1 Differential gearing W9 - control input Cs - Main Drive-input FS - Main Drive -output

Numerous differential functions can be obtained by combinations of the speed and rotational direction of the 3 busic elements

Advantages:

- · Zero backlash
- · consistent performance
- . High position Accuracy
- · High Torque to -weight Radio

· Affordable precision

II. Cycloidal Drive

- * It provides very high reduction ratio with compact design.
 - -> It can achieve higher reduction ratios of up to 10 times in the same space.
 - => They feature virtually zero backlash, higher load capacity, rigidity & high efficiency.

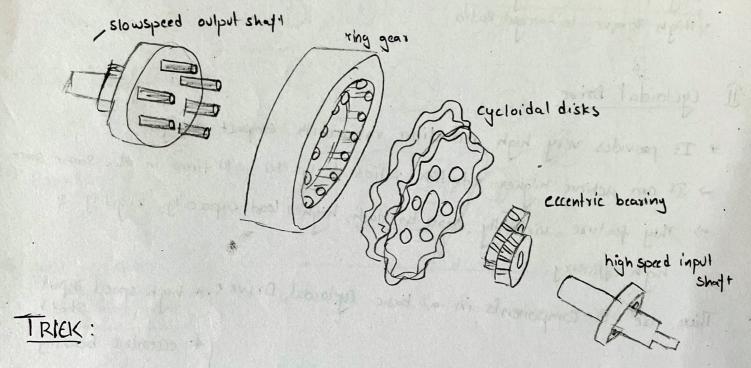
There are 5 components in a basic cycloidal Drive? * high speed input Shaft

* eccentric bearing * The input shaft is mounted eccentrically to a * cycloidal disks rolling-element bearing (typically a cylindrical roller * ring gear * slow speed output beasing), causing the cycloidal disc to wabble in a circle. The cycloidal disc will independently votate around the bearing as it is pushed against the ring geax.

=> The number of pins on the ring gear is larger than the number of Pins on the cycloidal disc. This causes the cycloidal disc to rotate. around the bearing faster than the input shaft is moving it around,

giving an overall rotation in the direction opposing the rotation of the input shaft.

if the cycloidal disc has holes that are larger (by an amount equal to the eccentricity of the input shatt) than the output voller pins that go inside them. The output pins will move abound in the holes to achieve Steady rotation of the output shadt from the wobbling movement of the egrooidal disc.



Ratio = N-n

Elleris house politioner is I form layer wit it n=no. of lobes on the cycloidal disk and within toppold of luncon (Control) N=no.4 rollers

Lillan Stocket See will be son eg: To get 18:1 ratio reduction

take
$$n = 15 = no \cdot d$$
 lobed

 $N = 16 = no \cdot d$ voller pins

strong on the son granted

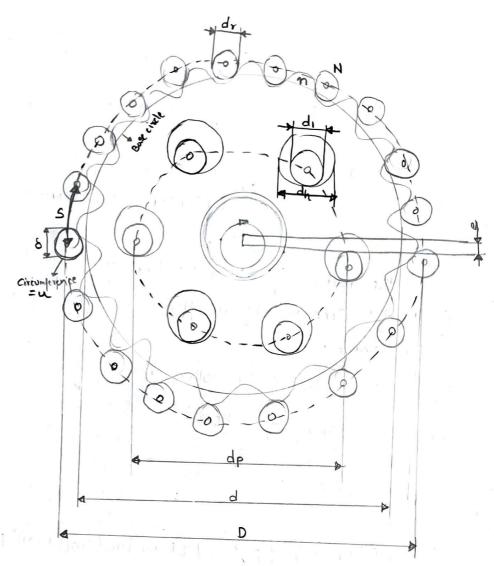
$$R = \frac{15}{L} = 1621$$

GEOMETRY OF THE CYCLOIDAL DISC

$$N = no \cdot of$$
 soller ping $n = no \cdot of$ lobes

$$\int g = \frac{N}{D}$$

(v) Hole diameter



$$x = \frac{d+\delta}{2} \sin(\phi) - e \cdot \sin(\phi + \frac{d}{\delta} \phi)$$

$$y = \frac{d+\delta}{2} \cos(\phi) - c \cdot \cos(\phi + \frac{d}{\delta}\phi)$$

d: base circle diameter

& : rolling circle diameter

e : eccentricity

φ: angle (parameter) = 0 - - - 2 1

For Rotor: Cycloidal disk

> These Two eggs define the Rotor's shape:

$$X = R\cos(\theta) - R_8\cos(\theta - \Psi) - E\cos(N\theta)$$

$$Y = -Rsin(\theta) + R_8 sin(\theta - \Psi) + Esin(N0)$$

where,
$$y = -\tan^{-1} \left[\frac{\sin((1-N)\theta)}{(R|EN) - \cos((1-N)\theta)} \right]$$
; $0 \le 0 \le 360^{\circ}$

=> R is the radius of the rotor that you want (Pitch circle Diametor)

=> E is the Eccentricity (or offset) from the input shaft to the center of the rotos.

=> Ro is the radius of the rollers and

=> N is the number of rollers.

Egy to use in CAD:

$$X = (R^* cos(t)) - (R_*^* cos(t+ ax(tan(sin((1-N)^*t))/((R/EN)-cos((1-N)^*t)))) - (E^* cos(N^*t))$$

the terminal this

$$Y = \left(-R^* sin(t)\right) + \left(R_*^* sin\left(t + arctan\left(sin\left((1-N)^*t\right)\right) \left(\left(R/EN\right) - cos\left((1-N)^*t\right)\right)\right)$$

$$+ \left(E^* sin\left(N^*t\right)\right)$$

NOTE:

** Cycloidal drives are not operated with a single cycloidal disk as

it will create unbalances & viberations at high speeds

=> 50, A second identical cycloidal disk is mounde with a 180° Offset this compensates for the unbalance

20:1 reduction cycloidal drives

20 teeth on the disk 21 - roller ping or teeth on casing

Shape: 2 diff types of equations - Explicit equations

Explicit equ are used when we have single variable equis - Parametric Curves worts the same way but a they use 2 ears to - define a conve

we use parametric eqn:

=1 2 egns that define the Rotor's shape :

 $X = R\cos\theta - R_{x}\cos(\theta-\psi) - E\cos(N\theta)$

Y=-Rsind + Rsin (0-4) + Esin (NO)

 $\psi = -\tan^{-1}\left[\frac{\sin((1-N)\theta)}{(R/EN)-\cos((1-N)\theta)}\right]; 0 \le \theta \le 360$

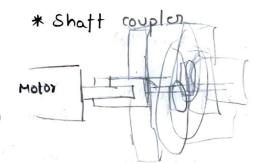
R - radius of rotor

E - eccentricity (offset) from the input shaft to the center of the rotor

Ry-radius of the Rollers

N-no-of vollows

* Bushings-



Ratio: 20:1 - No backlash - Backdrivable

output flange - (3D printed cycloidal Reducer) - Ball bearing - casing

=> 21- pins-Bushings - \$

* I designed & built - Vid no-8

Lots make it with inbuilt walls

- 6mm Dia Rollon Dia 21
- reduction ratio : 20:1 (2)

21×2×X×

rollors >> Nx = 21 >> Rx = 6 mm = 3 mm

out side imeter R = 80 = 40 mmradius of fric = Re E = eccentricity

$$N = 20$$

N = 21

D = 126

d = 120 e = 1

de=3

output. =>, No=6 from center of the disk

* eccentricity: e=1

=> Epitrochoid parametric Equations:

* 20:1

eccentric amount = 1.37 mm

Ring pin diameter - 8 mm

Ring pin pitch dia = 80.00 mm

cycloidal curve plot = 6 num pas tooth

* Center hole dia = 32 mm

+ pin dia = 4.9

* centor to pin dt = 50 mm

Zuan pend: 10:1



Cobe 1:

$$D \Rightarrow R = 40$$

 $E = 1$
 $R_{x} = 3.5$
 $N = 21$
 $dp = 25$
 $dh = de + 2c = 5$
 $de = 3$

E

- * two disks with 180 degree phase difference which eliminates viberations at high speeds. to increase to eque capacity.
- * to maximise efficiency, we employ bearings for outer rollers &
- * Needle voller bearings" large contact area allowing high torque & efficiency in a compact design.

=> off-the-shelf components:

-to minimise cost of the design, it is advisible to use standard

off the shelf components.

- roller, bearings, screws, nuts, washow

$$N=20$$
 $N=20$
 $S=3$
 $D=63$
 $D=70 \Rightarrow R=35$
 $R_1 \Rightarrow 0$