

# **Summary of changes from BSIM-CMG 111.1.1 to BSIM-CMG\_112.0.0**

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## **A. Summary of bug fixes**

1. 2021bug1(IBM): Technical manual update
2. 2021bug2(ADI): Change BETA OP type to `OPM`
3. 2021bug3(ADI, UCB): Appropriate bound for parameters
4. 2021bug4(Cadence, ADI, UCB): Protection for Junction Capacitance Grading Coefficient
5. 2021bug5(ADI): Incorrect derivative of  $\ln\_one\_plus\_exp$  function for  $x < -37$
6. 2021bug6(UCB): Corrections in  $T_{eff}$  implementation in cryogenic model (CRYOMOD=1 and 2)
7. 2021bug7(UCB): Non-zero threshold shift at  $T=T_{nom}$  for  $T_{nom} < 210K$  in CRYOMOD=2
8. 2021bug8(UCB): Impact ionization current missing in ISEFF/IDEFF ops for BULKMOD=0
9. 2021bug9(UCB): Default value of model parameter 'LSP' depends on parameters 'L' and 'XL'
10. 2021bug10(ADI): Conditional assignment of OP variables
11. 2021bug11(Silvaco): Correction in technical manual
12. 2021bug12(UCB): S/D velocity saturation model corrections: a) correct for voltage polarity reversal and b) make delta factor a function of voltage
13. 2021bug13(UCB): Units and typos correction in code/manual
14. 2021bug14(ADI): Remove unused macros
15. 2021bug15(ADI): Limit parameter MVSRSRSD's range
16. 2022bug1(Cadence): Allow  $minr = 0$
17. 2022bug2(Cadence, ADI): Reverse temperature sweep's order in QA

18. 2022bug3(Silvaco, ADI): No key for SmartSpice in QA perl script
19. 2022bug4(UCB): GIDLMOD=2 parameters missing in parameter table of manual
20. 2022bug5(Keysight): Typo in GIDLMOD=2
21. 2022bug6(Keysight, ADI, UCB): Divide by zero case in CRYOMOD=2
22. 2022bug7(Cadence): Code implementation issue in junction\_cap macro
23. 2022bug8(ADI): Use local variables in macros
24. 2022bug9(Cadence, ADI): Bound DTLOW and DTLOW1 to be  $> 0$
25. 2022bug10(UCB): Typos in manual
26. 2022bug12(UCB, ADI, Cadence): Inaccuracy in  $\exp(x) - 1$  calculation in Verilog-A for very small  $x$
27. 2022bug14(ADI): Change terminal “b” in QA with “e” for consistency with the code
28. 2023bug1(Cadence): Discontinuity in  $C_{ds}$  at  $V_{ds} = 0$  for small  $V_{gs}$  (accumulation region)
29. 2023bug2(ADI): Use bias-independent if-else conditions for warnings
30. 2023bug3(Cadence, UCB): Discontinuity in  $C_{ds}$  at  $V_{ds} = 0$  and a large negative gate voltage
31. 2023bug4(UCB): Incorrect units of binning parameters
32. 2024bug1(ADI): Correct the range of parameter TYPE.
33. 2024bug2(UCB): Gummel symmetry issue in Cryogenic Coulomb scattering model.
34. 2024bug3(UCB): Sign correction for variable  $x_{dpart}$  in NQSMOD=2
35. 2024bug4(ADI): Order-of-operations problem in macros  $\gamma_{func}$  and  $smooth_{maxx2}$ .
36. 2024bug5(ADI): Superfluous assignment to  $q_{m\_ln}$ .
37. 2024bug6(ADI): Use updated  $hypsmooth$  function.
38. 2024bug7(ADI): Initialize gate current variables.
39. 2024bug8(IBM): Set a lower limit of zero to  $\phi_{ib}$  to prevent negative square root evaluation.
40. 2024bug9(IBM,ADI): Check for  $W_{GAAeff}$  and  $L_{eff}$  bounds right after their evaluation to prevent a divide-by-zero error.

## B. Summary of Enhancements

1. 2021enh1(IBM): Max NGAA allowed from 3 to 6
2. 2021enh2(IBM, UCB): Enhance Gate to Substrate Capacitance model for GAA
3. 2021enh3(ADI):  $\ln(1.0 + \text{`lexp}(x))$  replacement with new function "ln\_one\_plus\_exp"
4. 2021enh4(TSMC): Width binning parameters due to etch in GAA
5. 2021enh5(UCB): Cryogenic Temperature Model
6. 2020enh6(UCB): Improve accuracy of C-V fitting for high  $V_d$  and  $V_g$
7. 2021enh7(UCB): Improve the accuracy of I-V near  $V_{dsat}$  at high  $V_g$ : S/D velocity saturation model
8. 2021enh8(UCB): Parasitic substrate GIDL/GISL model
9. 2022enh1(ADI): Add QA test to check any missing parameters
10. 2022enh2(UCB): Trap-assisted tunneling (TAT) GIDL model
11. 2022enh3(UCB): Add cryogenic model parameter extraction procedure in manual.
12. 2023enh1(IBM): Improve cryogenic model parameter extraction procedure in the manual.
13. 2023enh1: Reinstate the GAA functionality.
14. 2024enh2(UCB): Thin Film Transistor Model.
15. 2024enh3(ADI, UCB): Add QA tests for all parameters.
16. 2024enh4(Rapidus): Improved gds fitting in low gate overdrive.
17. 2024enh5(ADI,UCB): Change parameter case according to VA standard.
18. 2024enh6(UCB): Flexibility for capacitance tuning in the saturation region.
19. 2024enh7(ADI): Removing NF from parameters/nmosDefaultParameters and parameters/pmosDefaultParameters in the QA package, and redefining the parameter check with NF as an instance parameter.
20. 2024enh8(IBM): Improved Self-Heating model for GAAFETs.
21. 2024enh9(Intel): Additional parameters to model mobility degradation due to hot carriers.
22. 2024enh10(IBM): Improved Self-Heating model for GAAFETs
23. 2024enh12(CMC Policy): Removed TFT feature from 112.0.0beta3
24. 2024enh13(ADI, QA subcommittee): Extended QA to evaluate non-default

parameter values.

## C. Description of bug fixes

### 1. 2021bug1(IBM): Technical manual update

Description of GEOMOD=4 was missing in the manual. We have added them in the 111.2.0\_beta0\_1.

GEOMOD = 4: Unified model

### 2. 2021bug2(ADI): Change BETA OP type to `OPM

In BSIM-CMG111.1.0, BETA op variable was declared as `OPP. Since BETA op should scale with \$mfactor, it was changed to `OPM in BSIM-CMG 111.2.0beta0\_1.

```
`define OPM(nam,uni,des) (* units=uni, desc=des, multiplicity="multiply" *) real nam;
```

### 3. 2021bug3(ADI, UCB): Appropriate bound for parameters

Parameters NI0SUB, BG0SUB and NC0SUB that should physically be positive were allowed to be both positive and negative. These have been restricted to positive values in BSIMCMG111.2.0beta0\_1.

```
`MPRoz(NI0SUB, 1.1e16, "/m^3", "Intrinsic carrier constant at 300.15K")  
`MPRoz(BG0SUB, 1.12, "eV", "Bandgap of substrate at 300.15K")  
`MPRoz(NC0SUB, 2.86e25, "/m^3", "Conduction band density of states")
```

### 4. 2021bug4(Cadence, UCB): Protection for Junction Capacitance Grading

#### Coefficient

Some junction capacitance grading coefficients of BSIMCMG 111.1.0 like “MJS, MJD, MJSWS, MJSWD, MJSWGS, MJSWGD, MJS2, MJD2, MJSWS2, MJSWD2, MJSWGS2, MJSWGD2” had no protection mechanism when they were set to one. If they are set to one, numerical issues will occur due to the presence of terms like  $1/(1-MJ)$  and  $1/(1 - MJ2)$  in the  $Q_{ej}$  calculation in `junction_cap` macro.

There are two types of cases where  $1 / (1 - MJ)$  (or  $1/(1 - MJ2)$ ) appears in the  $Q_{ej}$  calculation depending on the term  $T1 = vex/PB$ .

1. For  $T1 < 0.9$ ,  $Q_{ej}$  involves the terms like  $(1.0 - arg * sarg) / (1.0 - MJ)$  where  $sarg = \text{pow}(arg, -MJ)$

For MJ = 1, (1.0 - arg \* sarg) / (1.0 - MJ) takes 0/0 form. Using the L'Hopital's rule, the limit of this term is a finite number as

$$\lim_{MJ \rightarrow 1} \frac{1 - \arg^{1-MJ}}{1 - MJ} = -\ln(\arg)$$

Therefore, (1.0 - arg \* sarg) / (1.0 - MJ) terms are replaced with -'ln(arg) for MJ=1. Similarly, for MJ2=1.

---

```

if (vex > vec) begin \
  arg = 1.0 - T1; \
  if (MJ == 0.5) begin \
    sarg = 1.0 / sqrt(arg); \
  end else begin \
    sarg = pow(arg, -MJ); \
  end \
  if (MJ != 1) begin \
    Qej = PB * Cz * (1.0 - arg * sarg) / (1.0 - MJ); \
  end else begin \
    Qej = -PB * Cz * `lln(arg); \
  end \
end else begin \
  arg = 1.0 - vec / PB; \
  if (MJ == 0.5) begin \
    sarg = 1.0 / sqrt(arg); \
  end else begin \
    sarg = pow(arg, -MJ); \
  end \
  if (MJ != 1) begin \
    Qec = PB * Cz * (1.0 - arg * sarg) / (1.0 - MJ); \
  end else begin \
    Qec = -PB * Cz * `lln(arg); \
  end \
  arg = 1.0 - (vex - vec) / pb2; \
  if (MJ2 == 0.5) begin \
    sarg = 1.0 / sqrt(arg); \
  end else begin \
    sarg = pow(arg, -MJ2); \
  end \
  if (MJ2 != 1) begin \
    Qej = Qec + SJ * pb2 * Cz * (1.0 - arg * sarg) / (1.0 - MJ2); \
  end else begin \
    Qej = Qec - SJ * pb2 * Cz * `lln(arg); \
  end \
end \
end \

```

2. For T1 >= 0.9

### BSIMCMG111.1.0

```

T2 = pow(0.1, -MJ); \
T3 = 1.0 / (1.0 - MJ); \
T4 = T2 * (T1 - 1.0) * (5.0 * MJ * (T1 - 1.0) + (1.0 + MJ)); \
T5 = T3 * (1.0 - 0.05 * MJ * (1.0 + MJ) * T2); \
Qej = PB * Cz * (T4 + T5); \

```

Here, for MJ=1, the term T5 takes the form of 0/0. T5 for the limit MJ tends to 1 is a constant.

$$\lim_{MJ \rightarrow 1} \frac{1 - 0.05MJ(1 + MJ)0.1^{-MJ}}{1 - MJ} = 1.5 - \ln(0.1)$$

The code is then modified as

```
end else begin \
    T2 = pow(0.1, -MJ); \
    T3 = 1.0 / (1.0 - MJ); \
    T4 = T2 * (T1 - 1.0) * (5.0 * MJ * (T1 - 1.0) + (1.0 + MJ)); \
    if (MJ != 1) begin \
        T5 = T3 * (1.0 - 0.05 * MJ * (1.0 + MJ) * T2); \
    end else begin \
        T5 = 1.5 - ln(0.1); \
    end \
    Qej = PB * Cz * (T4 + T5); \
end \
```

Note:

This bug was addressed in BSIM-CMG111.2.0beta0\_1 release. However, there was a term left that could take 1/0 form for MJ=1 in the junction\_cap macro.

```
T2 = pow(0.1, -MJ); \
T3 = 1.0 / (1.0 - MJ); \
T4 = T2 * (T1 - 1.0) * (5.0 * MJ * (T1 - 1.0) + (1.0 + MJ)); \
if (MJ != 1) begin \
    T5 = T3 * (1.0 - 0.05 * MJ * (1.0 + MJ) * T2); \
end else begin \
    T5 = 1.5 - ln(0.1); \
end \
Qej = PB * Cz * (T4 + T5); \
```

Further, T2 is not required in Qej calculations when MJ=1 and sqrt function can be used in T2 in place of pow function for MJ=0.5.

In BSIM-CMG111.2.0beta0\_2, the above issues have been corrected

```
T4 = T2 * (T1 - 1.0) * (5.0 * MJ * (T1 - 1.0) + (1.0 + MJ)); \
if (MJ != 1) begin \
    if (MJ == 0.5) begin \
        T2 = 1.0 / sqrt(0.1); \
    end else begin \
        T2 = pow(0.1, -MJ); \
    end \
    T3 = 1.0 / (1.0 - MJ); \
    T5 = T3 * (1.0 - 0.05 * MJ * (1.0 + MJ) * T2); \
end else begin \
    T5 = 1.5 - ln(0.1); \
end \
Qej = PB * Cz * (T4 + T5); \
```

Similar rearrangements are made at other places in the junction\_cap macro.

## 5. 2021bug5(ADI): Incorrect derivative of ln\_one\_plus\_exp function for x < -37

ln\_one\_plus\_exp function in BSIM-CMG 111.1.0beta0\_1 is defined as

### BSIM-CMG 111.1.0beta0\_1

```
// ln(1 + exp(x)) function
analog function real ln_one_plus_exp;
    input x; real x;
    begin
        if (x > 37) begin
            ln_one_plus_exp = x;
        end else if (x < -37) begin
            ln_one_plus_exp = 0.0;
        end else begin
            ln_one_plus_exp = ln(1.0 + exp(x));
        end
    end
endfunction
```

Since 0 is assigned to the function for x < -37 (neglecting exp(x) in comparison to 1), its derivative is also 0 in this range. However, considering the actual derivative expression of ln(1 + exp(x))

$$\frac{d\ln(1 + \exp(x))}{dx} = \frac{\exp(x)}{1 + \exp(x)} \neq 0 \text{ for } x < -37$$

In the revised BSIM-CMG 111.2.0beta0\_2 code, ln\_one\_plus\_exp function uses exp(x) for x < -37 which is also consistent with its Taylor series expansion.

### BSIM-CMG 111.1.0beta0\_2

```
// ln(1 + exp(x)) function
analog function real ln_one_plus_exp;
    input x; real x;
    begin
        if (x > 37) begin
            ln_one_plus_exp = x;
        end else if (x < -37) begin
            ln_one_plus_exp = exp(x);
        end else begin
            ln_one_plus_exp = ln(1.0 + exp(x));
        end
    end
endfunction
```

## 6. 2021bug6(UCB): Corrections in T<sub>eff</sub> implementation in cryogenic model

- A. The present T<sub>eff</sub> formulation for CRYOMOD=1 results in an unphysical behavior in two cases
  - i) For T<sub>nom</sub> < TLOW, T<sub>eff</sub> saturates to T<sub>nom</sub> below TLOW instead of saturating to TLOW (see red curve in Fig. 1). Also, a large difference between T<sub>eff</sub> and T can be seen for T > T<sub>nom</sub>.
  - ii) When smoothing factor DTLOW is large, T<sub>eff</sub> can become significantly smaller than T for T > T<sub>nom</sub> (see red curve in Fig. 2).

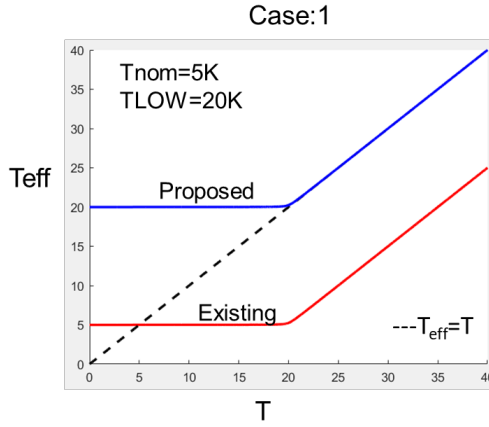


Fig. 1

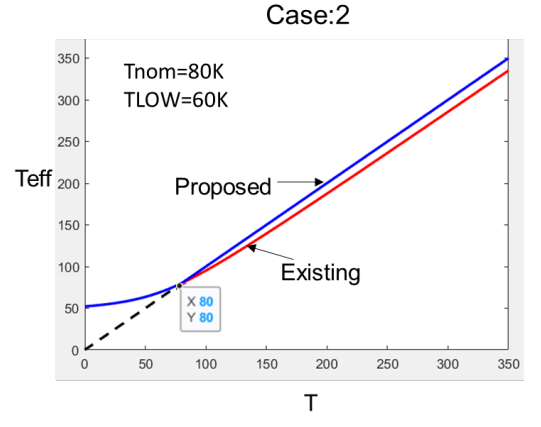


Fig. 2

### BSIM-CMG 111.2.0beta0\_1 CRYOMOD=1

$$T_{low0}(T) = \frac{T + TLOW + \sqrt{(T - TLOW)^2 + 0.25 \cdot DTLOW^2}}{2}$$

$$T_{low1}(T) = \frac{KLOW \cdot (TLOW1 - T) + \sqrt{[KLOW \cdot (TLOW1 - T)]^2 + 0.25 \cdot DTLOW1^2}}{2}$$

$$T_{eff}(T) = T_{low0}(T) + T_{low1}(T) - T_{low0}(T_{nom}) - T_{low1}(T_{nom}) + T_{nom}$$

### Code Implementation

```
DevTempLow0 = `smoothminx(DevTemp, TLOW, DTLOW);
DevTempLow1 = `smoothminx((-KLOW1 * (DevTemp - TLOW1)), 0.0, DTLOW1);
if (CRYOMOD == 1) begin
    DevTempeff = DevTempLow0 + DevTempLow1 - `smoothminx(Tnom, TLOW, DTLOW) - `smoothminx((-KLOW1 * (
        Tnom - TLOW1)), 0.0, DTLOW1) + Tnom;
end else begin
    .
    .
    .
end
```

In BSIM-CMG 111.2.0beta0\_2, we correct this behavior by calculating  $T_{eff}$  as

### BSIM-IMG 111.2.0beta0\_2 CRYOMOD=1

If  $T_{nom} > \tilde{T}LOW$  then

$$T1 = T_{low0}(T) + T_{low1}(T) - T_{low0}(T_{nom}) - T_{low1}(T_{nom}) + T_{nom}$$

end else

$$T1 = T_{low0}(T) + T_{low1}(T) - T_{low0}(T_{nom}) - T_{low1}(T_{nom}) + TLOW$$

end

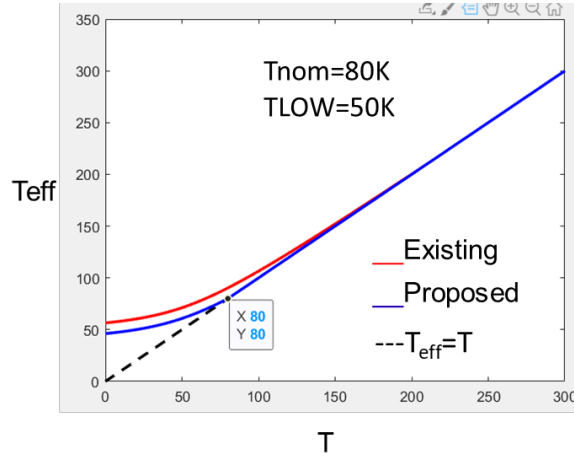
$$T_{eff} = \frac{T + T1 + \sqrt{(T - T1)^2 + 0.25 \cdot 0.04}}{2}$$

### Code Implementation



$T_{eff}$  using the proposed implementation shows correct behavior as evident in Fig. 1 and 2 (blue curves).

- B.  $T_{eff}$  formulation for CRYOMOD=2 does not ensure  $T_{eff}=T_{nom}$  at  $T=T_{nom}$  for  $T_{nom} < 210K$  (see red curve in Fig below). For a multi-temperature fitting, the fitting at  $T=T_{nom}$  must not get affected while tuning temperature model parameters only.



```

Tlow = TLOW;
if (CRYOMOD != 0) begin
    // Effective temperature for core model charge calculation at low temperatures
    DevTempLow0 = `smoothminx(DevTemp, Tlow, DTLOW);
    DevTempLow1 = `smoothminx((-KLOW1 * (DevTemp - TLOW1)), 0.0, DTLOW1);
    if (CRYOMOD == 1) begin
        T1 = `smoothminx(Tnom, Tlow, DTLOW);
        T2 = `smoothminx((-KLOW1 * (Tnom - TLOW1)), 0.0, DTLOW1);
        if (Tnom > Tlow) begin
            T3 = DevTempLow0 + DevTempLow1 - T1 - T2 + Tnom;
        end else begin
            T3 = DevTempLow0 + DevTempLow1 - T1 - T2 + Tlow;
        end
        DevTempeff = `smoothminx(DevTemp, T3, 0.2);
    end else begin
        .
        .
        .
    end
end

```

### BSIM-CMG 111.2.0beta0\_1 CRYOMOD=2

$$T_{low0}(T) = \frac{T + TLOW + \sqrt{(T - TLOW)^2 + 0.25 \cdot DTLOW^2}}{2}$$

$$T_{low1}(T) = \frac{KLOW \cdot (TLOW1 - T) + \sqrt{[KLOW \cdot (TLOW1 - T)]^2 + 0.25 \cdot DTLOW1^2}}{2}$$

$$T1 = T_{low0}(T) + T_{low1}(T) - T_{low0}(210) - T_{low1}(210) + 210$$

$$T_{eff} = \frac{T + T1 + \sqrt{(T - T1)^2 + 0.25 \cdot 0.01}}{2}$$

## Code Implementation

```

end else begin
    T1 = DevTempLow0 + DevTempLow1 - `smoothminx(210, TLOW, DTLOW) - `smoothminx((-KLOW1 * (210 - TLOW1)), 0.0, DTLOW1) + 210;
    DevTempeff = `smoothminx(DevTemp, T1, 0.1);
    DevTemp1 = `smoothmaxx2(DevTemp, 210, 0.1);
    delTemp1 = DevTemp1 - `smoothmaxx2(Tnom, 210, 0.1);
    delTRatio1 = (DevTemp1 - 210) / Tnom;
end

```

$T_{\text{eff}}$  is therefore modified in BSIM-CMG 111.2.0beta0\_2 for  $T_{\text{nom}} < 210$  K to correct for this behavior. The new formulation also takes care of the issues mentioned in A for CRYOMOD=1.

## BSIM-CMG 111.2.0beta0\_2 CRYOMOD=2

If  $T_{\text{nom}} > 210$  then

$$T1 = T_{\text{low0}}(T) + T_{\text{low1}}(T) - T_{\text{low0}}(210) - T_{\text{low1}}(210) + 210$$

$$T_{\text{eff}} = \frac{T + T1 + \sqrt{(T - T1)^2 + 0.25 \cdot 0.04}}{2}$$

end else

If  $T_{\text{nom}} > TLOW$  then

$$T1 = T_{\text{low0}}(T) + T_{\text{low1}}(T) - T_{\text{low0}}(T_{\text{nom}}) - T_{\text{low1}}(T_{\text{nom}}) + T_{\text{nom}}$$

end else

$$T1 = T_{\text{low0}}(T) + T_{\text{low1}}(T) - T_{\text{low0}}(T_{\text{nom}}) - T_{\text{low1}}(T_{\text{nom}}) + TLOW$$

end

$$T2 = \frac{T + T1 + \sqrt{(T - T1)^2 + 0.25 \cdot 0.04}}{2}$$

$$w_h = 0.5 + 0.5 \cdot \tanh[0.5 \cdot (T - 210)]$$

$$w_l = 1 - w_h$$

$$T_{\text{eff}} = w_l \cdot T2 + w_h \cdot T$$

end

end

## Code Implementation

```

end else begin
  if (Tlow > 210) begin
    $strobe("Warning: TLOW = %e is greater than 210 K. Set to 210 K", TLOW);
    Tlow = 210;
  end
  wh = 0.5 + 0.5 * tanh(0.5 * (DevTemp - 210));
  wl = 1.0 - wh;
  if (Tnom > 210) begin
    T1 = `smoothminx(210, Tlow, DTLOW);
    T2 = `smoothminx((-KLOW1 * (210 - TLOW1)), 0.0, DTLOW1);
    T3 = DevTempLow0 + DevTempLow1 - T1 - T2 + 210;
    DevTempeff = `smoothminx(DevTemp, T3, 0.2);
  end else begin
    T1 = `smoothminx(Tnom, Tlow, DTLOW);
    T2 = `smoothminx((-KLOW1 * (Tnom - TLOW1)), 0.0, DTLOW1);
    if (Tnom > Tlow) begin
      T3 = DevTempLow0 + DevTempLow1 - T1 - T2 + Tnom;
    end else begin
      T3 = DevTempLow0 + DevTempLow1 - T1 - T2 + Tlow;
    end
    T4 = `smoothminx(DevTemp, T3, 0.2);
    DevTempeff = wl * T4 + wh * DevTemp;
  end
  DevTemp1 = `smoothmaxx2(DevTemp, 210, 0.2);
  delTemp1 = DevTemp1 - `smoothmaxx2(Tnom, 210, 0.2);
  delTRatio1 = (DevTemp1 - 210) / Tnom;
end

```

#### 7. 2021bug7(UCB): Non-zero threshold shift at $T=T_{nom}$ for $T_{nom} < 210K$ in CRYOMOD=2

The CRYOMOD=2 expression for temperature threshold voltage shift in BSIM-CMG 111.2.0beta0\_1 does not become zero at  $T = T_{nom}$  where  $T_{nom} < 210K$ .

##### BSIM-CMG 111.2.0beta0\_1

```

T4 = KT11 / (1 + `lexp(KT12 * (DevTemp - TVTH))) - KT11 / (1 + `lexp(KT12 * (210 - TVTH)));
if (KT11 * KT12 > 0) begin
  dvth_temp = (KT1_i + KT1L / Leff) * TRatio_m1 + `smoothminx(T4, 0, 1.0e-4);
end else begin
  dvth_temp = (KT1_i + KT1L / Leff) * TRatio_m1 + `smoothmaxx2(T4, 0, 1.0e-4);
end

```

To ensure this, the threshold shift formulation in BSIM-CMG 111.2.0beta0\_2 is modified as

##### BSIM-CMG 111.2.0beta0\_2

```

DevTemp1 = `smoothmaxx2(DevTemp, 210, 0.2);
T4 = `smoothmaxx2(Tnom, 210, 0.2);
dvth_temp = (KT1_i + KT1L / Leff) * TRatio_m1 + KT11 / (1 + `lexp(KT12 * (DevTemp1 - TVTH))) - KT11 / (1 + `lexp(KT12 * (T4 - TVTH)));

```

#### 8. 2021bug8(UCB): Impact ionization current missing in ISEFF/IDEFF OPs for BULKMOD=0

For BULKMOD=0 (SOI), BSIM-CMG111.2.0beta0\_1 implementation does not consider Iii (impact ionization current)

- a) from drain to source in ISEFF for sigvds > 0
- b) from source to drain in IDEFF for sigvds < 0

### BSIM-CMG111.2.0beta0\_1

```

....//Total drain and source currents
....if (sigvds > 0.0) .begin
.....if (BULKMOD != 0) .begin
.....IDEFF = IDS + devsign * idsgen - devsign * (igd + igcd) + devsign * (Iii + igidl) - devsign * Ied;
.....ISEFF = -IDS - devsign * idsgen - devsign * (igs + igcs) + devsign * (igisl) - devsign * Ies;
.....end else .begin
.....IDEFF = IDS + devsign * idsgen - devsign * (igd + igcd + igbd) + devsign * (Iii + igidl - igisl);
.....ISEFF = -IDS - devsign * idsgen - devsign * (igs + igcs + igbs) + devsign * (igisl - igidl);
.....end
....end else .begin
.....if (BULKMOD != 0) .begin
.....IDEFF = -IDS - devsign * idsgen - devsign * (igs + igcs) + devsign * (igisl) - devsign * Ied;
.....ISEFF = IDS + devsign * idsgen - devsign * (igd + igcd) + devsign * (Iii + igidl) - devsign * Ies;
.....end else .begin
.....IDEFF = -IDS - devsign * idsgen - devsign * (igs + igcs + igbd) + devsign * (igisl - igidl);
.....ISEFF = IDS + devsign * idsgen - devsign * (igd + igcd + igbs) + devsign * (Iii + igidl - igisl);
.....end
....end

```

In BSIM-CMG 111.2.0beta0\_2, we correct this for BULKMOD=0. In addition, BULKMOD!=0, the contribution of parasitic substrate GIDL/GISL is also accounted for GIDLMOD=2 and GEOMOD=2, 3 or 5.

### BSIM-CMG111.2.0beta0\_2

```

....if (sigvds > 0.0) .begin
.....if (BULKMOD != 0) .begin
.....if (GIDLMOD == 2 && (GEOMOD == 2 || GEOMOD == 3 || GEOMOD == 5)) .begin
.....IDEFF = IDS + devsign * idsgen - devsign * (igd + igcd) + devsign * (Iii + igidl + igidlb) - devsign * Ied;
.....ISEFF = -IDS - devsign * idsgen - devsign * (igs + igcs) + devsign * (igisl + igislb) - devsign * Ies;
.....end else .begin
.....IDEFF = IDS + devsign * idsgen - devsign * (igd + igcd) + devsign * (Iii + igidl) - devsign * Ied;
.....ISEFF = -IDS - devsign * idsgen - devsign * (igs + igcs) + devsign * igisl - devsign * Ies;
.....end
.....end else .begin
.....IDEFF = IDS + devsign * idsgen - devsign * (igd + igcd + igbd) + devsign * (Iii + igidl - igisl);
.....ISEFF = -IDS - devsign * idsgen - devsign * (igs + igcs + igbs) + devsign * (igisl - igidl - Iii);
.....end
.....end else .begin
.....if (BULKMOD != 0) .begin
.....if (GIDLMOD == 2 && (GEOMOD == 2 || GEOMOD == 3 || GEOMOD == 5)) .begin
.....IDEFF = -IDS - devsign * idsgen - devsign * (igs + igcs) + devsign * (igisl + igislb) - devsign * Ied;
.....ISEFF = IDS + devsign * idsgen - devsign * (igd + igcd) + devsign * (Iii + igidl + igidlb) - devsign * Ies;
.....end else .begin
.....IDEFF = -IDS - devsign * idsgen - devsign * (igs + igcs) + devsign * igisl - devsign * Ied;
.....ISEFF = IDS + devsign * idsgen - devsign * (igd + igcd) + devsign * (Iii + igidl) - devsign * Ies;
.....end
.....end else .begin
.....IDEFF = -IDS - devsign * idsgen - devsign * (igs + igcs + igbd) + devsign * (igisl - igidl - Iii);
.....ISEFF = IDS + devsign * idsgen - devsign * (igd + igcd + igbs) + devsign * (Iii + igidl - igisl);
.....end
.....end
....end

```

## 9. 2021bug9(UCB): Vampyre error: Default value of model parameter 'LSP' depends on parameters 'L' and 'XL'

LSP is a model parameter defined as

```
`MPRoz(LSP, 0.2 * (L + XL), "m", "Thickness of the gate sidewall spacer")
```

The default of LSP depends on L and XL that can be both model and instance parameters.

After workgroup discussion it has been decided to make the default LSP independent of L and XL in BSIM-CMG 111.2.0beta0\_1 as

```
`MPRoz(LSP, 6.0e-9, "m", "Thickness of the gate sidewall spacer")
```

## 10. 2021bug10(ADI): Conditional assignment of OP variables

In BSIM-CMG 111.2.0beta0\_1, the OP variables IGBS, IGBD, IGBINV and IGBACC are only conditionally assigned a value.

### BSIM-CMG 111.2.0beta0\_1

```
if (BULKMOD == 0) begin
    IGBS = devsign * igbs;
    IGBD = devsign * igbd;
end else begin
    IGBINV = devsign * igbinv;
    IGBACC = devsign * igbacc;
end
```

This has been corrected as

### BSIM-CMG 111.2.0beta0\_2

```
if (BULKMOD == 0) begin
    IGBS = devsign * igbs;
    IGBD = devsign * igbd;
    IGBINV = 0.0;
    IGBACC = 0.0;
end else begin
    IGBINV = devsign * igbinv;
    IGBACC = devsign * igbacc;
    IGBS = 0.0;
    IGBD = 0.0;
end
```

## 11. 2021bug11(Silvaco): Correction in technical manual

In the technical manual NQSMOD was defined twice in Table 2

Parameter	Function	Controlled Components
RGATEMOD	Parasitics	Rg: parasitic gate resistance
RDSMOD	Parasitics	Rd: parasitic drain resistance Rs: parasitic source resistance
NQSMOD	Non-quasi static	Rii: Intrinsic input resistance
IGCMOD	Gate leakage	Igs: gate-to-source tunneling current Igd: gate-to-drain tunneling current Igs: gate-to-channel tunneling current at source side Igd: gate-to-channel tunneling current at drain side
NQSMOD	Non-quasi static	Rii: Intrinsic input resistance
IGBMOD	Gate leakage	For BULKMOD = 1, Igbinv: gate-to-substrate tunneling current at inversion Igbacc: gate-to-

This has been corrected in BSIM-CMG 111.2.0\_beta02.

## 12. 2021bug12(UCB): S/D velocity saturation model corrections: a) correct for voltage polarity reversal and b) make delta factor a function of voltage

In BSIM-CMG 111.2.0beta0\_2, the voltage dependent resistance at the drain side is expressed as

$$R_{vs,d} = R_0 \left[ 1 + \left( \frac{\delta_{vs,rd}^{MVSRS D} \cdot devsign \cdot V(di1, di)}{I_{sat,rd} \cdot R_0} \right)^{MVSRS D} \right]^{\frac{1}{MVSRS D}}$$

with

$$\delta_{vs,rd} = \frac{I_{DS}^{4-MVSRS D}}{I_{DS}^{4-MVSRS D} + VSRDFACTOR \cdot I_{sat,rd}^{4-MVSRS D}}$$

- In the resistance  $R_{vs,d}$  expression above,  $V(di1, di)$  can become negative. For this reason, we smoothly clamped the (second) term in brackets to a small number for its negative values in beta0\_2. However, according to physics,  $R_{vs,d}$  should not depend on the sign of the voltage across it. For example, in nmos, if the source is at a higher voltage w.r.t the drain, the beta0\_2 expression will clamp it to  $R_0$  and underestimate  $R_{vs,d}$ , and thereby overestimate the current. Therefore, in beta1 release we now use  $|V(di1, di)|$  instead of  $V(di1, di)$ .
- $\delta_{vs,rd}$  factor in beta1 is replaced with a voltage dependent factor. This makes  $R_{vs,d}$  completely a function of the voltage  $V(di1, di)$ .

The updated  $R_{vs,d}$  expression in BSIM-CMG 111.2.0 beta1 is

$$R_{vs,d} = R_0 \left[ 1 + \left( \frac{\delta_{vs,rd} \cdot |V(di1, di)|}{I_{sat,rd} \cdot R_0} \right)^{MVSRS D} \right]^{\frac{1}{MVSRS D}}$$

$$\delta_{vs,rd} = \frac{|V(di1, di)|^{4-MVSRSD}}{|V(di1, di)|^{4-MVSRSD} + VSRDFACTOR \cdot (R_0 I_{sat,rd})^{4-MVSRSD}}$$

Similar, changes are done for the source side  $R_{vs,s}$ .

## Code Changes

### BSIM-CMG 111.2.0 beta0\_2

```
// Velocity saturation in source/drain resistances
if (RDSMOD == 1) begin
    if (RDLCW > 0) begin
        rdstempvs = `hyposmooth((1.0 + PRTVSRSD * delTemp - 1.0e-6), 1.0e-3);
        `tempdep(VSATRSD_t, VSATRSD, -ATVSRSD)
        T0 = qis - PTWGLVSRSD;
        T0 = `smoothminx(T0, 0.1, 2.0);
        T1 = 10.0 * PSATXVSRSD * T0 / (10.0 * PSATXVSRSD + T0);
        vsatrsd_eff = VSATRSD_t * (1.0 + PTWGVSRSD * T1);
        vsatrsd_eff = `hyposmooth(vsatrsd_eff, 10.0);
        T2 = NFINTtotal * Weff0 * `q * vsatrsd_eff;
        if (GAVSRD == 0) begin
            T3 = 1.0;
        end else begin
            T3 = `smoothminx((devsign * V(di1, di) - RDVDS), 0, 0.5);
            T3 = 1.0 + T3 * GAVSRD;
        end
        isat_rd = T2 * NVSRD * T3;
        delta_vsr = pow(ids, 4 - MVSRSD) / (pow(ids, 4 - MVSRSD) + VSRDFACTOR * pow(isat_rd, 4 - MVSRSD));
        T4 = rdstempvs * RDLCW * WeffWRFactor;
        T5 = pow(delta_vsr, 1.0 / MVSRSD) * devsign * V(di1, di) / (isat_rd * T4);
        T5 = `smoothminx(T5, 0.0, 1.0e-3);
        Rvs_d = T4 * pow((1.0 + pow(T5, MVSRSD)), 1 / MVSRSD);
    end
    if (RSLCW > 0) begin
        if (RDLCW == 0.0) begin
            rdstempvs = `hyposmooth((1.0 + PRTVSRSD * delTemp - 1.0e-6), 1.0e-3);
            `tempdep(VSATRSD_t, VSATRSD, -ATVSRSD)
            T0 = qis - PTWGLVSRSD;
            T0 = `smoothminx(T0, 0.1, 2.0);
            T1 = 10.0 * PSATXVSRSD * T0 / (10.0 * PSATXVSRSD + T0);
            vsatrsd_eff = VSATRSD_t * (1.0 + PTWGVSRSD * T1);
            vsatrsd_eff = `hyposmooth(vsatrsd_eff, 10.0);
            T2 = NFINTtotal * Weff0 * `q * vsatrsd_eff;
        end
        isat_rs = T2 * NVSRD;
        delta_vsr = pow(ids, 4 - MVSRSD) / (pow(ids, 4 - MVSRSD) + VSRDFACTOR * pow(isat_rs, 4 - MVSRSD));
        T4 = rdstempvs * RSLCW * WeffWRFactor;
        T5 = pow(delta_vsr, 1.0 / MVSRSD) * devsign * V(si, sil) / (isat_rs * T4);
        T5 = V(sil, si);
        T5 = `smoothminx(T5, 0.0, 1.0e-3);
        Rvs_s = T4 * pow((1.0 + pow(T5, MVSRSD)), 1 / MVSRSD);
    end
end
```

## BSIM-CMG 111.2.0 beta1

```
// Velocity saturation in source/drain resistances
if (RDSDMOD == 1) begin
    if (RDLCW > 0) begin
        rdstempvs = `hypssmooth((1.0 + PRTVSRSD * delTemp - 1.0e-6), 1.0e-3);
        `tempdep(VSATRSD_t, VSATRSD, -ATVSRSD)
        T0 = qis - PTWGLVSRSD;
        T0 = `smoothminx(T0, 0.1, 2.0);
        T1 = 10.0 * PSATXVSRSD * T0 / (10.0 * PSATXVSRSD + T0);
        vsatrsd_eff = VSATRSD_t * (1.0 + PTWGVSRSD * T1);
        vsatrsd_eff = `hypssmooth(vsatrsd_eff, 10.0);
        T2 = NFINTtotal * Weff0 * `q * vsatrsd_eff;
        T5 = abs(V(dil, di));
        if (GAVSRD == 0) begin
            T3 = 1.0;
        end else begin
            T3 = `smoothminx((T5 - RDVDS), 0, 0.5);
            T3 = 1.0 + T3 * GAVSRD;
        end
        isat_rd = T2 * NVSRD * T3;
        T4 = rdstempvs * RDLCW * WeffWRFactor;
        vsat_rd = isat_rd * T4;
        delta_vsr_d = pow(T5, 4 - MVSRSD) / (pow(T5, 4 - MVSRSD) + VSRDFACTOR * pow(vsat_rd, 4 - MVSRSD));
        T6 = pow(delta_vsr_d, 1.0 / MVSRSD) * T5 / vsat_rd;
        Rvs_d = T4 * pow((1.0 + pow(T6, MVSRSD)), 1 / MVSRSD);
    end
    if (RSLCW > 0) begin
        if (RDLCW == 0.0) begin
            rdstempvs = `hypssmooth((1.0 + PRTVSRSD * delTemp - 1.0e-6), 1.0e-3);
            `tempdep(VSATRSD_t, VSATRSD, -ATVSRSD)
            T0 = qis - PTWGLVSRSD;
            T0 = `smoothminx(T0, 0.1, 2.0);
            T1 = 10.0 * PSATXVSRSD * T0 / (10.0 * PSATXVSRSD + T0);
            vsatrsd_eff = VSATRSD_t * (1.0 + PTWGVSRSD * T1);
            vsatrsd_eff = `hypssmooth(vsatrsd_eff, 10.0);
            T2 = NFINTtotal * Weff0 * `q * vsatrsd_eff;
        end
        isat_rs = T2 * NVSRD;
        T4 = rdstempvs * RSLCW * WeffWRFactor;
        vsat_rs = isat_rs * T4;
        T5 = abs(V(si, sil));
        delta_vsr_s = pow(T5, 4 - MVSRSD) / (pow(T5, 4 - MVSRSD) + VSRDFACTOR * pow(vsat_rs, 4 - MVSRSD));
        T6 = pow(delta_vsr_s, 1.0 / MVSRSD) * T5 / vsat_rs;
        Rvs_s = T4 * pow((1.0 + pow(T6, MVSRSD)), 1 / MVSRSD);
    end
end
```

## 13. 2021bug13(UCB): Units and typos correction in code/manual

### a) Units of SPRT and the corresponding binning parameters

#### BSIM-CMG 111.2.0beta0\_2:

```
`MPRCz(SPRT, 1.0e-2, "/K", "CRYOMOD != 0 parameter for corner temperature smoothing in dual-slope temperature model of series resistance")
`MPRnb(LSPRT, 0.0, "m/K", "L-term of SPRT")
`MPRnb(NSPRT, 0.0, "/K", "N-term of SPRT")
`MPRnb(PSPRT, 0.0, "m/K", "P-term of SPRT")
`MPRnb(WSPRT, 0.0, "m/K", "W-term of SPRT")
`MPRnb(P2SPRT, 0.0, "m^2/K", "WL-term of SPRT")
```

SPRT appears in terms like `smoothminx(rdstemp0, rdstemp1, SPRT\_i) and should be a unitless parameter (since rdstemp0 and rdstemp1 are unitless).

#### Corrected units in BSIM-CMG 111.2.0beta1:

```
`MPRCz(SPRT, 1.0e-2, "", "CRYOMOD != 0 parameter for corner temperature smoothing in dual-slope temperature model of series resistance")
`MPRnb(LSPRT, 0.0, "m", "L-term of SPRT")
`MPRnb(NSPRT, 0.0, "", "N-term of SPRT")
`MPRnb(PSPRT, 0.0, "m", "P-term of SPRT")
`MPRnb(WSPRT, 0.0, "m", "W-term of SPRT")
`MPRnb(P2SPRT, 0.0, "m^2", "WL-term of SPRT")
```



b) Units of binning parameters of TR0

**BSIM-CMG 111.2.0beta0\_2:**

```
`MPRnb(LTR0, 0.0, "m/K", "L-term of TR0")
`MPRnb(NTR0, 0.0, "/K", "N-term of TR0")
`MPRnb(PTR0, 0.0, "m/K", "P-term of TR0")
`MPRnb(WTR0, 0.0, "m/K", "W-term of TR0")
`MPRnb(P2TR0, 0.0, "(m^2)/K", "WL-term of TR0")
```

**Corrected units in BSIM-CMG 111.2.0beta1:**

```
`MPRnb(LTR0, 0.0, "m*K", "L-term of TR0")
`MPRnb(NTR0, 0.0, "K", "N-term of TR0")
`MPRnb(PTR0, 0.0, "m*K", "P-term of TR0")
`MPRnb(WTR0, 0.0, "m*K", "W-term of TR0")
`MPRnb(P2TR0, 0.0, "(m^2)*K", "WL-term of TR0")
```

c) Typo in eq 3.201 on page 24 of manual

**BSIM-CMG 111.2.0beta0\_2**

$$T_{low1}(T) = \frac{KLOW \cdot (TLOW1 - T) + \sqrt{[KLOW \cdot (TLOW1 - T)]^2 + 0.25 \cdot DTLOW1^2}}{2}$$

KLOW in the above expression should be KLOW1

**BSIM-CMG 111.2.0beta1**

$$T_{low1}(T) = \frac{KLOW1 \cdot (TLOW1 - T) + \sqrt{[KLOW1 \cdot (TLOW1 - T)]^2 + 0.25 \cdot DTLOW1^2}}{2}$$

**14. 2021bug14(ADI): Remove unused macros**

In BSIM-CMG 111.2.0beta1, the following macros have been defined but are never used in the code.

NOTICE in file [bsimcmg.va](#), line 36: Macro 'MEXPQM' is never used

NOTICE in file [bsimcmg.va](#), line 36: Macro 'DELTA\_ASYMM' is never used

They have been removed in BSIM-CMG 111.2.0beta2.

**15. 2021bug15(ADI): Limit parameter MVSRSR's range**

The drain/source velocity saturation model in BSIM-CMG 111.2.0 beta1 is given by

$$R_{vs,d} = R_0 \left[ 1 + \left( \frac{\delta_{vs,rd} \cdot |V(di1, di)|}{I_{sat,rd} \cdot R_0} \right)^{MVSRS D} \right]^{\frac{1}{MVSRS D}}$$

with

$$\delta_{vs,rd} = \frac{|V(di1, di)|^{4-MVSRS D}}{|V(di1, di)|^{4-MVSRS D} + VSRDFACTOR \cdot (R_0 I_{sat,rd})^{4-MVSRS D}}$$

In  $\delta_{vs,rd}$ ,  $MVSRS D \geq 4$  can result in a divide by zero situation when  $V(di1, di) = 0$ . We have therefore limited its range to (0, 4) in BSIM-CMG 111.2.0beta2.

```
`MPRoo(MVSRS D, .1.0, .", .0, .4, .Non-linear resistance parameter")
```

## 16. 2022bug1(Cadence): Allow minr = 0

In BSIM-CMG 111.2.0beta1, minr=0 was not allowed due to the use of `MPRoz macro

```
// Minimum resistance value
`MPRoz(minr, $simparam("minr", 1m), "Ohm", "minr is the value below which the simulator expects elimination of
source/drain resistance and it will improve simulation efficiency without significantly altering the results")
```

It has been corrected in BSIM-CMG 111.2.0beta2 replacing `MPRoz by `MPRcz

```
`MPRcz(minr, $simparam("minr", 1m), "Ohm", "minr is the value below which the simulator expects elimination of
source/drain resistance and it will improve simulation efficiency without significantly altering the results")
```

## 17. 2022bug2(Cadence, ADI): Reverse temperature sweep's order in QA

The temperature sweep in BSIM-CMG 111.2.0beta1 QA is performed from -273 C to 125 C as

```
tempSweep.....-273, .125, .1
```

However, Spectre simulates for a dummy point first and starts from -274 C which is not allowed.

In BSIM-CMG 111.2.0beta2 QA, we have reversed the order of the temperature sweep to avoid the aforementioned error as

```
tempSweep.....125, -.273, -.1
```

## 18. 2022bug3(Silvaco, ADI): No key for SmartSpice in QA perl script

The CMC QA suit 3.0.0 perl script does not have key for SmartSpice simulator. The following statement is added in the qaSpec file of BSIM-CMG 111.2.0beta2 as a workaround

```
nTypeSelectionArguments...bsimcmg_va
pins.....d.g.s.b
verilogaFile...../code/bsimcmg.va
keyLetter.....x
checkPolarity.....no
symmetricPins.....d.s
scaleParameters.....m
```

Note: The latest qa release 3.1.0 takes care of the above issue. Therefore, BSIM-CMG\_111.2.0 standard qaSpec file does not need keyletter x.

## 19. 2022bug4(UCB): GIDLMOD=2 parameters missing in parameter table of manual

In **BSIMCMG-111.2.0beta1**, GIDLMOD=2 parameters, AGIDLB, BGIDLB, CGIDLB, EGIDLB, PGIDLB, AGISLB, BGISLB, CGISLB, EGISLB and PGISLB were not listed in the parameters table (6.4) in the manual.

They have been added in **BSIMCMG-111.2.0beta2** as

AGIDLB <sup>(b)</sup>	$\Omega^{-1}$	6.055e-12	-	-	Pre-exponential coeff. for GIDL (GIDLMOD=2)
BGIDLB <sup>(b)</sup>	$Vm^{-1}$	0.3e9	-	-	Exponential coeff. for GIDL (GIDLMOD=2)
CGIDLB <sup>(b)</sup>	$V^3$	0.2	-	-	Parameter for body bias effect of GIDL (GIDLMOD=2)
EGIDLB <sup>(b)</sup>	$V$	0.2	-	-	Band bending parameter for GIDL (GIDLMOD=2)
PGIDLB <sup>(b)</sup>	-	1.0	-	-	Exponent of electric field for GIDL (GIDLMOD=2)
AGISLB <sup>(b)</sup>	$\Omega^{-1}$	AIGDLB	-	-	Pre-exponential coeff for GISL (GIDLMOD=2)
BGISLB <sup>(b)</sup>	$Vm^{-1}$	BGIDLB	-	-	Exponential coeff. for GISL (GIDLMOD=2)
CGISLB <sup>(b)</sup>	$V^3$	CGIDLB	-	-	Parameter for body bias effect of GISL (GIDLMOD=2)L
EGISLB <sup>(b)</sup>	$V$	EGIDLB	-	-	Band bending parameter for GISL (GIDLMOD=2)
PGISLB <sup>(b)</sup>	-	PGIDLB	-	-	Exponent of electric field for GISL (GIDLMOD=2)

## 20. 2022bug5(Keysight): Typo in GIDLMOD=2

BSIM-CMG 111.2.0beta2 has a typo in the following code snippet

```
if (sigvds > 0.0) begin
    igisl = T6;
    igislb = T7;
end else begin
    igidl = T6;
    igislb = T7;
end
```

igislb in the else condition should be igidlb.

Corrected code in BSIM-CMG 111.2.0beta3

```
if (sigvds > 0.0) begin
    igisl = T6;
    igislb = T7;
end else begin
    igidl = T6;
    igidlb = T7;
end
```

## 21. 2022bug6(Keysight, ADI, UCB): Divide by zero case in CRYOMOD=2

In the following condition for UDS\_t in CRYOMOD=2 of BSIMCMG111.2.0beta2,

UDS\_t will blow up if UDS1\_i\*(Tnom - 210)/Tnom is zero (or very close to zero).

Similarly for UDD\_t.

```
if (Tnom == 210) begin
    UDS_t = UDS_i * (`lexp(UDS1_i * delTRatio1) - 1);
    UDD_t = UDD_i * (`lexp(UDD1_i * delTRatio1) - 1);
end else begin
    UDS_t = UDS_i * (`lexp(UDS1_i * (DevTemp1 - 210) / Tnom) - 1) / abs(`lexp(UDS1_i * (Tnom - 210) / Tnom) - 1);
    UDD_t = UDD_i * (`lexp(UDD1_i * (DevTemp1 - 210) / Tnom) - 1) / abs(`lexp(UDD1_i * (Tnom - 210) / Tnom) - 1);
end
```

We provide protection for the above case in BSIMCMG111.2.0beta3 as

```
if (abs(UDS1_i * (Tnom - 210) / Tnom) < 1e-6) begin
    UDS_t = UDS_i * (`lexp(UDS1_i * delTRatio1) - 1);
end else begin
    UDS_t = UDS_i * (`lexp(UDS1_i * delTRatio1) - 1) / abs(`lexp(UDS1_i * (Tnom - 210) / Tnom) - 1);
end
if (abs(UDD1_i * (Tnom - 210) / Tnom) < 1e-6) begin
    UDD_t = UDD_i * (`lexp(UDD1_i * delTRatio1) - 1);
end else begin
    UDD_t = UDD_i * (`lexp(UDD1_i * delTRatio1) - 1) / abs(`lexp(UDD1_i * (Tnom - 210) / Tnom) - 1);
end
```

## 22. 2022bug7(Cadence): Code implementation issue in junction\_cap macro

The following portion of the code of junction\_cap macro in BSIM-CMG 111.2.0 has an implementation issue.

For  $T1 = v_{ex}/P_B > 0.9$

```

T4 = T2 * (T1 - 1.0) * (5.0 * MJ * (T1 - 1.0) + (1.0 + MJ)); \
if (MJ != 1) begin \
    if (MJ == 0.5) begin \
        T2 = 1.0 / sqrt(0.1); \
    end else begin \
        T2 = pow(0.1, -MJ); \
    end \
    T3 = 1.0 / (1.0 - MJ); \
    T5 = T3 * (1.0 - 0.05 * MJ * (1.0 + MJ) * T2); \
end else begin \
    T5 = 1.5 - ln(0.1); \
end \
Qej = PB * Cz * (T4 + T5); \

```

Here, T4 requires T2 but appears before T2 calculation. Further, T2 is missing for MJ=1.

The following shows the correct implementation in **BSIM-CMG 111.2.1**

```

if (MJ != 1) begin \
    if (MJ == 0.5) begin \
        T2 = 1.0 / sqrt(0.1); \
    end else begin \
        T2 = pow(0.1, -MJ); \
    end \
    T3 = 1.0 / (1.0 - MJ); \
    T5 = T3 * (1.0 - 0.05 * MJ * (1.0 + MJ) * T2); \
end else begin \
    T2 = 10.0; \
    T5 = 1.5 - ln(0.1); \
end \
T4 = T2 * (T1 - 1.0) * (5.0 * MJ * (T1 - 1.0) + (1.0 + MJ)); \
Qej = PB * Cz * (T4 + T5); \

```

## 23. 2022bug8(ADI): Use local variables in macros

The junction capacitance macro in BSIM-CMG 111.2.1 uses global variables T1, T2, T3, etc. In BSIM-CMG 111.3.0beta0\_1 these have now been defined locally in the macro itself as

### BSIM-CMG 111.3.0beta0\_1

```

`define junction_cap(block_name, vex, vec, pb2, Cz, PB, SJ, MJ, MJ2, Qej) \
begin: block_name \
    ...real T1, T2, T3, T4, T5; \
    ...real arg, sarg, Qec; \
    ... \
    ...if (Cz > 0.0) begin \
        ...T1 = vex / PB; \
        ...if (T1 < 0.9) begin \
            ...if (SJ > 0.0) begin \
                ...if (vex > vec) begin \
                    ...arg = 1.0 - T1; \

```

## 24. 2022bug9(Cadence, ADI): Bound DTLOW and DTLOW1 to be > 0

DTLOW and DTLOW1 are smoothing parameters used in the cryogenic model effective temperature formulation as

$$T_{low0}(T) = \frac{T + TLOW + \sqrt{(T - TLOW)^2 + 0.25 \cdot DTLOW^2}}{2}$$

$$T_{low1}(T) = \frac{KLOW1 \cdot (TLOW1 - T) + \sqrt{[KLOW1 \cdot (TLOW1 - T)]^2 + 0.25 \cdot DTLOW1^2}}{2}$$

**BSIM-CMG 111.2.1** defines DTLOW and DTLOW1 as real numbers

```
`MPRnb (DTLOW, .1.0, . "K", . "CRYOMOD != .0 . smoothing . parameter . for . TLOW")
`MPRnb (DTLOW1, .0.0, . "K", . "CRYOMOD != .0 . smoothing . parameter . for . TLOW1")
```

DTLOW and DTLOW1 are also allowed to be zero, which can result in temperature derivative discontinuity.

In **BSIM-CMG 111.3.0beta0\_1**, these parameters have been restricted to be positive numbers, and the default value of DTLOW1 has also been changed to 1.0e-3 as

```
`MPRoz (DTLOW, .1.0, . "K", . "CRYOMOD != .0 . smoothing . parameter . for . TLOW")
`MPRoz (DTLOW1, .1.0e-3, . "K", . "CRYOMOD != .0 . smoothing . parameter . for . TLOW1")
```

## 25. 2022bug10(UCB): Typos in manual

Min/max values of a few parameters were incorrectly specified in the **BSIM-CMG 111.2.1** manual

Name	Unit	Default	Min	Max	Description
TLOW	K	50.0	-	0	Transition temperature of SS at low temperatures (CRYOMOD ≠ 0)
DTLOW	K	1.0	-	0	Smoothing parameter for TLOW (CRYOMOD ≠ 0)
TLOW1	K	0.0	-	0	Transition temperature of SS at low temperatures (CRYOMOD ≠ 0)
DTLOW1	K	0.0	-	0	Smoothing parameter for TLOW1 (CRYOMOD ≠ 0)
KLOW1	-	0.0	-	0	Slope magnitude of effective low temperature below TLOW1 (CRYOMOD ≠ 0)

These typos have been corrected in **BSIM-CMG 111 .3.0beta0\_1** manual.

TLOW	$K$	50.0	0.0	-	Transition temperature of SS at low temperatures (CRYOMOD $\neq 0$ )
DTLOW	$K$	1.0	$> 0$	-	Smoothing parameter for TLOW (CRYOMOD $\neq 0$ )
TLOW1	$K$	0.0	0.0	-	Transition temperature of SS at low temperatures (CRYOMOD $\neq 0$ )
DTLOW1	$K$	1.0e-3	$> 0$	-	Smoothing parameter for TLOW1 (CRYOMOD $\neq 0$ )
KLOW1	-	0.0	0.0	-	Slope magnitude of effective low temperature below TLOW1 (CRYOMOD $\neq 0$ )

## 26. 2022bug12(UCB, ADI, Cadence): Inaccuracy in $\exp(x) - 1$ calculation in Verilog-A for very small x

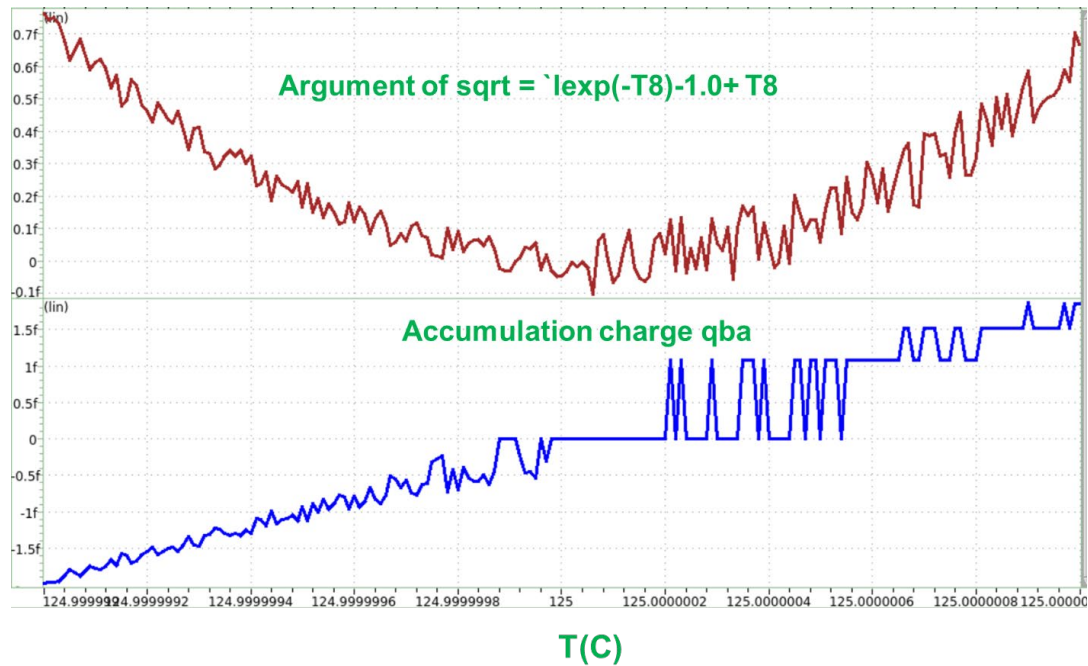
Cadence provided us with a test case where they observed a floating point error in accumulation charge at T very close to 125 °C. After investigation, the problem was found in the calculation of  $\exp(x) - 1$  terms (highlighted) when x becomes close to zero, which was happening in this test case.

```

T9 = K1_t / (2.0 * nVtm) * sqrt(Vtm);
T0 = T9 / 2.0;
T2 = (vge - (deltaPhi - Eg - Vtm * ln(NBODY_i / Nc) + DELVFBACC)) / Vtm;
if ((T2 * Vtm) > phib + T9 * sqrt(phib * Vtm)) begin
    T1 = sqrt(T2 - 1.0 + T0 * T0) - T0;
    T10 = 1.0 + T1 * T1;
    T6 = exp(-T10) - 1.0;
end else begin
    T3 = T2 * 0.5 - 3.0 * (1.0 + T9 / sqrt(2.0));
    T10 = T3 + sqrt(T3 * T3 + 6.0 * T2);
    if (T2 < 0.0) begin
        T4 = (T2 - T10) / T9;
        T6 = -T10 + T4 * T4;
        T10 = -ln(1.0 - T10 + T4 * T4);
    end else begin
        T11 = exp(-T10);
        T4 = sqrt(T2 - 1.0 + T11 + T0 * T0) - T0;
        T10 = 1.0 - T11 + T4 * T4;
        T6 = exp(-T10) - 1.0;
    end
end
end
T7 = sqrt(T6 + T10);
if (T10 > 1.0e-15) begin
    e0 = -(T2 - T10) - T9 * T7;
    e1 = 1.0 - T9 * 0.5 * T6 / T7;
    T8 = T10 - (e0 / e1);
    T11 = exp(-T8) - 1.0;
    T12 = sqrt(T11 + T8);
    qba = -T9 * T12 * Vtm;
end else begin
    if (T10 < -1.0e-15) begin
        e0 = -(T2 - T10) - T9 * T7;
        e1 = 1.0 + T9 * 0.5 * T6 / T7;
        T8 = T10 - e0 / e1;
        T12a = exp(-T8) + T8 - 1.0;
        if (T12a <= 0) begin
            T12 = 0.0;
        end else begin
            T12 = T9 * sqrt(T12a);
        end
    end else begin
        T8 = 0.0;
        T12 = 0.0;
    end
    qba = T12 * Vtm;
end

```

It was found that the value of  $\text{`lexp}(x) - 1$  using Verilog-A  $\text{exp}(x)$  function was inaccurate for very small  $x$  and resulted in a numerical noise, e.g., as shown in the figure below the calculation of the term  $\text{`lexp}(-T8) - 1.0 + T8$ . Note that mathematically, this term must  $\geq 0$  for any  $T8$  value, however, due to numerical noise it sometimes becomes negative and when used in the  $\text{sqrt}$  function, results in a floating-point error.



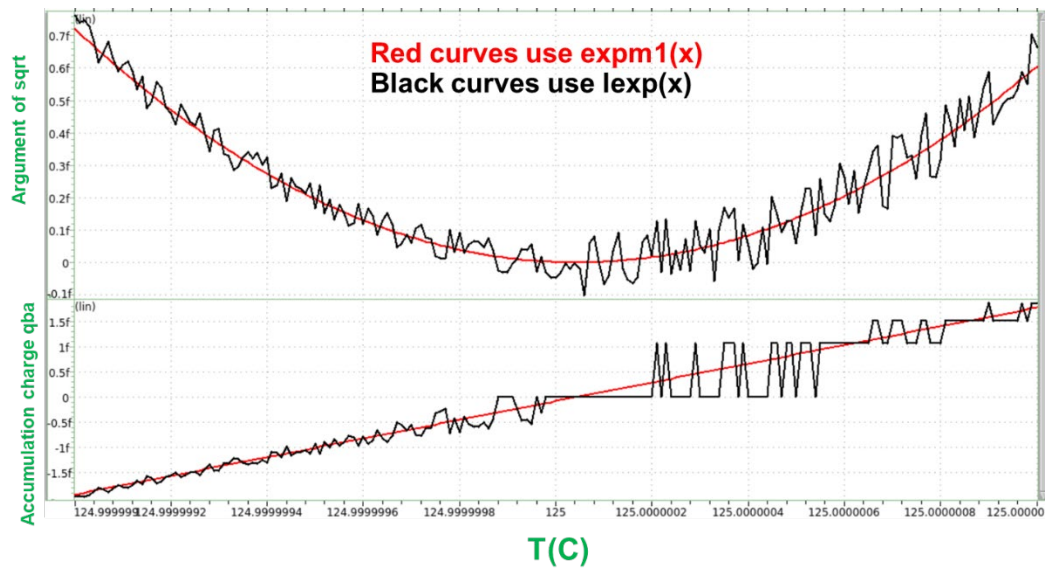
In **BSIM-CMG 112 .0.0beta0\_1** we have replaced the above highlighted  $\text{`lexp}(x) - 1$  terms with a new function called  $\text{expm1}(x)$

```
//exp(x) - 1 function
analog function real expm1;
  input x; real x;
  begin
    if (abs(x) < 1e-7) begin
      expm1 = x + 0.5 * x * x;
    end else begin
      expm1 = `lexp(x) - 1.0;
    end
  end
endfunction
```

This function uses a Taylor expansion up to the second order and ensures that the value of  $\text{exp}(x) - 1 + x$  remains always positive (higher order Taylor terms are numerically lost when  $x$  is small). Also, note that for  $|x| \geq 1e-7$ ,  $\text{expm1}$  becomes equal to  $\text{`lexp}(x) - 1$ . With  $\text{expm1}$  used in accumulation charge ( $q_{ba}$ ) calculation, we



do not see any numerical noise or floating-point errors since the argument of the sqrt function always remains positive as shown in the figure below.

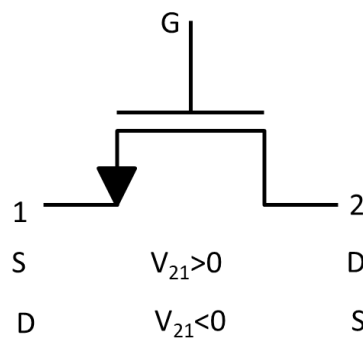


## 27. 2022bug14(ADI): Change terminal “b” in QA with “e” for consistency with the code

The body terminal in the BSIM-CMG code is denoted by “e”. For consistency, the body terminal named “b” in QA files (qaspec & reference files) is replaced with the letter “e”.

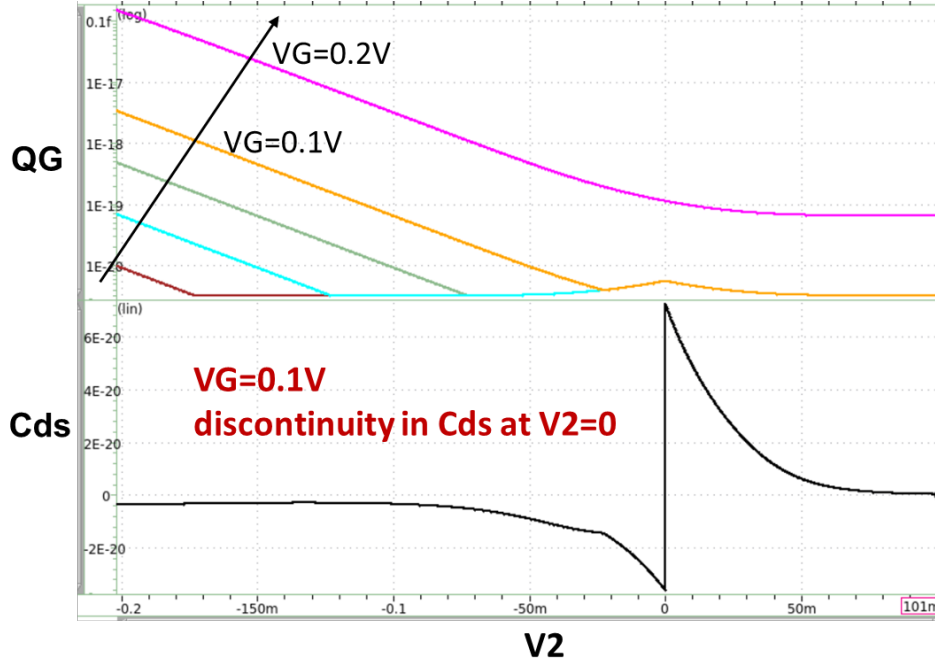
## 28. 2023bug1(Cadence): Discontinuity in Cds at Vds =0 for small Vgs (accumulation region)

A discontinuity in Cds capacitance is observed when Vgs is small and Vds is swept from a positive value to a negative value as shown in the case below.



$V_G=V_1=V_B=0$ ,  $V_2$  is swept across 0

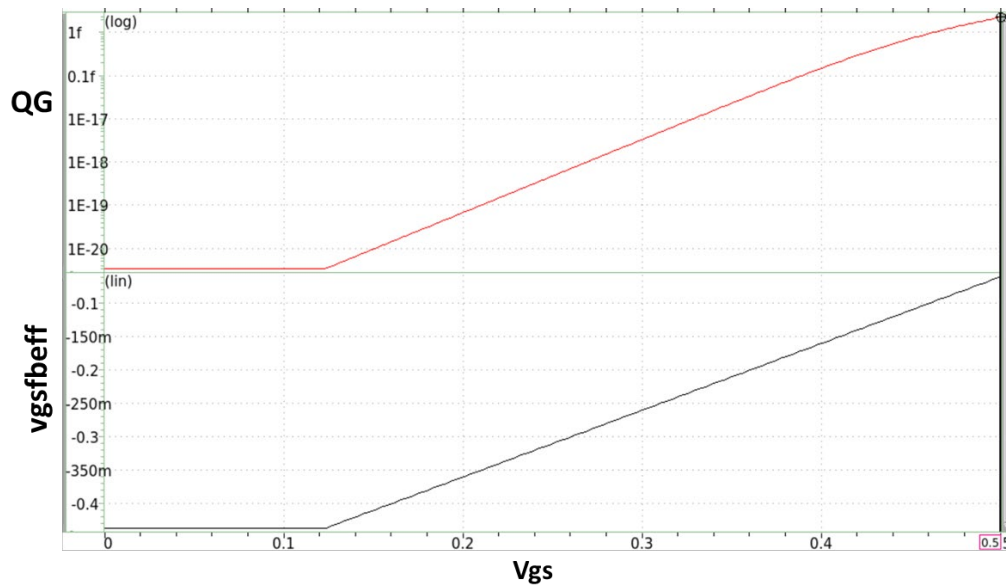
The following figure shows the gate terminal charge and  $C_{ds}$  as a function of  $V_2$  for different  $V_g$  values.



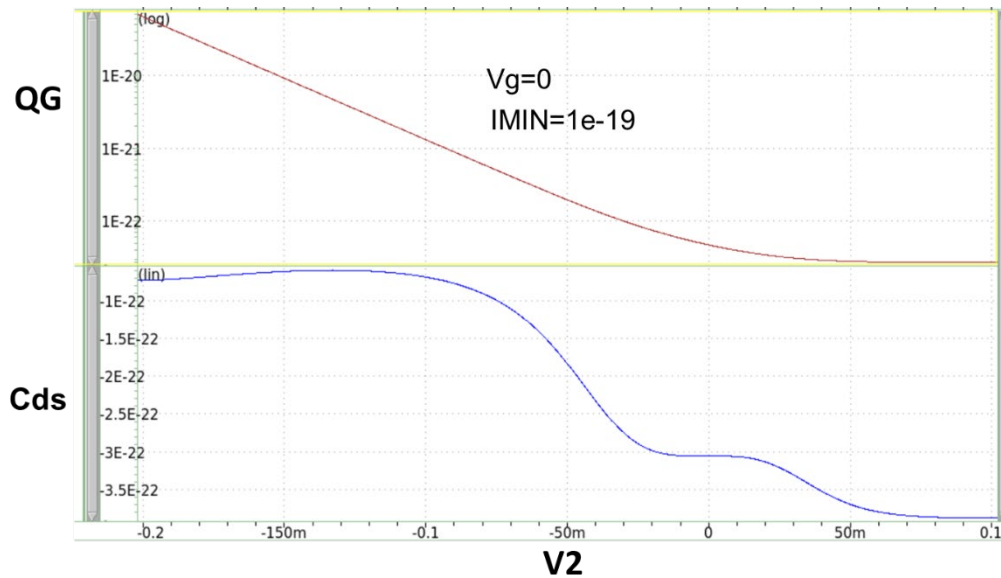
As shown for low  $V_g$ ,  $Q_g$  exhibits a change in slope  $V_2=0$ , and  $C_{ds}$  is discontinuous. For  $V_{21}>0$ , terminal 2 acts as the drain. As  $V_{21}=V_{ds}$  increases, the drain draws up electrons from the channel and  $Q_g$  decreases as expected from physics. However, for  $V_{21} < 0$ , the source and drain are swapped. Now  $V_{ds}$  still increases but  $V_{gs}$  also increases simultaneously. Physically,  $V_{gs}$  should take over and  $Q_g$  should increase for  $V_2<0$ . For  $V_g=0.2V$  this is the case, but for  $V_g=0.1V$  (or lower),  $Q_g$  starts to decrease first and then increases. This reduction of  $Q_g$  causes a discontinuity in capacitance at  $V_{ds}=0$ . It indicates an initial  $Q_g$  desensitivity w.r.t  $V_{gs}$  for  $V_2<0$ . We find this is due to the clamping used for calculating effective  $V_{gs}$  in accumulation region in BSIM-CMG as shown in the code snippet below.

```
.beta0=.u0_a*.cox*.Weff0./Leff;
.T0=- (dvch_qm+.nVtm*.ln(2.0*.cox*.IMIN./ (beta0*.nVtm*.q*.Nc*.TFIN))) ;
.T1=.vgsfb+.T0+.DELVTRAND;
.vgsfbefh=.hypsmooth(T1,.1.0e-4)-.T0;
```

$V_{gs}$  is clamped when device reaches accumulation region, and the current becomes very small. The lower limit of current can be set by the parameter  $IMIN$ . For small  $V_{gs}$ ,  $Q_g$  is also clamped and does not change w.r.t  $V_{gs}$  as shown in the figure below.



This desensitivity of  $Q_G$  results in the decrease in  $Q_G$  observed earlier for  $V_{21} < 0$  since the effect of  $V_{ds}$  takes over. To avoid this issue, the current limit  $IMIN$  can be reduced from the default value of  $1e-15A/m^2$ . As shown below, for  $IMIN=1e-19$ , the  $Q_G$  behavior is physical and discontinuity in capacitance for low  $V_{gs}$  goes away.



We have added a precautionary note in the technical manual of **BSIM-CMG 112.0.0beta0\_1** as

“ $V_{gsbeff}$  limiting for a small  $V_{gs}$  and  $V_{ds}$  being swept from positive to negative values can sometimes result in discontinuities in terminal capacitances. Such issues if

arise can be resolved by lowering the value of IMIN parameter.”

## 29. 2023bug2(ADI): Use bias-independent if-else conditions for warnings

Several instances of bias-dependent if-else conditions in BSIM-CMG 112.0.0beta0\_1 were using \$strobe conditions. These can be categorized into two types.

Type 1:

### BSIM-CMG 112.0.0beta0\_1

```
if (VSAT_t < 1000) begin
    $strobe("Warning: VSAT(%g) = %g is less than 1K, setting it to 1K.", DevTemp, VSAT_t);
    VSAT_t = 1000;
end
```

VSAT\_t is device temperature (DevTemp) dependent i.e., it is also bias dependent. In total, there were 11 VAMPyRE Warnings that applied to VSAT\_t, VSAT1\_t, VSATCV\_t, VSATR\_t, and VSAT1R\_t in CRYOMOD=0, 1, and 2, and TEMPMOD=0 and 1.

Since the if-else condition is bias-dependent here, the simulator must save the message during evaluation and then print the saved messages when the iteration converges. To avoid this, we have removed the \$strobe statement message as

### BSIM-CMG 112.0.0beta0\_2

```
if (VSAT_t < 1000) begin
    VSAT_t = 1000;
end
```

Type 2:

There were also if-else statements with bias-dependent charge density-based conditions.

### BSIM-CMG 112.0.0beta0\_1

```
if (qis < 0.0) begin
    $strobe("Warning: Negative source-side inversion carrier density. Vgs = %g. Vds = %g. Vbs = %g. qis = %g", V(g, s), V(d, s), V(e, s), qis);
end
if (qid < 0.0) begin
    $strobe("Warning: Negative drain-side inversion carrier density. Vgs = %g. Vds = %g. Vbs = %g. qid = %g", V(g, s), V(d, s), V(e, s), qid);
end
if (qis_cv < 0.0) begin
    $strobe("Warning: Negative source-side inversion carrier density for C-V. Vgs = %g. Vds = %g. Vbs = %g. qis_cv = %g", V(g, s), V(d, s), V(e, s), qis_cv);
end
if (qid_cv < 0.0) begin
    $strobe("Warning: Negative drain-side inversion carrier density for C-V. Vgs = %g. Vds = %g. Vbs = %g. qid_cv = %g", V(g, s), V(d, s), V(e, s), qid_cv);
end
end
```

## BSIM-CMG 112.0.0beta0\_2

The above warnings have now been removed from the code since they don't affect the code calculations in any way.

### 30. 2023bug3(Cadence, UCB): Discontinuity in Cds at Vds=0 and a large negative gate voltage

For test cases involving  $V_d$  sweeping from positive to negative values (or vice versa) and large negative  $V_{gs}$  (Fig. 1), it was found that the Cds and Csd capacitances are discontinuous at  $V_{ds}=0$  as shown in Fig. 2.

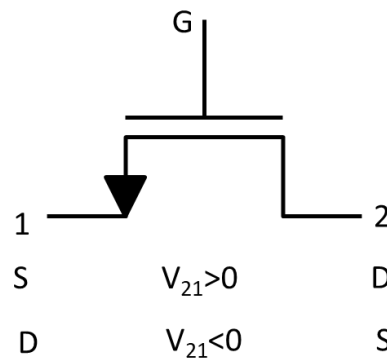
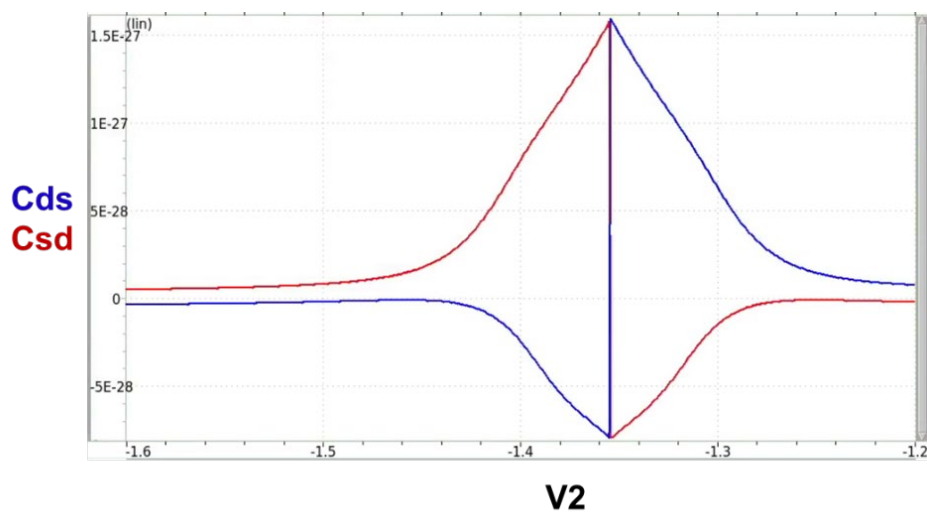


Fig. 1 Test setup for capacitance discontinuity check.  $V_1 = -1.35424$  V,  $V_g = -5.5566$  V,  $V_b = 0$  V, and  $V_2$  is swept from a positive to a negative value. Temperature = 125 C.



The fundamental reason for the discontinuity was found to be the Vgs clamping to a minimum level in the large negative Vgs region. The minimum Vgs level can be controlled using the parameter IMIN. It was suggested in the BSIM-CMG 112.0.0beta0\_1 manual that for such cases, the IMIN be reduced from its default value of 1e-15 to a smaller number to reduce the minimum Vgs and thereby get rid of the capacitance discontinuity. However, the Vgs clamping formulation shown below still put a limit to the minimum Vgs value achieved.

### BSIM-CMG 112.0.0beta0\_1

```

T0 = -(dvch_qm + nVtm * ln(2.0 * cox * IMIN / (beta0 * nVtm * q * Nc * TFIN)));
T1 = vgsfb + T0 + DELVTRAND;
vgsfb_eff = hypsmooth(T1, 1.0e-4) - T0;

```

Here the Vgs clamp is limited by  $\ln(x)$ , which gets clamped to LN\_N\_MINLOG = -87.498233534 for  $x < N\_MINLOG \cdot 1.0e-38$ , which results in the minimum Vgs limit of  $\sim -3V$  (at  $T=125C$ ), no matter how small IMIN becomes.

We have now rearranged the terms in the same formulation as follows, which can achieve a much smaller value of the minimum Vgs clamp.

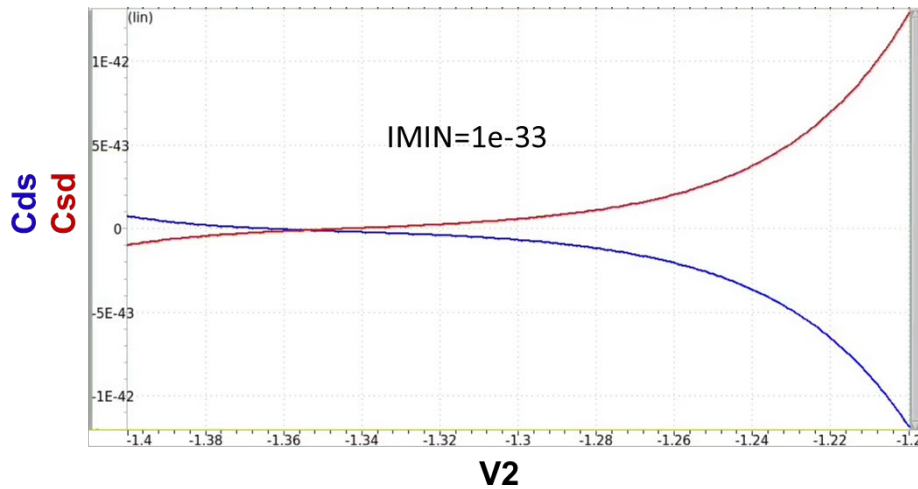
### BSIM-CMG 112.0.0beta0\_2

```

T3 = pow((2.0 * cox * IMIN / (beta0 * nVtm * q * Nc * TFIN)), nVtm);
T0 = -(dvch_qm + ln(T3));
T1 = vgsfb + T0 + DELVTRAND;
vgsfb_eff = hypsmooth(T1, 1.0e-4) - T0;

```

The above formulation can achieve a minimum Vgs clamp value of -88.498V at  $T = 125 C$  and solves the capacitance discontinuity issue with  $IMIN=1e-33$  as shown below.



### 31. 2023bug4(UCB): Incorrect units of binning parameters

The VAMPyRE testing of BSIM-CMG 112.0.0beta0\_1 flagged incorrect format of the units  $m \cdot V^{-1}$  of two parameters, PBTATD and PBTATS. The unit formats have now been corrected in BSIM-CMG 112.0.0beta0\_2 as  $V^{-1} \cdot m$  for both parameters.

### 32. 2024bug1(ADI): Correct the range of parameter TYPE.

In BSIM-CMG 112.0.0beta0\_3, TYPE=0 is also an allowed value due to the following definition

```
`MPIcc(TYPE,`ntype,`",`ptype,`ntype,"1:.NMOS;-1:.PMOS")
```

We have corrected it in BSIM-CMG 112.0.0beta0\_3 by defining a new macro MPity and using it for defining TYPE as

```
`define MPity(nam,def,uni,des) (*units=uni,desc=des*) parameter integer nam=def from[-1:1] exclude 0;

`MPity(TYPE,`ntype,`",`",`ntype,"1:.NMOS;-1:.PMOS")
```

### 33. 2024bug2(UCB): Gummel symmetry issue in Cryogenic Coulomb scattering model

For non-zero values UDS and UDD, the CRYOMOD=1 or 2 exhibits the Gummel symmetry issue. The issue is resolved in BSIM-CMG 112.0.0beta0\_4 by introducing a Vds dependent factor in Dmob as:

For CRYOMOD  $\neq 0$  or TFTMOD = 1

$$T1 = \begin{cases} q_{is} & \text{TFTMOD}=0 \\ q_{frees} & \text{TFTMOD}=1 \end{cases} \quad T2 = \begin{cases} q_{id} & \text{TFTMOD}=0 \\ q_{freed} & \text{TFTMOD}=1 \end{cases}$$

$$D_{mob} = \begin{cases} 1 + UA(T) \cdot (E_{effa})^{EU} + \frac{UD(T)}{\left(\frac{1}{2} \cdot \left(1 + \frac{UDS_{eff}(T) \cdot T1 + UDD_{eff}(T) \cdot T2}{1E-2/Cox} \cdot T3\right)\right)^{UCS(T)}} & \text{BULKMOD}=0 \\ 1 + (UA(T) + UC(T) \cdot V_{eff}) \cdot (E_{effa})^{EU} + \frac{UD(T)}{\left(\frac{1}{2} \cdot \left(1 + \frac{UDS_{eff}(T) \cdot T1 + UDD_{eff}(T) \cdot T2}{1E-2/Cox} \cdot T3\right)\right)^{UCS(T)}} & \text{BULKMOD}=1 \end{cases}$$

where  $T3 = 1 - \exp(-V_{dseff}^2 / 6.25 \times 10^{-4})$  is a factor to preserve Gummel symmetry.

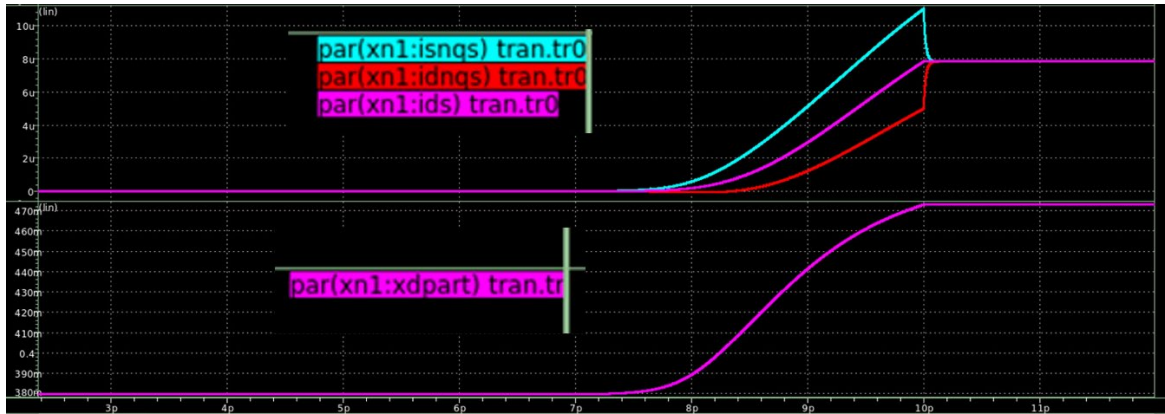
#### 34. 2024bug3(UCB): Sign correction for variable xdpart in NQSMOD=2

The existing model for NQSMOD=2 behaved incorrectly, with both the source and drain current components leading the drain-source current. This has been corrected by inverting the sign of the variable xdpart.

```
2649     if (NQSMOD == 2) begin
2650         |   xdpart = - qd / qg;
2651     end else begin
2652         |   xdpart = 0.0;
2653     end
```

With this change in place, the drain and source current components lag and lead, respectively, in transient simulations (as shown below):





### 35. 2024bug4(ADI): Order-of-operations problem in macros gammafunc and smoothmaxx2.

In BSIM-CMG 112.0.0beta0\_4 and older versions, the definitions of macros in general, and gammafunc and smoothmaxx2 in particular, did not conserve the order of operations. To correct this, all arguments after a minus, multiplication, or division sign in the macro are surrounded by a bracket. E.g.

The macro smoothmaxx2 was changed from:

```
`define smoothmaxx2(x,x0,deltax) (0.5*(x+x0-sqrt((x-x0)*(x-
x0))+0.25*deltax*deltax)))
```

To:

```
`define smoothmaxx2(x,x0,deltax) (0.5*(x+x0-sqrt((x-(x0))*(x-
(x0)))+0.25*deltax*deltax)))
```

### 36. 2024bug5(ADI): Superfluous assignment to qm\_ln.

The variable qm\_ln was being defined but never used. All instances of this variable were removed.

### 37. 2024bug6(ADI): Use updated hypsmooth function.

The hypsmooth macro was improved following the improvements in the hypsmooth function in BSIM-BULK, aimed at preventing divide-by-zero errors caused by large negative arguments to hypsmooth. The existing macro reads as:

```
`define hypsmooth(x, c) (0.5 * (x + sqrt((x) * (x) + 4.0 * c * c)))
```

In the case that  $|x|$  is large, we can use a Taylor series:

$$\sqrt{1 + \varepsilon} = 1 + \varepsilon/2 - \varepsilon^2/8 + \dots$$

$$\sqrt{x * x + 4.0 * c * c} = |x| * \sqrt{1.0 + 4.0 * c * c / (x * x)}$$

$$\approx |x| * (1 + 2 * (c/x)^2 - 2 * (c/x)^4 + \dots)$$

When  $x < 0$ , the leading 1 cancels the  $x$  in hypsmooth ( $x + |x| = 0$ ), and the hypsmooth macro evaluates to zero. This can create problems if the output of the hypsmooth macro is used as a denominator – leading to divide-by-zero errors. To prevent this, large negative cases are handled by an updated definition as:

```
`define hypsmooth(x, c) ((x < -1e4 * (c)) ? (-c) * (c) / (x)) : (0.5 * (x + sqrt((x) * (x) + 4.0 * (c) * (c))))
```

### 38. 2024bug7(ADI): Initialize gate current variables.

The variables igbacc\_v, igbd\_v, igbinv\_v, igbs\_v, igcd\_v, igcs\_v, igd\_v, igidl\_v, igisl\_v, and igs\_v were not initialized. This has been updated in the latest code, with these variables set to zero.

### 39. 2024bug8(IBM): Set a lower limit of zero to phib to prevent negative square root

## evaluation.

A lower limit of zero was introduced for the variable phib to prevent negative square root evaluations:

```
if (cryomod == 0) begin
    phib = Vtm * `lln(NBODY_i / ni);
    phib = `smoothminx(phib, 0, 1e-10);
    vbi = Vtm * `lln(NBODY_i * nsd / (ni * ni));
end else begin
    phib = Vtm * (`lln(NBODY_i) - niln);
    phib = `smoothminx(phib, 0, 1e-10);
    vbi = Vtm * (`lln(NBODY_i * nsd) - 2 * niln);
end
```

## 40. 2024bug9(IBM,ADI): Check for WGAAeff and Leff bounds right after their evaluation to prevent a divide-by-zero error

The evaluation of WGAAeff involves an unbounded term  $XW_i$ , which can lead to WGAAeff being zero.

```
WGAAeff = wga + XW_i;
WGAAeff1 = WGAAeff + DWBIN_i;
```

This can cause a divide-by-zero error in the following lines:

```
if (geomod == 5) begin
    Inv_W = 1.0e-6 / WGAAeff1;
    Inv_WL = 1.0e-12 / (WGAAeff1 * Leff1);
```

Similarly,  $L_g = 1 + XL_i$ ; and  $L_g$  can take a value of zero. This can cause  $Leff$  to be zero and a divide-by-zero error when evaluating  $Inv_L$ .

To prevent these conditions, the following check was introduced right after the assignments for WGAAeff and Leff:

```
if (geomod == 5) begin
    if (WGAAeff1 <= 0.0) begin
        $error("Fatal: WGAAeff1 = %g is not positive.", WGAAeff1);
    end else if (WGAAeff1 <= 1.0e-9) begin
        $strobe("Warning: WGAAeff1 = %g <= 1.0e-9.", WGAAeff1);
    end
end

if (Leff <= 0.0) begin
    $error("Fatal: Leff = %g is not positive.", Leff);
end else if (Leff <= 1.0e-9) begin
```

```

        $strobe("Warning: Leff = %g <= 1.0e-9.", Leff);
    end

    if (Leff1 <= 0.0) begin
        $error("Fatal: Leff1 = %g is not positive.", Leff1);
    end else if (Leff1 <= 1.0e-9) begin
        $strobe("Warning: Leff1 = %g <= 1.0e-9.", Leff1);
    end
    if (LeffCV <= 1.0e-9) begin
        $strobe("Warning: LeffCV = %g <= 1.0e-9.", LeffCV);
    end
    if (bulkmod != 0) begin
        if (LeffCV_acc <= 1.0e-9) begin
            $strobe("Warning: LeffCV_acc = %g <= 1.0e-9.", LeffCV_acc);
        end
    end
end

```

## D. Description of Enhancements

### 1. 2021enh3(ADI): $\ln(1.0 + \text{'lexp}(x))$ replacement with new function

#### "ln\_one\_plus\_exp"

BSIMCMG 111.1.0 uses  $\ln(1.0 + \text{'lexp}(x))$  terms at a few places.

$\ln(1.0 + \text{'lexp}(x))$  becomes

- numerically indistinguishable from  $x$  for  $x > 37$
- numerically indistinguishable from 0 for  $x < -37$

For these cases it is not required to compute  $\ln$  and  $\text{'lexp}$ .

Therefore,  $\ln(1.0 + \text{'lexp}(x))$  is replaced with a new function `ln_one_plus_exp` defined as

```

analog function real ln_one_plus_exp;
    input x; real x;
    begin
        if (x > 37) begin
            ln_one_plus_exp = x;
        end else if (x < -37) begin
            ln_one_plus_exp = 0.0;
        end else begin
            ln_one_plus_exp = ln(1.0 + exp(x));
        end
    end
endfunction

```

## 2. 2021enh5(UCB): Cryogenic Temperature Model

These models are introduced in BSIM-CMG111.2.0beta0\_1 to capture the device physics and temperature effects down to low cryogenic temperatures, such as for the CMOS circuits used in quantum computing applications.

Cryogenic models can be enabled by CRYOMOD switch which can have the following three settings

CRYOMOD = 0 Turns off cryogenic models (same temperature models as BSIM-CMG111.1.0)

CRYOMOD = 1 Most physical cryogenic models

CRYOMOD = 2 Cryogenic temperature expressions converge to BSIM-CMG111.1.0 temperature expressions for  $T > 210$  K (-63.15 C)

In summary, the cryogenic mode introduces new temperature models for the following effects

- Mobility power laws
- Drain bias dependence of Coulomb scattering
- Velocity Saturation and Pinch-Off Voltage
- Band Tail States and Fermi-Dirac Effects for SS and  $V_{th}$
- Source/Drain Resistances

For details of the above models, please refer to the BSIMCMG\_111.2.0 technical manual.

## 3. 2020enh6(UCB): Improve accuracy of C-V fitting for high $V_d$ and $V_g$

Existing BSIM-CMG C-V model scheme may not be sufficient to fit the CV data for different  $V_d$  and high  $V_g$  (see Fig. 4)

### Fitting using BSIM-CMG111.2.0beta0\_1

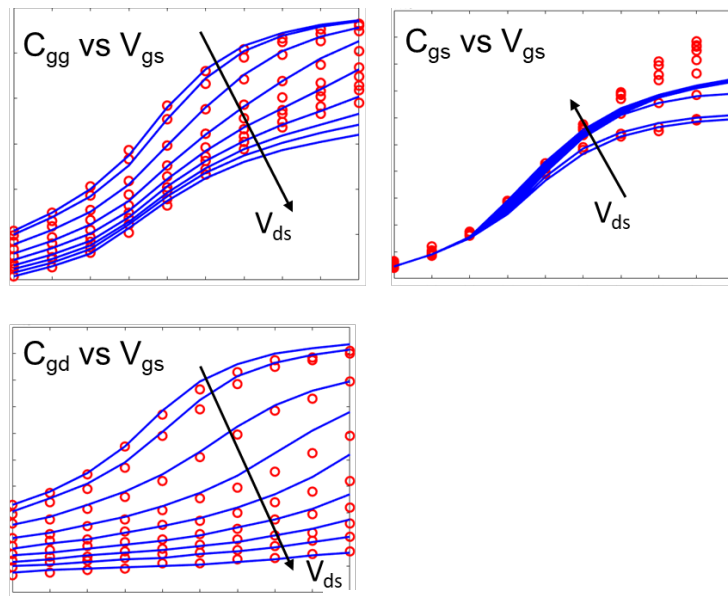


Fig. 4

To improve capacitance fitting flexibility additional, I-V and C-V parameters are decoupled

ETA0  $\rightarrow$  ETA0CV

U0  $\rightarrow$  U0CV

UA  $\rightarrow$  UACV

UD  $\rightarrow$  UDCV

UC  $\rightarrow$  UCCV

CVMOD=1 is used to enable this feature.

Fitting using the updated scheme is shown in Fig. 5. As can be seen the decoupling provides a much better fit to the C-V data.

### Fitting using BSIM-CMG111.2.0beta0\_2

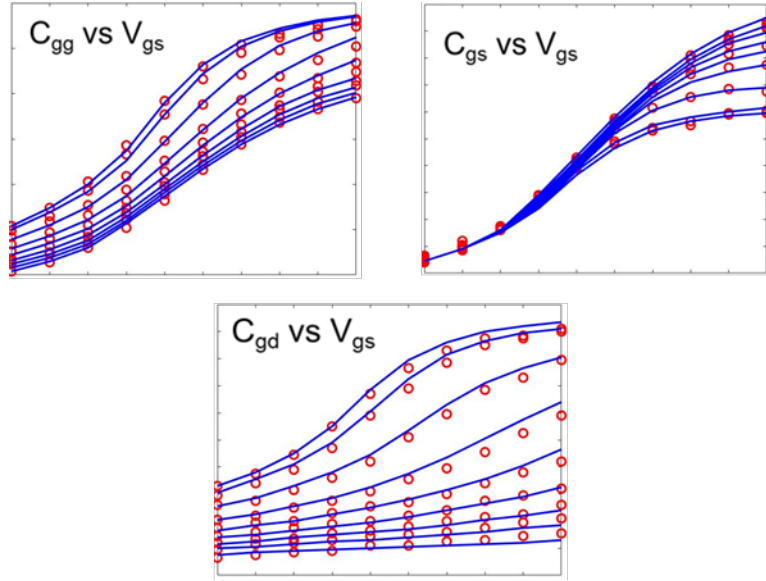


Fig. 5

#### 4. 2021enh7(UCB): Improve the accuracy of I-V near Vdsat at high Vg: S/D velocity saturation model

To capture velocity saturation effect in drain/ source regions, two bias dependent resistances,  $R_{vs,d}$  and  $R_{vs,s}$  are introduced in BSIM-CMG 111.2.0beta0\_2 with the help of two extra nodes di1 and si1. These resistances are added between di1 and di, and si1 and si, respectively. The regular (velocity independent) resistances  $R_{drain}$  and  $R_{source}$ , are now placed between d and di1, and s and si1, respectively. Nodes di1 and di are shorted when  $R_{vs,d}$  and  $R_{vs,s}$  are zero.

#### Code implementation:

$R_{drain}$  and  $R_{source}$  for RDSMOD=1

```

..// Both bias-dependent and bias-independent parts of parasitic resistances are external
..1: begin
.....Rdsi=.0.0;
.....Dr=.1.0;
.....T2=devsign.*V(gi,.si1)-.vfbsd;
.....T3=sqrt(T2.*T2+.0.1);
.....vgs_eff=.0.5.*(T2.+T3);
.....T4=.1.0+.PRWGS_i.*vgs_eff;
.....T1=.1.0./T4;
.....T0=.0.5.*(T1.+sqrt(T1.*T1+.0.01));
.....T5=RSW_i.*(1.0+.RSDR_a.*pow((V(s,.si1).*V(s,.si1)+.1.0e-6),(.0.5*.PRSDR)));
.....Rsource=.rdstemp.*(RSourceGeo+.(RSWMIN.+T5.*T0).*WeffWRFactor);
.....T2=devsign.*V(gi,.di1)-.vfbsd;
.....T3=sqrt(T2.*T2+.0.1);
.....vgd_eff=.0.5.*(T2.+T3);
.....T4=.1.0+.PRWGD_i.*vgd_eff;
.....T1=.1.0./T4;
.....T0=.0.5.*(T1.+sqrt(T1.*T1+.0.01));
.....T5=RDW_i.*(1.0+.RDDR_a.*pow((V(d,.di1).*V(d,.di1)+.1.0e-6),(.0.5*.PRDDR)));
.....Rdrain=.rdstemp.*(RDrainGeo+.(RDWMIN.+T5.*T0).*WeffWRFactor);
..end

```

```

// Velocity saturation in source/drain resistances
if (RDSMOD == 1) begin
  if (RDLCW > 0) begin
    rdstempvs = `hypssmooth((1.0 + PRTVSRSD * delTemp - 1.0e-6), 1.0e-3);
    `tempdep(VSATRSD_t, VSATRSD, -ATVSRSD)
    T0 = qis - PTWGLVSRSD;
    T0 = `smoothminx(T0, 0.1, 2.0);
    T1 = 10.0 * PSATXVSRSD * T0 / (10.0 * PSATXVSRSD + T0);
    vsatrsd_eff = VSATRSD_t * (1.0 + PTWGVSRSD * T1);
    vsatrsd_eff = `hypssmooth(vsatrsd_eff, 10.0);
    T2 = NFINTtotal * Weff0 * `q * vsatrsd_eff;
    if (GAVSRSD == 0) begin
      T3 = 1.0;
    end else begin
      T3 = `smoothminx((devsign * V(dil, di) - RDVDS), 0, 0.5);
      T3 = 1.0 + T3 * GAVSRSD;
    end
    isat_rd = T2 * NVSRSD * T3;
    delta_vsrds = pow(ids, 4 - MVSRSD) / (pow(ids, 4 - MVSRSD) + VSRDFACTOR * pow(isat_rd, 4 - MVSRSD));
    T4 = rdstempvs * RDLCW * WeffWRFactor;
    T5 = pow(delta_vsrds, 1.0 / MVSRSD) * devsign * V(dil, di) / (isat_rd * T4);
    T5 = `smoothminx(T5, 0.0, 1.0e-3);
    Rvs_d = T4 * pow((1.0 + pow(T5, MVSRSD)), 1 / MVSRSD);
  end
  if (RSLCW > 0) begin
    if (RDLCW == 0.0) begin
      rdstempvs = `hypssmooth((1.0 + PRTVSRSD * delTemp - 1.0e-6), 1.0e-3);
      `tempdep(VSATRSD_t, VSATRSD, -ATVSRSD)
      T0 = qis - PTWGLVSRSD;
      T0 = `smoothminx(T0, 0.1, 2.0);
      T1 = 10.0 * PSATXVSRSD * T0 / (10.0 * PSATXVSRSD + T0);
      vsatrsd_eff = VSATRSD_t * (1.0 + PTWGVSRSD * T1);
      vsatrsd_eff = `hypssmooth(vsatrsd_eff, 10.0);
      T2 = NFINTtotal * Weff0 * `q * vsatrsd_eff;
    end
    isat_rs = T2 * NVSRSD;
    delta_vsrds = pow(ids, 4 - MVSRSD) / (pow(ids, 4 - MVSRSD) + VSRDFACTOR * pow(isat_rs, 4 - MVSRSD));
    T4 = rdstempvs * RSLCW * WeffWRFactor;
    T5 = pow(delta_vsrds, 1.0 / MVSRSD) * devsign * V(si, sil) / (isat_rs * T4);
    T5 = `smoothminx(T5, 0.0, 1.0e-3);
    Rvs_s = T4 * pow((1.0 + pow(T5, MVSRSD)), 1 / MVSRSD);
  end
end

// External source/drain resistance
if (RDSMOD != 2 && RDRAINGeo > 0) begin
  gdpr = 1.0 / Rdrain;
  I(d, dil) <+ V(d, dil) * gdpr;
  if (RDSMOD == 1 && RDLCW > 0) begin
    gvs_d = 1.0 / Rvs_d;
    I(dil, di) <+ V(dil, di) * gvs_d;
  end else begin
    V(dil, di) <+ 0.0;
  end
end else begin
  V(d, dil) <+ 0.0;
  V(dil, di) <+ 0.0;
end

if (RDSMOD != 2 && RSourceGeo > 0) begin
  gspr = 1.0 / Rsource;
  I(s, sil) <+ V(s, sil) * gspr;
  if (RDSMOD == 1 && RSLCW > 0) begin
    gvs_s = 1.0 / Rvs_s;
    I(sil, si) <+ V(sil, si) * gvs_s;
  end else begin
    V(sil, si) <+ 0.0;
  end
end else begin
  V(s, sil) <+ 0.0;
  V(sil, si) <+ 0.0;
end

// Thermal noise for parasitics
if (RDSMOD != 2 && RDRAINGeo > 0) begin
  I(d, dil) <+ white_noise(4.0 * Vtm * `q * gdpr, "rd");
  if (RDSMOD == 1 && RDLCW > 0) begin
    I(dil, di) <+ white_noise(4.0 * Vtm * `q * gvs_d, "rd");
  end
end
if (RDSMOD != 2 && RSourceGeo > 0) begin
  I(s, sil) <+ white_noise(4.0 * Vtm * `q * gspr, "rs");
  if (RDSMOD == 1 && RSLCW > 0) begin
    I(sil, si) <+ white_noise(4.0 * Vtm * `q * gvs_s, "rs");
  end
end

// Self-heating
if (SHMOD != 0 && RTH0 > 0.0) begin
  Pwr(t) <+ (devsign * sigvds * V(di, si) * ids);
  if (RDSMOD != 2 && RDRAINGeo > 0) begin
    Pwr(t) <+ V(d, dil) * V(d, dil) * gdpr;
    if (RDSMOD == 1 && RDLCW > 0) begin
      Pwr(t) <+ V(dil, di) * V(dil, di) * gvs_d;
    end
  end
  if (RDSMOD != 2 && RSourceGeo > 0) begin
    Pwr(t) <+ V(s, sil) * V(s, sil) * gspr;
    if (RDSMOD == 1 && RSLCW > 0) begin
      Pwr(t) <+ V(sil, si) * V(sil, si) * gvs_s;
    end
  end
  Pwr(t) <+ Temp(t) * gth;
  Pwr(t) <+ ddt(Temp(t) * cth);
end else begin
  Temp(t) <+ 0.0;
end

```



```

....if (RDSMOD != 2) .begin
.....if (RDSMOD == 1 && (RDLCW > 0 || RSLCW > 0)) .begin
.....ITH = V(di, si) * ids + V(dil, di) * V(dil, di) * gvs_d + V(d, dil) * V(d, dil) * gdpr + V(sil, si) * V(sil, si) * gvs_s + V(s, sil) * V(s, sil) * gspr;
.....end .else .begin
.....ITH = V(di, si) * ids + V(d, dil) * V(d, dil) * gdpr + V(s, sil) * V(s, sil) * gspr;
.....end
.....end .else .begin
.....ITH = V(di, si) * ids;
.....end

```

## 5. 2021enh8(UCB): Parasitic substrate GIDL/GISL model

In geometries such as quadruple gate, the GIDL consists of two components (see Fig. below)

- a) D to S band to band tunneling
- b) D to E (substrate) band to band tunneling: Parasitic Substrate GIDL

Similarly, GISL consists of S to D BTBT tunneling and S to E BTBT tunneling.

BSIM-CMG 111.2.0beta0\_1 model, considers the GIDL/GISL current to be flowing from D to E/S to E for BULKMOD!=0, which underestimates the source current and overestimates the substrate current. For example, for sigvds > 0

```

..if (BULKMOD != 0) .begin
.....I(di, e) <+ devsign * (igidl + Iii);
.....I(si, e) <+ devsign * igisl;
.....I(gi, e) <+ devsign * (igbinv + igbacc);
..end .else .begin
.....I(di, si) <+ devsign * (igidl + Iii);
.....I(si, di) <+ devsign * igisl;
..end

```

In BSIM-CMG 111.2.0beta0\_2, we separate out D to S/S to D and D to E/S to E components of GIDL/GISL for the following geometries

GEOMOD = 2 (Quadruple gate)

GEOMOD = 3 (Cylindrical gate)

GIDLMOD = 2 is used to enable this feature.

### BSIM-CMG 111.2.0beta0\_2 GIDLMOD=2 model

### Drain to Source component of GIDL

$$T0 = AGIDL_i \cdot W_{eff0} \cdot \left( \frac{V_{ds} - V_{gs} - EGIDL_i + V_{fbsd}}{\epsilon_{ratio} \cdot EOT} \right)^{PGIDL_i} \\ \times \exp \left( - \frac{\epsilon_{ratio} \cdot EOT \cdot BGIDL(T)}{V_{ds} - V_{gs} - EGIDL_i + V_{fbsd}} \right) \times NFIN_{total} \\ I_{gidl} = T0 \cdot \frac{V_{de}^3}{CGIDL_i + V_{de}^3}$$

### Drain to Substrate component of GIDL

$$T0 = AGIDLB_i \cdot W_{effB} \cdot \left( \frac{V_{ds} - V_{gs} - EGIDLB_i + V_{fbsd}}{\epsilon_{ratio} \cdot EOT} \right)^{PGIDLB_i} \\ \times \exp \left( - \frac{\epsilon_{ratio} \cdot EOT \cdot BGIDLB(T)}{V_{ds} - V_{gs} - EGIDLB_i + V_{fbsd}} \right) \times NFIN_{total} \\ I_{gidlb} = T0 \cdot \frac{V_{de}^3}{CGIDLB_i + V_{de}^3}$$

where

$$W_{effB} = \begin{cases} TFIN\_BASE & \text{for } GEOMOD = 2 \\ D & \text{for } GEOMOD = 3 \end{cases}$$

### Code Implementation

```
...//Parasitic-substrate-GIDL
if (BULKMOD != 0 && (GIDLMD == 2 || GIDLMD == 3) && (GEOMOD == 2 || GEOMOD == 3)) begin
...BGIDLB_t = BGIDLB_i * `hypsmooth((1.0 + TGIDL_i * delTemp - 1.0e-6), 1.0e-3);
...if ((AGIDLB_i <= 0.0) || (BGIDLB_t <= 0.0)) begin
...T7 = 0.0;
...end else begin
...T1 = (-vgd_noswap - EGIDLB_i + vfbsd) / T0;
...T1 = `hypsmooth(T1, 1.0e-2);
...T2 = BGIDLB_t / (T1 + 1.0e-3);
...T3 = pow(T1, PGIDLB_i);
...T4 = -ved_jct * ved_jct * ved_jct;
...T4a = CGIDLB_i + abs(T4) + 1.0e-5;
...T5 = `hypsmooth((T4 / T4a), 1.0e-6) - 1.0e-6;
...T7 = AGIDLB_i * WeffB * T3 * `lexp(-T2) * T5;
...end
end

...//Parasitic-substrate-GISL
if (BULKMOD != 0 && (GIDLMD == 2 || GIDLMD == 3) && (GEOMOD == 2 || GEOMOD == 3)) begin
...BGISLB_t = BGISLB_i * `hypsmooth((1.0 + TGIDL_i * delTemp - 1.0e-6), 1.0e-3);
...if ((AGISLB_i <= 0.0) || (BGISLB_t <= 0.0)) begin
...T7 = 0.0;
...end else begin
...T1 = (-vgs_noswap - EGISLB_i + vfbsd) / T0;
...T1 = `hypsmooth(T1, 1.0e-2);
...T2 = BGISLB_t / (T1 + 1.0e-3);
...T3 = pow(T1, PGISLB_i);
...T4 = -ves_jct * ves_jct * ves_jct;
...T4a = CGISLB_i + abs(T4) + 1.0e-5;
...T5 = `hypsmooth((T4 / T4a), 1.0e-6) - 1.0e-6;
...T7 = AGISLB_i * WeffB * T3 * `lexp(-T2) * T5;
...end
end
```

## 9. 2022enh1(ADI): Add QA test to check any missing parameters

A test with all the default parameters specified is added to QA of BSIMCMG111.2.0beta3. The purpose of this test is to catch any accidentally deleted parameters during the model development. For nmos this test is

```
test.....765_ParamCheck
temperature.....27
biases.....V(s)=0.V(b)=0.V(d)=1
biasSweep.....V(g)=0.0,1.0,0.5
outputs.....I(d).I(g).I(s).I(b)
modelParameters.....parameters/nmosDefaultParameters
```

The file nmosDefaultParameters contains all the BSIMCMG parameters with their default values.

A similar test is added for the pmos.

## 10. 2022enh2(UCB): Trap-assisted tunneling (TAT) GIDL model

A new trap-assisted tunneling model has been added in BSIM-CMG 111.3.0beta0\_1 to capture the GIDL leakage in the advanced technology nodes. A new GIDL<sub>MOD</sub> = 3 can be used to enable this model. Note that GIDL<sub>MOD</sub>=3 retains all the features of GIDL<sub>MOD</sub>=2 as well. The relevant model equations are

$$\begin{aligned}
 T0 &= AGIDL_i \cdot W_{eff0} \cdot \left( \frac{V_{ds} - V_{gs} - EGIDL_i + V_{fbsd}}{\epsilon_{ratio} \cdot EOT} \right)^{PGIDL_i} \\
 &\quad \times \exp \left( -\frac{\epsilon_{ratio} \cdot EOT \cdot BGIDL(T)}{V_{ds} - V_{gs} - EGIDL_i + V_{fbsd}} \right) \times NFIN_{total} \\
 T1 &= ATATD_i \cdot W_{eff0} \cdot n_i \times NFIN_{total} \\
 &\quad \times \exp \left( \frac{BTATD_i \cdot (V_{ds} - V_{gs})^2 - CTATD(T) \cdot (V_{ds} - V_{gs}) - DTATD_i + V_{fbsd}}{V_{tm}} \right) \\
 I_{gidl} &= \begin{cases} (T0 + T1) \cdot \frac{V_{de}^3}{CGIDL_i + V_{de}^3} & \text{for } BULKMOD = 1 \\ (T0 + T1) \cdot V_{ds} & \text{for } BULKMOD = 0 \end{cases}
 \end{aligned}$$

$$\begin{aligned}
T0 &= AGISL_i \cdot W_{eff0} \cdot \left( \frac{-V_{ds} - V_{gd} - EGISL_i + V_{fbsd}}{\epsilon_{ratio} \cdot EOT} \right)^{PGISL_i} \\
&\times \exp \left( -\frac{\epsilon_{ratio} \cdot EOT \cdot BGISL(T)}{-V_{ds} - V_{gd} - EGISL_i + V_{fbsd}} \right) \times NFIN_{total} \\
T1 &= ATATS_i \cdot W_{eff0} \cdot n_i \times NFIN_{total} \\
&\times \exp \left( \frac{BTATS_i \cdot (-V_{ds} - V_{gd})^2 - CTATS(T) \cdot (-V_{ds} - V_{gd}) - DTATS_i + V_{fbsd}}{V_{tm}} \right) \\
I_{gisl} &= \begin{cases} (T0 + T1) \cdot \frac{V_{gs}^3}{CGISL_i + V_{gs}^3} & \text{for } BULKMOD = 1 \\ (T0 + T1) \cdot V_{sd} & \text{for } BULKMOD = 0 \end{cases}
\end{aligned}$$

## Code Changes:

```

...//GIDLcurrent
if ((AGIDL_i <= 0.0) || (BGIDL_t <= 0.0)) begin
...T6 = 0.0;
end else begin
...T1 = (-vgd_noswap - EGIDL_i + vfbds) / T0;
...T1 = hypsmooth(T1, 1.0e-2);
...T2 = BGIDL_t / (T1 + 1.0e-3);
...T3 = pow(T1, PGIDL_i);
...if (BULKMOD != 0) begin
...T4 = -ved_jct * ved_jct * ved_jct;
...T4a = CGIDL_i + abs(T4) + 1.0e-5;
...T5 = hypsmooth((T4 / T4a), 1.0e-6) - 1.0e-6;
...T6 = AGIDL_i * Weff0 * T3 * lexp(-T2) * T5;
end else begin
...T6 = AGIDL_i * Weff0 * T3 * lexp(-T2) * vds_noswap;
end
end
...//Trap Assisted Tunneling GIDL
if (GIDLMOD == 3 && ATATD_i > 0.0) begin
...if (BULKMOD != 0) begin
...CTATD_t = CTATD_i * hypsmooth((1.0 + TTAT_i * delTemp - 1.0e-6), 1.0e-3);
...T1 = (BTATD_i * vgd_noswap * vgd_noswap - CTATD_t * vgd_noswap - DTATD_i + vfbds) / Vtm;
...T2 = ATATD_i * Weff0 * ni * lexp(T1);
...T4 = -ved_jct * ved_jct * ved_jct;
...T4a = CGIDL_i + abs(T4) + 1.0e-5;
...T5 = hypsmooth((T4 / T4a), 1.0e-6) - 1.0e-6;
...T6 = T6 + T2 * T5;
end else begin
...CTATD_t = CTATD_i * hypsmooth((1.0 + TTAT_i * delTemp - 1.0e-6), 1.0e-3);
...T1 = (BTATD_i * vgd_noswap * vgd_noswap - CTATD_t * vgd_noswap - DTATD_i + vfbds) / Vtm;
...T2 = ATATD_i * Weff0 * ni * lexp(T1);
...T6 = T6 + T2 * vds_noswap;
end
end
...//GISLcurrent
if ((AGISL_i <= 0.0) || (BGISL_t <= 0.0)) begin
...T6 = 0.0;
end else begin
...T1 = (-vgs_noswap - EGISL_i + vfbds) / T0;
...T1 = hypsmooth(T1, 1.0e-2);
...T2 = BGISL_t / (T1 + 1.0e-3);
...T3 = pow(T1, PGISL_i);
...if (BULKMOD != 0) begin
...T4 = -ves_jct * ves_jct * ves_jct;
...T4a = CGISL_i + abs(T4) + 1.0e-5;
...T5 = hypsmooth((T4 / T4a), 1.0e-6) - 1.0e-6;
...T6 = AGISL_i * Weff0 * T3 * lexp(-T2) * T5;
end else begin
...T6 = AGISL_i * Weff0 * T3 * lexp(-T2) * (-vds_noswap);
end
end
...//Trap Assisted Tunneling GISL
if (GIDLMOD == 3 && ATATS_i > 0.0) begin
...if (BULKMOD != 0) begin
...CTATS_t = CTATS_i * hypsmooth((1.0 + TTAT_i * delTemp - 1.0e-6), 1.0e-3);
...T1 = (BTATS_i * vgs_noswap * vgs_noswap - CTATS_t * vgs_noswap - DTATS_i + vfbds) / Vtm;
...T2 = ATATS_i * Weff0 * ni * lexp(T1);
...T4 = -ves_jct * ves_jct * ves_jct;
...T4a = CGISL_i + abs(T4) + 1.0e-5;
...T5 = hypsmooth((T4 / T4a), 1.0e-6) - 1.0e-6;
...T6 = T6 + T2 * T5;
...itat = T2 * T5;
end else begin
...CTATS_t = CTATS_i * hypsmooth((1.0 + TTAT_i * delTemp - 1.0e-6), 1.0e-3);
...T1 = (BTATS_i * vgs_noswap * vgs_noswap - CTATS_t * vgs_noswap - DTATS_i + vfbds) / Vtm;
...T2 = ATATS_i * Weff0 * ni * lexp(T1);
...T6 = T6 + T2 * (-vds_noswap);
end
end
end

```

### 11. 2022enh3(UCB): Add cryogenic model parameter extraction procedure in manual.

Parameter extraction procedure for a multiple temperature fitting using the cryogenic model (CRYOMOD=1 or 2) has been added as section 6 in the BSIM-CMG 111 .3.0beta0\_1 manual.

### 12. 2023enh1(IBM): Improve cryogenic model parameter extraction procedure in the manual.

The cryogenic model extraction procedure has been updated in the manual of **BSIM-CMG 112.0.0beta0\_2** in a tabular form to make it easy to follow. Notes are also provided below each table for more details. For example:

#### 6.1 Drain Current Fitting in Linear Region

**Step 2.** Subthreshold region fitting: In this step, the  $V_{GS}$  dependence of the drain current  $I_{DS}$  in low  $V_{GS}$  region is extracted.

Extracted Parameters	Device & Experimental Data	Extraction Methodology
TLOW and DTLOW	$I_{ds}$ v.s. $V_{gs}$ @ $V_{ds} = 50mV$ @ multiple temperatures.	Observe Subthreshold swing (SS) @ different temperatures and tune TLOW and DTLOW to capture SS saturation.
TLOW1, KLOW1, DTLOW1	$I_{ds}$ v.s. $V_{gs}$ @ $V_{ds} = 50mV$ @ multiple temperatures.	Observe sub-threshold swing (SS) @ different temperatures in cryogenic range for a rise in SS with T reduction. Tune TLOW1, KLOW1, DTLOW1 to capture the SS rise if any.
TVTH, KT11, KT12, KT1	$I_{ds}$ v.s. $V_{gs}$ @ $V_{ds} = 50mV$ @ multiple temperatures.	Observe threshold voltage offset @ different temperatures and tune TVTH, KT11, KT12, KT1.

Notes:

- TLOW is used to extract the temperature at which SS saturates w.r.t temperature in the cryogenic range. DTLOW is used to smoothly transition to the SS saturation region @ low T from the usual SS behavior governed by the Boltzmann law  $(\ln(10)kT/q)$  @ high T. At very low temperatures, the SS may again start to rise with T and TLOW1 is the temperature below which this happens. DTLOW1 is used to capture the smoothness of this SS transition and KLOW1 is used to capture the rate at which the SS rises w.r.t T (assuming linear dependency on T).

### 13. 2023enh1: Reinstate the GAA functionality.

We have reinstated the GAA functionality i.e. GEOMOD=5 (GAAFET geometry and related effects selector) and SUBBANDMOD (GAA quantum subband model

selector) in the BSIM-CMG\_112.0.0beta0\_3 release. The technical manual has also been updated accordingly.

#### **14. 2024enh2(UCB): Thin Film Transistor Model.**

We have introduced compact models for capturing the device characteristics of Thin Film Transistors. The models can be enabled with  $TFTMOD = 1$ .

The full description of the models and an extraction procedure of the related parameters is available in the technical manual. Here is the summary of the models we introduced:

- Core model of charge density including the impact of trap charges
- Channel current model including trap limited conduction and percolation transport
- Source/Drain parasitic Schottky contacts in all RDSMODs
- Terminal charges  $qg$ ,  $qd$  and  $qs$
- Temperature dependence of traps

Other than the above models, the models for mobility, velocity saturation, non-saturation effect, lateral non-uniform doping effect, body effect, CLM and DIBL effects, Quantum mechanical effects, gat tunneling current, NQS model, and bias dependency of parasitic Source/Drain resistances are also modified for  $TFTMOD = 1$ .

#### **15. 2024enh3(ADI, UCB): Add QA tests for all parameters.**

Added QA tests 885 -1038 for  $TFTMOD=1$  and addressing the following issues:

- No test for parameter  $NGCON = 2$
- No test of values  $[0, 2, 3, 4, 5, 6]$  for parameter  $NGAA$
- No test for parameter  $MOBSCMOD = 1$
- No test for parameter  $TYPE = 0$
- No test for parameter  $BULKMOD = 2$

- No test of values [1, 2, 3, 4] for parameter GEOMOD
- No test for parameter CGEO1SW = 1
- No test for parameter RDSMOD = 1
- No test for parameter ASYMMOD = 1
- No test for parameter CVMOD = 1
- No test of values [2, 3] for parameter GIDLMOD
- No test of values [1, 2] for parameter IIMOD
- No test for parameter TNOIMOD = 1
- No test of values [1, 2] for parameter NQSMOD
- No test for parameter TEMPMOD = 1
- No test for parameter RGATEMOD = 1
- No test for parameter RGEOMOD = 1
- No test of values [1, 2, 3] for parameter CGEOMOD
- No test for parameter FNMOD = 1
- No test for parameter SH\_WARN = 1
- No test for parameter IGCLAMP = 0
- No test for parameter SDTERM = 1

#### 16. 2024enh4(Rapidus): Improved gds fitting in low gate overdrive.

Short channel devices tend to have the output conductance (gds) less sensitive to the drain voltage under low gate overdrive. This behavior is captured using an updated  $\Delta V_{th,DIBL}$  defined using a new parameter ETA1 as:

$$\Delta V_{th,DIBL} = \Theta_{DIBL} ETA0_i \cdot (V_{dsx} + ETA1 \sqrt{V_{dsx} + 0.01}) + DVTP0 \cdot \Theta_{DITS} \cdot (V_{dsx} + 0.01)^{DVTP1}$$

This expression follows a similar treatment as 2017enh6 for BSIM-IMG 102.9.1.

#### 17. 2024enh5(ADI,UCB): Change parameter case according to VA standard.

Changed the parameters in the code to lowercase to follow the latest Verilog-A standards. All variables with conflicting names were suffixed with `_v`. The parameter D, when converted to lowercase, conflicts with the drain node d. This

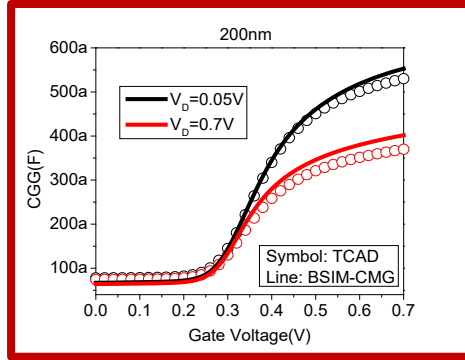
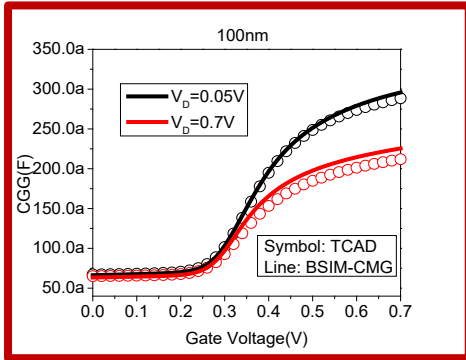
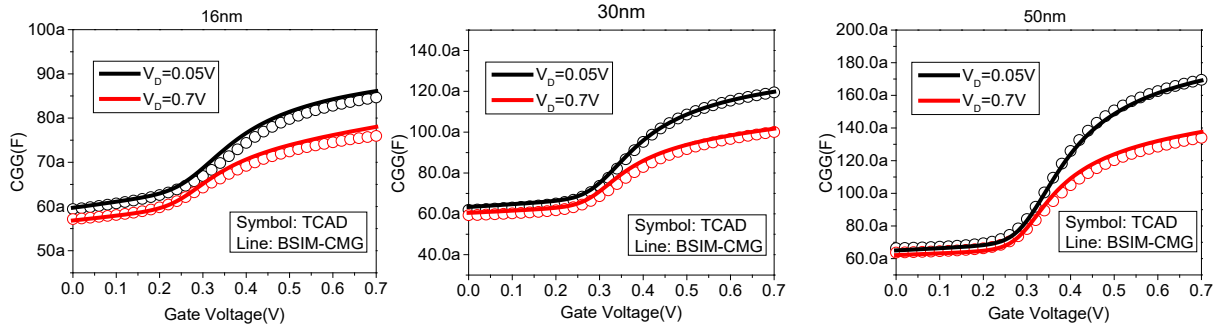
parameter was renamed to **dia**.

## 18. 2024enh6(UCB): Flexibility for capacitance tuning in the saturation region.

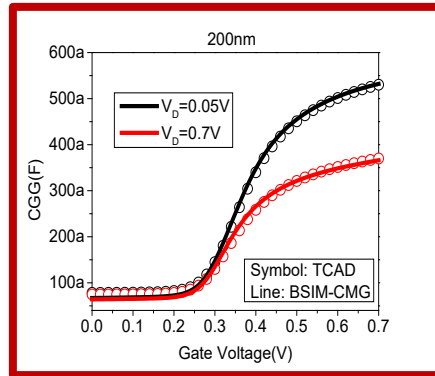
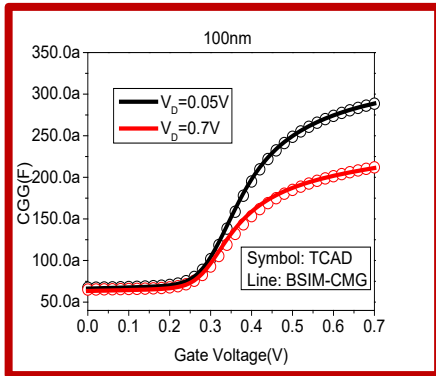
ASAT (CV fitting parameter for high  $V_D$ ) and its corresponding binning parameters have been added. The updated expression for gate charge now reads:

$$qg = qia + dqi * \frac{dqi}{6(2qia + nVtm)} * ASAT * DvsatCV$$

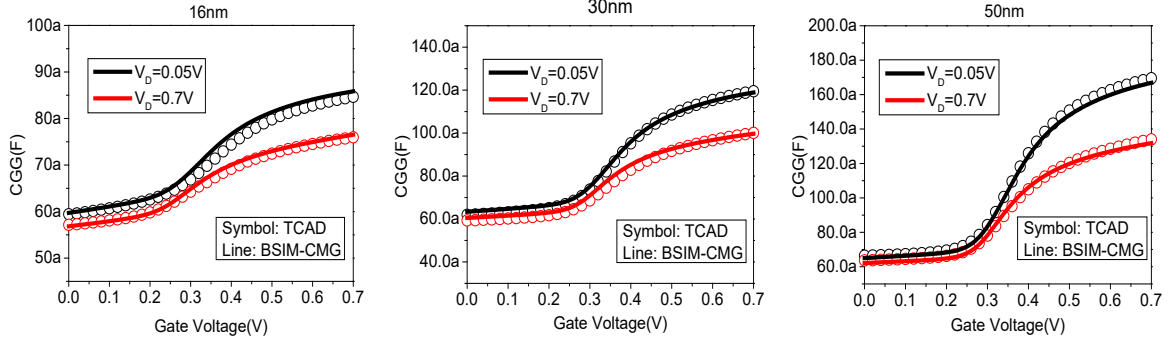
Before ASAT:



After ASAT:







Further, binning has been introduced for the parameter PQM, with an additional length scaling parameter PQML for fitting flexibility.

**19. 2024enh7(ADI): Removing NF from parameters/nmosDefaultParameters and parameters/pmosDefaultParameters in the QA package, and redefining the parameter check with NF as an instance parameter.**

NF is now defined as an instance parameter for the default parameter check in QA.

The updated qaSpec now reads:

```
test          1038_ParamCheck
temperature   27
biases        V(s)=0 V(e)=0 V(d)=1
biasSweep     V(g)=0.0,1.0,0.5
outputs       I(d) I(g) I(s) I(e)
instanceParameters NF=1
modelParameters parameters/nmosDefaultParameters
```

NF has been removed from the files parameters/nmosDefaultParameters and parameters/pmosDefaultParameters.

**20. 2024enh8(IBM): Improved Self-Heating model for GAAFETs.**

An improved self-heating model is implemented to include the impact of WGAA and NGAA on self-heating in GAAFETs. The model activates only when GEOMOD=5, and defines the thermal resistance and capacitance as:

$$\frac{1}{R_{th}} = G_{th} = \frac{\left( WTH0 \cdot NF^{BSHEXP} + FPITCH \cdot NFINTotal^{ASHEXP} + \frac{WGAA}{WGAANOM} \cdot NGAA^{CSHEXP} \right)}{RTH0}$$

$$C_{th} = CTH0 \cdot \left( WTH0 \cdot NF^{BSHEXP} + FPITCH \cdot NFINTotal^{ASHEXP} + \frac{WGAA}{WGAANOM} \cdot NGAA^{CSHEXP} \right)$$

**21. 2024enh9(Intel): Additional parameters to model mobility degradation due to hot carriers.**

In the source and drain regions, there is a chance for a concentration of hot-carrier defects which can be impacted by hot carriers and lead to interface states to appear at the Si surface. This can lead to a shift in the threshold voltage and a degradation in the mobility because of scattering. The mobility degradation is modeled with two model parameters **MUHC0** and **MUHC1** through the following equation:

$$u0mult\_v = U0MULT \cdot \left(1 - MUHC0 \cdot \exp(-MUHC1 \cdot V_{dseff})\right)$$

- Before stress: MUHC0/MUHC1=0 (default)
- After stress: MUHC0 is [0, 1) to model mobility degradation  
After stress: MUHC1 is [0, 3) to model the Vds dependence of mobility degradation.

## 22. 2024enh10(IBM): Improved Self-Heating model for GAAFETs

Linear scaling terms ASH and CSH have been introduced to improve flexibility.

When GEOMOD=5, thermal resistance ( $R_{th}$ ) and capacitance ( $C_{th}$ ) are defined as:

$$\begin{aligned} \frac{1}{R_{th}} = G_{th} &= \frac{(WTH0 \cdot NF^{BSHEXP} + ASH \cdot FPITCH \cdot NF_{INtotal}^{ASHEXP})}{RTH0} \\ &+ \frac{(CSH \cdot WGAA \cdot NF \cdot NGAA^{CSHEXP})}{RTH0} \\ C_{th} &= CTH0 \cdot (WTH0 \cdot NF^{BSHEXP} + ASH \cdot FPITCH \cdot NF_{INtotal}^{ASHEXP} \\ &+ CSH \cdot WGAA \cdot NF \cdot NGAA^{CSHEXP}) \end{aligned}$$

Otherwise:

$$\begin{aligned} \frac{1}{R_{th}} = G_{th} &= \frac{(WTH0 \cdot NF^{BSHEXP} + ASH \cdot FPITCH \cdot NF_{INtotal}^{ASHEXP})}{RTH0} \\ C_{th} &= CTH0 \cdot (WTH0 \cdot NF^{BSHEXP} + ASH \cdot FPITCH \cdot NF_{INtotal}^{ASHEXP}) \end{aligned}$$

## 23. 2024enh12(CMC Policy): Removed TFT feature from 112.0.0beta3

Following CMC recommendations, the TFT feature was removed from BSIM-CMG 112.0.0beta3.

**24. 2024enh13(ADI, QA subcommittee): Extended QA to evaluate non-default parameter values.**

The following tests were added to the QA, including 3 modelcards with randomly assigned non-default parameters. The tests include:

918\_ParamCheck\_DC\_NDefault  
919\_ParamCheck\_AC\_NDefault  
920\_ParamCheck\_AC\_Freq\_NDefault  
921\_ParamCheck\_Noise\_NDefault  
922\_ParamCheck\_DC\_AllMods\_NDefault  
923\_ParamCheck\_AC\_AllMods\_NDefault  
924\_ParamCheck\_AC\_Freq\_AllMods\_NDefault  
925\_ParamCheck\_Noise\_AllMods\_NDefault  
926\_ParamCheck\_DC\_AllMods\_NDefault  
927\_ParamCheck\_AC\_AllMods\_NDefault  
928\_ParamCheck\_AC\_Freq\_AllMods\_NDefault  
929\_ParamCheck\_Noise\_AllMods\_NDefault  
930\_ParamCheck\_DC\_AllMods\_NDefault  
931\_ParamCheck\_AC\_AllMods\_NDefault  
932\_ParamCheck\_AC\_Freq\_AllMods\_NDefault  
933\_ParamCheck\_Noise\_AllMods\_NDefault  
934\_ParamCheck\_DC\_AllMods\_NDefault  
935\_ParamCheck\_AC\_AllMods\_NDefault  
936\_ParamCheck\_AC\_Freq\_AllMods\_NDefault  
937\_ParamCheck\_Noise\_AllMods\_NDefault  
938\_ParamCheck\_DC\_AllMods\_NDefault  
939\_ParamCheck\_AC\_AllMods\_NDefault  
940\_ParamCheck\_AC\_Freq\_AllMods\_NDefault  
941\_ParamCheck\_Noise\_AllMods\_NDefault