

# **Stable Fluids**

by

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## 0 Abstract

# 1 Introduction

## 2 Mathematical Modelling

### 2.1 Basic Equations

Let  $\Omega \subset \mathbb{R}^2$  be the domain of interest, e.g.  $\Omega = (0, 1)^2$ . Now let  $u \in C^2(\mathbb{R} \times \Omega, \mathbb{R}^2)$  denote the velocity vector field and  $p \in C^2(\mathbb{R} \times \Omega, \mathbb{R})$  denote the pressure field. Both fields depend on the time  $t \in \mathbb{R}$  and the position in space  $x \in \Omega$ . The evolution of these fields is given by the Navier-Stokes equations

$$\operatorname{div} u = 0 \quad (2.1)$$

$$\frac{\partial u}{\partial t} = -(u \cdot \nabla)u - \frac{1}{\rho} \nabla p + \nu \Delta u + f, \quad (2.2)$$

where  $\nu, \rho$  are constants that determine the viscosity of the fluid and the density respectively. In  $\mathbb{R}^2$ , equation 2.2 can be written out as

$$\begin{pmatrix} \frac{\partial u_1}{\partial t} \\ \frac{\partial u_2}{\partial t} \end{pmatrix} = - \begin{pmatrix} u_1 \frac{\partial u_1}{\partial x_1} + u_2 \frac{\partial u_1}{\partial x_2} \\ u_1 \frac{\partial u_2}{\partial x_1} + u_2 \frac{\partial u_2}{\partial x_2} \end{pmatrix} - \frac{1}{\rho} \begin{pmatrix} \frac{\partial p}{\partial x_1} \\ \frac{\partial p}{\partial x_2} \end{pmatrix} + \nu \begin{pmatrix} \frac{\partial^2 u_1}{\partial x_1^2} + \frac{\partial^2 u_1}{\partial x_2^2} \\ \frac{\partial^2 u_2}{\partial x_1^2} + \frac{\partial^2 u_2}{\partial x_2^2} \end{pmatrix} + \begin{pmatrix} f_1 \\ f_2 \end{pmatrix}.$$

The pressure and velocity field that appears in the Navier-Stokes equations, are related. By combining equation 2.1 and 2.2 we obtain a single equation as follows.

By the Helmholtz-Hodge decomposition theorem we have that any vector field  $w = u + \nabla q + \text{res}$  uniquely decomposes into a divergence-free part  $u$ , a gradient field  $\nabla q$  and a residual term depending on the genus of the surface. In our case, the residual term vanishes.

Let  $P : C^2(\Omega, \mathbb{R}^2) \rightarrow \{f \in C^2(\Omega, \mathbb{R}^2), \operatorname{div} f = 0\}$  denote the projection operator onto the divergence free part. Obviously, the operator  $P$  is implicitly defined by

$$\operatorname{div} w = \Delta q. \quad (2.3)$$

With Neumann boundary condition ( $\frac{\partial q}{\partial n} = 0$  on  $\partial\Omega$ ,  $n$  is the outward normal), equation 2.3 is a Poisson equation. Let  $q$  denote the solution, then  $P$  is defined by  $Pw = w - \nabla q$ . If we now apply  $P$  to both sides of 2.2, the Navier-Stokes equation compress into our fundamental equation 2.4.

$$\frac{\partial u}{\partial t} = P \left( -(u \cdot \nabla)u - \frac{1}{\rho} \nabla p + \nu \Delta u + f \right) \quad (2.4)$$

### 2.2 Method of Solution and Discretization

Equation 2.4 consists of four parts, the **add force** term  $f$ , the **advection** term  $(u \cdot \nabla)u$ , the **diffusion** term  $\nu \Delta u$  and the **projection** operator  $P$ . The equation is solved from an initial state  $u^0 = u(0, x)$ . Both time and space are discretized with time step  $\Delta T$  and some equidistant grid points of distance  $h = \frac{1}{n}$ . Each of the four terms in equation 2.4 is applied

## 2.2 Method of Solution and Discretization

successively to the initial state  $u^0 \in C^2(\Omega, \mathbb{R})$ . The general procedure is

$$u^0 \xrightarrow{\text{add force}} u^1 \xrightarrow{\text{advect}} u^2 \xrightarrow{\text{diffuse}} u^3 \xrightarrow{\text{project}} u^4$$

The solution at time  $t + \Delta t$  is then given by  $u(x, t + \Delta t) = u^4(x)$ .

### 2.2.1 Add force

The add force step incorporates additional force by the user, or buoyancy force due to uplift of lighter gases and downlift of heavier gases.

$$u^1(x) = u^0(x) + \Delta t f(t, x)$$

The buoyancy force is computed using Archimedes' principle. In a simplified approach, heaviness is equal to the density of the smoke. After computing the average temperature of the fluid, the upward force is determined for each pixel separately depending on the difference with respect to the average temperature.

### 2.2.2 Advect

The advect step accounts for the advection or convection of the fluid itself, i.e. this step lets the fluid „flow“ a little. The advection step is fundamental to this particular fluid solver. That's why the solver is called „Stable“Fluids, as this solver will never blow up, independent of the size of the time step  $\Delta t$ .

The method can be understood intuitively: All particles in the fluid are moved by the velocity of the fluid itself. To obtain the velocity at the point  $x$  at time  $t + \Delta t$  we backtrace the point  $x$  through the velocity field at time  $t$ . This defines a path  $p : (-\delta, \delta) \times \Omega \rightarrow \Omega$  corresponding to a streamline of the fluid. The velocity  $u^2(x)$  is the set to be the velocity of  $u^1(p(-\Delta t, x))$  at the previous time step:

$$u^2(x) = u^1(p(-\Delta t, x)).$$

[tba] include a figure that illustrates the approach. [tba] [tba] include a comparison to other solvers of the advect step. [tba]

### 2.2.3 Diffuse

This step solves the diffusion of the fluid itself, i.e. the „friction“ between parts of the fluid with different velocity. This effect is equivalent to the diffusion equation

$$\frac{\partial u^2}{\partial t} = \nu \Delta u^2. \quad (2.5)$$

The most straightforward way would be to discretize the Laplacian and solve the resulting sparse linear system. However, this approach is unstable when the viscosity is large. For our implicit approach we proceed as follows, by approximating  $\frac{\partial u}{\partial t}$  with the backward difference



### 2.3 Moving substances through the Fluid

quotient:

$$\frac{u(t + \Delta t, x) - u(x, t)}{\Delta t} = \nu \Delta u(t - \Delta t, x)$$

finally, this gives

$$(I - \nu \Delta t) u^3(x) = u^2(x). \quad (2.6)$$

We now discretize 2.6 using a finite difference method and obtain

$$\left( \begin{bmatrix} 1 & & & \\ & \ddots & & \\ & & \ddots & \\ & & & 1 \end{bmatrix} - \begin{bmatrix} -4 & 1 & & & \\ & \ddots & \ddots & & \\ & 1 & \ddots & & \\ & & \ddots & \ddots & \\ & & & 1 & -4 \end{bmatrix} \right) \nu \frac{\Delta t}{h^2} u^3 = u^2. \quad (2.7)$$

The resulting square matrix has  $n * m$  rows and columns, where  $n, m$  denote the number of pixels in the x- and y-axis respectively. Solving such a system can be done efficiently by iterative schemes, e.g. Gauß-Seidel.

#### 2.2.4 Project

The last step makes the vectorfield mass preserving, i.e. divergence free. We already discussed in the derivation of our fundamental equation that the projection is obtained by solving

$$\operatorname{div} u = \Delta q.$$

When discretized, this equation becomes

$$\frac{1}{2h} \begin{bmatrix} 0 & 1 & & \\ 1 & \ddots & & \\ & \ddots & \ddots & \\ & & 1 & 0 \end{bmatrix} u_1^3 + \frac{1}{2h} \begin{bmatrix} 0 & & 1 & \\ & \ddots & & \\ 1 & & \ddots & \\ & 1 & & 0 \end{bmatrix} u_2^3 = \begin{bmatrix} -4 & 1 & & & \\ & \ddots & \ddots & & \\ & 1 & \ddots & & \\ & & \ddots & \ddots & \\ & & & 1 & -4 \end{bmatrix} q. \quad (2.8)$$

As in equation 2.7 we need to solve a sparse linear system.

### 2.3 Moving substances through the Fluid

Our solver enables us to compute the ambient fluid. However, we need to visualize the vector field. A substance, that is injected in the fluid and does not interact with it, will be advected by the vector field and diffuse at the same time. Let  $d \in C^2(\mathbb{R}^+ \times \Omega, \mathbb{R})$  denote the density field

## 2.4 Vorticity Confinement

of such a substance. The evolution of this scalar field is given by

$$\frac{\partial d}{\partial t} = -u \cdot \nabla a + \kappa \Delta - \alpha a + S$$

where  $\kappa$  is the diffusion constant,  $\alpha$  is the dissipation term and  $S$  is a source term. The dissipation term, which will be dropped in our modelling, describes the effect that kinetic energy is converted in thermal energy.

## 2.4 Vorticity Confinement

$$\begin{pmatrix} g & f & f \\ g & f & f \\ g & f & f \end{pmatrix}$$

## **3 Implementation**

## 4 Results

## 5 Extensions

## **6 Outlook**

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