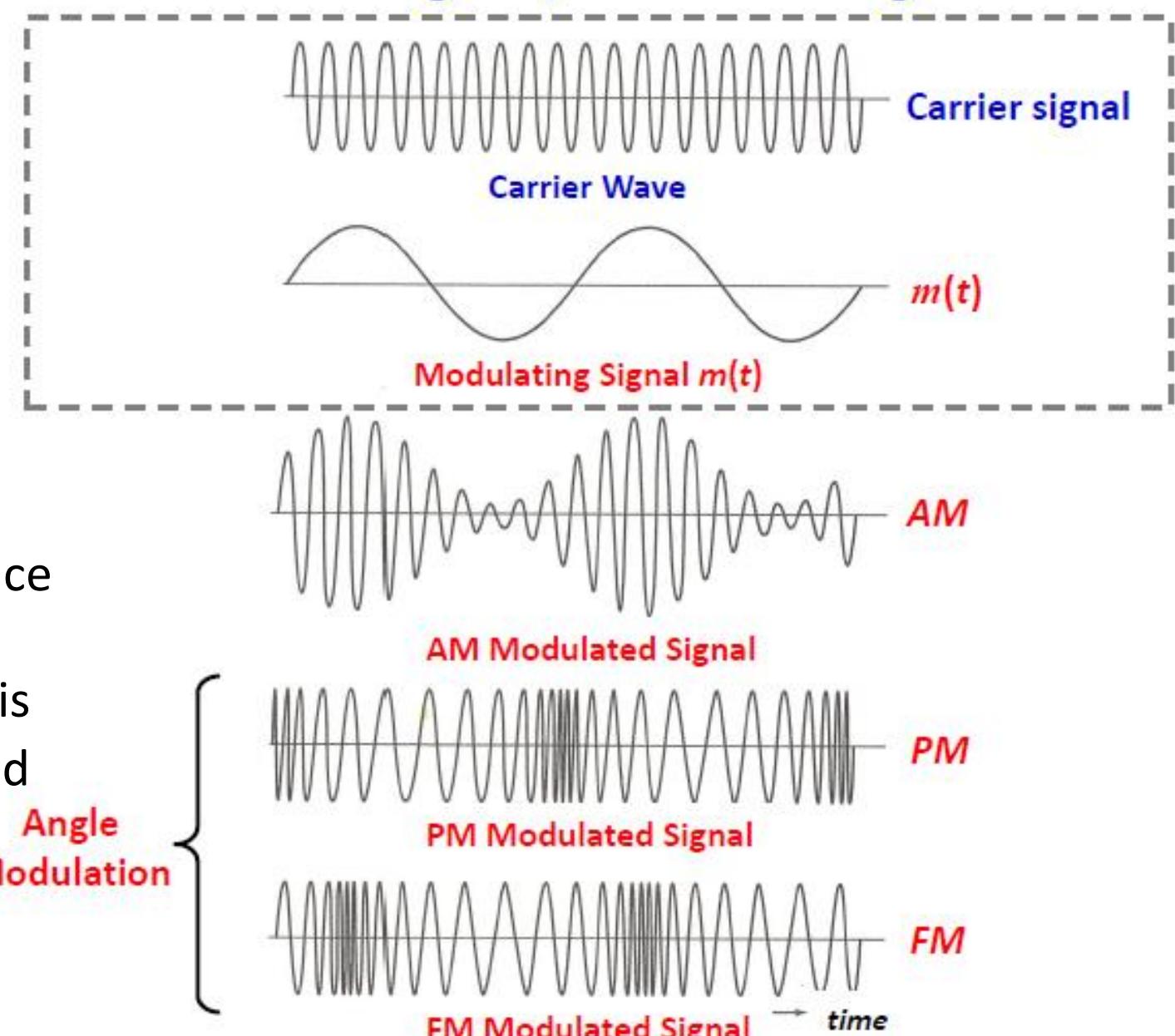


EE 361  
**Communication Theory**

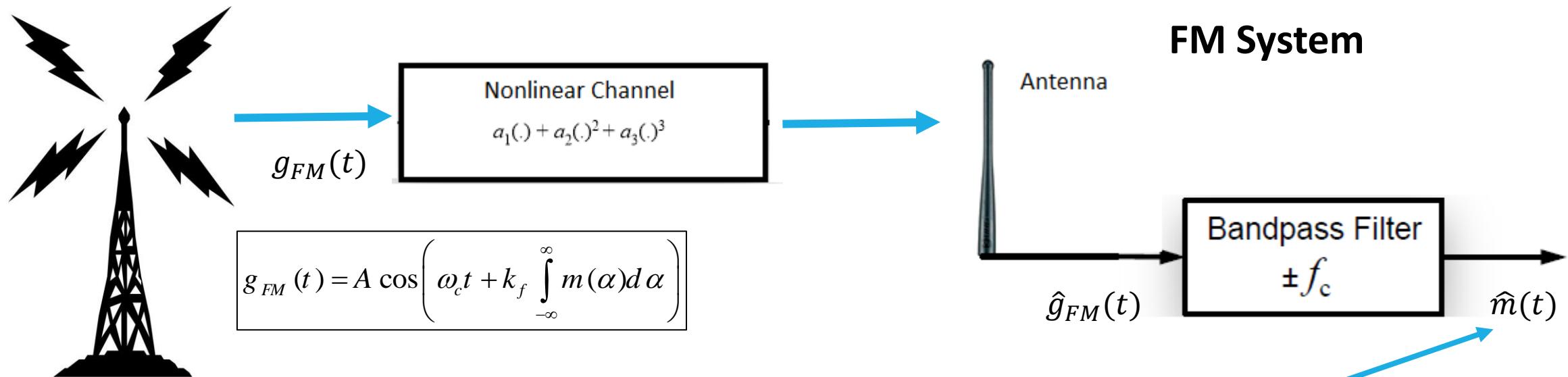
**Chapter 4  
Angle Modulation  
Part 13**

## Illustrating AM, PM and FM Signals

- Previously
  - Demodulation of FM
- Today
  - Effect of Non-linearity on FM signals
  - Effect of Noise and Interference on FM signals
  - Preemphasis and De-emphasis
  - Stereophonic FM Transmit and Receiver

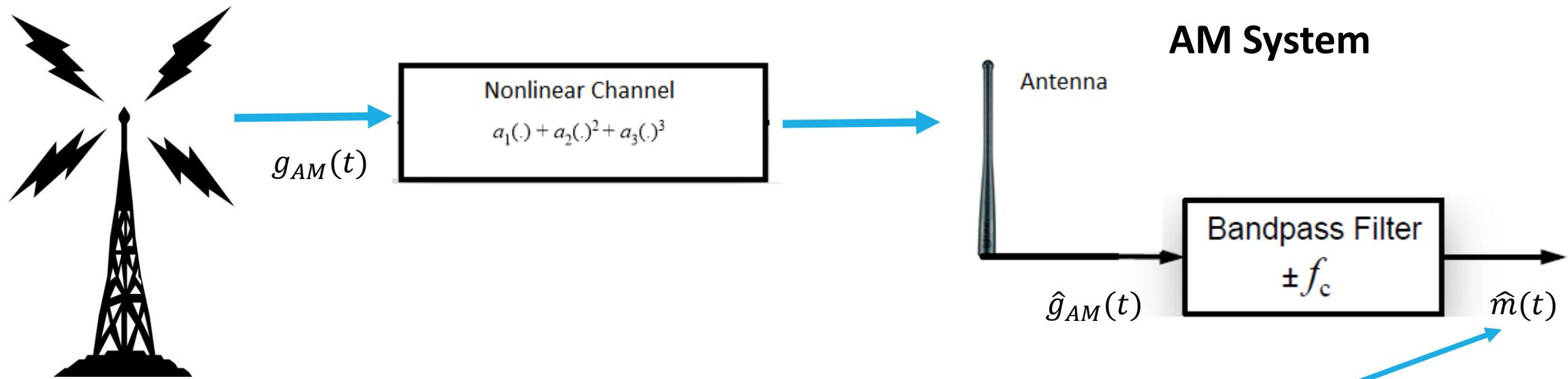


# Effect of Non-Linearity: FM Versus AM



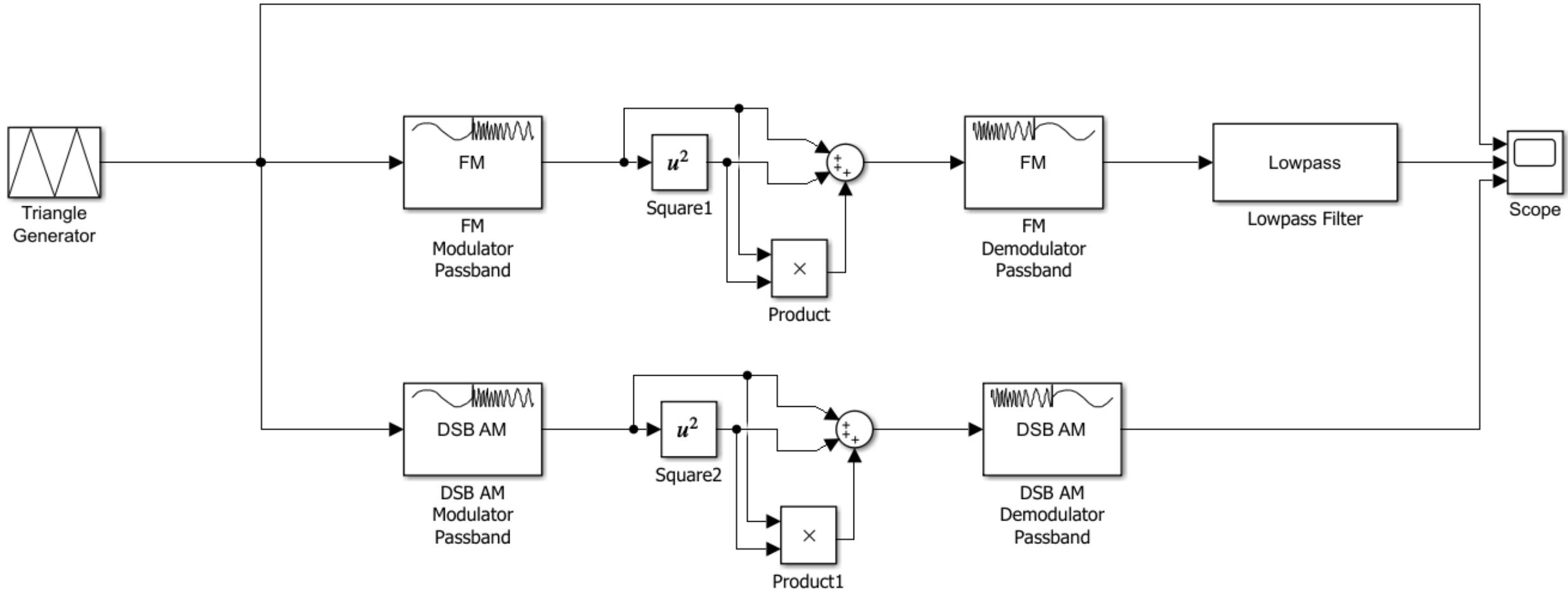
$$\begin{aligned}
 \hat{g}_{FM}(t) &= a_1 A \cos\left(\omega_c t + k_f \int_{-\infty}^{\infty} m(\alpha) d\alpha\right) + a_2 \left[ A \cos\left(\omega_c t + k_f \int_{-\infty}^{\infty} m(\alpha) d\alpha\right) \right]^2 + a_3 \left[ A \cos\left(\omega_c t + k_f \int_{-\infty}^{\infty} m(\alpha) d\alpha\right) \right]^3 \\
 &= a_1 A \cos\left(\omega_c t + k_f \int_{-\infty}^{\infty} m(\alpha) d\alpha\right) + \frac{a_2 A}{2} \left[ 1 + \cos\left(2\omega_c t + 2k_f \int_{-\infty}^{\infty} m(\alpha) d\alpha\right) \right] + \frac{a_3 A}{2} \left[ 1 + \cos\left(2\omega_c t + 2k_f \int_{-\infty}^{\infty} m(\alpha) d\alpha\right) \right] \cos\left(\omega_c t + k_f \int_{-\infty}^{\infty} m(\alpha) d\alpha\right) \\
 &= \underbrace{\frac{a_2 A}{2} + \left[ a_1 A + \frac{3a_3 A}{4} \right]}_{DC} \cos\left(\omega_c t + k_f \int_{-\infty}^{\infty} m(\alpha) d\alpha\right) + \underbrace{\frac{a_2 A}{2} \cos\left(2\omega_c t + 2k_f \int_{-\infty}^{\infty} m(\alpha) d\alpha\right)}_{\text{Around } 2\omega_c \text{ with } k_f \rightarrow 2k_f} + \underbrace{\frac{a_3 A}{4} \cos\left(3\omega_c t + 3k_f \int_{-\infty}^{\infty} m(\alpha) d\alpha\right)}_{\text{Around } 3\omega_c \text{ with } k_f \rightarrow 3k_f}
 \end{aligned}$$

# Effect of Non-Linearity: FM Versus AM

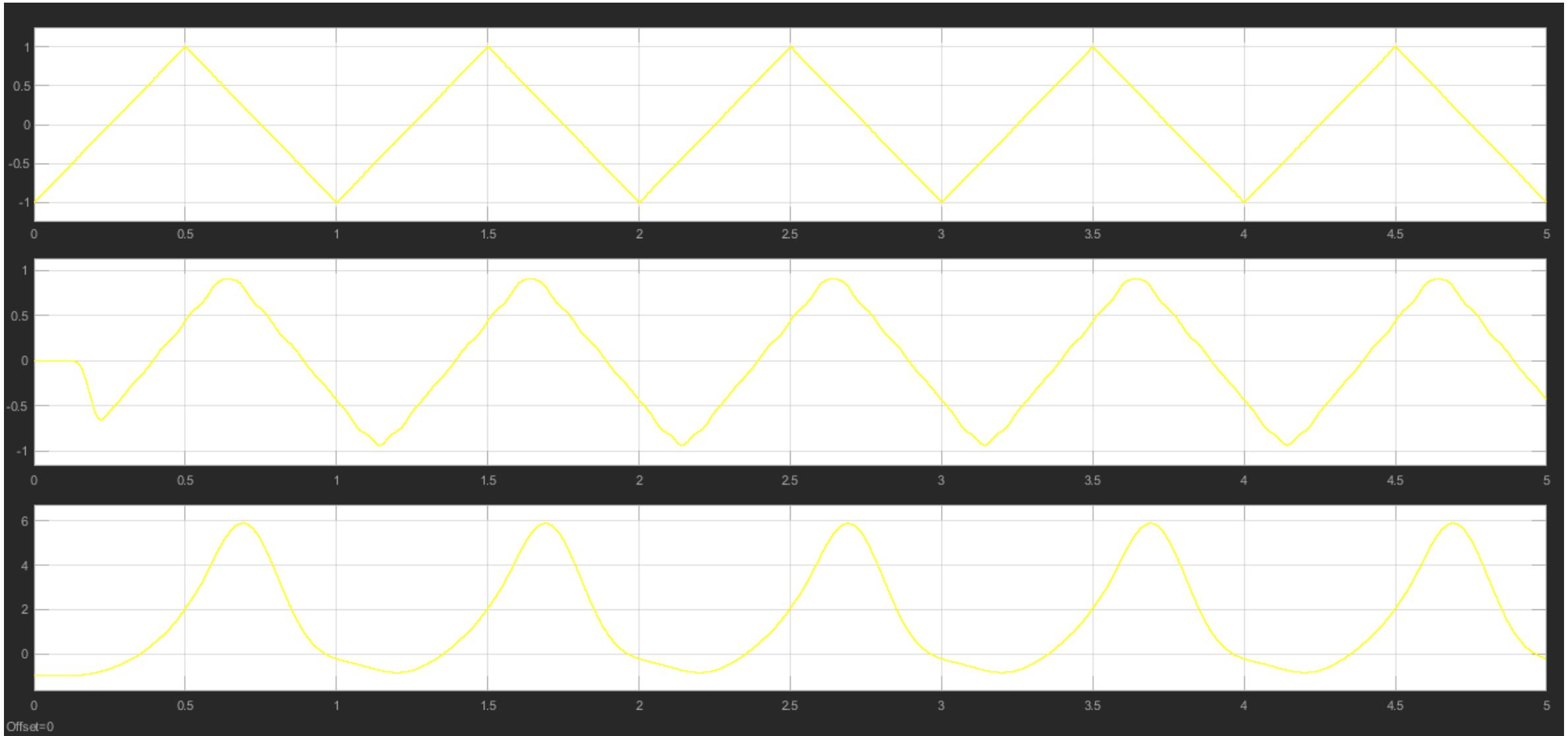


$$\begin{aligned}
 \hat{g}_{AM}(t) &= a_1 m(t) \cdot \cos(\omega_c t) + a_2 [m(t) \cdot \cos(\omega_c t)]^2 + a_3 [m(t) \cdot \cos(\omega_c t)]^3 \\
 &= a_1 m(t) \cdot \cos(\omega_c t) + \frac{a_2 m^2(t)}{2} [1 + \cos(2\omega_c t)] + \frac{a_3 m^3(t)}{2} \cdot \cos(\omega_c t) [1 + \cos(2\omega_c t)] \\
 &= \underbrace{\frac{a_2 m^2(t)}{2}}_{\text{Around } 0} + \underbrace{\left[ a_1 m(t) + \frac{3a_3 m^3(t)}{4} \right]}_{\text{Around } \omega_c} \cdot \cos(\omega_c t) + \underbrace{\frac{a_2 m^2(t)}{2} \cos(2\omega_c t)}_{\text{Around } 2\omega_c} + \underbrace{\frac{a_3 m^3(t)}{4} \cdot \cos(3\omega_c t)}_{\text{Around } 3\omega_c}
 \end{aligned}$$

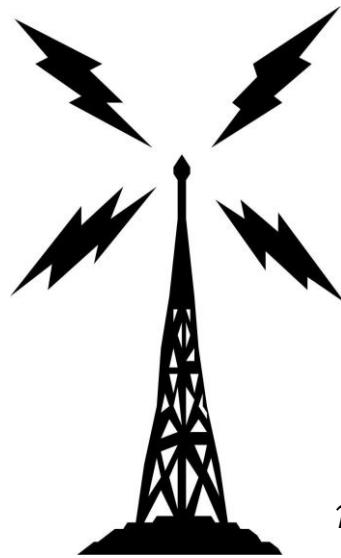
# Effect of Non-Linearity: FM Versus AM



# Effect of Non-Linearity: FM Versus AM



# Effect of Interference on FM System



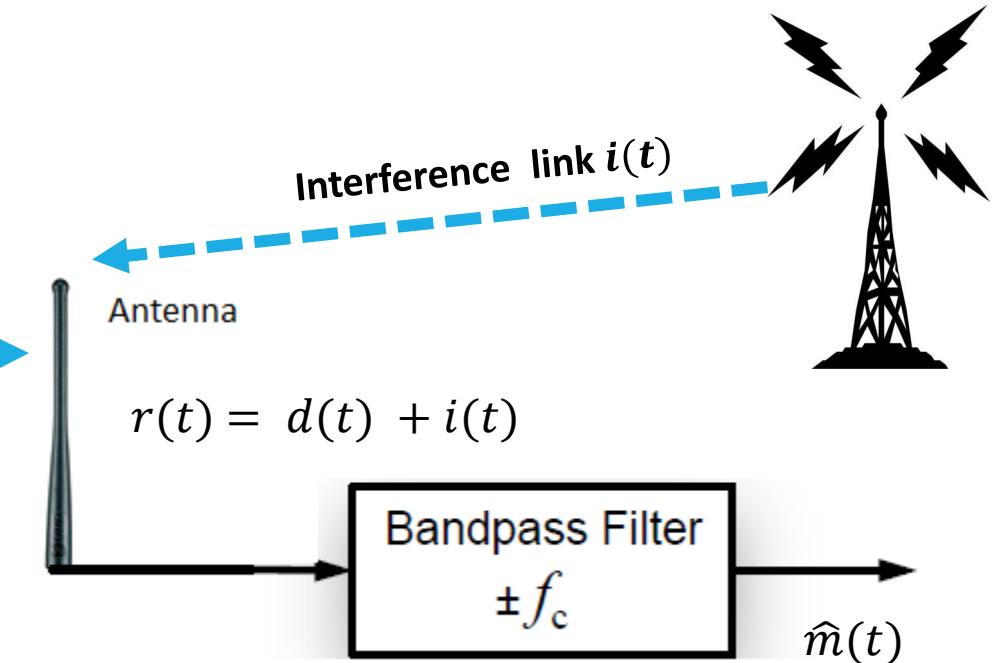
Desired Link  $d(t)$

$$d(t) = A \cos(\omega_c t); \\ i(t) = I \cos((\omega_c + \omega)t)$$

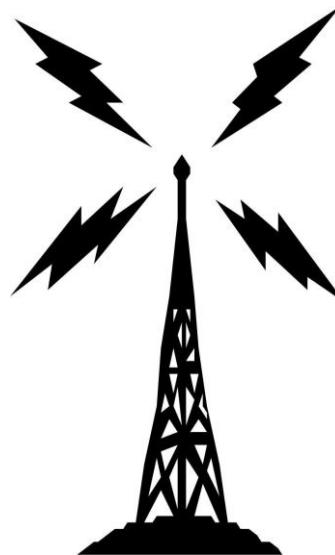
$$\begin{aligned} r(t) &= A \cos(\omega_c t) + I \cos((\omega_c + \omega)t) \\ &= A \cos(\omega_c t) + I \cos(\omega_c t) \cos(\omega t) - I \sin(\omega_c t) \sin(\omega t) \\ &= (A + I \cos(\omega t)) \cos(\omega_c t) - I \sin(\omega t) \sin(\omega_c t) \\ &= E(t) \cos(\omega_c t + \Phi(t)) \end{aligned}$$

$$E(t) = \sqrt{(A + I \cos(\omega t))^2 + (I \sin(\omega t))^2} \quad \% \text{ Envelop}$$

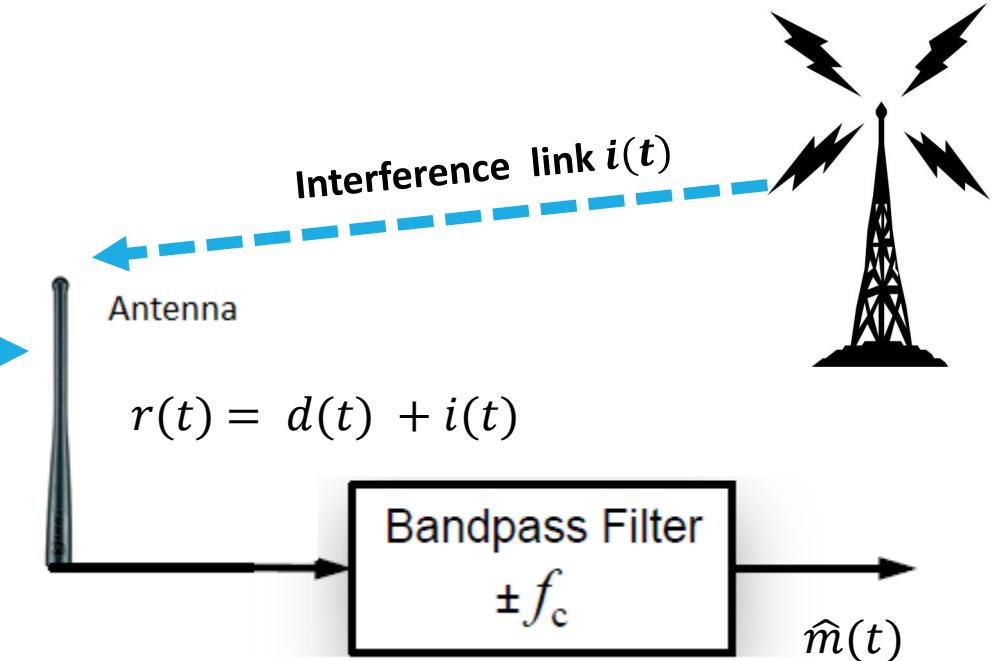
$$\Phi(t) = \tan^{-1} \left( \frac{I \sin(\omega t)}{A + I \cos(\omega t)} \right) \quad \% \text{ Phase}$$



## Effect of Interference on PM and FM System



Desired Link  $d(t)$



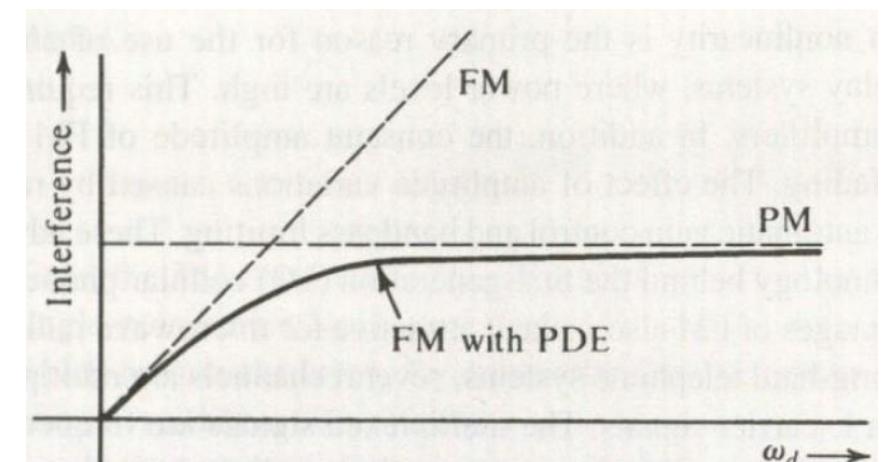
Considering that Interference signal is weak as compared to desired signal, i.e.,  $I \ll A$ , then

$$\begin{aligned}\Phi(t) &= \tan^{-1} \left( \frac{I \sin(\omega t)}{A + I \cos(\omega t)} \right) \\ &\approx \frac{I}{A} \sin(\omega t) \quad \tan^{-1} x = x - \frac{x^3}{3} + \frac{x^5}{5} - \frac{x^7}{7} + \dots \quad |x| \ll 1\end{aligned}$$

Therefore;

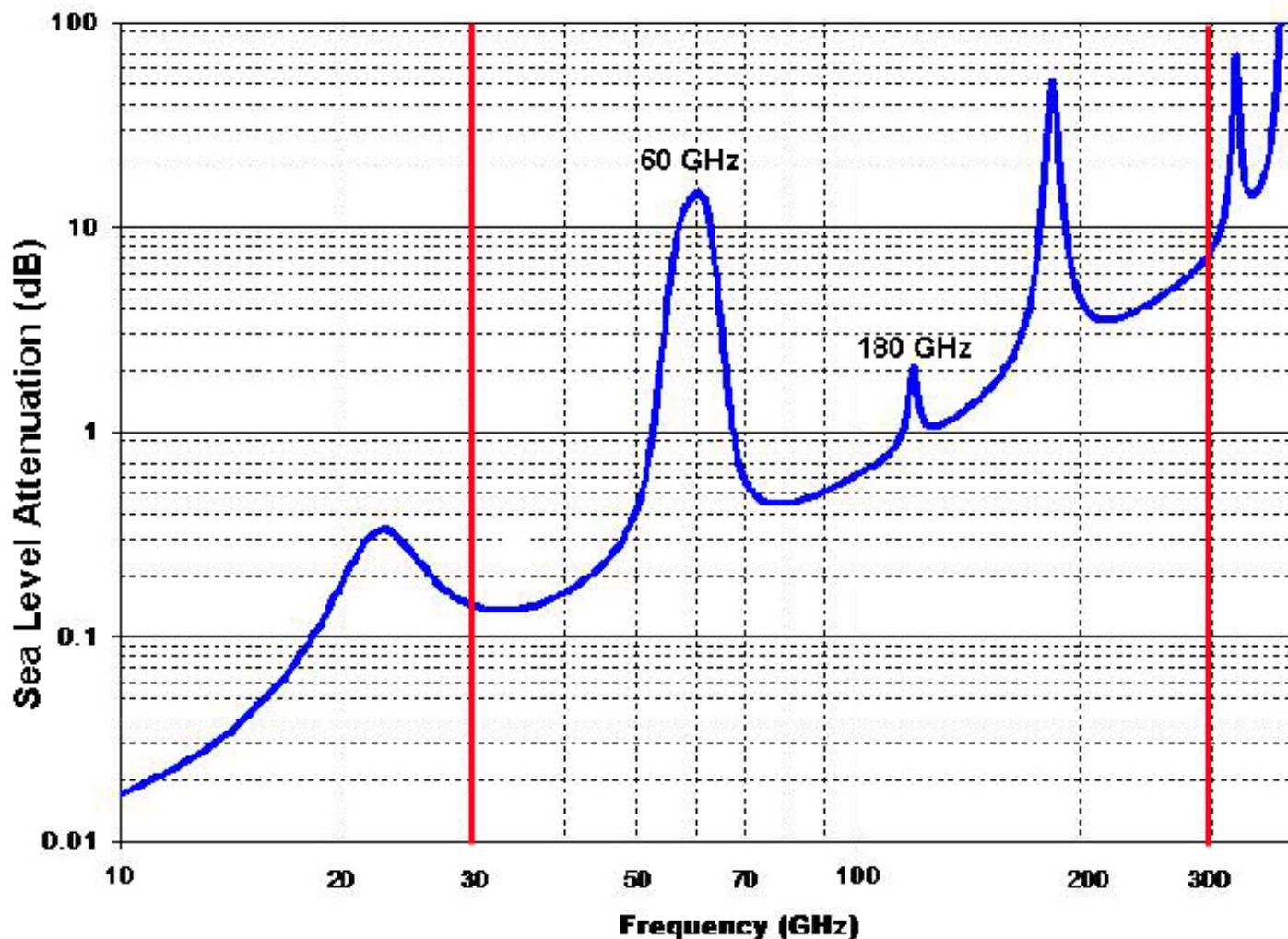
$$\hat{g}_{PM}(t) \approx \cos \left( \omega_c t + \frac{I}{A} \sin(\omega t) \right) \quad \% \text{ For PM direct use } \Phi(t)$$

$$\hat{g}_{FM}(t) \approx \cos \left( \omega_c t + \frac{I\omega}{A} \cos(\omega t) \right) \quad \% \text{ For FM use } \frac{d}{dt} \Phi(t)$$



# FM Broadcast Preemphasis and Deemphasis filtering

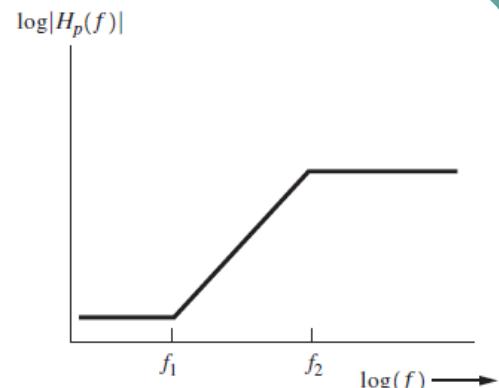
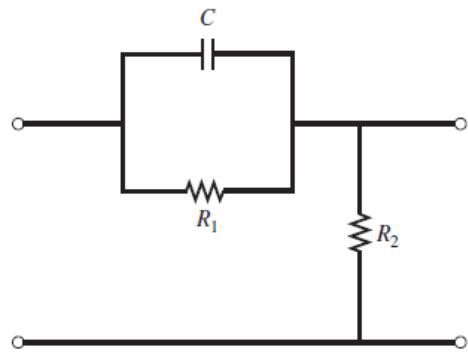
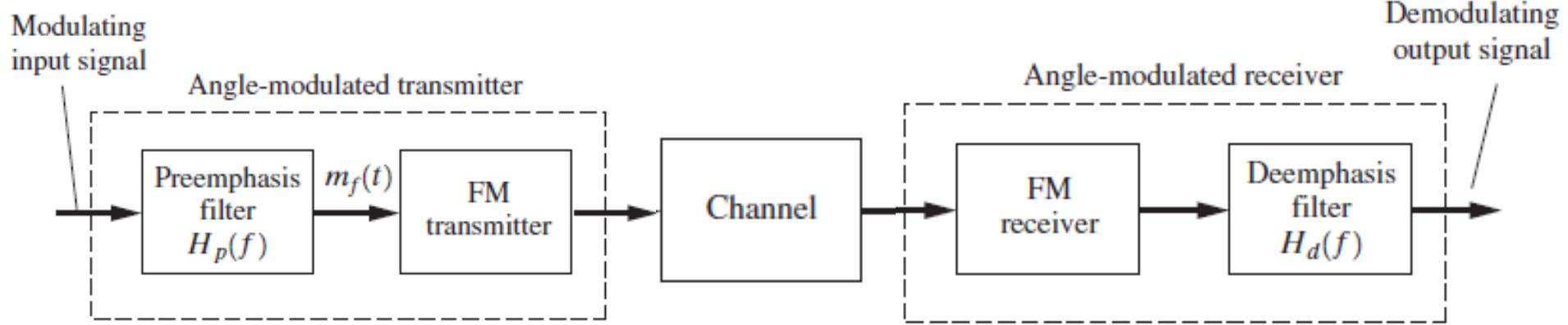
**Rational of Use:** Noise power non-linearly increase with frequency



In angle-modulated systems, the signal-to-noise ratio at the output of the receiver can be improved if the level of the modulation is

- boosted at the top end of the (e.g., audio) spectrum (at the transmitter); this is called preemphasis, and
- attenuated at high frequencies on the receiver output—called deemphasis.

# FM Broadcast Preemphasis and Deemphasis filtering

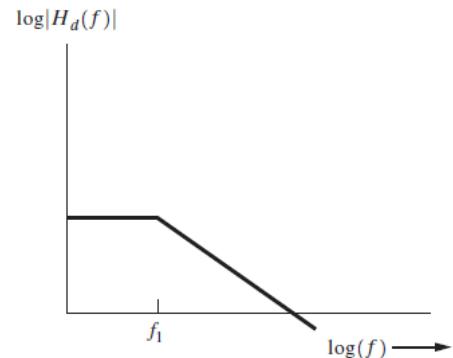
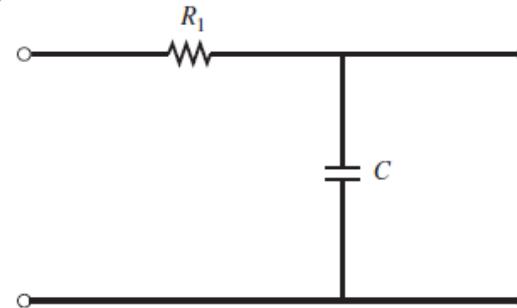


Preemphasis Filter

$$H_p(f) = K \frac{1 + j(f/f_1)}{1 + j(f/f_2)}$$

$$\text{where } f_1 = \frac{1}{2\pi\tau_1} = \frac{1}{2\pi R_1 C}$$

$$f_2 = \frac{1}{2\pi\tau_2} = \frac{R_1 + R_2}{2\pi R_1 R_2 C}$$

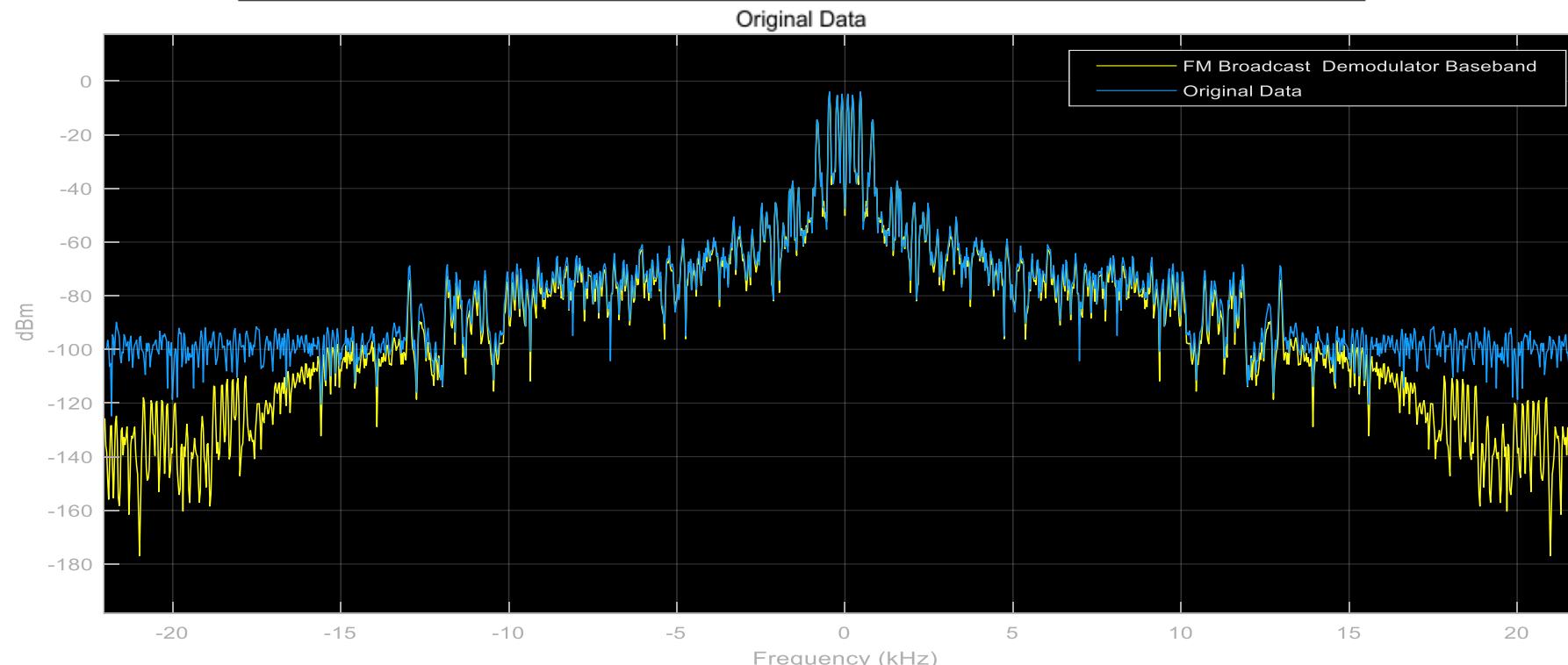
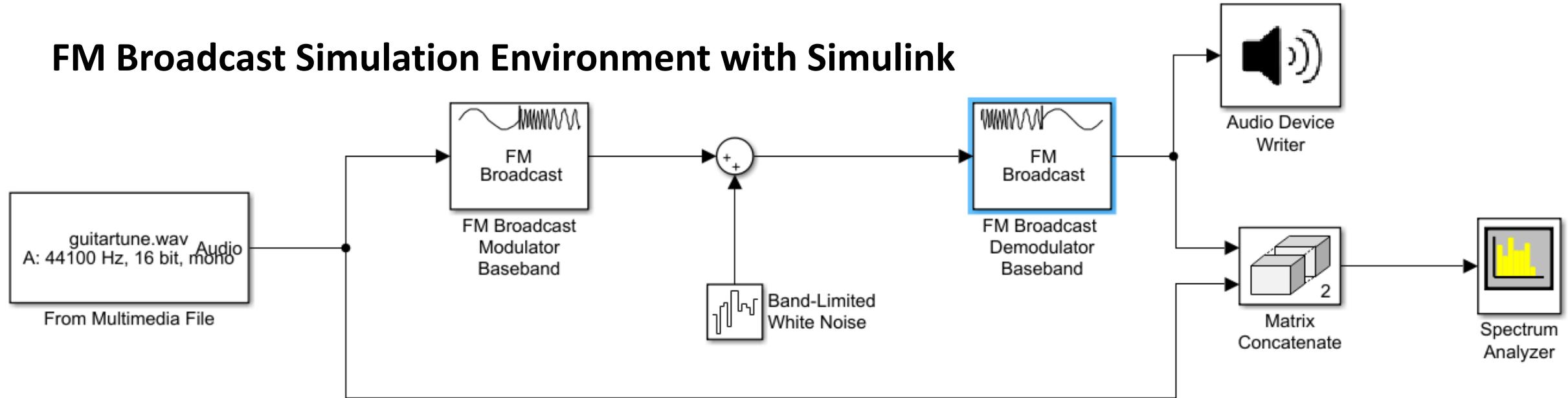


Deemphasis Filter

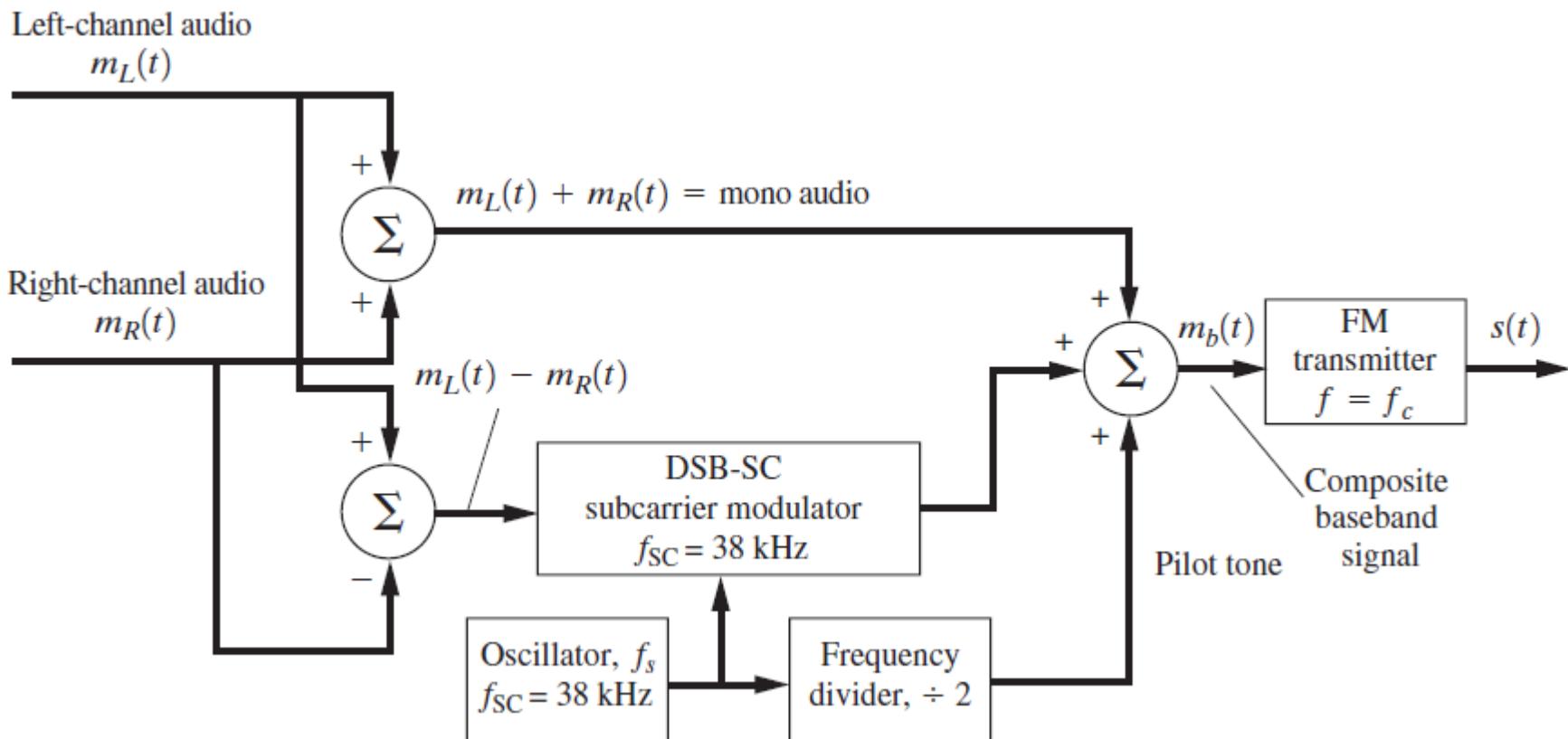
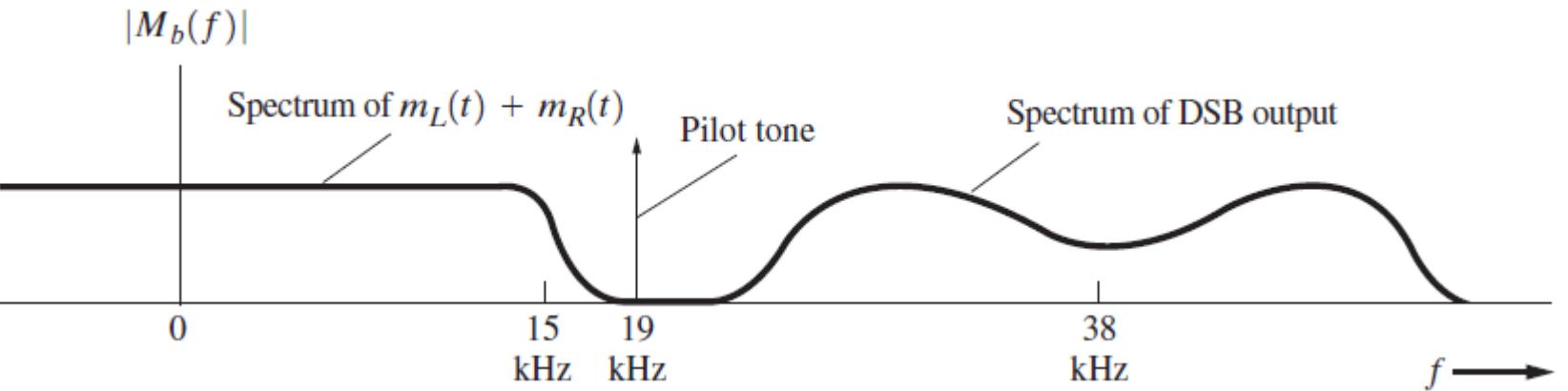
$$H_d(f) = \frac{1}{1 + j(f/f_1)}$$

$$\text{where } f_1 = \frac{1}{2\pi\tau_1} = \frac{1}{2\pi R_1 C}$$

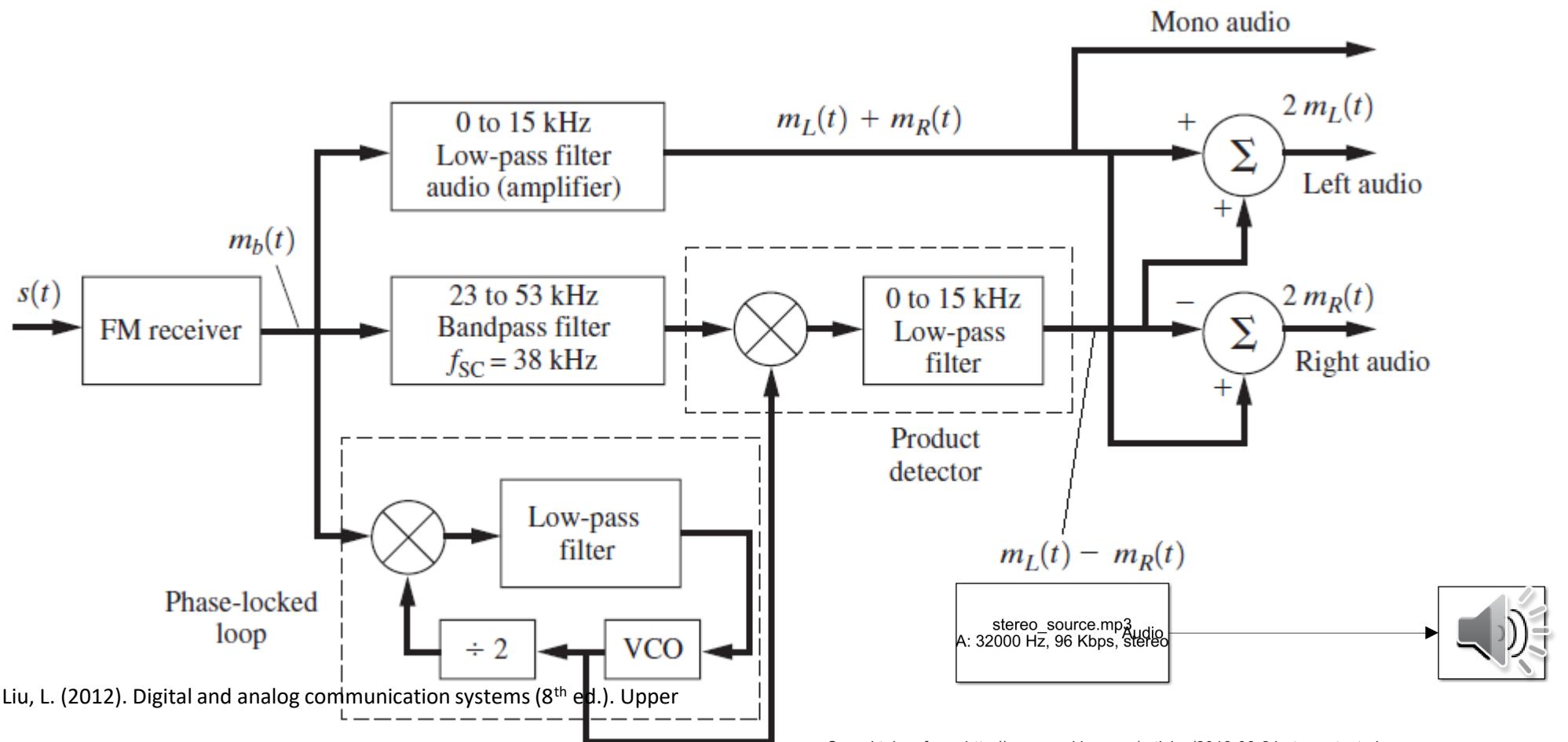
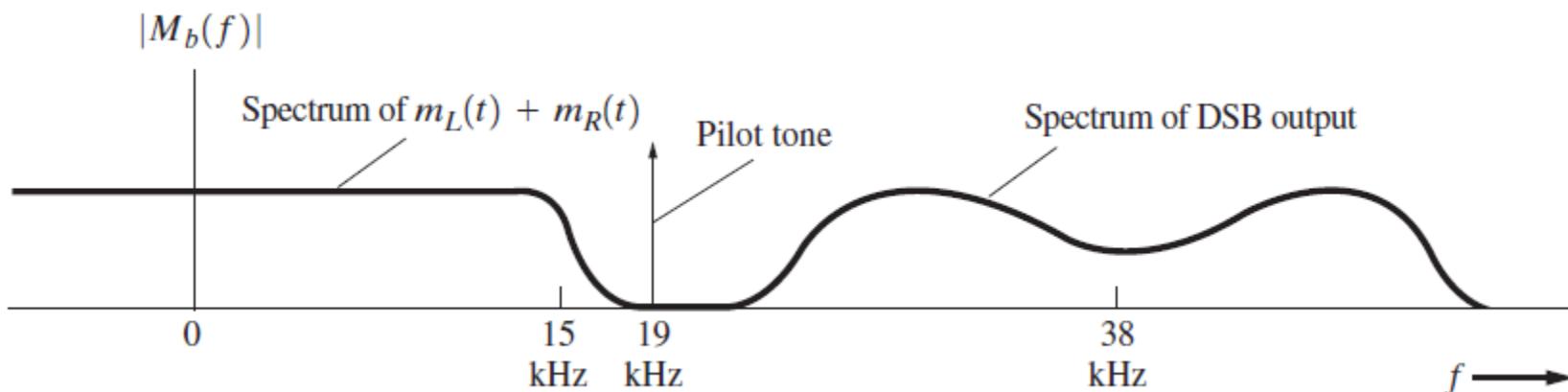
# FM Broadcast Simulation Environment with Simulink



# FM Stereo Transmitter



# FM Stereo Receiver



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