```
clear all
clc
T04=857+273
                           % Turbine inlet temperature
m=48
                            % inlet mass rate
T06A=927+273
                           % max afterburner temperature
                           % 0 if afterburner not used, 1 if used
afterburner=0;
T inf=220
                           % ambient temperature
P_inf=0.25*101325
                           % ambient pressure
M inf=0.85
                           % flight mach number
gamma=1.4
                           % ratio of specific heats
R=287 ;
                            % gas constant
u=M_inf*sqrt(gamma*R*T_inf)
                             % inlet velocity
Cp=gamma*R/(gamma-1);
                                   % specific heat
prc=linspace(4.4, 4.4,1)
                                   % compressor pressure ratio
% isentropic efficiencies
e diff=0.97 ;
                               % inlet/diffuser
e_n_hot=0.98;
                               % hot stream nozzle
e_comp=0.835;
                               % compressor
e_turb=0.865;
                               % turbine
e_burner=0.95;
                               % burner/combustor
e ab=0.5;
                               % afterburner
                              % burner pressure loss in %
del p1=0.0;
del p2=0;
                              % afterburner pressure loss in %
Q=45000000;
                               % fuel heat content
prc_critical= 1/(1-(gamma-1)/(e_n_hot*(gamma+1)))^(gamma/(gamma-1))  % to check if nozzle chokes or not
% diffuser stage
T02=T_inf*(1+(gamma-1)*0.5*M_inf^2)
P02=P inf*(1+(T02/T inf-1)*e diff)^(gamma/(gamma-1))
for i=1:length(prc)
    f ab(i)=0;
                                       % initializing the afterburner fuel fraction
    % compressor stage
    P03(i)=(P02*prc(i))
    T03(i)=T02*(1+(prc(i)^{(gamma-1)/gamma)-1)/e\_comp)
    % burner fuel air ratio
    f(i)=(T04-T03(i))/(e_burner*Q/(Cp)-T04)
    % turbine inlet pressure
    P04(i)=(P03(i))*(1-del p1) % # given pressure loss is zero
    % compressor turbine power balance
    T05(i)=T04-(T03(i)-T02)/0.99 \%-B*(T08-T02);
    P05(i)=(P04(i)*(1-(1-T05(i)/T04)/e_{turb})^{(gamma/(gamma-1))}
    T06(i)=(T05(i))
    P06(i)=(P05(i))
                                                          % if the afterburner is disabled
    if afterburner==0
                                                           % loops if nozzle doesn't choke
        if P_inf/P06(i) > 1/prc_critical
        v7(i) = (sqrt(2*e_n_hot*Cp*T06(i)*(1-(P_inf/P06(i))^((gamma-1)/gamma)))) % exit velocity, complete expansion to P_inf
           t(i)=(1+f(i))*v7(i)-u
                                                          % unchoked thrust without afterburner
                                        % TSEC
           s=(f(i))/t(i)
           sprintf('no afterburner, nozzle does not choke ')
                                                      % runs if nozzle chokes
        T7(i)=2*T05(i)/(gamma+1)
                                               % critical temperature
        v7(i)=(gamma*R*T7(i))^0.5
                                               % exit choked velocity
        p7(i)=P06(i)/prc_critical
                                               % critical pressure
        rho7(i)=P06(i)/(R*T7(i))
                                               % critical density at exit
        t(i) = (1+f(i))*v7(i)-u + (p7(i)-P_inf)/(rho7(i)*v7(i)) % choked thrust without afterburner
       s=(f(i))/t(i)
                       %TSFC
```

```
sprintf('no afterburner, nozzle chokes, nozzle diameter -')
      d=2*sqrt(m/(rho7(i)*v7(i)*3.14))
       end
   else
       P_06(i)=P05(i)*(1-del_p2)
                                      % loss in afterburner
       f_ab(i)=((1+f(i))*(T06A-T05(i)))/(e_ab*Q/Cp-T06A)
                                                        % fuel fraction in afterburner
       if P inf/P06(i) >1/prc critical
                                                      % nozzle unchoked with afterburner
           % unchoked thrust with afterburner
           t(i)=(1+f(i)+f_ab(i))*v7(i)-u
           s=(f(i)+f_ab(i))/t(i)
                                       %TSFC
           sprintf(' afterburner on, nozzle does not choke ')
       else
                                               % nozzle choked with afterburner
       T7(i)=2*T06A/(gamma+1)
                                             % critical temperature
       p7(i)=P06(i)/prc_critical
                                             % critical pressure
       v7(i)=(gamma*R*T7(i))^0.5
                                             % critical choked velocity at exit
       rho7(i)=p7(i)/(R*T7(i))
                                             % critical denstiy
       t(i) = (1 + f(i) + f_ab(i)) * v7(i) - u + (p7(i) - P_inf) / (rho7(i) * v7(i))  % choked thrust with afterburner
       s=(f(i)+f_ab(i))/t(i)
                                         % TSFC
        sprintf(' afterburner on, nozzle chokes ')
         d=2*sqrt(m/(rho7(i)*v7(i)*3.14))
       end
   end
   e\_prop(i) = 2*t(i)*u/(t(i)*u*2 + (1+f(i)+f\_ab(i))*(v7(i)-u)^2) \\ \hspace{0.5cm} \% \ propulsive \ efficiency
   e_{therm(i)}=(t(i)*u*2+(1+f(i)+f_ab(i))*(v7(i)-u)^2)/(2*(f(i)+f_ab(i))*Q) %thermal efficiency
end
e overall=e prop.*e therm
%hold on
 thrust=t*m
   % plot(prc,t)
    % title('Variation of specific thrust with afteburner disabled')
    % xlabel('Compressor pressure ratio \pi_C')
    % ylabel('t N/kg.s')
 % plot(prc,e_prop,'o')
   plot(prc,e_therm,'*' )
 %
   plot(prc,e_prop.*e_therm,'+' )
    title('T_{04}=1630 K & B=0')
 %
    xlabel(' Compressor pressure ratio \pi_C')
    ylabel('\eta')
 %
T04 =
       1130
   48
T06A =
       1200
```

file:///E:/ACADEMICS/Sem%205/Propulsion/html/turbo_afterburner.html

T_inf = 220

P inf =

2.5331e+04

```
M_inf =
  0.8500
u =
 252.7175
prc =
  4.4000
prc_critical =
  1.9202
T02 =
 251.7900
P02 =
 4.0091e+04
P03 =
 1.7640e+05
T03 =
 410.7090
f =
  0.0174
P04 =
 1.7640e+05
T05 =
 969.4757
P05 =
 9.4147e+04
T06 =
969.4757
P06 =
 9.4147e+04
```

T7 =

```
807.8964
v7 =
 569.7480
p7 =
  4.9029e+04
rho7 =
   0.4060
 429.3598
  4.0437e-05
ans =
no afterburner, nozzle chokes, nozzle diameter -
d =
   0.5141
e_prop =
   0.6797
e_therm =
   0.2043
e_overall =
   0.1389
thrust =
  2.0609e+04
```

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