

PN junction

$$I_{tot} = A \cdot J_{tot}; \quad J_{tot} = J_{tot}^{drift} + J_{tot}^{diff}; \quad J_{tot}^{drift} = (\mu_n \cdot n + \mu_p \cdot p) \cdot q \cdot E; \quad J_{tot}^{diff} = q \cdot \left(D_n \cdot \frac{dn}{dx} - D_p \cdot \frac{dp}{dx} \right);$$

$$I_D = I_S \cdot (e^{\frac{V_F}{V_T}} - 1); \quad r_D = \left(\frac{dI_D}{dV_F} \right)^{-1} \approx \frac{V_T}{I_D}, \quad v_f \ll V_F; \quad n_i \approx 5.2 \cdot 10^{15} \cdot T^{\frac{3}{2}} \cdot e^{-\frac{E_g}{2 \cdot k \cdot T}};$$

$$C_j = \frac{C_{j0}}{\sqrt{1 + \frac{V_R}{V_0}}}; \quad C_{j0} = A \cdot \sqrt{\frac{\epsilon \cdot q}{2} \cdot \frac{N_A \cdot N_D}{N_A + N_D} \cdot \frac{1}{V_0}}; \quad V_0 = V_T \cdot \ln \left(\frac{N_A \cdot N_D}{n_i^2} \right).$$

BJT

$$I_C = I_S \cdot e^{\frac{V_{BE}}{V_T}} \cdot \left(1 + \frac{V_{CE}}{V_A} \right) \approx I_S \cdot e^{\frac{V_{BE}}{V_T}}; \quad I_S = \frac{q \cdot A \cdot D_n \cdot n_i^2}{W_B \cdot N_A}; \quad V_A = \frac{I'_C}{\frac{dI_C}{dV_{CE}}};$$

$$\beta_F = \frac{I_C}{I_B} = \frac{1}{\frac{W_B^2}{2 \cdot \tau_b \cdot D_n} + \frac{D_p}{D_n} \cdot \frac{W_B}{L_p} \cdot \frac{N_A}{N_D}}; \quad g_m = \frac{dI_C}{dV_{BE}} = \frac{I_C}{V_T}; \quad r_\pi = \frac{dV_{BE}}{dI_B} = \frac{\beta_F}{g_m}; \quad r_o = \frac{dV_{CE}}{dI_C} = \frac{V_A}{I_C}.$$

MOSFET

$$V_{ov} = V_{GS} - V_{th}; \quad V_{th} = V_{th0} + \gamma \cdot \left(\sqrt{2 \cdot \phi_f + V_{Bias}} - \sqrt{2 \cdot \phi_f} \right); \quad k' = \mu_n \cdot C_{ox}; \quad \frac{g_m}{I_D} = \frac{2}{V_{ov}};$$

$$\gamma = \frac{1}{C_{ox}} \cdot \sqrt{2 \cdot q \cdot \epsilon \cdot N_A}; \quad C_{ox} = \frac{\epsilon_{ox}}{t_{ox}}; \quad V_A = \frac{1}{\lambda} = \frac{I_D}{\frac{dI_D}{dV_{DS}}}; \quad r_{in} \rightarrow \infty; \quad r_o = \frac{dV_{DS}}{dI_D} = \frac{V_A}{I_D};$$

$$I_D = \begin{cases} k' \cdot \frac{W}{L} \cdot V_{ov} \cdot V_{DS} & V_{DS} \ll V_{ov}, \\ \frac{k'}{2} \cdot \frac{W}{L} \cdot (2 \cdot V_{ov} \cdot V_{DS} - V_{DS}^2) & V_{DS} < V_{ov}, \\ \frac{k'}{2} \cdot \frac{W}{L} \cdot V_{ov}^2 \cdot \left(1 + \frac{V_{DS}}{V_A} \right) & V_{DS} \geq V_{ov} \end{cases}; \quad g_m = \frac{dI_D}{dV_{GS}} = k' \cdot \frac{W}{L} \cdot V_{ov} = \sqrt{2 \cdot k' \cdot \frac{W}{L} \cdot I_D}.$$

Common Source/Emitter Amplifier

$$r_{in}^{cs} \rightarrow \infty; \quad r_o^{cs} = \left(r_o \cdot (1 + g_m \cdot R_S) \right) \parallel R_D;$$

$$g_m^{cs} = \frac{g_m}{1 + g_m \cdot R_S}; \quad a^{cs} = \frac{g_m \cdot R_D}{1 + g_m \cdot R_S};$$

$$r_{in}^{ce} \approx r_\pi + (\beta + 1) \cdot R_E; \quad r_o^{ce} = \left(r_o \cdot (1 + g_m \cdot R_E) \right) \parallel R_C;$$

$$g_m^{ce} = \frac{g_m}{1 + g_m \cdot R_E}; \quad a^{ce} = \frac{g_m \cdot R_C}{1 + g_m \cdot R_E}.$$

Common Drain/Collector Amplifier

$$r_{in}^{cd} \rightarrow \infty; \quad r_o^{cd} = \frac{1}{g_m + g_{mb} + \frac{1}{r_o} + \frac{1}{R_L}};$$

$$g_m^{cd} = g_m; \quad a^{cd} = \frac{g_m}{g_m + g_{mb} + \frac{1}{r_o} + \frac{1}{R_L}} \approx \frac{g_m \cdot R_L}{1 + g_m \cdot R_L};$$

$$r_{in}^{cc} = r_\pi + (\beta + 1) \cdot (R_L \parallel r_o); \quad r_o^{cc} = r_o \parallel \left(\frac{r_\pi + R_S}{\beta + 1} \right) \approx \frac{1}{g_m} + \frac{R_S}{\beta + 1};$$

$$g_m^{cc} = g_m + \frac{1}{r_\pi}; \quad a^{cc} = \frac{1}{1 + \frac{R_S + r_\pi}{(\beta + 1) \cdot (R_L \parallel r_o)}} \approx \frac{g_m \cdot R_L}{1 + g_m \cdot R_L}.$$

Common Gate/Base Amplifier

$$r_{in}^{cg} = \frac{1}{g_m} \cdot \left(1 + \frac{R_D}{r_o} \right); \quad r_o^{cg} \approx r_o \cdot (1 + g_m \cdot R_S); \quad V_A \rightarrow \infty \implies r_o \rightarrow \infty;$$

$$g_m^{cg} = g_m; \quad a^{cg} = g_m \cdot (R_D \parallel r_o^{cg}) = g_m \cdot R_D; \quad a_i^{cg} = 1;$$

$$r_{in}^{cb} \approx \frac{\alpha}{g_m} \cdot \left(1 + \frac{R_C}{r_o} \right) \approx \frac{1}{g_m} \cdot \left(1 + \frac{R_C}{r_o} \right); \quad r_o^{cb} \approx r_o \cdot (1 + g_m \cdot (R_E \parallel r_\pi)); \quad V_A \rightarrow \infty \implies r_o \rightarrow \infty;$$

$$g_m^{cb} = g_m; \quad a^{cb} = g_m \cdot (R_C \parallel r_o^{cb}) \approx g_m \cdot R_C; \quad a_i^{cb} = \alpha = \frac{\beta}{\beta + 1}.$$

MOSFET/BJT Cascode Amplifier

$$r_{in}^{mcas} \rightarrow \infty; \quad r_o^{mcas} = r_{o1} + r_{o2} + g_{m2} \cdot r_{o1} \cdot r_{o2} \approx g_{m2} \cdot r_{o1} \cdot r_{o2}$$

$$g_m^{mcas} = g_m; \quad a^{mcas} = g_m \cdot (R_D \parallel r_o^{mcas});$$

$$r_{in}^{bcas} = r_\pi; \quad r_o^{bcas} \approx (1 + g_m \cdot (r_{o2} \parallel r_\pi)) \cdot r_{o1};$$

$$g_m^{bcas} = g_m; \quad a^{bcas} = g_m \cdot (R_C \parallel r_o^{bcas})$$

MOSFET/BJT Differential Pair

Amplifications: $a_{dm} = \left. \frac{v_{od}}{v_{id}} \right|_{v_{ic}=0}$; $a_{cm} = \left. \frac{v_{oc}}{v_{ic}} \right|_{v_{id}=0}$; $a_{dmcm} = \left. \frac{v_{od}}{v_{ic}} \right|_{v_{id}=0}$; $a_{cmdm} = \left. \frac{v_{oc}}{v_{id}} \right|_{v_{ic}=0}$;

MOSFET Differential Mode: $r_{in}^{dm} \rightarrow \infty$; $r_o^{dm} \approx R_D$; $g_m^{dm} = g_m$; $a^{dm} = -g_m \cdot R_D$;

MOSFET Common Mode: $r_{in}^{cm} \rightarrow \infty$; $r_o^{cm} \approx R_D$; $g_m^{cm} = \frac{g_m}{1 + 2 \cdot g_m \cdot R_{Tail}}$;
 $a^{cm} = -g_m^{cm} \cdot R_D$; $CMRR = \frac{a^{dm}}{a^{cm}} = 1 + 2 \cdot g_m \cdot R_{Tail}$;

BJT Differential Mode: $r_{in}^{dm} = 2 \cdot r_\pi$; $r_o^{dm} \approx R_C$; $g_m^{dm} = g_m$; $a^{dm} = -g_m \cdot R_C$;

BJT Common Mode: $r_{in}^{cm} = r_\pi + (\beta + 1) \cdot 2 \cdot R_{Tail}$; $r_o^{cm} \approx R_C$; $g_m^{cm} = \frac{g_m}{1 + 2 \cdot g_m \cdot R_{Tail}}$;
 $a^{cm} = -g_m^{cm} \cdot R_C$; $CMRR = \frac{a^{dm}}{a^{cm}} = 1 + 2 \cdot g_m \cdot R_{Tail}$.

Operational Amplifier

Non-inverting amplification: $a^+ = \left(1 + \frac{R_2}{R_1}\right) \cdot \frac{1}{\frac{1}{a} \cdot \left(1 + \frac{R_2}{R_1}\right) + 1} \approx 1 + \frac{R_2}{R_1}$;

Inverting amplification: $a^- = -\frac{R_2}{R_1} \cdot \frac{1}{\frac{1}{a} \cdot \left(1 + \frac{R_2}{R_1}\right) + 1} \approx -\frac{R_2}{R_1}$;

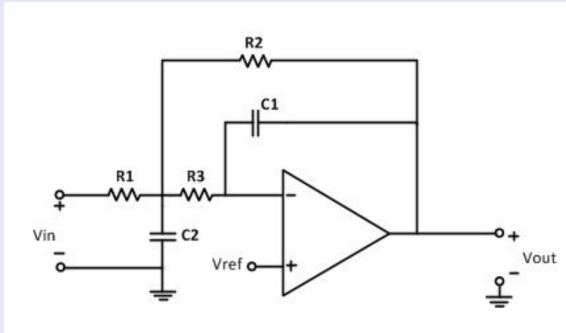
Output voltages: $v_o^{int} = -\frac{1}{R \cdot C} \cdot \int v_s dt$; $v_o^{diff} = -\frac{1}{R \cdot C} \cdot \frac{dv_s}{dt}$;

$$v_o^{DISO} = -v_1 \cdot \frac{R_3}{R_1} + v_2 \cdot \frac{R_4}{R_2 + R_2} \cdot \left(1 + \frac{R_3}{R_1}\right) = \frac{R_3}{R_1} \cdot (v_2 - v_1) \Bigg|_{\substack{R_1=R_2, \\ R_3=R_4}}$$

$$v_o^{instr} = \frac{R_4}{R_3} \cdot \left(1 + \frac{2 \cdot R_2}{R_1}\right) \cdot (v_2 - v_1)$$

Active Amplifiers

MFB

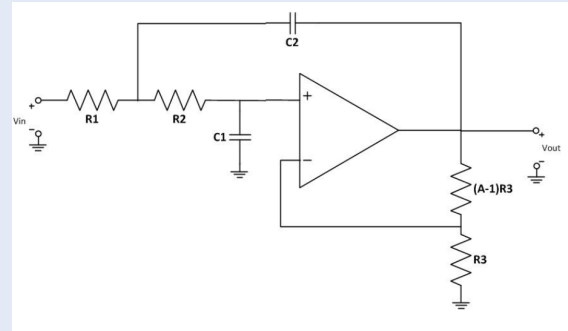


$$R_2 = \frac{a_1 - \sqrt{a_1^2 - \frac{4 \cdot b_1 \cdot C_1}{C_2} \cdot (1 + |A_0|)}}{4 \cdot \pi \cdot f_g \cdot C_1};$$

$$R_1 = \frac{R_2}{|A_0|}; \quad R_3 = \frac{b_1}{4 \cdot \pi^2 \cdot C_1 \cdot C_2 \cdot R_2};$$

$$C_2 \geq \frac{4 \cdot b_1 \cdot (1 + |A_0|)}{a_1^2} \cdot C_1.$$

Sallen-Key



$$R_1 = \frac{a_1 \pm \sqrt{a_1^2 - 4 \cdot b_1 \cdot \frac{C_1 + (1 - A_0) \cdot C_2}{C_2}}}{4 \cdot \pi \cdot f_g \cdot (C_1 + (1 - A_0) \cdot C_2)};$$

$$R_2 = \frac{b_1}{4 \cdot \pi^2 \cdot f_g^2 \cdot R_1 \cdot C_1 \cdot C_2}$$

$$\frac{C_1}{C_2} \leq \frac{a_1^2}{4 \cdot b_1} + (A_0 - 1).$$

Load Regulators

$$V_{dropout} = I_L \cdot R_{DS(on)}.$$