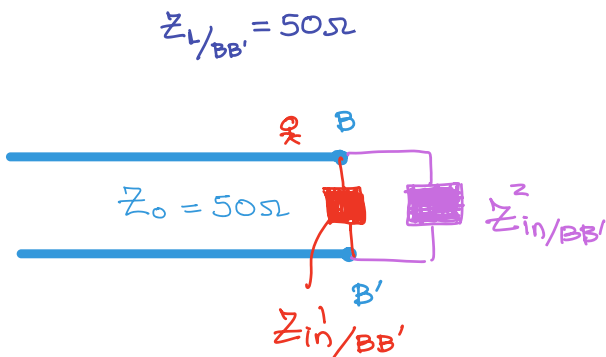
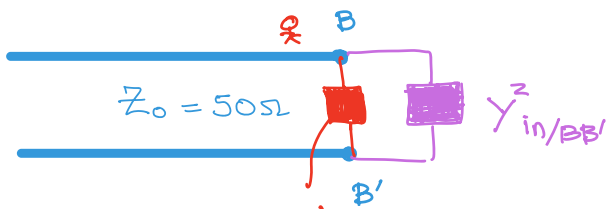


$Z'_{12/BB'}$ = impedance at
BB' presented by #1 = reactive

$Z'_{12/BB'}$ = impedance at BB'
presented by #2

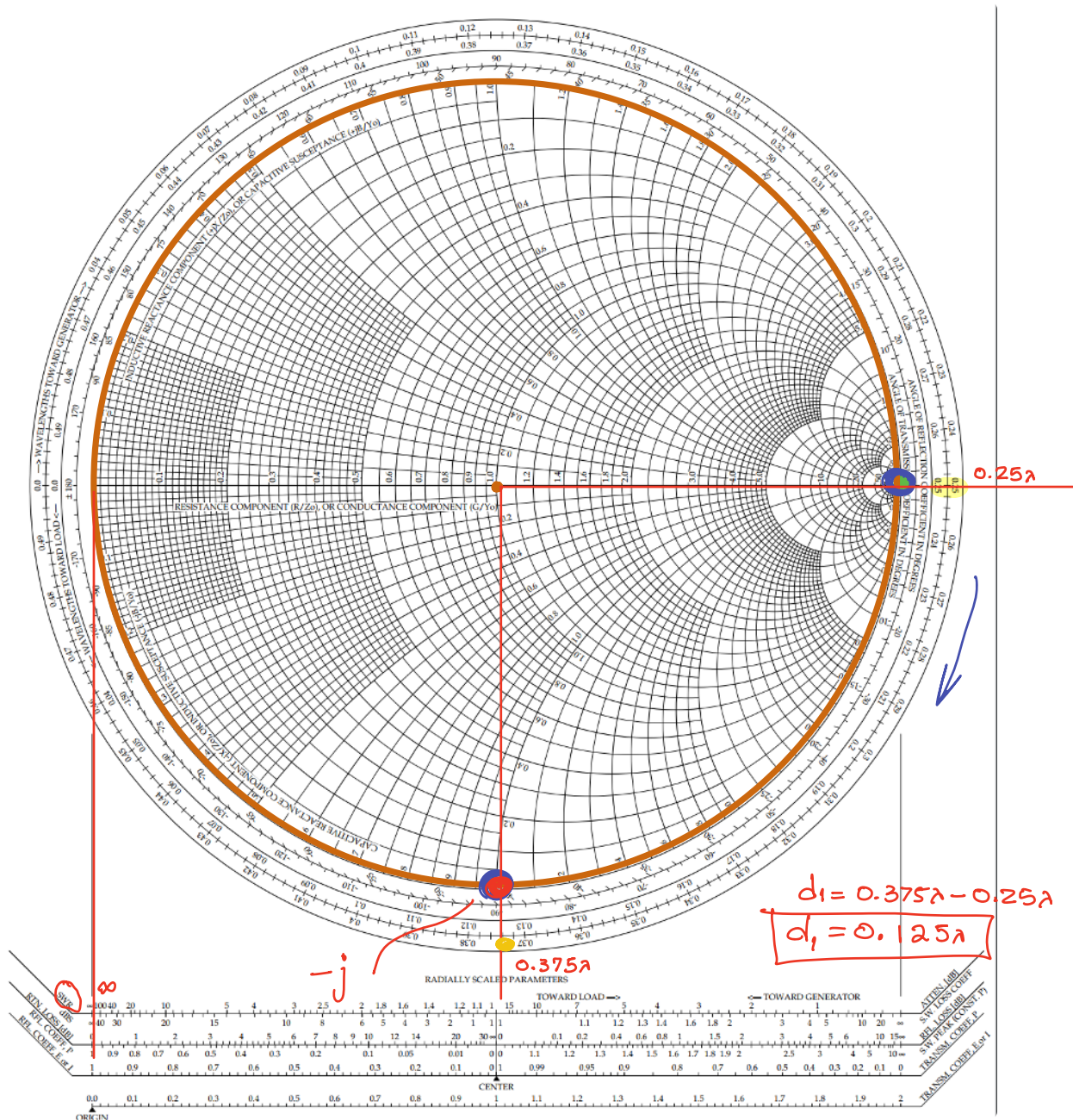


on the Smith Chart
we will admittances



$Y'_{in/BB'}$ = reactive = jX $\left\{ \begin{array}{l} \text{if } X > 0 \Rightarrow \text{cap.} \\ \text{if } X < 0 \Rightarrow \text{ind.} \end{array} \right.$

Transmission Line #1



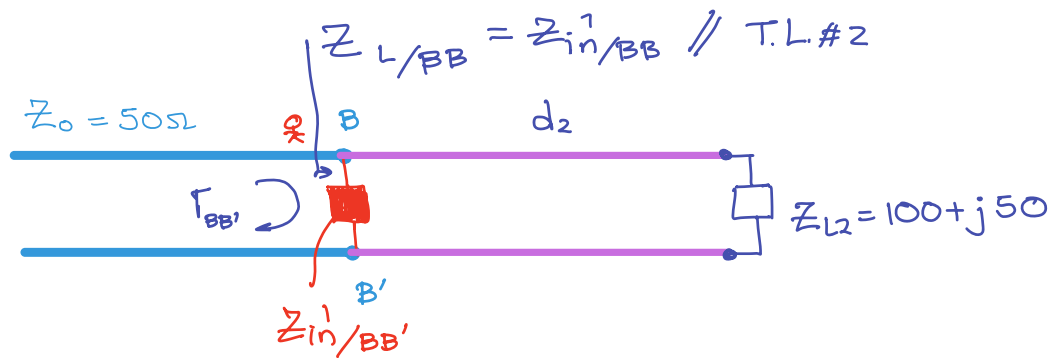
$$d_1 = 0.375\lambda - 0.25\lambda$$

$$d_1 = 0.125\lambda$$

$$VSWR = \frac{1 + |\Gamma|}{1 - |\Gamma|}$$

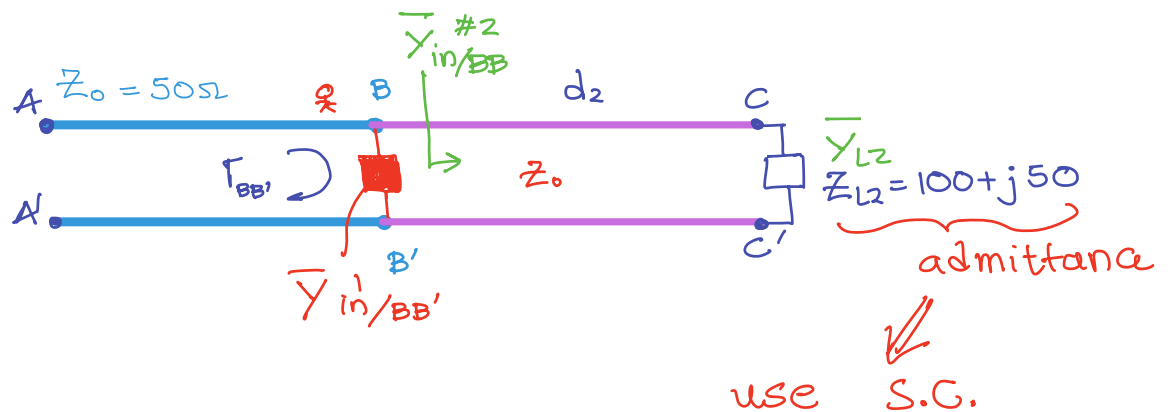
$$Z_L^{\#1} = 0 = \text{short}$$

$$Y_L^{\#1} = \frac{1}{Z_L^{\#1}} = \infty$$



What is d_2 and Z_{in}'/BB' so that $\Gamma_{BB'} = 0$

Because Z_{in}'/BB' (or T.L #1) is connected with T.L #2 \Rightarrow We change all loads and in general all impedances into admittances

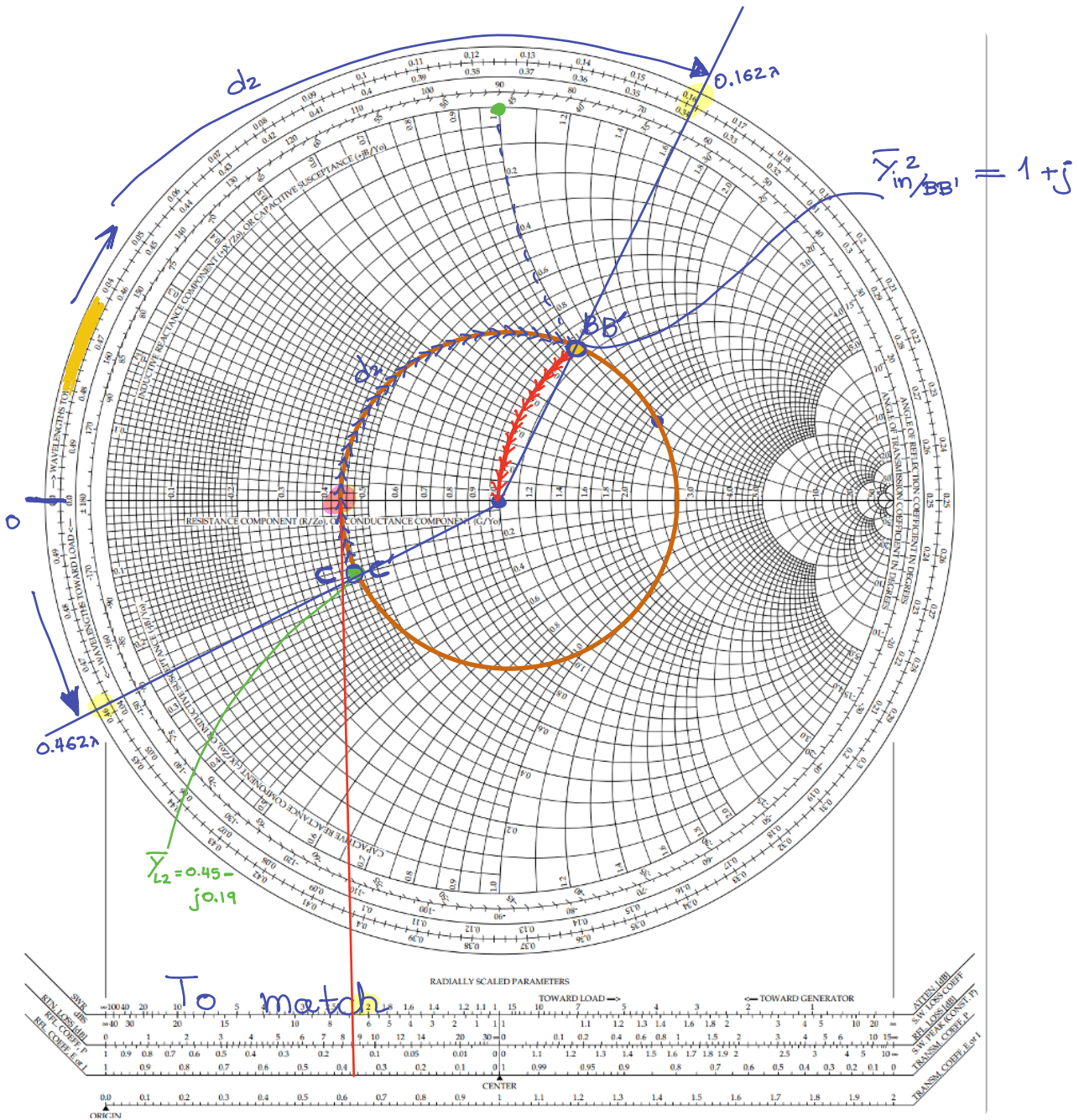


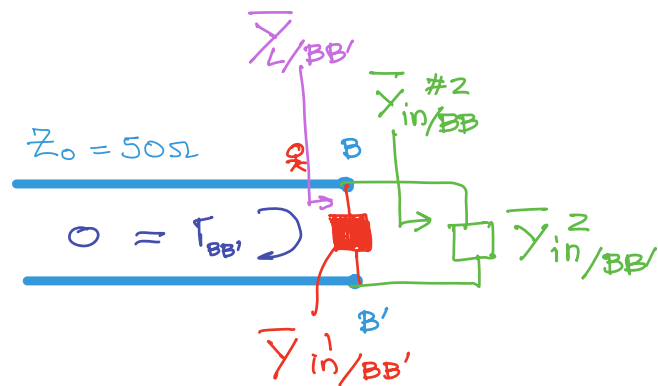
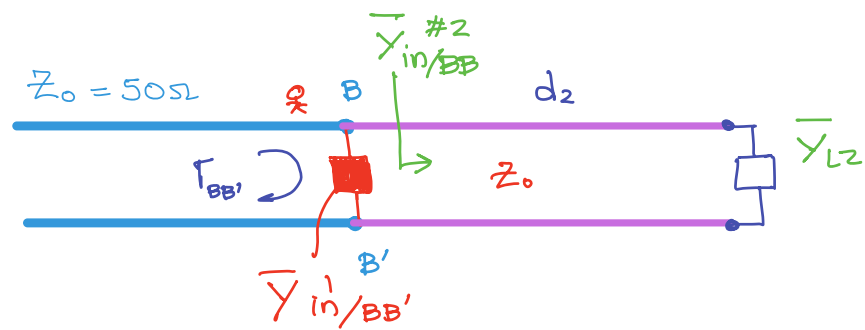
$$Z_{L2} \rightarrow Y_{L2} \Rightarrow Z_{L2} \rightarrow \bar{Z}_{L2} \Rightarrow \bar{Z}_{L2} \rightarrow \bar{Y}_{L2}$$

using S.C.

$$\bar{Z}_{L2} = \frac{100 + j50}{50} = \underline{2 + j}$$

$$(0.5 - 0.462)\lambda + 0.162\lambda = 0.038\lambda + 0.162\lambda = 0.2\lambda = d_2$$





$$\boxed{\bar{Y}_{L/BB'} = \bar{Y}_{in/BB'} + \bar{Y}_{in/BB}^2} = 1$$

?
?(1+j)

$$\bar{Y}_{L/BB'} = 1 = \bar{Y}_{in/BB'}^1 + (1+j) \Rightarrow$$

$$\Rightarrow X = \bar{Y}_{in/BB'}^1 + 1 + j \Rightarrow$$

$$\Rightarrow \boxed{\bar{Y}_{in/BB'}^1 = -j}$$

