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THEORY OF MACHINES

MECHANICAL ENGINEERING

Date of Test: 27/05/2023

ANSWER KEY >

1.	(a)	7.	(d)	13.	(c)	19.	(b)	25.	(b)
2.	(a)	8.	(a)	14.	(a)	20.	(d)	26.	(c)
3.	(b)	9.	(a)	15.	(a)	21.	(c)	27.	(b)
4.	(d)	10.	(c)	16.	(c)	22.	(a)	28.	(b)
5.	(c)	11.	(b)	17.	(a)	23.	(d)	29.	(b)
6.	(d)	12.	(b)	18.	(b)	24.	(c)	30.	(a)



DETAILED EXPLANATIONS

1. (a)

$$f = \frac{1}{2\pi} \sqrt{\frac{k}{m}}$$

$$12 = \frac{1}{2\pi} \sqrt{\frac{k}{m}}$$

$$6 = \frac{1}{2\pi} \sqrt{\frac{k - 800}{m}}$$
...(i)

Divide equation (i) by equation (ii),

$$2 = \sqrt{\frac{k}{k - 800}}$$

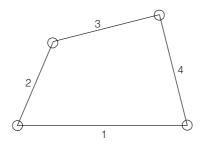
$$\frac{k}{k - 800} = 4$$

$$3k = 3200, k = \frac{3200}{3}$$

(a)

2.

Here all are turning pairs



3. (b)

Arc of contact =
$$\frac{\text{path of contact}}{\cos \phi}$$
$$\cos \phi = \frac{25.4}{27} = 0.94074$$
$$\phi = \cos^{-1}(0.94074)$$
$$\phi = 19.8^{\circ}$$

4. (d)

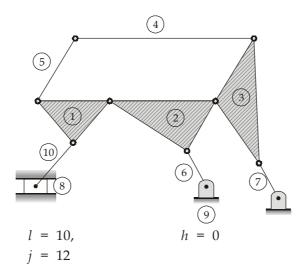
Damping coefficient,
$$c = \frac{F}{v} = \frac{0.05}{0.04} = 1.25 \text{ N/m/s}$$

Critical damping coefficient,

$$c_c = 2\sqrt{mK} = 1.897 \text{ N/m/s}$$

Damping ratio,
$$\xi = \frac{c}{c_c} = \frac{1.25}{1.897} = 0.658 \approx 0.66$$



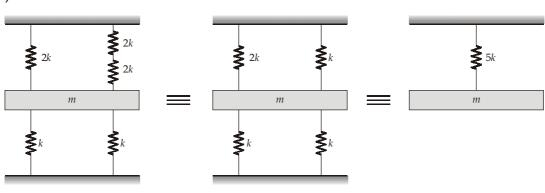


By Gruebler's criterion

$$f = 3(l-1) - 2j - h$$

= 3(10 - 1) - 2 × 12 - 0 = 27 - 24
$$F = 3$$

6. (d)



$$\omega_n = \sqrt{\frac{k_{eq}}{m}} = \sqrt{\frac{5k}{m}}$$

Given,

$$\Delta E = 18 \text{ kJ}$$

$$N_1 = 100 \text{ rpm}$$

$$N_2 = 98 \text{ rpm}$$

$$N_2 = 98 \text{ rpm}$$

We know that,

$$\Delta E = \frac{1}{2} (I\omega_1^2) - \frac{1}{2} (I\omega_2^2) = \frac{1}{2} I(\omega_1^2 - \omega_2^2)$$

$$18 \times 10^{3} = \frac{I}{2} \times \left[\left(\frac{2\pi \times 100}{60} \right)^{2} - \left(\frac{2\pi \times 98}{60} \right)^{2} \right]$$

$$I = \frac{36 \times 10^{3} \times 60^{2}}{4\pi^{2} (100^{2} - 98^{2})}$$

$$I = 8289.915 \text{ kgm}^{2}$$

Kinetic energy at 140 rpm, $E = \frac{1}{2}I\omega^2 = \frac{1}{2} \times 8289.915 \times \left(\frac{2\pi \times 140}{60}\right)^2 = 890909.088 \text{ J}$ Kinetic energy at 140 rpm, E = 890.91 kJ

Angular speed,
$$\omega = \frac{2\pi N}{60} = \frac{2\pi \times 200}{60} = 20.944 \text{ rad/s}$$

Crank radius, $r = \frac{300}{2} = 150 \text{ mm}$

Mass to be balanced at the crank pin = $(c \times m_{\text{reci}}) + (m_{\text{rev.}}) = (0.6 \times 50) + 60 = 90 \text{ kg}$ Now, $m_c \times r_c = mr$ $90 \times 0.15 = m \times 0.25$ m = 54 kg

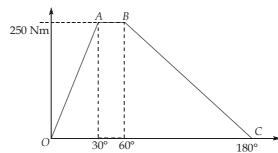
Pitch line velocity
$$V_p = \omega_1 r_1$$

= $2\pi N \times \frac{mT}{2} = 2 \times \pi \times 300 \times \frac{80 \times 8}{2}$
= 603185.7895 mm/minutes = 10053.0964 mm/s = 10.0530 m/s

10. (c)

As per given turning moment diagram,

Net energy produce in one cycle = Area of OABC = Area of trapezium OABC



$$= \frac{AB + OC}{2} \times 250 = \frac{\frac{\pi}{6} + \pi}{2} \times 250 = 145.8\pi \text{ N.m}$$

$$T_{\text{mean}} \times \pi = \text{Area of OABC}$$

$$\Rightarrow T_{\text{mean}} = \frac{145.8\pi}{\pi} = 145.8 \,\text{Nm}$$

11. (b)

Given:
$$d = 10 \times 16 = 160 \text{ mm}$$

 $D = 10 \times 50 = 500 \text{ mm}$
 $\phi = 20^{\circ}$
 $r_A = \frac{d}{2} + \text{addendum} = 80 + 12 = 92 \text{ mm}$

$$R_{A} = \frac{D}{2} + \text{addendum} = 250 + 8 = 258 \text{ mm}$$
Path of approach = $\sqrt{R_{A}^{2} - (R\cos\phi)^{2}} - R\sin\phi$
Path of approach = $\sqrt{258^{2} - (250\cos 20^{\circ})^{2}} - (250\sin 20^{\circ}) = 21.15 \text{ mm}$
Path of recess = $\sqrt{r_{A}^{2} - (r\cos\phi)^{2}} - r\sin\phi$

$$= \sqrt{92^{2} - (80\cos 20^{\circ})^{2}} - (80\sin 20^{\circ}) = 25.67 \text{ mm}$$

$$\omega_{\text{gear}} = \frac{2\pi \times 800}{60} = 83.77 \text{ rad/s}$$

$$\omega_{\text{pinion}} = \frac{T_{G}}{t_{n}} \times \omega_{\text{gear}} = \frac{50}{16} \times 83.77 = 261.799 \text{ rad/s}$$

Maximum sliding velocity = $(\omega_p + \omega_G) \times 25.67$ Maximum velocity of sliding = $(83.77 + 261.799) \times 25.67 = 8870.756 \text{ mm/s} = 8.87 \text{ m/s}$

12. (b)

$$T_A = 72$$
 $T_B = 32$
 $N_{arm} = 18 \text{ rpm}$
 $r_A = r_C + 2r_B$
 $T_A = T_C + 2T_B$
 $72 = 32 + 2T_B$
 $T_B = \frac{40}{2} = 20$

		(32)	(20)	(72)
Condition	arm	Gear C	Gear B	Gear A
Arm fixed	0	+1	$-\frac{32}{20}$	$-\frac{32}{20} \times \frac{20}{72}$
Gear <i>C</i> rotates by <i>x</i> revolutions	0	х	$-\frac{32}{20}x$	$-\frac{32}{72}x$
add + <i>y</i> revolutions to all	у	<i>x</i> + <i>y</i>	$y - \frac{32}{20}x$	$y - \frac{32}{72}x$

$$y = 18 \text{ rpm}$$

Gear A is fixed

$$y = \frac{32}{72}x$$
$$y = \frac{32}{72}x$$

$$\frac{18 \times 72}{32} = x$$

$$x = 40.5$$
Speed of 'B' $N_B = y - \frac{32}{20}x$

$$= 18 - \frac{32}{20} \times 40.5$$

$$N_B = -46.8 \text{ rpm}$$

13. (c)

Given, m = 1 tonne = 1000 kg

Logarithmic decrement of n cycles is given by

$$\delta = \frac{1}{n} \log_e \frac{x_0}{x_n}$$

n = 4

Given,

$$\delta = \frac{1}{4} \log_e \frac{5}{0.128} = 0.916$$

$$\delta = \frac{2\pi\xi}{\sqrt{1-\xi^2}}$$
 or $0.916 = \frac{2\pi\xi}{\sqrt{1-\xi^2}}$

 $\xi = 0.144$

 $T_d = 0.64$ seconds

$$\omega_d = \frac{2\pi}{T_d} = \frac{2\pi}{0.64} = 9.817 \text{ rad/s}$$

$$\omega_d = \sqrt{1 - \xi^2} \, \omega_n$$

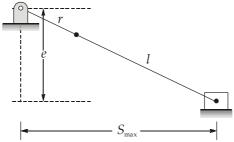
$$\omega_n = \frac{9.817}{\sqrt{1 - 0.144^2}} = 9.92 \text{ rad/s}$$

$$\sqrt{\frac{k}{m}} = 9.92$$

$$k = 9.92^2 \times 1000 = 98406.4 \text{ N/m} = 98.406 \text{ N/mm}$$

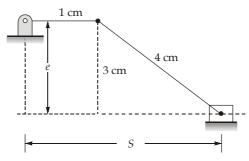
14. (a)

At
$$S = S_{\text{max}}$$
: $r + l = \sqrt{S_{\text{max}}^2 + e} = \sqrt{4^2 + 3^2} = 5 \text{ cm}$



Given, r = 1 cm, at $\theta = 0$:

So,
$$l = 5 - 1 = 4$$
 cm



$$S = \sqrt{4^2 - 3^2} + 1 = \sqrt{7} + 1$$

So, at
$$\theta = 0$$
, $S = 3.645$ or 3.65 cm

15. (a)

$$m = 120 \text{ kg}, \qquad E = 200 \times 10^9 \text{ N/m}^2$$

$$l = 0.7 \text{ m}, \qquad d = 0.04 \text{ m}$$

$$a = 0.25 \text{ m}, \qquad b = 0.7 - 0.25 = 0.45 \text{ m}$$

$$I = \frac{\pi}{64} \times d^4 = \frac{\pi}{64} \times (0.04)^4$$

$$= 0.1256 \times 10^{-6} \text{ m}^4$$

$$\Delta = \frac{mga^3b^3}{3EIl^3} = \frac{120 \times 9.81 \times (0.25)^3 \times (0.45)^3}{3 \times 200 \times 10^9 \times 0.1256 \times 10^{-6} \times (0.7)^3}$$

$$= 6.48 \times 10^{-5} \text{ m}$$

$$f = \frac{1}{2\pi} \sqrt{\frac{g}{\Lambda}} = \frac{1}{2\pi} \sqrt{\frac{9.81}{6.48 \times 10^{-5}}} = 61.90 \text{ Hz}$$

16. (c)

$$MF = \frac{1}{\sqrt{\left(1 - \left(\frac{\omega}{\omega_n}\right)^2\right)^2 + \left(2\xi \frac{\omega}{\omega_n}\right)^2}}$$

According to question, $\frac{\omega}{\omega_n} = k$

So,
$$MF = \frac{1}{\sqrt{(1-k^2)^2 + (2\xi k)^2}}$$

For MF to be maximum, $(1 - k)^2 + (2\xi k)^2$ should be minimum. So, for the denominator to be minimum

$$\frac{d((1-k^2)^2 + (2\xi k)^2)}{dk} = 0$$

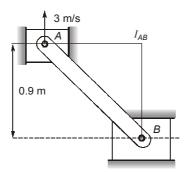
$$2(1-k^2)(-2k) + 8\xi^2 k = 0$$

$$k(k^2 - 1 + 2\xi^2) = 0$$

$$k = \sqrt{1-2\xi^2} = \sqrt{1-2\times0.32^2}$$

$$k = 0.89$$

17. (a)



$$I_{AB} \cdot B = 0.9 \text{ m}$$
 $AB = 1.5 \text{ m}$

$$I_{AB} \cdot A = \sqrt{(AB)^2 - (I_{AB}B)^2} = \sqrt{(1.5)^2 - (0.9)^2} = \sqrt{2.25 - 0.81} = 1.2 \text{ m}$$

$$\frac{V_B}{V_A} = \frac{I_{AB} \cdot B}{I_{AB} \cdot A} = \frac{0.9}{1.2}$$

$$V_B = V_A \times \frac{0.9}{1.2} = 3 \times \frac{9}{12} = 2.25 \text{ m/s}$$

18. (b)

:.

$$\frac{N_F}{N_A} = \frac{T_{\text{input}}}{T_{\text{output}}} = \frac{T_E}{T_F} \times \frac{T_C}{T_D} \times \frac{T_A}{T_B} = \frac{26 \times 25 \times 20}{50 \times 75 \times 65}$$

$$N_F = 0.0533 \ N_A = 0.0533 \times 975 = 52 \text{ rpm}$$

19. (b)

$$\omega_{AB} \times 0.2 = \omega_{BD} \times 0.25$$

$$15 \times 0.2 = \omega_{BD} \times 0.25$$

$$\omega_{BD} = 12 \text{ rad/s}$$

20. (d)

$$\omega_{\text{max}} = \frac{\omega_{1}}{\cos \alpha}$$

$$\omega_{\text{min}} = \omega_{1} \cos \alpha$$

$$\omega_{\text{max}} - \omega_{\text{min}} = \omega_{1} \left[\frac{1}{\cos \alpha} - \cos \alpha \right]$$

 $\alpha = 16.1^{\circ}$

Variation of speed, w

Permissible variation of speed = ± 4 % of mean speed

or,
$$\omega_1 \left[\frac{1}{\cos \alpha} - \cos \alpha \right] = 0.08 \,\omega_1$$
or,
$$\cos^2 \alpha + 0.08 \cos \alpha - 1 = 0$$

$$\cos \alpha = 0.96$$

Now,

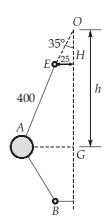
$$h = GO = GH + HO = AE \cos\theta + EH \cot\theta$$

$$h = 400\cos35^{\circ} + 25\cot35^{\circ} = 363.4 \text{ mm}$$

$$h' = 400\cos30^{\circ} + 25\cot30^{\circ} = 389.7 \text{ mm}$$

$$h = \frac{g}{\omega^{2}} \text{ and } h' = \frac{g}{\omega'^{2}}$$

$$\frac{\omega'}{\omega} = \sqrt{\frac{h}{h'}} = \sqrt{\frac{363.4}{389.7}} = 0.966$$
Decrease in speed = $(1 - 0.966) \times 100 = 3.44\%$



22. (a)

As per given data, $I = 1.5 \text{ kg-m}^2$

The angular velocity of spin of the disc,

$$\omega = \frac{2\pi \times 500}{60} = \frac{100\pi}{6} \, \text{rad/s}$$

The angular velocity of precession,

$$\omega_p = \frac{2\pi}{5} \text{ rad/s}$$

Gyroscopic couple, $T = I\omega\omega_p$

=
$$1.5 \times \frac{100\pi}{6} \times \frac{2\pi}{5} = 10\pi^2 = \frac{20\pi^2}{2} \text{ kg-m}^2/\text{s}^2$$

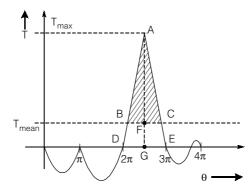
Disturbing force,
$$F = (1 - c) \text{ mr}\omega^2 \cos\theta$$

= $(1 - 0.4) \times 6 \times 0.10 \times 15^2 \times \cos 60 = 40.5 \text{ N}$

$$\omega = \frac{2\pi N}{60} = \frac{2\pi \times 120}{60} = 12.57 \text{ rad/sec}$$

for SHM
$$a_{\text{max}} = \frac{h}{2} \left(\frac{\pi \omega}{\phi_a} \right)^2 = \frac{30}{2} \left(\frac{\pi \times 12.57}{180 \times \frac{\pi}{180}} \right)^2 = 2370.0735 \text{ mm/s}^2 = 2.37 \text{ m/s}^2$$

26. (c)



$$P = \frac{2\pi N T_{\text{mean}}}{60}$$

$$\Rightarrow T_{\text{mean}} = \frac{60 \times 40 \times 10^3}{2 \times \pi \times 130} = 2938.245 \,\text{N-m}$$

$$\Rightarrow$$
 Energy produced = $T_{mean} \times 4\pi = 36923.076 \text{ N-m}$

Now, work done during the power stroke

$$= 1.5 \times 36923.076$$

= 55384.615 Nm

Now, from similar triangles ABC, ADE;

$$\frac{AF}{AG} = \frac{BC}{DE}$$

$$\frac{1}{2} \times T_{\text{max}} \times \pi = 55384.6$$

$$\Rightarrow T_{\text{max}} = 35258.93 \text{ Nm} = AG$$

Now,
$$\frac{35258.93 - 2938.245}{35258.93} = \frac{BC}{\pi}$$

$$\Rightarrow BC = 2.879 \text{ rad}$$

Now, maximum fluctuation of energy = $\frac{1}{2} \times AF \times BC$

$$= \frac{1}{2} \times (35258.93 - 2938.245) \times 2.879$$

= 46525.62 N-m

27. (b)

For the Hartnell governor spring stiffness is given by

$$k = 2\left(\frac{a}{b}\right)^2 \left(\frac{F_1 - F_2}{r_1 - r_2}\right)$$

$$k = 2\left(\frac{a}{b}\right)^2 \left(\frac{1500 - 100}{20 - 15}\right)$$

$$k = 2\left(\frac{1400}{5}\right) = 560 \text{ N/cm} \quad (\because \text{ a and b are same})$$

28. (b)

Given,

Lift,
$$h = 25 \,\mathrm{mm}$$

Offset,
$$x = 12 \,\mathrm{mm}$$

Speed,
$$N = 300 \text{ rpm}$$

$$\omega = \frac{2\pi N}{60} = \frac{2\pi \times 300}{60} = 10\pi \text{ rad/s}$$

Ascent angle, $\phi_a = 60^{\circ}$

Descent angle, $\phi_d = 90^{\circ}$

Dwell angle,
$$\delta_1 = 45^{\circ}$$

Now,

$$\delta_2 = 360^{\circ} - (60^{\circ} + 90^{\circ} + 45^{\circ}) = 165^{\circ}$$

During out stroke:

$$(a_{\text{uniform}})_{\text{o.s}} = \frac{4h\omega^2}{\phi_a^2} = \frac{4 \times 25 \times (10\pi)^2 \times 10^{-3}}{\left(60 \times \frac{\pi}{180}\right)^2}$$

= $100 \times 100 \times 10^{-3} \times 9 = 90 \text{ m/s}^2$

During return stroke:]

$$(a_{\text{uniform}})_{\text{r.s.}} = \frac{4\hbar\omega^2}{\phi_d^2} = \frac{4\times25\times(10\pi)^2\times10^{-3}}{\left(90\times\frac{\pi}{180}\right)^2} = 40 \text{ m/s}^2$$

$$\frac{\left(a_{\text{uniform}}\right)_{o.s}}{\left(a_{\text{uniform}}\right)_{r.s}} = \frac{90}{40} = 2.25$$

29. (b)

(i) Controlling force, F = 3r - 60

At lower extreme radii, $F_1 = 3 \times 120 - 60 = 300 \text{ N}$

Controlling force at maximum speed, $F_1 = 300 + 30 = 330 \text{ N}$

Controlling force at minimum speed, $F_2 = 300 - 30 = 270 \text{ N}$

Coefficient of insensitiveness,= $\frac{N_1 - N_2}{N_{\text{mean}}} \frac{(N_1 - N_2)(N_1 + N_2)}{2 \times N_{\text{mean}}^2}$

$$= \frac{N_1^2 - N_2^2}{2N_{\text{mean}}^2} = \frac{F_1 - F_2}{2F} = \frac{330 - 270}{2 \times 300}$$
 $\{F \propto \omega^2 \propto N^2\}$

Coefficient of insensitiveness = $\frac{60}{600}$ = 0.1 = 10%

(ii) At upper extreme radii:

$$F = 3r - 60 = 3 \times 190 - 60 = 510 \text{ N}$$

Controlling force at maximum speed, $F_1 = 510 + 30 = 540 \text{ N}$

Controlling force at minimum speed, $F_2 = 510 - 30 = 480 \text{ N}$

Coefficient of insensitiveness,=
$$\frac{F_1 - F_2}{2F} = \frac{540 - 480}{2 \times 510} = \frac{60}{2 \times 510} = 0.0588 = 5.88\%$$

Coefficient of insensitiveness at upper extreme radii = 5.88%

Coefficient of insensitiveness at lower extreme radii = 10.00%

 $\left(\frac{X_0}{X_1} = \frac{X_1}{X_2} = \frac{X_2}{X_3} = \frac{X_3}{X_4}\right)$

30. (a)

Given: Mass,
$$m = 12 \text{ kg}$$

Number of oscillations,
$$N = 45$$

Time,
$$t = 7$$
 seconds

$$\frac{X_0}{X_4} = \left(\frac{X_0}{X_1}\right) \times \left(\frac{X_1}{X_2}\right) \times \left(\frac{X_2}{X_3}\right) \times \left(\frac{X_3}{X_4}\right)$$

$$\frac{X_0}{X_4} = \left(\frac{X_0}{X_1}\right)^4$$

$$\frac{X_0}{X_1} = \left(\frac{X_0}{X_4}\right)^{1/4} = \left(\frac{1}{0.4}\right)^{0.25} = 1.25743$$

Logarithmic decrement,
$$\delta = \ln\left(\frac{X_0}{X_4}\right) = \ln(1.25743) = 0.229$$

$$\therefore \qquad \delta = \frac{2\pi\xi}{\sqrt{1-\xi^2}}$$

$$(0.229)^2 (1 - \xi^2) = (2\pi)^2 \xi^2$$

$$1 - \xi^2 = 752.8159\xi^2$$
$$\xi = 0.03672$$

$$\omega_d = \sqrt{1 - \xi^2 \omega_n}$$
 $\{\omega_d = 45 \times 2\pi/7 = 40.392 \text{ rad/s}\}$

$$40.392 = \sqrt{1 - \xi^2} \omega_n = 0.9993255 \omega_n$$

$$\omega_n = 40.419262$$

 $\omega_n \ = \ 40.419262$ Damping coefficient, $C = 2\xi\omega_{\rm n}{\rm m}$

$$= 2 \times 12 \times 40.419262 \times 0.03642$$

$$C = 35.6206 \text{ kg/s}$$