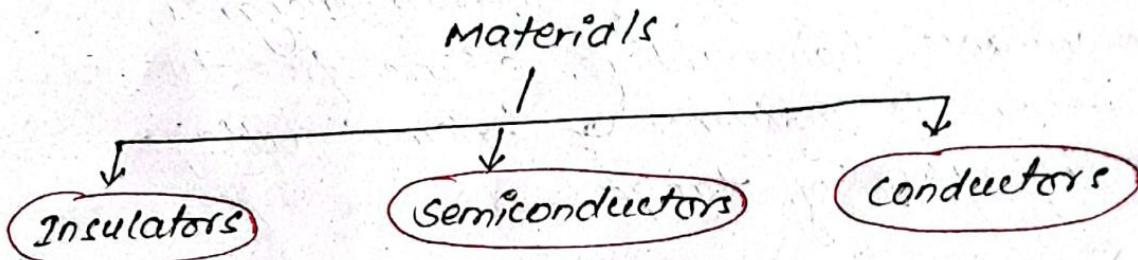


## Semiconductor and semiconductor materials

Based on the electrical conductivity, all the materials in nature are classified as:

- insulator
- semiconductor and
- conductors.



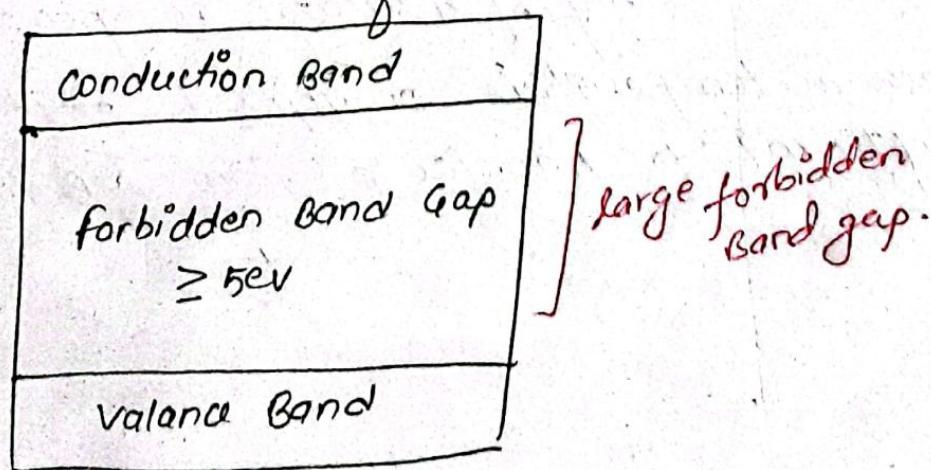
### a) Insulators:

An insulator is a material that are characterized by poor electrical conductivity. for eg: glass, quartz, rubber, bakelite, mica etc.

The resistivity level of an insulator is of the order of  $10^{20}$  to  $10^{12}$   $\Omega \cdot \text{m} \cdot (\text{ohm-meter})$

$$[\because \text{Resistance } (R) = \frac{\rho l}{A} \therefore \rho = \frac{RA}{l}]$$

The energy band structure of an insulator is as shown below:



Band structure of a material defines the band of energy level that an electron can occupy. Valence band is the range of electron energy where the electrons remain bonded to the atom and do not contribute to the electric current.

Conduction band is the range of electron energies higher than valence band where e<sup>-</sup>s are free to accelerate under the influence of external voltage source resulting flow of charge.

The energy band between the valence band and conduction band is called forbidden band gap or forbidden energy gap. It is the energy required by an e<sup>-</sup> to move from valence band to conduction band.

$$1\text{eV} = 1.6 \times 10^{-19} \text{J}$$

There is a large forbidden band gap  $\geq 5\text{eV}$ . Because of this large gap, there are very few e<sup>-</sup>s in the conduction band and hence conductivity of insulator is poor.

Even an increase in temperature or applied electric field is insufficient to transfer e<sup>-</sup>s from VB to CB.

## b. Conductors:

Conductors or conducting materials are good conductors of electricity and characterized by a large conductivity & small resistivity. for eg., Copper, Aluminium, silver etc. The resistivity of conductors is in the range of  $10^{-8} \Omega\text{-m}$ .

In a conductor, there is no forbidden energy gap between valence band and conduction band i.e. they overlap each other. Electrons randomly move through the solid. So electrons in the conductors are called free electrons.

Therefore at a room temperature ( $25^\circ\text{C}$ ) when electric field is applied, an electric current flows through a conductor. The resistance of the conductor increases with the increase in temperature. (Temp ↑, collision ↑, resistance ↑ & flow of current ↓)

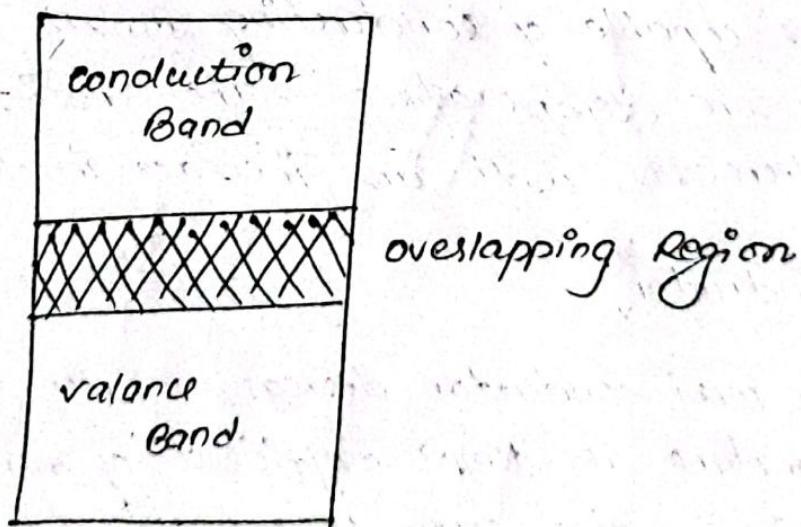


fig: Energy level diagram  
of conductor.

## Semiconductor

A semiconductor is a material that has the conductivity somewhere between the insulator and conductor. The resistivity of semiconductor material lies in the range of  $10^{-5}$  to  $10^5 \Omega\text{m}$ .

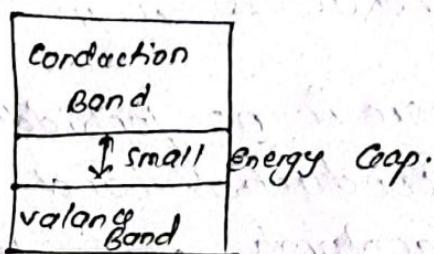


Fig: Semiconductor's energy band diagram.

Thus semiconductor acts as a insulator at absolute zero. However at normal room temperature ( $25^\circ\text{C}$ ) some  $e^-$ s can easily jump to conduction band due to low energy gap between valence band and conduction band. Thus semiconductors are capable of conducting small current even at normal room temperature. The resistance of semiconductor decreases with an increase in temperature.

### Types of semiconductor

The resistance of semiconductor decreases with an increase in temperature. i.e. temp<sup>r</sup> coefficient of resistance of semiconductor is negative. They behave like an insulator at very low temperature but act as conductor at high temperatures.

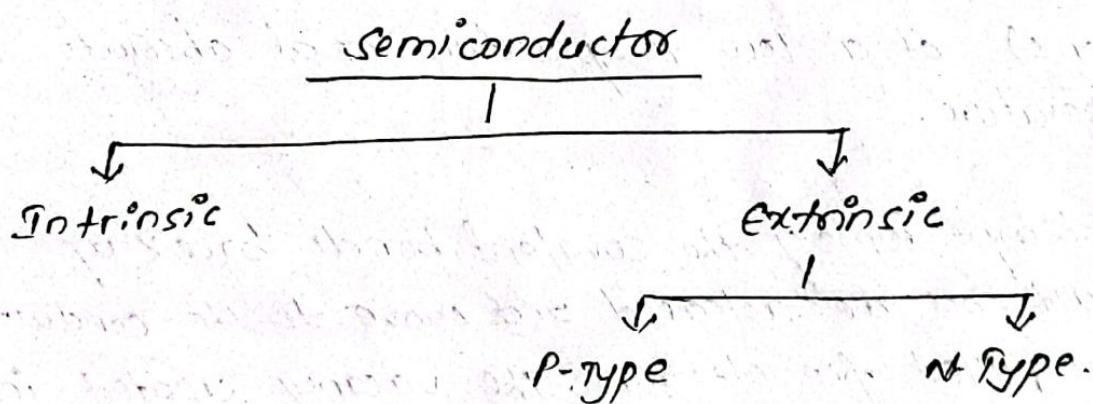
→ The mostly used semiconductors are Germanium (Ge), and silicon (Si).

## Properties of semiconductor (S/C)

1. The resistivity of S/C depends on illumination and decreases in brighter surroundings. (negative temp, light coefficient)
2. The resistivity of S/C depends on the magnitude of electric field.
3. S/C are non-linear elements. [do not follow Ohm's law]
4. The conductivity of S/C changes considerably when small amount of impurities added to it. So that its conductivity can be controlled.

There are 2 types of S/C:

1. Intrinsic (pure) S/C
2. Extrinsic (impure) S/C



### 1. Intrinsic semiconductors

The extremely pure form of semiconductors in which there are almost equal no of holes and electrons. In V.B and C.B respectively are called intrinsic semiconductors.

Pure Germanium and Silicon are widely used intrinsic semiconductors.

## Production of Holes and free electrons

let us consider a structure of silicon atom. silicon atomic no. is 14 and has 4 valence electrons. These 4 electrons are shared by 4 neighbouring atoms in the crystal structure by means of covalent bond.

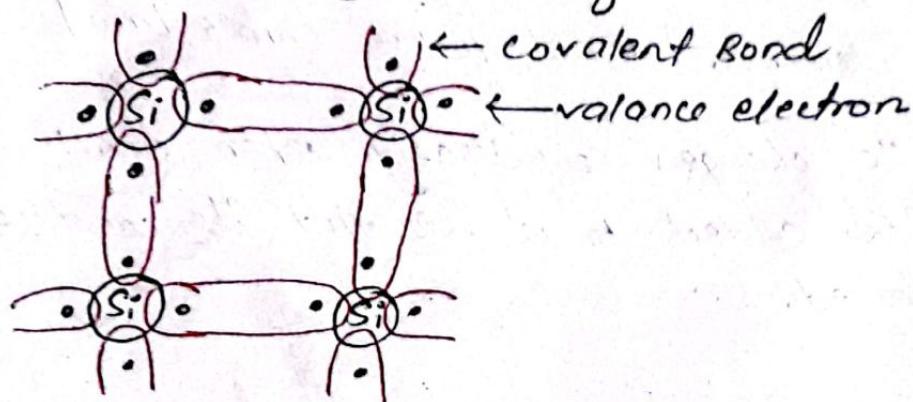


fig: Crystal structure of  $\text{Si}$  at absolute zero  
 $(-273^{\circ}\text{C})$

Thus, pure Si acts as poor conductor (due to lack of free electrons) at a low temperature or at absolute zero temperature.

At room temp<sup>r</sup> some of the covalent bonds break up. As a result, e<sup>-</sup>s are released and move to the conduction band, are called free electrons. The vacancy created in broken bond is called a hole. Since hole is created after a removal of e<sup>-</sup> from the covalent bond, it is considered as positive charge.

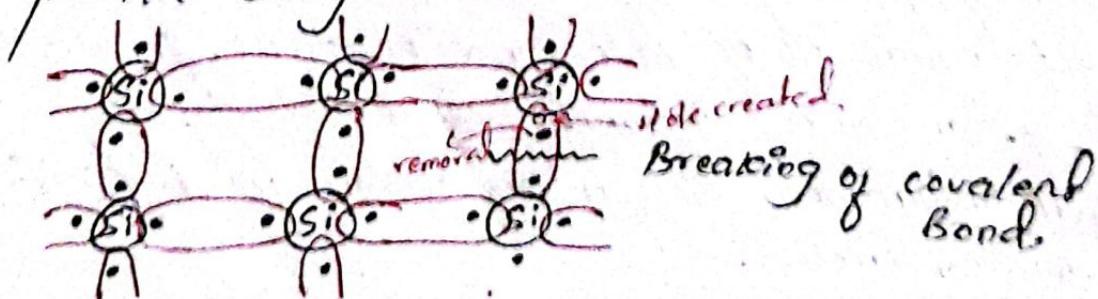


fig: production of hole and free e<sup>-</sup>

electrons and holes are created in pairs. where a free electron approaches the hole, it gets attracted and falls into the hole. This process of merging of free e<sup>-</sup> and a hole is called recombination.

During this process, both the free e<sup>-</sup>s and hole disappear. However, an energy is released and causes another covalent bond to break down and generate a new electron hole pair.

### Conduction in Intrinsic semiconductors

when an e<sup>-</sup>s are released during the breakdown of covalent bonds, they move randomly through a crystal lattice. When an external electric field is applied to the pure intrinsic s/c, the free e<sup>-</sup>s in the conduction band move towards the +ve terminal while holes move towards the -ve terminal of power supply (battery). as a result, an electric current flows. This current is very small.

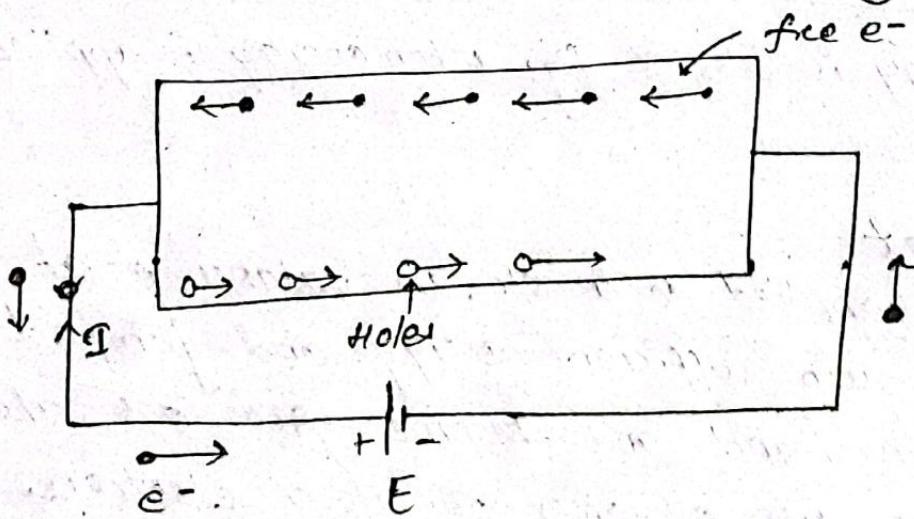


fig: conduction of current in Intrinsic s/c.

Total current in the semiconductor is the sum of electron current and hole current.

i.e.  $I = I_e + I_h$

## II. conduction in semiconductor

SIC consists of 2 types of charge carriers: positive charge carriers called holes and negative charge carriers called electrons.

The movement of these charge carriers give rise to the flow of current in SIC. Thus we can say that SIC possess two types of current:

i) Electron current

ii) Hole current

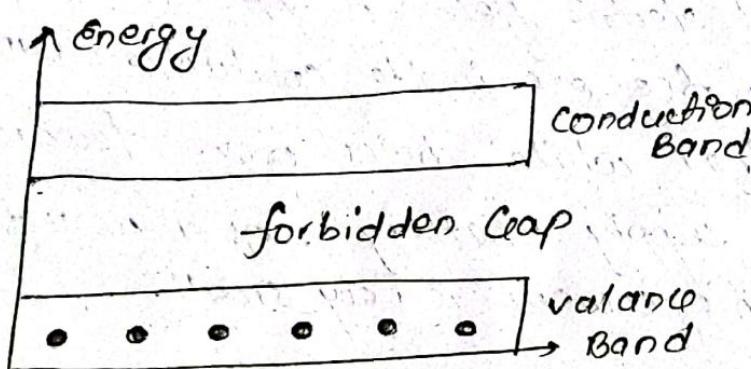


fig: when no energy is applied

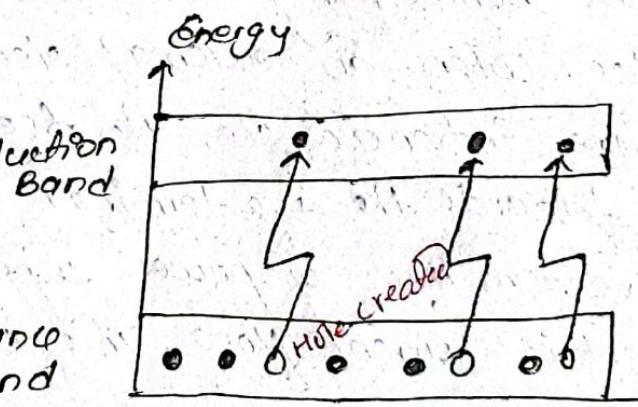


fig: when energy is applied

i) electron current

When an energy is applied to a SIC, the valence e- at valence band can gain sufficient energy and jumps to the conduction band and becomes free e-s. The movement of these free e-s gives rise to a electron current ( $I_e$ ).

### (iii) Hole current

When a valence e<sup>-</sup> gain sufficient energy and jumped to conduction band, they leave a hole at the valence band. Further valence electrons can move through this hole. Thus relative motion of valence e<sup>-</sup>s at valence band through holes give rise to hole current ( $I_h$ ).

Thus, total current in a s/c is the sum of e<sup>-</sup> current and hole current.

$$\text{i.e. } I = I_e + I_h$$

## 2. Extrinsic Semiconductor

An intrinsic s/c has very limited applications/significance as it conduct very small amount of current at room temperature. However, the electrical conductivity of intrinsic s/c can be increased significantly by adding small amount of impurities to it during the crystallization process. (process of separating solid compounds from the solution in the form of crystals.)

This process of adding an impurity to a pure s/c is called doping and the resulted s/c formed is called extrinsic s/c.

There are 2 types of s/c on the basis of type of impurities added.

- ① N-type semiconductors
- ② P-type semiconductors.

is N-type semiconductor

when a small amount of pentavalent impurity is added, such as Arsenic (As), Antimony (Sb), Bismuth (Bi), phosphorous (P) to a pure s/c during crystallization process, the resulting crystal is called N-type s/c.

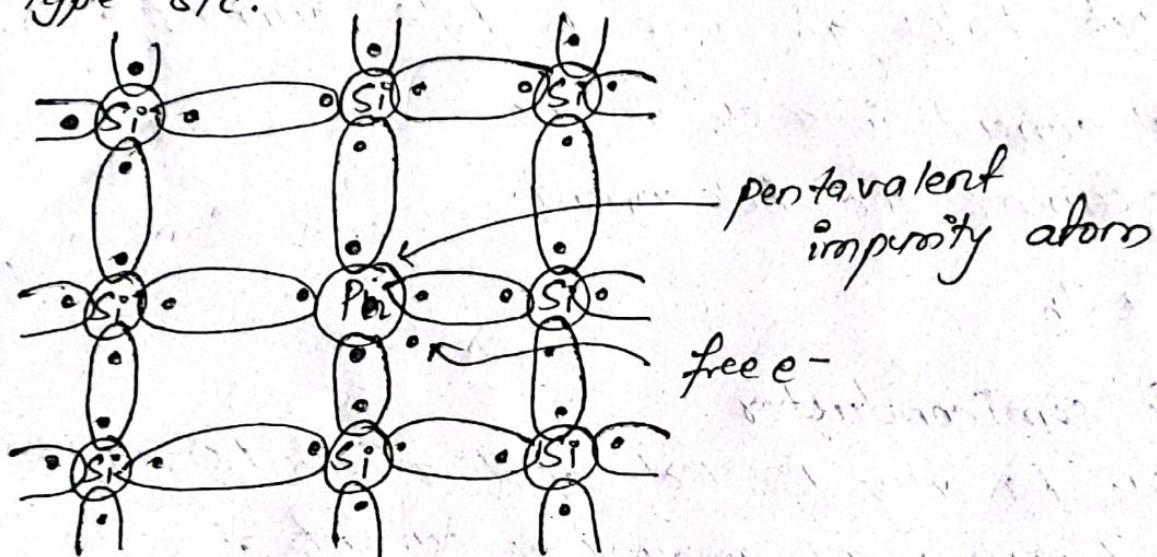
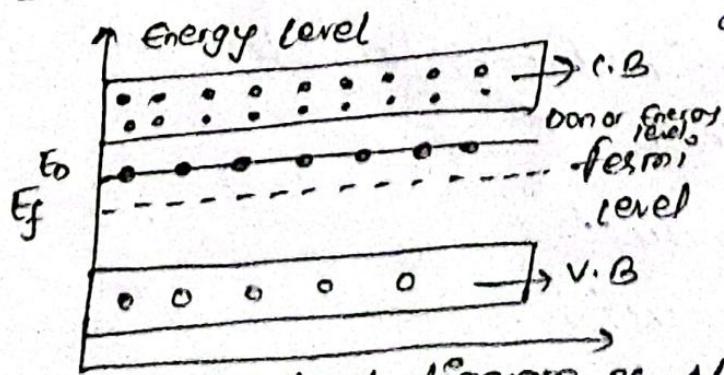


fig: crystal structure of N-type s/c.

for each impurity added, one free  $e^-$  is generated, which then moves to conduction band. As the pentavalent impurity donates electron to crystal lattice, it is also called donor impurity or donor agent.

In N-type semiconductor,  $e^-$ s are majority charge carriers.



\* Fermi level: the highest energy level that an electron can occupy at the absolute zero temperature.

Fermi level lies between valence band and conduction band because at absolute zero temp the electrons are all in the lowest energy state.

fig: Energy level diagram of N-type semiconductor.

## (ii) P-type semiconductor

When a small amount of trivalent impurity such as aluminium, Gallium, Indium, Boron is added to a pure SiC, then P-type SiC is formed.

The crystal structure of P-type SiC is as shown below:

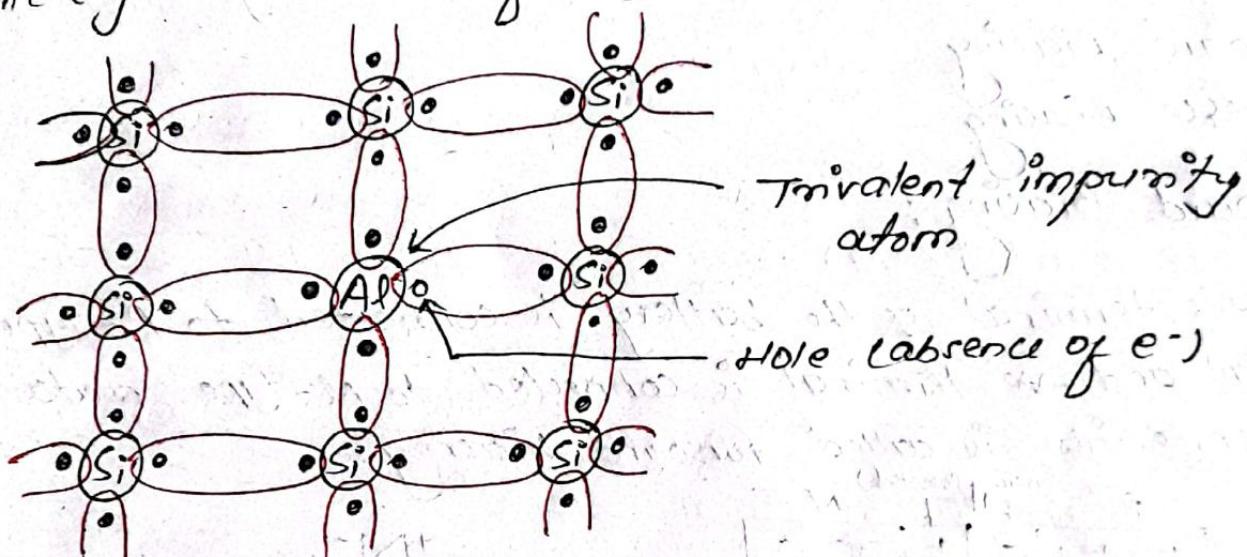
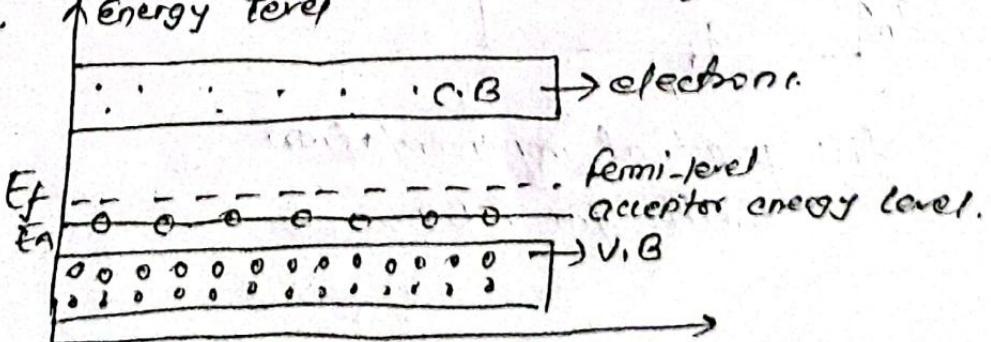


fig: crystal structure of P-type SiC.

The 3 valence e<sup>-</sup>s of the trivalent impurity forms 3 covalent bonds with the neighbouring atoms and a vacancy exists in the fourth bond giving rise to the holes, which can accept an electron. So, trivalent impurities are also called acceptor impurities or acceptor agents.

In P-type SiC, holes are majority carriers of e<sup>-</sup>s are minority carriers. ↑ Energy level



\* P-type semiconductor  
In Fermi-level shift  
from V.B to E.F. (eV)

fig: Energy band diagram of P-type SiC.

## #. Biasing of PN Junction (operation of PN junction Diode)

The process of connecting the diode terminals (i.e. P and N) with the source terminal (voltage source) is known as biasing of diode.

A PN junction diode can be biased in two ways:

i) Forward Biasing

ii) Reverse Biasing

is forward Biasing:

If the +ve terminal of the battery is connected to P-type material and -ve terminal is connected to N-type material, the connection is called forward biasing;

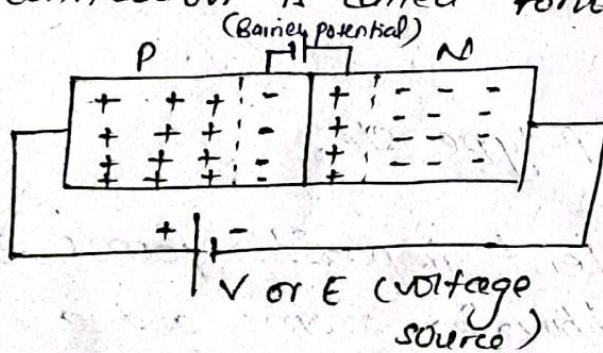


fig: forward Biasing of diodo.

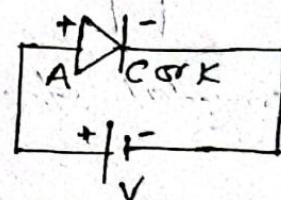


fig: symbolic circuit for forward Biasing.

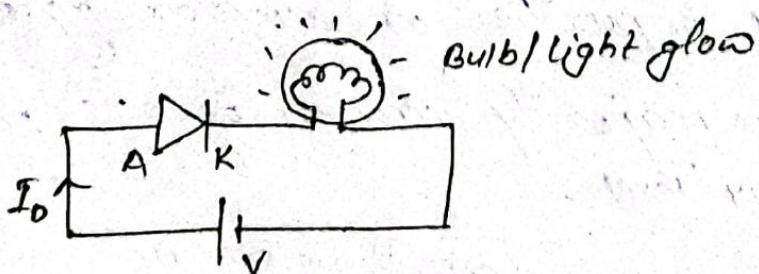


fig: practical implementation circuit for F.B.

The -ve terminal of battery flows electrons on N-region, these electrons repels the electrons on N-region towards depletion region. If the electrons have sufficient energy to cross the barrier potential they will transfer to P-region for this the battery should have potential difference more than barrier potential. In P-region these electrons recombine with holes but due to attraction of positive terminal of battery these electrons move towards the terminal through holes finally electrons reached to the cell. The cell again pumps electrons to N-region and the process continues. So we can conclude that current flows through diode during forward biased condition.

### (ii) Reverse Biasing

When a +ve terminal of a source is connected to -ve terminal of a diode (N-type SiC) and -ve terminal of a source is connected to the terminal of a diode (P-type SiC), then the diode is said to be Reverse Biased.

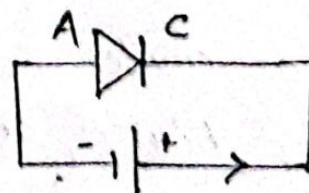
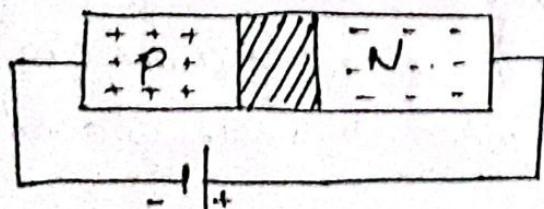


fig: Reverse biasing of PN junction diode.

In reverse biasing, the +ve terminal of a source attracts the e-s from N-type SiC whereas the -ve terminal of a source attracts the holes from P-type SiC, away from the junction. Due to the movement of e-s and holes the depletion

region widens and diode doesn't conduct current.  
When a diode is reverse biased, the majority charge carriers gives rise to small current, which is negligible.

When reverse bias voltage is greater than a breakdown voltage, the diode breakdown and acts as a short circuit, so it conducts high current.

## # Voltage - Current (V-I) characteristic of PN junction Diode:

### i. Ideal Diode :

- The diode that acts like perfect conductor when forward biased and perfect insulator when reverse biased is called an ideal diode.
- It produces zero current when reverse biased.
- It produces zero voltage when forward biased.
- It has zero resistance when forward biased.
- It has infinite resistance when reverse biased.

So, ideal acts as switch - The switch is closed (short circuited) when forward biased and open when reverse biased.

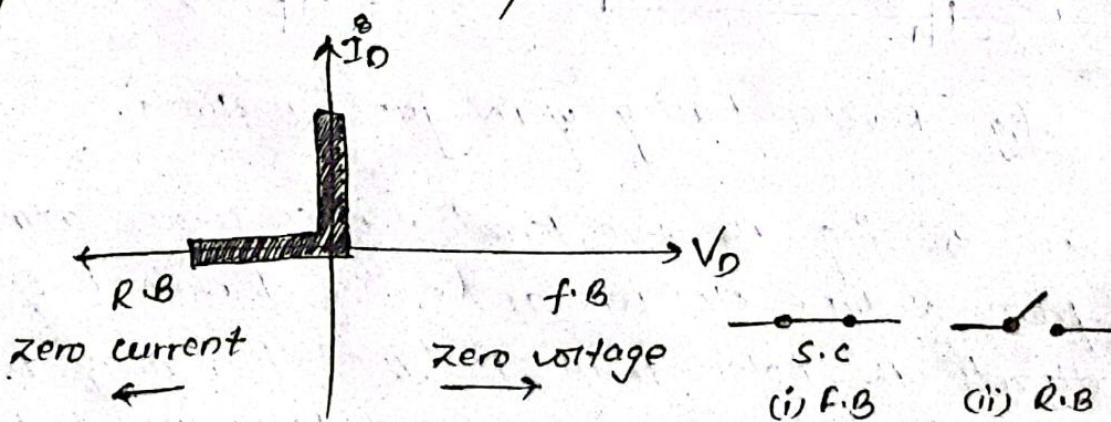


fig: V-I characteristic curve of Ideal diode.

### (iii) Real / practical diode V-I characteristics.

If ' $V_D$ ' is the voltage (applied) across a diode and ' $I_D$ ' be the current flowing through it, then the relationship between  $V_D$  and  $I_D$  is given by,

$$I_D = I_s \left( e^{\frac{V_D}{\eta V_T}} - 1 \right) \quad \textcircled{1}$$

② Reverse saturation current is the part of the reverse current in a Si diode caused by diffusion of minority carriers from the neutral region to the depletion region.

Reverse saturation current is the term for negative current produced by a reverse bias.

where,  $I_s$  = reverse saturation current

$V_T$  = Thermal voltage = 0.026 V at room temp

$\eta$  = Emission coefficient ( $1 \leq \eta \leq 2$ )  
(value 1 or 2 ~~total~~, numerical ~~value~~)

$V_D$  = voltage drop across diode.

When eqn ① is plotted in a graph, then V-I characteristics of diode is obtained as shown below:

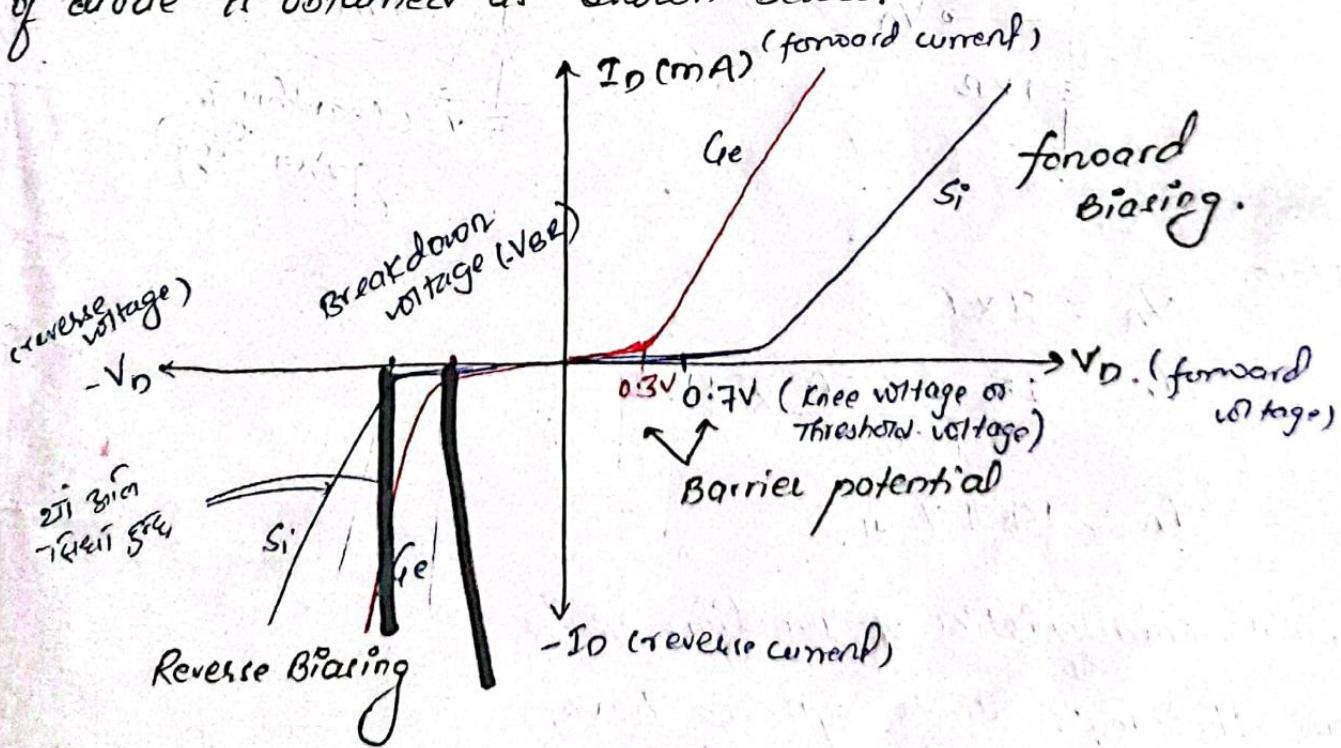
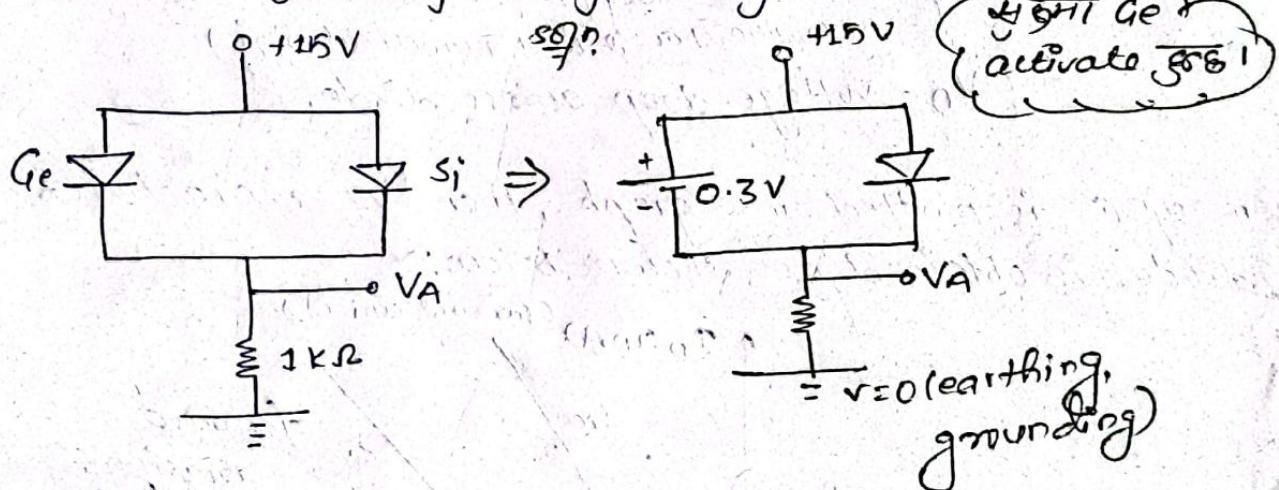


fig: V-I characteristics of a diode.

**operation:** When a diode is forward biased small amount of current flows through it until the supply voltage is greater than barrier potential.

When the supply voltage exceeds the barrier potential, then the current rises sharply as shown in above figure. Also when the diode is reverse biased, negligible amount of current flows through it, but if the supply voltage exceeds the breakdown voltage ( $V_{BR}$ ), the diode is broken down (destroyed) and it acts as short circuit due to which the current increases sharply as shown in above figure.

Q. Determine voltage  $V_A$  for the following.



Here,

$$V_A = I \times R$$

$$V_A = \frac{15 - 0.3 - 0}{1k\Omega} \times 1k\Omega$$

$$V_A = 14.7 V$$

## # Terminal characteristics of Junction Diode.

From Shockley's diode eqn we have,

$$I_D = I_s (e^{\frac{V_D}{mV_T}} - 1) \quad \text{--- (1)}$$

Where,

$I_D$  = diode current

$I_s$  = leakage saturation current

$V_D$ : voltage drop across diode

$V_T$ : Thermal voltage

where,

$V_T$  is given by.

$$V_T = \frac{K T}{q}$$

$K$  = Boltzmann's constant

( $K = 1.38 \times 10^{-23}$  Joule/Kelvin)

$T$  = absolute Room Temp

$q$  = electronic charge

( $q = e = 1.67 \times 10^{-19} C$ )

## # Diode Resistance

Diode shows two types of resistive effects:

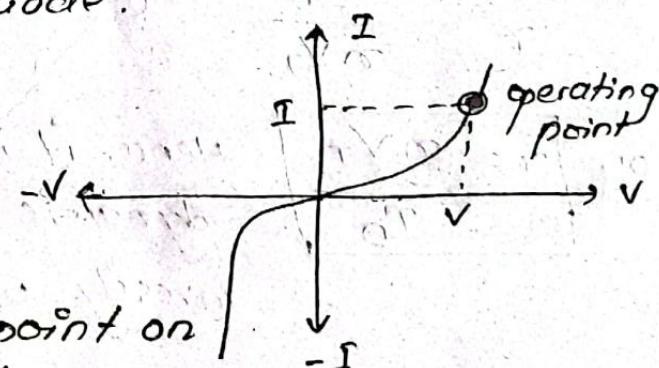
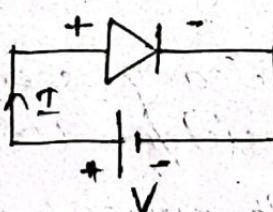
i) static resistance (DC resistance)

ii) dynamic resistance (AC resistance)

i) static Resistance or DC Resistance

If 'V' be the dc voltage applied to a diode and 'I' be the current flowing through it, then the ratio of V and I is called static resistance of a diode.

$$\text{i.e. } R_{DC} = \frac{V}{I}$$



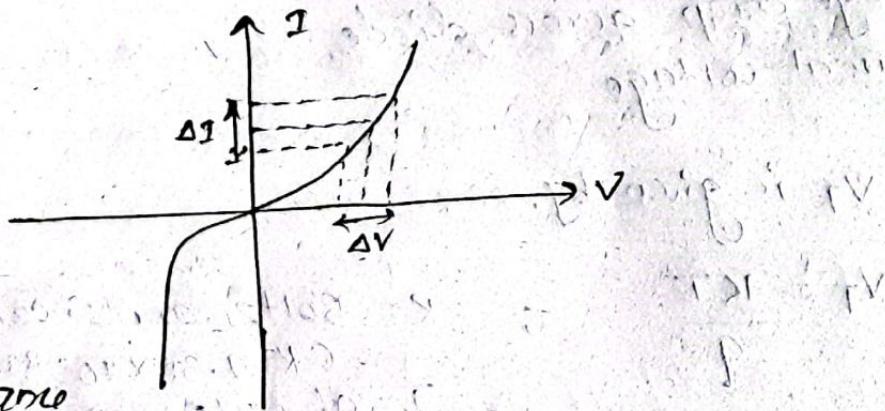
→ Its value depends on operating point on VI characteristic curve of diode.

fig: I vs V

ii) Dynamic Resistance or AC Resistance

When the voltage applied across a diode is changed by  $\Delta V$ , then the current flowing through it will also change by  $\Delta I$ . The ratio of change in voltage to change in current is called dynamic or AC resistance of a diode.

Here,



dynamic resistance

$$r = \frac{\Delta V}{\Delta I} = \frac{dV}{dI_D} \quad \textcircled{1}$$

We know that,

$$I_D = I_s (e^{\frac{V}{nV_T}} - 1) \approx I_s (e^{\frac{V}{nV_T}}) \quad \textcircled{11}$$

Now,

$$\frac{dI_D}{dV} = \frac{d}{dV} \left[ I_s e^{\frac{V}{nV_T}} \right]$$

$$\text{or, } \frac{1}{r} = \frac{I_s}{nV_T} e^{\frac{V}{nV_T}} \quad \left[ \because r = \frac{dV}{dI_D} \right]$$

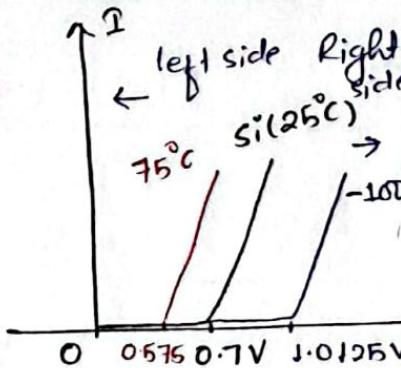
$$\text{or, } \frac{1}{r} = \frac{I_D}{nV_T} \quad (\because \text{from eqn } \textcircled{11})$$

$$\boxed{\text{or, } r = \frac{nV_T}{I_D}}$$

Hence, it is clearly seen that the dynamic resistance ( $r$ ) varies inversely with current across diode.

#. Temperature Dependence of V-I characteristics

forward bias for Si diode, characteristic in forward biased shifted towards left side by increasing temp at the rate of  $2.5 \text{ mV}/\text{C}$ .



e.g.: find threshold voltage at  $75^\circ\text{C}$  and at  $-100^\circ\text{C}$  for Si PN junction diode.

soln. ① for  $75^\circ\text{C}$

$$\text{New threshold voltage } (V_{Th}) = V_{Th0} - 2.5 \times 10^{-3} \times 50^\circ\text{C}$$

[→ यदि temp increase हो तो left side दर्शाएँ, यहाँ Si को  $25^\circ\text{C}$  already है, तो  $75^\circ\text{C}$  पुणे  $50^\circ\text{C}$  से पुछ, तो temp  $2.5 \text{ mV}$  की rate के change होते हैं।]

$$\begin{aligned} \therefore V_{Th} &= 0.7 - 2.5 \times 10^{-3} \times 50 \\ &= 0.7 - 0.125 \\ &= 0.575 \text{ V} \end{aligned}$$

[increase  $\rightarrow$  ग्रन्हि -ve  
decrease  $\rightarrow$  ग्रन्हि +ve  
reference to  $Si(25^\circ\text{C})$  लिये]

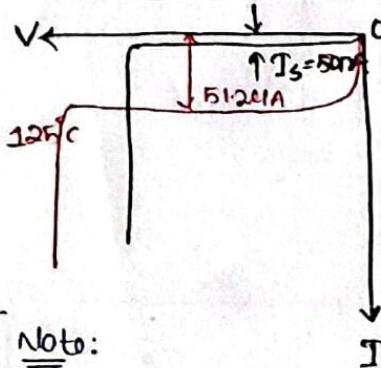
② for  $-100^\circ\text{C}$

$-100^\circ\text{C}$  पुणे की लाई  $25^\circ\text{C}$  to  $0^\circ\text{C}$  and  $0^\circ\text{C}$  to  $-100^\circ\text{C}$

∴ Total temperature  $125^\circ\text{C}$ .

$$\begin{aligned} \text{Now, } V_{Th} &= V_{Th0} + 2.5 \times 10^{-3} \times 125 \\ &= 0.7 + 2.5 \times 10^{-3} \times 125 \\ &= 0.7 + 0.3125 \\ &= 1.0125 \text{ V} \end{aligned}$$

### Reverse Bias



while we increase temp in reverse bias, the reverse saturation current also increases. The reverse saturation current will double in every  $10^\circ$  rise in temperature.

It is given by,

$$I_{(new)} = I_{(old)} 2^{\left(\frac{\Delta T}{10}\right)} \quad \text{where, } \Delta T = \text{change in Temp}$$

e.g.: find the reverse current at  $125^\circ\text{C}$  temp where room temp is  $25^\circ\text{C}$ . The reverse saturation current is  $50 \text{ nA}$  at room temp.

soln. we know,

$$\begin{aligned} I_{(new)} &= I_{(old)} \times 2^{\frac{\Delta T}{10}} \left( \frac{125 - 25}{10} \right) \\ &= 50 \text{ nA} \times 2 \\ &= 50 \text{ nA} \times 2^{10} \\ &= 50 \times 10^{-9} \times 1024 = 51.2 \text{ mA} \quad (\text{micro ampere}) \end{aligned}$$

depletion capacitance = transition capacitance

## Junction capacitance.

The depletion layer across the junction diode behaves as an insulating material or dielectric constant of the capacitor, similarly the P and N side acts as parallel plate of the capacitor. So junction exhibits the properties of capacitor which is called junction capacitance.

Types.

1. Diffusion capacitance ( $C_D$ )
2. Transition capacitance ( $C_T$ )

-  $C_D$   
Diffusion capacitance

$C_T$   
Transition capacitance.

✓ 1. It occurs when diode is forward biased.

✓ 2. With forward biasing the depletion width decreases so  $C_D$  increases with increasing forward biasing.

✓ 3.  $C_D$  is directly proportional to forward diode current  $I_D$  i.e.

$$C_D \propto I_D$$

✓ 1. It occurs when diode is reversed biased.

✓ 2. With reverse biasing the depletion width increases so,  $C_T$  decreases with increasing reverse biasing.

✓ 3.  $C_T$  is inversely proportional to ~~square root of~~ square root of reverse voltage.  
i.e.

$$C_T \propto \frac{1}{\sqrt{V_B}}$$

4.  $C_D$  v/s forward voltage ( $V$ ) & ( $C_T$  v/s) reverse voltage curve is  
curve. i.e.

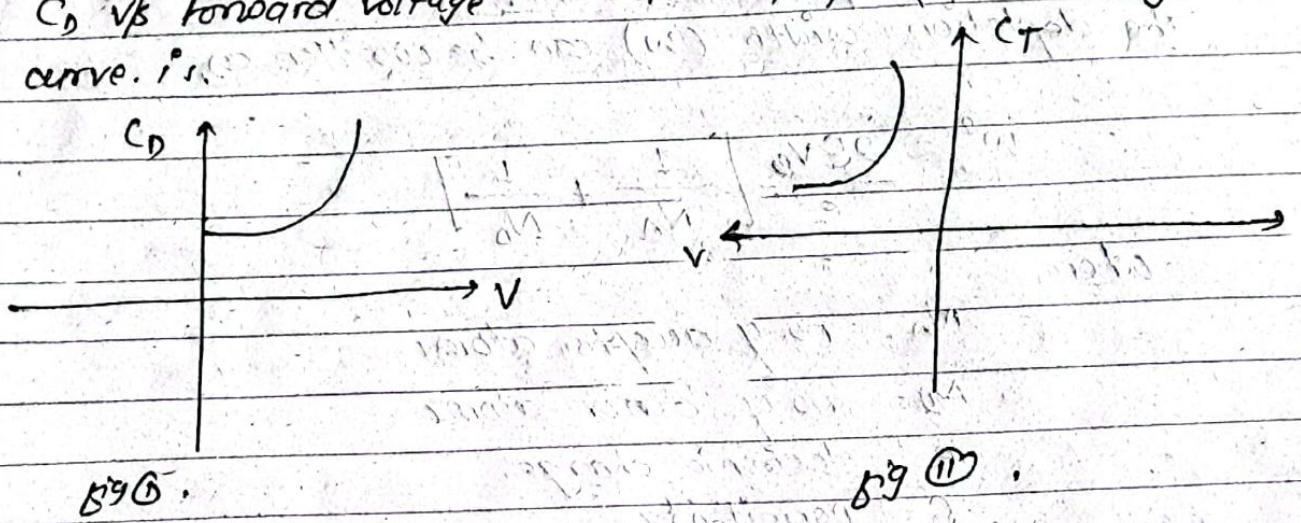


Fig 6.

Fig 11.

short note

i. Diffusion capacitance ( $C_D$ ):

We have,

$$\text{Capacitance } (C_D) = \frac{dQ}{dV}$$

$$\text{or, } C_D = \frac{d}{dV} (ixt) \quad [ \because Q = ixt ]$$

$$\text{or, } C_D = \frac{T dI_D}{dV_D} \quad \text{where, } T \text{ is mean life time of charge carriers.}$$

$$\text{or, } C_D = T \frac{\partial}{\partial V_D} I_S e^{\frac{V_D}{nV_T}}$$

$$\text{or, } C_D = \frac{T}{nV_T} I_S e^{\frac{V_D}{nV_T}}$$

$$\text{or, } C_D = \frac{T}{nV_T} I_D$$

$\therefore C_D \propto I_D$

proved.

2018  
2.

## Transition capacitance ( $C_T$ ):

The depletion width ( $w$ ) can be written as,

$$w^2 = \frac{2EV_B}{e} \left[ \frac{1}{N_A} + \frac{1}{N_D} \right]$$

where,

$N_A$  = no. of acceptor atoms

$N_D$  = no. of donor atoms

$e$  = electronic charge.

$\epsilon$  = permittivity.

We ~~also~~, know,

$$C_T = \frac{EA}{w} \quad \text{where } A = \text{area of plates}$$

$$\begin{aligned} \therefore C_T &= \frac{EA}{\sqrt{\frac{2EV_B}{e} \left( \frac{1}{N_A} + \frac{1}{N_D} \right)}} \\ &= \frac{EA}{\sqrt{\frac{2EV_B(N_A+N_D)}{e N_A N_D}}} \end{aligned}$$

$$= EA \times \frac{e N_A}{\sqrt{2EV_B(N_A+N_D)}}$$

$$\therefore C_T \propto \frac{1}{\sqrt{V_B}}$$

8 Transition capacitance is inversely proportional to the sq. root of the applied voltage.

2018: what do you mean by junction breakdown of a diode? Distinguish b/w a zener ~~diode~~ breakdown and avalanche breakdown.

## #. Junction Breakdown

In reverse biasing a very small current flows due to minority charge carriers. This current is called leakage saturation current ( $I_s$ ). If reverse voltage is further increased a large current flows suddenly at a certain reverse bias voltage. This mechanism of producing large reverse current is called junction breakdown.

Types:

- i) Zener Breakdown
- ii) Avalanche Breakdown.

### 1. Zener Breakdown

✓ 1. It occurs due to high electric field intensity across the junction.

✓ 2. It occurs normally at low reverse voltage. ( $< 4V$ )

✓ 3. It occurs in heavily doped diode.

✓ 4. Zener Breakdown voltage decreases with rise of temperature.  
(negative temp coeff)

✓ 5. The width of depletion layer is thin.

### Avalanche Breakdown

✓ 1. It occurs due to collision of charge carriers with other atoms.

✓ 2. It occurs normally at high reverse voltage. ( $> 6V$ )

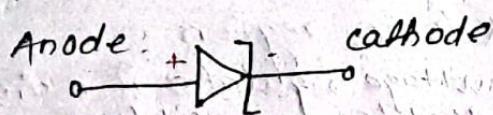
✓ 3. It occurs in lightly doped diode.

✓ 4. Avalanche Breakdown voltage increases with rise of temperature.  
(positive temp coeff)

✓ 6. The width of depletion layer is large in order.

## #.2. Zener Diode

Zener diode is a special type of diode which works in breakdown region. It acts as simple diode when forward biased current flows from anode to cathode. But when operated in reverse breakdown they have extremely stable breakdown voltage over wide range of current levels so they are considered as the backbone of voltage regulators.



- doping level high  
PN junction diode ~~series~~

fig: circuit symbol of zener diode.

The VI characteristics of zener diode is;

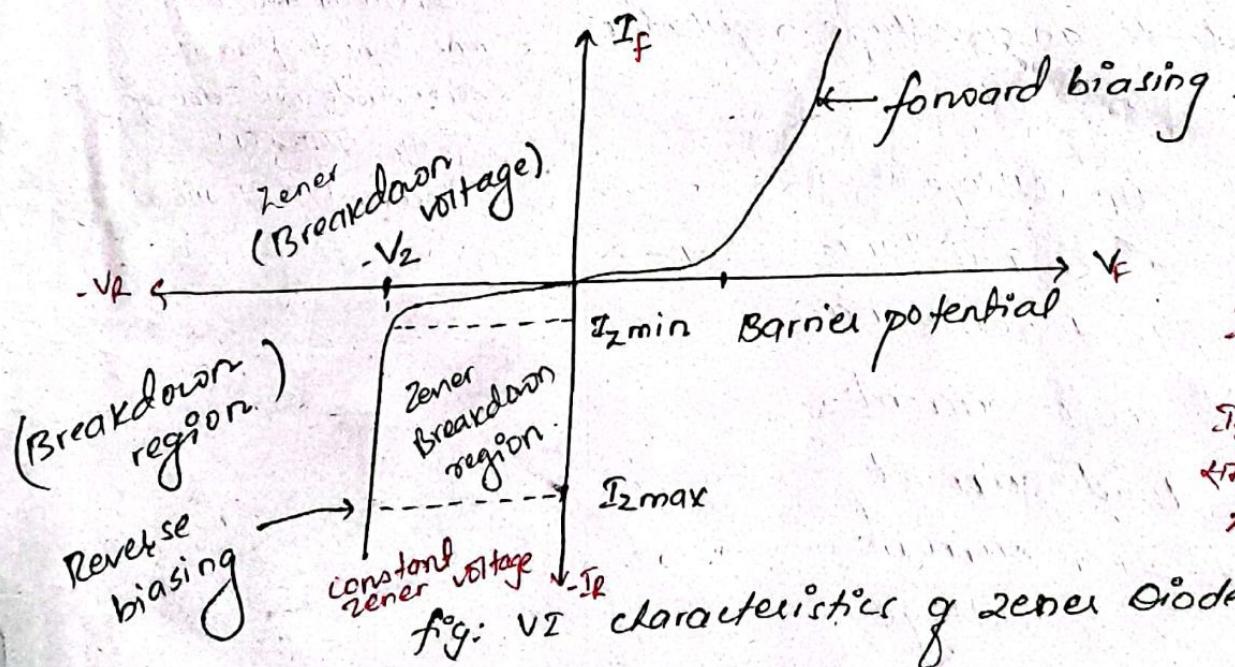


fig: VI characteristics of zener diode.

Applications of zener diode:

1. As a voltage regulator (stabilizer).
2. A clipper in wave shaping circuit
3. (Voltage regulation, input AC voltage vary ~~IR~~ load AC constant voltage provide  $\frac{V_o}{V_i}$ )

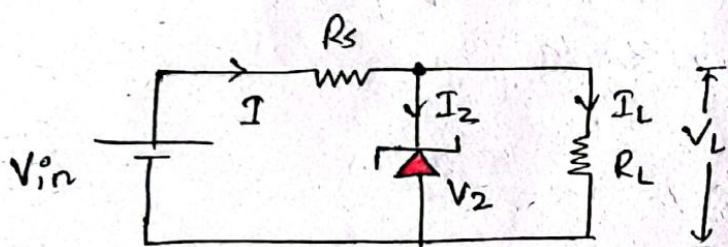
[eg: shunt regulator  
stabilize #]

## Zener Diode as a voltage Regulator

To use zener diode as a voltage regulator, following condition must be satisfied,

- 1) Zener diode must be operated in reverse bias and connected in parallel with load.
- 2) Input voltage must be greater than zener voltage ( $V_{in} > V_z$ )

i.e. it must be operated in a breakdown region



Defn: voltage regulator is a circuit that has an ability to maintain constant output voltage either input voltage is varying or load current is varying.

$R_s$  = series resistance  
~~to, control with zener~~  
max current flow ~~so~~ S.P.R.  
Zener diode ~~over~~ damage  
~~over~~ overvoltage  
current limit ~~over~~ &

fig: zener diode as a voltage regulator.

Here,

$V_{in}$  = input voltage

$R_s$  = source resistance

$R_L$  = load resistance

$I$  = source current

$I_L$  = load current

$I_z$  = zener current

$V_z$  = zener voltage

$V_L$  = load voltage

When zener diode regulate voltage across load, the load voltage will be equal to zener voltage.

$$\text{i.e. } V_L = V_z$$

from above figure,

$$I = I_2 + I_L$$

$$\text{and } V_L = I_L \cdot R_L$$

### case 1: when $V_{in}$ changes

let  $V_{in}$  is increased. As  $V_{in}$  increased, the current  $I$  also increases. If  $I$  increased, both  $I_L$  and  $I_Z$  must be increased, but the zener diode conducts the increased current (ie. only  $I_Z$  increases) and maintain  $I_L$  constant.

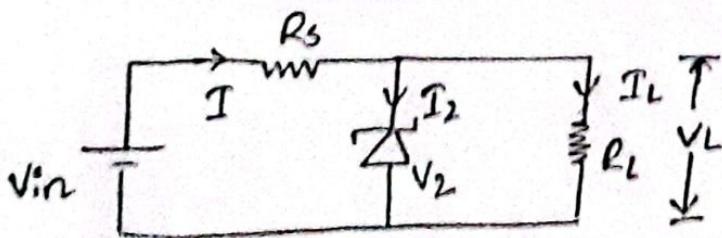
Thus,  $V_L = I_L R_L$  becomes constant even if  $V_{in}$  increases.

### case 2: when $R_L$ changes

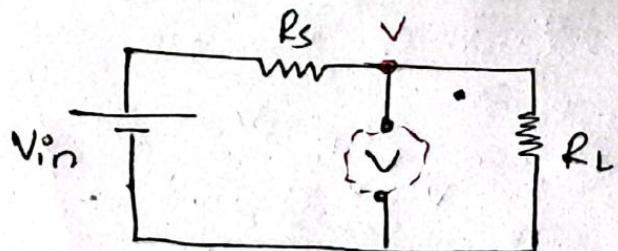
Suppose  $R_L$  increases. When  $R_L$  increases, the zener diode conducts more (ie.  $I_Z$  increases) and minimizes the value of  $I_L$ . So that even increase of  $R_L$ , as  $I_L$  decreases,  $V_L = R_L I_L$  remains constant.

## H. Zener Diode Numerical : Different cases

case I:  $V_{in} = \text{constant}$  and  $R_L = \text{constant}$



Here we have to find whether the zener diode is 'ON' or 'OFF'. For that, remove zener diode from circuit and find open circuit voltage 'V'.



Here,

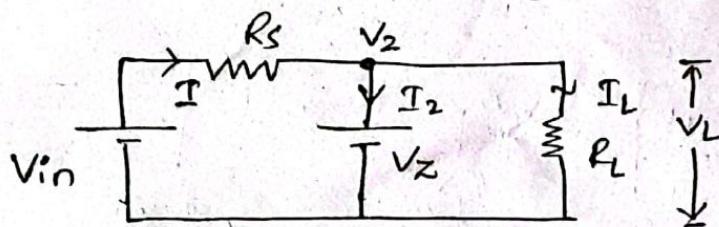
$$V = \frac{R_L}{R_L + R_S} * V_{in}$$

a) If  $V < V_Z$ , zener diode is off

b) If  $V > V_Z$ , zener diode is on.

c) If zener diode is on:

Replace zener diode by voltage source with value  $V_Z$ .



$$\text{Here, } V_L = V_Z$$

$$I = \frac{V_{in} - V_Z}{R_S}$$

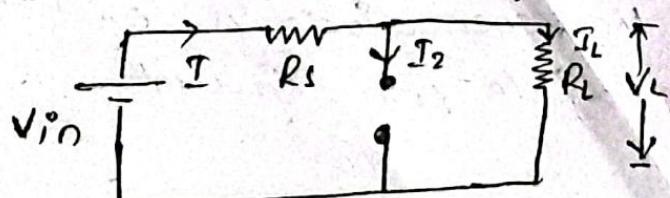
$$I_L = \frac{V_L}{R_L} \text{ and, } V_R = I \cdot R_S \text{ (i.e. voltage across series resistance)}$$

$$I_Z = I - I_L$$

$$\text{power across zener diode } (P_Z) = V_Z I_Z$$

b) If zener diode is off:

Replace zener diode by open circuit.



Here,  $I_2 = 0$

$$V_L = \frac{R_L}{R_L + R_S} \times V_{in}$$

$$I = I_L = \frac{V_{in}}{R_L + R_S} \quad \text{or,} \quad I_L = \frac{V_L}{R_L}$$

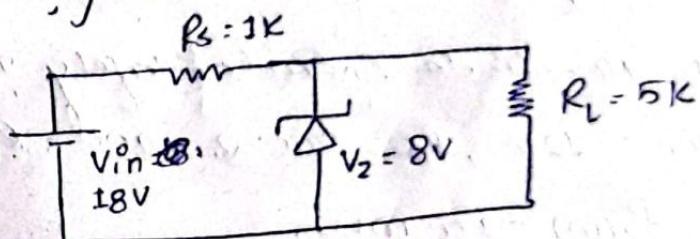
$$\boxed{P_2 = V_2 \cdot I_2 = 0} \quad \text{and, voltage across } (V_2) = I \cdot R_S$$

Q.N.1. for the circuit shown below; find

i) load voltage ( $V_L$ )

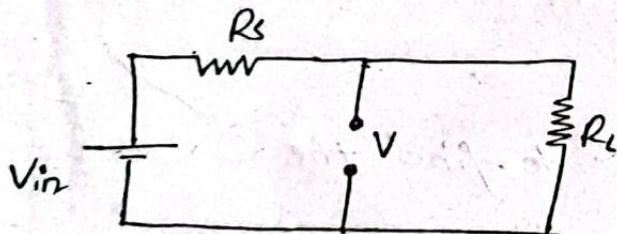
ii) zener current ( $I_2$ )

iii) power across zener diode



soln Here,

removing zener diode and have to find open ckt voltage  $V$ .



Here,

$$V = \frac{R_L}{R_S + R_L} \times V_{in}$$

$$V = \frac{5}{5+1} \times 18$$

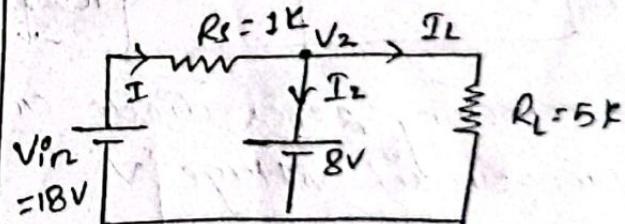
$$V = 15 \text{ V}$$

Here, it is clearly seen that

$$\boxed{18V} > V_2$$

$(15V > 8V)$ . So zener diode is on.  $\therefore I_2 = 10mA - 1.6mA$

now replace zener diode by its (breakdown) voltage source with value  $V_2$ .



Now,

i) load voltage ( $V_L$ ) =  $V_2 = 8V$

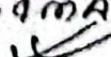
ii) current flowing through zener diode ( $I_2$ ) = ?

We know,  $I_2 = I - I_L$

$$\text{where, } I = \frac{V_{in} - V_2}{R_S} = \frac{18 - 8}{1} = 10mA$$

$$I_L = \frac{V_L}{R_L} = \frac{8}{5} = 1.6mA$$

$$\therefore I_2 = 10mA - 1.6mA$$



(iii) Power across zener diode,

$$\begin{aligned}P_2 &= I_2 \cdot V_2 \\&= 8.4 \text{ mA} * 8 \text{ V} \\&= 67.2 \text{ mW}\end{aligned}$$

Q.2. for the circuit shown below find,

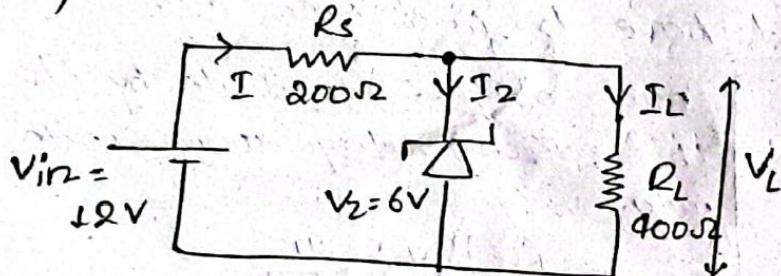
- (i) Load voltage ( $V_L$ )
- (ii) Zener diode current ( $I_2$ )
- (iii)  $P_2$

Is the diode operate safely? Assume

$$V_{in} = 12 \text{ V}, R_s = 200 \Omega, \text{ and } R_L = 400 \Omega, V_z = 6 \text{ V}$$

$$P_2(\text{max}) = 100 \text{ mW.}$$

equation, Here,



Step 1: removing zener diode and have to find the open circuit voltage 'V'

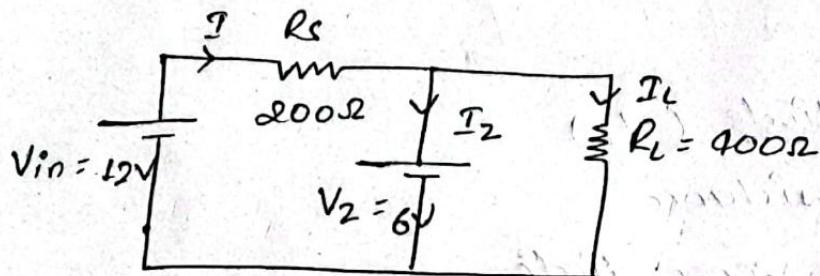
calculation,

$$\begin{aligned}V &= V_{in} * \frac{R_L}{R_L + R_s} \\&= 12 * \frac{400}{400 + 200} = 8 \text{ V}\end{aligned}$$

Here, we get,

$V > V_z$ , so zener diode operates  
(ie. ON state).

Now replace zener diode with voltage source



i) we know,  $V_L = V_z$  (when zener diode operates)

$$\therefore \text{load voltage } (V_L) = V_z = 6V$$

ii) we know,

$$I = I_z + I_L \quad \text{--- (1)}$$

therefore,

$$I_z = I - I_L$$

$$I_z = \frac{V_{in} - V_z}{R_s} - \frac{V_L}{R_L}$$

$$I_z = \frac{12 - 6}{200} - \frac{6}{400} = 0.015 A$$

iii)  $P_z = V_z I_z$

$$= 6 \times 0.015$$

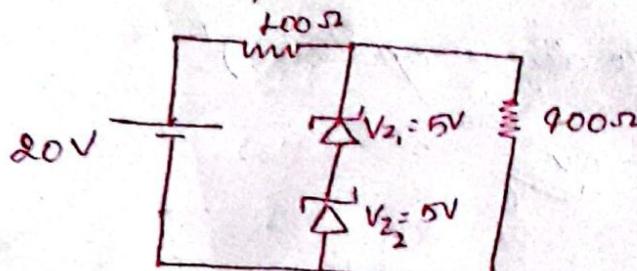
$$= 0.09 W$$

$$= 90 mW$$

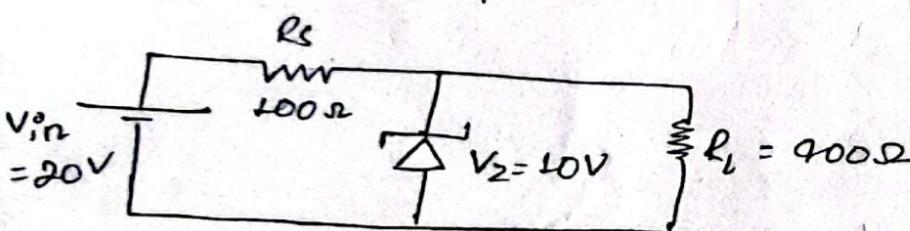
Here,  $P_z$  (90mW) <  $P_{cm}$ , so the diode operate safely.

Q.3. for the circuit shown below, find

1. load voltage ( $V_L$ )
2. current through zener diode ( $I_Z$ )
3. voltage across series resistance
4. power dissipated across zener diode.



Sol. Here the equivalent circuit is,



Note:

Remember:

In series

↳ voltage add & current same

↳ current same & voltage add

In parallel/ shunt

↳ voltage same & current add

↳ current add & voltage same

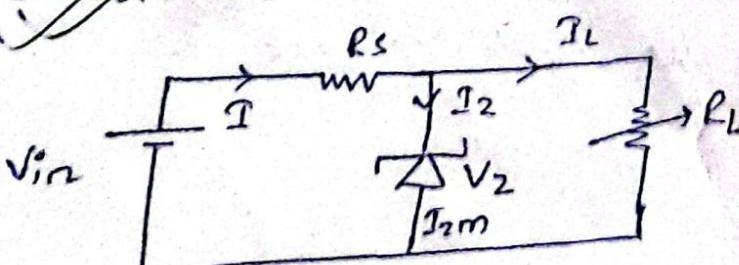
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Homework

ans:

$$\boxed{\begin{aligned} V_L &= 10V \\ I_Z &= 0.075A \\ P_Z &= 0.75 \text{ Watt} \end{aligned}}$$

case 2:  $R_L$  = variable and  $V_{in}$  = constant.



Here,  $I_{zm}$  = maximum zener current

Here we have to find range of  $R_L$  [ $R_{L,\min}$  and  $R_{L,\max}$ ] required for safe turn on of zener diode.

Since, zener diode must be ON,

$$V_L = V_Z$$

for minimum value of  $R_L$  [ $R_{L,\min}$ ]

The open circuit voltage is given by,

$$V = \frac{R_L}{R_L + R_S} * V_{in} \quad \text{--- (1)}$$

for minimum condition,  $V = V_Z$

Now, eqn (1) becomes,

$$\therefore V_Z = \frac{R_L}{R_L + R_S} * V_{in}$$

$$\text{or, } V_Z (R_L + R_S) = R_L \cdot V_{in}$$

$$\text{or, } V_Z \cdot R_L + V_Z \cdot R_S = R_L \cdot V_{in}$$

$$\text{or, } \cancel{V_{in} R_L} - V_Z R_L = V_Z R_S$$

$$\text{or, } R_L [V_{in} - V_Z] = V_Z \cdot R_S$$

$$\text{or, } R_L = \frac{V_Z \cdot R_S}{V_{in} - V_Z}$$

$$\therefore R_{L,\min} = \boxed{\frac{V_Z \cdot R_S}{V_{in} - V_Z}}$$

concept:

for  $R_{L,\min}$ ,  $I_L$  should be max  
for  $I_L(\max)$ ,  $I_Z$  should be zero

and,

$$\boxed{I_{L,\max} = \frac{V_L}{R_{L,\min}}}$$

for maximum value of  $R_L$  [ $R_{L,\max}$ ]

As we know,

$$R_L = \frac{V_L}{I_L}$$

$$R_{L,\max} = \frac{V_L}{I_{L,\min}} \quad \text{--- ①}$$

$$\text{Again, } I = I_L + I_Z$$

$$\therefore I_L = I - I_Z$$

Here,  $I_L \rightarrow I_{L,\min}$ , when  $I_Z \rightarrow I_{Zm}(\max)$

$$\therefore I_{L,\min} = I - I_{Zm} \quad \text{--- ②}$$

from eqn ① and ②

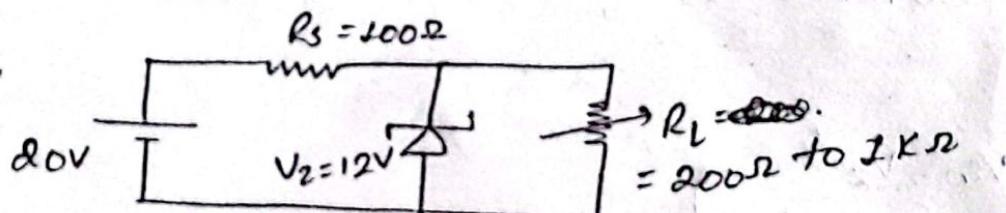
$$R_{L(\max)} = \frac{V_L}{I - I_{Zm}}$$

where,

$$I = \frac{V_{in} - V_Z}{R_S}$$

- Q. A zener diode voltage regulator has 12V zener voltage with variable load resistance. calculate. ( $V_{in} = 20V$ )
- maximum and minimum load current
  - maximum and minimum power dissipation across load.
  - voltage drop across series resistance.
  - minimum value of load resistance to ensure that zener diode is ON.

Soln: Given,



Given,

$$V_{in} = 20V$$

$$R_s = 100\Omega$$

$$V_z = 12V$$

$$R_L(\min) = 200\Omega$$

$$R_L(\max) = 1k = 1000\Omega$$

i) maximum load current,  $I_L(\max) = \frac{V_L}{R_{L,\min}} = \frac{V_z}{R_{L,\min}} = \frac{12}{200} = 60mA$

and,  $I_L(\min) = \frac{V_L}{R_{L,\max}} = \frac{V_z}{R_{L,\max}} = \frac{12}{1000} = 12mA$

ii) maximum power dissipation ( $P_z(\max)$ ) =  $V_z \cdot I_z(\max)$   
 minimum power dissipation ( $P_z(\min)$ ) =  $V_z \cdot I_z(\min)$

Here,

$$I = \frac{V_{in} - V_z}{R_s} = \frac{20 - 12}{100} = 80mA$$

$$\therefore I_z(\min) = I - I_L(\max) = 80mA - 60mA = 20mA$$

$$I_z(\max) = I - I_L(\min) = 80mA - 12mA = 68mA$$

$$\therefore P_{Z(\min)} = 12 * 20 = 240 \text{ mW}$$

$$P_{Z(\max)} = 12 * 68 = 816 \text{ mW}$$

(iii) voltage drop across series resistance or gate voltage

$$V_R = IR_s$$

$$V_R = 80 \text{ mA} * 100 \Omega = 8 \text{ V}$$

Or,

$$\begin{cases} V_R = V_{in} - V_Z \\ V_R = 20 - 12 = 8 \text{ V} \end{cases}$$

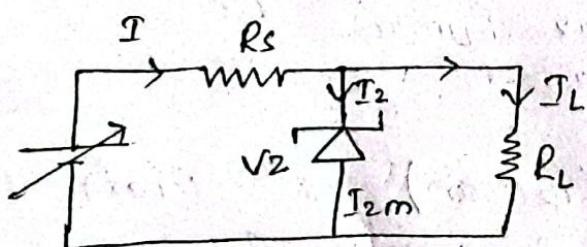
(iv) minimum load resistance

$$R_{L,\min} = \frac{V_Z \cdot R_s}{V_{in} - V_Z} = \frac{12 * 0.1 \text{ k}}{20 - 12} = 0.15 \text{ k}\Omega$$

thus,

$0.15 \text{ k}\Omega$  is the ideal load resistance, which ensure to operate zener diode in ON state.

case 3:  $V_{in}$  = variable and  $R_L$  = constant.



$I_{2m}$ : maximum zener current.

Here, we have to find range of  $V_{in}$  [ie,  $V_{in,\max}$  and  $V_{in,\min}$ ] required for safe turn ON of zener diode. Zener must be ON. Thus,

$$\underline{V_L = V_2}$$

for minimum value of  $V_{in}$  [ $V_{in(min)}$ ]

The open circuit voltage is given by,

$$V = \frac{R_L}{R_L + R_S} \times V_{in}$$

for minimum condition,  $V = V_2$

$$\text{so, } V_2 = \frac{R_L}{R_S + R_L} \times V_{in}$$

$$\text{or, } V_2(R_S + R_L) = R_L \cdot V_{in}$$

$$\text{or, } V_{in} = \frac{V_2(R_S + R_L)}{R_L}$$

$$\boxed{\text{or, } V_{in(min)} = \frac{V_2(R_S + R_L)}{R_L}}$$

Also,

$$\boxed{I_{min} = \frac{V_{in(min)} - V_2}{R_S}}$$

for maximum value of  $V_{in}$  [ $V_{in(max)}$ ]

We know that,

$$I = \frac{V_{in} - V_2}{R_S}$$

$$\text{or, } I R_S = V_{in} - V_2$$

$$\Rightarrow V_{in} = V_2 + I \cdot R_S \quad \text{--- (1)}$$

Here,  $V_{in} \rightarrow V_{in(max)}$ , when  $I \rightarrow I_{max}$

$$V_{in(max)} = I_{max} \cdot R_s + V_Z \quad \text{--- (11)}$$

again,

$$P = I_L + I_2 \quad \text{--- (111)}$$

Here,

$I \rightarrow I_{max}$  when,  $I_2 \rightarrow I_{2m}$

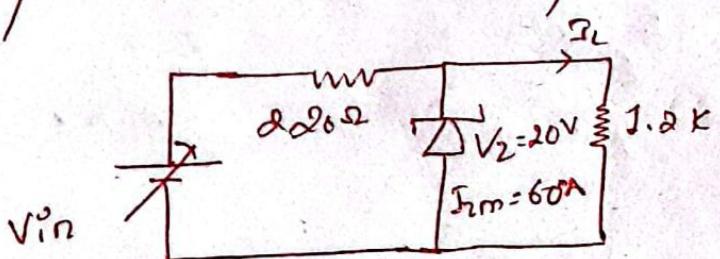
$\therefore$  Egn (111) becomes,

$$I_{max} = I_L + I_{2m} \quad \text{--- (111)}$$

Now, from egn (11) and (111)

$$V_{in(max)} = (I_L + I_{2m}) \cdot R_s + V_Z$$

Q. Determine the range of values of  $V_{in}$  that maintain zener diode in ON-state. Also find the max power that can be dissipated in diode.



Now here,

$$V_{in(max)} = (I_L + I_{2m}) \cdot R_s + V_Z$$

$$\text{where, } V_Z = V_L = I_L R_L$$

$$\Rightarrow I_L = \frac{V_Z}{R_L} = \frac{20}{1.2 \times 10^3} = 16.67 \text{ mA}$$

$$\begin{aligned} \therefore V_{in(max)} &= (16.67 \text{ mA} + 60 \text{ mA}) \cdot 220 + 20V \\ &= 36.867 \text{ V} \end{aligned}$$

Also,

$$V_{in(\min)} = \frac{R_s + R_L}{R_L} * V_2$$
$$= \frac{(1.2 \times 10^3 + 220)}{1.2 \times 10^3} * 20$$

$$\therefore V_{in(\min)} = 23.67 \text{ V}$$

Thus, the range of values of  $V_{in}$  that maintain zener diode in ON state = 23.67 V to 36.86 V.

Also,

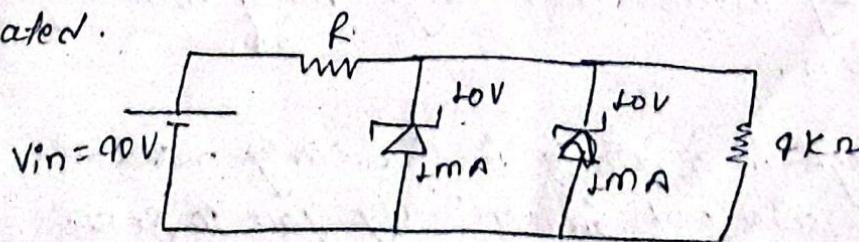
maximum power dissipation in zener diode is

$$P_{max} = I_{2m} * V_2$$
$$= 60 * 20$$
$$= 1200 \text{ mW}$$
$$= 1.2 \text{ W}$$

### Homework

① for the circuit shown below find  $V_o$ ,  $R_s$ ,  $I_{2m}$ ,  $V_{in}$  varies from 20V to 90V. Given,  $V_2 = 10V$ ,  $R_m = 100 \text{ mW}$ ,  $R_L = 10 \text{ k}\Omega$

② A zener diode rating connected in the circuit shown below is 10V, 1mA. ~~fixed~~ in each branch. find the value of series resistance  $R_s$ , so that the output across the load is regulated.



## # Diode switching Time (Switches polarity charge ~~switch~~ to zero?)

A P-N junction diode may be used as an electrical switch. The electrical circuit can be made 'ON' and 'OFF' by forward biasing or reverse biasing the diode. In both cases diode response is accompanied by transient and an interval of time elapses before the diode recovers to its steady state.

The time interval for the recovery of steady state of the diode is called recovery time.

It is of two types:

i) forward Recovery time

ii) Reverse Recovery time.

i) forward Recovery time

The time required for the diode to recover from ~~forward~~ backward biased to forward biased condn.

The diode takes certain interval of time called forward recovery time ( $t_{frr}$ ).

This is defined as time interval b/w instant of 20% diode voltage to 90% of its final value.

ii) Reverse Recovery time

When PN junction is forward biased a large no of electrons cross over from N-region to P-region and a large no of holes cross over from P-region to N-region. They establish a large no of minority carriers in each region.

If the external voltage in a diode is suddenly reversed the diode current will not immediately fall to zero.

A large current flows due to large no of minority carriers for certain interval of time  $t_1$  to  $t_2$  as shown in fig below.

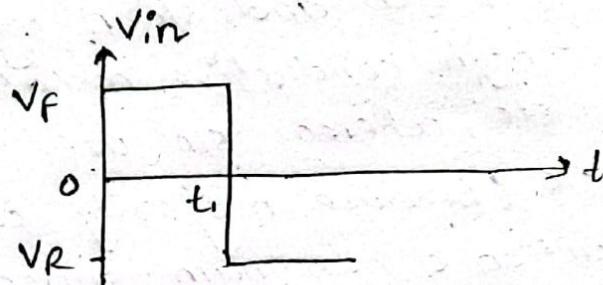
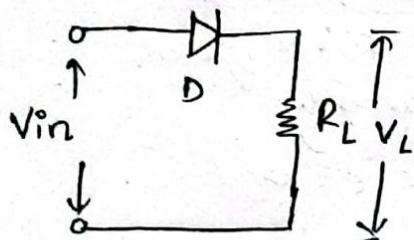
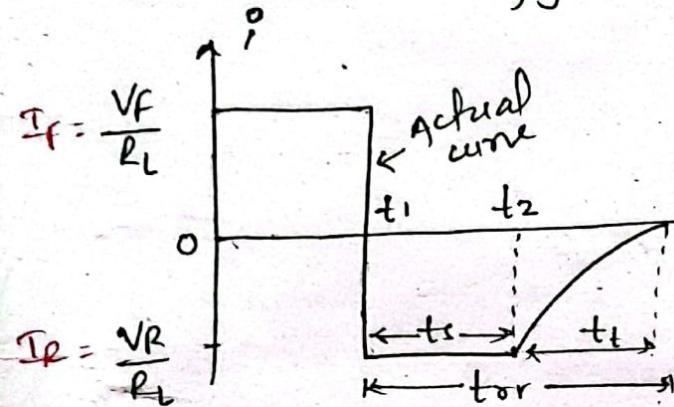


fig @



$$I_F = \frac{V_F}{R_L}$$

$$I_F = \frac{V_R}{R_L}$$

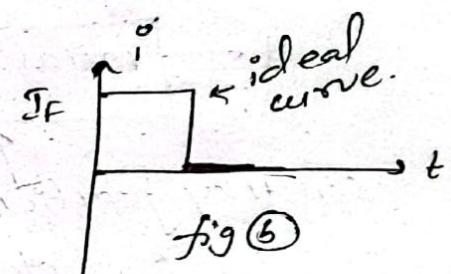


fig ⑤

(in storage time period H.T current or simply polarity change starts from zero at end of gap)

fig ⑥

During time interval  $t_1$  to  $t_2$  the stored minority charge carriers causes large reverse current. This time interval is called storage time ( $t_s$ ). After  $t_2$  diode begins to reverse and diode current begins to fall exponentially to normal steady state reverse saturation current.

The time elapsed b/w  $t_2$  and time instant when diode is nominally recovered is called transition time ( $t_t$ ). The sum of storage time ( $t_s$ ) and transition time ( $t_t$ ) is called reverse recovery time ( $t_{rr}$ ) of diode.

$$\text{i.e. } t_{rr} = t_s + t_t$$

### #. 3. Schottky Diode.

- It is a metal semiconductor diode designed to be used for fast switching applications.
- It consists of metal and sic n-region. The metals used are high conductive metals like silver, gold, platinum etc, whereas sic used are normally n-type sic (because majority carrier is e- and for conduction of maximum current).

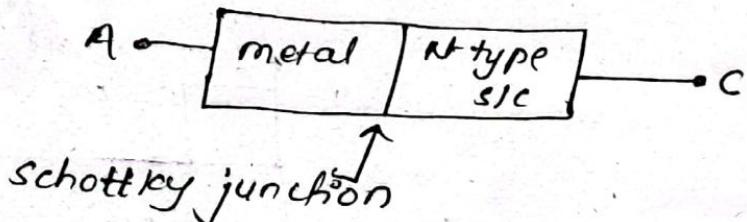


fig: structure of schottky diode

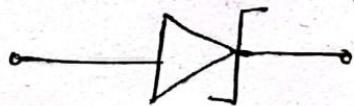


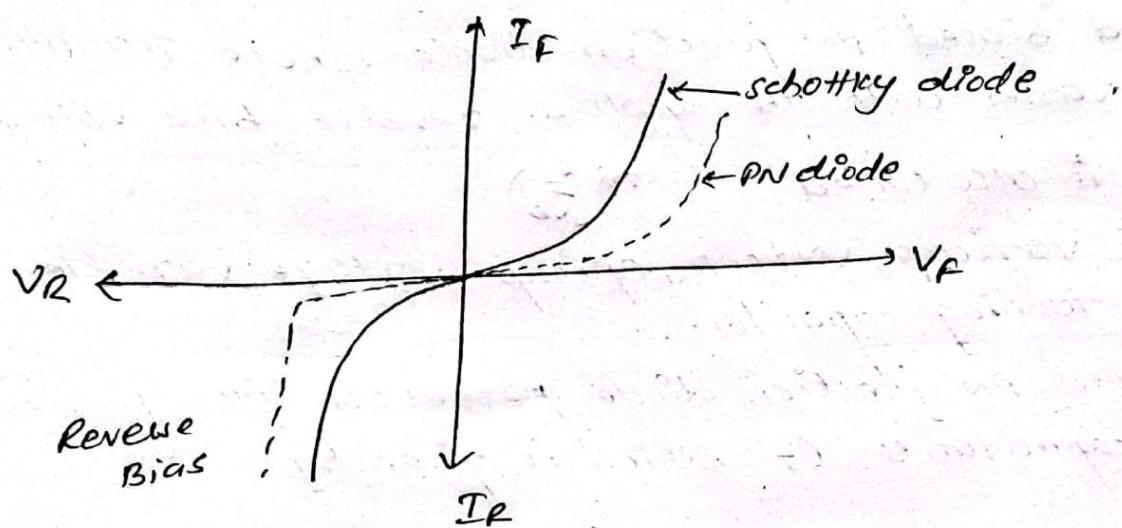
fig: circuit symbol of schottky diode.

- It is unipolar diode (ie. only e's conduct current). It is also called hot carrier diode, because the e- must gain high energy to cross metal sic junction to conduct current.

The metal-sic junction is called schottky junction.

- The metal region of schottky diode is called +ve terminal or anode, whereas the sic region is called -ve terminal or cathode.

The VI characteristics of PN and schottky diode is,



### Applications:

1. To rectify the very high frequency signal.
2. As a switching device in digital computer.  
( depletion region यातली कूने खरकार रेवर्स रेकवरी टाईम  
होताच येणे मुळे fast switching device की दुसरा काम  
जाती )
3. In clipping and clamping circuits
4. In mixing and detecting circuits used in communication.

## Non-Linear model

The electronic devices which do not follow Ohm's law or whose V-I characteristic curve is not straight line are non-linear device.

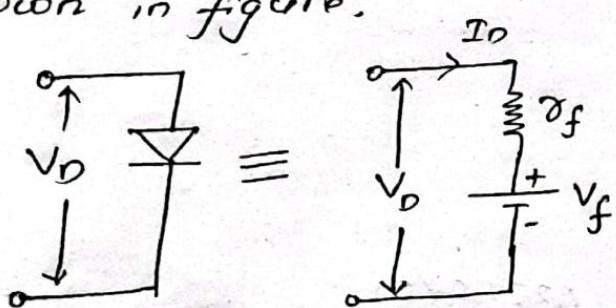
Properties of non-linear device:

1. They do not follow Ohm's law.
2. Their V-I characteristic curve is not straight line
3. They do not follow network theories, like Thévenin's, Norton's, superposition theorem etc.
4. The circuit containing non-linear device can be analyzed by using KCL or KVL.
5. The internal resistance of non-linear device depends on operating conditions like temperature, current, voltage etc.
6. Example, diodes, transistors, FET etc.

[field effect transistor]

Piecewise linear model of diode

Although diode is non linear device, it can be considered as linear device when it's operated in small linear region. The piecewise linear model of diode is shown in figure.



a) diode

b) piecewise linear model of diode

As derived in previous chapter,

$$\gamma_f = \frac{\Delta V}{\Delta I_D}$$

$$\gamma_f = \frac{\partial V}{\partial I_D} \quad \text{--- (1)}$$

we have,  $I_D = I_s (e^{\frac{V_D - V_T}{\eta V_T}} - 1)$

$$\frac{dI_D}{dV_D} = I_s \frac{e^{\frac{V_D - V_T}{\eta V_T}}}{\eta V_T} = \frac{I_D}{\eta V_T}$$

$$\therefore \boxed{\gamma_f = \frac{\eta V_T}{I_D}}$$

where  $\gamma_f$  is diode forward resistance.

$$\boxed{V_T = \frac{kT}{q}}$$

from figure, we have

$$V_D = I_D \gamma_f + V_f$$

$$\boxed{V_f = V_D - I_D \gamma_f}$$

### Numerical:

find piecewise linear model of S-I diode with  $\eta = 1.6$  and  $I_s = 10^{-11} A$  in the vicinity operating point.

Assume  $I_0 = 1mA$ .

so, here,

$$\eta = 1.6$$

$$I_s = 10^{-11} A$$

$$I_0 = 1mA = 1 \times 10^{-3} A$$

we know,

$$V_T = \frac{kT}{q} = \frac{1.38 \times 10^{-23} \times 298}{1.6 \times 10^{-19}} \xrightarrow{(25+273)} \\ = 0.025 V$$

Now,

$$\sigma_f = \frac{m V_T}{I_D}$$
$$= \frac{1.6 \times 0.025}{1 \times 10^{-3}} = 41.4 \Omega$$

Again,

$$V_f = V_0 - I_0 \sigma_f \quad \text{--- (1)}$$

where,

$$I_0 = I_s (e^{\frac{V_0}{m V_T}})$$

$$\Rightarrow e^{\frac{V_0}{m V_T}} = \frac{I_D}{I_s}$$

$$\Rightarrow \frac{V_0}{m V_T} = \ln \left( \frac{I_D}{I_s} \right)$$

$$\Rightarrow V_0 = m V_T \ln \left( \frac{I_D}{I_s} \right)$$

$$\Rightarrow V_0 = 1.6 \times 0.025 \ln \left( \frac{10^{-3}}{10^{-11}} \right)$$

$$\Rightarrow V_0 = 0.76 V$$

from eqn (1)

$$V_f = 0.76 - 10^{-3} \times 41.4$$

$$\boxed{V_f = 0.7186 V} \quad \text{ans}$$

[Note: If  $I_s$  is not given take  $V = 0.7 V$  for Si and  $0.3 V$  for Ge.]

#. Taking an appropriate example of non-linear device show that non-linear device does not follow principle of superposition theorem.

Proof:

Consider a non-linear device (square law device) whose characteristic eqn is given by,

$$I_S = A (V_S - V_{TR})^2 \quad \text{--- (1)}$$

where,

$I_S$  = current through non-linear device

$V_S$  = voltage across non-linear device

$A$  = constant =  $3mA/V^2$

$V_{TR}$  = Threshold voltage = 0

$\therefore$  Eqn (1) becomes,

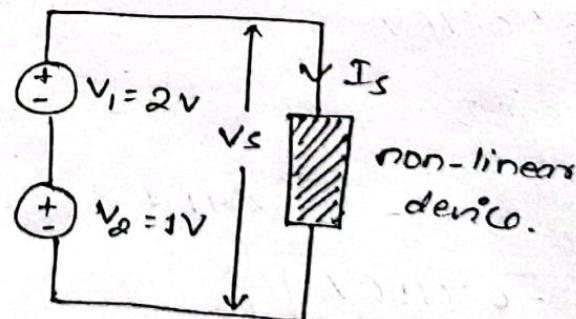
$$I_S = V_S^2 \quad \text{--- (2)}$$

Now, let the non-linear device be connected to a source.  
Here,

$$\begin{aligned} V_S &= V_1 + V_2 \\ &= (2 + 1)V \\ &= 3V \end{aligned}$$

from eqn (2),

$$I_S = V_S^2 = (3)^2 = 9mA$$



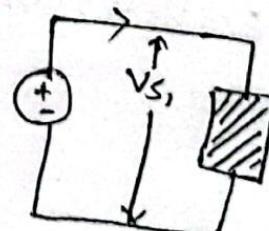
Now, to apply superposition theorem firstly

$$V_{S1} = V_1 = 2V$$

$\therefore$  from (2)  $I_{S1} = V_{S1}^2$

$$I_{S1} = V_{S1}^2 = (2)^2 = 4mA$$

$$V_1 = 2V$$



Now, consider source  $V_2$  only

$$V_{12} = V_2 = 1V$$

so, from eqn ⑪

$$I_{S2} = V_S^2 = 1^2 = 1mA$$

$$V_2 = 1V$$

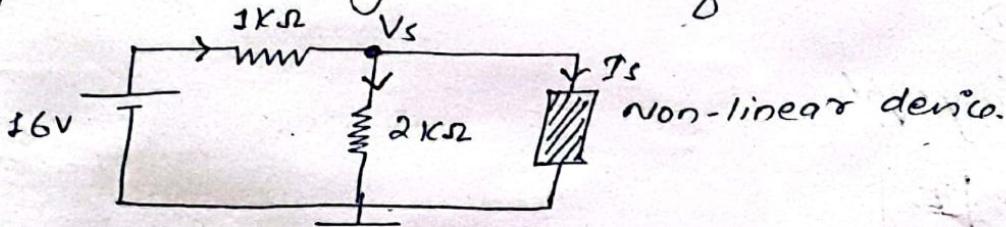
from superposition theorem,

$$I_S + I_{S2} = 4 + 1 = 5mA$$

$$I_S = 9mA$$

Since,  $I_S \neq I_S + I_{S2}$ , this proves that non-linear device does not follow principle of superposition.

# from the circuit given below, find  $I_S$  and  $V_S$ .



Soln

$$\text{Given, } I_S = A(V_S - V_{TR})^2 \quad \text{--- ①}$$

where,

$$A = 1mA/V^2$$

$$V_{TR} = 0$$

from eqn ①,

$$I_S = V_S^2 \quad \text{--- ②}$$

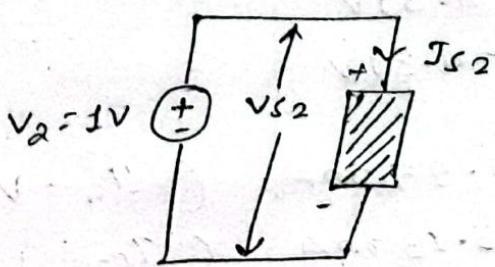
Now, using KCL,

$$-\left(\frac{V_S - 16}{1}\right) - \left(\frac{V_S}{2}\right) - I_S = 0 \quad \left| \frac{16 - V_S}{1} = \frac{V_S}{2} + I_S\right.$$

$$\text{or, } 16 - V_S = \frac{V_S}{2} + V_S^2. \quad [\because I_S = V_S^2]$$

$$\text{or, } 32 - 2V_S = V_S + 2V_S^2$$

$$\text{or, } 2V_S^2 + 3V_S - 32 = 0$$



$$\therefore V_{S1} = 3.3 \text{ V}$$

$$V_{S2} = -4.8 \text{ V}$$

$$\therefore I_S = 20.95 \text{ mA } (I_{S1} = V_{S1}^2)$$

$$I_S = 23.13 \text{ mA } (I_{S2} = V_{S2}^2)$$

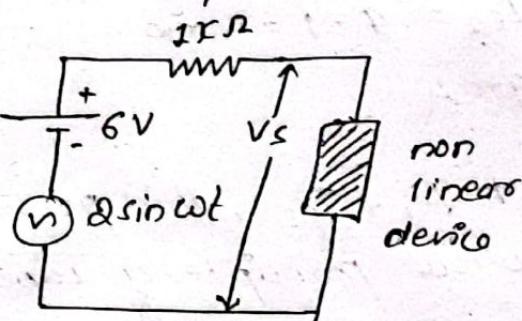
Eg: #. Graphical Analysis of ckt with non-linear devices.  
find the operating point ( $I_S$  and  $V_S$ ) for the ckt given below.

Given,  $I_S = A(V_S - V_{TR})^2$  —①

where,

$$A = 1 \text{ mA/V}^2 \text{ and}$$

$$V_{TR} = 0$$



Eqn ① becomes,

$$I_S = V_S^2 - ②$$

To plot eqn ① in graph,

$V_S$	0	1	2	3	4
$I_S$	0	1	4	9	16

Now, applying KVL in given ckt:

$$2\sin \omega t + 6 - I_S \times 1 - V_S = 0$$

$$\text{or, } 2\sin \omega t + 6 = I_S + V_S \quad ③$$

Take  $\omega t = 0$ , then eqn ③ becomes,

$$2\sin 0 + 6 = I_S + V_S$$

$$\therefore I_S = 6 - V_S$$

To plot in graph.

$V_S$	0	6V
$I_S$	6mA	0

Now, take  $\omega t = \pi/2$  then ⑪ becomes,

$$2\sin \frac{\pi}{2} + 6 = I_c + V_c$$

$$\therefore I_c = 8 - V_c \quad (\because \sin \frac{\pi}{2} = 1)$$

To plot in graph,

$V_s$	0	$8V$
$I_c$	$8mA$	0

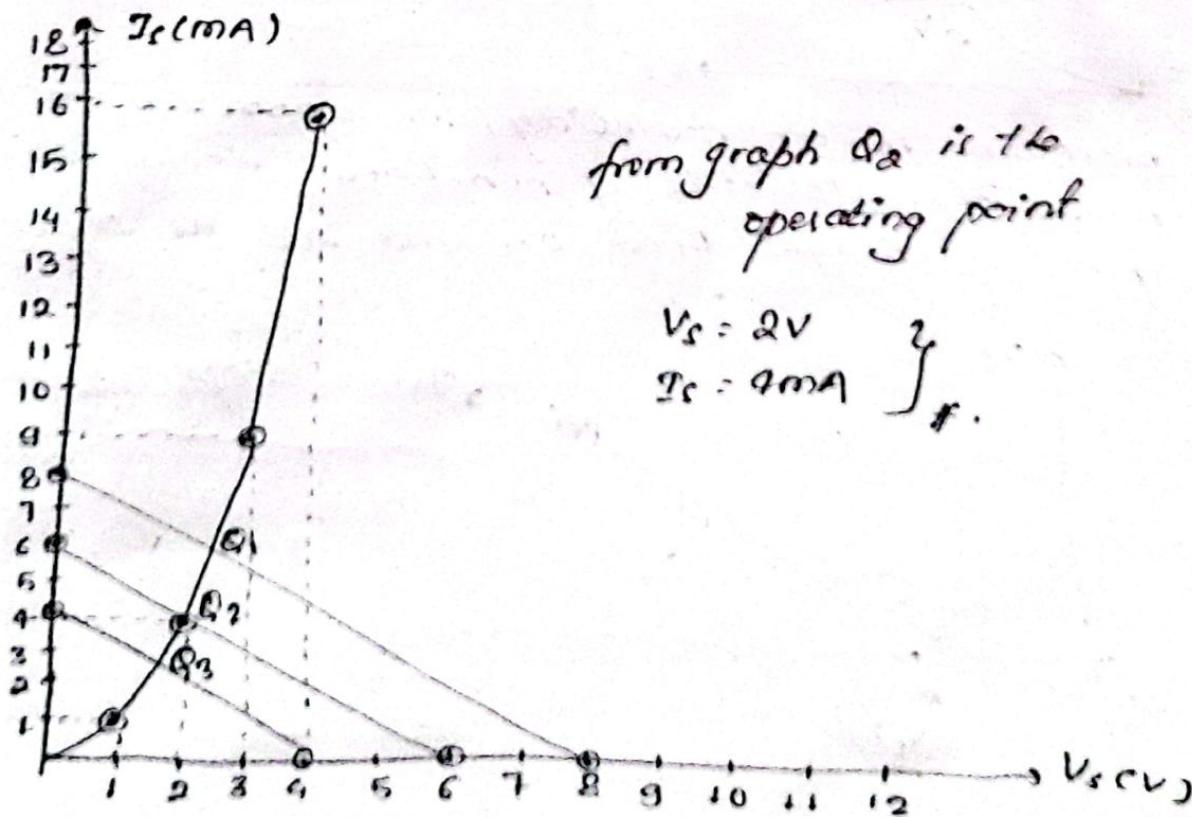
finally, take  $\omega t = \frac{3\pi}{2}$  then eqn ⑪ becomes.

$$2\sin \frac{3\pi}{2} + 6 = I_c + V_c$$

$$\therefore I_c = 9 - V_c \quad (\because \sin \frac{3\pi}{2} = -1)$$

To plot graph,

$V_s$	0	$9V$
$I_c$	$9mA$	0



#. Piecewise linear modeling of non-linear device.  
Consider a non-linear device with V-I characteristics as,

$$I_s = A (V_s - V_{TR})^2 - 0$$

where,

$$A = \text{constant} = 1 \text{mA/V}^2$$

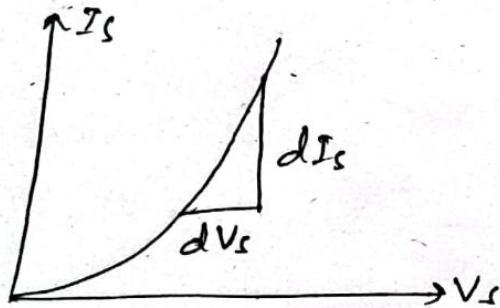
$I_s$  = current in non-linear device

$V_s$  = voltage across non-linear device

$V_{TR}$  = Threshold voltage = 0

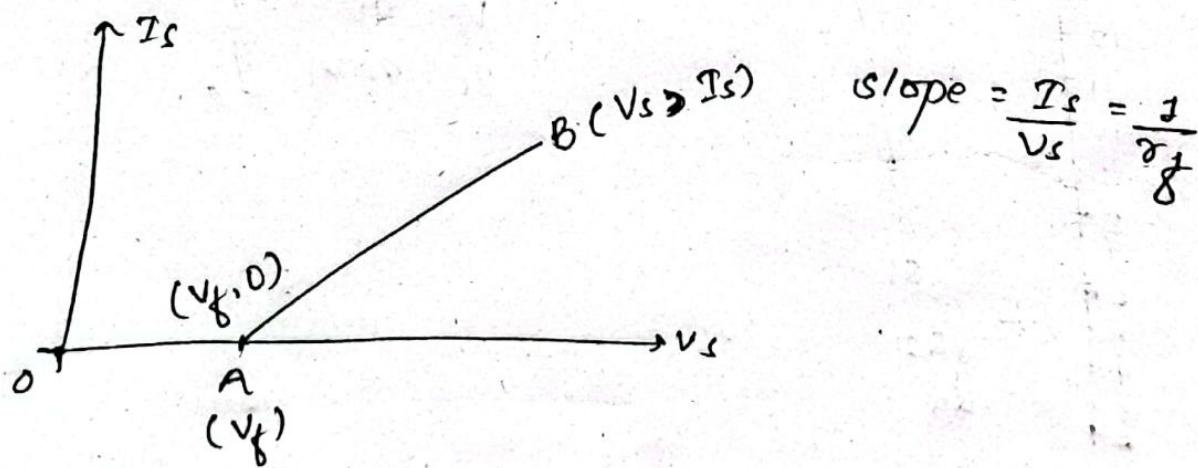
$$\therefore I_s = V_s^2 - ⑪$$

If we plot the graph of above eqn ⑩, we get a non-linear characteristic as shown in fig below:



$$\text{slope} = \frac{dI_s}{dV_s}$$

In piecewise linear modeling, we approximate the non-linear characteristics of non-linear device by using two pieces of straight lines OA and AB as shown in fig.



Here, eqn of OA:  $I_C = 0$  for  $V_S < V_f$

eqn of AB:  $I_C - 0 = \frac{1}{\gamma_f} (V_S - V_f)$   $\left[ \because Y - Y_1 = m (x - x_1) \right]$

where,  $I_C = \frac{1}{\gamma_f} (V_S - V_f)$  — (III) two point formula

$$\gamma_f = \frac{1}{\text{slope}} = \frac{1}{\frac{d I_C}{d V_S}}$$

$$\therefore \gamma_f = \frac{d V_S}{d I_C}$$
 — (III)

from eqn (II),  $I_C = \frac{V_S - V_f}{\gamma_f}$

or,  $I_C \cdot \gamma_f = V_S - V_f$

$$\therefore V_f = V_S - I_C \cdot \gamma_f$$

$\left. \begin{array}{l} \gamma_f = \text{barrier resistance} \\ V_f = \text{barrier voltage} \end{array} \right\}$

from eqn (I),  $I_C = V_S^2$

$$I_C = V_S^2$$

$$\therefore \frac{d I_C}{d V_S} = 2 V_S$$

$$\frac{d I_C}{d V_S} = \frac{d}{d V_S} (V_S^2)$$

$$\therefore \frac{d V_S}{d I_C} = \frac{1}{2 V_S}$$

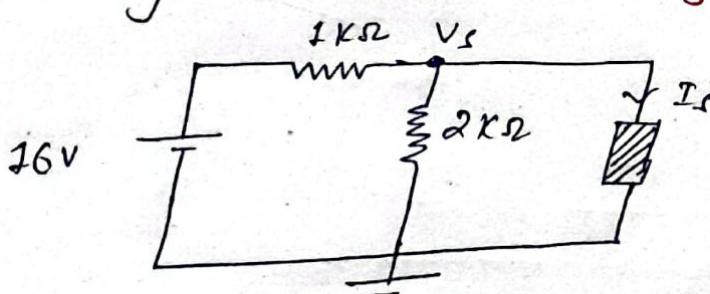
$$\frac{d I_C}{d V_S} = 2 V_S \Rightarrow \frac{d V_S}{d I_C} = \frac{1}{2 V_S}$$

$$\therefore \gamma_f = \frac{1}{2 V_S}$$

from eqn (III).

$$\therefore \boxed{\gamma_f = \frac{1}{2 V_S}}$$

Q. # find the piecewise linear model of the diode in the following circuit. ( $\gamma_f = ?$   $V_f = ?$ )



Given,

$$I_C = A (V_S - V_{TR})^2$$

$$\therefore I_C = V_S^2$$
 — (I)

using KCL,

$$\frac{16 - V_S}{I} = \frac{V_S}{2} + I_S$$

$$\text{or, } 16 - V_S = \frac{V_S}{2} + V_S^2$$

$$\text{or, } 16 - V_S = \frac{V_S + 2V_S^2}{2}$$

$$\text{or, } 32 - 2V_S = V_S + 2V_S^2$$

$$\text{or, } 2V_S^2 + 3V_S - 32 = 0$$

$$\begin{aligned} V_{S1} &= 3.31V \\ V_{S2} &= -4.81V \end{aligned} \quad \left. \begin{array}{l} \\ \end{array} \right\}$$

from eqn ①.

$$I_{S1} = 10.95 \text{ mA}$$

$$I_{S2} = 23.18 \text{ mA}$$

$$\gamma_f = \frac{J}{2V_S} = \frac{2}{2 \times (8.31)} = 0.15 \text{ k}\Omega$$

$$\therefore V_f = V_{S1} - I_{S1} \cdot \gamma_f$$

$$V_f = 3.31 - 10.95 \times 0.15 \quad (\because I_S = 10.95 \text{ mA})$$

$$\boxed{V_f = 1.66V}$$

$$\text{where, } V_S = -4.81$$

$$V_f = -4.81 - 23.18 \times 0.15$$

$$\boxed{\boxed{V_f = -8.28V}}$$