

Reliability in Microelectronics

Final Project

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Project Background

An electric scooter company is developing a new motor control system. The task, as a reliability engineer, is to evaluate the reliability of two key components:

- A silicon controller chip (65nm node)
- A GaN power transistor module

Test data was provided from an accelerated life testing. The goal is to extract reliability models for each component and determine the maximum voltage and temperature that ensure long-term mission success.

Theory Section

Series System in Reliability:

In reliability engineering, a series system is one in which all components must operate successfully for the system to function. If any single component fails, the entire system is considered to have failed. This configuration is common in systems with no redundancy (parallel system) and represents a conservative reliability model. The reliability of the overall system is calculated as the product of the individual component reliability:

$$R_{\text{system}} = R_1 \cdot R_2 \cdot R_3 \cdot \dots \cdot R_n$$

As more components are added in series, the system reliability decreases—even if each component is highly reliable. For example, if three components each have a reliability of 0.99, the system reliability would be:

$$R_{\text{system}} = 0.99 \times 0.99 \times 0.99 \approx 0.9703$$

Thus, series systems are highly sensitive to individual component failures and are often used to model worst-case reliability scenarios.

In a series system, the entire system fails if just one component stops working. This makes the system unreliable, especially if it has a lot of parts. Redundancy helps solve this issue by adding backup components in **parallel**. That way, even if one component fails, the system can keep running because another component can take over.

For example, let's say a single component has a reliability of $R=0.9$, meaning it has a 90% chance of working. If we add another identical component in parallel, the new reliability becomes:

$$R_{\text{parallel}} = 1 - (1 - R)^2 = 1 - (0.1)^2 = 0.99$$

So instead of a 10% chance of failure, it drops to just 1%. This shows how redundancy can make systems much more reliable by reducing the impact of individual failures. It's especially useful in systems where uptime is critical and failures can't be tolerated.

Weibull Analysis (Silicon)

Given data shows TTF (Time-to-Fail) samples for Silicon under 3 Voltages under 3 voltages (1.0 V, 1.2 V, 1.4 V) and 3 temperatures (100°C, 120°C, 140°C).

$k = 0.00008617$ (Boltzmann Constant)

$$T[K] = T[C] + 273$$

Using Weibull and Weibit analysis:

$x - axis: Weibull = \ln(TTF)$

$y - axis: Weibit = \ln(-\ln(1 - R(t)))$

Where $F(t) = \frac{\#failures}{N+0.5}$, $N = 30$

The Weibull analysis was plotted for each different T and V to derive the shape parameter (β) and characteristic life (θ) using: $y = \beta \ln(t) - \ln(\theta)$. The plots for each condition can be viewed below with their linear equations. Each temperature will be combined to one graph each for simplicity and comparison between voltages. Each of the equations are listed top to bottom in order from V=1V until V=1.4V

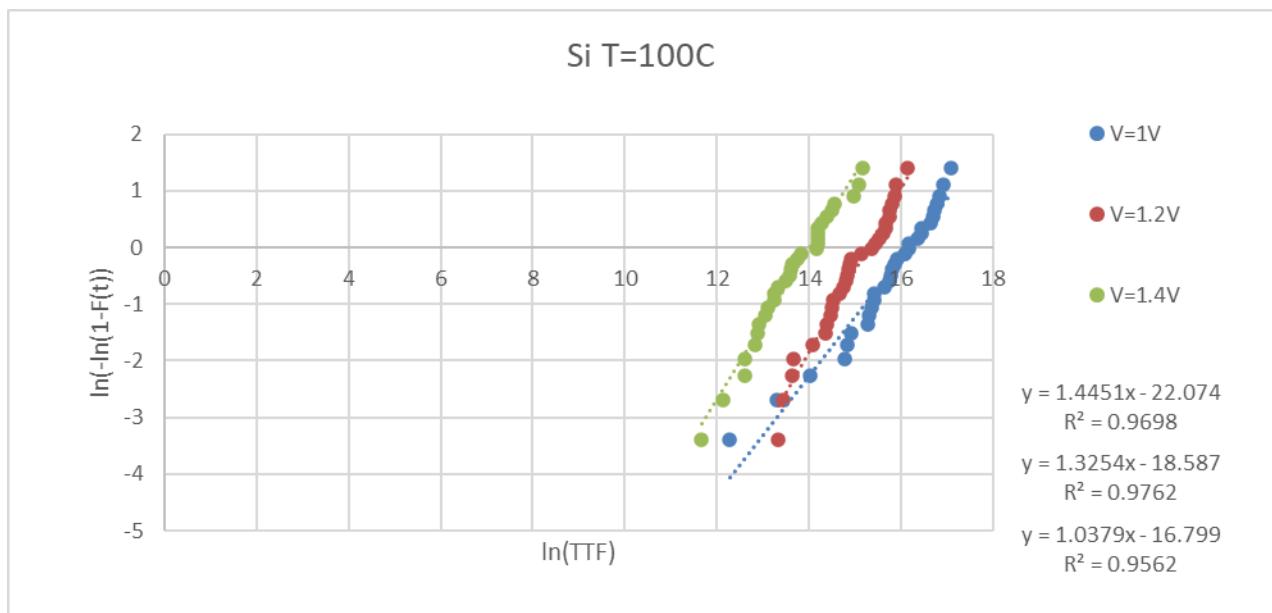


Image 1 – Si Weibull Graph T=100C

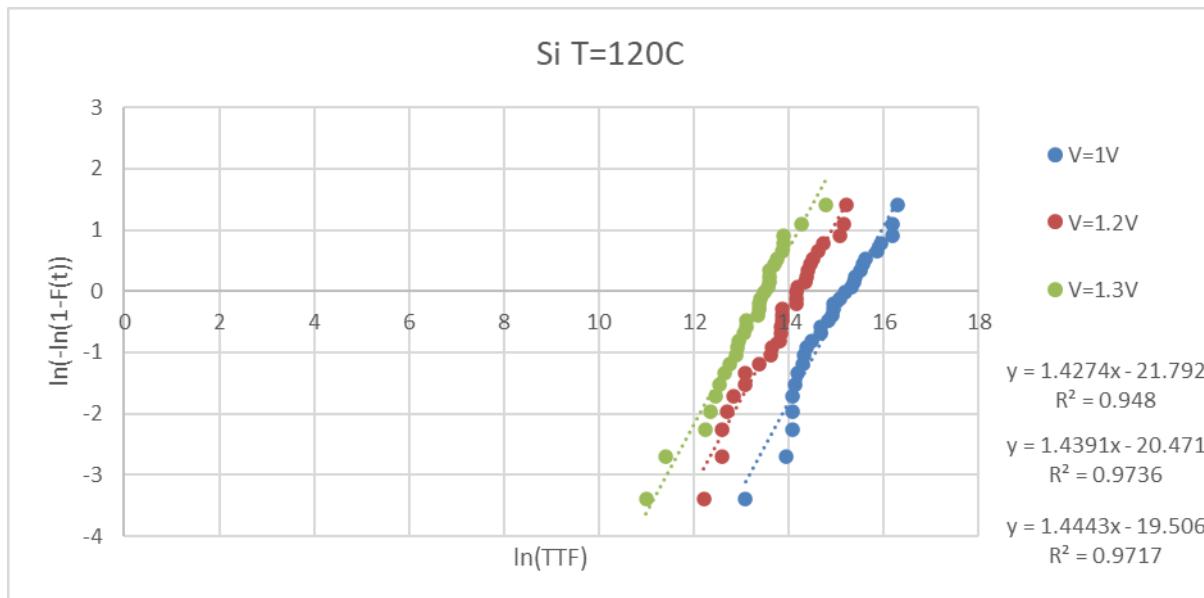


Image 2 – Si Weibull Graph T= 120C

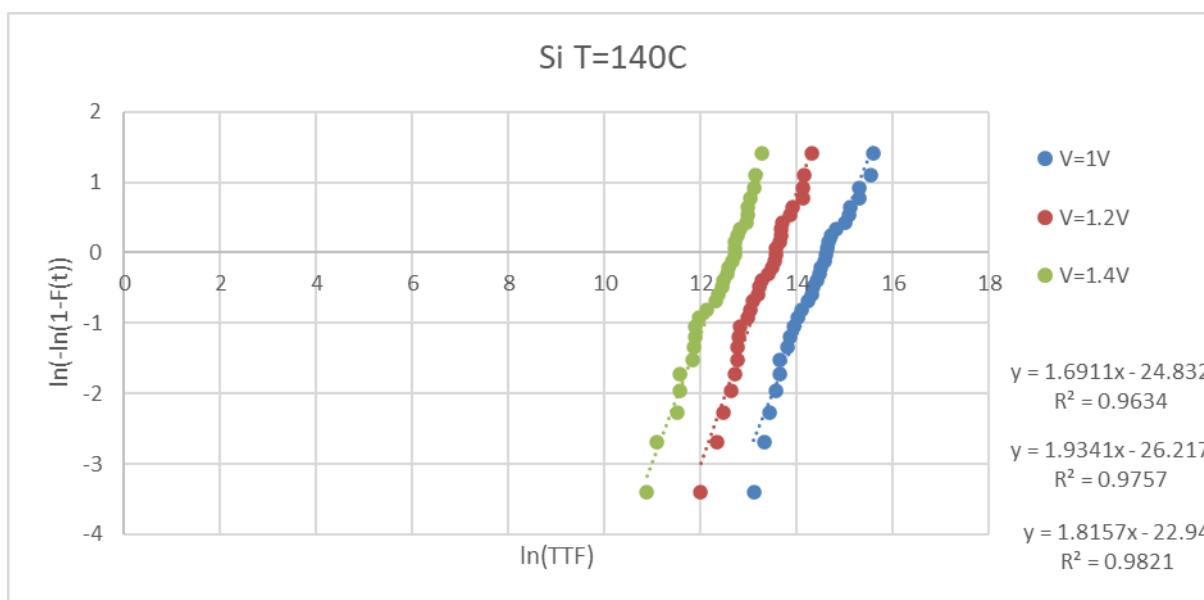


Image 3 – Si Weibull Graph T=140C

Using the linear equations from the graphs the, β is found from the slope, and $\theta = \exp\left(\frac{\text{intercept}}{\beta}\right)$.

$MTTF = \theta \cdot \Gamma\left(1 + \frac{1}{\beta}\right)$, $\Gamma(Z)$ is the Gamma function calculated in Excel.

Table 1 – Silicon β , θ , MTTF calculation and values

	$\beta = \text{slope}$	b- intercept	$\theta = \exp(b/\beta)$	$(1+1/\beta)$	$\Gamma(1+1/\beta)$	MTTF
T100C_V1_0	1.0379	16.779	10493822.74	1.963483958	0.985106906	10337537.25
T100C_V1_2	1.4451	22.074	4304052.029	1.691993634	0.907145945	3904403.345
T100C_V1_4	1.3254	18.587	1231435.304	1.754489211	0.920091209	1133032.798
T120C_V1_0	1.4274	21.792	4269122.555	1.700574471	0.908747718	3879555.378
T120C_V1_2	1.4391	20.471	1505841.99	1.694878744	0.907678254	1366820.028
T120C_V1_4	1.4443	19.506	733442.4372	1.69237693	0.907216299	665390.9334
T140C_V1_0	1.6911	24.832	2383149.605	1.591331086	0.892568402	2127124.034
T140C_V1_2	1.9341	26.217	770767.4043	1.517036348	0.886897729	683591.8608
T140C_V1_4	1.8157	22.94	306890.3343	1.550751776	0.888923518	272802.0356

Once MTTF was calculated, the TTF can be used to find the Ea and Gamma of the materials.

Using the equation: $TTF = A \cdot e^{\frac{Ea}{KT}} \cdot e^{-\gamma \cdot V}$ for silicon the Ea and γ can be found by using 2 graphs, one dependent on V and the other dependent on $\frac{1}{KT}$. The slopes of the graphs will be the Ea and γ values, which can be resubstituted into the equations until the graphs show no change. At this point the values can be confirmed. Afterwards the A can be found by solving for A in the equation $TTF = A \cdot e^{\frac{Ea}{KT}} \cdot e^{-\gamma \cdot V}$ using calculated Ea and gamma, and T and V values from the experiment data.

Table 2 – Silicon T' and V' for Ea and Gamma, A calculation

	T100C_V1_0	T100C_V1_2	T100C_V1_4	T120C_V1_0	T120C_V1_2	T120C_V1_4	T140C_V1_0	T140C_V1_2	T140C_V1_4
Voltage	1	1.2	1.4	1	1.2	1.4	1	1.2	1.4
Temp [K]	373	373	373	393	393	393	413	413	413
MTTF	10337537.25	3904403.345	1133032.798	3879555.378	1366820.028	665390.9334	2127124.034	683591.8608	272802.0356
1/KT	31.1125	31.1125	31.1125	29.5292	29.5292	29.5292	28.0992	28.0992	28.0992
Ln(TTF)	16.15129222	15.17761554	13.94040849	15.17123111	14.12799745	13.40813002	14.57028141	13.43511632	12.51650167
T'=exp(Ea/KT)	12566105.83	12566105.83	12566105.83	5469129.842	5469129.842	5469129.842	2580042.109	2580042.109	2580042.109
V'=exp(-V*Gamm	0.006584084	0.002410985	0.000882863	0.006584084	0.002410985	0.000882863	0.006584084	0.002410985	0.000882863
ln(TTF/V')	21.17439222	21.20533554	20.97274849	20.19433111	20.15571745	20.44047002	19.59338141	19.46283632	19.54884167
ln(TTF/T')	-0.195221513	-1.168898197	-2.406105247	-0.343398972	-1.386632631	-2.106500067	-0.193034872	-1.328199954	-2.246814611
A=TTF/(V'*T')	124.9456056	128.8722757	102.1287991	107.7378572	103.6569997	137.8050401	125.2191157	109.8944155	119.7642693

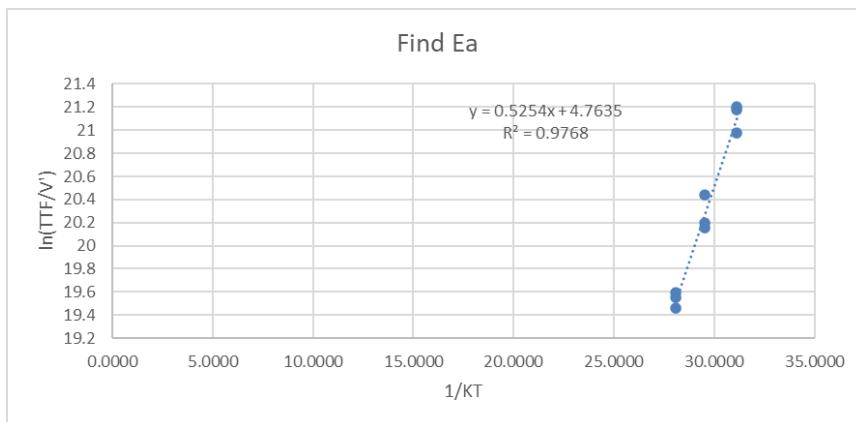


Image 4 – Si finding Ea

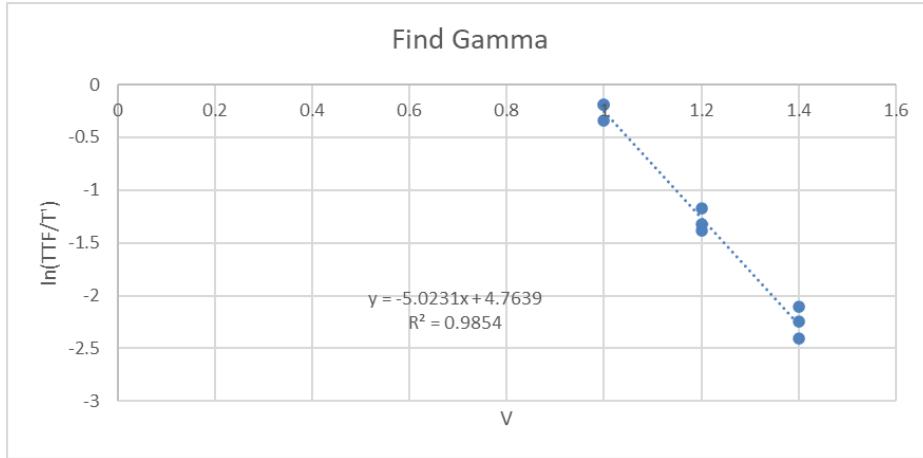


Image 5 – Si finding Gamma

Using the slope from the graphs in accordance with our equations the following parameters were found;

$$Ea = 0.5254$$

$$\gamma = 5.0231$$

The values from table 2 show the A constant for each condition. The average of these values is;

$$A_{avg} = 117.78$$

To get a more accurate A value, the *solver* will be used to minimize the sum of the error between the measured and calculated TTF values (based off of the each T/V individual calculated A values, or by a constant A value).

Table 3 – Finding the optimized A value using solver

	TTFmeas	Voltage	Temp [K]	1/KT	A=TTF/(V*T')	TTF calc	Error=((mea-calc)^2)
T100C_V1_0	10337537	1	373	31.11251187	124.9456056	10120752.89	46995456909
T100C_V1_2	3904403	1.2	373	31.11251187	128.8722757	3706055.33	39341934949
T100C_V1_4	1133033	1.4	373	31.11251187	102.1287991	1357097.269	50204887256
T120C_V1_0	3879555	1	393	29.52917793	107.7378572	4404842.073	2.75926E+11
T120C_V1_2	1366820	1.2	393	29.52917793	103.6569997	1612981.625	60595531456
T120C_V1_4	665390.9	1.4	393	29.52917793	137.8050401	590647.6732	5586554946
T140C_V1_0	2127124	1	413	28.09919353	125.2191157	2077968.225	2416293515
T140C_V1_2	683591.9	1.2	413	28.09919353	109.8944155	760918.2141	5979364921
T140C_V1_4	272802	1.4	413	28.09919353	119.7642693	278635.8913	34033873.25
					SUM		4.8708E+11

After using the solver, the optimized A value was found: $A_{solver} = 122.325$

Using all this information the lifetime model equation for Silicon can be built:

$$TTF(T, V) = 122.325 \cdot e^{\frac{0.5254}{KT}} \cdot e^{-5.0231 \cdot V}$$

GaN Analysis

The given information for GaN includes the time in hours and RDS values at different Temperatures and Voltages. The RDS vs time plot will be graphed for each condition as an exponential curve. Using the following the TTF can be calculated:

$$TTF = 20\% \text{ rise in RDS}$$

$$TTF = 1.2 \text{ RDS}$$

$$e^{at} = 1.2 \rightarrow \frac{\ln(1.2)}{a} = t = TTF$$

The GaN degradation curves can be viewed below:

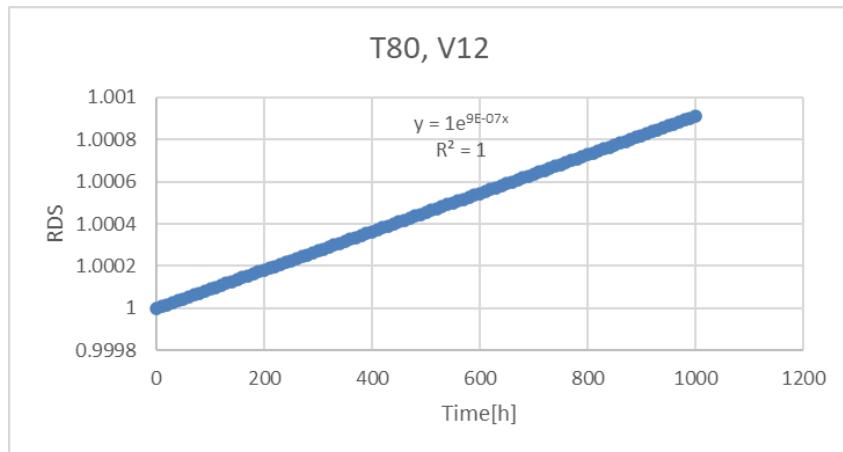


Image 6 – GaN Degradation Curve T80, V12

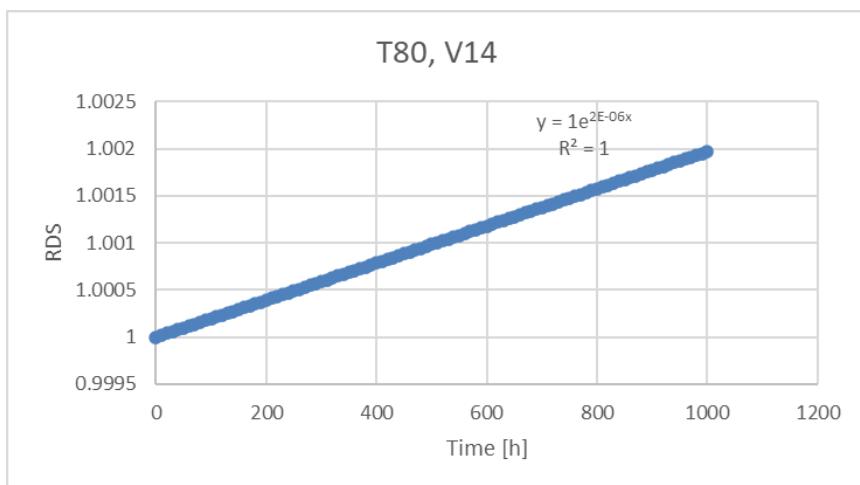


Image 7 – GaN Degradation Curve T80, V14

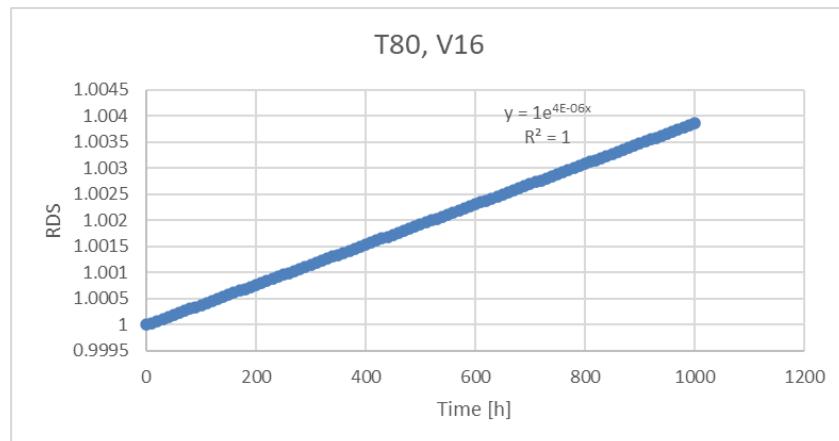


Image 8 – GaN Degradation Curve T80, V16

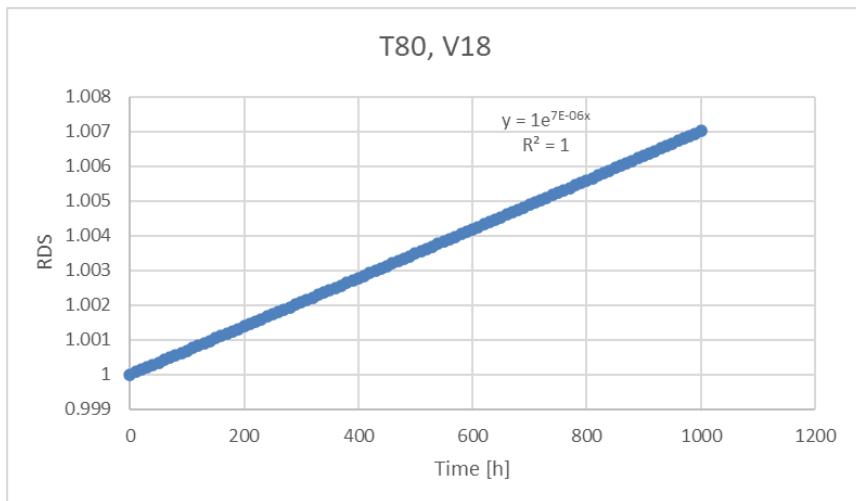


Image 9 – GaN Degradation Curve T80, V18

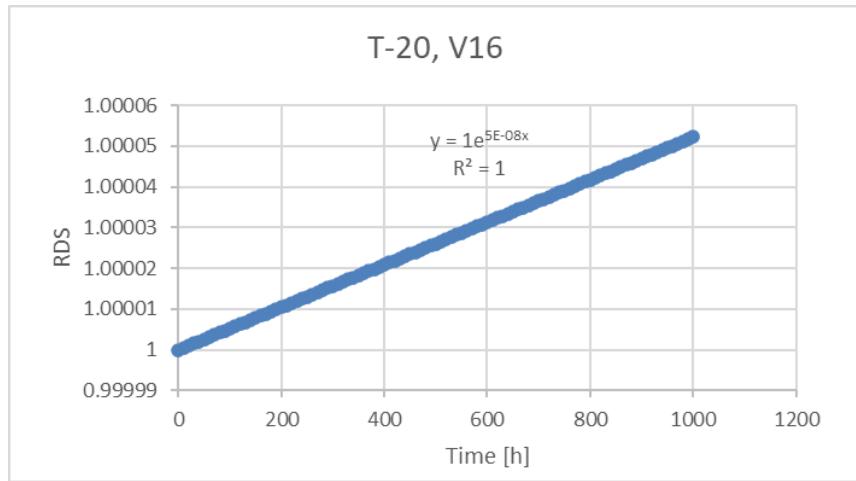


Image 10 – GaN Degradation Curve T -20, V16

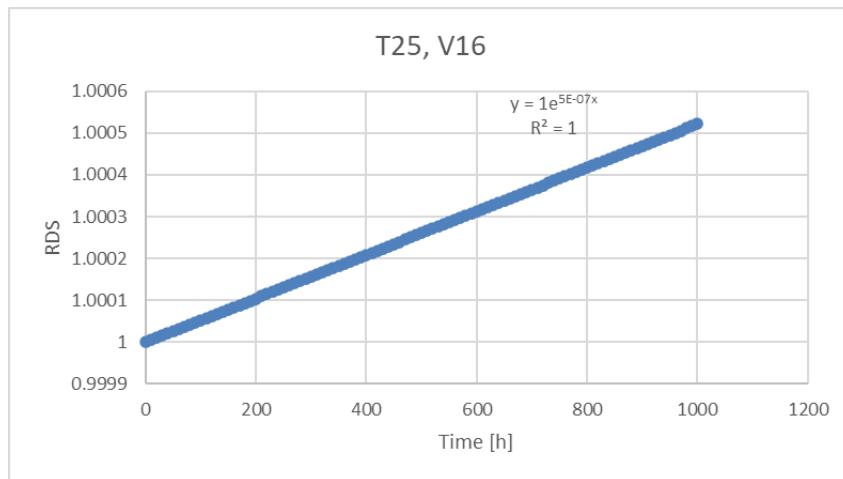


Image 11 – GaN Degradation Curve T25, V16

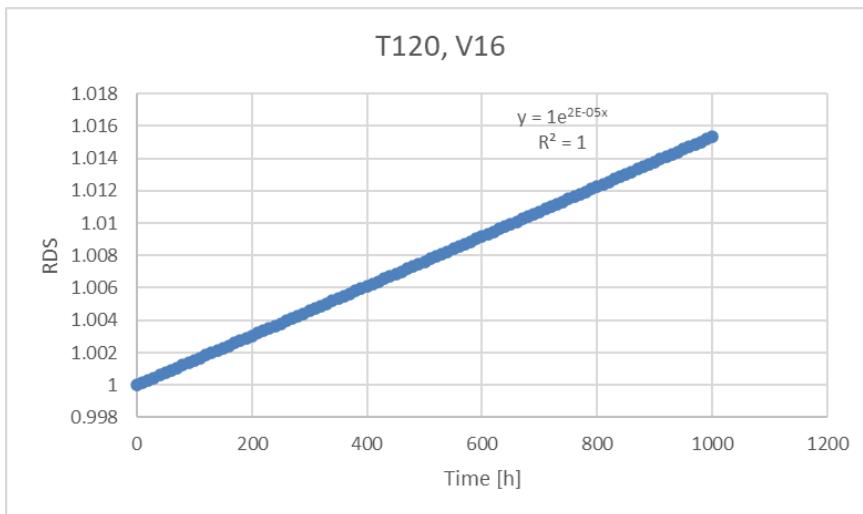


Image 12 – GaN Degradation Curve T120, V16

Using the exponential equation from the graphs, the a values of each condition can be obtained. This can be used to calculate the TTF for each condition using the equations above.

Table 4 – TTF of GaN Trials

	T80C_V12V	T80C_V14V	T80C_V16V	T80C_V18V	T-20C_V16V	T25C_V16V	T120C_V16V
a	9.00E-07	2.00E-06	4.00E-06	7.00E-06	5.00E-08	5.00E-07	2.00E-05
TTF	202579.51	91160.78	45580.39	26045.94	3646431.14	364643.11	9116.08

The equation $TTF(T, V) = -\gamma V * e^{\frac{Ea}{KT}}$ is used for GaN to find Ea and γ values.

Using the same method as with Silicon and Graphing $\ln(TTF)$ vs $1/KT$ and $\ln(TTF)$ vs V .

At least 3 trials of the same T values and same V values are needed to obtain a usable model. In this case there are 4 of each T and V.

Afterwards the A constant values from the TTF equation will be found for each condition by solving for A using the found Ea and gamma values.

In the first graph T= 80C is constant. Using log laws the equation can be written as the following:

$$\text{Constant } T: \ln(TTF) = -\gamma \ln(V) + \ln(C)$$

Table 5 – Finding Ea for GaN T=80C

V	T(K)	TTF	1/KT	Ln(TTF)	LN(V)	A
12	353	202579.5	32.875260	12.21889	2.484907	439803.8
14	353	91160.78	32.875260	11.42038	2.639057	432899.5
16	353	45580.39	32.875260	10.72723	2.772589	426388.4
18	353	26045.94	32.875260	10.16762	2.890372	443087.2

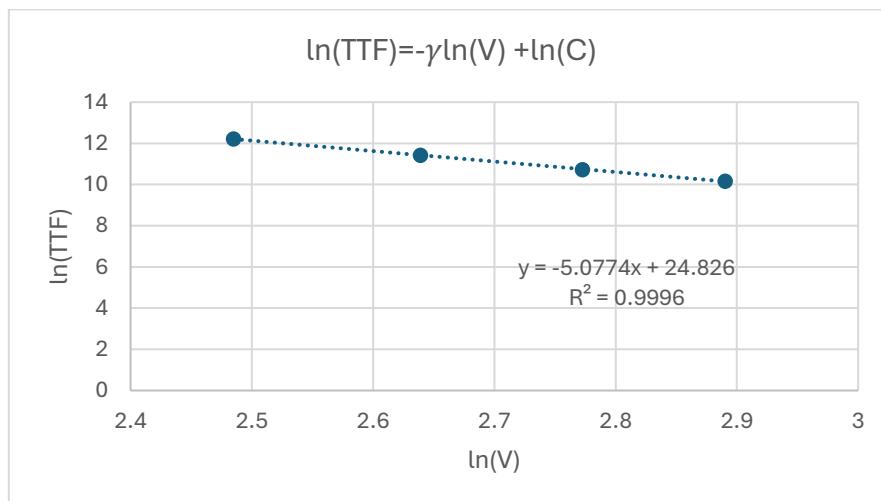


Image 13 – GaN deriving Gamma

In the second graph Voltage is constant at V=16V.

$$\text{Constant } V: \ln(TTF) = \frac{Ea}{KT} + \ln(C)$$

Table 6 – Finding Ea for GaN V=16V

V	T(K)	TTF	1/KT	Ln(TTF)	A
16	253	3646431.136	45.869434	15.10926	316358.4
16	298	364643.1136	38.942842	12.80667	383465.4
16	353	45580.3892	32.875260	10.72723	426388.4
16	393	9116.07784	29.529178	9.117795	284624.8

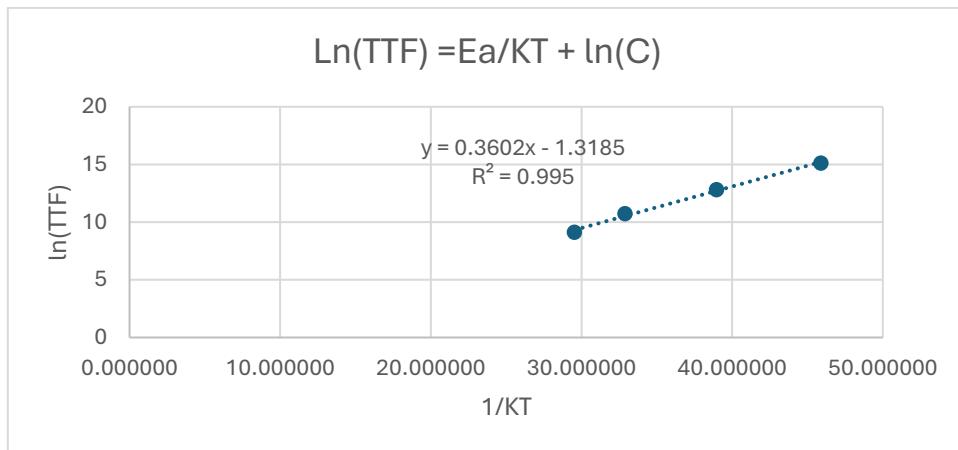


Image 14 – GaN deriving E_a

Using the outcomes of the slopes of each graph:

$$E_a = 0.3602$$

$$\gamma = 5.0774$$

A is calculated table 5 and 6 by solving the TTF equation for A. Then the average A value is found;

$$A_{avg} = 384480.3382$$

To get a more accurate A value , the solver will be used to minimize the sum of the error between the measured and calculated TTF values (based off of the each T/V individual calculated A values).

Table 7 – Optimizing A using solver

	V	T(K)	1/KT	A	$\ln(A)$	TTFmeas	MODELindA	Error=(meas-calc)^2
T80C_V12V	12	353	32.87526041	439803.7753	12.99408394	202579.5075	146040.9506	3196608417
T80C_V14V	14	353	32.87526041	432899.5122	12.97826091	91160.7784	66766.56321	595077734.5
T80C_V16V	16	353	32.87526041	426388.4307	12.96310602	45580.3892	33893.05451	136593792.2
T80C_V18V	18	353	32.87526041	443087.1765	13.00152182	26045.93668	18637.55305	54884148.12
T-20C_V16V	16	253	45.86943449	316358.4393	12.66463115	3646431.136	3654489.219	64932705.59
T25C_V16V	16	298	38.94284203	383465.3951	12.85700466	364643.1136	301494.873	3987700289
T120C_V16V	16	393	29.52917793	284624.7764	12.55892702	9116.07784	10154.84773	1079042.89
						SUM		8036876129

$$A_{solver} = 317057.546$$

With this the life time equation can be build for GaN:

$$TTF(T, V) = 317057.546 \cdot V^{-5.0774} \cdot e^{\frac{0.3602}{KT}}$$

Reliability Prediction

Using the fitted compact models, a safe operating region will be determined for the electric scooter.

Using the TZ: 342785912

The safe operating region will be:

$$R(t = 17 \text{ yrs.}) \geq 99.12\% \text{ where } R(t) = e^{\frac{-t}{TTF(V,T)}}.$$

$$t = 17 \text{ yrs.} \cdot 365 \text{ days} \cdot 24 \text{ hours} = 148920 \text{ [hours]}$$

$$TTF_{Si}(T, V) = 122.325 \cdot e^{\frac{0.5254}{KT}} \cdot e^{(-5.0231 \cdot V)}$$

$$TTF_{GaN}(T, V) = 317057.546 \cdot V^{(-5.0774)} \cdot e^{\frac{0.3602}{KT}}$$

A sweep of the reliability for each of the materials was done using Temperatures from 10°C to 200°C (jumps of 10°C) and Voltages of 0.1V to 2V (jumps of 0.1V) for the Si component and 1V to 20V (jumps of 1V) for the GaN component.

The reliability of the system was found by taking the minimum reliability at each given temperature:

$$TTF_{sys} = \min(TTF_{Si}, TTF_{GaN}).$$

$$R(t)_{sys} = e^{\left(\frac{-t}{TTF_{sys}(T,V)}\right)}$$

The calculated values were then filtered to give the highest Voltage for each material at the given temperature where the $R(t = 17 \text{ yrs.})_{sys} \geq 99.12\%$. These values were graphed and plotted.

These values show the required parameters the electric scooter needs to last the required 17 years and the requested reliability of 99.12%.

Table 8 – TTF Si (T/V)

T V	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9	2
10	1.68369e+11	1.0189e+11	61653948280	37308727146	22576674489	13661849920	8267211512	5002747548	3027318581	1821924898	1.109e+09	670821144	405934798	245643808	148646730	89950772.64	54432018.17	32938512	19932120.98	12061548.11
20	80707481250	4.8839e+10	29553768799	17883907304	10822110128	654879630	3962880595	239062874	1451124643	878131675.4	531384867	321557557	194584507	117749155	712536862	43117828.01	26091942.61	15789048.3	59544540.64	5781693.047
30	40611108973	2.4575e+10	14871128508	899893704	5445565726	3295281673	199407723	120676827	73019874.7	44186614.7	267386668	161804194	97912765	59250068	35854064.2	21696412.58	13129175.99	7944873.9	4807691.004	2909283.783
40	21351806381	1.2921e+10	7818684705	4731329897	2863075349	1732536196	1048411691	634426615.4	38391133.3	232316722.3	140582095	85070610	51478880	31151475.9	18850729.7	11407164.5	6902831.04	4177118.37	2527704.612	1529592.902
50	11681885768	7069073446	4277716833	2588579882	1566430426	947895909.4	573610180.5	347104086.5	21043509.7	127103878.9	76914522	46543376	2104324.8	10313510.1	62410206.65	3776539.889	2285362.59	1382944.188	836862.6634	
60	66270186109	4010253786	242672965	1468489803	888628983.2	537737114.9	325401500.7	196910597.6	1119156744.5	72105462.67	43633262	26403849	1597779.9	9668660.77	5850808.21	3540506.538	2142470.93	1296475.99	784538.097	47748.4504
70	388857063	2351453312	1422937743	861064011.1	521056690.4	315307655.6	190802497.1	115460542.3	69868775.48	42279775.31	25584811	15482167	9368742.2	5669318.1	3430681.22	2076012.21	1256259.741	760201.953	460021.9132	278373.6081
80	2348477912	1421137236	85974467.9	520397373.9	314909886.2	190516061.1	115314444.9	69780367.36	22622676.8	25525437.17	15462577	9356887.5	5662144.5	3426340.22	2073385.34	1254670.139	759240.0352	459438.827	278021.3695	168239.4024
90	1459270301	88304975	534361083.1	323358558.6	195674349.7	118408652.2	71652768.74	43359325.28	26238080.14	15877480.68	9607958.8	58140705.5	3518278.5	2129020.03	1288336.43	779612.5575	471767.8753	285481.493	172753.7336	104538.6725
100	930176742.1	562878960	340615615.2	206117132.9	124727905.1	574576746.8	45673333.4	27638358.63	16724832.87	10120718.03	6124362.2	3706042.6	2242642	1357092.59	821219.058	496945.2665	300717.081	181973.28	110117.109	66635.66151
110	607026645.1	367330757	222283298.6	13451057.2	81396533.67	49255581.35	29860688.6	18036593.89	10914505.54	6604707.737	3996714.7	2418536.7	1463532	885628.85	535921.646	324302.9037	196245.8024	118754.495	71862.02544	43485.95303
120	404839609.5	244801705	148245689.7	89708090.74	54285163.78	32849645.81	19878345.29	12029006.76	727917.184	4404826.902	2665498.1	1612976.1	970602.13	590645.63	357418.099	216284.998	130880.7027	79199.955	47926.38758	29001.75199
130	275479316.3	166701127	100876053.1	61043245.6	36939171.59	22353044.9	13526524.68	8185321.98	4953193.642	2997331.967	1813779.9	1097574.3	664176.43	401913.876	243210.623	147174.3337	80597.798	53892.850	32612.24488	1974.68658
140	190981613.2	115568931	69934364.86	42319465.49	2506882.55	15496700.92	9377537.081	5674640.182	3433901.771	207961.068	1257439.1	760915.9	460453.76	278634.932	168610.63	102031.5864	61742.49541	37362.309	22609.0901	13681.47101
150	15520342.8	81520342.3	5953051.83	2185425.32	18064028.55	10931107.11	6614753.864	4002793.883	2422215.429	1465758.107	886975.95	536736.81	324796.13	196544.303	118935.06	71971.33157	43521.0975	26354.7327	1548.07047	9650.675057
160	96570062.79	5847557.1	33562388.52	2139884.28	1249132.33	783932.868	4741761.941	2869388.0	1736356.208	1050723.3	635825.44	38475.81	232828.95	140892.06	852851.799	51592.3892	31220.16072	18892.293	11432.31578	6918.050866
170	70274151.72	425250811.1	25732352.98	15571994.02	9423099.288	5702211.294	3450585.91	2088057.162	1263548.517	764612.6188	462690.94	279988.72	169429.91	102527.323	62042.4808	37543.8403	22718.94879	13747.9445	8319.31051	5034.273999
180	51861311.6	31382897.2	1890769.99	11491907.26	94954111.524	4208149.788	2546482.693	1540956.105	932480.607	564273.0976	341459.25	206627.64	125036.83	75663.6871	45786.4571	27706.81328	16765.25692	10145.785	6139.530969	3715.221687
190	38778522.29	23466093.4	1420065.03	8592902.264	519883.179	3146581.244	1904094.455	1152226.945	697248.4637	421926.7932	255321.06	154502.74	93494.42	56576.3935	34236.1404	20717.35641	12536.71858	7586.35943	4590.742717	2778.001608
200	29354681.75	17763433.5	1074920.68	6504680.847	3936185.267	2381908.478	1441367.114	872216.1983	527805.2268	319391.4054	193273.7	116955.95	70773.69	42827.3676	25916.1759	15682.6864	9490.8287	5742.74505	3475.114149	2102.899663

This table shows all the TTF values for Silicon under 20 different voltages for each of the 20 different temperatures. As Temperature and Voltages grows, the TTF becomes smaller.

Table 9 – R(t=17 yrs.) Si (T/V)

T	V	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
10	0.1	0.99999116	0.99999153	0.99999190	0.99999240	0.99999304	0.99999367	0.99999438	0.99999503	0.99999569	0.99999632	0.99999693	0.99999754	0.99999814	0.99999863	0.998345797	0.997267849	0.99545204	0.992556484	0.977292934	
20	0.2	0.99999116	0.99999153	0.99999190	0.99999240	0.99999304	0.99999367	0.99999438	0.99999503	0.99999569	0.99999632	0.99999693	0.99999754	0.99999814	0.99999863	0.998345797	0.997267849	0.99545204	0.992556484	0.977292934	
30	0.3	0.99999116	0.99999153	0.99999190	0.99999240	0.99999304	0.99999367	0.99999438	0.99999503	0.99999569	0.99999632	0.99999693	0.99999754	0.99999814	0.99999863	0.998345797	0.997267849	0.99545204	0.992556484	0.977292934	
40	0.4	0.99999116	0.99999153	0.99999190	0.99999240	0.99999304	0.99999367	0.99999438	0.99999503	0.99999569	0.99999632	0.99999693	0.99999754	0.99999814	0.99999863	0.998345797	0.997267849	0.99545204	0.992556484	0.977292934	
50	0.5	0.99999116	0.99999153	0.99999190	0.99999240	0.99999304	0.99999367	0.99999438	0.99999503	0.99999569	0.99999632	0.99999693	0.99999754	0.99999814	0.99999863	0.998345797	0.997267849	0.99545204	0.992556484	0.977292934	
60	0.6	0.99999116	0.99999153	0.99999190	0.99999240	0.99999304	0.99999367	0.99999438	0.99999503	0.99999569	0.99999632	0.99999693	0.99999754	0.99999814	0.99999863	0.998345797	0.997267849	0.99545204	0.992556484	0.977292934	
70	0.7	0.99999116	0.99999153	0.99999190	0.99999240	0.99999304	0.99999367	0.99999438	0.99999503	0.99999569	0.99999632	0.99999693	0.99999754	0.99999814	0.99999863	0.998345797	0.997267849	0.99545204	0.992556484	0.977292934	
80	0.8	0.99999116	0.99999153	0.99999190	0.99999240	0.99999304	0.99999367	0.99999438	0.99999503	0.99999569	0.99999632	0.99999693	0.99999754	0.99999814	0.99999863	0.998345797	0.997267849	0.99545204	0.992556484	0.977292934	
90	0.9	0.99999116	0.99999153	0.99999190	0.99999240	0.99999304	0.99999367	0.99999438	0.99999503	0.99999569	0.99999632	0.99999693	0.99999754	0.99999814	0.99999863	0.998345797	0.997267849	0.99545204	0.992556484	0.977292934	
100	0.1	0.99999116	0.99999153	0.99999190	0.99999240	0.99999304	0.99999367	0.99999438	0.99999503	0.99999569	0.99999632	0.99999693	0.99999754	0.99999814	0.99999863	0.998345797	0.997267849	0.99545204	0.992556484	0.977292934	
110	0.2	0.99999116	0.99999153	0.99999190	0.99999240	0.99999304	0.99999367	0.99999438	0.99999503	0.99999569	0.99999632	0.99999693	0.99999754	0.99999814	0.99999863	0.998345797	0.997267849	0.99545204	0.992556484	0.977292934	
120	0.3	0.99999116	0.99999153	0.99999190	0.99999240	0.99999304	0.99999367	0.99999438	0.99999503	0.99999569	0.99999632	0.99999693	0.99999754	0.99999814	0.99999863	0.998345797	0.997267849	0.99545204	0.992556484	0.977292934	
130	0.4	0.99999116	0.99999153	0.99999190	0.99999240	0.99999304	0.99999367	0.99999438	0.99999503	0.99999569	0.99999632	0.99999693	0.99999754	0.99999814	0.99999863	0.998345797	0.997267849	0.99545204	0.992556484	0.977292934	
140	0.5	0.99999116	0.99999153	0.99999190	0.99999240	0.99999304	0.99999367	0.99999438	0.99999503	0.99999569	0.99999632	0.99999693	0.99999754	0.99999814	0.99999863	0.998345797	0.997267849	0.99545204	0.992556484	0.977292934	
150	0.6	0.99999116	0.99999153	0.99999190	0.99999240	0.99999304	0.99999367	0.99999438	0.99999503	0.99999569	0.99999632	0.99999693	0.99999754	0.99999814	0.99999863	0.998345797	0.997267849	0.99545204	0.992556484	0.977292934	
160	0.7	0.99999116	0.99999153	0.99999190	0.99999240	0.99999304	0.99999367	0.99999438	0.99999503	0.99999569	0.99999632	0.99999693	0.99999754	0.99999814	0.99999863	0.998345797	0.997267849	0.99545204	0.992556484	0.977292934	
170	0.8	0.99999116	0.99999153	0.99999190	0.99999240	0.99999304	0.99999367	0.99999438	0.99999503	0.99999569	0.99999632	0.99999693	0.99999754	0.99999814	0.99999863	0.998345797	0.997267849	0.99545204	0.992556484	0.977292934	
180	0.9	0.99999116	0.99999153	0.99999190	0.99999240	0.99999304	0.99999367	0.99999438	0.99999503	0.99999569	0.99999632	0.99999693	0.99999754	0.99999814	0.99999863	0.998345797	0.997267849	0.99545204	0.992556484	0.977292934	
190	1.0	0.99999116	0.99999153	0.99999190	0.99999240	0.99999304	0.99999367	0.99999438	0.99999503	0.99999569	0.99999632	0.99999693	0.99999754	0.99999814	0.99999863	0.998345797	0.997267849	0.99545204	0.992556484	0.977292934	
200	0.99999116	0.99999153	0.99999190	0.99999240	0.99999304	0.99999367	0.99999438	0.99999503	0.99999569	0.99999632	0.99999693	0.99999754	0.99999814	0.99999863	0.998345797	0.997267849	0.99545204	0.992556484	0.977292934		

This table shows the reliability of Silicon under the different temperatures and voltage conditions lin a time of 17 years. Marked in red on the table shows at which Temperatures and Voltages the reliability of below the desired reliability of 92.12%.

Table 10 – TTF GaN

T	V	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
10	2.44087E+11	3114835699	722892488.3	32821354.7	92254583.66	42176673.49	21410326.08	11773408	6895616.686	4250166	16504482	1092600	754546.92	429173.1	88000.485	348700.439	264900.059	204231.822			
20	4.97796E+11	1.4743E+10	188147358	436653919.9	140632748	57525195.98	25647277.4	12932654.14	711157.839	4165208.665	2567258.2	16504482	1092600	754546.92	429173.1	88000.485	348700.439	264900.059	204231.822		
30	3.10851E+11	9.2606589	1.27657935.4	87821602.72	3479878.83	1590929.63	807616.193	444099.673	167119.95	3437298.105	1603187.9	103063.3	686460	471195.39	331948.23	283915.498	17737.4606				
40	2.00047E+11	5.92947053	7.6513135	1.4782907	1.028395.61	1.203895.61	1.279695.61	1.351695.61	1.427695.61	1.497695.61	1.567695.61	1.637695.61	1.707695.61	1.777695.61	1.847695.61	1.917695.61	1.987695.61	2.057695.61	2.127695.61	2.197695.61	
50	1.33020E+11	2.99950183	1.99950183	1.99950183	1.99950183	1.99950183	1.99950183	1.99950183	1.99950183	1.99950183	1.99950183	1.99950183	1.99950183	1.99950183	1.99950183	1.99950183	1.99950183	1.99950183	1.99950183	1.99950183	
60	8966839471	2.65665384	339308561	78683790	25341619.9	10401251.26	4590752.53	2390273.62	1281485.66	750588.712	462612.519	294706.198	138033.624	69312.768	303281.443	44171.203	153933.761	11349.1619	84647.098	64322.372	4975.3142
70	6220756270	1.9993218	1.9993218	1.9993218	1.9993218	1.9993218	1.9993218	1.9993218	1.9993218	1.9993218	1.9993218	1.9993218	1.9993218	1.9993218	1.9993218	1.9993218	1.9993218	1.9993218	1.9993218	1.9993218	
80	4404630798	1.30417248	1.6648452	1.86753759	1.244397.3	493087.74	252884.486	114439.049	578536.625	62927.268	32081.732	102652.747	492165.747	21362.226	153933.761	11349.1619	10637.9659	10.9659	10.9659	10.9659	10.9659
90	3178562156	1.20417248	1.20417248	1.20417248	1.20417248	1.20417248	1.20417248	1.20417248	1.20417248	1.20417248	1.20417248	1.20417248	1.20417248	1.20417248	1.20417248	1.20417248	1.20417248	1.20417248	1.20417248	1.20417248	
100	1.70405E+11	1.5915685	1.5915685	1.5915685	1.5915685	1.5915685	1.5915685	1.5915685	1.5915685	1.5915685	1.5915685	1.5915685	1.5915685	1.5915685	1.5915685	1.5915685	1.5915685	1.5915685	1.5915685	1.5915685	
110	1.07302E+11	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	
120	6202307292	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	1.5905168	
130	3.97320562	1.5905168	1.5905168	1.5905168	1																

Table 12 – TTF System = Min(TTF Si, TTF GaN)

T V	0.1 1	0.2 2	0.3 3	0.4 4	0.5 5	0.6 6	0.7 7	0.8 8	0.9 9	1 10	1.1 11	1.2 12	1.3 13	1.4 14	1.5 15	1.6 16	1.7 17	1.8 18	1.9 19	2 20
10	1.683696e+11	2.4408e+10	3114853699	722894288.3	232821354.7	9225583.66	21410673.49	11773408	6895616.686	4250166	2732362.1	1819856.5	1248173.1	880008485	63424177.5	466113.5826	348700.439	264990.0569	204231.8221	
20	80707481250	1.4743e+10	1881487358	436653919.9	140632748	55725195.98	25472677.4	12932654.14	711157.839	4165208.665	2567258.2	1650482.6	428538.922	281549.921	210623.02	16063.8393	12363.6082			
30	40611108973	9.99998896	1174941381	272679355.2	87812602.72	34798978.83	15092929.63	8076116.193	4440399.673	2601067.715	1603187.9	1030663.1	686407.0	471195.539	331948.823	239195.4185	175821.821	131531.886	99955.82893	77037.4606
40	21291887500	7.6581e+09	176518530.7	40565519.7	13078389.01	10000000.0	3479799.03	1603187.9	4440399.673	2601067.715	1603187.9	1030663.1	686407.0	471195.539	331948.823	239195.4185	175821.821	131531.886	99955.82893	49577.4606
50	11681885765	3.916470653	116055811.4	410655811.7	14810808.43	34737988.74	14011512.79	34737988.105	1890146.129	623327.25	1107074.741	50546.834	293214.44	101804.6237	141279.552	101804.6237	74531.58519	55981.6483	42542.47625	12624
60	6527801609	265653846	33093863.03	35341619.79	10041521.26	315973.532	332047.363	1281495.668	705658.129	462812.59	270406.05	98788.68	136967.209	98788.68	60921.73482	58234.40314	39854.5681	28842.53845	17337.7008	
70	388587063	1842446294	235130560.2	5456882.21	17574955.63	6964009.881	3183785.122	1616201.247	888737.742	520528.5292	320381.73	206257.47	137375.27	94296.169	66429.1627	47668.0516	35185.45601	26312.3052	20003.2703	15416.82126
80	234877912	1304574241	1664854954	238637597.2	12443977.31	49030879.074	2254284.486	1144354.049	629272.2685	368561.1128	227165.46	146040.49	97268.795	66765.5633	47035.282	33893.0546	24913.12214	18637.5531	14163.3494	10905.90659
90	1459270301	88304975	120143397.3	27882737.25	89810810.519	3558326.659	1626801.554	82821.6551	454113.5382	265971.6611	163933.66	105390.27	70193.903	48418.064	33942.9516	24458.8800	17978.52313	13449.7666	10220.96341	7877.450211
100	93017642.1	562878960	88231209.62	20476621	6594887.301	2613199.608	606468.9798	333493.094	195324.936	120390.02	77396.769	51549.175	35384.0226	24927.116	17962.17371	13203.1295	9877.27339	7506.99676	5785.61657	
120	404839695.0	244881075	49881184.47	11576381.21	3728396.995	1477362.454	675146.1298	342664.9789	188539.0432	110426.2226	680504.05	43755.974	2943.133	22004.2249	14092.4896	13045.48775	7464.33054	5584.07954	4241.543738	3270.562978
130	29793137.2	115568931	28981641.77	6916338.632	2227559.165	882653.3924	403529.104	204845.557	112641.186	65374.4209	40663.844	2614.219	17414.64	14951.5753	8419.59597	6097.039866	4450.5382451	3316.22260	2336.316105	1554.065251
140	1990813.2	115568931	28981641.77	6916338.632	2227559.165	882653.3924	403529.104	204845.557	112641.186	65374.4209	40663.844	2614.219	17414.64	14951.5753	8419.59597	6097.039866	4450.5382451	3316.22260	2336.316105	1554.065251
150	13471515.2	81520342.2	23459805.57	5444203.903	1753515.331	69281.8359	217657.475	161254.1006	88672.49934	51934.5678	32010.514	20570.035	13706.415	9408.26147	6637.81704	4775.96453	3510.57708	2616.269216	1985.798584	1538.19965
160	96570062.9	5843757.1	1867754.43	4333567.77	9830479.05	55304.7867	252838.4403	128349.6802	70578.5828	41337.46982	25478.665	16378.917	10909.577	7488.47532	5275.43325	3801.41331	2794.232486	2090.37053	1588.548056	124.317877
170	70274151.72	42525051.1	15015648.04	3485003.965	1122412.195	44475.15987	20330.2001	1032117.5572	56758.61103	323243.18883	20489.693	13172.488	8733.751	6022.15859	4242.45181	3075.03995	2247.094429	1681.05553	1277.494986	984.5844952
180	51861311.6	31382897.2	1219287.33	911359.003	361122.6457	165096.9666	83809.0284	46085.99462	26992.29938	16636.91	10695.597	7123.718	4889.7083	3444.224639	1824.651933	1364.57933	1037.280823	20315.460989	799.4479298	
190	3877852.29	23466093.4	989867.845	231838.985	74675.9126	29286.0991	15264.5461	68665.03852	37867.42327	22114.29129	16360.681	8762.9414	5836.54053	4006.21525	2023.07059	1703.22792	20315.460989	1494.86969	1118.315	849.8479566
200	29354681.75	17763433.5	8253801.703	1915343.99	616934.6876	24448.043	111760.5939	56733.6016	31197.41226	18272.14317	11262.175	7240.2678	4822.2921	3310.08389	2331.86675	1680.31493	125.117104	923.99406	702.1759589	541.177515

To find the TTF of the system, the minimum TTF for each condition was taken.

Table 13– R(t) System

T V	0.1 1	0.2 2	0.3 3	0.4 4	0.5 5	0.6 6	0.7 7	0.8 8	0.9 9	1 10	1.1 11	1.2 12	1.3 13	1.4 14	1.5 15	1.6 16	1.7 17	1.8 18	1.9 19	2 20
10	0.99998116	0.99998389	0.99998210	0.999980405	0.999965372	0.99674534	0.99308023	0.98740072	0.9836203	0.98051613	0.9858503	0.979731168	0.974417263	0.96472008	0.95837022	0.95177064	0.944513831	0.9375133	0.930402888	0.923004424
20	0.99998116	0.99998896	0.99998053	0.9999632	0.999948162	0.999943209	0.999937265	0.99993209	0.999927265	0.999922265	0.999917265	0.999912265	0.999907265	0.999902265	0.999897265	0.999892265	0.999887265	0.999882265	0.999877265	0.999872265
30	0.99998116	0.99998896	0.99998053	0.9999632	0.999948162	0.999943209	0.999937265	0.99993209	0.999927265	0.999922265	0.999917265	0.999912265	0.999907265	0.999902265	0.999897265	0.999892265	0.999887265	0.999882265	0.999877265	0.999872265
40	0.99998116	0.99998896	0.99998053	0.9999632	0.999948162	0.999943209	0.999937265	0.99993209	0.999927265	0.999922265	0.999917265	0.999912265	0.999907265	0.999902265	0.999897265	0.999892265	0.999887265	0.999882265	0.999877265	0.999872265
50	0.99998116	0.99998896	0.99998053	0.9999632	0.999948162	0.999943209	0.999937265	0.99993209	0.999927265	0.999922265	0.999917265	0.999912265	0.999907265	0.999902265	0.999897265	0.999892265	0.999887265	0.999882265	0.999877265	0.999872265
60	0.99998116	0.99998896	0.99998053	0.9999632	0.999948162	0.999943209	0.999937265	0.99993209	0.999927265	0.999922265	0.999917265	0.999912265	0.999907265	0.999902265	0.999897265	0.999892265	0.999887265	0.999882265	0.999877265	0.999872265
70	0.99998116	0.99998896	0.99998053	0.9999632	0.999948162	0.999943209	0.999937265	0.99993209	0.999927265	0.999922265	0.999917265	0.999912265	0.999907265	0.999902265	0.999897265	0.999892265	0.999887265	0.999882265	0.999877265	0.999872265
80	0.99998116	0.99998896	0.99998053	0.9999632	0.999948162	0.999943209	0.999937265	0.99993209	0.999927265	0.999922265	0.999917265	0.999912265	0.999907265	0.999902265	0.999897265	0.999892265	0.999887265	0.999882265	0.999877265	0.999872265
90	0.99998116	0.99998896	0.99998053	0.9999632	0.999948162	0.999943209	0.999937265	0.99993209	0.999927265	0.999922265	0.999917265	0.999912265	0.999907265	0.999902265	0.999897265	0.999892265	0.999887265	0.999882265	0.999877265	0.999872265
100	0.99998116	0.99998896	0.99998053	0.9999632	0.999948162	0.999943209	0.999937265	0.99993209	0.999927265	0.999922265	0.999917265	0.999912265	0.999907265	0.999902265	0.999897265	0.999892265	0.999887265	0.999882265	0.999877265	0.999872265
110	0.99998116	0.99998896	0.99998053	0.9999632	0.999948162	0.999943209	0.999937265	0.99993209	0.999927265	0.999922265	0.999917265	0.999912265	0.999907265	0.999902265	0.999897265	0.999892265	0.999887265	0.999882265	0.999877265	

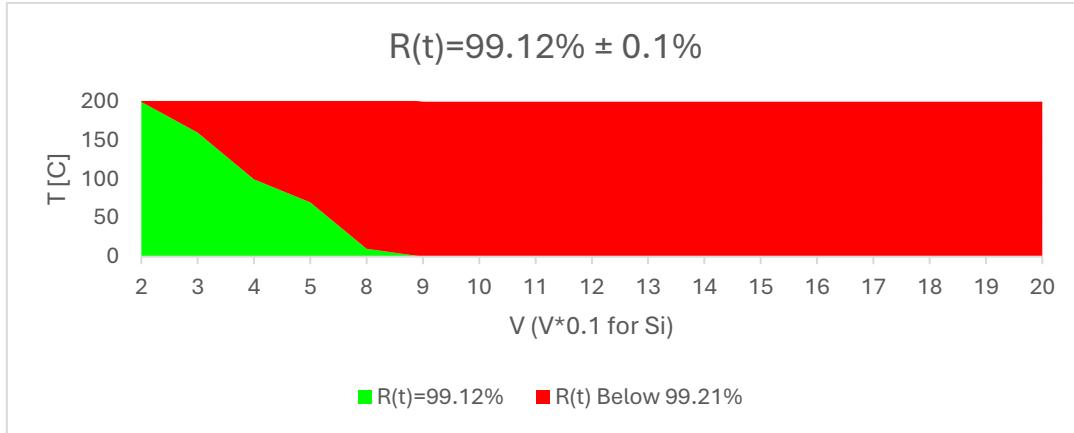


Image 15 – Boundary curve in the (Voltage, Temperature) plane where reliability is exactly 99.21%.

This graph shows where the system has a reliability of exactly 99.21% and marked in red above that is where the Reliability is lower than that.

To test which Material is the limiting factor the following logic was used in an excel equation:

IF(TTFSi<=TTFGan), if true then paste "Si", if false then paste "GaN" . If The TTF or Si was lower than it is the limiting factor, if the TTf of GaN is lower than it is the limiting factor.

Table 16 – Limiting Factor per T/V

T V	0.1 1	0.2 2	0.3 3	0.4 4	0.5 5	0.6 6	0.7 7	0.8 8	0.9 9	1 10	1.1 11	1.2 12	1.3 13	1.4 14	1.5 15	1.6 16	1.7 17	1.8 18	1.9 19	2 20
10	Si	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN							
20	Si	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN							
30	Si	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN							
40	Si	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN							
50	Si	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN							
60	Si	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN							
70	Si	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN							
80	Si	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN							
90	Si	Si	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN						
100	Si	Si	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN						
110	Si	Si	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN						
120	Si	Si	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN						
130	Si	Si	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN						
140	Si	Si	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN						
150	Si	Si	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN						
160	Si	Si	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN						
170	Si	Si	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN						
180	Si	Si	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN						
190	Si	Si	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN						
200	Si	Si	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN	GaN						

Based on the results, it can be clearly seen that GaN is the limiting factor at almost every condition, except for the lowest voltages. Since the system is in series, one does rely upon the other and the GaN failing first will cause the whole system to fail. These results assume of both components being at the same temperatures and Silicon have voltage 10% that of GaN at any given moment.

According to the data, the system is more sensitive to changes in Voltage rather than changes in temperature. This can be seen in Table 13 when looking at the change in system Reliability and how it changes based on T and V. For example, as $V=0.1V$, as the temperature is raised the $R(t)$ stays stable and high. When the temperature stays stable, for example at $100C$, as the voltage rises, the Reliability quickly drops and becomes unreliable even at relatively low voltages. From this it can be concluded that the system is more sensitive to Voltage.