

# 第二十讲 重力梯度稳定系统

主讲: 刘莹莹

西北工业大学 精确制导与控制研究所



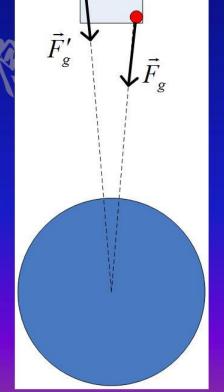
# 第二十讲 重力梯度稳定系统

- 1、重力梯度稳定原理
- 2、重力梯度力矩
- 3、重力梯度卫星稳定性分析

#### 1、重力梯度稳定原理

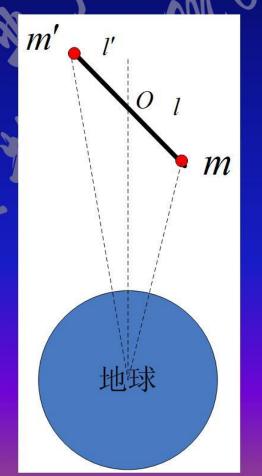
在引力场中,由于物体内各质点所受的引力不同,对其质心产生重力梯度为矩。

利用航天器重力梯度力矩,以及在轨道运动中产生的离心力力矩,产生一个恢复力矩。使航天器的某根体坐标轴指向地球。



### 用哑铃式结构说明重力梯度稳定原理

- (1) 哑铃两端质量相等 m = m'
- (2)哑铃两端距中心的臂长相等 1=1
- (3)哑铃臂无质量。





### 俯仰通道

哑铃式卫星在轨道平面内,即俯仰通 , 偏离当地垂线时的情况。

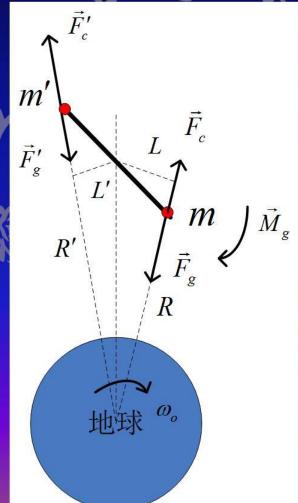
$$M_{g} = F_{g}L - F_{g}'L'$$

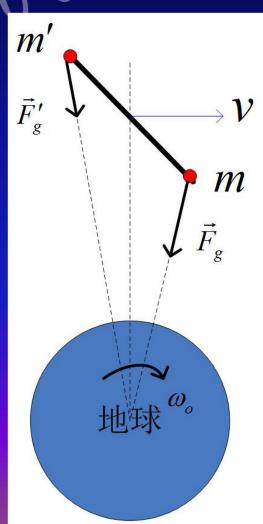
$$F_{g} > F_{g}' \quad L > L'$$

$$M_{c} = F_{c}'L' - F_{c}L$$

$$M_c = F_c' L' - F_c L$$

$$= m' \omega_0^2 R' L' - m \omega_0^2 R L$$





#### 滚动通道

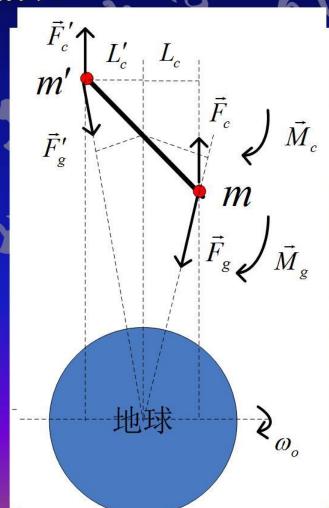
在轨道法平面(即滚动平面)内哑铃式 卫星偏离铅垂线的情况。

$$M_{g} = F_{g}L - F_{g}'L'$$

$$F_{g} > F_{g}' \quad L > L'$$

$$M_{c} = F_{c}'L_{c}' - F_{c}L_{c}$$

$$F_{c}' > F_{c} \quad L = L'$$

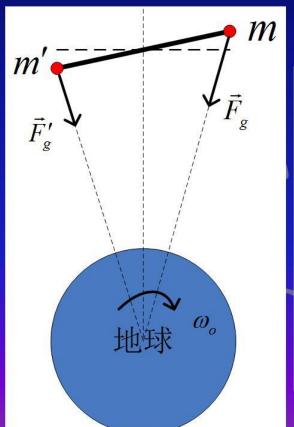


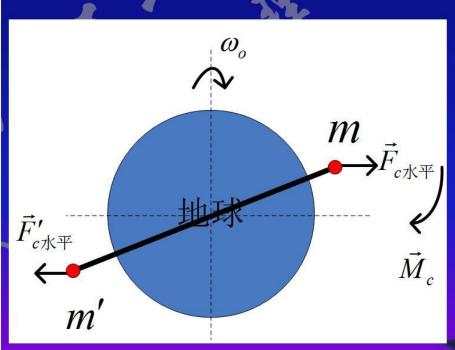






偏航平面内哑铃式卫星的情况。 在轨道平面内、水平平面内的投影





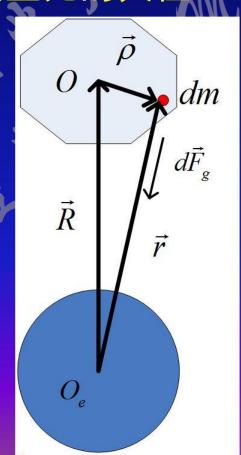
# 2、重力梯度力矩

任意质量分布航天器重力梯度力矩 从地球中心到任一质量元的矢径:

$$\vec{r} = \vec{R} + \vec{\rho}$$

#### 重力:

$$dF_g = -\frac{\mu dm}{r^3} \cdot \vec{r}$$





### 力矩

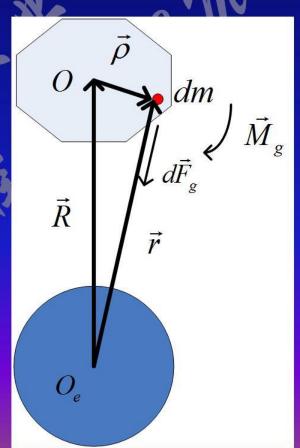
$$d\vec{M}_g = \vec{\rho} \times d\vec{F}_g$$

# 整个航天器受到的重力梯度力矩

$$\vec{M}_g = \int_m \vec{\rho} \times (-\frac{\mu}{r^3} \vec{r}) dm$$

$$= -\int_m \frac{\mu}{r^3} \vec{\rho} \times (\vec{R} + \vec{p}) dm$$

$$=-\int_{m}\frac{\mu}{r^{3}}\,\bar{\rho}\times\bar{R}dm$$





#### 整个航天器受到的重力梯度力矩

$$\vec{M}_{g} = -\int_{m} \frac{\mu}{r^{3}} \vec{\rho} \times \vec{R} dm$$

$$r = \left[ (\vec{R} + \vec{\rho}) \cdot (\vec{R} + \vec{\rho}) \right]^{1/2}$$

$$= \left[ R^{2} + 2\vec{R} \cdot \vec{\rho} + \rho^{2} \right]^{1/2} = R \left[ 1 + \frac{2\vec{R} \cdot \vec{\rho}}{R^{2}} + \frac{\rho^{2}}{R^{2}} \right]^{1/2}$$

$$\frac{1}{r^{3}} = \frac{1}{R^{3}} \left[ 1 + \frac{2\vec{R} \cdot \vec{\rho}}{R^{2}} \right]^{-3/2} \approx \frac{1}{R^{3}} (1 - \frac{3\vec{R} \cdot \vec{\rho}}{R^{2}})$$

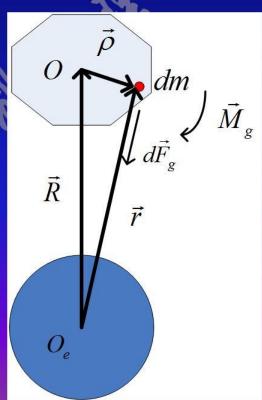
$$\vec{M}_{g} = -\frac{\mu}{R^{3}} \int_{m} (1 - \frac{3\vec{R} \cdot \vec{\rho}}{R^{2}}) \vec{\rho} \times \vec{R} dm$$

$$\vec{M}_g = -\frac{\mu}{R^3} \int_m (1 - \frac{3\vec{R} \cdot \vec{\rho}}{R^2}) \vec{\rho} \times \vec{R} dm$$

$$= -\frac{\mu}{R^3} \int_m \vec{\rho} \times \vec{R} dm + \frac{\mu}{R^3} \int_m \frac{3\vec{R} \cdot \vec{\rho}}{R^2} \vec{\rho} \times \vec{R} dm$$

$$=\frac{3\mu}{R^5}\int_m(\vec{R}\cdot\vec{\rho})(\vec{\rho}\times\vec{R})dm$$

$$\vec{\rho} = \begin{bmatrix} x \\ y \\ z \end{bmatrix} \qquad \vec{R} = \begin{bmatrix} R_x \\ R_y \\ R_z \end{bmatrix}$$

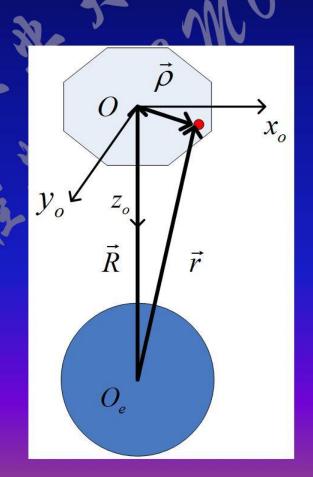


$$\vec{M}_g = \frac{3\mu}{R^5} \int_m (\vec{R} \cdot \vec{\rho}) (\vec{\rho} \times \vec{R}) dm$$

$$\vec{
ho} = \begin{bmatrix} x \\ y \\ z \end{bmatrix}$$
  $\vec{R} = \begin{bmatrix} R_x \\ R_y \\ R_z \end{bmatrix}$ 

$$\vec{R} = A \begin{bmatrix} 0 \\ 0 \\ -R \end{bmatrix}$$

$$= R \begin{bmatrix} \cos \varphi \sin \theta \\ -\sin \varphi \\ -\cos \varphi \cos \theta \end{bmatrix}$$



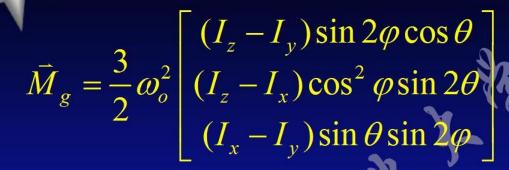
$$\vec{M}_g = \frac{3\mu}{R^5} \int_m (\vec{R} \cdot \vec{\rho}) (\vec{\rho} \times \vec{R}) dm$$

$$= \frac{3\mu}{R^5} \begin{bmatrix} (I_z - I_y)R_yR_z \\ (I_x - I_z)R_xR_z \\ (I_y - I_x)R_xR_y \end{bmatrix} + I_{xy}R_xR_z - I_{xz}R_xR_y + I_{yz}(R_z^2 + R_y^2) \\ - I_{xy}R_yR_z + I_{xz}(R_x^2 - R_z^2) + I_{yz}R_xR_y \\ + I_{xy}(R_y^2 - R_x^2) + I_{xz}R_yR_z - I_{yz}R_xR_z \end{bmatrix}$$

$$I_{xy} = I_{yz} = I_{xz} = 0$$

$$\vec{M}_{g} = \frac{3\mu}{2R^{3}} \begin{bmatrix} (I_{z} - I_{y}) \sin 2\varphi \cos \theta \\ (I_{z} - I_{x}) \cos^{2} \varphi \sin 2\theta \\ (I_{x} - I_{y}) \sin \theta \sin 2\varphi \end{bmatrix}$$

$$\omega_0^2 = \frac{\mu}{R^3}$$



#### 小角度情况下

$$\vec{M}_g = 3\omega_o^2 \begin{bmatrix} (I_z - I_y)\varphi \\ (I_z - I_x)\theta \end{bmatrix}$$

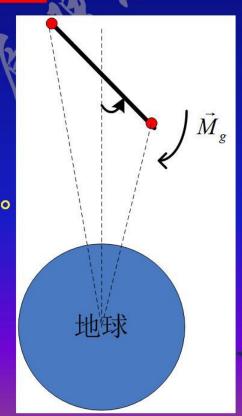


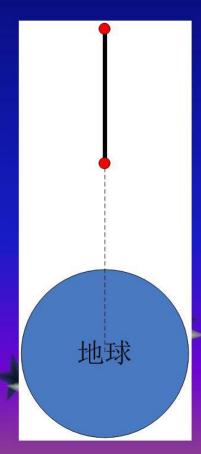


$$\vec{M}_{g} = \frac{3}{2}\omega_{o}^{2} \begin{bmatrix} (I_{z} - I_{y})\sin 2\varphi \cos \theta \\ (I_{z} - I_{x})\cos^{2}\varphi \sin 2\theta \\ (I_{x} - I_{y})\sin \theta \sin 2\varphi \end{bmatrix}$$

# 重力梯度力矩具有如下性质:

- (1) 随高度的增加而减少。
- (2) 与航天器的质量分布有关。
- (3) 与航天器的角位置有关。





# 3、稳定性分析

# 线性化航天器的姿态运动方程:

$$\begin{cases} I_{x}\ddot{\varphi} + \left(I_{y} - I_{z} - I_{x}\right)\omega_{0}\dot{\psi} + \left(I_{y} - I_{z}\right)\omega_{0}^{2}\varphi = M_{x} \\ I_{y}\ddot{\theta} = M_{y} \\ I_{z}\ddot{\psi} - \left(I_{y} - I_{z} - I_{x}\right)\omega_{0}\dot{\varphi} + \left(I_{y} - I_{x}\right)\omega_{0}^{2}\psi = M_{z} \end{cases}$$

# 将重力梯度力矩代入

$$\vec{M}_g = 3\omega_o^2 \begin{bmatrix} (I_z - I_y)\varphi \\ (I_z - I_x)\theta \\ 0 \end{bmatrix}$$

$$\begin{cases} I_{x}\ddot{\varphi} + (I_{y} - I_{z} - I_{x})\omega_{0}\dot{\psi} + 4(I_{y} - I_{z})\omega_{0}^{2}\varphi = 0 \\ I_{y}\ddot{\theta} + 3(I_{x} - I_{z})\omega_{0}^{2}\theta = 0 \\ I_{z}\ddot{\psi} - (I_{y} - I_{z} - I_{x})\omega_{0}\dot{\varphi} + (I_{y} - I_{x})\omega_{0}^{2}\psi = 0 \end{cases}$$

# 忽略偏航和滚动通道间的耦合

$$\begin{cases} I_x \ddot{\varphi} + 4(I_y - I_z) \omega_0^2 \varphi = 0 \\ I_y \ddot{\theta} + 3(I_x - I_z) \omega_0^2 \theta = 0 \\ I_z \ddot{\psi} + (I_y - I_x) \omega_0^2 \psi = 0 \end{cases}$$

$$\ddot{\phi} + \frac{4(I_y - I_z)\omega_0^2}{I_x} \varphi = 0 \qquad \Omega_x^2 \stackrel{\triangle}{=} \frac{4(I_y - I_z)\omega_0^2}{I_x} > 0$$

$$\ddot{\theta} + \frac{3(I_x - I_z)\omega_0^2}{I_y} \theta = 0 \qquad \Omega_z^2 \stackrel{\triangle}{=} \frac{3(I_x - I_z)\omega_0^2}{I_z} > 0$$

$$\ddot{\psi} + \frac{(I_y - I_x)\omega_0^2}{I_z} \psi = 0 \qquad \Omega_z^2 \stackrel{\triangle}{=} \frac{(I_y - I_x)\omega_0^2}{I_z} > 0$$

$$\ddot{\psi} + \frac{(I_y - I_x)\omega_0^2}{I_z} = 0 \qquad \Omega_z^2 \stackrel{\triangle}{=} \frac{(I_y - I_x)\omega_0^2}{I_z} > 0$$

$$\begin{cases} \ddot{\varphi} + \Omega_x^2 \varphi = 0 \\ \ddot{\theta} + \Omega_y^2 \theta = 0 \end{cases}$$

$$\ddot{\psi} + \Omega^2 \psi = 0$$

$$\begin{cases} \varphi = \frac{\dot{\varphi}_0}{\Omega_x} \sin \Omega_x t + \varphi_0 \cos \Omega_x t \\ \theta = \frac{\dot{\theta}_0}{\Omega_y} \sin \Omega_y t + \theta_0 \cos \Omega_y t \end{cases}$$

$$\psi = \frac{\dot{\psi}_0}{\Omega_z} \sin \Omega_z t + \psi_0 \cos \Omega_z t$$

$$\Omega_{x} = 2\omega_{0}\sqrt{\frac{\left(I_{y} - I_{z}\right)}{I_{x}}} \quad \Omega_{y} = \omega_{0}\sqrt{\frac{3\left(I_{x} - I_{z}\right)}{I_{y}}} \quad \Omega_{z} = \omega_{0}\sqrt{\frac{I_{y} - I_{x}}{I_{z}}}$$

姿态运动是在平衡姿态周围无阻尼振荡, 称为天平动。

设计重力梯度稳定航天器应解决三个问题:

- (1)增大起稳定作用的恢复力矩和限制扰动力矩。
  - (2)捕获重力场。
  - (3)天平动阻尼。

