

1. (a) Consider the causal, complex coefficient transfer function shown below:

$$H_M(z) = \frac{\sum_{n=0}^{M-1} d^*[M-n]z^{-n} + z^{-M}}{1 + \sum_{n=1}^M d[n]z^{-n}}, M > 1 \quad (1)$$

- (i) Show that the transfer function in (1) above is an allpass filter.

[5]

**Answer**

The condition for an allpass transfer function is that  $|H_M(z)| = 1$ , for  $|z| = 1$ , which implies that  $|H_M(e^{j\omega})| = 1$  for all  $\omega$ . The given function is of the form:

$$\begin{aligned} H_M(z) &= \frac{\sum_{n=0}^{M-1} d^*[M-n]z^{-n} + z^{-M}}{1 + \sum_{n=1}^M d[n]z^{-n}} = \frac{\sum_{n=0}^M d^*[M-n]z^{-n}}{\sum_{n=0}^M d[n]z^{-n}}, d^*[0] = 1 \\ &= \frac{z^{-M} \sum_{n=0}^M d^*[M-n]z^{M-n}}{\sum_{n=0}^M d[n]z^{-n}} = \frac{z^{-M} \sum_{r=0}^M d^*[r]z^r}{\sum_{n=0}^M d[n]z^{-n}}, \\ r &= M - n, d^*[0] = 1 \end{aligned}$$

If we denote the denominator polynomial of the allpass function as  $A_M(z)$  with

$$A_M(z) = \sum_{n=0}^M d[n]z^{-n}$$

then it follows that the given  $H_M(z)$  can be written as:

$$H_M(z) = \frac{z^{-M} \bar{A}_M(z^{-1})}{A_M(z)}$$

$\bar{A}_M(z)$  is a polynomial that is obtained from the polynomial  $A_M(z)$  if we complex conjugate the coefficients of  $A_M(z)$  but we make no changes to the variable  $z$ .

For  $z = e^{j\omega}$  we see that  $|H_M(e^{j\omega})| = 1$ . This comes from the fact that  $\bar{A}_M(z^{-1})$  becomes the complex conjugate of  $A_M(z)$  since every term in  $\bar{A}_M(z^{-1})$  is now the complex conjugate of the corresponding term in  $A_M(z)$ . In that case  $|\bar{A}_M(z^{-1})| = |A_M(z)|$  and  $|H_M(e^{j\omega})| = 1$ . Therefore,  $H_M(z)$  is an allpass filter.

**Note that** the coefficients  $d[n]$  are constants and do not change with the location of  $z$ . Furthermore, the coefficients in this particular exercise are complex.

- (ii) Comment on the locations of the zeros and the poles of a causal, real, stable, allpass filter's transfer function within the  $z$  -plane, with respect to the unit circle. Justify your answer.

[5]

**Answer**

We have proven in the lectures that if  $z_0$  is a pole of an allpass filter, then  $1/z_0$  is a zero of the allpass filter. The poles of a causal stable transfer function must lie inside the unit circle. As a result, ALL zeros of a causal stable allpass transfer function lie outside the unit circle in a mirror-image symmetry with its poles situated inside the unit circle.

- (b) Given an allpass filter

$$H(z) = \frac{d + ez + fz^2}{1 + bz + cz^2}$$

with poles at  $\frac{1}{2}$  and  $\frac{1}{3}$ , find  $b, c, d, e, f$ .

[5]

**Answer**

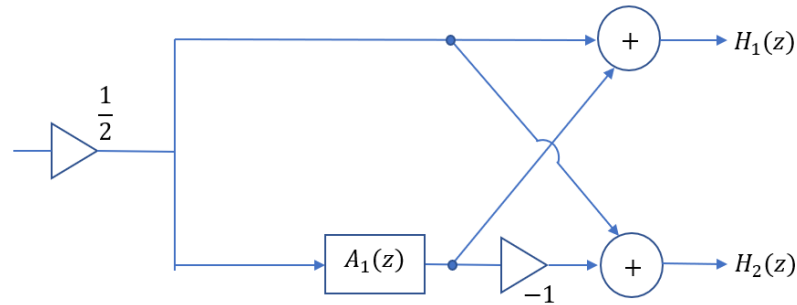
$$1 + bz + cz^2 = c \left( \frac{1}{c} + \frac{b}{c}z + z^2 \right) = c \left( z - \frac{1}{2} \right) \left( z - \frac{1}{3} \right) = c \left( \frac{1}{6} - \frac{5}{6}z + z^2 \right)$$

$$c = 6, b = -5$$

$$H(z) = \frac{d + ez + fz^2}{1 - 5z + 6z^2}$$

and therefore,  $d = 6, e = -5, f = 1$ .

- (c) In the structure below,  $A_1(z)$  is a first-order allpass transfer function. Find the type of filters  $H_1(z)$  and  $H_2(z)$  (lowpass etc.).



[5]

**Answer**

$$H_1(z) = \frac{1}{2}(1 + A_1(z))$$

$$H_1(z) = \frac{1}{2} \left( 1 + \frac{-az+1}{z-a} \right) = \frac{1}{2} \frac{(1-a)(z+1)}{z-a}$$

$$z = 1 \Rightarrow \omega = 0, H_1(1) = 1$$

$$z = -1 \Rightarrow \omega = \pi, H_1(-1) = 0$$

Therefore,  $H_1(z)$  is a lowpass filter.

$$H_2(z) = \frac{1}{2} \left( 1 - \frac{-az+1}{z-a} \right) = \frac{1}{2} \frac{(1+a)(z-1)}{z-a}$$

$$z = 1, H_2(1) = 0$$

$$z = -1, H_2(-1) = 1$$

Therefore,  $H_2(z)$  is a highpass filter.

- (d) Consider the cascade of two causal LTI systems with impulse responses  $h_1[n] = a\delta[n] + b\delta[n-1]$  and  $h_2[n] = c^n u[n]$ ,  $a, b, c$  are real coefficients and  $|c| < 1$ . Determine the frequency response  $H(e^{j\omega})$  of the overall system. Find all the possible sets of values of  $a, b, c$  for which the overall transfer function has an amplitude equal to 1 for all frequencies [5]

**Answer**

$$H(z) = H_1(z)H_2(z) = \frac{(a + bz^{-1})z}{z - c} = \frac{az + b}{z - c}$$

$|H(e^{j\omega})| = 1$  implies that  $H(z)$  is an allpass filter.

$$|H(e^{j\omega})|^2 = \frac{a^2 + b^2 + 2ab\cos(\omega)}{1 + c^2 - 2cc\cos(\omega)}$$

In order for this relationship to be satisfied for every  $\omega$  the following conditions must hold:

1.  $a^2 + b^2 = 1 + c^2$
2.  $ab = -c$

From these two conditions we obtain:

$$a^2 + b^2 = 1 + a^2 b^2, a^2(1 - b^2) = (1 - b^2)$$

If  $b^2 \neq 1$  then  $a^2 = 1$

- $a = 1 \Rightarrow b = -c, H(z) = \frac{z+b}{z+b} = 1$
- $a = -1 \Rightarrow b = c, H(z) = \frac{-z+b}{z-b} = -1$

If  $b^2 = 1$  then

- $b = 1 \Rightarrow a = -c, H(z) = \frac{az+1}{z+a}$
- $b = -1 \Rightarrow a = c, H(z) = \frac{az-1}{z-a}$

Therefore, there are 4 solutions to the problem. Specific values for  $a, b, c$  must be found.

2. (a) Design a length-5 FIR bandpass filter with an antisymmetric impulse response  $h[n]$ , satisfying the following magnitude response values:  $|H(e^{j0.3\pi})| = 0.3$  and  $|H(e^{j0.6\pi})| = 0.8$ . [4]

**Answer**

The generic form of a length-5 FIR bandpass filter with an antisymmetric impulse response  $h[n]$  is given by:

$$\begin{aligned} H(e^{j\omega}) &= h[0] + h[1]e^{-j\omega} + 0e^{-j2\omega} + h[3]e^{-j3\omega} + h[4]e^{-j4\omega} \\ &= h[0] + h[1]e^{-j\omega} - h[1]e^{-j3\omega} - h[0]e^{-j4\omega} \\ &= e^{-j2\omega}[h[0](e^{j2\omega} - e^{-j2\omega}) + h[1](e^{j\omega} - e^{-j\omega})] \\ &= 2je^{-j2\omega}[h[0]\sin(2\omega) + h[1]\sin(\omega)] \end{aligned}$$

$$|H(e^{j\omega})| = 2[h[0]\sin(2\omega) + h[1]\sin(\omega)]$$

Thus,

$$|H(e^{j0.3})| = 2[h[0]\sin(0.6\pi) + h[1]\sin(0.3\pi)] = 0.3$$

$$|H(e^{j0.6})| = 2[h[0]\sin(1.2\pi) + h[1]\sin(0.6\pi)] = 0.8$$

Solving these two equations we get:

$$h[0] = -0.133 \text{ and } h[1] = 0.34$$

As we see here, we have only two unknown coefficients due to the condition of anti-symmetry and for that reason we are given two pieces of information so that we are able to form two equations with two unknowns and solve them.

- (b) We have shown that a real-coefficient FIR transfer function  $H(z)$  with a symmetric impulse response has a linear phase response. As a result, the all-pole IIR transfer function  $G(z) = \frac{1}{H(z)}$  will also have a linear-phase response. What are the practical difficulties in implementing  $G(z)$ ? Justify your answer. [4]

**Answer**

$G(z)$  must have poles outside the unit circle making it unstable.

- (c) A simple averaging filter is defined by the following input-output relationship:

$$y[n] = \frac{1}{N}(x[n] + x[n-1] + \dots + x[n-(N-1)])$$

- (i) Let  $N = 4$ . Determine the filter's transfer function and its zeros and poles. [3]

[Hint: You may use the relationship  $\sum_{i=0}^{N-1} z^{-i} = \frac{1-z^{-N}}{1-z^{-1}}$ ,  $z \neq 1$ .]

**Answer**

$$\begin{aligned} Y(z) &= \frac{1}{N}[1 + z^{-1} + \dots + z^{-(N-1)}]X(z) = H(z)X(z) \\ H(z) &= \frac{1}{N} \frac{1 - z^{-N}}{1 - z^{-1}} = \frac{1}{N} \frac{z^N(1 - z^{-N})}{z^{N-1}z(1 - z^{-1})} = \frac{1}{N} \frac{1 - z^{-N}}{z^{N-1}(z - 1)} \end{aligned}$$

$$\text{For } N = 4 \text{ we have } H(z) = \frac{1}{4} \frac{1 - z^{-4}}{z^3(z - 1)}$$

$$z^4 - 1 = 0 \Rightarrow z^4 = 1 \Rightarrow z^2 = \pm 1$$

$$z^2 = 1 \Rightarrow z = \pm 1$$

$$z^2 = -1 \Rightarrow z = \pm j$$

The zero at 1 is cancelled with the pole at 1.

Therefore, we have zeros at  $-1, \pm j$  and a triple pole at 0.

- (ii) Determine a general form for zeros and poles for any  $N$ .

[3]

**Answer**

$$H(z) = \frac{1}{N} \frac{1}{z^{N-1}} \frac{z^N - 1}{z - 1}$$

Zeros are found from  $z^N - 1 = 0 \Rightarrow z^N = 1 \Rightarrow z = e^{j\frac{2\pi k}{N}}, k = 0, \dots, N-1$

Poles at  $z = 0$  with multiplicity  $N-1$  and a pole at  $z = 1$  which is cancelled by the zero at  $z = 1$ .

Therefore, zeros are at  $z = e^{j\frac{2\pi k}{N}}, k = 1, \dots, N-1$ .

- (iii) A recursive implementation of a filter refers to writing the current output as a function of the previous output and the current and past inputs. By comparing  $y[n]$  and  $y[n-1]$  determine a recursive implementation of the filter. [3]

**Answer**

$$y[n-1] = \frac{1}{N} (x[n-1] + x[n-2] + \dots + x[n-1-(N-1)])$$

$$y[n] = \frac{1}{N} (x[n] + x[n-1] + \dots + x[n-(N-1)])$$

$$y[n] - y[n-1] = \frac{1}{N} (x[n] - x[n-1-(N-1)]) \Rightarrow$$

$$y[n] - y[n-1] = \frac{1}{N} (x[n] - x[n-N])$$

We observe that the current output is a function of the previous output, the current input and the input that is distanced by  $N$  samples.

- (d) An FIR digital filter has the transfer function

$$H(z) = (1 - z^{-1})^3 (1 + z^{-1})^3$$

- (i) Sketch the pole-zero diagram of this system.

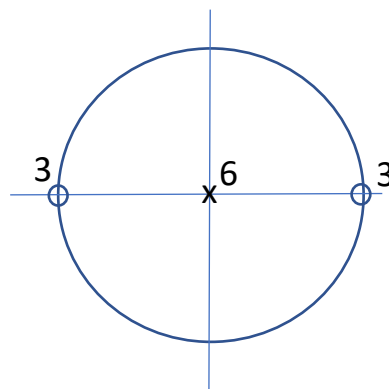
[4]

**Answer**

Using polynomial expansion, we obtain

$$H(z) = \frac{(z-1)^3 (z+1)^3}{z^6}$$

We see that we have 3 zeros at 1, 3 zeros at  $-1$  and 6 poles at 0



- (ii) Sketch **roughly** the amplitude response of the above filter. Would you classify this as a low-pass, high-pass, band-pass, or band-stop filter? Please briefly explain. [4]

**Answer**

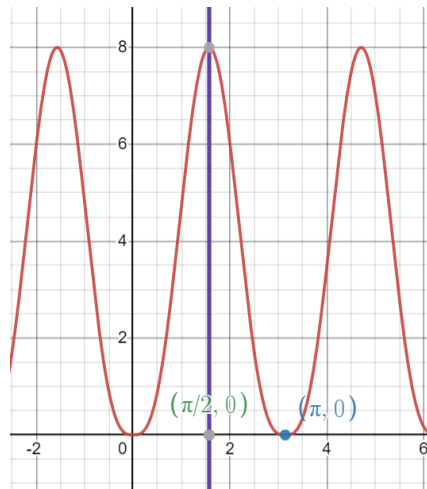
This is the Type 3 linear phase filter it can only be band pass. This answer is not complete. To prove the statement by using the expression given we see that:

$$z = 1 \Rightarrow \omega = 0 \Rightarrow H(e^{j\omega}) = 0$$

$$z = -1 \Rightarrow \omega = \pi \Rightarrow H(e^{j\pi}) = 0$$

$$z = \pm j \Rightarrow \omega = \frac{\pi}{2} \Rightarrow H(e^{\pm j\pi/2}) = 8$$

I have provided here an accurate plot of the amplitude response but in the exam paper an approximate plot based on the above results is considered as a complete answer.



3. (a) The bilinear transformation from the  $s$  -plane to the  $z$  -plane is given by

$$s = \frac{1 - z^{-1}}{1 + z^{-1}}$$

- (i) Explain using mathematical relations, where each point  $s = \sigma + j\Omega$  on the  $s$  -plane is mapped on the  $z$  -plane through the bilinear transformation. [5]

**Answer**

$$z = \frac{1 + s}{1 - s}$$

For  $s = j\Omega_0$  we have that  $z = \frac{1+j\Omega_0}{1-j\Omega_0}$  which has a magnitude equal to 1. This implies that a point on the imaginary axis in the  $s$  -plane is mapped onto a point on the unit circle in the  $z$  -plane where  $|z| = 1$ . In the general case, for  $s = \sigma_0 + j\Omega_0$

$$z = \frac{1 + \sigma_0 + j\Omega_0}{1 - \sigma_0 - j\Omega_0} \Rightarrow |z|^2 = \frac{(1 + \sigma_0)^2 + \Omega_0^2}{(1 - \sigma_0)^2 + \Omega_0^2}$$

A point in the left half  $s$  -plane with  $\sigma_0 < 0$  is mapped onto a point inside the unit circle in the  $z$  -plane as  $|z| < 1$ . Likewise, a point in the right half  $s$  -plane with  $\sigma_0 > 0$  is mapped onto a point outside the unit circle in the  $z$  -plane as  $|z| > 1$ .

- (ii) Prove that the relationship between the continuous-time angular frequency and the discrete-time angular frequency is non-linear. [5]

**Answer**

The variable  $s$  is reduced on the imaginary axis to  $s = j\Omega$ . The variable  $z$  is reduced on the unit circle to  $z = e^{-j\omega}$ . Since the bilinear transformation maps one plane to the other and vice versa and we have proven that the imaginary axis on the  $s$  plane is mapped to the unit circle on the  $z$  plane, we can write that:

$$j\Omega = \frac{1 - e^{-j\omega}}{1 + e^{-j\omega}} = j \tan\left(\frac{\omega}{2}\right) \Rightarrow \Omega = \tan\left(\frac{\omega}{2}\right) \text{ which is a non-linear relationship.}$$

- (b) A given real-coefficient, digital IIR lowpass filter has a rational transfer function  $H_L(z)$  and a cutoff frequency  $\omega_c$ . The transfer function of  $H_L(z)$  is transformed by replacing  $z$  by  $F(z) = \frac{az+b}{cz+d}$  to a real highpass rational transfer function  $H_H(z) = H_L(F(z))$  of the same order as  $H_L(z)$  but different cutoff frequency. By using the constraints  $H_H(e^{j\pi}) = H_L(e^{j0}) = 1$  and  $H_H(e^{j0}) = H_L(e^{j\pi}) = 0$ , derive relationships among the parameters  $a, b, c, d$  and explain what type of filter is  $F(z)$ . [5]

**Answer**

$$H_H(e^{j0}) = H_L(F(e^{j0})) = H_L(F(1)) = 0$$

$$\text{Therefore, } F(1) = \frac{a+b}{c+d} = e^{j\pi} = -1 \Rightarrow a + b = -c - d$$

$$H_H(e^{j\pi}) = H_L(F(e^{j\pi})) = H_L(F(-1)) = 1$$

$$\text{Therefore, } F(-1) = \frac{-a+b}{-c+d} = 1 \Rightarrow -a + b = -c + d$$

$$\text{Therefore, } b = -c \text{ and } a = -d$$

$$F(z) = \frac{az + b}{-bz - a} = -\frac{az + b}{bz + a}$$

$F(z)$  is an allpass filter.

- (c) Consider the Finite Impulse Response (FIR) filter transfer functions  $G_1(z) = \frac{1}{4}(z + 2 + z^{-1})$  and  $G_2(z) = \frac{1}{4}(-z + 2 - z^{-1})$ . Explain the type of filters  $G_1(z)$  and  $G_2(z)$  (lowpass etc.), by using the following two approaches:

- (i) Experimental approach. In this approach you will apply the filters to the signal  $x[n] = u[n]$ , with  $u[n]$  the discrete unit step function and observe the effects they have on  $x[n]$ . [5]

### Answer

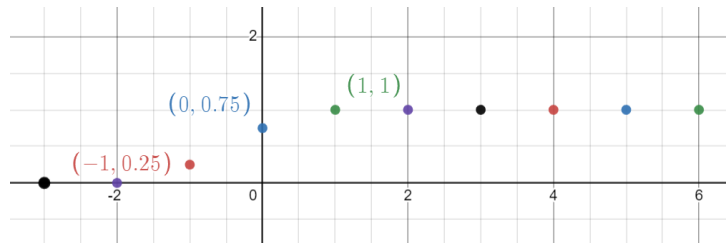
The input-output relationship of the given transfer function  $G_1(z)$  is

$$y[n] = \frac{1}{4}(x[n+1] + 2x[n] + x[n-1])$$

If  $x[n] = u[n]$ , with  $u[n]$  the discrete unit step function we have:

$$y[n] = \frac{1}{4}(u[n+1] + 2u[n] + u[n-1])$$

$$y[n] = \begin{cases} 0 & n < -1 \\ 1/4 & n = -1 \\ 3/4 & n = 0 \\ 1 & n \geq 1 \end{cases}$$



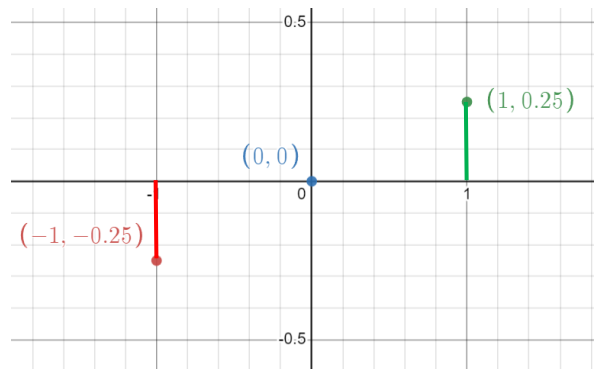
The input-output relationship of the given transfer function  $G_2(z)$  is

$$y[n] = \frac{1}{4}(-x[n+1] + 2x[n] - x[n-1])$$

If  $x[n] = u[n]$ , with  $u[n]$  the discrete unit step function we have:

$$y[n] = \frac{1}{4}(-u[n+1] + 2u[n] - u[n-1])$$

$$y[n] = \begin{cases} 0 & n < -1 \\ -1/4 & n = -1 \\ 1/4 & n = 0 \\ 0 & n \geq 1 \end{cases}$$



As we see by applying  $u[n]$  as input to  $G_1(z)$ ,  $G_1(z)$  is a lowpass filter because the sharpness of  $u[n]$  at  $n = 0$  is destroyed by applying the filter.



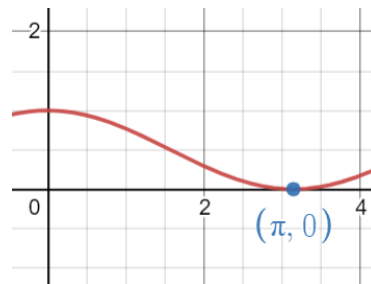
On the other hand,  $G_2(z)$  is a highpass filter because we see by applying  $u[n]$  as input to  $G_2(z)$ , the constant areas are eliminated, and we are left only with an enhanced abrupt change around  $n = 0$  which is the original abrupt change point.

- (ii) Mathematical approach. In this approach you must find the frequency response of the two filters. [5]

**Answer**

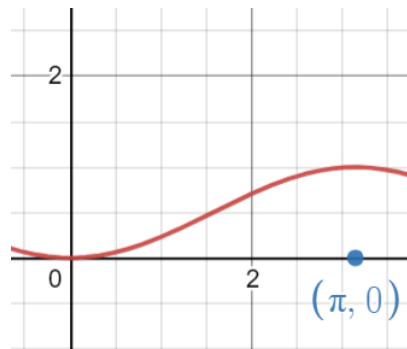
$$G_1(z) = \frac{1}{4}(z + 2 + z^{-1}) = \frac{1}{4}(2 + 2\cos(\omega)) = \frac{1}{2}(1 + \cos(\omega))$$

$|G_1(e^{j\omega})| = \frac{1}{2}|1 + \cos(\omega)|$ . We observe that  $|G_1(e^{j\omega})|$  decreases as the frequency approaches  $\pi$ .



$$G_2(z) = \frac{1}{4}(-z + 2 - z^{-1}) = \frac{1}{4}(2 - 2\cos(\omega)) = \frac{1}{2}(1 - \cos(\omega))$$

$$|G_2(e^{j\omega})| = \frac{1}{2}|1 - \cos(\omega)|$$



We observe that  $|G_2(e^{j\omega})|$  increases as the frequency approaches  $\pi$ .

4. (a) Consider the multirate structure of **Figure 1** below, where  $H_0(z)$ ,  $H_1(z)$  and  $H_2(z)$  are ideal, zero phase, real-coefficient lowpass, bandpass and highpass filters respectively, with frequency responses as follows:

$$H_0(e^{j\omega}) = u(\omega) - u(\omega - \frac{2\pi}{3})$$

$$H_1(e^{j\omega}) = u(\omega - \frac{\pi}{3}) - u(\omega - \frac{2\pi}{3})$$

$$H_2(e^{j\omega}) = u(\omega - \frac{\pi}{3}) - u(\omega - \pi)$$

The function  $u(\omega)$  is the well-known unit step function, defined as

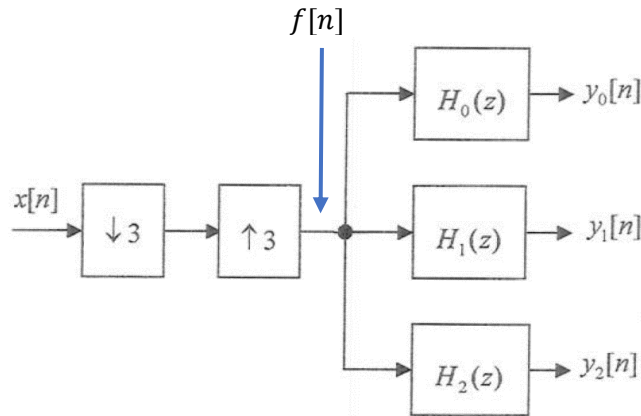
$$u(\omega) = \begin{cases} 1 & \omega \geq 0 \\ 0 & \text{elsewhere} \end{cases}$$

If the input is a real sequence with a Discrete Time Fourier Transform

$$X(e^{j\omega}) = (-\frac{3\omega^2}{\pi} + \frac{\pi}{3}) \left( u(\omega) - u(\omega - \frac{\pi}{3}) \right)$$

sketch the Discrete Time Fourier Transform of the outputs  $y_0[n]$ ,  $y_1[n]$  and  $y_2[n]$ .

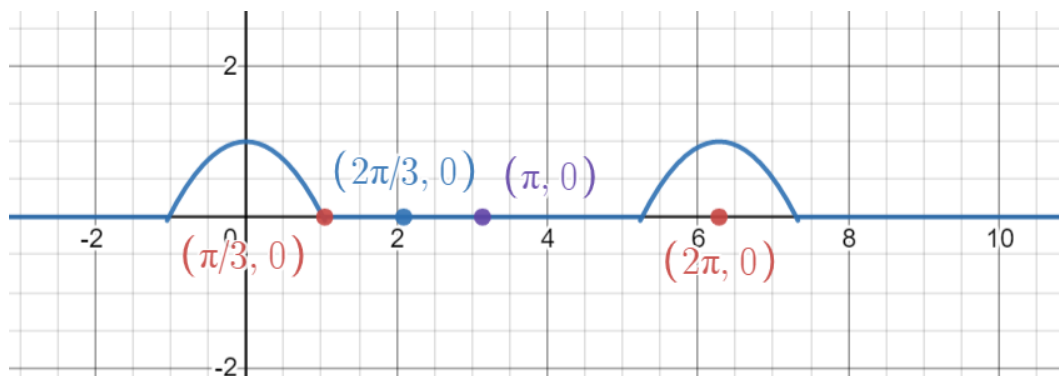
Notice that all frequency domain representations above are provided only within the range  $[0, \pi]$ . [15]



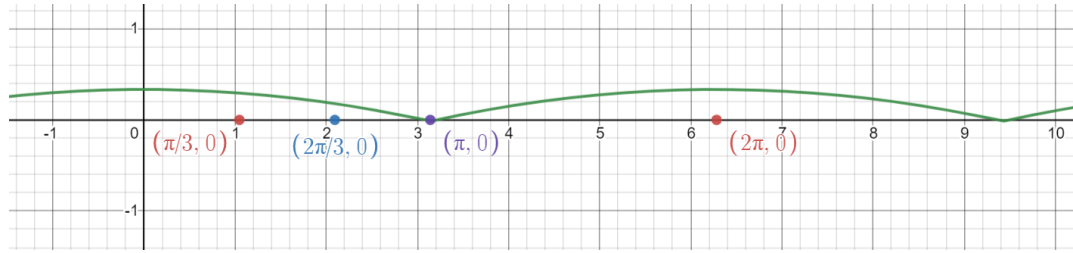
**Figure 1**

**Answer**

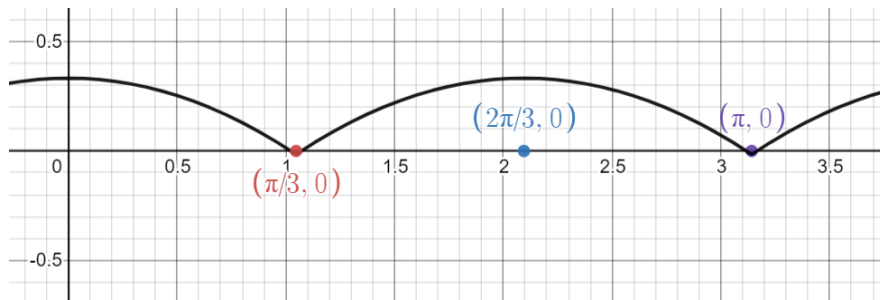
The DTFT of the input is shown below:



After decimation by 3:



After interpolation by 3 we obtain the DTFT of the signal  $f[n]$  shown below.



The output of the three filters is obvious.

- (b) Develop an expression for the output  $y[n]$  as a function of the input  $x[n]$  for the multirate structure of Figure 3 below. [10]

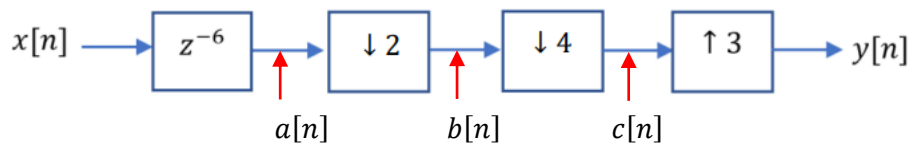


Figure 2

**Answer**

$$a[n] = x[n - 6]$$

$$b[n] = a[2n]$$

$$c[n] = b[4n] = a[8n] = x[8n - 6]$$

$$y[n] = \begin{cases} x[\frac{8n}{3} - 6] & n \text{ is a multiple of 3} \\ 0 & \text{otherwise} \end{cases}$$

It is important that the answer specifies clearly that the relationship  $y[n] = x[\frac{8n}{3} - 6]$  is only valid if  $n$  is a multiple of 3. If this is not specified, then the signal given is different.