirect levelling (trigonometric levelling).

1. Direct Levelling:

It is the branch of levelling in which the vertical distances with respect to the horizontal line (perpendicular to the direction of gravity) may be used to determine the relative difference in elevation between two adjacent points. A level provides horizontal line of sight i.e. a line tangential to the level surface at a point where the instrument stands. The difference in the elevation of the two, points is the vertical distance between the two-levellines. With a level set up at any place, the difference in the elevation between any two points within proper lengths of sight is given by the difference between the rod readings taken on these points. By a succession of instrument stations and related readings, the difference in elevation between widely separated points is thus obtained.

Following are some special methods of direct levelling:

a) Simple Levelling

It is the method of levelling which is used to determine the difference of elevation between two points which are visible from a single point. This method is applied when the distancebetween two points is not too long. In this type of levelling, only the middle wire reading against the staff held is observed and recorded.

b) Differential Levelling

It is the method of direct levelling the object of which is solely to determine the difference in the elevation of two points regardless of the horizontal positions of the points with respect to each other. This type of levelling is also known as fly levelling. All three wire readings are observed and recorded. This method was employed at the survey camp to transfer the RL to major and minor traverse stations.

c) Profile levelling

It is the method of levelling the object of which is to determine the elevations of the points at measured intervals along the given line in order to obtain the profile of the surface alongthat line.

d) Cross-sectioning

It is the process of taking the levels on each side of the main line at right angles to that line, in order to determine a vertical cross- section of the surface of the ground, or of underlying strata, or of both.

e) Reciprocal levelling

It is the method of levelling in which the difference in the elevation between two points isaccurately determined by two sets of reciprocal observations when it is not possible to setup the level between the two points.

2. Indirect levelling

Indirect method of trigonometric levelling is the process of levelling in which the elevations of the points are computed from the vertical angles and horizontal distances measured in the field, just as the length of any side in any triangle can be computed from proper trigonometric relations.

Adjustment of level

A. Temporary adjustment of level:

The adjustment of level that needs to be done before each observation is known as the temporary adjustment of level. The temporary adjustment of the level is done in followingsteps:

a) Setting up the level:

The operation of setting up includes the fixing the instrument on the stand and levelling the instrument approximately.

b) Levelling up:

Accurate levelling is done with the help of foot screws and with reference to the plate levels. The purpose of levelling is to make the vertical and horizontal line of sight truly horizontal.

c) Removal of parallax:

Parallax is a condition arising when the image formed by the objective not formed in the plane of cross hairs. Parallax is eliminated by focusing the eyepiece for distinct vision of the crosshairs and by focusing the objective to bring the image of the object in the plane of the cross hairs.

B. Permanent adjustment of level:

Permanent adjustment of the level is the adjustment of level that is done when the corresponding relationship between the parts of the instrument is disturbed. To check the need of the permanent adjustment of the auto level the two-peg test is carried out. Two staffs were placed at A and B of known length (about 50 m). First the instrument was setupon the line near B and both staff readings (Top, Middle, and Bottom) were taken. Then, theinstrument was setup at the middle C on the line and again both staff readings on A and Bwas taken. Then computation was done in order to check whether the adjustment was within the required accuracy or not.

Booking and calculation of reduced levels:

There are two methods of booking and reducing the elevation of points from the observed staff readings. They are as follows:

a. Height of Instrument method (HI method)

b. Rise and fall method

HI Method:

In this method, firstly the height of instrument is calculated by back sighting to a known station i.e. adding back sight (BS) to RL of BM or previous known station for each setting of instrument. The RL of the next station is then calculated by subtracting the foresight (FS) to the HI. If any intermediate sights (IS) are taken, then their RL is also calculated by subtracting IS from HI. HI is calculated for every new set up of instrument.

Arithmetic Check:

$$\sum BS - \sum FS = Last R.L. - First R.L.$$

Rise and Fall Method:

It is the method which was mostly used in the survey camp for fly levelling as well as in the case of transferring RL from TBM to the entire major and the minor traverse stations. In rise and fall method, the height of instrument is not at all calculated but the difference of level or elevation between consecutive points is found by comparing the staff readings on the two points for the same setting of the instrument. The difference between their staff readings indicates a rise or fall according as the staff reading at the point is smaller or greater than that at the preceding point. The figures for rise and fall worked out thus for all the points give the vertical distance of each point above or below the preceding one, and if the level of any one point is known the level of the next will be obtained by adding its rise or subtracting its fall, as the case may be.

$$\sum BS - \sum FS = Last R.L. - First R.L. = \sum Rise - \sum Fall$$

Fly Levelling:

The fly levelling was carried out between TBM1 and TBM2 and check levelling was performed to check the results.

Level transfer to the major and minor traverse stations:

The R. L of the temporary benchmark was then transferred to the control stations of the major and minor traverse. The closing error was found to be within the permissible limits. The misclosure was adjusted in each leg of the levelling path by using the following formula:

Permissible error = $\pm 25\sqrt{k}$ mm.

Where k is the total perimeter in Km

Actual Error (e) =
$$\Sigma BS - \Sigma F.S.$$
 = Last R.L. – First R.L. Correction i^{th} leg = -(e * (L1 + L2 + ... + Li)/P

Where L1, L2, Li = Length of 1^{st} , 2^{nd} , i^{th} leg.

Detailing:

Detailing can be done by using total station either in EDM mode or in Co-ordinate mode.

Contouring:

A contour is an imaginary line of constant elevation on the ground surface. It is the line in which the surface of the ground is intersected by the level surface.

Contour interval and Horizontal Equivalent:

The vertical distance between any two consecutive contours is called the contour interval. The contour interval is kept constant for a contour plan or the topographic map otherwise the general appearance of the map will be misleading. The horizontal distance between twopoints on two consecutive contours is known as horizontal equivalent and it depends upon the steepness of the ground. The choice of the proper contour interval depends upon the following considerations:

- **❖** The nature of the ground
- ❖ The scale of the map
- ❖ The purpose and the extent of the survey
- Time and expense of field and the office work

Characteristics of Contours:

The characteristic features of the contour which are used while plotting and reading a contour map or the topographic map are summed up as follows:

- i Two contour lines of different elevations cannot cross each other. They can cross each other only in the case of overhanging cliff.
- ii Two contour lines of different elevations cannot unite to form a single. If they do, it is only in the case of vertical cliff.
- iii Closely spaced contour lines represent a steep slope. Broadly spaced contour lines represent a gentle slope. Equally spaced contour lines represent a uniform slope. A series of straight, parallel and equally space contours represent a plane surface.
- iv A contour line cannot split into two or more contour lines.
- v A series of closed contour lines with higher value of contour i.e. with contour having higher value of elevation inside represent a hill whereas a series of closed contour lines with lower value of contour inside represent a pond or the depressed land.
- vi A contour line must close upon itself, though not necessary within the limits of the map.
- vii Contour lines cross a watershed or the ridge line at right angles. They form curves of U-shaped round it with the concave side of the curve towards the higher ground.
- viiiContour lines cross a valley line at right angles. They form sharp curves of V- shaped across it with the convex side of the curve towards the higher ground.

Methods of Locating Contours:

The location of a point in topographic survey involves both horizontal as well as vertical control. The methods of locating contours, therefore, depend upon the instruments used which are:

- a) Direct method
- b) Indirect method

In the direct method, the contour to be plotted is actually traced on the ground. Only those

points are surveyed which needs to be plotted. After having surveyed those points, they are plotted and the contours are drawn through them. The method is slow and tedious and is used for the small areas where great accuracy is required.

In the indirect method, some suitable guide points are selected and surveyed; the guide points need not necessarily be on the contours. These guide points, having been plotted, serve as basis for the interpolation of contours. This is the method most used in engineering surveys.

Interpolation of the Contour lines:

Interpolation of the contour is the process of spacing the contours proportionately between the plotted ground points established by indirect methods. The method of interpolation is based on the assumption that the slope of the ground between the two points, which are surveyed, is uniform. There are different methods of interpolation of contours. They are as follows:

- Estimation
- **❖** Arithmetic calculations
- Graphical method

Estimation:

This method is extremely rough and is used for small scale work only. The position of the contour points between the guides points are located by estimation.

Arithmetic Calculations:

The method, though accurate, is time consuming. The position of contour points between the guide points are located by arithmetic calculation.

 $X=H\times Y/V$

where,

X= Horizontal distance of the point to be located H= Horizontal distance between two guide points V= Vertical distance between two guide points

Y= Vertical distance between the point to be located and lower elevation point

Graphical Method:

In the graphical method, the interpolation is done with the help of a tracing paper or a tracing cloth.

Result

The longest distance of the traverse was 156.3195m and the least distance of the traverse was 90.9275m.

Comments and Conclusion:

In this way, topographical map of the detail area was created, for which first the control stations were located and the lengths between the stations were taken. Levelling and then fly levelling were done to determine elevations of several points. The measurements related to details were taken with total station which were plotted later on A1 paper on scale 1:500.

CHAPTER-3

ROAD ALIGNMENT SURVEY

Introduction:

Roads are paths prepared to provide ways between different places for the use of the vehicles, people and the animals. Roads are used in countries like Nepal, where there are less chances of airways and almost negligible chances of other transportation systems. Rural road alignment has mainly two important tasks – to run a road between two points, i.e. to fix or choose appropriate road alignment between two points which are far apart andto carry out the survey for the safe, economical and appropriate construction along the route. This specific job is essential for an engineer combating with the mountainous topography of Nepal. This part of the survey camp deals with the road alignment survey carried out at Bhalam-Bridge to Swine Farm beside Kali Stream.

Objectives of road alignment survey:

The following are objectives of carrying out road alignment survey:

- To set out curve with appropriate radius and deflection angle.
- To prepare plan, cross-section and L-section of the road.
- To work in co-ordination with team members to ease out setting of curve.
- To get technical knowledge on working procedure & methodology on setting out curve.

Brief description of the area:

The site for the road alignment survey is located at Bhalam-Bridge to Swine Farm beside Kali Stream, which is almost 20 minutes' walk from the campus area where the topographic survey was carried out. The place was accessible via various suspension bridges and a motorable bridge from Dip & Batulechaur areas. The area was surrounded by hills and Kalistream flowing beside made the environment cooler. The land was undulated with no large boulders or rocks of any kind along the proposed site. The soil is uniform throughout the whole length of the road. Soft clayey soil was found along the road course.

Technical specifications (Norms):

- 1. Simple horizontal circular curves had to be set out where the road changed its direction, determining and pegging three points on the curve- the beginning of the curve, the middle of curve and the end of the curve along the centerline of the road.
- 2. A convenient radius and deflection angle was chosen.
- 3. The plan was drawn in A1 paper on scale 1:1000.
- 4. L-section was drawn in graph paper to determine total cut and fill.

5. Cross sections were drawn in graphs to determine cuts and fills. They were drawn on scale 1:100.

Instruments used:

The equipment used in the surveying during the road alignment survey are as follows:

- 1. Theodolite
- 2. Tripod stand
- 3. Ranging rods
- 4. Level machine
- 5. Levelling staff
- 6. Measuring Tape
- 7. Pegs
- 8. Hammer
- 9. Marker
- 10. Field book

Methodology:

Fixing of stations:

By visual inspection and self-judgment, the appropriate location for the stations to be placed is decided which is basically done by inspecting where the road had turns. The stations were named IPO, IP1, and IP2 and so on.

Measurement of Lengths and Deflection Angles:

The distances between the IP's were measured with the help of measuring tape by rangingbetween IP's. One set of horizontal angles was measured for the deflection angle. The faceleft reading was observed, and the deflection angles were calculated. As the traverse formed as open traverse, no angular correction could be made. So as far as possible, both the linear measurements as well as the angular measurements were observed carefully and precisely.

Horizontal Alignment:

The center line of the road for fixing the direction of the proposed road in the horizontal plane is known as horizontal alignment. For fixing horizontal alignment, the bearing of theinitial line connecting two initial IP's was measured using compass. The interior angle was measured with the help of theodolite at each IP and the deflection angles were computed.

Deflection angle (Δ) = (360° or 180°) – observed angle

Curve Setting:

Curves are generally used on rural road where it is necessary to change the direction of themotion of the vehicle. A curve may be circular, parabolic or spiral and is always tangential to the two straight directions commonly known as tangents. Curves which are generally used on highways are as follows:

- 1. Simple Circular Curve
- 2. Transition Curve
- 3. Vertical Curve

Simple Circular Curve:

A simple circular curve is the one which consists of a single arc of a circle. It is tangential to both straight lines namely tangents. During the road survey, it is always kept in mind that the radius of the simple circular curve should not be less than 12m. As far as possible, flat circular curves are preferred to that of the sharp one. Flat curves are comfortable to thepassengers and there is less possibility of accident. Before setting out the curve, its elements are essential to be computed. Some essential elements of simple circular curve are as follows:

• Length of Tangent = $RTan\Delta/2$

Where, R= radius of simple circular curve & Δ = deflection angle

- Length of long chord = $2R\sin\Delta/2$
- Apex distance = R (Sec $\Delta/2$ -1)
- Mid ordinate = R $(1 \cos \Delta/2)$
- Length of curve = $\pi R\Delta/180$
- Chainage of T1= Chainage of IP RTan $\Delta/2$
- Chainage of T2= Chainage of T1 + $\pi R\Delta/180$

Setting out of Simple Circular Curves a simple circular curve can be set in the field by various linear and angular methods which are listed as follows:

- **a. Linear method:** Linear method is defined as the method of setting curve in which onlychain or tape is used, i.e. no angular instruments are used to set the curve. This method is preferable where high accuracy is not required and the length of the curve to be set is short. Some common linear methods of setting of the simple circular curve are as follows:
- By ordinates from the long chord
- By perpendicular offset from tangents

- By radial offset from tangents
- By offset from the chords produced
- By successive bisection of the curves
- **b. Angular method:** Angular method is the one in which both angles and the distances are used to set the curve in the field. Generally, tangential deflection angle is observed with the help of theodolite and the distance is measured by making use of tape provided. Someof the most common angular methods of setting out of simple circular curve are as follows:
- Rankine's method of tangential angles
- Two Theodolite method

Levelling and fly levelling to determine reduced levels:

Levelling operation was carried out to determine the reduced levels of the road at various chainages. L-section and similarly, cross-sections were drawn with its help to determine total volume of cut/fill required.

After setting out curve, following works are done:

- 1. The plan of the road is drawn on scale 1:1000 in A1 paper.
- 2. The longitudinal section of the road is drawn to determine total height of cut/fill.
- 3. Cross sections at every 20 m intervals are drawn using the data obtained from the field likeside slopes, chainage, etc. considering drainage and maintaining a stable slope. The cross-sections are drawn in scale 1:100 in graph papers.

Result:

The highest elevation of the road leveling was found to be 1030.699m and the lowest elevation was found to be 999.252. The latitude and departure of each station of traverse was tabulated in the table.

Comments and Conclusion:

Survey of the road alignment is done to make safe, easy, short and economical road. Geological stability and soil stability are also considered. Horizontal curves are set according to Road design standards for comfort and other factors. While setting the road alignment, it should be kept in mind that the minimum IP points should be taken as far as possible and deflection angles should be minimal as far as possible. In this way, road survey work was carried out successfully.

CHAPTER-4

BRIDGE SITE SURVEY

Introduction:

The bridge site survey is intended to determine the appropriate location for bridge site selection. This survey was carried out on Kali Stream. Bridges are important infrastructures in engineering and therefore, appropriate measures should be taken during their site selection and construction. Bridge site survey included determination of length of bridge axis by triangulation, determination of R.L. of a station by reciprocal levelling, and drawingcross-sections of river.

Location:

The venue for this survey was in Kali stream. It lies besides the Bhalam-Dadagaon Road. This site could be accessible from the Pashchimanchal Campus at an estimated 20 minutes' walk.

Geology of the area:

This site was surrounded by vertical cliffs on sides. There was huge elevation difference as we proceeded towards south. The river was basically wide with not that large volume ofwater as the survey was carried out in dry season, making us easy to perform the survey.

Objectives of bridge site survey:

The following are objectives of carrying out bridge site survey:

- To determine the length of bridge axis by triangulation.
- To perform reciprocal levelling to determine the elevation of one of the stations.
- To determine the L-section, contour map and cross-sections to get general idea on thelayout of river.
- To determine if bridge placed on that axis will be feasible or not in long-term.

Technical specifications (Norms):

- 1. First of all, triangulation was done to determine the length of bridge axis.
- 2. Then, reciprocal levelling was carried out to determine the elevation of one of the stations.
- 3. Marks were made at intervals of every 25m upstream and downstream about the main station up to total length of 150m upstream and 75m downstream.
- 4. From these data, reduced levels of all staff positions were calculated and These data were utilized to draw the L-section, cross-section and contour map of riverin appropriate scales.

Instruments used:

- Pegs
- Theodolite
- Tripod stand
- Ranging rods
- Levelling staffs
- Markers
- Field book

Methodology:

Following steps were adopted during the bridge site survey:

Triangulation:

Triangulation surveying is the tracing and measurement of a series or network of trianglesto determine distances and relative positions of points spread over an area, by measuring the length of one side of each triangle and deducing its angles and length of other two sides by observation from this baseline.

Triangulation is preferred for hills and undulating areas, since it is easy to establish stationsat reasonable distances apart, with inter-visibility. In plane and crowded areas, it is not suitable as the inter-visibility of stations is affected. The difficulty is overcome by buildingtowers which is quite expensive.

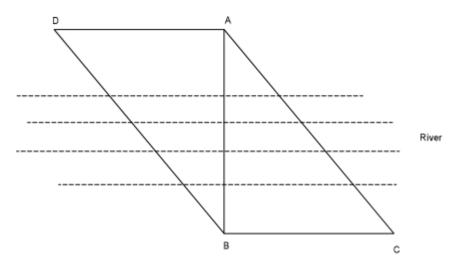


Figure 12: Triangulation

Reciprocal levelling:

It is better to keep distance of fore sight and back sight equal in levelling the following errors are eliminated by doing so:

- Error which occurs due to non-parallelism of line of collimation and axis of bubble tube.
- Errors which are occur due to curvature and refraction.

But in levelling across obstacles like ravines and rivers, it is not possible to maintain equaldistances for back sight and fore sight. In such case reciprocal levelling as described belowis used:

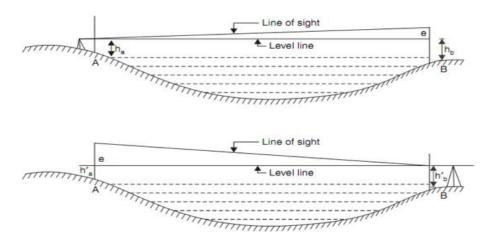


Figure 13: Reciprocal Levelling

Referring to first figure:

Since A is very near, error in reading at A is negligible. Therefore, ha is accurate reading. Assume error in hb be 'e',

Then accurate reading at B = hb - e

- \therefore Difference in elevations = H = ha (hb e) ... (i)
- (ii) Referring to second figure, since B is very near to instrument, hb' may be taken asaccurate reading.

Accurate reading at A = ha' - e

Difference in elevations H = (ha' - e) - hb' ...

(ii) From equations (i) and (ii) we obtain,

$$2 H = h_a - (h_b - e) + (h_{a'} - e) - h_{b'}$$

= $(h_a + h_{a'}) - (h_b + h_{b'})$
Therefore, $H = ((h_a + h_{a'}) - (h_b + h_{b'})/2)$

Therefore, the true difference in the elevations of the 2 points is equal to the mean of the 2 apparent differences in the elevations.

GIS works:

Finally, the reduced levels of all the staff positions were determined. Knowing chainage and elevations, contour map was drawn on scale 1:500 with contour interval 1 m. longitudinal section of river was drawn indicating high floodlevel and existing flood levels. Cross sections at each 10 m interval were drawn.

Result:

The smallest RL was found to be 899.678 along downstream and the highest RL at the bed level was found to be 904.081 along upstream. By reciprocal leveling the leveling difference of the station of bridge was found to be 0.8775.

Comments and conclusion:

Hence, in this way, bridge site survey was carried out across Kali Stream and length of bridge axis was determined by triangulation, reduced level of one of the stations by reciprocal levelling, reduced level across different intervals upstream and downstream were determined and finally these data were plotted in the form of longitudinal section, cross-sections and contour maps to decide the feasibility of bridge siteselection. The data agrees to feasibility of the bridge site selection as high flood level determined is not that high, also the length of bridge axis is not that high. No meandering of river also hints feasibility for the bridge construction.

Recommendation:

Since, survey is not the work to be done by single individual, team work is the must in the survey field and in our project work. In each and every task whenever there is confusion it's better to ask for teacher's help rather them assuming the conclusion by oneself. We should be careful on selecting the proper and least control stations for the topographic maps. We should be careful so that we make mistakes at least as possible. Division of workand management of time is must. Afterall, we should have fun along with our work.

In our road site survey, we should take the proper care while selecting the curves so as notto form the reverse curve. We should be skillful on using all the instruments and also be co-operative in group while and after completion of survey work. In bridge-site survey, fast and careful data observation should be done since there is a lot more chance of error occurrence. We should be prepared for all climatic condition and the situations you didn'thope for. In conclusion, survey is not just a work to be done, it is the skill to be learnt, teamwork to be done to move forward to know little more about the real field.

Bibliography:

- 1. Agor, R., A Textbook of Surveying and Leveling, Khanna Publishers.
- 2. Jain, A.K., Jain, A.K. and Punmiya, B.C., Surveying Volume I and II. Lakshmi Prakashan.
- 4. Surveying manuals: G.I. Book House, Er. M.K. Mishra
- 5. Surveying and Levelling by NN Basak
- 6. Websites: www.wikipedia.com, www.theconstructor.org/surveying, etc.

BRIDGE SITE SURVEY

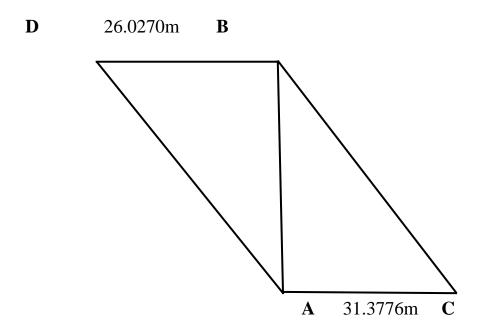
Triangulation Survey

Inst.	Sighted]	HCR		Anglo	Mean	Horiz. Angle	
Stn.	to	D	M	S	Angle	Mean	Homz. Angle	
	В	0	0	0	86°30'47"			
	D	179	59	44	80 3047	86°30'44"		
	С	86	30	47	86°30'41"	80 30 44		
A	C	266	30	25	80 3041		86°31'6.75"	
A	В	60	0	0	86°31'21"		00 31 0.73	
	D	240	0	3	80 31 21	86°31'29.5"		
	С	146	31	21	86°31'28"	00 31 29.3		
	C	326	31	41	00 31 20			
	A	0	0	0	50°10'48"			
	A	179	59	57	30 1046	50°10'37.5"		
	В	50	10	48	50°10'27"	30 10 37.3		
C	D	230	10	14	30 1027		50°10'21.75"	
	A	60	0	0	50°10'3"		30 10 21.73	
	A	240	0	17	30 10 3	50°10'6"		
	В	110	10	3	50°10'9"	30 100		
	D	290	10	26	30 10 9			
	A	0	0	0	96°2'37"			
	A	180	0	5	90 231	96°2'40.5"		
	D	96	2	37	0692!44"	90 240.3		
D	D	276	2	49	96°2'44"		96°2'32"	
В	A	60	0	0	96°2'20"		90 2 32	
	A	239	59	46	90 2 20	0602122 5"		
	D	156	2	20	96°2'27"	96°2'23.5"		
	D	336	2	13	90 221			
	D	0	0	0	10026112"			
	В	180	0	2	49°36'43"	10026115 5"		
	Α	49	36	43	1002611011	49°36'45.5"		
D	A	229	36	50	49°36'48"		10026111 75"	
D	D	60	0	0	40026"21"		49°36'41.75"	
	В	239	59	43	49°36"21"	4002612011		
		109	36	21	10026"55"	49°36'38"		
	A	289	36	38	49°36"55"			
В	С	0	0	0	43°18'21"	43°18'14.5"	43°18'15.75"	

		180	0	22			
	A	43	18	21	43°18'8"		
	A	223	18	30	43 166		
	C	60	0	0	43°18'19"		
	C	239	59	57	43 16 19	43°18'17"	
	A	103	18	19	43°18'15"	45 1617	
	A	283	18	19	43 16 13		
	D	0	0	0	34°20'14"		
	D	179	59	54	34 20 14	34°20'16.5"	
	В	34	20	14	34°20'19"	34 20 10.3	
A	Б	214	20	13	34 2019		34°20'11.25"
A	D	60	0	0	34°20'5"		34 20 11.23
	D	240	0	20	34 203	34°20'6"	
	В	94	20	5	34°20'7	34 200	
	Б	274	20	27	34 20 7		

Reciprocal Leveling

	First Set (Instrument at bank A)												
	Readi	ng at A		Reading	at B	Mean Central	Mean Central Value						
T	M	В	T	M	В	Value(a ₁)	(b ₁)						
1.038	1.023	1.008	2.065	1.904	1.743	1.023	1.904						
	Level difference=h=a ₁ -b ₁ =-0.881												
			Second S	Set (Instru	ıment at	bank B)							
	Readi	ng at A		Readi	ng at B	Mean	Mean						
Т	M	В	Т	M	В	Central Value(a ₂)	Central Value(b ₂)						
0.62													
	Level difference=h'=a ₂ -b ₂ =-0.874												
	True level difference between two points (H)=(h+h')/2=-0.8775												



Here, From ABD, AB= 35.144m From ABC, AB= 35.134 Span of Bridge= 35.1390m

ROAD ALIGNMENT SURVEY

Road Alignment Sheet

	Distance	Chainage	Deflection	on Angle(D	egrees)		Tangant	Length	Anov	Mid	Chainaga	Chainaga	Chainaga	_
IP	between IP	of IP	Degree	Minutes	Second	Radius	Tangent Length	of curve	Apex distance	ordinate	Chainage of B.C	Chainage of M.C	Chainage of E.C	Remarks
SP		0												
IP1	35.65	35.65	38	7	16	30	10.3698	19.9682	1.74166	1.64609	25.2802	35.2643	45.2484	LHC
IP2	37.011	71.88959	60	4	43	20	11.5709	20.9798	3.10599	2.68847	60.3187	70.8086	81.2985	RHC
IP3	60.37	130.0975	85	12	25	20	18.4042	29.7548	7.17933	5.28293	111.693	126.571	141.448	LHC
IP4	60.67	183.7139	60	49	29	20	11.7455	21.2404	3.19388	2.75407	171.968	182.589	193.209	RHC
IP5	85.32	266.7833	27	7	28	15	3.61993	7.10402	0.43061	0.4186	263.163	266.715	270.267	RHC
IP6	20.44	287.0875	50	17	34	15	7.04456	13.1719	1.57184	1.42275	280.043	286.629	293.215	RHC
IP7	52.33	338.5003	34	32	3	30	9.32905	18.0893	1.41705	1.35314	329.171	338.216	347.261	LHC
IP8	71.35	409.2815	46	46	34	30	12.9806	24.5018	2.68785	2.46683	396.301	408.552	420.803	RHC
IP9	65.46	473.2821	15	32	52	50	6.82872	13.5735	0.46416	0.45989	466.453	473.24	480.027	RHC
IP10	52.74	525.9381	17	7	55	40	6.0276	11.9652	0.4516	0.44656	519.911	525.893	531.876	RHC
IP11	32.651	558.4991	46	40	38	30	12.9498	24.45	2.67566	2.45656	545.549	557.774	569.999	LHC
IP12	61.702	618.7514	27	58	39	30	7.47671	14.6549	0.91765	0.89042	611.275	618.602	625.93	RHC
IP13	46.622	665.0748	30	46	26	30	8.25951	16.1197	1.11623	1.07618	656.815	664.875	672.935	LHC
IP14	79.11	743.7855	21	26	1	30	5.68001	11.2271	0.53297	0.52367	738.105	743.719	749.333	RHC
IP15	48.201	791.8536	39	17	52	30	10.716	20.5846	1.85645	1.74827	781.138	791.43	801.722	LHC
IP16	146.666	937.672	30	45	21	40	11.0059	21.4803	1.4865	1.43324	926.666	937.406	948.146	RHC
IP17	45.31	982.4505	25	19	31	30	6.74304	13.2656	0.74847	0.73025	975.707	982.34	988.973	RHC
IP18	54.83	1037.06												

CROSS SECTION LEVELLING

Chainan		Distance	•	DC	10	F.C		D.	Dame aulea
Chainage	Left	Centre	Right	BS	IS	FS	HI	RL	Remarks
				0.694			897.694	897	BM
0+000		0			1.193			896.501	СР
			3.5		1.286			896.408	
			5.5		1.491			896.203	
	4				0.952			896.742	
0+020		0			1.42			896.274	СР
			3.5		1.34			896.354	
			7		1.342			896.352	
	4				1.419			896.275	
0+025.285		0			1.371			896.323	BC1
			3.5		1.31			896.384	
			6		1.282			896.412	
	4.5				1.488			896.206	
0+035.265		0			1.1279			896.5661	MC1
	3				1.126			896.568	
	6				1.265			896.429	
			3		1.125			896.569	
0+045.248			3.5		1.27			896.424	EC1
	3.5				0.812			896.882	
	7				0.364			897.33	
		0		1.435		1.05	898.079	896.644	
0+060.319		0			0.78			897.299	BC2
			3.5		0.975			897.104	
			5.5		1.143			896.936	
	5				0.249			897.83	
0+070.809		0			0.845			897.234	MC2
			3.5		1.054			897.025	
			7		1.315			896.764	
	3				0.685			897.394	
	7				0.43			897.649	
0+081.298		0			1.318			896.761	EC2
	3.5				1.196			896.883	
	7				0.955			897.124	
			3.5		1.405			896.674	
0+100	3.5				2.195			895.884	
	7				2.12			895.959	
		0		0.105		2.253	895.931	895.826	СР
0+111.761		0			1.445			894.486	BC3
	3.5				1.265			894.666	
	7				1.085			894.846	
0+126.518		0			2.281			893.65	MC3
	3.5				2.25			893.681	
			3.5		2.215			893.716	43

			7		2.335			893.596	
0+141.449		0			2.445			893.486	EC3/Bridge
0+160		0		3.085		2.385	896.631	893.546	CP/Bridge
0+171.987		0			3.205			893.426	BC4/Bridge
0+182.603		0			2.875			893.756	MC4
			3.5		2.85			893.781	
			7		2.629			894.002	
	3.5				2.716			893.915	
	7				2.837			893.794	
0+193.219		0			1.754			894.877	EC4
			3.5		1.805			894.826	
0+200		0		3.65		0.805	899.476	895.826	СР
			3.5		3.715			895.761	
			7		3.295			896.181	
					3.2			896.276	
0+220	3.5				0.375			899.101	СР
	7				0.371			899.105	
			3.5		1.286			898.19	
		0		3.154		0.48	902.15	898.996	
0+240		0			0.277			901.873	СР
	3.5				0.686			901.464	
	7			3.562		0.645	905.067	901.505	
0+263.182	7				0.442			904.625	BC5
	3.5				1.751			903.316	
		0		1.92		0.244	906.743	904.823	
0+266.730		0			1.59			905.153	MC5
	3.5				1.916			904.827	
	7				1.94			904.803	
0+270.253		0			1.282			905.461	
	3.5				1.452			905.291	
	7				1.531			905.212	
			3.5		1.282			905.461	
0+280.034			3.5		0.06			906.683	BC6
	3.5				0.332			906.411	
	7				0.236			906.507	
		0		2.66		0.35	909.053	906.393	
0+286.611		0			2.0225			907.0305	MC6
	2				1.9125			907.1405	
			3.5		1.72			907.333	
			5.5		1.455			907.598	
		0			1.43			907.623	EC6
0+293.201			3.5		1.16			907.893	
			7		0.72			908.333	
0+300			3.5		0.635			908.418	СР
			7		0.14			908.913	
		0		3.865		0.709	912.209	908.344	
0+320		0			1.8925			910.3165	CP 44

	3.5	1			1.86			910.349	
	3.5		3.5		1.86			910.349	
			3.5 5		2.485			910.789	
0+329.165		0	3		1.047			911.162	BC7
01323.103	3.5	U			1.047			911.134	ВС7
	5.5				0.96			911.134	
	3		3.5		0.685			911.524	
0+338.206	3.5		3.3		0.083			911.769	MC7
01338.200	7				0.44			911.769	IVIC7
		0		2.926	0.173	0.25	914.885	911.959	
0+347.247		0		2.320	1.903	0.23	714.003	912.982	EC7
0.317.217	3.5	0			2.235			912.65	107
	5.5				1.998			912.887	
	5.5		2		1.884			913.001	
0+360	3.5		2		1.206			913.679	СР
0.300	5.5				1.25			913.635	Cr
	3.5		5		1.405			913.48	
		0	3	3.585	1.405	0.691	917.779	914.194	
0+380		0		3.303	3.055	0.031	317.773	914.724	СР
0.300	3.5	U			1.966			915.813	Ci
	3.3		3.5		1.797			915.982	
			5.5		1.184			916.595	
0+396.298			3.5		0.246			917.533	BC8
	3.5		0.0		0.689			917.09	
	0.0	0		2.56	0.000	0.407	919.932	917.372	
0+408.543		0			2.342		0 20 10 0 2	917.59	MC8
			3.5		2.275			917.657	
			7		2.074			917.858	
	3.5				2.448			917.484	
	3.5				1.643			918.289	EC8
	7				1.73			918.202	
			3.5		1.425			918.507	
0+420.789		0		3.5125		1.496	921.9485	918.436	
0+440			3.5		0.8525			921.096	СР
			5		0.9775			920.971	
	3.5				1.927			920.0215	
	5				2.277			919.6715	
		0		3.47		1.614	923.8045	920.3345	
0+466.45			3.5		0.124			923.8045	BC9
			7		0.112			923.6925	
		0		2.715		0.131	926.3885	923.6735	
0+473.233		0			1.351			925.0375	МС9
			3.5		1.335			925.0535	
	3.5				0.254			926.1345	
0+480.017			3.5		1.565			924.8235	EC9
		0		0.858		1.643	925.6035	924.7455	
0+500		0			1.168			924.4355	CP 45

	3.5				0.896			924.7075	
0+519.601	3.3	0			3.055			922.5485	BC10
0 10 10 10 10 10 10 10 10 10 10 10 10 10	3.5				2.618			922.9855	BCIO
	0.0		3		3.055			922.5485	
0+525.886		0		0.874	3.033	3.401	923.0765	922.2025	MC10
			3.5	0.07 1	0.851	51.101	323.07.03	922.2255	111020
			5		0.897			922.1795	
0+531.866		0			0.927			922.1495	EC10
			3.5		1.204			921.8725	
			5		1.11			921.9665	
0+545.548		0			1.392			921.6845	BC11
			3.5		1.45			921.6265	
			5		1.804			921.2725	
0+557.768		0			1.501			921.5755	MC11
ı	3.5				1.444			921.6325	
ı			3.5		1.507			921.5695	
0+569.988			3.5		1.459			921.6175	EC11
			5		1.676			921.4005	
		0		1.649		1.462	923.2635	921.6145	
0+580		0			1.451			921.8125	СР
			3.5		1.414			921.8495	
			5		0.898			922.3655	
0+600		0			1.749			921.5145	СР
			3.5		1.368			921.8955	
	3.5				1.734			921.5295	
0+611.2725		0			2.576			920.6875	BC12
	2				2.391			920.8725	
			2		2.121			921.1425	
0+618.5925		0		0.491		3.126	920.6285	920.1375	MC12
			3.5		0.317			920.3115	
0+625.9125		0			1.042			919.5865	EC12
			3.5		1.012			919.6165	
0+640		0		0.279		4.062	916.8455	916.5665	СР
			3.5		0.043			916.8025	
			7		0.355			916.4905	
0+656.801		0			1.324			915.5215	BC13
	2				1.15			915.6955	
			3.5		1.141			915.7045	
0+664.8615		0			1.954			914.8915	MC13
	3.5				1.707			915.1385	
			3.5		1.833			915.0125	
0+672.922		0			2.43			914.4155	EC13
	3				2.074			914.7715	
			3		2.786			914.0595	
			5		3.344			913.5015	
0+700		0		1.935		2.682	916.0985	914.1635	СР
	3.5				2.069			914.0295	46

	5				1.75			914.3485	
0+720		0			1.67			914.4285	СР
			3.5		1.325			914.7735	
	2				1.339			914.7595	
0+738.777		0			2.09			914.0085	BC14
			2		2.092			914.0065	
0+743.706		0		0.438		2.398	914.1385	913.7005	MC14
			3		0.546			913.5925	
0+749.317		0			0.976			913.1625	EC14
			3.5		0.356			913.7825	
0+760		0			2.0095			912.129	СР
	3				1.592			912.5465	
0+781.13		0			2.397			911.7415	BC15
	3			1.025		3.901	911.2625	910.2375	
0+791.418		0			1.81			909.4525	MC15
	2				1.66			909.6025	
			3		1.662			909.6005	
0+801.706	3				3.075			908.1875	EC15
		0		0.301		3.116	908.4475	908.1465	
			3		0.192			908.2555	
0+820		0			2.251			906.1965	СР
			3		2.252			906.1955	
	1.5				1.972			906.4755	
0+840		0		1.347		4.101	904.3465	904.3465	СР
			3		1.386			902.9605	
	3				1.353			902.9935	
0+860		0			1.612			902.7345	СР
	3				1.55			902.7965	
0+880	3				1.303			903.0435	СР
		0		3.485		1.33	906.5015	903.0165	
0+900		0			1.601			904.9005	СР
	3.5				1.484			905.0175	
0+920	3				1.883			904.6185	СР
		0				1.96		904.5415	

FLY LEVELLING TABLE OF ROAD

S.N	Ва	ck Sight (I	3S)	F	ore Sight ((FS)	Rise	Fall	Reduced Level (RL)	Distan	ice
	Тор	Middle	Bottom	Тор	Middle	Bottom				BS	FS
1	0.972	0.905	0.84						924.737		
2	0.51	0.474	0.439	3.885	3.81	3.73		2.905	921.832	7	7
3	0.555	0.486	0.419	3.206	3.152	3.099		2.678	919.154	7	7
4	0.566	0.484	0.401	2.41	2.335	2.26		1.849	917.305	12	12
5	0.48	0.404	0.326	2.761	2.68	2.6		2.196	915.109	12	12
6	0.24	0.176	0.111	3.205	3.155	3.074		2.751	912.358	12	12
7	0.626	0.576	0.526	2.456	2.41	2.361		2.234	910.124	12	12
8	0.894	0.86	0.896	2.5	2.445	2.392		1.869	908.255	8	8
9	0.44	0.405	0.37	2.136	2.105	2.074		1.245	907.01	6	6
10	0.885	0.849	0.812	2.307	2.272	2.236		1.867	905.143	6	6
11	0.61	0.575	0.54	2.118	2.086	2.056		1.237	903.906	6	6
12	0.491	0.455	0.419	2.441	2.406	2.371		1.831	902.075	6	6
13	0.395	0.36	0.324	2.286	2.54	2.221		2.085	899.99	6	6
14	0.321	0.287	0.254	2.424	2.39	2.355		2.03	897.96	6	6
15	0.471	0.432	0.394	2.804	2.766	2.701		2.479	895.481	6	6
16	1.406	1.285	1.101	2.554	2.51	2.466		2.078	893.403	6	6
17	1.746	1.701	1.655	1.6	1.47	1.4		0.185	893.218	18	18
18	2.501	2.459	2.415	0.9	0.855	0.81	0.846		894.064	6	6
19	2.485	2.375	2.26	0.772	0.724	0.675	1.735		895.799	15	15
20	0.83	0.71	0.6	1.66	1.555	1.45	0.82		896.619	15	15
21	1.526	1.482	1.437	1.536	1.475	1.411		0.765	895.854	15	15
21				0.84	0.76	0.699	0.722		896.576		
	·				ΣFS		Σ Rise		Last RL-		
		ΣBS=			213		=	Σ Fall =	First RL		
		17.74			45.901		4.123	32.284	-28.161		

TOPOGRAPHICAL SURVEY

Traverse Horizontal Angle

Inst.	Sighted		HCR		A1-	Maria	TT:- A1-	
Stn.	to	D	M	S	Angle	Mean	Horiz. Angle	
	A6	0	0	0	132°22'51"			
	A0	179	59	52	132 22 31	132°22'57"		
	A4	132	22	51	132°23'3'	132 2231		
A5	A4	312	22	55	132 23 3		132°22'55.75"	
AS	A6	60	0	0	132°22'49"		132 22 33.13	
	Au	239	59	49	132 2249	132°22'54.5"		
	A4	192	22	58	132°23'0"	132 22 34.3		
	Λ4	372	22	49	132 230			
	A5	0	0	0	147°47'10"			
	AJ	179	59	51	147 47 10	147°47'7.5"		
	A3	147	47	10	147°47'5"	147 47 7.3		
A4	AS	327	46	56	147 47 3		147°47'6.75"	
Λ4	A5	60	0	0	147°47'3"		147 47 0.73	
	AJ	239	59	54	147 47 3	147°47'6"		
	A3	207	47	3	147°47'9"	147 470		
	AS	387	47	3	14/ 4/ /			
	A4	0	0	0	132°0'33"			
	Λ+	180	0	4	132 033	132°0'36"		
	A2	132	0	33	132°0'39"	132 030		
A3	112	312	0	43	132 037		132°0'45.25"	
113	A4	60	0	0	132°0'48"		132 043.23	
	7 1 1	239	59	49	132 0 40	132°0'54.5"		
	A2	192	0	48	132°1'1"	132 034.3		
	112	372	0	50	132 11			
	A3	0	0	0	115°33'12"			
	713	180	0	4	113 33 12	115°33'12"		
	A1	115	33	12	115°33'12"	113 33 12		
A2	711	295	33	16	113 33 12		115°33'17.25"	
112	A3	60	0	0	115°33'42"		110 00 17.20	
	713	240	0	2	113 33 12	115°33'22.5"		
	A1	175	33	42	115°33'03"	113 33 22.3		
	711	355	33	5	119 99 09			
	A2	0	0	0	110°5'45"			
	712	179	59	55	110 3 13	110°5'46"		
	A7	110	5	45	110°5'47"			
A1	11/	290	5	42	110 5 17		110°5'50"	
***	A2	60	0	0	110°5'54"		110 550	
		239	59	58	3	110°5'54"		
	A7	170	5	54	110°5'54"	110 55 1		
	11/	350	5	52	110 00 1			

	A 1	0	0	0	140°28'56"		
	A1	179	59	59	140 28 30	140°28'54.5"	
	A6	140	28	56	140°28'53"	140 26 34.3	
A7	Au	320	28	52	140 28 33		140°28'54.5"
A	A1	60	0	0	140°28'59"		140 26 34.3
	Al	240	0	9	140 20 39	140°28'54.5"	
	A6	200	28	59	140°28'50"	140 26 34.3	
	Au	380	28	59	140 28 30		
	A7	0	0	0	121°38'36"		
	A/	179	59	58	121 36 30	121°38'35"	
	A5	121	38	36	121°38'34"	121 3633	
A6	AS	301	38	32	121 36 34		121°38'34"
Au	A7	60	0	0	121°38'34"		121 36 34
	A/	239	59	56	121 38 34	121°38'33"	
	A5	181	38	34	10102012111	121 3033	
		361	38	27	121°38'31"		

Major Traverse Table

Gales Table

Line	Length	Point	<u> </u>	H. Angle	eļje	E Ξ	Corrected H.Angle	rted zle		WCB	m	Consecutive	Consecutive Co-ordinate
			D	M	S	D	Z	S	D	M	N	Latitude	Longitude
A5A6	91.5265	A5	121	38	34	121	38	56.36	42	32	50.36	67.42932035	61.89012004
A4A5	105.93495	A4	132	22	55.75	132	23	18.11	354	56	8.47	105.5214053	-9.351291745
A3A4	91.0299	A3	147	47	6.75	147	47	29.11	322	43	37.58	72.43795992	-55.12880061
A2A3	120.5336	A2	132	0	45.25	132	1	7.61	274	44	45.19	9.972546637	-120.120344
A1A2	156.52	A1	115	33	17.25	115	33	39.61	210	18	24.8	-135.1291759	-78.98491134
A7A1	125.5546	A7	110	κ	50	110	9	12.36	140	24	37.16	-96.75589864	80.01408413
A6A7	123.97535	A6	140	28	54.5	140	29	16.86	100	53	54	-23.43963248	121.739357
SUMMATION	815.0749		768	173	263.5							0.036525172	0.058213451

Corrected Consecutive Coordinate	Independent Coordinate	Coordinate
Latitude Longitude	Northing	Easting
67.42521886 61.88358313	3128940.92	792226.248
105.5166581 -9.358857724	3129046.437	792216.8891
72.43388068 -55.13530206	3129118.871	792161.7538
9.96714528 -120.1289526	3129128.838	792041.6249
-135.1361899 -78.99609016	3128993.701	791962.6288
96.761525 80.0051169	3128896.94	792042.6339
-23.44518807 121.7305025	3128873.495	792164.3644
-3.817E-10 -1.42322E-10		
10	-1.42322E-10	-1.42322E-1U

TRAVERSE DISTANCE TABLE

Line	Forward Distance	Backward Distance	Mean M	Discrepency D	Precision
1-2	156.313	156.326	156.3195	0.013	0.0000831
2-3	121.295	121.311	121.303	0.016	0.0001319
3-4	90.775	90.742	90.7585	0.033	0.0003636
4-5	105.334	105.356	105.345	0.022	0.00020884
5-6	90.936	90.919	90.9275	0.017	0.00018696
6-7	124.662	124.696	124.679	0.034	0.0002727
0-7	124.002	124.090	124.679	0.034	0.0002727
7-1	125.148	125.189	125.1685	0.041	0.00032756

DIFFERENTIAL LEVELLING OF COLLEGE TRAVERSE

		Back Sigh	nt		Fore Sigh	nt				Dist	ance	
S.N	Тор	Middle	Bottom	Тор	Middle	Bottom	Rise	Fall	RL	BS	FS	Remarks
BM	1.095	1.073	1.052						957.55	5		BM
1	1.424	1.374	1.325	1.196	1.171	1.145		0.098	957.452	10	5	
2	1.595	1.545	1.496	1.093	1.043	0.993	0.331		957.783	10	10	
3	1.548	1.498	1.449	1.215	1.166	1.117	0.379		958.162	10	10	
4	1.783	1.759	1.734	1.102	1.052	1.004	0.446		958.608	5	10	
5	1.81	1.785	1.76	1.088	1.063	1.037	0.6965		959.305	5	5	
6	1.756	1.732	1.708	1.124	1.099	1.074	0.686		959.991	5	5	
7	2.425	2.375	2.325	1.67	1.043	1.018	0.689		960.68	10	5	
8	1.612	1.545	1.481	0.212	0.162	0.112	2.213		962.893	12.9	10	
9	1.436	1.387	1.339	1.034	0.97	0.905	0.5755		963.468	10	12.9	A7
10	1.257	1.208	1.157	1.846	1.799	1.748		0.4125	963.056	10	10	
11	1.128	1.076	1.025	1.444	1.394	1.344		0.186	962.87	10	10	
12	1.457	1.408	1.36	1.626	1.578	1.529		0.502	962.368	10	10	
13	1.467	1.423	1.378	2.03	1.98	1.93		0.572	961.796	10	10	
14	1.309	1.245	1.181	1.51	1.461	1.412		0.038	961.758	12.75	10	
15	1.315	1.265	1.215	1.201	1.141	1.081	0.104		961.862	10	12.75	A6
16	1.607	1.558	1.509	1.215	1.166	1.118	0.099		961.961	10	10	
17	1.485	1.435	1.385	1.203	1.153	1.103	0.405		962.366	10	10	
18	1.5	1.45	1.4	1.268	1.218	1.168	0.217		962.583	10	10	
19	1.434	1.404	1.374	1.243	1.188	1.132	0.262		962.845	5.1	11.13	
20	1.315	1.265	1.215	1.127	1.102	1.076	0.302		963.147	10	5.1	A5
21	1.527	1.477	1.427	1.187	1.138	1.09	0.127		963.274	10	10	
22	1.533	1.483	1.433	1.17	1.12	1.071	0.357		963.631	10	10	
23	1.55	1.5	1.45	1.2	1.5	1.1		0.017	963.614	10	10	
24	1.571	1.511	1.451	1.086	1.036	0.986	0.464		964.078	13.13	10	
25	1.192	1.142	1.092	0.65	0.58	0.51	0.931		965.009	10	13.13	A4
26	1.571	1.522	1.474	1.12	1.061	1.011	0.081		965.09	10	10	
27	1.514	1.464	1.414	1.122	1.072	1.022	0.45		965.54	10	10	
28	1.513	1.463	1.412	1.18	1.13	1.08	0.334		965.874	10	10	
29	1.135	1.108	1.079	0.902	0.853	0.804	0.61		966.484	6.3	10	
30	1.474	1.424	1.374	1.146	1.116	1.086		0.008	966.476	10	6.3	A3
31	1.108	1.106	1.007	1.109	1.058	1.008	0.366		966.842	10	10	
32	1.731	1.681	1.63	1.196	1.147	1.098		0.0409	966.801	10	10	
33	1.465	1.415	1.366	0.966	0.917	0.869	0.7635		967.564	10	10	
34	1.474	1.425	1.375	1.065	1.019	0.969	0.3965		967.961	10	10	
35	1.596	1.545	1.495	1.224	1.175	1.125	0.25		968.211	10.25	10	
36	1.442	1.392	1.343	1.223	1.172	1.12	0.373		968.584	10	10.25	A2
37	1.561	1.512	1.462	1.414	1.364	1.314	0.028		968.612	10	10	
38	1.611	1.562	1.512	1.412	1.372	1.323	0.14		968.752	10	10	
39	1.524	1.476	1.424	1.503	1.453	1.404	0.109		968.861	10	10	
40	1.555	1.505	1.456	1.486	1.436	1.386	0.04		968.901	10	10	
41	1.599	1.549	1.499	1.544	1.494	1.444	0.011		968.912	10	10	

42	1.603	1.553	1.504	1.656	1.607	1.559	0.058	968.854	10	10	
43	1.408	1.372	1.334	1.686	1.637	1.588	0.084	968.77	8.5	10	
44				1.66	1.621	1.574	0.249	968.521		8.5	A1

FLY LEVELLING OF COLLEGE TRAVERSE

C NI		Back Sigh	t		Fore Sigh	nt	Rise	Fall	RL	Dist	ance	Remarks
S.N	Тор	Middle	Bottom	Тор	Middle	Bottom				BS	FS	
B.M	1.69	1.64	1.598						968.521			A1
1	1.545	1.44	1.33	1.358	1.304	1.248	0.336		968.857			
2	1.385	1.28	1.175	1.48	1.37	1.26	0.07		968.927			
3	1.272	1.144	1.014	1.463	1.36	1.258		0.08	968.847			
4	1.056	0.946	0.836	1.512	1.389	1.266		0.245	968.602			A2
5	0.745	0.64	0.534	1.704	1.591	1.478		0.645	967.957			
6	1.401	1.323	1.243	1.96	1.852	1.744		1.212	966.745			
7	1.144	1.065	0.986	1.636	1.554	1.471		0.231	966.514			A3
8	1.132	1.015	0.9	1.85	1.805	1.715		0.74	965.774			
9	0.695	0.615	0.535	2.019	1.841	1.665		0.826	964.948			A4
10	1.067	0.992	0.918	1.483	1.415	1.347		0.8	964.148			
11	1.116	1.054	0.989	1.532	1.483	1.424		0.491	963.657			
12	1.278	1.214	1.149	1.626	1.557	1.486		0.503	963.154			
13	1.046	1.961	0.875	1.341	1.29	1.238		0.076	963.078			A5
14	1.185	1.136	0.988	1.746	1.684	1.627	0.2765		963.354			
15	1.008	0.939	0.871	1.881	1.794	1.708		0.658	962.696			
16	1.23	1.158	1.088	1.71	1.699	1.685		0.76	961.936			A6
17	1.183	1.734	1.635	1.333	1.258	1.185		0.1	961.836			
18	1.906	1.802	1.697	1.215	1.141	1.065	0.593		962.429			
19	1.073	1.028	0.983	0.85	0.736	0.624	1.066		963.495			
20	1.865	1.809	1.751	1.034	0.973	0.91	0.0555		963.551			A7
21	0.357	0.326	0.295	2.885	2.805	2.725		0.996	962.555			
22	0.978	0.939	0.9	2.277	2.227	2.177		1.901	960.654			
23	1.019	0.981	0.945	2.038	2.01	1.964		1.071	959.583			
24	1.278	1.19	1.1	2.272	2.218	2.163		1.237	958.346			
25	1.359	1.313	1.267	1.928	1.819	1.707		0.629	957.717			
26				1.635	1.541	1.445		0.2285	957.488			BM

TOTAL STATION DATA TABLE

IOIALSI	ATION DATE	A TABLE		
Point	N	E	Elevation	Feature
BS	3128994	791962.7	968.803	BS1
1001	3128892	792043.3	962.442	SH
1002	3128895	792045.1	963.423	SH
1003	3128900	792047.8	963.604	SH
1004	3128904	792048.9	963.645	SH
1005	3128912	792026.4	964.54	SH
1006	3128911	792049.3	964.065	SH
1007	3128915	792032.5	964.07	SH
1008	3128893	792047.2	963.44	SH
1009	3128887	792052.4	962.878	SH
1010	3128886	792048.9	962.505	SH
1011	3128883	792052.1	962.474	SH
1012	3128887	792046.4	961.638	SH
1013	3128882	792051.5	961.707	SH
1014	3128885	792047.2	961.302	SH
1015	3128880	792051.1	961.184	SH
1016	3128893	792051.2	963.409	SH
1017	3128887	792057.9	963.084	SH
1018	3128896	792052.1	963.465	SH
1019	3128894	792059.6	963.393	SH
1020	3128900	792052.7	963.498	SH
1021	3128899	792068.1	963.123	SH
1022	3128902	792036.3	963.789	SH
1023	3128904	792075.2	962.904	SH
1024	3128903	792037.4	963.906	SH
1025	3128907	792083.3	962.925	SH
1026	3128904	792091.8	962.415	SH
1027	3128902	792099.4	962.507	SH
1028	3128895	792100.7	962.355	SH
1029	3128906	792038.5	963.86	SH
1030	3128910	792035.2	964.073	SH
1031	3128917	792031.6	964.142	SH
1032	3128955	792014.9	965.846	SH
1033	3128957	792018.4	967.091	SH
1034	3128956	792022.8	966.525	SH
1035	3128956	792026.1	966.677	SH
1036	3128938	792031.1	964.466	SH
1037	3128941	792032.6	964.874	SH
1038	3128952	792028.2	966.673	SH
1039	3128953	792023.6	965.568	SH
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1040 3128945 792019.5 965.473 SH 1041 3128945 792022.1 964.674 SH 1042 3128954 792014.5 965.487 SH 1043 3128959 792017.9 964.615 SH 1044 3128959 792001.2 967.754 SH 1045 3128947 792009.9 964.618 SH 1046 3128956 79196.6 966.869 SH 1047 3128948 792005.2 964.622 SH 1048 3128953 791993.1 966.319 SH 1049 3128945 792000.7 964.79 SH 1050 3128953 791993.1 966.327 SH 1051 3128953 791993.1 966.327 SH 1051 3128953 791993.1 966.327 SH 1052 3128958 791991.2 966.71 SH 1053 3128960 791993.1 967.652 SH 1054 3128970 791983.8 967.968 BC 1055 3128970 792005.6 968.183 BC 1056 3128972 792007 968.183 BC 1057 3128970 79205.6 968.148 BC 1059 3128958 791987 965.59 TRE 1060 3128958 791987 965.59 TRE 1061 3128946 791982.4 965.294 TRE 1061 3128946 791995.3 964.793 TRE 1061 3128940 791995.3 964.793 TRE 1062 3128927 792027.4 964.463 TRE 1063 3128926 792029.3 964.246 TRE 1064 3128926 792029.3 964.246 TRE 1065 3128927 792015.2 964.796 CHAU 1067 312893 792015.2 964.96 CHAU 1067 312893 792015.2 964.96 CHAU 1067 312893 792015.2 964.93 CHAU 1067 312893 792011.3 964.904 CHAU 1069 3128931 792017.5 962.898 TRE 1071 3128893 792007.7 963.11 TRE 1072 3128804 792098.5 964.904 CHAU 1069 3128854 792097.7 963.11 TRE 1072 3128804 792097.7 963.11 TRE 1073 3128884 792072.7 962.931 POL 1076 3128856 792038.4 963.898 PATH 1079 3128862 792038.4 963.898 PATH 1079 3128923 792019.5 964.83 PATH 1080 3128937 792009.5 964.83 PATH 1081 3128937 792009.5 964.83 PATH 1081 3128937 792009.5 964.83 PATH 1081					
1042 3128954 792014.5 965.487 SH 1043 3128945 792017.9 964.615 SH 1044 3128959 792001.2 967.754 SH 1045 3128947 792009.9 964.618 SH 1046 3128956 791996.6 966.869 SH 1047 3128948 792005.2 964.622 SH 1048 3128953 791993.1 966.319 SH 1049 3128945 792000.7 964.79 SH 1050 3128949 791988.6 965.27 SH 1051 3128958 791993.1 966.327 SH 1052 3128958 791993.1 966.327 SH 1053 3128958 791993.1 966.327 SH 1053 3128960 791933.1 967.652 SH 1054 3128970 791983.8 967.968 BC 1055 3128970 792005.6 968.183 BC 1056 3128972 792007 968.183 BC 1057 3128970 791987 965.95 TRE 1060 3128958 791987 965.995 TRE 1060 3128958 791987 965.599 TRE 1060 3128935 792019.8 964.793 TRE 1061 3128946 791982.4 965.294 TRE 1062 3128922 792027.4 964.463 TRE 1064 3128940 791985.3 964.793 TRE 1064 3128940 791985.3 964.794 TRE 1066 3128925 792015.2 964.796 CHAU 1066 3128925 792015.2 964.796 CHAU 1066 3128925 792013.2 964.93 CHAU 1069 3128931 792011.3 964.904 CHAU 1069 3128931 792011.3 964.904 CHAU 1069 3128931 792011.3 964.904 CHAU 1069 3128931 792015.2 964.797 CHAU 1069 3128931 792015.2 964.796 CHAU 1069 3128931 792015.2 964.796 CHAU 1069 3128931 792015.2 964.797 CHAU 1069 3128931 792015.2 964.796 CHAU 1069 3128931 792015.2 964.93 CHAU 1069 3128931 792015.2 964.93 CHAU 1069 3128931 792017.5 962.898 TRE 1070 3128884 79207.7 963.11 TRE 1071 3128893 79207.7 963.11 TRE 1072 3128800 792064.6 963.703 TRE 1073 3128882 79207.7 962.931 POL 1076 3128880 79208.5 962.223 POL 1076 3128862 79208.5 962.223 POL 1076 3128862 79208.5 962.224 POL 1077 3128862 79208.5 962.224 POL 1078 3128905 79203.1 964.407 PATH 10	1040	3128953	792019.5	965.473	SH
1043 3128945 792017.9 964.615 SH 1044 3128959 792001.2 967.754 SH 1045 3128947 792009.9 964.618 SH 1046 3128956 791996.6 966.869 SH 1047 3128948 792005.2 964.622 SH 1048 3128953 791993.1 966.319 SH 1049 3128945 792000.7 964.79 SH 1050 3128949 791988.6 965.27 SH 1051 3128953 791993.1 966.327 SH 1052 3128958 791991.2 966.71 SH 1052 3128958 791991.2 966.71 SH 1053 3128960 791983.8 967.652 SH 1054 3128970 791983.8 967.968 BC 1055 3128977 792011.3 968.233 BC 1057 3128970 792005.6 968.148 BC 1057 3128970 792005.6 968.148 BC 1058 3128970 792005.6 968.148 BC 1058 3128959 791987 965.995 TRE 1059 3128958 791984.1 965.59 TRE 1060 3128935 792019.8 964.793 TRE 1062 3128922 792027.4 964.463 TRE 1063 3128946 791982.4 965.294 TRE 1064 3128926 792029.3 964.246 TRE 1065 3128927 792015.2 964.796 CHAU 1066 3128925 792015.2 964.796 CHAU 1067 3128929 792007.8 964.797 CHAU 1068 3128935 792011.3 964.904 CHAU 1069 3128935 792007.8 964.797 CHAU 1069 3128935 792007.8 964.796 CHAU 1073 3128880 792070.7 963.11 TRE 1074 3128884 792071.5 962.898 TRE 1074 3128880 792070.7 963.11 TRE 1073 3128880 792070.7 963.11 TRE 1074 3128880 792071.5 962.898 TRE 1074 3128880 792065.3 962.223 POL 1075 3128880 792039.9 961.005 POL 1076 3128820 792038.4 963.898 PATH 1079 3128820 79203.1 964.707 PATH 1080 3128929 792023.1 964.	1041	3128945	792022.1	964.674	SH
1044 3128959 792001.2 967.754 SH 1045 3128947 792009.9 964.618 SH 1046 3128956 791996.6 966.869 SH 1047 3128948 792005.2 964.622 SH 1048 3128953 791993.1 966.319 SH 1049 3128945 792000.7 964.79 SH 1050 3128949 791988.6 965.27 SH 1051 3128953 791993.1 966.327 SH 1052 3128958 791993.1 966.327 SH 1053 3128960 791993.1 967.652 SH 1054 3128970 791983.8 967.968 BC 1055 3128970 791983.8 967.968 BC 1056 3128972 792007 968.183 BC 1057 3128970 79205.6 968.148 BC 1058 3128959 791987 965.995 TRE 1059 3128958 791984.1 965.59 TRE 1060 3128935 792019.8 964.793 TRE 1061 3128946 791982.4 965.294 TRE 1063 3128922 792027.4 964.463 TRE 1064 3128920 791995.3 965.294 TRE 1065 3128927 792015.2 964.796 CHAU 1066 3128927 792015.2 964.796 CHAU 1067 3128929 792093 964.246 TRE 1068 3128921 792013.2 964.93 CHAU 1069 3128935 792013.2 964.93 CHAU 1069 3128935 792013.2 964.797 CHAU 1068 3128931 792011.3 964.904 CHAU 1069 3128935 792007.8 964.797 CHAU 1069 3128935 792007.8 964.794 CHAU 1069 3128935 792007.9 963.11 TRE 1071 3128890 792007.9 963.11 TRE 1072 3128900 792064.6 963.703 TRE 1073 3128880 79207.7 962.931 POL 1075 3128880 79207.7 962.931 POL 1076 3128880 79207.7 962.931 POL 1077 312880 79208.8 962.223 POL 1078 3128905 79208.4 963.898 PATH 1080 3128929 792023.1 964.707 PATH	1042	3128954	792014.5	965.487	SH
1045 3128947 792009.9 964.618 SH 1046 3128956 791996.6 966.869 SH 1047 3128948 792005.2 964.622 SH 1048 3128953 791993.1 966.319 SH 1049 3128945 792000.7 964.79 SH 1050 3128949 791988.6 965.27 SH 1051 3128953 791993.1 966.327 SH 1052 3128958 791991.2 966.71 SH 1053 3128960 791993.1 967.652 SH 1054 3128970 791983.8 967.968 BC 1055 3128977 792011.3 968.233 BC 1056 3128972 792007 968.183 BC 1057 3128970 792005.6 968.148 BC 1058 3128958 791984.1 965.59 TRE 1060 3128935 792019.8 964.793 TRE 1061 3128946 791982.4 965.294 TRE 1062 3128922 792027.4 964.463 TRE 1063 3128940 791995.3 965.29 TRE 1064 3128926 792015.2 964.796 CHAU 1066 3128927 792015.2 964.796 CHAU 1067 3128927 792013.2 964.93 CHAU 1068 3128951 792013.2 964.93 CHAU 1069 3128951 792013.2 964.93 CHAU 1069 3128951 792013.2 964.93 CHAU 1069 3128951 792007.8 964.796 CHAU 1070 3128893 792070.7 963.11 TRE 1071 3128893 792070.7 963.11 TRE 1072 3128804 792065.3 962.293 POL 1075 3128884 792072.7 962.931 POL 1076 3128884 792072.7 962.931 POL 1077 3128862 79208.4 963.898 PATH 1079 3128923 79209.2 964.430 PATH 1080 3128929 79203.1 964.707 PATH 1080 3128929 79203.1 964.707 PATH	1043	3128945	792017.9	964.615	SH
1046 3128956 791996.6 966.869 SH 1047 3128948 792005.2 964.622 SH 1048 3128953 791993.1 966.319 SH 1049 3128945 792000.7 964.79 SH 1050 3128949 791988.6 965.27 SH 1051 3128953 791993.1 966.327 SH 1052 3128958 791991.2 966.71 SH 1053 3128960 791993.1 967.652 SH 1054 3128970 791983.8 967.968 BC 1055 3128977 792011.3 968.233 BC 1056 3128972 792007 968.183 BC 1057 3128970 791987 965.995 TRE 1058 3128959 791987 965.995 TRE 1059 3128958 791984.1 965.59 TRE 1060 3128946 791982.4 965.594 TRE 1061 3128946 791982.4 965.294 TRE 1062 3128920 792007.4 964.463 TRE 1064 3128940 791995.3 964.246 TRE 1064 3128926 792027.4 964.463 TRE 1064 3128926 792027.3 964.246 TRE 1065 3128927 792015.2 964.796 CHAU 1066 3128925 792013.2 964.904 CHAU 1067 3128929 792007.8 964.797 CHAU 1068 3128925 792013.2 964.797 CHAU 1068 3128925 792013.2 964.797 CHAU 1069 3128935 792007.8 964.797 CHAU 1069 3128935 792007.8 964.797 CHAU 1069 3128935 792007.8 964.794 TRE 1071 3128893 792007.7 963.11 TRE 1072 3128900 792064.6 963.703 TRE 1073 3128882 792071.5 962.898 TRE 1074 3128893 792007.7 963.11 TRE 1072 3128900 792064.6 963.703 TRE 1074 3128884 792072.7 962.931 POL 1075 3128880 792065.3 962.223 POL 1078 3128905 792033.4 963.898 PATH 1079 3128923 792019.2 964.433 PATH 1079 3128923 792019.2 964.433 PATH 1079 3128929 792023.1 964.707 PATH 1080 3128929 792023.1 964.433 PATH 1080 3128929 792023.1 964.707 PATH 1080 3128929 792023.1	1044	3128959	792001.2	967.754	SH
1047 3128948 792005.2 964.622 SH 1048 3128953 791993.1 966.319 SH 1049 3128945 792000.7 964.79 SH 1050 3128949 791988.6 965.27 SH 1051 3128953 791993.1 966.327 SH 1052 3128958 791991.2 966.71 SH 1053 3128960 791993.1 967.652 SH 1054 3128970 791983.8 967.968 BC 1055 3128970 792007 968.183 BC 1056 3128970 792005.6 968.148 BC 1057 3128970 792005.6 968.148 BC 1058 3128959 791987 965.995 TRE 1059 3128958 791987 965.995 TRE 1060 3128935 792019.8 964.793 TRE 1061 3128946 791982.4 965.59 TRE <	1045	3128947	792009.9	964.618	SH
1048 3128953 791993.1 966.319 SH 1049 3128945 792000.7 964.79 SH 1050 3128949 791988.6 965.27 SH 1051 3128953 791993.1 966.327 SH 1052 3128960 791991.2 966.71 SH 1053 3128960 791993.1 967.652 SH 1054 3128970 791983.8 967.968 BC 1055 3128970 792007 968.183 BC 1056 3128972 792007 968.183 BC 1057 3128970 792005.6 968.148 BC 1058 3128959 791987 965.995 TRE 1059 3128958 791984.1 965.995 TRE 1060 3128935 792019.8 964.793 TRE 1061 3128940 791982.4 965.294 TRE 1062 3128940 791995.3 965.29 TRE	1046	3128956	791996.6	966.869	SH
1049 3128945 792000.7 964.79 SH 1050 3128949 791988.6 965.27 SH 1051 3128953 791993.1 966.327 SH 1052 3128958 791991.2 966.71 SH 1053 3128960 791993.1 967.652 SH 1054 3128970 791983.8 967.968 BC 1055 3128977 792011.3 968.233 BC 1056 3128972 792007 968.183 BC 1057 3128970 792005.6 968.148 BC 1058 3128959 791987 965.995 TRE 1059 3128958 791984.1 965.59 TRE 1060 3128946 791982.4 965.294 TRE 1061 3128940 791995.3 965.29 TRE 1062 3128922 792027.4 964.463 TRE 1063 3128940 791995.3 965.29 TRE	1047	3128948	792005.2	964.622	SH
1050 3128949 791988.6 965.27 SH 1051 3128953 791993.1 966.327 SH 1052 3128958 791991.2 966.71 SH 1053 3128960 791993.1 967.652 SH 1054 3128970 791983.8 967.968 BC 1055 3128977 792011.3 968.233 BC 1056 3128972 792007 968.183 BC 1057 3128970 792005.6 968.183 BC 1058 3128959 791987 965.995 TRE 1059 3128958 791984.1 965.59 TRE 1060 3128935 792019.8 964.793 TRE 1061 3128946 791982.4 965.294 TRE 1062 3128922 792027.4 964.463 TRE 1063 3128940 791995.3 965.29 TRE 1064 3128927 792015.2 964.796 CHAU	1048	3128953	791993.1	966.319	SH
1051 3128953 791993.1 966.327 SH 1052 3128958 791991.2 966.71 SH 1053 3128960 791993.1 967.652 SH 1054 3128970 791983.8 967.968 BC 1055 3128977 792011.3 968.233 BC 1056 3128972 792007 968.183 BC 1057 3128970 792005.6 968.183 BC 1058 3128959 791987 965.995 TRE 1059 3128958 791984.1 965.99 TRE 1060 3128946 791982.4 965.294 TRE 1061 3128946 791982.4 965.294 TRE 1062 3128922 792027.4 964.463 TRE 1063 3128940 791995.3 965.29 TRE 1064 3128926 792029.3 964.796 CHAU 1065 3128927 792015.2 964.796 CHAU </td <td>1049</td> <td>3128945</td> <td>792000.7</td> <td>964.79</td> <td>SH</td>	1049	3128945	792000.7	964.79	SH
1052 3128958 791991.2 966.71 SH 1053 3128960 791993.1 967.652 SH 1054 3128970 791983.8 967.968 BC 1055 3128977 792011.3 968.233 BC 1056 3128972 792007 968.183 BC 1057 3128970 792005.6 968.148 BC 1058 3128958 791987 965.995 TRE 1059 3128958 791984.1 965.59 TRE 1060 3128935 792019.8 964.793 TRE 1061 3128946 791982.4 965.294 TRE 1062 3128922 792027.4 964.463 TRE 1063 3128946 791982.4 965.29 TRE 1063 3128922 792027.4 964.463 TRE 1063 3128920 792015.2 964.796 CHAU 1065 3128927 792015.2 964.796 CHAU<	1050	3128949	791988.6	965.27	SH
1053 3128960 791993.1 967.652 SH 1054 3128970 791983.8 967.968 BC 1055 3128977 792011.3 968.233 BC 1056 3128972 792007 968.183 BC 1057 3128970 792005.6 968.148 BC 1058 3128959 791987 965.995 TRE 1059 3128958 791984.1 965.59 TRE 1060 3128935 792019.8 964.793 TRE 1061 3128946 791982.4 965.294 TRE 1062 3128922 792027.4 964.463 TRE 1063 3128940 791995.3 965.29 TRE 1064 3128926 792029.3 964.246 TRE 1065 3128927 792015.2 964.796 CHAU 1066 3128925 792013.2 964.94 CHAU 1067 3128929 792007.8 964.797 CHA	1051	3128953	791993.1	966.327	SH
1054 3128970 791983.8 967.968 BC 1055 3128977 792011.3 968.233 BC 1056 3128972 792007 968.183 BC 1057 3128970 792005.6 968.148 BC 1058 3128959 791987 965.995 TRE 1059 3128958 791984.1 965.59 TRE 1060 3128935 792019.8 964.793 TRE 1061 3128946 791982.4 965.294 TRE 1062 3128922 792027.4 964.463 TRE 1063 3128940 791995.3 965.29 TRE 1064 3128926 792029.3 964.26 TRE 1065 3128927 792015.2 964.796 CHAU 1066 3128925 792013.2 964.93 CHAU 1067 3128929 792009.3 964.797 CHAU 1068 3128951 792007.3 964.704 TR	1052	3128958	791991.2	966.71	SH
1055 3128977 792011.3 968.233 BC 1056 3128972 792007 968.183 BC 1057 3128970 792005.6 968.148 BC 1058 3128959 791987 965.995 TRE 1059 3128958 791984.1 965.59 TRE 1060 3128935 792019.8 964.793 TRE 1061 3128946 791982.4 965.294 TRE 1062 3128922 792027.4 964.463 TRE 1063 3128940 791995.3 965.29 TRE 1064 3128926 792029.3 964.246 TRE 1065 3128927 792015.2 964.796 CHAU 1066 3128925 792013.2 964.93 CHAU 1067 3128929 792009.3 964.797 CHAU 1068 3128931 792011.3 964.904 CHAU 1069 3128935 792007.8 964.704 <td< td=""><td>1053</td><td>3128960</td><td>791993.1</td><td>967.652</td><td>SH</td></td<>	1053	3128960	791993.1	967.652	SH
1056 3128972 792007 968.183 BC 1057 3128970 792005.6 968.148 BC 1058 3128959 791987 965.995 TRE 1059 3128958 791984.1 965.59 TRE 1060 3128935 792019.8 964.793 TRE 1061 3128946 791982.4 965.294 TRE 1062 3128922 792027.4 964.463 TRE 1063 3128940 791995.3 965.29 TRE 1064 3128926 792029.3 964.246 TRE 1065 3128927 792015.2 964.796 CHAU 1066 3128925 792013.2 964.93 CHAU 1067 3128929 792009.3 964.797 CHAU 1068 3128931 792011.3 964.904 CHAU 1069 3128935 792007.8 964.784 TRE 1070 3128893 79207.7 963.11	1054	3128970	791983.8	967.968	BC
1057 3128970 792005.6 968.148 BC 1058 3128959 791987 965.995 TRE 1059 3128958 791984.1 965.59 TRE 1060 3128935 792019.8 964.793 TRE 1061 3128946 791982.4 965.294 TRE 1062 3128922 792027.4 964.463 TRE 1063 3128940 791995.3 965.29 TRE 1064 3128926 792029.3 964.246 TRE 1065 3128927 792015.2 964.796 CHAU 1066 3128927 792013.2 964.93 CHAU 1067 3128929 792009.3 964.797 CHAU 1068 3128931 792011.3 964.904 CHAU 1069 3128931 792007.8 964.704 TRE 1070 3128893 79207.7 963.11 TRE 1072 3128900 792064.6 963.703 <	1055	3128977	792011.3	968.233	BC
1058 3128959 791987 965.995 TRE 1059 3128958 791984.1 965.59 TRE 1060 3128935 792019.8 964.793 TRE 1061 3128946 791982.4 965.294 TRE 1062 3128922 792027.4 964.463 TRE 1063 3128940 791995.3 965.29 TRE 1064 3128926 792029.3 964.246 TRE 1065 3128927 792015.2 964.796 CHAU 1066 3128927 792015.2 964.796 CHAU 1066 3128925 792013.2 964.796 CHAU 1067 3128929 792009.3 964.797 CHAU 1068 3128931 792011.3 964.904 CHAU 1069 3128951 792007.8 964.784 TRE 1070 3128893 792070.7 963.11 TRE 1071 3128893 792070.7 963.703	1056	3128972	792007	968.183	BC
1059 3128958 791984.1 965.59 TRE 1060 3128935 792019.8 964.793 TRE 1061 3128946 791982.4 965.294 TRE 1062 3128922 792027.4 964.463 TRE 1063 3128940 791995.3 965.29 TRE 1064 3128926 792029.3 964.246 TRE 1065 3128927 792015.2 964.796 CHAU 1066 3128925 792013.2 964.93 CHAU 1067 3128929 792009.3 964.797 CHAU 1068 3128931 792011.3 964.904 CHAU 1069 3128951 792007.8 964.784 TRE 1070 3128893 792070.7 963.11 TRE 1071 3128893 792070.7 963.11 TRE 1072 3128800 792064.6 963.703 TRE 1073 3128884 792071.5 962.898	1057	3128970	792005.6	968.148	BC
1060 3128935 792019.8 964.793 TRE 1061 3128946 791982.4 965.294 TRE 1062 3128922 792027.4 964.463 TRE 1063 3128940 791995.3 965.29 TRE 1064 3128926 792029.3 964.246 TRE 1065 3128927 792015.2 964.796 CHAU 1066 3128925 792013.2 964.93 CHAU 1067 3128929 792009.3 964.797 CHAU 1068 3128931 792011.3 964.904 CHAU 1069 3128951 792007.8 964.784 TRE 1070 3128935 792020.4 964.704 TRE 1071 3128893 792070.7 963.11 TRE 1072 3128900 792064.6 963.703 TRE 1073 3128884 792071.5 962.898 TRE 1074 3128880 792039.9 961.005	1058	3128959	791987	965.995	TRE
1061 3128946 791982.4 965.294 TRE 1062 3128922 792027.4 964.463 TRE 1063 3128940 791995.3 965.29 TRE 1064 3128926 792029.3 964.246 TRE 1065 3128927 792015.2 964.796 CHAU 1066 3128925 792013.2 964.93 CHAU 1067 3128929 792009.3 964.797 CHAU 1068 3128931 792011.3 964.904 CHAU 1069 3128951 792007.8 964.784 TRE 1070 3128935 792020.4 964.704 TRE 1071 3128893 792070.7 963.11 TRE 1072 3128900 792064.6 963.703 TRE 1073 3128882 792071.5 962.898 TRE 1074 3128884 792072.7 962.931 POL 1075 3128880 792039.9 961.005	1059	3128958	791984.1	965.59	TRE
1062 3128922 792027.4 964.463 TRE 1063 3128940 791995.3 965.29 TRE 1064 3128926 792029.3 964.246 TRE 1065 3128927 792015.2 964.796 CHAU 1066 3128925 792013.2 964.93 CHAU 1067 3128929 792009.3 964.797 CHAU 1068 3128931 792011.3 964.904 CHAU 1069 3128951 792007.8 964.784 TRE 1070 3128935 792020.4 964.704 TRE 1071 3128893 792070.7 963.11 TRE 1072 3128900 792064.6 963.703 TRE 1073 3128882 792071.5 962.898 TRE 1074 3128884 792072.7 962.931 POL 1075 3128880 792039.9 961.005 POL 1076 3128856 792065.3 962.224	1060	3128935	792019.8	964.793	TRE
1063 3128940 791995.3 965.29 TRE 1064 3128926 792029.3 964.246 TRE 1065 3128927 792015.2 964.796 CHAU 1066 3128925 792013.2 964.93 CHAU 1067 3128929 792009.3 964.797 CHAU 1068 3128931 792011.3 964.904 CHAU 1069 3128951 792007.8 964.784 TRE 1070 3128935 792020.4 964.704 TRE 1071 3128893 792070.7 963.11 TRE 1072 3128900 792064.6 963.703 TRE 1073 3128882 792071.5 962.898 TRE 1074 3128884 792072.7 962.931 POL 1075 3128880 792039.9 961.005 POL 1076 3128856 792065.3 962.223 POL 1078 3128905 792038.4 963.898	1061	3128946	791982.4	965.294	TRE
1064 3128926 792029.3 964.246 TRE 1065 3128927 792015.2 964.796 CHAU 1066 3128925 792013.2 964.93 CHAU 1067 3128929 792009.3 964.797 CHAU 1068 3128931 792011.3 964.904 CHAU 1069 3128951 792007.8 964.784 TRE 1070 3128935 792020.4 964.704 TRE 1071 3128893 792070.7 963.11 TRE 1072 3128900 792064.6 963.703 TRE 1073 3128882 792071.5 962.898 TRE 1074 3128884 792072.7 962.931 POL 1075 3128880 792039.9 961.005 POL 1076 3128856 792065.3 962.223 POL 1078 3128905 792038.4 963.898 PATH 1079 3128923 792019.2 964.43	1062	3128922	792027.4	964.463	TRE
1065 3128927 792015.2 964.796 CHAU 1066 3128925 792013.2 964.93 CHAU 1067 3128929 792009.3 964.797 CHAU 1068 3128931 792011.3 964.904 CHAU 1069 3128951 792007.8 964.784 TRE 1070 3128935 792020.4 964.704 TRE 1071 3128893 792070.7 963.11 TRE 1072 3128900 792064.6 963.703 TRE 1073 3128882 792071.5 962.898 TRE 1074 3128884 792072.7 962.931 POL 1075 3128880 792039.9 961.005 POL 1076 3128856 792065.3 962.223 POL 1077 3128862 792098.5 962.224 POL 1078 3128905 792038.4 963.898 PATH 1080 3128929 792023.1 964.43	1063	3128940	791995.3	965.29	TRE
1066 3128925 792013.2 964.93 CHAU 1067 3128929 792009.3 964.797 CHAU 1068 3128931 792011.3 964.904 CHAU 1069 3128951 792007.8 964.784 TRE 1070 3128935 792020.4 964.704 TRE 1071 3128893 792070.7 963.11 TRE 1072 3128900 792064.6 963.703 TRE 1073 3128882 792071.5 962.898 TRE 1074 3128884 792072.7 962.931 POL 1075 3128880 792039.9 961.005 POL 1076 3128856 792065.3 962.223 POL 1078 3128905 792038.4 963.898 PATH 1079 3128923 792019.2 964.43 PATH 1080 3128929 792023.1 964.707 PATH	1064	3128926	792029.3	964.246	TRE
1067 3128929 792009.3 964.797 CHAU 1068 3128931 792011.3 964.904 CHAU 1069 3128951 792007.8 964.784 TRE 1070 3128935 792020.4 964.704 TRE 1071 3128893 792070.7 963.11 TRE 1072 3128900 792064.6 963.703 TRE 1073 3128882 792071.5 962.898 TRE 1074 3128884 792072.7 962.931 POL 1075 3128880 792039.9 961.005 POL 1076 3128862 792065.3 962.223 POL 1077 3128862 792098.5 962.224 POL 1078 3128905 792038.4 963.898 PATH 1079 3128923 792019.2 964.43 PATH 1080 3128929 792023.1 964.707 PATH	1065	3128927	792015.2	964.796	CHAU
1068 3128931 792011.3 964.904 CHAU 1069 3128951 792007.8 964.784 TRE 1070 3128935 792020.4 964.704 TRE 1071 3128893 792070.7 963.11 TRE 1072 3128900 792064.6 963.703 TRE 1073 3128882 792071.5 962.898 TRE 1074 3128884 792072.7 962.931 POL 1075 3128880 792039.9 961.005 POL 1076 3128856 792065.3 962.223 POL 1078 3128962 792098.5 962.224 POL 1079 3128923 792019.2 964.43 PATH 1080 3128929 792023.1 964.707 PATH	1066	3128925	792013.2	964.93	CHAU
1069 3128951 792007.8 964.784 TRE 1070 3128935 792020.4 964.704 TRE 1071 3128893 792070.7 963.11 TRE 1072 3128900 792064.6 963.703 TRE 1073 3128882 792071.5 962.898 TRE 1074 3128884 792072.7 962.931 POL 1075 3128880 792039.9 961.005 POL 1076 3128856 792065.3 962.223 POL 1077 3128862 792098.5 962.224 POL 1078 3128905 792038.4 963.898 PATH 1079 3128923 792019.2 964.43 PATH 1080 3128929 792023.1 964.707 PATH	1067	3128929	792009.3	964.797	CHAU
1070 3128935 792020.4 964.704 TRE 1071 3128893 792070.7 963.11 TRE 1072 3128900 792064.6 963.703 TRE 1073 3128882 792071.5 962.898 TRE 1074 3128884 792072.7 962.931 POL 1075 3128880 792039.9 961.005 POL 1076 3128856 792065.3 962.223 POL 1077 3128862 792098.5 962.224 POL 1078 3128905 792038.4 963.898 PATH 1079 3128923 792019.2 964.43 PATH 1080 3128929 792023.1 964.707 PATH	1068	3128931	792011.3	964.904	CHAU
1071 3128893 792070.7 963.11 TRE 1072 3128900 792064.6 963.703 TRE 1073 3128882 792071.5 962.898 TRE 1074 3128884 792072.7 962.931 POL 1075 3128880 792039.9 961.005 POL 1076 3128856 792065.3 962.223 POL 1077 3128862 792098.5 962.224 POL 1078 3128905 792038.4 963.898 PATH 1079 3128923 792019.2 964.43 PATH 1080 3128929 792023.1 964.707 PATH	1069	3128951	792007.8	964.784	TRE
1072 3128900 792064.6 963.703 TRE 1073 3128882 792071.5 962.898 TRE 1074 3128884 792072.7 962.931 POL 1075 3128880 792039.9 961.005 POL 1076 3128856 792065.3 962.223 POL 1077 3128862 792098.5 962.224 POL 1078 3128905 792038.4 963.898 PATH 1079 3128923 792019.2 964.43 PATH 1080 3128929 792023.1 964.707 PATH	1070	3128935	792020.4	964.704	TRE
1073 3128882 792071.5 962.898 TRE 1074 3128884 792072.7 962.931 POL 1075 3128880 792039.9 961.005 POL 1076 3128856 792065.3 962.223 POL 1077 3128862 792098.5 962.224 POL 1078 3128905 792038.4 963.898 PATH 1079 3128923 792019.2 964.43 PATH 1080 3128929 792023.1 964.707 PATH	1071	3128893	792070.7	963.11	TRE
1074 3128884 792072.7 962.931 POL 1075 3128880 792039.9 961.005 POL 1076 3128856 792065.3 962.223 POL 1077 3128862 792098.5 962.224 POL 1078 3128905 792038.4 963.898 PATH 1079 3128923 792019.2 964.43 PATH 1080 3128929 792023.1 964.707 PATH	1072	3128900	792064.6	963.703	TRE
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	1081	3128937	792009.5	964.83	PATH

1082	3128941	792006.9	964.817	PATH
1083	3128942	792031.8	964.828	PATH
1084	3128907	792067.9	963.191	PATH
1085	3128907	792076.6	962.907	PATH
1086	3128876	792070.4	962.885	PATH
1087	3128868	792067.3	962.734	PATH
1088	3128887	792007.2	958.137	ROAD
1089	3128889	792003.4	958.163	ROAD
1090	3128893	792014.2	958.383	ROAD
1091	3128895	792020.2	958.769	ROAD
1092	3128900	792019.9	958.805	ROAD
1093	3128890	792030.2	959.57	ROAD
1094	3128893	792034.1	959.764	ROAD
1095	3128883	792038	960.31	ROAD
1096	3128885	792042.4	960.486	ROAD
1097	3128861	792059.4	961.945	ROAD
1098	3128865	792061.4	961.855	ROAD
1099	3128856	792067.5	962.125	ROAD
1100	3128859	792072.4	962.067	ROAD
1101	3128855	792078.4	962.206	ROAD
1102	3128859	792077.1	962.113	ROAD
1103	3128858	792089.3	962.086	ROAD
1104	3128863	792089	962.04	ROAD
1105	3128863	792097.3	961.93	ROAD
1106	3128867	792095.5	961.921	ROAD
1107	3128874	792119.9	961.749	ROAD
1108	3128878	792118	961.705	ROAD
1109	3128883	792100.4	962.385	TT
1110	3128880	792101	962.363	TT
1111	3128880	792099.8	962.322	TT
1112	3128882	792099.2	962.396	TT
1113	3128916	792089.5	963.845	TOL
1114	3128916	792095.2	963.884	TOL
1115	3128920	792089.5	964.544	TOL
1116	3128915	792066.5	964.086	TOL
1117	3128914	792057.3	964.084	TOL
1118	3128916	792057.1	964.103	TOL
1119	3128914	792049.1	964.111	TOL
1120	3128913	792039.8	964.132	TOL
1121	3128916	792125.4	964.724	BC
1122	3128898	792126.2	962.395	BC
1123	3128898	792128	962.282	BC

1124 3128896 792129.5 962.271 BC 1125 3128896 792131.2 962.044 BC 1126 3128895 792131.9 961.707 BC 1127 3128886 792131.9 961.707 BC 1128 3128944 792121.3 966.619 BC 1129 3128945 792132.6 966.642 BC 1130 3128950 792120.9 966.633 BC 1131 3128950 792116.5 966.61 BC CP1					
1126	1124	3128896	792129.5	962.271	BC
1127 3128886 792131.9 961.707 BC 1128 3128944 792121.3 966.619 BC 1129 3128945 792132.6 966.642 BC 1130 3128950 792120.9 966.633 BC 1131 3128950 792116.5 966.61 BC CP1 CP1 CP1 CP1 BS-2 3128897 792042.6 963.168 BS-2 2001 3129001 791967.1 968.659 SH 2002 3129000 791964.2 968.568 SH 2004 3129000 791968.2 968.665 SH 2005 3129002 791963.6 967.882 SH 2006 3129016 791963.6 968.783 SH 2007 3129016 791963.6 968.783 SH 2007 3129016 791963.6 968.783 SH 2007 3129016 791963.6 968.713 SH 2	1125	3128896	792131.2	962.044	ВС
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2025 3129018 792007.5 968.642 SH 2026 3129023 791980.3 968.252 SH 2027 3128970 791915.1 967.987 SH 2028 3128966 791942.4 968.143 SH 2029 3128980 791970.8 969.062 SH 2030 3128971 791972.9 969.243 SH 2031 3128983 791975.8 969.043 SH	2023	3129020	791980.3	969.151	SH
2026 3129023 791980.3 968.252 SH 2027 3128970 791915.1 967.987 SH 2028 3128966 791942.4 968.143 SH 2029 3128980 791970.8 969.062 SH 2030 3128971 791972.9 969.243 SH 2031 3128983 791975.8 969.043 SH	2024	3129022	791978.9	968.913	SH
2027 3128970 791915.1 967.987 SH 2028 3128966 791942.4 968.143 SH 2029 3128980 791970.8 969.062 SH 2030 3128971 791972.9 969.243 SH 2031 3128983 791975.8 969.043 SH	2025	3129018	792007.5	968.642	SH
2028 3128966 791942.4 968.143 SH 2029 3128980 791970.8 969.062 SH 2030 3128971 791972.9 969.243 SH 2031 3128983 791975.8 969.043 SH	2026	3129023	791980.3	968.252	SH
2029 3128980 791970.8 969.062 SH 2030 3128971 791972.9 969.243 SH 2031 3128983 791975.8 969.043 SH	2027	3128970	791915.1	967.987	SH
2030 3128971 791972.9 969.243 SH 2031 3128983 791975.8 969.043 SH	2028	3128966	791942.4	968.143	SH
2031 3128983 791975.8 969.043 SH	2029	3128980	791970.8	969.062	SH
	2030	3128971	791972.9	969.243	SH
2032 3128970 791974.9 969.203 SH	2031	3128983	791975.8	969.043	SH
	2032	3128970	791974.9	969.203	SH

2033 2034 2035 2036 2037	3128984 3128971 3128991 3128994 3129000	791986.8 791978.9 791992.5 791983.6	968.676 969.217 968.809	SH SH SH
2035 2036 2037	3128991 3128994	791992.5		
2036 2037	3128994	+	968.809	СП
2037		791983.6		D11
	3129000	00.0	968.081	SH
2029		791981.5	966.809	SH
2038	3129006	791990.9	965.744	SH
2039	3128990	791970.3	967.748	SH
2040	3128975	791960.1	968.485	SH
2041	3129004	791993.3	965.586	ROAD
2042	3129008	791990.8	965.651	ROAD
2043	3128997	791981.7	966.902	ROAD
2044	3129001	791979.1	966.912	ROAD
2045	3128989	791972.5	967.718	ROAD
2046	3128991	791968.4	967.821	ROAD
2047	3128975	791962.8	968.5	ROAD
2048	3128977	791958.5	968.485	ROAD
2049	3128973	791955.8	968.738	ROAD
2050	3128970	791959.2	968.673	ROAD
2051	3128966	791948.4	968.874	ROAD
2052	3128961	791953.6	968.853	ROAD
2053	3128959	791946.4	968.876	ROAD
2054	3128955	791949.4	968.947	ROAD
2055	3128954	791942.9	968.936	ROAD
2056	3128951	791946.6	968.984	ROAD
2057	3128976	791952.1	968.687	ROAD
2058	3128974	791948	968.653	ROAD
2059	3128982	791951.5	968.463	ROAD
2060	3128981	791947.3	968.473	ROAD
2061	3128989	791951.1	968.222	ROAD
2062	3128990	791947.1	968.205	ROAD
2063	3128997	791949.8	968.004	ROAD
2064	3128997	791945.1	968.001	ROAD
2065	3129008	791949	967.768	ROAD
2066	3129008	791944.3	967.831	ROAD
2067	3128991	791945.7	968.569	POL
2068	3128973	791925.9	968.859	POL
2069	3128960	791953.7	969.108	POL
2070	3128992	791977	967.57	POL
2071	3129001	791970.4	968.285	TRE
2072	3129012	791986.5	966.427	TRE
2073	3129002	791972.3	968.075	TRE
2074	3129009	791984.9	966.383	TRE

2075	3129005	791975.8	967.454	TRE
2076	3129009	791985	966.378	TRE
2077	3128993	791964.4	968.583	TRE
2078	3129007	791954.2	968.387	TRE
2079	3128992	791963.1	968.592	TRE
2080	3128984	791954.7	968.807	TRE
2081	3128969	791944.3	969.155	TRE
2082	3128981	791956.6	968.795	TRE
2083	3128974	791930.3	969.105	TRE
2084	3128981	791956.7	968.805	TRE
2085	3128946	791948.5	969.643	TRE
2086	3128953	791953.4	969.644	TRE
2087	3128962	791961	969.459	TRE
2088	3128965	791963.4	969.485	TRE
2089	3128975	791967.9	969.3	TRE
2090	3128976	791954.4	968.698	PARK
2091	3129001	791971.8	968.101	PARK
2092	3129013	791953	968.171	PARK
2093	3129001	791970.3	968.36	GYM
2094	3129010	791955.5	968.228	GYM
2095	3128999	791968.6	968.349	GYM
2096	3129007	791954.5	968.411	GYM
2097	3129005	791942.3	967.917	BC
2098	3129004	791939.5	968.042	BC
2099	3128998	791940	968.062	BC
2100	3128997	791924.8	968.632	BC
2101	3128993	791931.1	968.682	BC
2102	3128981	791932	968.697	BC
2103	3128994	791943.5	968.078	PATH
2104	3128991	791937.3	968.425	PATH
2105	3128977	791938.3	968.94	PATH
2106	3128976	791920.8	968.82	PATH
2107	3129004	791968	968.307	SH
2108	3129006	791968.6	968.106	SH
2109	3129008	791966.2	968.169	SH
2110	3129009	791966.2	967.585	SH
2111	3129008	791964.2	968.258	SH
2112	3129011	791960.7	968.289	SH
2113	3129012	791960.6	967.657	SH
2114	3128958	791889.4	967.64	OFF-1
BS-3	3128994	791962.6	968.511	BS-3

3001	3128963	791895.9	967.714	SH
3002	3128974	791894.6	967.811	SH
3003	3128976	791891.3	967.985	SH
3004	3128986	791893.9	968.35	SH
3005	3128987	791883.4	967.798	SH
3006	3128979	791880.4	967.479	SH
3007	3128968	791882.5	967.413	SH
3008	3128979	791873.3	967.465	SH
3009	3128969	791875.8	967.374	SH
3010	3128978	791863.6	967.41	SH
3011	3128969	791859.5	967.187	SH
3012	3128984	791867.3	967.443	SH
3013	3128969	791848.6	967.022	SH
3014	3128992	791873.8	967.602	SH
3015	3128982	791848.9	967.338	SH
3016	3128979	791869.8	967.438	TRE
3017	3128995	791895.4	968.087	TRE
3018	3128995	791891.6	968.248	TRE
3019	3128993	791885.3	967.826	TRE
3020	3129005	791869.8	968.058	TRE
3021	3129006	791876.5	967.857	TRE
3022	3129009	791867.4	967.569	TRE
3023	3129001	791882	968.122	TRE
3024	3129002	791888.2	967.632	TRE
3025	3128980	791916.6	968.671	BC
3026	3128980	791914.1	968.674	BC
3027	3128976	791908.2	968.682	BC
3028	3128976	791898.9	968.666	BC
3029	3128988	791897.9	968.634	BC
3030	3128996	791894.6	968.032	TAP
3031	3128982	791870.6	967.522	SU-PARK
3032	3128986	791867.4	967.378	SU-PARK
3033	3128989	791870.2	967.58	SU-PARK
3034	3128988	791874.2	967.534	SU-PARK
3035	3128983	791875	967.632	SU-PARK
3036	3128990	791887.4	967.991	BE-PARK
3037	3128994	791881.3	967.684	BE-PARK
3038	3128996	791884.3	967.777	BE-PARK
3039	3128995	791887.3	967.978	BE-PARK
3040	3128994	791890.6	968.526	BE-PARK
3041	3128991	791890.4	968.451	BE-PARK
3042	3128999	791876.7	967.654	L-PARK

3043 3128998 791864.3 967.709 L-PARK 3044 3129013 791875.9 967.428 L-PARK 3045 3129011 791862.4 967.582 L-PARK 3046 3128999 791879.4 967.664 B-PARK 3047 3129021 791878.4 967.305 B-PARK 3048 3129023 791903 967.327 B-PARK 3049 3129000 791892.7 967.768 B-PARK 3050 3129000 791891 967.766 B-PARK 3051 3129011 791891.4 968.134 B-PARK 3052 3128983 791856.9 967.329 BB 3053 3128992 791856.2 967.329 BB 3054 3128982 791847.5 967.386 BB 3055 3128974 791842.4 967.025 BB 3056 3128974 791842.4 967.025 BB 3058 3128970 791842.4 967.025 BB 3059 3128969 791818.8 966.929 BB 3060 3128968 791842.7 967.041 BB 3059 3128969 791818.8 966.929 BB 3060 3128968 791843.7 967.004 BB 3061 3128993 791859.9 967.134 TAP 3062 3128969 791843.7 967.002 PATH 3063 3128969 791844.2 967.01 PATH 3064 3128999 791871.6 967.737 PATH 3065 3128997 791871.6 967.737 PATH 3066 3128998 791879.9 967.91 PATH 3067 3128999 791879.3 967.808 OFF-2 OFF-2 OFF-2 OFF-2 58-4 3128989 791879.9 967.633 BS-4 4001 3128998 791912.7 968.635 BC 4003 3128998 791912.7 968.635 BC 4004 3128998 791912.7 968.635 BC 4005 3128998 791912.7 968.635 BC 4006 3128998 791912.7 968.635 BC 4007 3129002 791922 968.636 BC 4008 3128998 791915.4 968.856 BC 4009 3128998 79192.1 968.635 BC 4000 3128998 79192.1 968.635 BC 4001 3128998 791908.1 968.366 L-POL 4010 3128998 791859.8 967.556 L-POL 4011 3128998 791860.5 966.634 FSU					
3045 3129011 791862.4 967.582 L-PARK 3046 3128999 791879.4 967.664 B-PARK 3047 3129021 791878.4 967.305 B-PARK 3048 3129023 791903 967.327 B-PARK 3049 3129000 791891.7 967.766 B-PARK 3050 3129001 791891.4 968.134 B-PARK 3051 3129011 791891.4 968.134 B-PARK 3052 3128983 791856.9 967.329 BB 3053 3128992 791856.9 967.329 BB 3054 3128975 791848.6 967.355 BB 3055 3128975 791842.4 967.025 BB 3056 3128970 791842.7 967.041 BB 3057 3128969 791812.3 967.024 BB 3059 3128969 791842.7 967.041 BB 3060 3128968 791899.2 967.02	3043	3128998	791864.3	967.709	L-PARK
3046 3128999 791879.4 967.664 B-PARK 3047 3129021 791878.4 967.305 B-PARK 3048 3129023 791903 967.327 B-PARK 3049 3129000 791891.7 967.768 B-PARK 3050 3129000 791891 967.766 B-PARK 3051 3129011 791891.4 968.134 B-PARK 3052 3128983 791856.9 967.329 BB 3053 3128992 791856.2 967.29 BB 3055 3128975 791848.6 967.355 BB 3056 3128974 791842.4 967.025 BB 3057 3128970 791842.7 967.041 BB 3058 3128969 791827.3 967.024 BB 3059 3128969 791827.3 967.024 BB 3060 3128968 791809.4 966.468 BB 3061 3128998 791859.9 967.134 TAP 3063 3128969 791844.2 967.002 PATH 3063 3128969 791844.2 967.168 PATH 3064 3128969 791844.2 967.168 PATH 3065 3128997 791844.2 967.168 PATH 3066 3128998 791879.9 967.717 PATH 3066 3128998 791879.9 967.777 PATH 3066 3128998 791879.9 967.777 PATH 3067 3128999 791879.9 967.777 PATH 3067 3128999 791879.9 967.777 PATH 3067 3128999 791879.3 967.808 OFF-2	3044	3129013	791875.9	967.428	L-PARK
3047 3129021 791878.4 967.305 B-PARK 3048 3129023 791903 967.327 B-PARK 3049 3129000 791892.7 967.766 B-PARK 3050 3129001 791891.4 968.134 B-PARK 3051 3129011 791891.4 968.134 B-PARK 3052 3128983 791856.9 967.329 BB 3053 3128992 791856.2 967.329 BB 3054 3128982 791847.5 967.386 BB 3055 3128975 791848.6 967.355 BB 3056 3128974 791842.7 967.041 BB 3057 3128970 791842.7 967.041 BB 3058 3128969 791872.3 967.024 BB 3059 3128968 79189.9 967.134 TAP 3060 3128996 791843.7 967.002 PATH 3061 3128996 791844.2 967.168	3045	3129011	791862.4	967.582	L-PARK
3048 3129023 791903 967.327 B-PARK 3049 3129000 791892.7 967.768 B-PARK 3050 3129000 791891 967.766 B-PARK 3051 3129011 791891.4 968.134 B-PARK 3052 3128983 791856.9 967.329 BB 3053 3128992 791845.2 967.29 BB 3054 3128982 791847.5 967.386 BB 3055 3128974 791842.4 967.025 BB 3056 3128970 791842.7 967.041 BB 3058 3128969 791827.3 967.024 BB 3059 3128969 791843.7 967.041 BB 3060 3128969 791843.7 967.024 BB 3061 3128969 791843.7 967.024 BB 3061 3128969 791843.7 967.002 PATH 3062 3128969 791843.7 967.134	3046	3128999	791879.4	967.664	B-PARK
3049 3129000 791892.7 967.768 B-PARK 3050 3129000 791891 967.766 B-PARK 3051 3129011 791891.4 968.134 B-PARK 3052 3128983 791856.9 967.329 BB 3053 3128992 791856.2 967.29 BB 3054 3128982 791847.5 967.386 BB 3055 3128975 791848.6 967.355 BB 3056 3128974 791842.4 967.025 BB 3057 3128970 791842.7 967.041 BB 3058 3128969 791827.3 967.024 BB 3059 3128969 791827.3 967.024 BB 3060 3128968 791809.4 966.468 BB 3061 3128998 791859.9 967.134 TAP 3062 3128969 791843.7 967.002 PATH 3063 3128969 791844.2 967.168 PATH 3064 3128969 791844.2 967.168 PATH 3064 3128998 791871.6 967.737 PATH 3065 3128998 791871.6 967.737 PATH 3066 3128998 791879.9 967.777 PATH 3067 3128999 791879.3 967.808 OFF-2 OFF-2 OFF-2 OFF-2 BS-4 3128998 791879.3 967.808 OFF-2 OFF-2 BS-4 3128994 791912.7 968.679 BC 4004 3128994 791912.1 968.679 BC 4005 3128998 791912.1 968.679 BC 4006 3128998 791912.1 968.679 BC 4006 3128998 79192.1 968.679 BC 4006 3128998 79192.3 968.678 BC 4007 3129002 791912.9 968.636 BC 4008 3128998 79192.3 968.678 BC 4008 3128998 79192.3 968.678 BC 4008 3128998 79192.3 968.679 BC 4008 3128998 79192.3 968.678 BC 4008 3128998 79192.3 968.678 BC 4008 3128998 79192.3 968.678 BC 4009 3128999 791908.1 968.679 BC 4001 3128998 79192.3 968.678 BC 4001 3128998 79192.3 968.636 BC 4001 3128998 791908.1 968.679 BC 4001 3128998 791908.1 966.734 FSU	3047	3129021	791878.4	967.305	B-PARK
3050 3129000 791891 967.766 B-PARK 3051 3129011 791891.4 968.134 B-PARK 3052 3128983 791856.9 967.329 BB 3053 3128992 791856.2 967.29 BB 3054 3128982 791847.5 967.386 BB 3055 3128975 791848.6 967.355 BB 3056 3128974 791842.4 967.025 BB 3057 3128970 791842.7 967.041 BB 3058 3128969 791827.3 967.024 BB 3059 3128969 791818.8 966.929 BB 3060 3128968 791809.4 966.468 BB 3061 3128993 791859.9 967.134 TAP 3062 3128969 791843.7 967.002 PATH 3063 3128969 791844.2 967.168 PATH 3064 3128969 791844.2 967.168 PATH 3064 3128969 791844.2 967.168 PATH 3065 3128969 791871.6 967.737 PATH 3065 3128997 791871.6 967.737 PATH 3066 3128998 791877.9 967.777 PATH 3068 3128998 791879.3 967.808 OFF-2 O	3048	3129023	791903	967.327	B-PARK
3051 3129011 791891.4 968.134 B-PARK 3052 3128983 791856.9 967.329 BB 3053 3128992 791856.2 967.29 BB 3054 3128982 791847.5 967.386 BB 3055 3128975 791848.6 967.355 BB 3056 3128970 791842.4 967.025 BB 3057 3128970 791842.7 967.041 BB 3058 3128969 791827.3 967.024 BB 3059 3128969 791818.8 966.929 BB 3060 3128968 791809.4 966.468 BB 3061 3128996 791843.7 967.002 PATH 3062 3128969 791843.7 967.002 PATH 3063 3128969 791844.2 967.168 PATH 3064 3128969 791871.6 967.077 PATH 3065 3128997 791871.6 967.777	3049	3129000	791892.7	967.768	B-PARK
3052 3128983 791856.9 967.329 BB 3053 3128992 791856.2 967.29 BB 3054 3128982 791847.5 967.386 BB 3055 3128975 791848.6 967.355 BB 3056 3128974 791842.4 967.025 BB 3057 3128960 791842.7 967.041 BB 3058 3128969 791842.7 967.041 BB 3059 3128969 791818.8 966.929 BB 3060 3128968 791809.4 966.468 BB 3061 3128993 791843.7 967.002 PATH 3062 3128969 791843.7 967.002 PATH 3063 3128969 791844.2 967.168 PATH 3064 3128969 791844.2 967.168 PATH 3065 3128997 791871.6 967.737 PATH 3066 3128998 791871.6 967.777 <t< td=""><td>3050</td><td>3129000</td><td>791891</td><td>967.766</td><td>B-PARK</td></t<>	3050	3129000	791891	967.766	B-PARK
3053 3128992 791856.2 967.29 BB 3054 3128982 791847.5 967.386 BB 3055 3128975 791848.6 967.355 BB 3056 3128974 791842.4 967.025 BB 3057 3128970 791842.7 967.041 BB 3058 3128969 791827.3 967.024 BB 3059 3128969 791818.8 966.929 BB 3060 3128969 791818.9 967.024 BB 3061 3128963 791809.4 966.468 BB 3061 3128969 791843.7 967.002 PATH 3062 3128969 791843.7 967.168 PATH 3063 3128969 791844.2 967.168 PATH 3064 3128996 791871.6 967.737 PATH 3066 3128998 791879.9 967.91 PATH 3067 3128999 791899.2 967.91	3051	3129011	791891.4	968.134	B-PARK
3054 3128982 791847.5 967.386 BB 3055 3128975 791848.6 967.355 BB 3056 3128974 791842.4 967.025 BB 3057 3128970 791842.7 967.041 BB 3058 3128969 791827.3 967.024 BB 3059 3128969 791818.8 966.929 BB 3060 3128968 791809.4 966.468 BB 3061 3128993 791859.9 967.134 TAP 3062 3128969 791843.7 967.002 PATH 3063 3128961 791844.2 967.168 PATH 3064 3128969 791844.2 967.168 PATH 3065 3128997 791871.6 967.737 PATH 3066 3128998 791879.9 967.717 PATH 3067 3128999 791899.2 967.91 PATH 3068 3128998 791879.3 967.633	3052	3128983	791856.9	967.329	BB
3055 3128975 791848.6 967.355 BB 3056 3128974 791842.4 967.025 BB 3057 3128970 791842.7 967.041 BB 3058 3128969 791827.3 967.024 BB 3059 3128969 791818.8 966.929 BB 3060 3128968 791809.4 966.468 BB 3061 3128993 791859.9 967.134 TAP 3062 3128969 791843.7 967.002 PATH 3063 3128961 791844.2 967.168 PATH 3064 3128969 791848.6 967.011 PATH 3065 3128997 791871.6 967.737 PATH 3066 3128998 791877.9 967.777 PATH 3067 3128998 791879.3 967.808 OFF-2 OFF-2 DF-2 OFF-2 BS-4 3128998 791912.7 968.95.9 BC 400	3053	3128992	791856.2	967.29	BB
3056 3128974 791842.4 967.025 BB 3057 3128970 791842.7 967.041 BB 3058 3128969 791827.3 967.024 BB 3059 3128969 791818.8 966.929 BB 3060 3128968 791809.4 966.468 BB 3061 3128993 791859.9 967.134 TAP 3062 3128969 791843.7 967.002 PATH 3063 3128961 791844.2 967.168 PATH 3064 3128969 791848.6 967.011 PATH 3065 3128997 791871.6 967.737 PATH 3066 3128998 791877.9 967.777 PATH 3067 3128999 791879.3 967.808 OFF-2 OFF-2 OFF-2 OFF-2 BS-4 3128958 791894.9 967.633 BS-4 4001 3128993 791912.7 968.995 BC 4	3054	3128982	791847.5	967.386	BB
3057 3128970 791842.7 967.041 BB 3058 3128969 791827.3 967.024 BB 3059 3128969 791818.8 966.929 BB 3060 3128968 791809.4 966.468 BB 3061 3128993 791859.9 967.134 TAP 3062 3128969 791843.7 967.002 PATH 3063 3128961 791844.2 967.168 PATH 3064 3128969 791848.6 967.011 PATH 3065 3128997 791871.6 967.737 PATH 3066 3128998 791879.9 967.777 PATH 3067 3128999 791899.2 967.91 PATH 3068 3128996 791879.3 967.808 OFF-2 OFF-2 OFF-2 OFF-2 BS-4 3128989 791912.7 968.995 BC 4002 3128993 791912.6 968.474 BC 40	3055	3128975	791848.6	967.355	BB
3058 3128969 791827.3 967.024 BB 3059 3128969 791818.8 966.929 BB 3060 3128968 791809.4 966.468 BB 3061 3128993 791859.9 967.134 TAP 3062 3128969 791843.7 967.002 PATH 3063 3128961 791844.2 967.168 PATH 3064 3128969 791848.6 967.011 PATH 3065 3128997 791871.6 967.737 PATH 3066 3128998 791877.9 967.91 PATH 3068 3128999 791899.2 967.91 PATH 3068 3128996 791879.3 967.808 OFF-2 OFF-2 OFF-2 OFF-2 BS-4 3128988 791912.7 968.995 BC 4001 3128989 791912.7 968.635 BC 4003 3128994 791921.4 968.635 BC 400	3056	3128974	791842.4	967.025	BB
3058 3128969 791827.3 967.024 BB 3059 3128969 791818.8 966.929 BB 3060 3128968 791809.4 966.468 BB 3061 3128993 791859.9 967.134 TAP 3062 3128969 791843.7 967.002 PATH 3063 3128961 791844.2 967.168 PATH 3064 3128969 791848.6 967.011 PATH 3065 3128997 791871.6 967.737 PATH 3066 3128998 791877.9 967.91 PATH 3068 3128999 791899.2 967.91 PATH 3068 3128996 791879.3 967.808 OFF-2 OFF-2 OFF-2 OFF-2 BS-4 3128988 791912.7 968.995 BC 4001 3128989 791912.7 968.635 BC 4003 3128994 791921.4 968.635 BC 400					BB
3059 3128969 791818.8 966.929 BB 3060 3128968 791809.4 966.468 BB 3061 3128993 791859.9 967.134 TAP 3062 3128969 791843.7 967.002 PATH 3063 3128961 791844.2 967.168 PATH 3064 3128969 791848.6 967.011 PATH 3065 3128997 791871.6 967.737 PATH 3066 3128998 791877.9 967.777 PATH 3067 3128999 791899.2 967.91 PATH 3068 3128996 791879.3 967.808 OFF-2 OFF-2 OFF-2 OFF-2 BS-4 3128958 791889.4 967.633 BS-4 4001 3128993 791912.7 968.995 BC 4002 3128993 791915.4 968.456 BC 4003 3128994 791921.2 968.635 BC					
3061 3128993 791859.9 967.134 TAP 3062 3128969 791843.7 967.002 PATH 3063 3128961 791844.2 967.168 PATH 3064 3128969 791848.6 967.011 PATH 3065 3128997 791871.6 967.737 PATH 3066 3128998 791877.9 967.777 PATH 3067 3128999 791899.2 967.91 PATH 3068 3128996 791879.3 967.808 OFF-2 OFF-2 OFF-2 OFF-2 OFF-2 BS-4 3128958 791889.4 967.633 BS-4 4001 3128989 791912.7 968.995 BC 4002 3128993 791912.6 968.474 BC 4003 3128994 791915.4 968.635 BC 4004 3128998 791921.2 968.635 BC 4005 3128998 791921.1 968.679 BC <td></td> <td>3128969</td> <td></td> <td></td> <td></td>		3128969			
3062 3128969 791843.7 967.002 PATH 3063 3128961 791844.2 967.168 PATH 3064 3128969 791848.6 967.011 PATH 3065 3128997 791871.6 967.737 PATH 3066 3128998 791877.9 967.777 PATH 3067 3128999 791899.2 967.91 PATH 3068 3128996 791879.3 967.808 OFF-2 OFF-2 OFF-2 OFF-2 BS-4 3128958 791889.4 967.633 BS-4 4001 3128989 791912.7 968.995 BC 4002 3128993 791912.6 968.474 BC 4003 3128994 791915.4 968.456 BC 4004 3128994 791921.2 968.635 BC 4005 3128998 791921.1 968.679 BC 4006 3128998 791922.3 968.678 BC 4	3060	3128968	791809.4	966.468	BB
3062 3128969 791843.7 967.002 PATH 3063 3128961 791844.2 967.168 PATH 3064 3128969 791848.6 967.011 PATH 3065 3128997 791871.6 967.737 PATH 3066 3128998 791877.9 967.777 PATH 3067 3128999 791899.2 967.91 PATH 3068 3128996 791879.3 967.808 OFF-2 OFF-2 OFF-2 OFF-2 BS-4 3128958 791889.4 967.633 BS-4 4001 3128989 791912.7 968.995 BC 4002 3128993 791912.6 968.474 BC 4003 3128994 791915.4 968.456 BC 4004 3128994 791921.2 968.635 BC 4005 3128998 791921.1 968.679 BC 4006 3128998 791922.3 968.678 BC 4	3061	3128993	791859.9	967.134	TAP
3063 3128961 791844.2 967.168 PATH 3064 3128969 791848.6 967.011 PATH 3065 3128997 791871.6 967.737 PATH 3066 3128998 791877.9 967.777 PATH 3067 3128999 791899.2 967.91 PATH 3068 3128996 791879.3 967.808 OFF-2 OFF-2 OFF-2 OFF-2 BS-4 3128958 791889.4 967.633 BS-4 4001 3128989 791912.7 968.995 BC 4002 3128993 791912.6 968.474 BC 4003 3128994 791915.4 968.456 BC 4004 3128994 791921.2 968.635 BC 4005 3128998 791921.1 968.679 BC 4006 3128998 791922.3 968.678 BC 4007 3129002 79194.5 967.971 BC 4009	3062	3128969			
3065 3128997 791871.6 967.737 PATH 3066 3128998 791877.9 967.777 PATH 3067 3128999 791899.2 967.91 PATH 3068 3128996 791879.3 967.808 OFF-2 OFF-2 OFF-2 OFF-2 BS-4 3128958 791889.4 967.633 BS-4 4001 3128989 791912.7 968.995 BC 4002 3128993 791912.6 968.474 BC 4003 3128994 791915.4 968.456 BC 4004 3128994 791921.2 968.635 BC 4005 3128998 791921.1 968.679 BC 4006 3128998 791922.3 968.636 BC 4007 3129002 791922 968.636 BC 4008 3129002 79194.5 967.971 BC 4009 3128998 79180.1 968.386 L-POL 4011 <td>3063</td> <td>3128961</td> <td>791844.2</td> <td></td> <td>PATH</td>	3063	3128961	791844.2		PATH
3066 3128998 791877.9 967.777 PATH 3067 3128999 791899.2 967.91 PATH 3068 3128996 791879.3 967.808 OFF-2 OFF-2 OFF-2 OFF-2 BS-4 3128958 791889.4 967.633 BS-4 4001 3128989 791912.7 968.995 BC 4002 3128993 791912.6 968.474 BC 4003 3128994 791915.4 968.456 BC 4004 3128994 791921.2 968.635 BC 4005 3128998 791921.1 968.679 BC 4006 3128998 791922.3 968.636 BC 4007 3129002 791922 968.636 BC 4008 3129002 79194.5 967.971 BC 4009 3128999 791908.1 968.386 L-POL 4010 3128998 791859.8 967.556 L-POL 4012 </td <td>3064</td> <td>3128969</td> <td>791848.6</td> <td>967.011</td> <td>PATH</td>	3064	3128969	791848.6	967.011	PATH
3067 3128999 791899.2 967.91 PATH 3068 3128996 791879.3 967.808 OFF-2 OFF-2 OFF-2 OFF-2 BS-4 3128958 791889.4 967.633 BS-4 4001 3128989 791912.7 968.995 BC 4002 3128993 791912.6 968.474 BC 4003 3128994 791915.4 968.456 BC 4004 3128994 791921.2 968.635 BC 4005 3128998 791921.1 968.679 BC 4006 3128998 791922.3 968.678 BC 4007 3129002 791922 968.636 BC 4008 3129002 791914.5 967.971 BC 4009 3128999 791908.1 968.386 L-POL 4010 3128998 791859.8 967.556 L-POL 4012 3129001 791904.6 967.859 B-PARK 401	3065	3128997	791871.6	967.737	PATH
3068 3128996 791879.3 967.808 OFF-2 OFF-2 OFF-2 OFF-2 OFF-2 BS-4 3128958 791889.4 967.633 BS-4 4001 3128989 791912.7 968.995 BC 4002 3128993 791912.6 968.474 BC 4003 3128994 791915.4 968.456 BC 4004 3128994 791921.2 968.635 BC 4005 3128998 791921.1 968.679 BC 4006 3128998 791922.3 968.678 BC 4007 3129002 791922 968.636 BC 4008 3129002 791914.5 967.971 BC 4009 3128999 791908.1 968.386 L-POL 4010 3128998 791896 968.209 L-POL 4012 3129001 791904.6 967.556 L-POL 4013 3128998 791861.1 966.734 FSU <td>3066</td> <td>3128998</td> <td>791877.9</td> <td>967.777</td> <td>PATH</td>	3066	3128998	791877.9	967.777	PATH
OFF-2 DFF-2 BS-4 3128958 791889.4 967.633 BS-4 4001 3128989 791912.7 968.995 BC 4002 3128993 791912.6 968.474 BC 4003 3128994 791915.4 968.456 BC 4004 3128994 791921.2 968.635 BC 4005 3128998 791921.1 968.679 BC 4006 3128998 791922.3 968.678 BC 4007 3129002 791922 968.636 BC 4008 3129002 791914.5 967.971 BC 4009 3128999 791908.1 968.386 L-POL 4010 3128998 791896 968.209 L-POL 4011 3128995 791859.8 967.556 L-POL 4012 3129001 791904.6 967.859 B-PARK 4013 3128998 791861.1 966.734 FSU	3067	3128999	791899.2	967.91	PATH
BS-4 3128958 791889.4 967.633 BS-4 4001 3128989 791912.7 968.995 BC 4002 3128993 791912.6 968.474 BC 4003 3128994 791915.4 968.456 BC 4004 3128994 791921.2 968.635 BC 4005 3128998 791921.1 968.679 BC 4006 3128998 791922.3 968.678 BC 4007 3129002 791922 968.636 BC 4008 3129002 791914.5 967.971 BC 4009 3128999 791908.1 968.386 L-POL 4010 3128998 791896 968.209 L-POL 4011 3128995 791859.8 967.556 L-POL 4012 3129001 791904.6 967.859 B-PARK 4013 3128998 791861.1 966.734 FSU	3068	3128996	791879.3	967.808	OFF-2
4001 3128989 791912.7 968.995 BC 4002 3128993 791912.6 968.474 BC 4003 3128994 791915.4 968.456 BC 4004 3128994 791921.2 968.635 BC 4005 3128998 791921.1 968.679 BC 4006 3128998 791922.3 968.678 BC 4007 3129002 791922 968.636 BC 4008 3129002 791914.5 967.971 BC 4009 3128999 791908.1 968.386 L-POL 4010 3128998 791896 968.209 L-POL 4011 3128995 791859.8 967.556 L-POL 4012 3129001 791904.6 967.859 B-PARK 4013 3128998 791861.1 966.734 FSU	OFF-2				OFF-2
4002 3128993 791912.6 968.474 BC 4003 3128994 791915.4 968.456 BC 4004 3128994 791921.2 968.635 BC 4005 3128998 791921.1 968.679 BC 4006 3128998 791922.3 968.678 BC 4007 3129002 791922 968.636 BC 4008 3129002 791914.5 967.971 BC 4009 3128999 791908.1 968.386 L-POL 4010 3128998 791896 968.209 L-POL 4011 3128995 791859.8 967.556 L-POL 4012 3129001 791904.6 967.859 B-PARK 4013 3128998 791861.1 966.734 FSU	BS-4	3128958	791889.4	967.633	BS-4
4003 3128994 791915.4 968.456 BC 4004 3128994 791921.2 968.635 BC 4005 3128998 791921.1 968.679 BC 4006 3128998 791922.3 968.678 BC 4007 3129002 791922 968.636 BC 4008 3129002 791914.5 967.971 BC 4009 3128999 791908.1 968.386 L-POL 4010 3128998 791896 968.209 L-POL 4011 3128995 791859.8 967.556 L-POL 4012 3129001 791904.6 967.859 B-PARK 4013 3128998 791861.1 966.734 FSU	4001	3128989	791912.7	968.995	BC
4004 3128994 791921.2 968.635 BC 4005 3128998 791921.1 968.679 BC 4006 3128998 791922.3 968.678 BC 4007 3129002 791922 968.636 BC 4008 3129002 791914.5 967.971 BC 4009 3128999 791908.1 968.386 L-POL 4010 3128998 791896 968.209 L-POL 4011 3128995 791859.8 967.556 L-POL 4012 3129001 791904.6 967.859 B-PARK 4013 3128998 791861.1 966.734 FSU	4002	3128993	791912.6	968.474	BC
4005 3128998 791921.1 968.679 BC 4006 3128998 791922.3 968.678 BC 4007 3129002 791922 968.636 BC 4008 3129002 791914.5 967.971 BC 4009 3128999 791908.1 968.386 L-POL 4010 3128998 791896 968.209 L-POL 4011 3128995 791859.8 967.556 L-POL 4012 3129001 791904.6 967.859 B-PARK 4013 3128998 791861.1 966.734 FSU	4003	3128994	791915.4	968.456	BC
4006 3128998 791922.3 968.678 BC 4007 3129002 791922 968.636 BC 4008 3129002 791914.5 967.971 BC 4009 3128999 791908.1 968.386 L-POL 4010 3128998 791896 968.209 L-POL 4011 3128995 791859.8 967.556 L-POL 4012 3129001 791904.6 967.859 B-PARK 4013 3128998 791861.1 966.734 FSU	4004	3128994	791921.2	968.635	ВС
4007 3129002 791922 968.636 BC 4008 3129002 791914.5 967.971 BC 4009 3128999 791908.1 968.386 L-POL 4010 3128998 791896 968.209 L-POL 4011 3128995 791859.8 967.556 L-POL 4012 3129001 791904.6 967.859 B-PARK 4013 3128998 791861.1 966.734 FSU	4005	3128998	791921.1	968.679	BC
4008 3129002 791914.5 967.971 BC 4009 3128999 791908.1 968.386 L-POL 4010 3128998 791896 968.209 L-POL 4011 3128995 791859.8 967.556 L-POL 4012 3129001 791904.6 967.859 B-PARK 4013 3128998 791861.1 966.734 FSU	4006	3128998	791922.3	968.678	BC
4009 3128999 791908.1 968.386 L-POL 4010 3128998 791896 968.209 L-POL 4011 3128995 791859.8 967.556 L-POL 4012 3129001 791904.6 967.859 B-PARK 4013 3128998 791861.1 966.734 FSU	4007	3129002	791922	968.636	BC
4010 3128998 791896 968.209 L-POL 4011 3128995 791859.8 967.556 L-POL 4012 3129001 791904.6 967.859 B-PARK 4013 3128998 791861.1 966.734 FSU	4008	3129002	791914.5	967.971	BC
4011 3128995 791859.8 967.556 L-POL 4012 3129001 791904.6 967.859 B-PARK 4013 3128998 791861.1 966.734 FSU	4009	3128999	791908.1	968.386	L-POL
4012 3129001 791904.6 967.859 B-PARK 4013 3128998 791861.1 966.734 FSU	4010	3128998	791896	968.209	L-POL
4013 3128998 791861.1 966.734 FSU	4011	3128995	791859.8	967.556	L-POL
	4012	3129001	791904.6	967.859	B-PARK
4014 3129006 791860.5 966.697 FSU	4013	3128998	791861.1	966.734	FSU
	4014	3129006	791860.5	966.697	FSU

4015	3128998	791850.2	966.641	FSU
4016	3129026	791874.8	966.481	BC-GE
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4019	3129021	791866.3	966.451	BC-GE
4020	3129020	791844.8	966.432	BC-GE
4021	3129030	791877.5	966.603	G-TOL
4022	3129036	791877.2	966.526	G-TOL
4023	3129031	791883.7	966.574	G-TOL
4024	3129047	791875.6	966.596	PATH
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4026	3129018	791877.2	967.01	PATH
4027	3128997	791866.4	967.721	PATH
4028	3128996	791858	966.538	PATH
4029	3128994	791845.1	966.445	PATH
4030	3128991	791836.3	966.442	ВС
4031	3128997	791842.7	967.046	ВС
4032	3128996	791827.3	966.651	BC
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BS-5	3128996	791879.2	967.811	BS-5
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5003	3129005	791832.2	966.331	ВС
5004	3129015	791831.3	966.403	ВС
5005	3129023	791831.7	966.464	ВС
5006	3129022	791816	966.395	ВС
5007	3129024	791815.6	966.396	ВС
5008	3129025	791809.6	966.326	BC
5009	3129019	791810	966.321	BC
5010	3129025	791806.2	966.347	BC
5011	3129001	791811.4	966.274	BC
5012	3128988	791797.6	966.471	BC
5013	3128988	791801.4	966.406	BC
5014	3128989	791803	966.338	BC
5015	3128989	791803	966.331	BC
5016	3128989	791812.4	966.492	BC
5017	3128990	791825.9	966.472	BC
5018	3128981	791826.7	966.496	BC
5019	3128982	791837.1	966.51	BC
5020	3128994	791837.3	966.41	PATH
5021	3128990	791794.7	966.413	PATH
5022	3129006	791825.2	966.664	TRE

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5026	3128975	791826.4	966.552	TRE
5027	3128972	791829.6	966.471	TRE
5028	3128973	791837.1	966.733	TRE
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5034	3128995	791823.7	966.42	SH
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5043	3129002	791857	966.305	SH
5044	3128998	791857.8	966.622	SH
5045	3129002	791863	966.048	OFF-4
OFF-4				OFF-4
BS-6	3128941	791871.7	965.158	BS-6
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6002	3128997	791865.4	966.359	TRE
6003	3128994	791865.9	966.466	TRE
6004	3128987	791866.9	966.208	TRE
6005	3128985	791867.2	966.203	TRE
6006	3128980	791867.6	966.294	TRE
6007	3128996	791859	966.874	TRE
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6010	3128956	791869.7	965.664	SH
6011	3128979	791861.4	966.269	SH
6012		701070.6	966.629	SH
0012	3128996	791859.6	700.027	511
6012	3128996 3128999	791859.6 791869.4	965.871	SH
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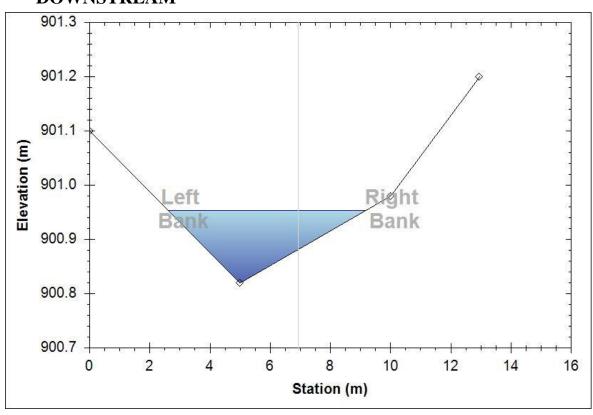
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6029	3129012	791864.8	965.751	BTOL
6030	3129006	791875	965.667	BTOL
6031	3128996	791879.1	964.628	BC
6032	3128998	791900.1	964.706	BC
6033	3128992	791854.4	966.291	BC
6034	3128987	791855.9	966.278	BC
6035	3128987	791858.8	966.307	BC
6036	3128974	791860	966.316	BC
6037	3128969	791860.4	966.296	BC
6038	3128970	791877.8	964.921	BC
6039	3128972	791865.3	965.819	PATH
6040	3129015	791859.5	966.318	PATH
6041	3128941	791871.7	965.168	OFF-5
OFF-5				OFF-5
BS-7	3129002	791863	966.06	BS-7
7001	3128949	791880	964.887	BC
7002	3128952	791903.7	964.689	BC
7003	3128978	791876	964.982	BC
7004	3128922	791901.3	964.347	BC
7005	3128921	791881.1	964.531	BC
7006	3128901	791881.9	964.502	BC
7007	3128900	791869	964.581	BC
7008	3128923	791868.5	964.609	BC
7009	3128947	791868.5	965.141	PATH
7010	3128949	791894.4	964.842	PATH
7011	3128946	791868	965.122	PATH
7012	3128926	791871.2	964.774	PATH
7013	3128944	791852.5	965.517	PATH
7014	3128925	791853.7	964.609	PATH
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7016	3128932	791841.2	964.933	TRE

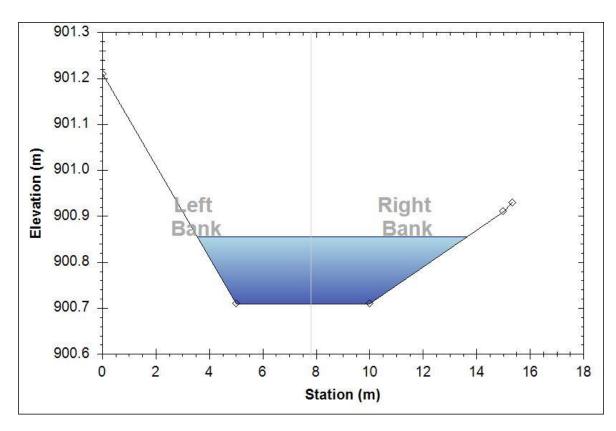
7017	3128935	701050 4	065.07	TED E
	3120733	791850.4	965.07	TRE
7018	3128929	791868	965.383	TRE
7019	3128943	791866.1	965.37	TRE
7020	3128943	791872.9	965.328	TRE
7021	3128939	791873.8	965.127	TRE
7022	3128944	791904.9	964.888	TRE
7023	3128938	791880.5	964.99	SH
7024	3128938	791903.7	964.768	SH
7025	3128935	791883.1	965.212	SH
7026	3128930	791901.5	964.76	SH
7027	3128934	791888.6	965.158	SH
7028	3128929	791904.6	964.752	SH
7029	3128937	791890.8	964.956	SH
7030	3128943	791893.6	965.138	SH
7031	3128949	791899.8	964.787	SH
7032	3128928	791854.8	964.828	SH
7033	3128934	791853.3	964.959	SH
7034	3128935	791865	965.21	SH
7035	3128947	791862.7	966.047	SH
7036	3128941	791840.6	964.916	SH
7037	3128945	791847.5	965.864	SH
7038	3128934	791832	964.829	SH
7039	3128946	791814	965.637	SH
OFF-6				OFF-6
8001	3128962	791838.1	966.419	BC
8002	3128959	791816.6	966.433	BC
8003	3128965	791815.4	966.417	ВС
8004	3128965	791812.4	966.372	BC
8005	3128956	791813.3	966.398	BC
8006	3128955	791798.4	966.488	BC
8007	3128939	791796	964.329	BC
8008	3128937	791767.9	963.736	BC
8009	3128939	791787	964.322	BC
8010	3128938	791775.4	963.752	BC
8011	3128942	791786.7	964.347	BC
8012	3128940	791775.2	963.766	BC
8013	3128919	791818	962.566	PATH
8014	3128927	791817.3	964.523	PATH
8015	3128950	791802.1	966.461	PATH
8016	3128951	791808.2	966.785	TRE
8017	3128952	791812.8	966.762	TRE
	3128953	791820.2	966.658	TRE

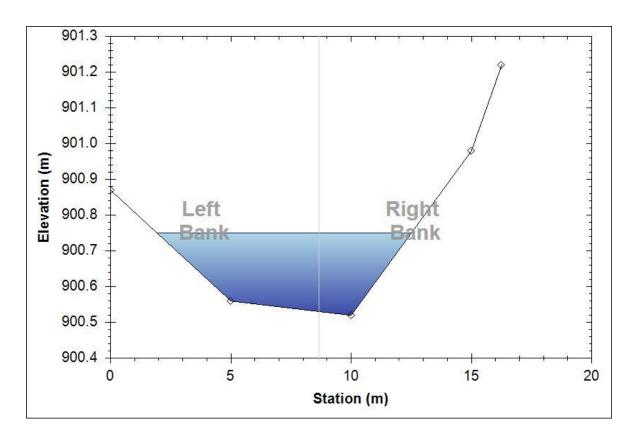
8019	3128953	791827.2	966.712	TRE
8020	3128954	791830.3	966.561	TRE
8021	3128948	791822.2	965.601	SH
8022	3128951	791830.2	966.13	SH
8023	3128938	791807.7	965.571	SH
8024	3128928	791809.3	964.422	SH
8025	3128947	791834	965.221	SH
8026	3128942	791833.5	965.126	SH
8027	3128937	791833.6	964.93	SH
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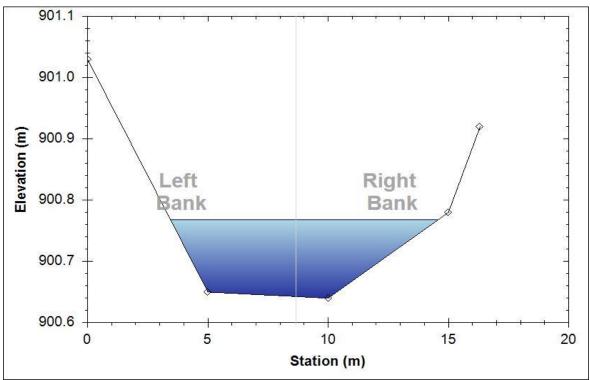
BRIDGE SITE SURVEY GRAPHS

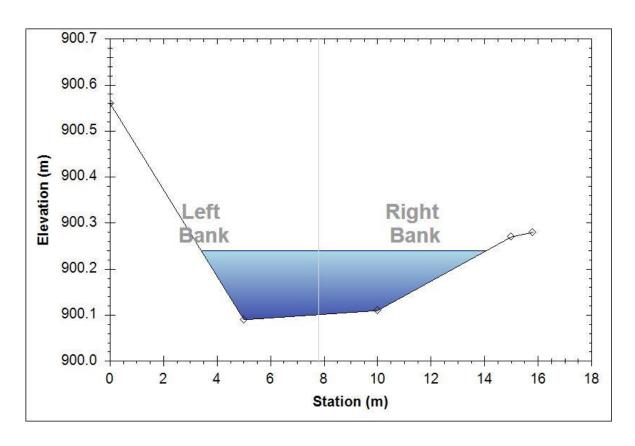
DOWNSTREAM

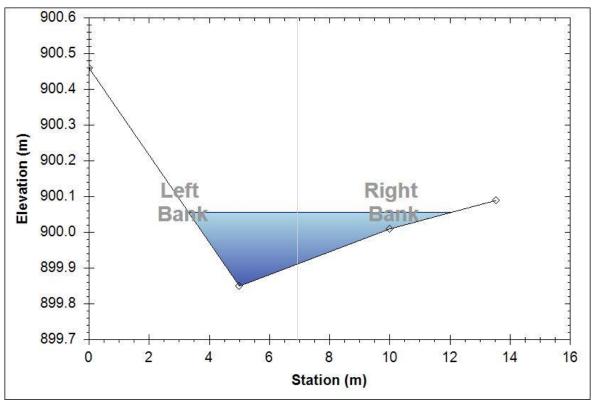


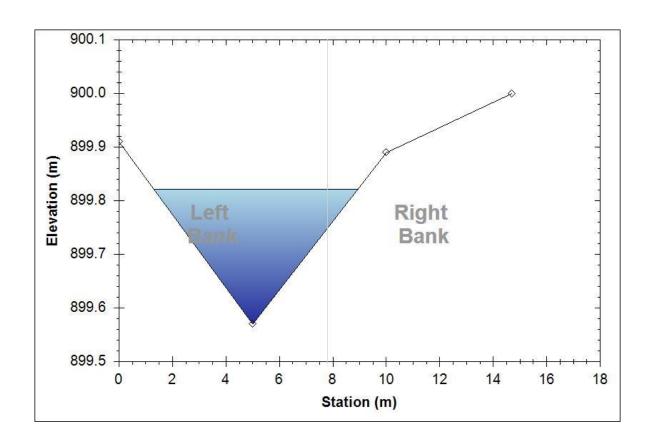












UPSTREAM

