## Şahin Utku Bozkurt 030170161 HW-2

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## Calculating and drawing the ideal air standard cycle of Single cylinder SI engine

```
% Given engine parameters
bore = 0.085; % m
stroke = 0.090; % m
CR = 12; % Compression Ratio
LHV = 49*10^6; %J/kg
stoich air = 17; %
rpm = 1501.5; % Revolutions per minute
lambda = 0.91; % Air-fuel ratio
moment = 25.11; % Nm
Vd=pi*0.25*bore^2*stroke;%m^3
advance = 7; % degrees
water flow=2.92*10^-4; % m3/s, water flow
mfc = 1.097/3600; % kg/s, mean fuel consumption
m_fuel = mfc; % kg/s, mass flow rate of fuel
m water=0.291; % kg/s, mass of water flow
m_air=17.56/3600; % kg/s, mass of air flow
T_diff = 30; % K, temperature difference of cooling water
T_manifold = 353; % K, temperature of intake manifold
T_atmos = 298; % K, temperature of ambient air
T_exhaust=777.9; % K, temperature of ambient air
c_v_water=4190; % J/(kg*°C)
c_v_air=1006; % J/(kg*°C)
displacement=stroke;
% Constants
R = 287; % J/kg-K, gas constant of air
k = 1.3; % Specific heat ratio of air
% Initial conditions
P1 = 10e5; % Pa
T1 = T_atmos; % K
Vc=Vd/(CR-1);% m3
V1=Vd+Vc;% m3
V1 = (pi/4) * bore^2 * stroke; % m3
% Process 1-2: Isentropic compression
V2 = V1/CR;
P2 = P1 * (V1/V2)^k;
T2 = T1 * (V1/V2)^{(k-1)};
% Process 2-3: Constant volume heat addition
Q_{in} = LHV * m_{fuel};
T3 = T2+((Q_in)/((m_air+m_fuel)*c_v_air));
P3 = P2 * (T3/T2);
V3=V2;
% Process 3-4: Isentropic expansion
V4 = V1;
```

```
P4 = P3/(CR^k);
T4=T3/(CR^{(k-1)});
% Process 4-1: Constant volume heat rejection
Q_out_water = m_water * c_v_water * (71.6-67.8);
Q_out_air = (m_air+m_fuel) * c_v_air * (T_exhaust-T_manifold);
Q_out=Q_out_air+Q_out_water;
% Plotting the cycle
V = [V1 \ V2 \ V3 \ V4 \ V1];
P = [P1 \ P2 \ P3 \ P4 \ P1];
plot(V,P,'-o');
xlabel('Volume (m^3)');
ylabel('Pressure (Pa)');
title('Ideal air standard cycle for Single cylinder SI engine');
% Calculate effective power
effective_power = moment *(2*pi*rpm/60);
% Calculate brake specific fuel consumption
bsfc = (m_fuel*3600 / effective_power)*10^6;% g/kWh
% Calculate effective efficiency
effective efficiency = effective power*10^6 /(bsfc*LHV);
%Indicated Power
ipow=Q_in-Q_out;% W
% Calculate indicated mean effective pressure (IMEP)
imep = (ipow/(Vd*(rpm/60)*0.5))/1000;% kPa
% Calculate brake mean effective pressure (BMEP)
bmep = (effective_power/(Vd*(rpm/60)*0.5))/1000;% kPa
% Calculate friction mean effective pressure (FMEP)
fmep = bmep - imep;
% Calculate mechanical efficiency
mechanical_efficiency = bmep/imep;
% Calculate volumetric efficiency
volumetric_efficiency=(2*m_air/((rpm/60)*Vd));
% Calculate energy lost (Ofriction)
Q_out_friction=Q_in-Q_out-effective_power;
% Display results
fprintf('Effective power: %f W\n', effective power);
fprintf('BSFC: %f g/Wh\n', bsfc);
fprintf('Effective efficiency: %f %%\n', effective_efficiency*100);
fprintf('IMEP: %f kPa\n', imep);
fprintf('BMEP: %f kPa\n', bmep);
fprintf('FMEP: %f kPa\n', fmep);
fprintf('Mechanical efficiency: %f %% ', (mechanical_efficiency*100));
fprintf('\nVolumetric efficiency: %f %% ', (volumetric_efficiency*100));
fprintf('\nrate of energy lost(Qfriction) %f % ', (Q_out_friction*100/Q_in));
fprintf('\nrate of heat rejected with exhaust gas %f % ', (Q_out_air*100/Q_in));
fprintf('\nrate of heat rejected with cooling water %f % ', (Q_out_water*100/Q_in));
```

Effective power: 3948.213846 W

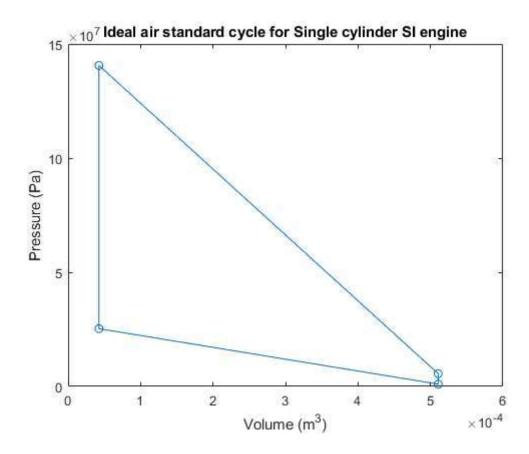
BSFC: 277.847159 g/Wh

Effective efficiency: 29.000042 %

IMEP: 1264.879436 kPa BMEP: 617.854671 kPa FMEP: -647.024765 kPa

Mechanical efficiency: 48.846922 % Volumetric efficiency: 76.332182 % rate of energy lost(Qfriction) 27.690770

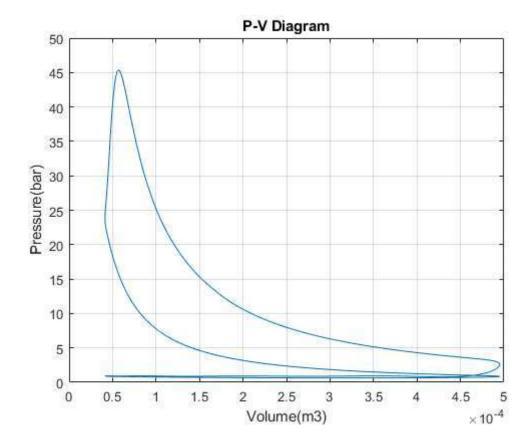
rate of heat rejected with exhaust gas 14.836239 rate of heat rejected with cooling water 31.030616



## Drawing the real cycle of single cylinder SI engine

```
v_values=readmatrix('1500_7_90_1732_Şahin Utku Bozkurt.xlsx','Range','B2:B721');  % L
p_values=readmatrix('1500_7_90_1732_Şahin Utku Bozkurt.xlsx','Range','C2:C721');  % bar

plot(v_values/1000,p_values);
title('P-V Diagram');
ylabel('Pressure(bar)');
xlabel('Volume(m3)');
grid
```



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