

Bilkent University

Spring 2019-2020

EEE 313: Electronic Circuit Design

Midterm #1

Name and Surname:

Student ID:

Signature:

Exam Duration: 120 minutes

Question#	Your score	Out of
1		25
2		15
3		20
4		20
5		20
Total:		100

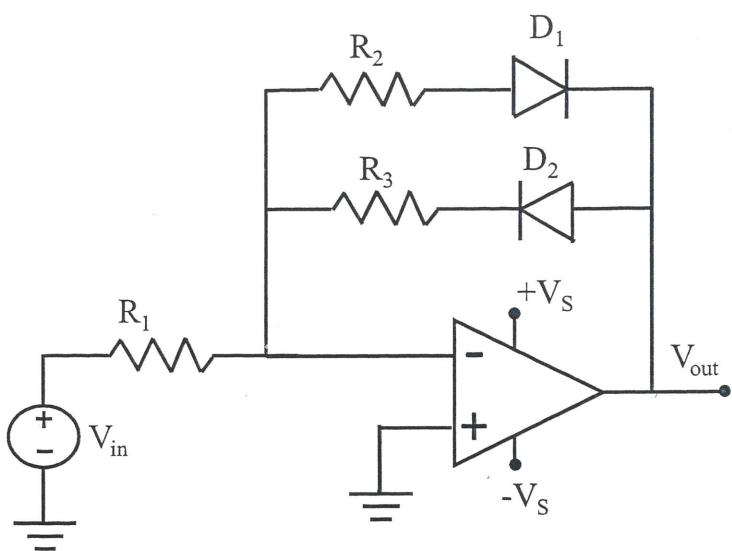
Instructions:

1. Calculators without extensive memory are allowed
2. Clearly explain all your answers in order to receive credit
3. Put a box around your final answer
4. Cheat sheets are not allowed
5. Indicate the units for your final answers
6. Write your student ID on the bottom of every page

Student ID:

1. (25 points)

a. (10 points)



You are given the OPAMP circuit on the left with two diodes. Plot V_{out}/V_{in} by assuming OPAMP always operates in the linear region without going into saturation. The diodes are ideal with 0V turn on potential. Explain the circuit operation as much as possible. Verify the states of the diodes whenever you make assumptions.

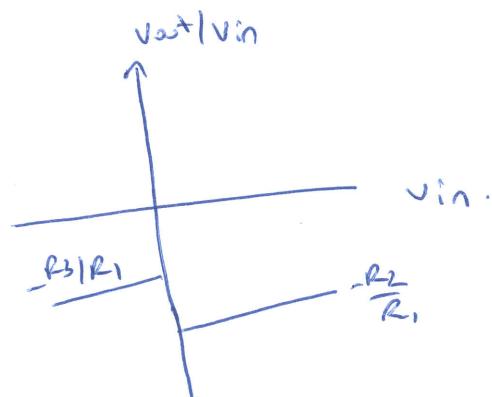
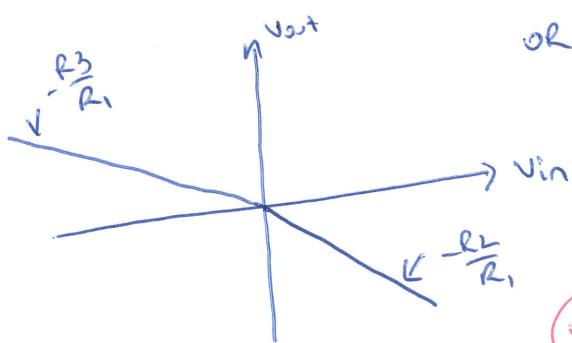
$$\frac{V_{in} - 0}{R_1} + \frac{V_{out} - 0}{R_{2,3}} < 0 \Rightarrow \frac{V_{out}}{V_{in}} = -\frac{R_{2,3}}{R_1}, \text{ inverting amplifier. } \textcircled{02}$$

D_1 turns on when $V_{out} < 0$, $V_{in} > 0$, D_2 off

D_2 turns on when $V_{out} > 0$, $V_{in} < 0$, D_1 off

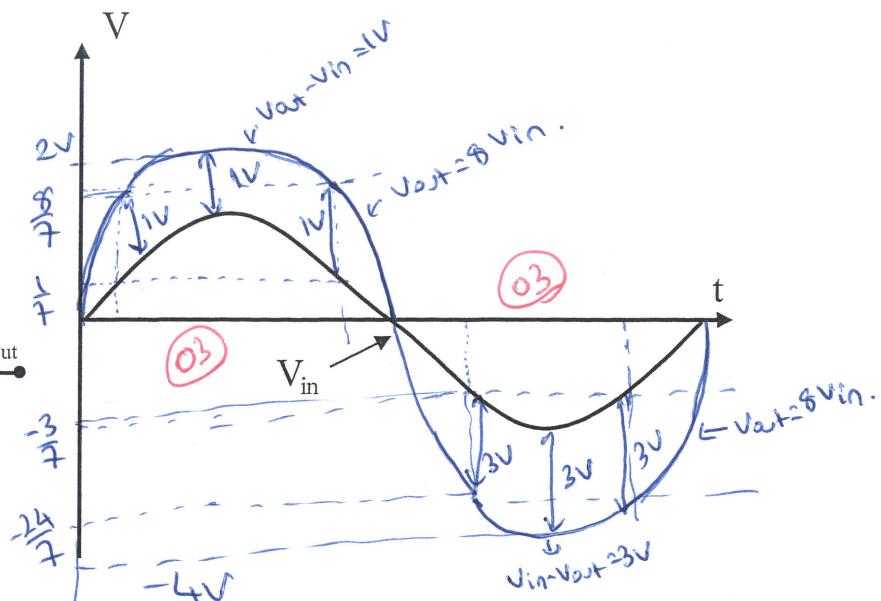
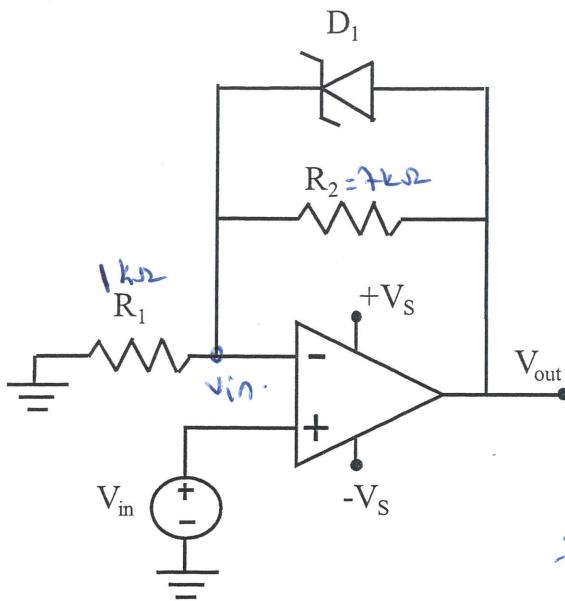
so when $V_{in} > 0$ $\frac{V_{out}}{V_{in}} = -\frac{R_2}{R_1}$

$V_{in} < 0$ $\frac{V_{out}}{V_{in}} = -\frac{R_3}{R_1}$



explaining the circuit operation.

b. (15 points)



The OPAMP circuit is modified with a Zener diode for this part of the question. $V_{in} = 1 \sin \omega t$, $R_1 = 1k\Omega$, $R_2 = 7k\Omega$, and the Zener voltage is 3V in reverse bias and $V_{on} = 1V$ in forward bias for the Zener diode. By assuming ideal and linear OPAMP operation without saturation, find and plot $V_{out}(t)$ for one period on the provided graph. $V_{in}(t)$ is plotted for reference. Clearly label all the critical voltage values and explain the reasoning behind your answer.

w/o Zener

$$V_+ = V_- = V_{in}, \quad \frac{V_{in}}{R_1} + \frac{V_{in} - V_{out}}{R_2} = 0 \quad (03)$$

$$V_{in} \left(\frac{1}{R_1} + \frac{1}{R_2} \right) = \frac{V_{out}}{R_2} \Rightarrow V_{in} \left(\frac{R_1 + R_2}{R_1 R_2} \right) = \frac{V_{out}}{R_2}, \quad \frac{V_{out}}{V_{in}} = 1 + \frac{R_2}{R_1} = 8$$

when the + cycle of V_{in} , when $V_{out} - V_{in} < 1V$ regular $V_{out} = 8V_{in}$.

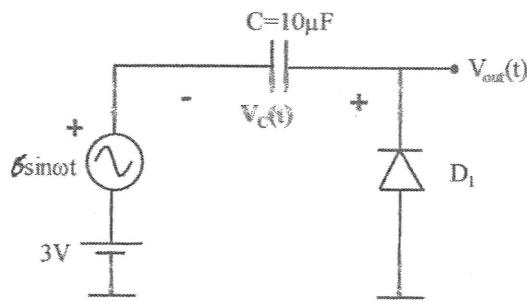
(02)

when $V_{out} - V_{in} = 1V$ Zener turns on forward bias and $V_{out} - V_{in} = 1V$
 $7V_{in} = 1V \quad V_{in} = \frac{1}{7}V \quad V_{out} = \frac{8}{7}V$ V_{out} follows V_{in} with 1V increase.

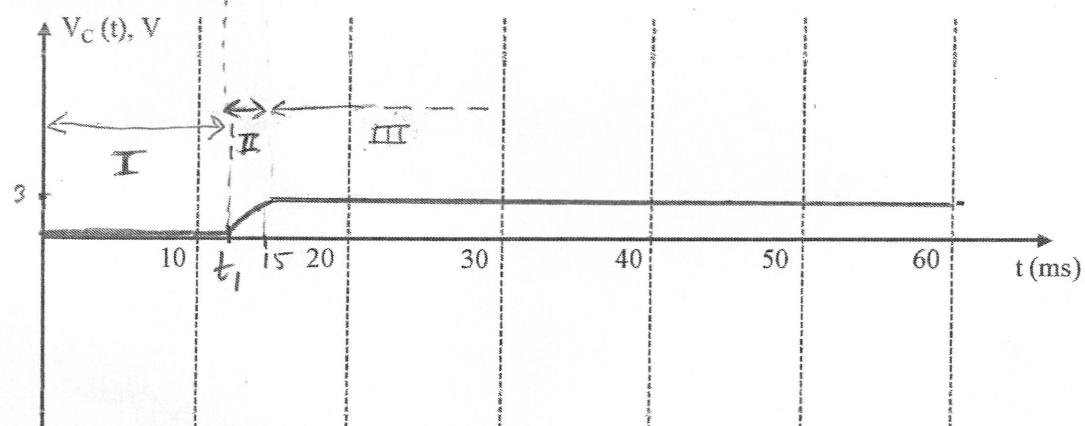
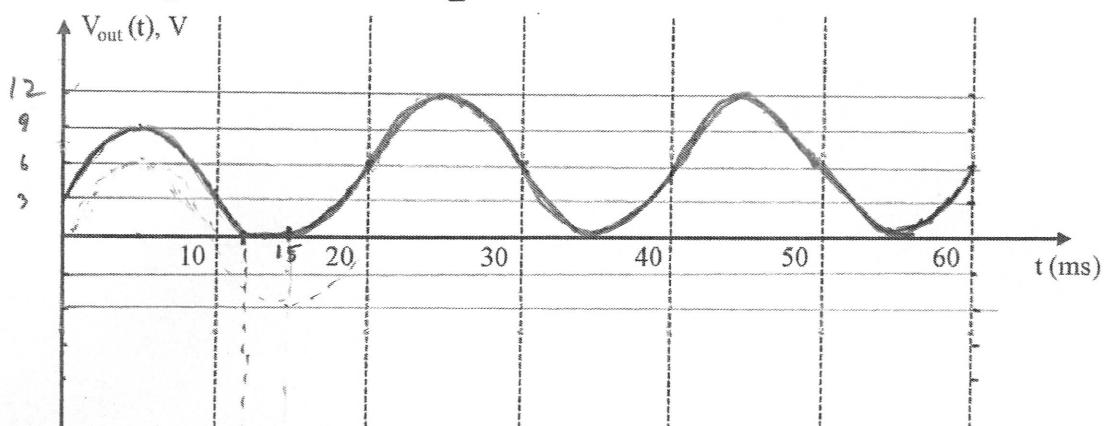
The - cycle of V_{in} :

(03) when $V_{in} - V_{out} < 3V$ regular $V_{out} = 8V_{in}$.
 when $V_{in} - V_{out} > 3V$ Zener turns on reverse bias and $V_{in} - V_{out} = 3V$
 $-7V_{in} = 3V \quad V_{in} = -\frac{3}{7}V \quad V_{out} = -\frac{24}{7}V$ V_{out} follows V_{in} with 3V decrease.

2. (15 points)



You are given the clamper circuit shown on the left. Find and plot $V_{out}(t)$ and $V_c(t)$ for $0 < t < 60\text{ms}$ by assuming the diode is ideal and $\omega = 2\pi f$, $f = 50\text{Hz}$. The graphs are provided below. The capacitor voltage at $t=0$ is 0V, $V_c(0)=0\text{V}$.



$$6\sin\omega t = 3$$

$$\sin\omega t = \frac{3}{6} = 0.5$$

$$\omega t = 0.5236$$

$$t = \frac{0.5236}{2\pi \times 50} = 0.00175 = 1.7\text{ ms} \quad t_1 = 11.7\text{ msec.}$$

Phase I : 3p

Phase II : 2p

Phase III : 8p

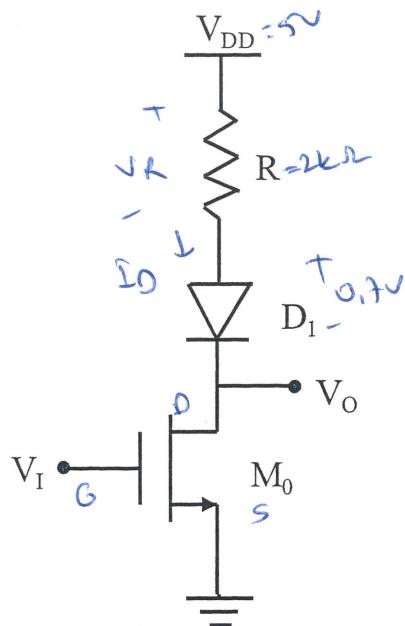
$t_1 : 2p$

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$$\omega t = 30^\circ$$

$$t = \frac{30^\circ}{360^\circ \times 50} = 0.0017$$

3. (20 Points)



For the diode-transistor circuit shown on the left: $R=2k\Omega$, $K_N=0.1\text{mA/V}^2$, $V_{TN}=1\text{V}$, $\lambda=0$, and the diode is ideal with $V_{ON}=0.7\text{V}$. $V_{DD} = 5\text{V}$ and the input voltage is varied between 0 and 5V.

- i. Find V_o when V_I is slightly larger than V_{TN}
 - ii. Find V_o when $V_I = 5V$
 - iii. Find the V_I ranges when M_0 is OFF, in SAT and in NON-SAT. What is the value of V_I when M_0 moves from NON SAT to SAT?

(1) when $V_I > V_{IN}$ transistor will start to conduct current + I_{ON}
 Larger than zero diode will turn on $V_o = \frac{V_{DD}}{5} - I_{ON} \cdot R_D = 4.3V$

$$\text{Q1) } V_I = 5V \text{ large } V_{GS}, \text{ transistor will likely be in NON-SAT} \\ I_D = 0.1 [2L(5 - 11. V_D - V_D^2)] \quad (2) \\ V_D = 5 - 2I_D - 0.1 = 4.3 - 2I_D \\ I_D = \frac{4.3 - V_D}{2} \quad (2) \\ \text{Ans: } I_D = 1.105 \times$$

$$\frac{4V_3 - V_0}{2} = 0.1 \left[8V_0 - V_0^2 \right]$$

$$\frac{4V_3 - 10V_0}{2} = 8V_0 - V_0^2 \Rightarrow V_0^2 - 18V_0 + 20 = 0$$

$$V_0 = 1.94 \text{ V}$$

$$I_D = 1.175 \text{ mA}$$

so Non Sat is correct (Q1)

check $V_{DS} - V_{TH} > V_{DS}$

$$V_{DS} - V_{TH} = V_I - 1$$

at the Non-SAT SAT Boundary

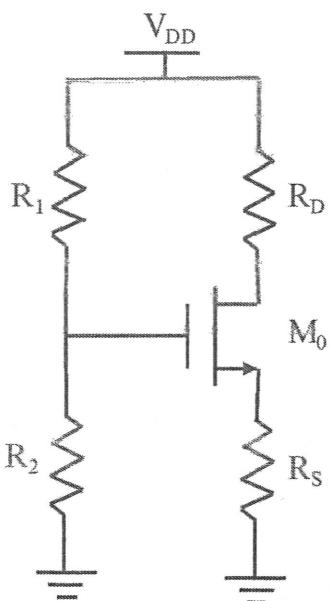
$$\frac{4.3V_0}{2} = 0.1V_0^2 \quad 0.2V_0^2 - V_0 = 0$$

$$V_0 = 2.76V \quad V_0 = -2.76V \times$$

$$V_S = V_0 + I = 3.76V$$

Student ID:

4. (20 Points)



$V_{DD} = 10V$
 $R_1 = R_2 = 10M\Omega$
 $R_S = 6k\Omega$
 $V_{IN} = 1V$
 $K_N = 0.5mA/V^2$
 $\lambda = 0$

Find ID and VDS for the circuit shown on the left when

- a. $R_D = 6k\Omega$
- b. $R_D = 14k\Omega$

Do not forget to verify the state of the M_0 transistor in each case.

Solution

a) $V_G = \frac{10}{10+10} \times 10 = 5V$. Assume SAT:

$$I_D = 0.5(V_{GS}-1)^2$$

$$V_{GS} = 2V$$

$$I_D = \frac{2}{6} = 0.5mA$$

$$V_{DS} = 10 - 0.5(6+6)$$

$$V_{DS} = 4V > 2-1 \checkmark \text{ check (1p)}$$

$$\therefore \boxed{I_D = 0.5mA \quad V_{DS} = 4V} \quad (8p)$$

Also $V_G = V_{GS} + I_D R_G \Rightarrow$

$$5 = V_{GS} + 6I_D \Rightarrow \frac{5-V_{GS}}{6} = 0.5(V_{GS}-1)^2$$

$$5-V_{GS} = 3(V_{GS}^2 - 2V_{GS} + 1)$$

$$5-V_{GS} = 3V_{GS}^2 - 6V_{GS} + 3$$

$$0 = 3V_{GS}^2 - 5V_{GS} - 2 = 0$$

$$(V_{GS}-2)(3V_{GS}+1) = 0$$

$$V_{GS} = \begin{cases} 2 > 1V \\ \frac{-1}{3} > 1V \end{cases} \checkmark \text{ check (1p)}$$

only this (2p)

b) Assume SAT again. All are the same until $V_{GS} = 10 - 0.5(6+14) = 0 > 2-1 \times$

∴ TR must be NONSAT.

$$I_D = 0.5[2(V_{GS}-1)V_{DS} - V_{DS}^2] \quad V_{GS} = 5 - 6I_D$$

$$2I_D = 2(4-6I_D)(10-20I_D) - (10-20I_D)^2 \quad V_{DS} = 10 - (6+14)I_D = 10 - 20I_D$$

$$= 2(40-80I_D-60I_D+120I_D^2) - (100-400I_D+400I_D^2)$$

$$= 80 - 280I_D + 240I_D^2 - 100 + 400I_D - 400I_D^2$$

$$= -20 + 120I_D - 160I_D^2$$

$$\Rightarrow 160I_D^2 - 118I_D + 20 = 0 \Rightarrow I_D = \begin{cases} 0.4735mA \Rightarrow V_{GS} = 2.16V > 1 \\ 0.264mA \Rightarrow V_{GS} = 3.416V > 1 \end{cases}$$

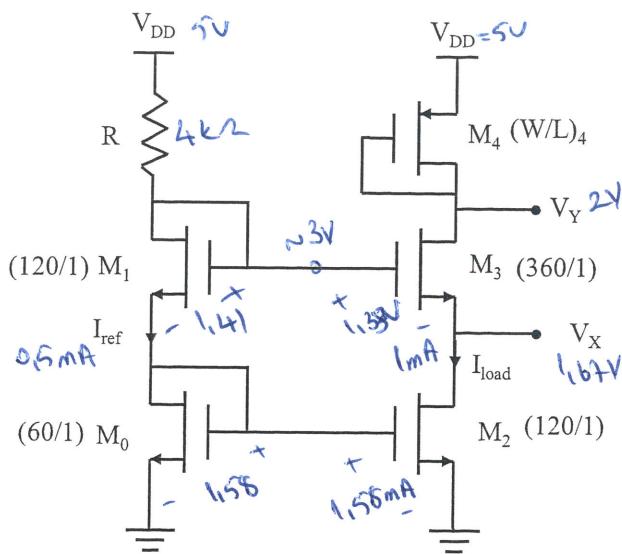
$$I_D = 0.4735 \Rightarrow V_{DS} = 0.5296 < 2.16-1 \checkmark \text{ check (1p)}$$

$$I_D = 0.264 \Rightarrow V_{DS} = 4.72V < 3.416-1 \times \uparrow \text{ check (1p)}$$

only this (2p)

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$$\boxed{I_D = 0.4735mA \quad V_{DS} = 0.5296V} \quad (8p)$$



$V_{DD} = 5V$
 $R = 4k\Omega$
 $V_{TN} = 1V$ for nMOS
 $V_{TP} = -1V$ for pMOS
 $K_P = K_N = 50 \mu A/V^2$ for all
 $K_N = (W/L) K_N / 2$
 $\lambda = 0$

M_1 and M_0 forms a cascode current mirror and generates the reference current that is used to bias M_2 , M_3 , and M_4 . Calculate the (W/L) ratio of M_4 to keep M_3 in saturation with minimum V_{DS} . Specify I_{ref} , I_{load} , V_X and V_Y in your solution. Verify the states of all transistors.

$$I_{ref} = \frac{0.05}{2} \cdot \left(\frac{120}{1}\right) \cdot (1.41 - 1)^2 \quad (02)$$

$$\boxed{I_{ref} = 0.5 \text{ mA}} \quad (02)$$

$$I_{load} = \frac{(W/L)_2}{(W/L)_0} \cdot I_{ref} = 1 \text{ mA} \quad (02)$$

M_2 SAT needs to be checked

Assume M_3 is in SAT

$$I = \frac{0.05}{2} \left(\frac{360}{1}\right) \cdot (V_{GS3} - 1)^2$$

$$V_{GS3} = 1.33V \quad (03)$$

$$\boxed{V_X = 3 - 1.33 = 1.67V} \quad (03)$$

M_2 is in SAT. $1.58 - 1 < 1.67V$

for M_3 to be in SAT with min V_{DS}

$$V_{DS3} = V_{GS3} - V_{TN} = 0.33V \quad (02)$$

$$V_Y = V_X = 0.33V \Rightarrow V_Y = 2V$$

M_4 is in SAT by default $V_{SO} = V_{SG} = 2V$

$$\text{for } M_4 \quad \downarrow \quad \frac{5-2}{2} \\ I_{MA} = \frac{0.05}{2} \cdot \left(\frac{W}{L}\right)_4 (3 - 1)^2$$

$$\boxed{\left(\frac{W}{L}\right)_4 = 10} \quad (03)$$

$M_1 - M_0$ in SAT by default ($V_{GS} = V_{DS}$)

$$V_{GS1} + V_{GS0} = 5 - 4 \cdot I_{ref} \rightarrow 0.5 \quad (02)$$

$$I_0 = I_1 = I_{ref}$$

$$\frac{K_N}{2} \cdot \left(\frac{W}{L}\right)_1 \cdot (V_{GS1} - 1)^2 = \frac{K_N}{2} \cdot \left(\frac{W}{L}\right)_0 \cdot (V_{GS0} - 1)^2 \quad (03)$$

$$2 \cdot (V_{GS1} - 1)^2 = (V_{GS0} - 1)^2$$

$$V_{GS0} = r_2 V_{GS1} - r_2 + 1$$

use *

$$V_{GS1} + (2V_{GS1} - r_2 + 1) = 5 - 4 \cdot \frac{0.05}{2} \cdot \frac{120}{1} \cdot (V_{GS1} - 1)^2 \\ = 5 - 12(V_{GS1} - 1)^2$$

$$V_{GS1}(1+r_2) - r_2 + 1 = 5 - 12(V_{GS1}^2 - 2V_{GS1} + 1) \\ - 12V_{GS1}^2 + 24V_{GS1} - 12 \cdot$$

$$12V_{GS1}^2 - V_{GS1}(23+r_2) + 6 - r_2 = 0$$

$$\boxed{V_{GS1} = 1.41} \quad (03)$$

$$V_{GS1} = 0.33 \times V_{TN}$$

$$V_{GS0} = 2V_{GS1} - r_2 + 1$$

$$V_{GS0} = 1.58V$$

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