

Week 9

Task 1 Use a weather forecast website, and utilize the psychrometric chart and the formula we went through in the class to determine the absolute humidity, the wet-bulb temperature and the mass of water vapour in the air in Classroom A (Aula A) of Piacenza campus in the moment that you are solving this exercise (provide the inputs that you utilized)

Umidità: Relative humidity, Pressione atmosferica: Air total pressure (1 hPa: 0.1 kPa),
Temperatura effettiva: temperature to be utilized.

Il tempo oggi in Piacenza Lunedì, 02 Dicembre 2019							
	13:00	14:00	16:00	18:00	20:00	21:00	22:00
							
PartlyCloud	PartlyCloud	LightCloud	LightCloud	PartlyCloud	Cloud	PartlyCloud	
Temperatura effettiva	10°C	10°C	9°C	6°C	7°C	7°C	8°C
Temperatura percepita	10°C	10°C	8°C	5°C	7°C	6°C	7°C
Precipitazioni	0 mm	0 mm	0 mm	0 mm	0 mm	0 mm	0 mm
Umidità	79 %	77 %	89 %	90 %	90 %	92 %	91 %
Pressione atmosferica	1016 hPa	1015 hPa	1016 hPa	1017 hPa	1019 hPa	1019 hPa	1020 hPa

According to the data The time is 8 pm

Relative humidity is

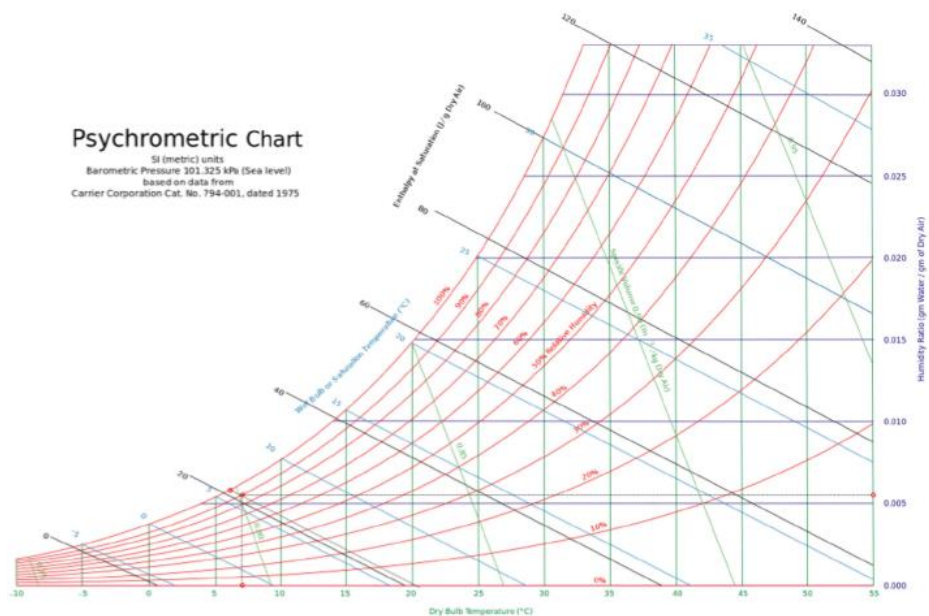
=90%

Total air pressure =

101.9 kPa

Temperature in kelvin

scale $T = 230$ K



The absolute humidity

$W = 0.0055$

Bulb temperature $T_{wb} = 6^\circ\text{C}$

$$W = \frac{0.622 p_v}{p - p_v} = 0.005$$

$$P = 101.2 \text{ Ka}$$

$$P_v \approx 0.823 \text{ kPa}$$

$$\phi = \frac{mv}{mg}$$

$$\phi = 20\%$$

$$\therefore \text{gas} \geq \text{water vapour}$$

$$\therefore R_{sp} = 0.4615$$

$$mv = \frac{0.883}{0.4615 \times 230}$$

$$mv \approx 8.41 \times 10^{-3}$$

$$mg = \frac{mv}{80\%} \approx 8.34 \times 10^{-3}$$

ask 2 Utilize the same methodology we went through in the class and determine the sensible and latent load corresponding to internal gains, the ventilation, and the infiltration in a house with a *good* construction quality and with the same geometry as that of the example which is located in Brindisi, Italy

BRINDISI, Italy

WMO#: 163200

Lat: 40.65N Long: 17.95E Elev: 10 StdP: 101.2 Time Zone: 1.00 (EUW) Period: 86-10 WBAN: 99999

Annual Heating and Humidification Design Conditions

Coldest Month	Heating DB		Humidification DP/MCDB and HR						Coldest month WS/MCDB				MCWS/PCWD to 99.6% DB	
			99.6%			99%			0.4%		1%			
	99.6%	99%	DP	HR	MCDB	DP	HR	MCDB	WS	MCDB	WS	MCDB	MCWS	PCWD
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)
2	2.9	4.1	-5.1	2.5	7.2	-3.0	3.0	7.4	13.4	10.2	12.4	10.6	3.4	250

Annual Cooling, Dehumidification, and Enthalpy Design Conditions

Hottest Month	Hottest Month DB Range	Cooling DB/MCWB						Evaporation WB/MCDB						MCWS/PCWD to 0.4% DB	
		0.4%		1%		2%		0.4%		1%		2%			
		DB	MCWB	DB	MCWB	DB	MCWB	WB	MCDB	WB	MCDB	WB	MCDB	MCWS	PCWD
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)
8	7.1	32.8	23.6	31.1	24.3	29.9	24.3	27.2	29.7	26.3	29.0	25.6	28.3	4.2	180

	Dehumidification DP/MCDB and HR						Enthalpy/MCDB								Hours 8 to 4 & 12.8/20.6	
	0.4%			1%			2%		0.4%		1%		2%			
	DP	HR	MCDB	DP	HR	MCDB	DP	HR	MCDB	Enth	MCDB	Enth	MCDB	Enth	MCDB	
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)	
26.3	21.8	29.2	25.4	20.7	28.5	24.7	19.7	27.9	86.0	30.1	82.2	29.1	78.5	28.3	1236	

Extreme Annual Design Conditions

Extreme Annual WS			Extreme Max WB	Extreme Annual DB				n-Year Return Period Values of Extreme DB							
				Mean		Standard deviation		n=5 years		n=10 years		n=20 years		n=50 years	
1%	2.5%	5%		Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)
11.3	9.9	8.7	31.4	0.4	37.3	1.4	3.0	-0.6	39.4	-1.4	41.1	-2.2	42.8	-3.2	44.9

$$q_{ig} = 136 + 2.2 + 22 = 620 \text{ W}$$

$$q_{ig} = 136 + 2.2 \times 22 \times 200 + 22 + 2 = 88 \text{ W}$$

A simple information :

$$A_{ul} = 1.4 \text{ m}^2$$

$$A_{es} = A_{wall} = A_{roof} =$$

$$200 + 144 = 344 \text{ m}^2$$

$$\therefore A_l = A_e = A_s = 344 \times 1.4 = 481.6 \text{ cm}^2$$

$$T_{\text{cooling}} = 24^\circ\text{C} = 71^\circ\text{K}$$

$$T_{\text{heating}} = 20^\circ\text{C} = 24^\circ\text{K}$$

$$DR = 7.1^\circ\text{C} = 71^\circ\text{K}$$

$$DF_{\text{heating}} = 0.073$$

$$DF_{\text{cooling}} = 0.033$$

The rate of air flow:

$$Q_{i_{\text{heating}}} = A_l \times ID_{f_{\text{heating}}}$$

$$= 481.6 \times 0.033$$

$$\cong 35.157 \text{ l/s}$$

$$Q_{i_{\text{cooling}}} = A_l \times ID_{T_{\text{cooling}}}$$

$$\cong 481.6 \times 0.0033$$

$$\cong \frac{35.157 L}{s}$$

$$\cong 15.893 \text{ l/s}$$

Building :

$$Q_v - V_{\text{cooling}} = 0.05 A_c f + 3.5(Nbr + 1)$$

$$0.05 \times 200 + 3.5(Nbr + 1) = 17$$

$$Q_i - V_{\text{heating}} = Q_{i_{\text{heating}}} + Q_v \cong 35.157 = 52.157 \text{ l/s}$$

$$C_{\text{sensible}} = 1, 2, 3 C_{\text{latent}}$$

$$3010 \text{ W cooling} = 0.0039$$

$$q_{\text{inf}} - V_e = C_s Q_{i_{\text{vc}}} \Delta T$$

$$\cong 300 \times 32.893 \times 0.0039$$

$$= 386.13 \text{ W}$$

$$q_{\text{inf}} - V_e = C_s Q_{i_{\text{vh}}} \Delta T_{\text{heating}}$$

$$123 \times 52 \times 157 \times 241$$