

1. (a) Consider the causal, complex coefficient transfer function shown below:

$$H_M(z) = \frac{\sum_{n=0}^{M-1} d^*[M-n]z^{-n} + z^{-M}}{1 + \sum_{n=1}^M d[n]z^{-n}}, M > 1 \quad (1)$$

- (i) Show that the transfer function in (1) above is an allpass filter. [5]

Answer

The condition for an allpass transfer function is that $|H_M(z)| = 1$, for $|z| = 1$, which implies that $|H_M(e^{j\omega})| = 1$ for all ω . The given function is of the form:

$$\begin{aligned} H_M(z) &= \frac{\sum_{n=0}^{M-1} d^*[M-n]z^{-n} + z^{-M}}{1 + \sum_{n=1}^M d[n]z^{-n}} = \frac{\sum_{n=0}^{M-1} d^*[M-n]z^{-n}}{\sum_{n=0}^M d[n]z^{-n}}, d^*[0] = 1 \\ &= \frac{z^{-M} \sum_{n=0}^{M-1} d^*[M-n]z^{M-n}}{\sum_{n=0}^M d[n]z^{-n}} = \frac{z^{-M} \sum_{r=0}^{M-1} d^*[r]z^r}{\sum_{n=0}^M d[n]z^{-n}}, \\ r &= M - n, d^*[0] = 1 \end{aligned}$$

If we denote the denominator polynomial of the allpass function as $A_M(z)$ with

$$A_M(z) = \sum_{n=0}^{M-1} d[n]z^{-n}$$

then it follows that the given $H_M(z)$ can be written as:

$$H_M(z) = \frac{z^{-M} \bar{A}_M(z^{-1})}{A_M(z)}$$

$\bar{A}_M(z)$ is a polynomial that is obtained from the polynomial $A_M(z)$ if we complex conjugate the coefficients of $A_M(z)$ but we make no changes to the variable z .

For $z = e^{j\omega}$ we see that $|H_M(e^{j\omega})| = 1$. This comes from the fact that $\bar{A}_M(z^{-1})$ becomes the complex conjugate of $A_M(z)$ since every term in $\bar{A}_M(z^{-1})$ is now the complex conjugate of the corresponding term in $A_M(z)$. In that case $|\bar{A}_M(z^{-1})| = |A_M(z)|$ and $|H_M(e^{j\omega})| = 1$. Therefore, $H_M(z)$ is an allpass filter.

Note that the coefficients $d[n]$ are constants and do not change with the location of z . Furthermore, the coefficients in this particular exercise are complex.

- (ii) Comment on the locations of the zeros and the poles of a causal, real, stable, allpass filter's transfer function within the z -plane, with respect to the unit circle. Justify your answer. [5]

Answer

We have proven in the lectures that if z_0 is a pole of an allpass filter, then $1/z_0$ is a zero of the allpass filter. The poles of a causal stable transfer function must lie inside the unit circle. As a result, ALL zeros of a causal stable allpass transfer function lie outside the unit circle in a mirror-image symmetry with its poles situated inside the unit circle.

- (b) Given an allpass filter

$$H(z) = \frac{d + ez + fz^2}{1 + bz + cz^2}$$

with poles at $\frac{1}{2}$ and $\frac{1}{3}$, find b, c, d, e, f . [5]

Answer

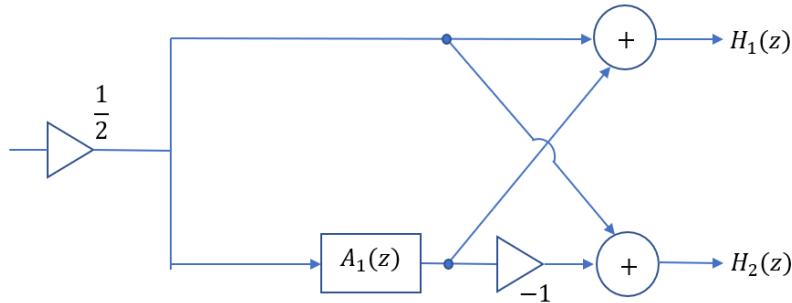
$$1 + bz + cz^2 = c \left(\frac{1}{c} + \frac{b}{c}z + z^2 \right) = c \left(z - \frac{1}{2} \right) \left(z - \frac{1}{3} \right) = c \left(\frac{1}{6} - \frac{5}{6}z + z^2 \right)$$

$$c = 6, b = -5$$

$$H(z) = \frac{d + ez + fz^2}{1 - 5z + 6z^2}$$

and therefore, $d = 6, e = -5, f = 1$.

- (c) In the structure below, $A_1(z)$ is a first-order allpass transfer function. Find the type of filters $H_1(z)$ and $H_2(z)$ (lowpass etc.).



[5]

Answer

$$H_1(z) = \frac{1}{2}(1 + A_1(z))$$

$$H_1(z) = \frac{1}{2}\left(1 + \frac{-az+1}{z-a}\right) = \frac{1}{2} \frac{(1-a)(z+1)}{z-a}$$

$$z = 1 \Rightarrow \omega = 0, H_1(1) = 1$$

$$z = -1 \Rightarrow \omega = \pi, H_1(-1) = 0$$

Therefore, $H_1(z)$ is a lowpass filter.

$$H_2(z) = \frac{1}{2}\left(1 - \frac{-az+1}{z-a}\right) = \frac{1}{2} \frac{(1+a)(z-1)}{z-a}$$

$$z = 1, H_2(1) = 0$$

$$z = -1, H_2(-1) = 1$$

Therefore, $H_2(z)$ is a highpass filter.

- (d) Consider the cascade of two causal LTI systems with impulse responses $h_1[n] = a\delta[n] + b\delta[n-1]$ and $h_2[n] = c^n u[n]$, a, b, c are real coefficients and $|c| < 1$. Determine the frequency response $H(e^{j\omega})$ of the overall system. Find all the possible sets of values of a, b, c for which the overall transfer function has an amplitude equal to 1 for all frequencies [5]

Answer

$$H(z) = H_1(z)H_2(z) = \frac{(a + bz^{-1})z}{z - c} = \frac{az + b}{z - c}$$

$|H(e^{j\omega})| = 1$ implies that $H(z)$ is an allpass filter.

$$|H(e^{j\omega})|^2 = \frac{a^2 + b^2 + 2ab\cos(\omega)}{1 + c^2 - 2cc\cos(\omega)}$$

In order for this relationship to be satisfied for every ω the following conditions must hold:

$$1. a^2 + b^2 = 1 + c^2$$

$$2. ab = -c$$

From these two conditions we obtain:

$$a^2 + b^2 = 1 + a^2b^2, a^2(1 - b^2) = (1 - b^2)$$

If $b^2 \neq 1$ then $a^2 = 1$

- $a = 1 \Rightarrow b = -c, H(z) = \frac{z+b}{z+b} = 1$
- $a = -1 \Rightarrow b = c, H(z) = \frac{-z+b}{z-b} = -1$

If $b^2 = 1$ then

- $b = 1 \Rightarrow a = -c, H(z) = \frac{az+1}{z+a}$
- $b = -1 \Rightarrow a = c, H(z) = \frac{az-1}{z-a}$

Therefore, there are 4 solutions to the problem. Specific values for a, b, c must be found.

2. (a) Design a length-5 FIR bandpass filter with an antisymmetric impulse response $h[n]$, satisfying the following magnitude response values: $|H(e^{j0.3\pi})| = 0.3$ and $|H(e^{j0.6\pi})| = 0.8$. [4]

Answer

The generic form of a length-5 FIR bandpass filter with an antisymmetric impulse response $h[n]$ is given by:

$$\begin{aligned} H(e^{j\omega}) &= h[0] + h[1]e^{-j\omega} + 0e^{-j2\omega} + h[3]e^{-j3\omega} + h[4]e^{-j4\omega} \\ &= h[0] + h[1]e^{-j\omega} - h[1]e^{-j3\omega} \\ &\quad - h[0]e^{-j4\omega} = e^{-j2\omega}[h[0](e^{j2\omega} - e^{-j2\omega}) + h[1](e^{j\omega} - e^{-j\omega})] \\ &= 2je^{-j2\omega}[h[0]\sin(2\omega) + h[1]\sin(\omega)] \end{aligned}$$

$$|H(e^{j\omega})| = 2[h[0]\sin(2\omega) + h[1]\sin(\omega)]$$

Thus,

$$|H(e^{j0.3})| = 2[h[0]\sin(0.6\pi) + h[1]\sin(0.3\pi)] = 0.3$$

$$|H(e^{j0.6})| = 2[h[0]\sin(1.2\pi) + h[1]\sin(0.6\pi)] = 0.8$$

Solving these two equations we get:

$$h[0] = -0.133 \text{ and } h[1] = 0.34$$

As we see here, we have only two unknown coefficients due to the condition of anti-symmetry and for that reason we are given two pieces of information so that we are able to form two equations with two unknowns and solve them.

- (b) We have shown that a real-coefficient FIR transfer function $H(z)$ with a symmetric impulse response has a linear phase response. As a result, the all-pole IIR transfer function $G(z) = \frac{1}{H(z)}$ will also have a linear-phase response. What are the practical difficulties in implementing $G(z)$? Justify your answer. [4]

Answer

$G(z)$ must have poles outside the unit circle making it unstable.

- (c) A simple averaging filter is defined by the following input-output relationship:

$$y[n] = \frac{1}{N}(x[n] + x[n-1] + \dots + x[n-(N-1)])$$

- (i) Let $N = 4$. Determine the filter's transfer function and its zeros and poles. [3]

[Hint: You may use the relationship $\sum_{i=0}^{N-1} z^{-i} = \frac{1-z^{-N}}{1-z^{-1}}$, $z \neq 1$.]

Answer

$$\begin{aligned} Y(z) &= \frac{1}{N}[1 + z^{-1} + \dots + z^{-(N-1)}]X(z) = H(z)X(z) \\ H(z) &= \frac{1}{N} \frac{1-z^{-N}}{1-z^{-1}} = \frac{1}{N} \frac{z^N(1-z^{-N})}{z^{N-1}z(1-z^{-1})} = \frac{1}{N} \frac{1}{z^{N-1}} \frac{z^N - 1}{z - 1} \end{aligned}$$

$$\text{For } N = 4 \text{ we have } H(z) = \frac{1}{4} \frac{1}{z^3} \frac{z^4 - 1}{z - 1}$$

$$z^4 - 1 = 0 \Rightarrow z^4 = 1 \Rightarrow z^2 = \pm 1$$

$$z^2 = 1 \Rightarrow z = \pm 1$$

$$z^2 = -1 \Rightarrow z = \pm j$$

The zero at 1 is cancelled with the pole at 1.

Therefore, we have zeros at $-1, \pm j$ and a triple pole at 0.

- (ii) Determine a general form for zeros and poles for any N .

[3]

Answer

$$H(z) = \frac{1}{N} \frac{1}{z^{N-1}} \frac{z^N - 1}{z - 1}$$

Zeros are found from $z^N - 1 = 0 \Rightarrow z^N = 1 \Rightarrow z = e^{j\frac{2\pi k}{N}}, k = 0, \dots, N-1$

Poles at $z = 0$ with multiplicity $N-1$ and a pole at $z = 1$ which is cancelled by the zero at $z = 1$.

Therefore, zeros are at $z = e^{j\frac{2\pi k}{N}}, k = 1, \dots, N-1$.

- (iii) A recursive implementation of a filter refers to writing the current output as a function of the previous output and the current and past inputs. By comparing $y[n]$ and $y[n-1]$ determine a recursive implementation of the filter.

[3]

Answer

$$y[n-1] = \frac{1}{N} (x[n-1] + x[n-2] + \dots + x[n-1-(N-1)])$$

$$y[n] = \frac{1}{N} (x[n] + x[n-1] + \dots + x[n-(N-1)])$$

$$y[n] - y[n-1] = \frac{1}{N} (x[n] - x[n-1-(N-1)]) \Rightarrow$$

$$y[n] - y[n-1] = \frac{1}{N} (x[n] - x[n-N])$$

We observe that the current output is a function of the previous output, the current input and the input that is distanced by N samples.

- (d) An FIR digital filter has the transfer function

$$H(z) = (1 - z^{-1})^3 (1 + z^{-1})^3$$

- (i) Sketch the pole-zero diagram of this system.

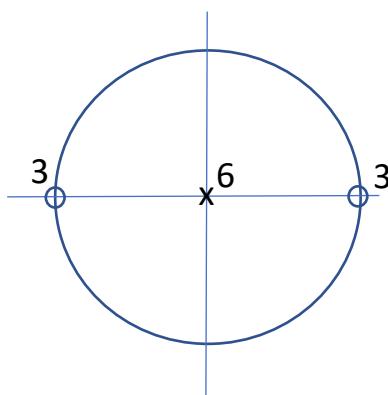
[4]

Answer

Using polynomial expansion, we obtain

$$H(z) = \frac{(z-1)^3(z+1)^3}{z^6}$$

We see that we have 3 zeros at 1, 3 zeros at -1 and 6 poles at 0



- (ii) Sketch **roughly** the amplitude response of the above filter. Would you classify this as a low-pass, high-pass, band-pass, or band-stop filter? Please briefly explain. [4]

Answer

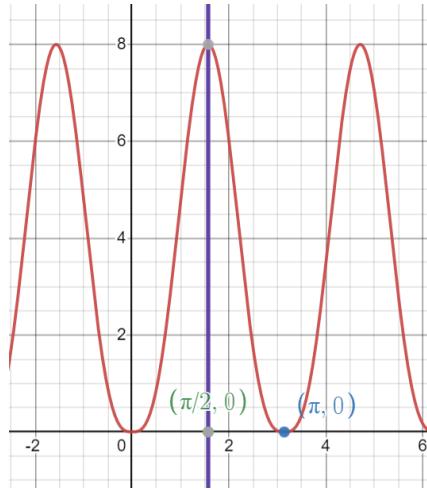
This is the Type 3 linear phase filter it can only be band pass. This answer is not complete. To prove the statement by using the expression given we see that:

$$z = 1 \Rightarrow \omega = 0 \Rightarrow H(e^{j\omega}) = 0$$

$$z = -1 \Rightarrow \omega = \pi \Rightarrow H(e^{j\pi}) = 0$$

$$z = \pm j \Rightarrow \omega = \frac{\pi}{2} \Rightarrow H(e^{\pm j\pi/2}) = 8$$

I have provided here an accurate plot of the amplitude response but in the exam paper an approximate plot based on the above results is considered as a complete answer.



3. (a) The bilinear transformation from the s -plane to the z -plane is given by

$$s = \frac{1 - z^{-1}}{1 + z^{-1}}$$

- (i) Explain using mathematical relations, where each point $s = \sigma + j\Omega$ on the s -plane is mapped on the z -plane through the bilinear transformation. [5]

Answer

$$z = \frac{1 + s}{1 - s}$$

For $s = j\Omega_0$ we have that $z = \frac{1+j\Omega_0}{1-j\Omega_0}$ which has a magnitude equal to 1. This implies that a point on the imaginary axis in the s -plane is mapped onto a point on the unit circle in the z -plane where $|z| = 1$. In the general case, for $s = \sigma_0 + j\Omega_0$

$$z = \frac{1 + \sigma_0 + j\Omega_0}{1 - \sigma_0 - j\Omega_0} \Rightarrow |z|^2 = \frac{(1 + \sigma_0)^2 + \Omega_0^2}{(1 - \sigma_0)^2 + \Omega_0^2}$$

A point in the left half s -plane with $\sigma_0 < 0$ is mapped onto a point inside the unit circle in the z -plane as $|z| < 1$. Likewise, a point in the right half s -plane with $\sigma_0 > 0$ is mapped onto a point outside the unit circle in the z -plane as $|z| > 1$.

- (ii) Prove that the relationship between the continuous-time angular frequency and the discrete-time angular frequency is non-linear. [5]

Answer

The variable s is reduced on the imaginary axis to $s = j\Omega$. The variable z is reduced on the unit circle to $z = e^{-j\omega}$. Since the bilinear transformation maps one plane to the other and vice versa and we have proven that the imaginary axis on the s plane is mapped to the unit circle on the z plane, we can write that:

$$j\Omega = \frac{1-e^{-j\omega}}{1+e^{-j\omega}} = j\tan\left(\frac{\omega}{2}\right) \Rightarrow \Omega = \tan\left(\frac{\omega}{2}\right)$$

which is a non-linear relationship.

- (b) A given real-coefficient, digital IIR lowpass filter has a rational transfer function $H_L(z)$ and a cutoff frequency ω_c . The transfer function of $H_L(z)$ is transformed by replacing z by $F(z) = \frac{az+b}{cz+d}$ to a real highpass rational transfer function $H_H(z) = H_L(F(z))$ of the same order as $H_L(z)$ but different cutoff frequency. By using the constraints $H_H(e^{j\pi}) = H_L(e^{j0}) = 1$ and $H_H(e^{j0}) = H_L(e^{j\pi}) = 0$, derive relationships among the parameters a, b, c, d and explain what type of filter is $F(z)$. [5]

Answer

$$H_H(e^{j0}) = H_L(F(e^{j0})) = H_L(F(1)) = 0$$

$$\text{Therefore, } F(1) = \frac{a+b}{c+d} = e^{j\pi} = -1 \Rightarrow a + b = -c - d$$

$$H_H(e^{j\pi}) = H_L(F(e^{j\pi})) = H_L(F(-1)) = 1$$

$$\text{Therefore, } F(-1) = \frac{-a+b}{-c+d} = 1 \Rightarrow -a + b = -c + d$$

$$\text{Therefore, } b = -c \text{ and } a = -d$$

$$F(z) = \frac{az + b}{-bz - a} = -\frac{az + b}{bz + a}$$

$F(z)$ is an allpass filter.

- (c) Consider the Finite Impulse Response (FIR) filter transfer functions $G_1(z) = \frac{1}{4}(z + 2 + z^{-1})$ and $G_2(z) = \frac{1}{4}(-z + 2 - z^{-1})$. Explain the type of filters $G_1(z)$ and $G_2(z)$ (lowpass etc.), by using the following two approaches:
- Experimental approach. In this approach you will apply the filters to the signal $x[n] = u[n]$, with $u[n]$ the discrete unit step function and observe the effects they have on $x[n]$. [5]

Answer

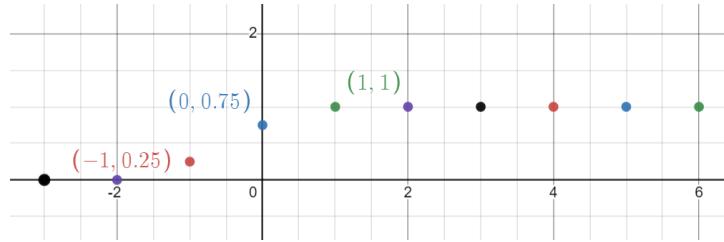
The input-output relationship of the given transfer function $G_1(z)$ is

$$y[n] = \frac{1}{4}(x[n+1] + 2x[n] + x[n-1])$$

If $x[n] = u[n]$, with $u[n]$ the discrete unit step function we have:

$$y[n] = \frac{1}{4}(u[n+1] + 2u[n] + u[n-1])$$

$$y[n] = \begin{cases} 0 & n < -1 \\ 1/4 & n = -1 \\ 3/4 & n = 0 \\ 1 & n \geq 1 \end{cases}$$



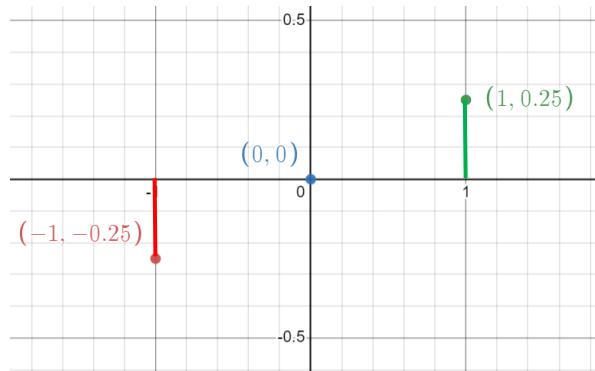
The input-output relationship of the given transfer function $G_2(z)$ is

$$y[n] = \frac{1}{4}(-x[n+1] + 2x[n] - x[n-1])$$

If $x[n] = u[n]$, with $u[n]$ the discrete unit step function we have:

$$y[n] = \frac{1}{4}(-u[n+1] + 2u[n] - u[n-1])$$

$$y[n] = \begin{cases} 0 & n < -1 \\ -1/4 & n = -1 \\ 1/4 & n = 0 \\ 0 & n \geq 1 \end{cases}$$



As we see by applying $u[n]$ as input to $G_1(z)$, $G_1(z)$ is a lowpass filter because the sharpness of $u[n]$ at $n = 0$ is destroyed by applying the filter.

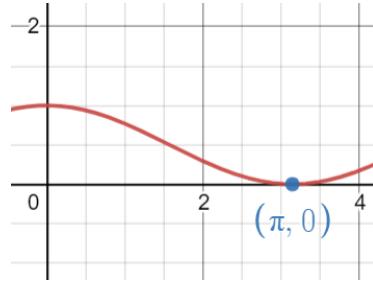
On the other hand, $G_2(z)$ is a highpass filter because we see by applying $u[n]$ as input to $G_2(z)$, the constant areas are eliminated, and we are left only with an enhanced abrupt change around $n = 0$ which is the original abrupt change point.

- (ii) Mathematical approach. In this approach you must find the frequency response of the two filters. [5]

Answer

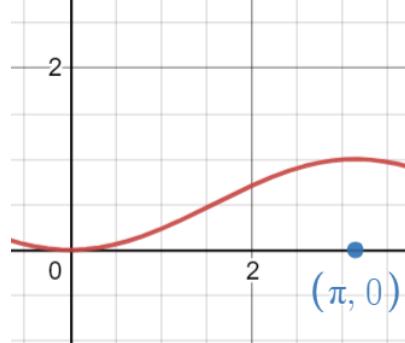
$$G_1(z) = \frac{1}{4}(z + 2 + z^{-1}) = \frac{1}{4}(2 + 2\cos(\omega)) = \frac{1}{2}(1 + \cos(\omega))$$

$|G_1(e^{j\omega})| = \frac{1}{2}|1 + \cos(\omega)|$. We observe that $|G_1(e^{j\omega})|$ decreases as the frequency approaches π .



$$G_2(z) = \frac{1}{4}(-z + 2 - z^{-1}) = \frac{1}{4}(2 - 2\cos(\omega)) = \frac{1}{2}(1 - \cos(\omega))$$

$$|G_2(e^{j\omega})| = \frac{1}{2}|1 - \cos(\omega)|$$



We observe that $|G_2(e^{j\omega})|$ increases as the frequency approaches π .

4. (a) Consider the multirate structure of **Figure 1** below, where $H_0(z)$, $H_1(z)$ and $H_2(z)$ are ideal, zero phase, real-coefficient lowpass, bandpass and highpass filters respectively, with frequency responses as follows:

$$H_0(e^{j\omega}) = u(\omega) - u(\omega - \frac{2\pi}{3})$$

$$H_1(e^{j\omega}) = u(\omega - \frac{\pi}{3}) - u(\omega - \frac{2\pi}{3})$$

$$H_2(e^{j\omega}) = u(\omega - \frac{\pi}{3}) - u(\omega - \pi)$$

The function $u(\omega)$ is the well-known unit step function, defined as

$$u(\omega) = \begin{cases} 1 & \omega \geq 0 \\ 0 & \text{elsewhere} \end{cases}$$

If the input is a real sequence with a Discrete Time Fourier Transform

$$X(e^{j\omega}) = \left(-\frac{3\omega^2}{\pi} + \frac{\pi}{3}\right) \left(u(\omega) - u\left(\omega - \frac{\pi}{3}\right)\right)$$

sketch the Discrete Time Fourier Transform of the outputs $y_0[n]$, $y_1[n]$ and $y_2[n]$.

Notice that all frequency domain representations above are provided only within the range $[0, \pi]$. [15]

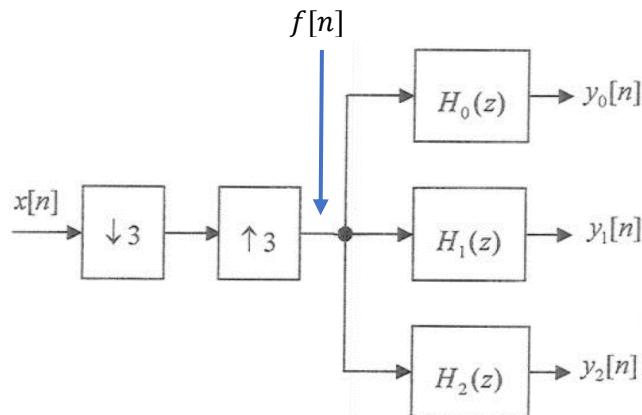
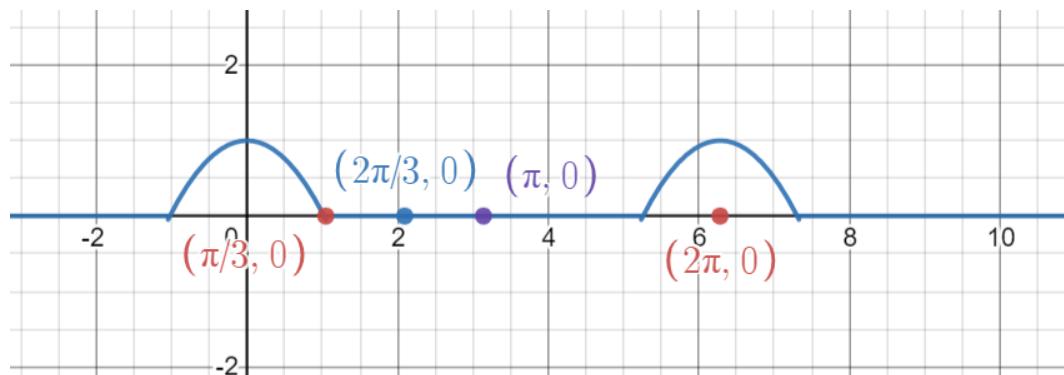


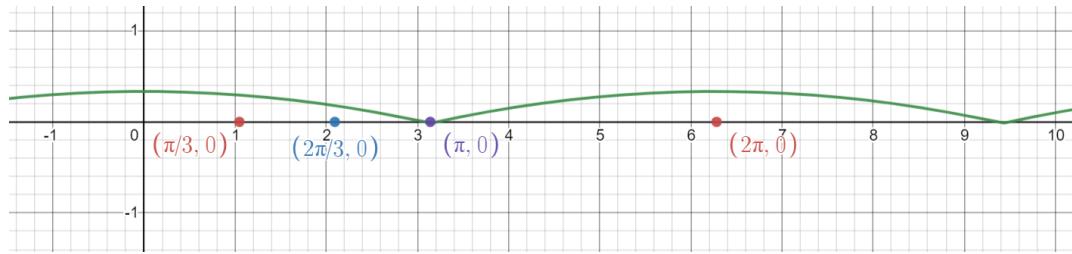
Figure 1

Answer

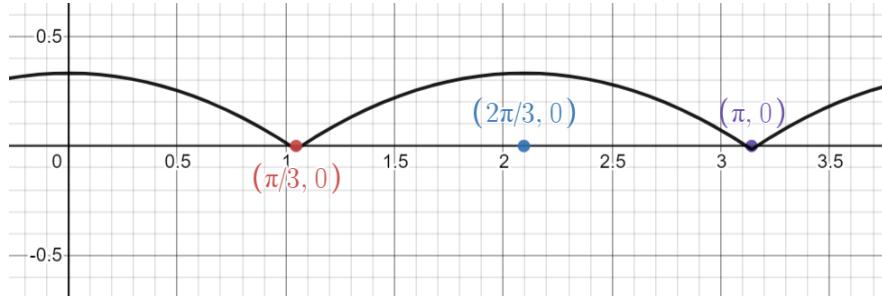
The DTFT of the input is shown below:



After decimation by 3:



After interpolation by 3 we obtain the DTFT of the signal $f[n]$ shown below.



The output of the three filters is obvious.

- (b) Develop an expression for the output $y[n]$ as a function of the input $x[n]$ for the multirate structure of Figure 3 below. [10]

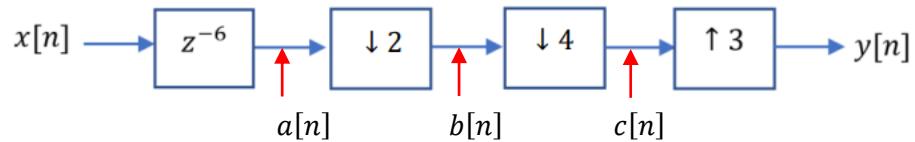


Figure 2

Answer

$$a[n] = x[n - 6]$$

$$b[n] = a[2n]$$

$$c[n] = b[4n] = a[8n] = x[8n - 6]$$

$$y[n] = \begin{cases} x[\frac{8n}{3} - 6] & n \text{ is a multiple of 3} \\ 0 & \text{otherwise} \end{cases}$$

It is important that the answer specifies clearly that the relationship $y[n] = x[\frac{8n}{3} - 6]$ is only valid if n is a multiple of 3. If this is not specified, then the signal given is different.