

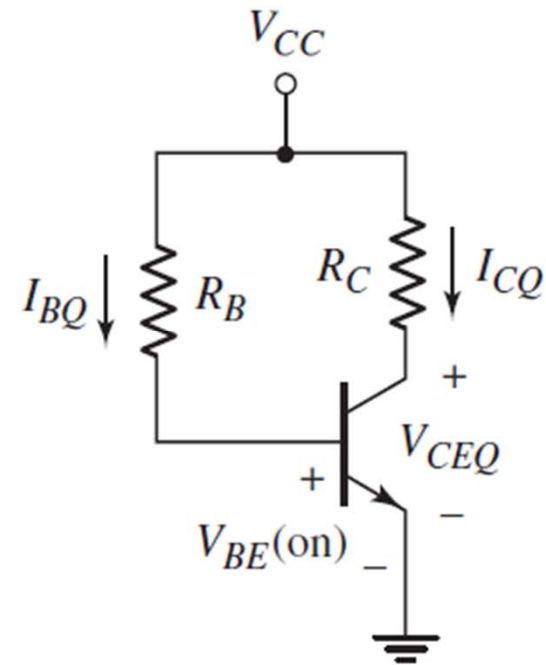
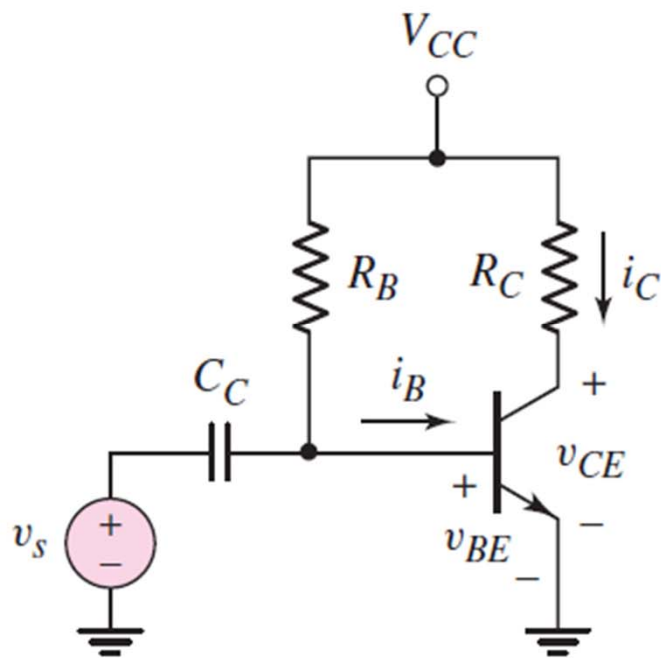
# **Bipolar Transistor Biasing**

**Linear amplifier** - keep the transistor in the forward-active mode,

- The signal source is not connected to ground
- May not want DC base current flowing through signal source

### **Single Base Resistor Biasing:**

- **Decoupling signal** source from **DC bias** by using a capacitor.
- The **signal** is connected to **ground**



DC equivalent

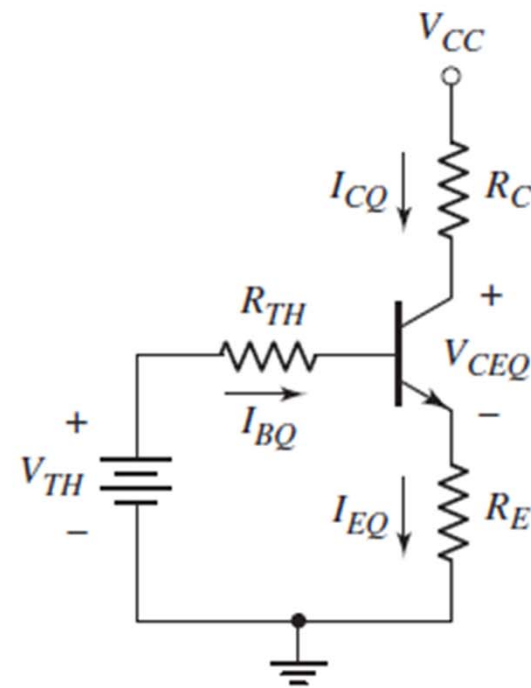
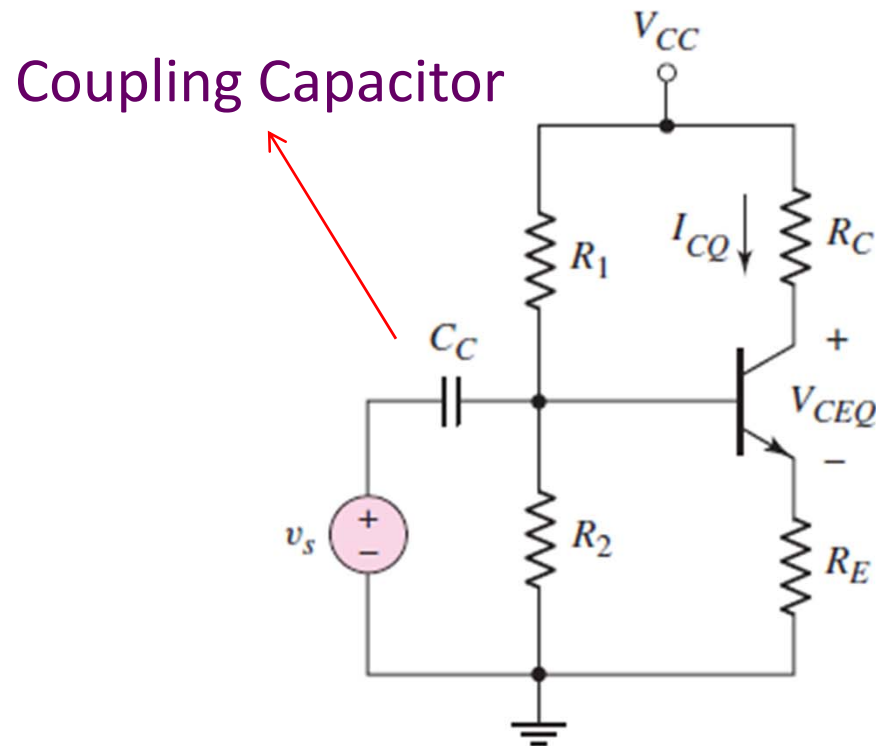
$$I_{BQ} = \frac{I_{CQ}}{\beta}$$

$$R_B = \frac{V_{CC} - V_{BE(on)}}{I_{BQ}} \quad R_C = \frac{V_{CC} - V_{CEQ}}{I_{CQ}}$$

$\beta$	50	100	150
Q-point values	$I_{CQ} = 0.50 \text{ mA}$ $V_{CEQ} = 9 \text{ V}$	$I_{CQ} = 1 \text{ mA}$ $V_{CEQ} = 6 \text{ V}$	$I_{CQ} = 1.5 \text{ mA}$ $V_{CEQ} = 3 \text{ V}$

# Voltage Divider Biasing and Bias Stability

Single bias resistor  $R_B$  is replaced by a pair of resistors  $R_1$  and  $R_2$ , and an emitter resistor  $R_E$  is added



DC equivalent

$$V_{TH} = [R_2/(R_1 + R_2)]V_{CC}$$

$$R_{TH} = R_1 \parallel R_2$$

Kirchhoff's law in BE loop:

$$V_{TH} = I_{BQ}R_{TH} + V_{BE}(\text{on}) + I_{EQ}R_E$$

$$I_{EQ} = (1 + \beta)I_{BQ}$$

$$I_{BQ} = \frac{V_{TH} - V_{BE}(\text{on})}{R_{TH} + (1 + \beta)R_E}$$

$$I_{CQ} = \beta I_{BQ} = \frac{\beta(V_{TH} - V_{BE}(\text{on}))}{R_{TH} + (1 + \beta)R_E}$$

Bias stability:

$$R_{TH} \ll (1 + \beta)R_E$$

$$I_{CQ} \cong \frac{\beta(V_{TH} - V_{BE(\text{on})})}{(1 + \beta)R_E}$$

$$\beta \gg 1 \quad \beta/(1 + \beta) \cong 1$$

$$I_{CQ} \cong \frac{(V_{TH} - V_{BE(\text{on})})}{R_E}$$

General rule  $\rightarrow R_{TH} \cong 0.1(1 + \beta)R_E$