ESE GATE PSUs State Engg. Exams

WORKDOOK 2025



Detailed Explanations of Try Yourself Questions

Electronics Engineering
Network Theory



Basics



Detailed Explanation of Try Yourself Questions

T1. (b)

Writing node equation at the top center node

$$\frac{V_1 - 0}{2 + 3} + \frac{(V_1 - 1)}{1} + \frac{V_1 - \alpha V_x}{5} = 0$$

$$V_1 \cdot V_1 - 1 \cdot V_1 - \alpha V_x$$

$$\frac{V_1}{5} + \frac{V_1 - 1}{1} + \frac{V_1 - \alpha V_x}{5} = 0$$
 ...(i)

Since

$$V_x = \left(\frac{2}{2+3}\right)V_1 = \frac{2}{5}V_1$$
 (Voltage Division)

Now, by substituting

$$V_1 = (5/2) V_x$$
 into equation (1), we get

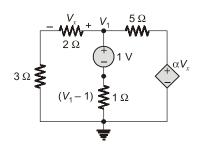
$$\frac{1}{5} \left(\frac{5}{2} V_x \right) + \left(\frac{5}{2} V_x - 1 \right) + \frac{1}{5} \left(\frac{5}{2} V_x - V_x \right) = 0$$

$$\frac{V_x}{2} + \frac{5}{2}V_x + \frac{V_x}{2} = 1$$

$$\frac{7}{2}V_x - \alpha + \frac{V_x}{5} = 1$$

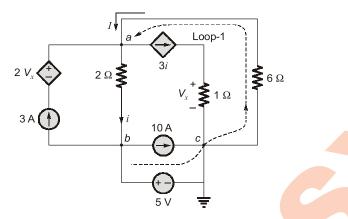
$$35 V_x - 2 \alpha V_x = 10$$

$$V_x = \frac{10}{(35 - 2\alpha)}$$





T2. Sol.



Taking node 'C' as reference,

KCL at node 'a':

$$I + 3 = 3i + i$$

 $I = 4i - 3$...(i)

KVL in loop-1

$$2i + 5 + 6I = 0$$

 $6I = -2i - 5$...(ii)

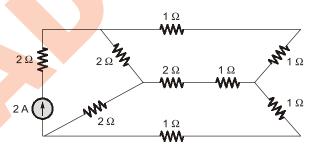
Solving equation (i) and (ii), we get

$$I = -1 \text{ A}, \quad i = \frac{1}{2} \text{ A}$$

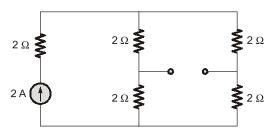
 $i = 0.5 \text{ A}$

T3. Sol.

Transform Δ to Y the circuit can be reduced as below,



From balanced bridge
Network can be reduced to



Total resistance across current source,

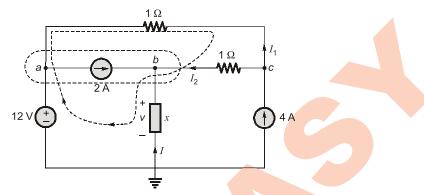


...(i)

$$R_{eq} = 2 + \frac{4 \times 4}{4 + 4} = 4 \Omega$$

Power delivered by current source, $P = I^2 R_{eq} = 2^2 \times 4 = 16 \text{ W}$

T4. (b)



$$V = AI + B$$

At node C;

$$4 = I_1 + I_2$$
 ...(ii)

KVL in loop-1,

$$-12 - I_1 + I_2 + V = 0$$

 $V - I_1 + I_2 = 12$...(iii)

KCL at node (b),

$$2 + I + I_2 = 0$$
 ...(iv)

From equation (ii) and (iii),

$$I_1 = 4 - I_2$$

and

$$I_{1} = 4 - I_{2}$$

$$V + I_{2} - 4 + I_{2} = 12$$

$$2I_{2} = 12 - V + 4$$
...(v)

From equation (iv) and (v),

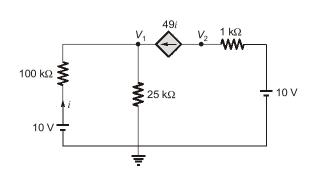
$$2+I+6-\frac{V}{2}+2 = 0$$

$$10+I-\frac{V}{2} = 0$$

$$V = 2I+20$$

$$A = 2, B = 20$$

T5. (c)





KCL at node V_1 ,

$$i + 49i = \frac{V_1}{25}$$

$$50i = \frac{V_1}{25}$$
...(i)

$$i = \frac{10 - V_1}{100K}$$
 ...(ii)

From equation (i) and (ii),

$$50 \times \frac{10 - V_1}{100 \text{K}} = \frac{V_1}{25}$$

$$\Rightarrow \frac{1}{2K}(10-V_1) = \frac{V_1}{25}$$

$$\Rightarrow 10 - V_1 = \frac{(2K) \cdot V_1}{25}$$

$$10 = 81 V_1$$

$$\Rightarrow V_1 = \frac{10}{81} \text{ volts}$$

and
$$i = \frac{10 - \frac{10}{81}}{(100 \text{ K})}$$

$$V_2 = 10 - 1 \text{K} \times \frac{\left(10 - \frac{10}{81}\right)}{100 \text{ K}} \times 49$$

= 5.16 volts

T6. (a)

Transform current source to voltage source,

Applying KCL, at node V_1 ,

$$\frac{V_1 + 8}{8} + \frac{V_1 - 14}{8} + \frac{V_1 - 1}{4} = 0$$

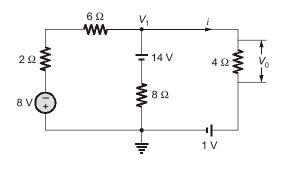
$$V_1 = 2 V$$

$$i = \frac{V_1 - 1}{4} = \frac{1}{4} A$$

Current,

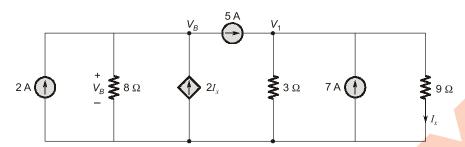
then,

$$V_0 = \frac{1}{4} \times 4 = 1 \text{ V}$$





T7. (a)



By KCL at node 1,

$$\frac{V_1}{3} + \frac{V_1}{9} = 5 + 7$$

$$V_1 = 27 \text{ V}$$

$$I_x = \frac{V_1}{9} = \frac{27}{9} = 3 \text{ A}$$

By KCL at node B,

$$2 + 2I_x = \frac{V_B}{8} + 5$$

$$2 + 2(3) = \frac{V_B}{8} + 5$$

 $V_B = 24 \text{ V}$



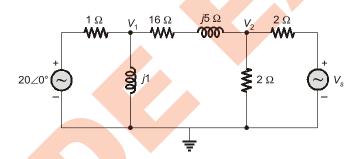


Steady State AC Analysis



Detailed Explanation of Try Yourself Questions

T1. Sol.



From given data current in 16 Ω is equal to zero, hence

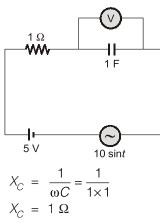
$$V_{1} = V_{2}$$

$$V_{1} = 20 \angle 0 \times \frac{j1}{1+j1} = 20 \frac{1 \angle 90}{\sqrt{2} \angle 45} = \frac{20}{\sqrt{2}} \angle 45^{\circ}$$

$$V_{1} = V_{2} = \frac{20}{\sqrt{2}} \angle 45^{\circ}$$

$$V_{S} = 2 V_{2} = 2 \frac{20}{\sqrt{2}} \angle 45^{\circ} = 20\sqrt{2} \angle 45^{\circ} V$$

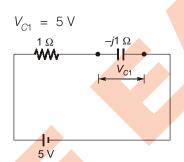
T2. (b)



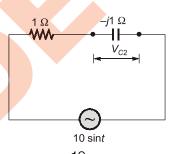
•:

using superposition principle,

(i) For 5 V source In steady-state,



(ii) For 10 sint source:



$$V_{C2} = \frac{10}{\sqrt{2} \times \sqrt{2}} \times 1 = 5 \text{ V}$$

 $V_C = \sqrt{V_{C1}^2 + V_{C2}^2} = \sqrt{5^2 + (5)^2} = \sqrt{50} = 7.07 \text{ V}$

T3. (c)

Now,

$$I = 4.24 \sin(500t + 45^{\circ})$$

$$P = 180 \text{ W}, \quad \text{p.f.} = 0.8 \text{ lag}$$

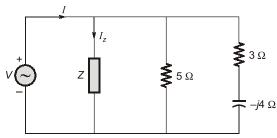
Power dissipated in resistor = $P = I_{Or}^2 \times R$ •:•

$$180 = \left(\frac{4.24}{\sqrt{2}}\right)^2 \times R$$

$$R = 20.02 \simeq 20 \Omega$$







$$V = 50 \angle 30^{\circ}$$

$$I = 27.9 \angle 57.8^{\circ}$$

$$Z_{eq} = \frac{V}{I} = \frac{50\angle 30^{\circ}}{27.9\angle 57.8^{\circ}} = 1.8\angle -27.8 \Omega$$

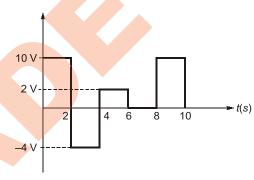
= 1.8\angle -27.8\circ \Omega

$$\frac{1}{Z_{eq}} = \frac{1}{Z} + \frac{1}{5} + \frac{1}{3 - j4}$$

$$\frac{1}{1.8\angle 27.8} = \frac{1}{Z} + \frac{1}{5} + \frac{3+j4}{25}$$

$$\frac{1}{Z} = \frac{1}{1.8\angle -27.8} - \frac{1}{5} - \frac{3+j4}{25}$$
$$Z = 5\angle -30^{\circ} \Omega$$

T5. Sol.



Rms value
$$= \left[\frac{1}{T} \int_{0}^{T} f^{2}(t) d(t) \right]^{1/2} = \left[\frac{1}{10} \int_{0}^{10} f^{2}(t) \cdot d(t) \right]^{1/2}$$

$$= \left[\frac{1}{10} \left\{ \int_{0}^{2} 100 dt + \int_{2}^{4} 16 dt + \int_{4}^{6} 4 dt + \int_{6}^{8} 0 + \int_{8}^{10} 100 dt \right\} \right]^{1/2}$$

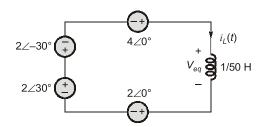
$$= \left[\frac{1}{10} \left\{ 100 \times 2 + 16 \times 2 + 4 \times 2 + 100 \times 2 \right\} \right]^{1/2}$$

$$= \left[\frac{1}{10} (440) \right]^{1/2} = \sqrt{44} = 6.633 \text{ unit}$$



T6. (c)

Given redundant network can be reduced as,



$$X_L = \omega L = 100 \left(\frac{1}{50}\right) = 2$$

$$i_{L}(t) = \frac{V_{eq}}{jX_{L}}$$

$$i_{L}(t) = \frac{2+j2}{j2} = \sqrt{2} \angle -45$$

$$i_{l}(t) = 1.414 \cos(100t - 45^{\circ}) A$$

T7. (a)

Current,

$$i(t) = C \frac{dv(t)}{dt}$$

For

$$0 < t < 0.5 \text{ s}, v(t) = 30t^2 \text{ V}$$

$$i(t) = 20 \times 10^{-6} (60t) = 1.2 t \text{ mA}$$

For
$$0.5 \text{ s} < t < 1 \text{ s}, \ v(t) = 30 (t-1)^2$$

$$i(t) = (20 \times 10^{-6}) [60 (t-1)] = 1.2(t-1) \text{ mA}$$



Transient Response

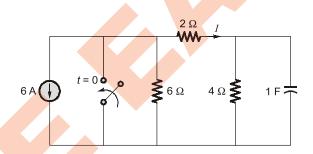


Detailed Explanation

Try Yourself Questions

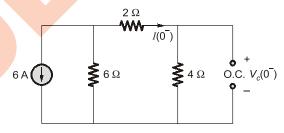
T1. (c)

For the given circuit,



For t < 0; at

Steady-state:

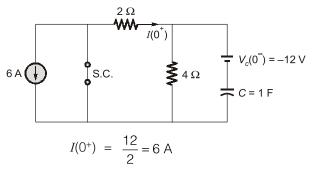


$$I(0^{-}) = -\frac{6}{12} \times 6 = -3 \text{ A}$$

and

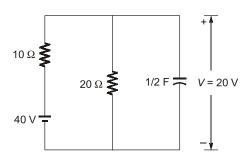
$$V_{\rm C}(0^{-}) = -12 \text{ V}$$

after closing switch at $t = 0^+$, the circuit reduced as:

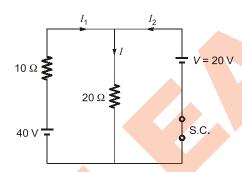




T2. (c)



Suppose at time t = 0, the voltage 'V' = 20 VThe circuit can be reduced as



at $t = 0^+$;

$$I = \frac{20}{20} = 1 \text{ A}$$

and

$$I_1 = \frac{40 - 20}{10} = 2 \text{ A}$$

$$I_2 = -1 \text{ A}$$

Current flowing across capacitor at $t = 0^+$;

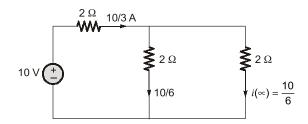
$$\left. \frac{dV}{dt} \right|_{t=0^+} = -I_2 \text{ or } \left| \frac{dV}{dt} \right|_{\text{at } t=0^+} = 2 \text{ V/s}$$

T3. Sol.

From given data,

$$i(0^+) = \frac{\Psi(0^+)}{L} = \frac{10}{1} = 10 \text{ A}$$

at $t = \infty$;



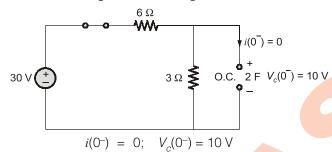


$$i(t) = [i(0^{+}) - i(\infty)] e^{-Rt/L} + i(\infty)$$

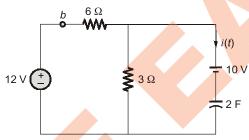
$$i(t) = \left[10 - \frac{10}{6}\right] e^{-\frac{3t}{1}} + \frac{10}{6} = [1.67 + (8.333) e^{-3t}] A.$$

T4. (c)

At at t < 0; the circuit is behaving as shown in figure,



At t > 0; now here we can find,



$$i(\infty) = 0$$

and

$$V_c(\infty) = 4 \text{ V}$$

Here,

$$V_c(t) = V_c(\infty) + [V(0^+) - V(\infty)] e^{-t/\tau}$$

 $\tau = R_{eq} \cdot C = (6 \mid |3) \times 2$
 $= 2 \times 2 = 4 \text{ sec}$

$$= 2 \times 2 = 4 \text{ sec}$$

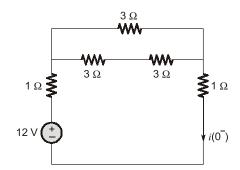
$$V_c(t) = 4 + [10 - 4] e^{-t/4} = 4 + 6e^{-t/4}$$

$$i_c(t) = -C \frac{dV}{dt} = -C \times \left[\frac{d[4 + 6e^{-t/4}]}{dt} \right]$$

= $-2 \times \frac{6}{4} \cdot e^{-t/4} = -3e^{-t/4} \text{ A}$

T5. (b)

At $t = 0^-$



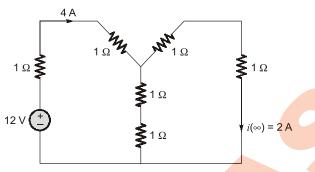


$$i(0^{-}) = \frac{12}{R_{eq}} = \frac{12}{4} = 3 \text{ A}$$

$$i(0^+) = i(0^-) = 3 A$$

At $t = \infty$;

Transform Δ to Y;



$$i(\infty) = 2 A$$

$$i(t) = [(i(0^+) - i(\infty)]e^{-\frac{Rt}{L}} + i(\infty)$$

$$i(t) = (3-2)e^{-3t} + 2$$

$$i(t) = (2 + e^{-3t})A$$

T6. Sol.

$$F(s) = \frac{4e^{-2s(s+2)}}{s}$$

Initial value = $\underset{s \to \infty}{\text{Lim }} s \cdot F(s)$

$$f(0) = \lim_{s \to \infty} \frac{s \times 4e^{-2s}(s+2)}{s} = \lim_{s \to \infty} 4e^{-2s}(s+2)$$

$$= \lim_{s \to \infty} \frac{4(s+2)}{\left[1 + 2s + \frac{(2s)^2}{2!} + \frac{(2s)^3}{3!} + \dots\right]}$$

$$= \lim_{s \to \infty} \frac{4s\left[1 + \frac{2}{s}\right]}{s\left[\frac{1}{s} + 2 + \frac{2^2s}{2!} + \frac{2^3s^2}{3!} + \dots\right]}$$

$$= \frac{4[1+0]}{[0+2+\infty+\infty+\dots\infty]} = \frac{4}{\infty} = 0$$

$$f(\infty) = \lim_{s \to 0} s \cdot F(s) = \lim_{s \to 0} \frac{s \times 4e^{-2s} \cdot (s+2)}{s}$$

Final value,

$$f(\infty) = \lim_{s \to 0} s \cdot F(s) = \lim_{s \to 0} \frac{s \times 4e^{-2s} \cdot (s+2)}{s}$$
$$= 4e^{-2 \times 0} (0+2) = 8e^{-0} = 8(1)$$
$$= 8$$





The series connected capacitors can be replaced with an equivalent capacitor as shown

$$v_o(0) = 20 \text{ V}$$

$$C_{eq} = \frac{(30)(45)}{30 + 45} = 18\mu F$$

$$v_o(t) = v_o(0) + \frac{1}{20} \int_0^t i(t)dt$$

 $V_{o}(t) = V_{o}(0) + \frac{1}{C_{eq}} \int_{0}^{t} i(t)dt$

-ve sign is taken because current flows from -ve to +ve polarity.

$$v_{o}(t) = 20 - \frac{1}{C_{eq}} \int_{0}^{t} i(t)dt$$

$$= 20 - \frac{1}{18 \times 10^{-6}} \int_{0}^{t} i(900 \times 10^{-6}) e^{-2.5t} dt$$

$$= 20 - \frac{900 \times 10^{-6}}{18 \times 10^{-6}} \left[\frac{e^{-2.5t}}{-2.5} \right]_{0}^{t}$$

$$= 20 + 20 \left[e^{-2.5t} - 1 \right] = 20 e^{-2.5t} \text{ V}$$



Graph Theory

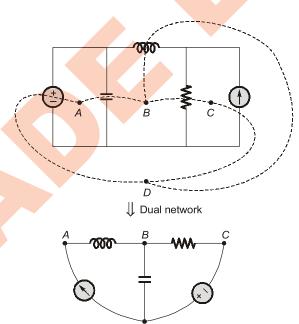


Detailed Explanation of Try Yourself Questions

T1. (c)

T2. (d)

Dual of the given network is

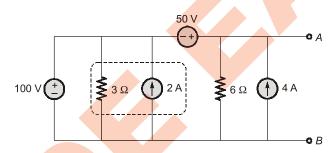


Network Theorems



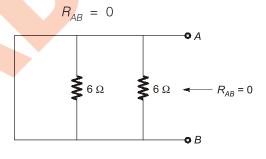
Detailed Explanation of Try Yourself Questions

T1. (d)



 $V_{AB} = 50 + 100 = 150 \text{ V}$

For R_{AB} ;



then here,

$$I_N \ = \ \frac{V_{AB}}{R_{AB}} = \infty$$

Therefore, norton's equivalent circuit between terminals A and B does not exist.

T2. (a)

$$Z_S = \frac{R(j\omega L)}{R + j\omega L}$$



To seperate peal and imaginary,

$$Z_{S} = \frac{R(j\omega L)}{R + j\omega L} \times \frac{R - j\omega L}{R - j\omega L} = \frac{R\omega^{2}L^{2}}{R^{2} + \omega^{2}L^{2}} + j\frac{R^{2}\omega L}{R^{2} + \omega^{2}L^{2}}$$

From maximum power theorems,

$$Z_{L} = Z_{S}^{*}$$

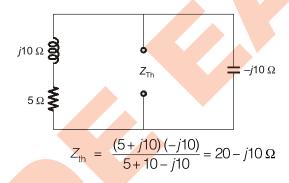
$$R_{1} - j \frac{1}{\omega C} = \frac{R \omega^{2} L^{2}}{R^{2} + \omega^{2} L^{2}} - j \frac{R^{2} \omega L}{R^{2} + \omega^{2} L^{2}}$$

Compare real and imaginary part on both sides

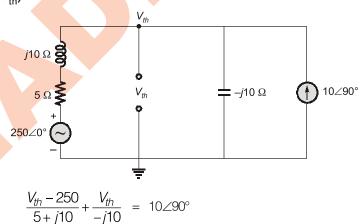
$$R_1 = \frac{R\omega^2 L^2}{R^2 + \omega^2 L^2}$$
$$C = \frac{R^2 + \omega^2 L^2}{R^2 \omega^2 L}$$

T3. Sol.

Case-1: To find (Z_{th})



Case-2: To find (V_{th})

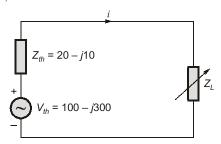


$$5+j10 - j10$$

 $V_{th} = (100 - j300) V$



From maximum power theorem,



$$Z_L = Z_{th}^*$$

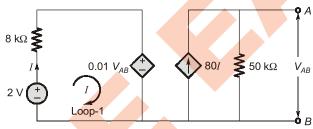
 $Z_I = 20 + j10$

$$i = \frac{\sqrt{100^2 + 300^2}}{40}$$

$$P_L = i^2 R_L = i^2 \times 20 = 1250 \text{ W}$$

Current,

T4. (c)



$$V_{AB} = V_{Th} = 50 \text{ K} \times 80I$$
 ...(i)

KVL in loop-1,

$$\begin{array}{rcl}
-2 + (8 \times I) \times 10^3 + 0.01 \times V_{AB} &= 0 \\
2 &= 10^3 [8I + 0.01 \times 50 \times 80I]
\end{array}$$

$$2 = 10^3 [8I + 0.01 \times 50 \times 80I]$$

$$2 = 10^3 [8I + 40I]$$

$$2 = 48I \times 10^3$$

$$I = \frac{2}{48K} \qquad \dots (ii)$$

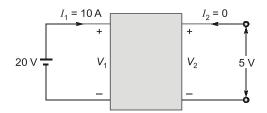
Now,

 \Rightarrow

$$V_{\text{Th}} = 50 \text{K} \times 80 \times \frac{2}{48 \text{ K}} = 166.67 \text{ V}$$

T5. (b)

From the given network,



$$I_2 = 0$$

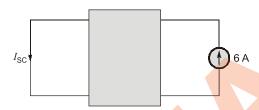
$$Z_{11} = \frac{V_1}{I_1} = \frac{20}{10} = 2 \Omega$$

$$Z_{21} = \frac{V_2}{I_1} = \frac{5}{10} = 0.5 \,\Omega$$

For a reciprocal network,

$$Z_{12} = Z_{21} = 0.5$$

: For the given second network,



$$I_{SC} = I_1, \qquad I_2 = 6 \text{ A}$$

$$\cdot$$
:

$$\frac{I_1}{I_2} = \frac{Z_{12}}{Z_{11}} = \frac{V_1/I_2}{V_1/I_1} = \frac{0.5}{2} = \frac{1}{4}$$

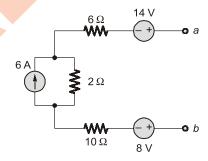
$$I_{SC} = I_1 = \frac{6}{4} = 1.5 \text{ A}$$



Combining the parallel resistance and adding the parallel connected current sources.

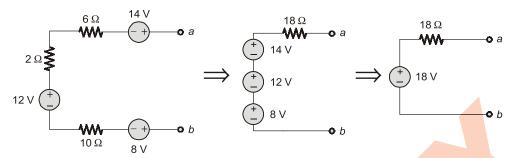
$$9A - 3A = 6A \text{ (upward)}$$

$$3\Omega | 6\Omega = 2\Omega$$

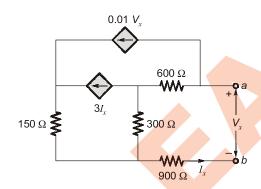




Source transformation of 6 A source



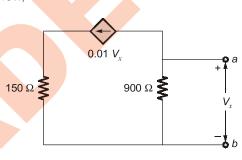
T7. (d)



For V_{OC} across a and b,

 $I_x = 0$; as O.C.

Now, circuit is reduced as below,



$$V_x = -900 \times 0.01 \ V_x$$

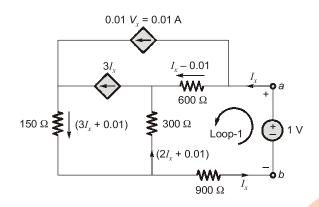
Only one case is possible,

i.e.

For R_{Th}:

$$V_{OC} = 0 \text{ V}$$

$$R_{Th} = \frac{V_x}{I_x}$$
$$V_x = 1 \text{ V}$$



KVL in loop-1,

 \Rightarrow

22

$$1 = 600(I_x - 0.01) - 300(2I_x + 0.01) + 900I_x$$

$$1 = 600I_x - 6 - 600I_x - 3 + 900I_x$$

$$10 = 900 I_{x}$$

$$I_x = \frac{1}{90}$$

$$R_{\rm Th} = 90 \, \Omega$$



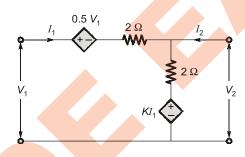
Two-Port Networks



Detailed Explanation of

Try Yourself Questions

T1. (a)



For
$$I_2 = 0$$
;

$$V_{2} = (2 \times I_{1} + KI_{1})$$

$$V_{2} = (2 + K) I_{1}$$

$$\frac{V_{2}}{I_{1}} = Z_{21} = (2 + K)$$
...(i)

For $I_1 = 0$;

$$Z_{12} = \frac{V_1}{I_2};$$

$$V_1 = 0.5 V_1 + 2I_2$$

$$0.5 V_1 = 2I_2$$

$$Z_{12} = \frac{V_1}{I_2} = 4 \qquad ...(ii)$$

 \Rightarrow

From equation (i) and (ii), From reciprocal network,

$$Z_{12} = Z_{21}$$

2 + K = 4
K = 2

T2. Sol.

To find Z_{22} ;

$$Z_{22} = \frac{V_2}{I_2} \bigg|_{I_1 = 0}$$

For $I_1 = 0$;

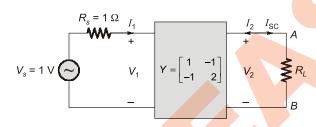
 R_{Th} from port port-2.

$$R_{\text{Th}} = 1.732 \,\Omega$$

 $Z_{22} = 1.732 \,\Omega$

T3. Sol.

$$I_{SC} = \text{for } V_2 = 0;$$



$$\begin{bmatrix} I_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} 1 & -1 \\ -1 & 2 \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix}$$

$$I_1 = V_1 - V_2$$

$$I_2 = V_1 - V_2$$

For $V_2 = 0$;

$$\therefore$$
 For $V_2 = 0$; then,

$$\therefore \quad \text{For } V_2 = 0$$
then,

$$I_{SC} = -I_2 = -V_1$$

$$= -(V_S - I_1 R_S)$$

$$-V_1 = V_S + I_1 R_S$$

$$I_1 = V_1$$

$$-V_1 = -V_S + V_1 \times R_S$$

$$V_S = V_1 (1 + R_S)$$

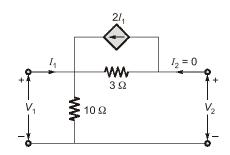
$$V_1 = \frac{V_S}{(1 + R_S)} = \frac{1}{2}$$

$$I_{SC} = -V_1 = -0.5 \text{ A}$$

Now,

T4. Sol.

To find Z-parameters:





we need to get;

$$Z_{11} = \frac{V_1}{I_1}\Big|_{I_2=0}; \qquad Z_{21} = \frac{V_2}{I_1}\Big|_{I_2=0}$$

then the circuit becomes,

$$V_1 = 10 I_1$$

 $Z_{11} = \frac{V_1}{I_1} = 10$

and

$$V_2 = V_1 - 3 \times 2I_1$$

 $V_2 = 10I_1 - 6I_1; \quad Z_{21} = \frac{V_2}{I_1} = 4$

For

$$Z_{12} = \frac{V_2}{I_1}\Big|_{I_1=0}$$

and

$$Z_{22} = \frac{V_2}{I_2} \bigg|_{I_1 = 0}$$

then the circuit becomes.

$$V_1 = 10I_2;$$
 $Z_{12} = \frac{V_1}{I_2} = 10;$

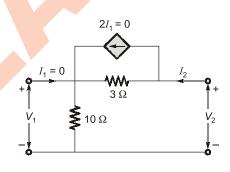
and

$$V_2 = 13I_2$$

$$Z_{22} = \frac{V_2}{I_2} = 13$$

then,

$$[Z] = \begin{bmatrix} 10 & 10 \\ 4 & 13 \end{bmatrix}$$



T5. Sol.

Given,

$$[h] = \begin{bmatrix} 16 \Omega & 3 \\ -2 & 0.015 \end{bmatrix}$$

٠, ١

$$V_1 = 16 I_1 + 3 V_2$$

$$I_2 = -2I_1 + 0.01 V_2$$

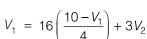
From the given circuit,

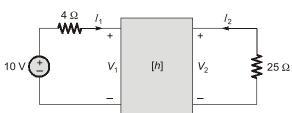
$$I_2 = -\frac{V_2}{25}$$

KVL in the loop:
$$-10 + 4I_1 + V_1 = 0$$

$$I_1 = \frac{10 - V_1}{4}$$

Substituting I_1 and I_2 in the equation (i) and (ii),





...(i) ...(ii)



$$5 V_1 - 3 V_2 = 40$$

$$\left(-\frac{V_2}{25}\right) = -2\left(\frac{10-V_1}{4}\right) + 0.01V_2$$

$$0.5 V_1 + 0.05 V_2 = 5$$

$$0.5 V_1 + 0.05 V_2 = 5$$

 $V_1 = 9.71 V; V_2 = 2.8571 V$

The ratio,

$$\frac{V_2}{V_1} = \frac{2.8571}{9.71} = 0.294$$

$$I_1 = \frac{10 - V_1}{4} = \frac{10 - 9.71}{4} = 0.072 \text{ A}$$

$$\frac{I_1}{V_1} = \frac{0.072}{9.71} = 0.0074 \, \text{U}$$

$$\frac{V_2}{V_1} = \frac{2.8571}{0.072} = 39.682 \,\Omega$$

$$\frac{I_2}{I_1} = -0.11$$

T6. Sol.

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix} = \begin{bmatrix} \frac{11}{34} & -10 \\ \frac{1}{34} & -4 \end{bmatrix}$$

T7. (c)

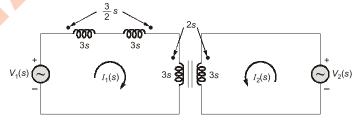
For first transformer,

For second transformer,

$$M = K\sqrt{L_1 \cdot L_2}$$

$$M_1 = \frac{1}{2}\sqrt{3 \times 3} = \frac{3}{2}H$$

$$M_2 = \frac{2}{3}\sqrt{3 \times 3} = 2H$$



By KVL for Loop 1,

$$V_1(s) = 9s I_1(s) - 3s I_1(s) + 2s I_2(s)$$

$$V_1(s) = 6s I_1(s) + 2s I_2(s)$$

$$V_1 = Z_{11} I_1 + Z_{12} I_2$$

(i)

...(ii)



We find,

$$Z_{11} = 6s$$

 $Z_{12} = 2s$

By KVL for Loop 2,

$$V_2(s) = 2s I_1(s) + 3s I_2(s)$$

 $V_2 = Z_{21} I_1 + Z_{22} I_2$

We find,

$$Z_{21} = 2s$$
$$Z_{22} = 3s$$

:.

$$[Z] = \begin{bmatrix} 6s & 2s \\ 2s & 3s \end{bmatrix}$$

 $V_{\scriptscriptstyle 1} = 100 \angle 0^{\circ}$

T8. (c)

From circuit,

and

•.•

 $V_2 = -10 I_2$ $V_1 = 40 I_1 + j20 I_2$ $V_2 = j30 I_1 + 50 I_2$

 $-10I_2 = j30I_1 + 50I_2$

 $-60I_2 = j30I_1; \quad I_2 = -\frac{1}{2} \times I_1$

From equation (i),

From equation (ii),

 $100 = 40I_1 + j20 \times \left(-\frac{j}{2}\right)I_1$

 \Longrightarrow

 $100 = 50 I_1$ $I_1 = 2\angle 0^{\circ} A$

then,

 $I_2 = -\frac{j}{2} \times 2 \text{ A} = 1 \angle -90^{\circ} \text{ A}$





Resonance



Detailed Explanation of

Try Yourself Questions

T1. Sol.

For reactive power from source to zero.

The network is behaving as purely resistive.

••

$$Y_{eq} = Y_1 + Y_2$$

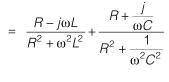
$$Y_{eq} = \frac{1}{R + X_L} + \frac{1}{R + X_C}$$

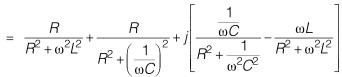
•:

$$R + X_L R + X_C$$

$$X_L = j\omega L, \quad X_C = -j\frac{1}{\omega C}$$

$$Y_{eq} = \frac{1}{R + j\omega L} + \frac{1}{R - \frac{j}{\omega C}}$$





 \therefore $I_m(Y_{eq}) = 0$; for resistive network

$$\frac{\frac{1}{\omega C}}{R^2 + \frac{1}{\omega^2 C^2}} = \frac{\omega L}{R^2 + \omega^2 L^2}$$



$$\frac{1}{\omega C} \times (R^2 + \omega^2 L^2) = \omega L \left(R^2 + \frac{1}{\omega^2 C^2} \right)$$

$$\frac{1}{\omega^2 L C} [R^2 + \omega^2 L^2] = R^2 + \frac{1}{\omega^2 C^2}$$

$$\frac{R^2}{\omega^2 L C} + \frac{L}{C} = R^2 + \frac{1}{\omega^2 C^2}$$

$$R^2 \left[1 - \frac{1}{\omega^2 L C} \right] = \frac{L}{C} - \frac{1}{\omega^2 C^2}$$

$$R^2 = \frac{\left(\frac{L}{C} - \frac{1}{\omega^2 C^2} \right)}{\left(1 - \frac{1}{\omega^2 L C} \right)}$$

$$R = \sqrt{\frac{\frac{L}{C} - \frac{1}{\omega^2 C^2}}{1 - \frac{1}{\omega^2 L C}}}$$

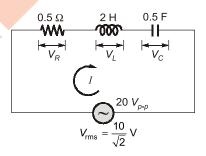
$$L = 4 \text{ H, } C = 1 \text{ F}$$

$$R = \sqrt{\frac{4 - \frac{1}{\omega^2}}{1 - \frac{1}{4\omega^2}}} = 2 \Omega$$

T2. (a)

or,

Voltage across 'R' is maximum.



When V_C and V_L are in phase opposition i.e. at resonance.

: At resonance:

Total impedance,

$$Z = R = 0.5 \Omega$$

Current,

$$I = \frac{10/\sqrt{2}}{0.5} = \frac{20}{\sqrt{2}} = 10\sqrt{2} = 14.142 \text{ A}$$



Voltage across capacitor,

$$V_C = \frac{I}{\omega_0 C}$$

•:•

$$\omega_0 = \frac{1}{\sqrt{LC}}$$

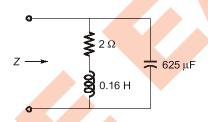
$$V_C = \frac{I}{\frac{1}{\sqrt{LC}} \times C} = I\sqrt{\frac{L}{C}}$$

$$= 10\sqrt{2}\sqrt{\frac{2}{0.5}} = 10\sqrt{2} \times 2 = 20\sqrt{2}$$

$$= \frac{40}{\sqrt{2}} V$$

T3. (c)

T4. (d)



At resonance,

$$\omega_0 = \sqrt{\frac{1}{LC} - \frac{R^2}{L^2}}$$

$$= \sqrt{\frac{10^6}{0.16 \times 625} - \frac{4}{0.16 \times 0.16}} = \sqrt{10^4 - 156.25}$$

$$= 99.216 \text{ rad/sec.}$$

Z at ω = ω₀ =
$$\frac{\omega_0^2 L^2}{R}$$
 + R = 2 + $\frac{(99.216)^2 \times (0.16)^2}{2}$
= 2 + 126 = 128 Ω

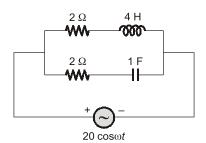
T5. Sol.

(i) At resonance;

$$Y_{eq} = G_{eq} = \frac{R}{R^2 + \frac{1}{(\omega C)^2}} + \frac{R}{R^2 + (\omega L)^2}$$

Average power consumed,

$$P = V_{\rm rms}^2 \times G_{eq} = (20/\sqrt{2})^2 \times G_{eq}$$





$$\begin{split} \because \omega_0 \text{ (resonant frequency)} &= \frac{1}{\sqrt{LC}} = \frac{1}{\sqrt{4 \times 1}} = 0.5 \text{ rad/sec.} \\ G_{eq} &= \frac{2}{4 + \frac{1}{(0.5 \times 1)^2}} + \frac{2}{4 + (0.5 \times 4)^2} \\ &= \frac{2}{4 + 4} + \frac{1}{4 + 4} = 0.5 \text{ to} \\ P &= \frac{20^2}{2} \times 0.5 = 100 \text{ W} \\ R_1 &= R_2 = R = 2 \Omega \\ L &= 1 \text{ H; } C = 1 \text{ F} \\ \omega_0 &= \frac{1}{\sqrt{1 \times 1}} = 1 \text{ rad/sec.} \\ G_{eq} &= \frac{2}{(2)^2 + (1 \times 1)^2} + \frac{2}{(2)^2 + \left(\frac{1}{1 \times 1}\right)^2} \\ &= \frac{2 + 2}{4 + 1} = \frac{4}{5} \text{ to} \\ P &= \frac{(20)^2 \times 4}{2 \times 5} = 160 \text{ W} \end{split}$$



Filters and Magnetic Coupled Circuits



Detailed Explanation

Try Yourself Questions

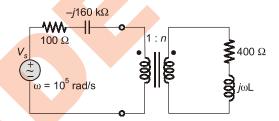


T2. (c)

In phaser domain,

$$L \Rightarrow j\omega L$$

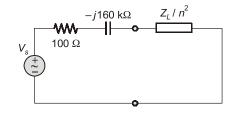
$$C \Rightarrow \frac{1}{j\omega C} = \frac{1}{j(10^5)(62.5 \times 10^{-12})} = -j160 \text{ k}\Omega$$



Load impedance,

$$Z_I = 400 + j\omega L$$

Reflecting the secondary impedance to the primary side



For maximum power transfer

$$Z_I/n^2 = Z_s^*$$

$$\frac{Z_L}{n^2} = (100 - j160 \times 10^3) \qquad Z_s = (100 - j160 \times 10^3) \Omega$$

$$Z_c = (100 - i160 \times 10^3) \Omega$$

$$\frac{400 + j\omega L}{n^2} = 100 + j160 \times 10^3$$



Comparing real parts on both sides of the equation,

$$\frac{400}{n^2} = 100 \Rightarrow n = 2$$

Comparing imaginary parts,

$$\frac{\omega L}{n^2} = 160 \times 10^3$$

 \Rightarrow

$$L = \frac{160 \times 10^3}{10^5} \times 4 = 6.4 \text{ H}$$

