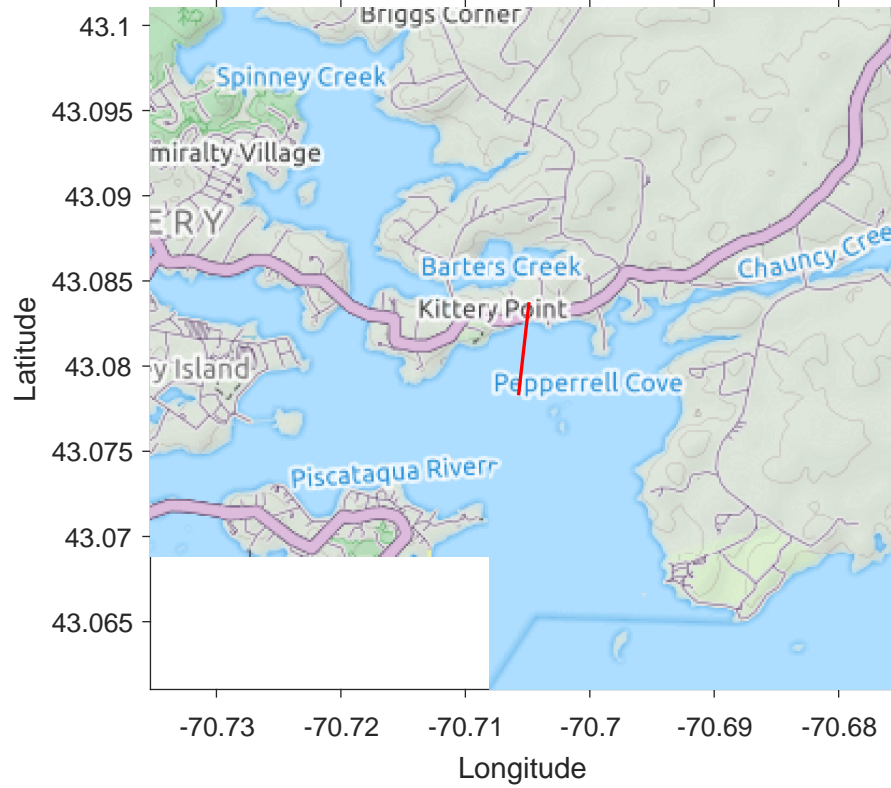
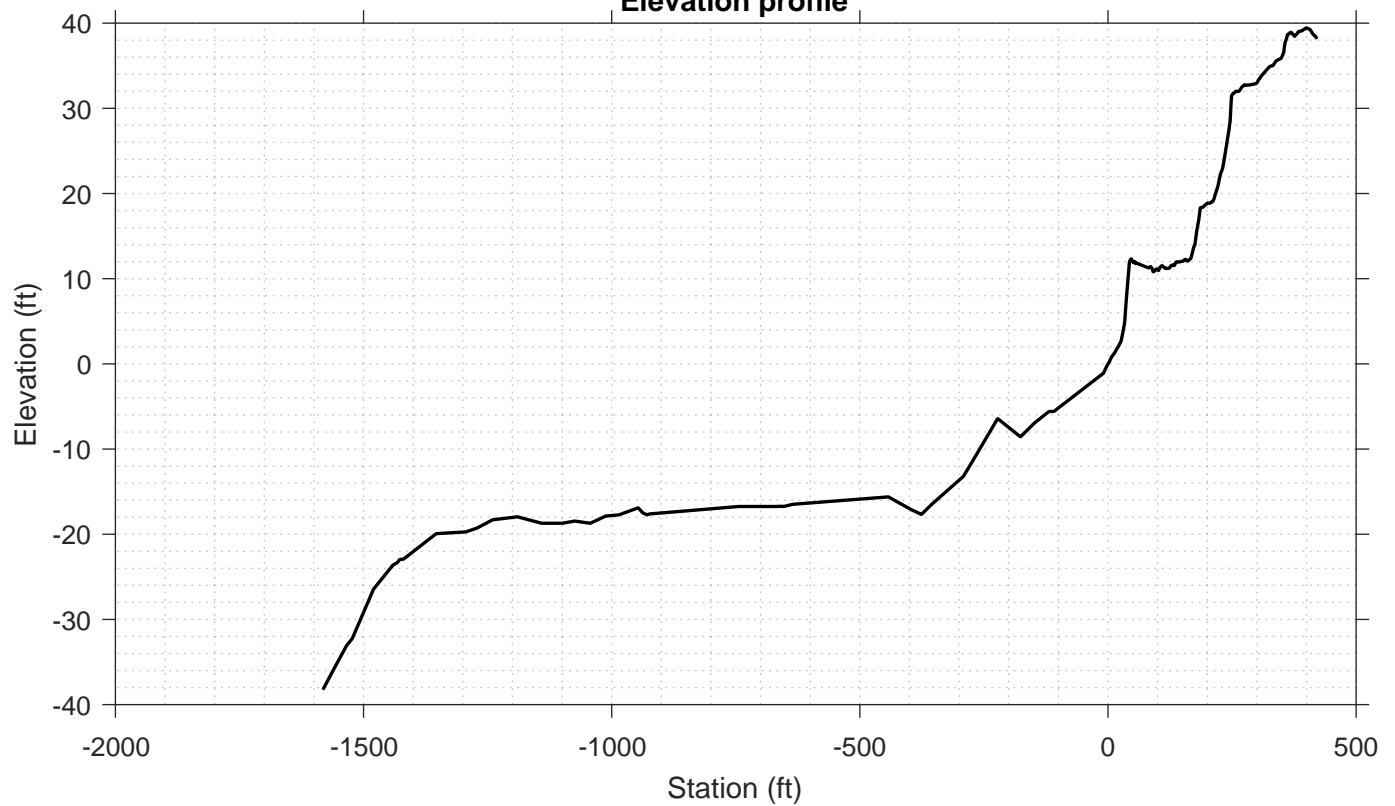


Transect Number: YK-06



Elevation profile



DATA LOG FOR TRANSECT ID: YK-06

PART 1: USER INPUT

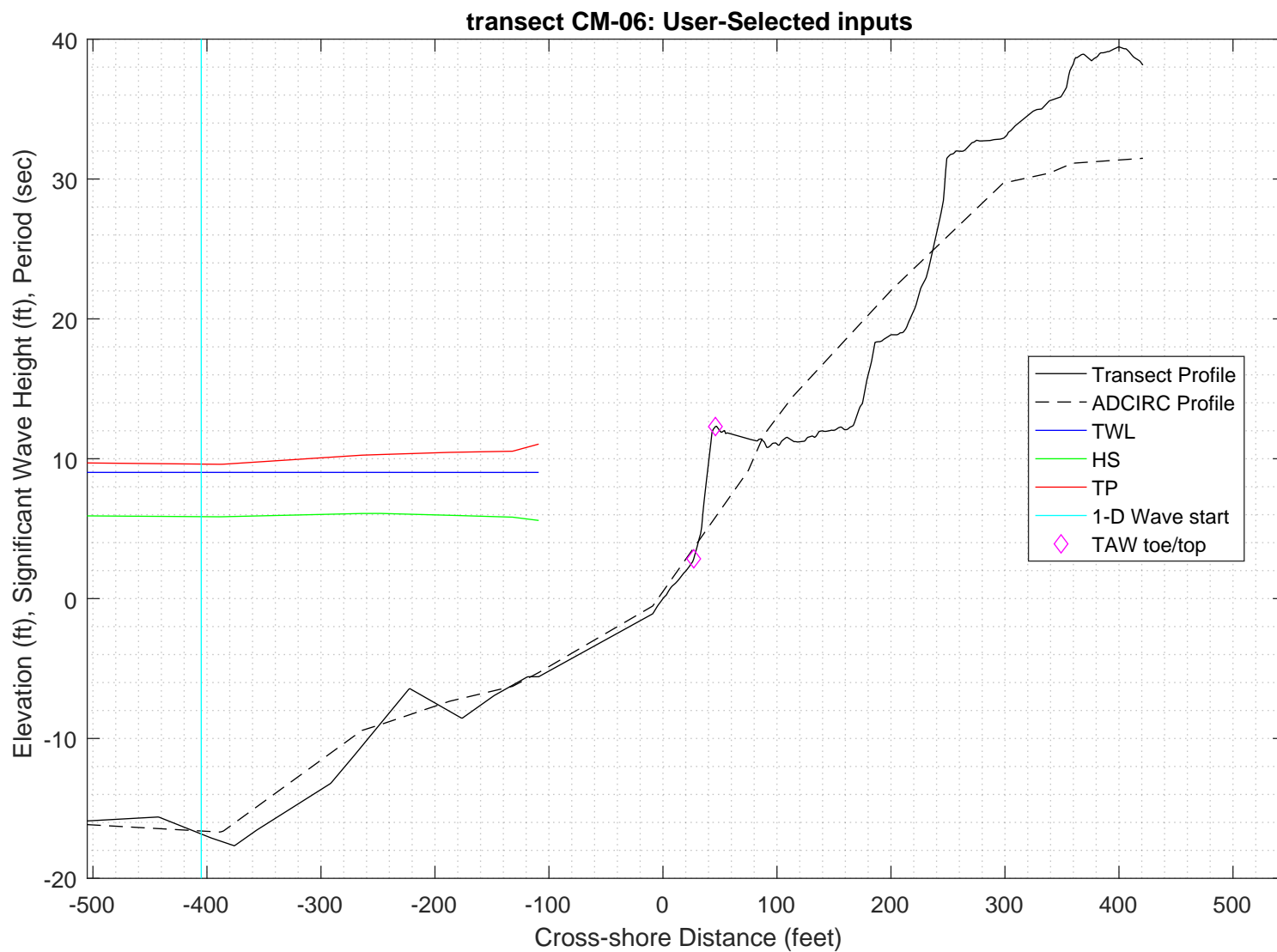
SWAN 1-D / WHAFIS input

station: -405 ft
LON: -70.7052 deg E
LAT: 43.0815 deg N
Bottom ELEV: -16.8296 ft-NAVD88
TWL: 9.0235 ft-NAVD88
HS: 5.8592 ft
TP: 9.6175 sec
Wave Direction bin: 90 deg CCW from East (90 deg sector)
Transect Direction: 81.199 deg CCW from East

TAW/RUNUP input

toe sta: 27 ft
toe elev: 2.8452 ft-NAVD88
top sta: 46 ft
top elev: 12.3021 ft-NAVD88
Wave and water level conditions at toe to be calculated in SWAN 1-D

PART 1 COMPLETE



PART 2: SWAN 1-D

swan input grid name: 2_swan/gridfiles/YK-06zmeters_xmeters.grd
swan file name: 2_swan/swanfiles/YK-06.swn
swan output name: 2_swan/swanfiles/YK-06.dat

Boundary Conditions:

TWL- 2.7504 meters
HS- 1.7859 meters
PER- 9.6175 seconds

Batch File: 2_swan/swanfiles/runswan.dat

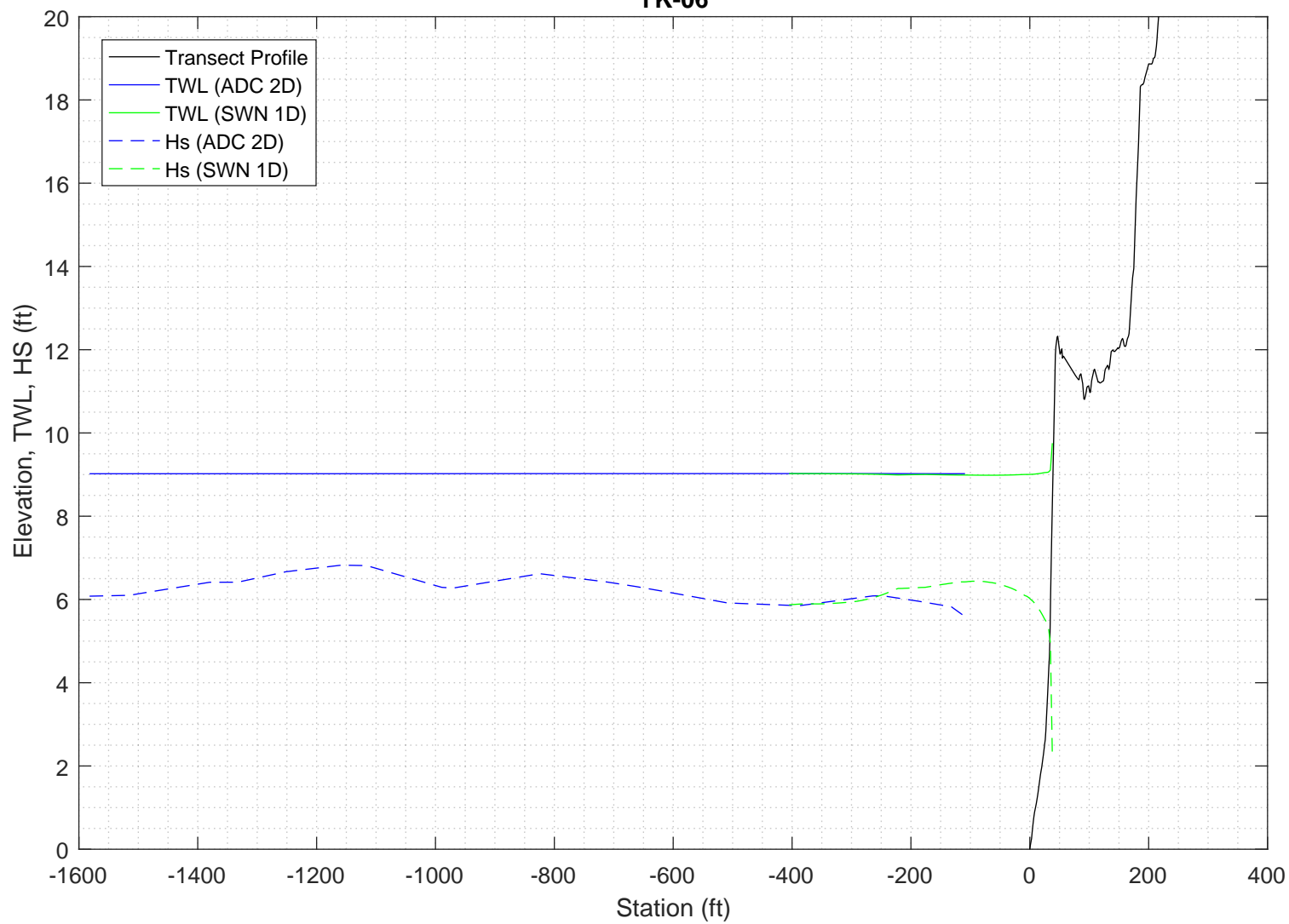
SWAN maximum additional wave setup: 0.73082 feet

SWAN output at toe:

SETUP- 0.028035 feet
HS- 5.4588 feet
PER- 9.7161 seconds

PART 2 COMPLETE

2-D ADCIRC+SWAN and SWAN 1-D results, Transect:
YK-06



Execution started at 20200206.151503

```

-----
                        SWAN
SIMULATION OF WAVES IN NEAR SHORE AREAS
VERSION NUMBER 41.20A
-----

```

PROJECT '2018FemaAppeal' '1'

'100-year Wind and Wave conditions'

! -- SET commands -----

SET DEPMIN=0.01 MAXMES=999 MAXERR=3 PWTAIL=4

SET LEVEL 0

SET CARTESIAN

! -- MODE commands -----

MODE STATIONARY ONED

!-- COORDINATES commands-----

COORDINATES CART

!

! -- computational (CGRID) grid commands -----

! xlenc=length of grid in meters

! mxc = number of mesh cells (one less than number of grid points)

!CGRID REGular [xpc] [ypc] [alpc] [xlenc] [ylenc] [mxc] [myc] &

! [CIRCle|SECTOR[dir1] [dir2]] [mdc] [flow] [fhigh] [msc]

CGRID REGULAR 0 0 0 135 0. 135 0 &
CIRCLE 36 0.03 0.8 30

Resolution in sigma-space: df/f = 0.1157

! -- READgrid ---- not used in 1-D mode -----

! -- INPgrid commands -----

!INPgrid BOTtom REGular [xpinp] [ypinp] [alpinp] [mxinp] [myinp] [dxinp] [dyinp]

!

INPGRID BOTTOM REGULAR 0 0 0 135 0 1 1

!READinp BOTtom [fac] 'fname1' [idla] [nhedf] [FREE|FORmat[form]|UNFormatted]

READ BOTTOM -1. '../gridfiles/YK-06zmeters_xmeters.grd' 1 0 FREE

!-----

! -- WIND [vel] [dir]

WIND 25.1 0

! -- BOUnd SHAPespec

BOUND SHAPE JONSWAP 3.3 PEAK DSPR POWER

! -- BOUndspec

! BOU SIDE W CCW CON FILE 'swanspec.txt' 1

BOUN SIDE W CCW CONSTANT PAR 1.7859 9.6175 0 2

!-- BOUndnest1 - optional for boundary from parent run

!-- BOUndnest2

!-- BOUndnest3

!-- INITial -- usest to specify initial values

!

!----- P H Y S I C S -----

!-- GEN1 [cf10] [cf20] [cf30] [cf40] [edmlpm] [cdrag] [umin] [cfpm]

!-- GEN2 [cf10] [cf20] [cf30] [cf40] [cf50] [cf60] [edmlpm] [cdrag] [umin] [cfpm]

```

GEN3 KOMEN

!   whitecapping ( on by default)
!-- WCAPPING KOMen [cds2] [stpm] [powst] [delta] [powk]

    WCAP KOM

!   quadruplet wave interactions
!-- QUADrupl [iquad] [lambda] [Cn14] [Csh1] [Csh2]

! -- BREaking CONstant [alpha] [gamma]

    BREAK    CON      1.      0.73

!-- FRIction JONswap CONstant [cfjon]

    FRIC      JONSWAP CON      0.038

!-- TRIad [itriad] [trfac] [cutfr]   [a] [b] [urcrit] [urslim]

! TRIAD      1      0.65    2.5    0.95 -0.75  0.2      0.01

    TRIAD

!-- VEGEtation [height] [diamtr] [nstems] [drag]

!-- MUD [layer] [rhom] [viscm]

!- LIMiter [ursell] [qb] deactivates quadruplets with Ursell number exceeds ursell

!-- OBSTacle -- not in 1-D

!-- SETUP [supcor]

    SETUP      0

!

! ----- N U M E R I C S -----

!

!-- PROP can use BBST or GSE instead of default

! -- NUMeric -- lots of options

!     NUM ACCUR npnts=100. stat 30

    NUMeric STOPC

!

! -----O U T P U T -----

!

!OUTPut OPTions "comment" (TABLE [field]) (BLOck [ndec] [len]) (SPEC [ndec])

OUTPUT OPTIONS '%' TABLE 16

$BLOCK 9 1000 SPEC 8

!CURve 'sname' [xpl] [ypl] <[int] [xp] [yp] >

CURVE 'curve' 0      0      135 135    0

!TABLE 'sname' < HEADER|NOHEADER|INDEXed > 'fname' <output parameters> (output time)

Table 'curve'   HEADER 'YK-06.dat' XP YP HSIGN TPS RTP TMM10 DIR &
DSPR DEPTH SETUP

!QUANTITY XP hexp=99999

!

!-----

COMPUTE STATIONARY

-----
COMPUTATIONAL PART OF SWAN
-----

One-dimensional mode of SWAN is activated
Gridresolution      : MXC      136 MYC      1
                   : MCGRD     137
                   : MSC       31 MDC      36
                   : MTC       1
                   : NSTATC    0 ITERMX   50
Propagation flags   : ITFRE    1 IREFR    1
Source term flags   : IBOT     1 ISURF    1
                   : IWCAP     1 IWIND    3
                   : ITRIAD    1 IQUAD    2
                   : IVEG      0 ITURBV   0

```

```

      : IMUD      0
Spatial step      : DX      0.1000E+01 DY      0.1000E+01
Spectral bin      : df/f    0.1157E+00 DDIR    0.1000E+02
Physical constants : GRAV    0.9810E+01 RHO     0.1025E+04
Wind input        : WSPEED   0.2510E+02 DIR     0.0000E+00
Tail parameters   : E(f)     0.4000E+01 E(k)    0.2500E+01
                  : A(f)     0.5000E+01 A(k)    0.3000E+01
Accuracy parameters : DREL    0.1000E-01 NPNTS   0.9950E+02
                  : DHABS    0.0000E+00 CURVAT   0.5000E-02
                  : GRWMX    0.1000E+00
Drying/flooding   : LEVEL    0.0000E+00 DEPMIN   0.1000E-01
The Cartesian convention for wind and wave directions is used
Scheme for geographic propagation is SORDUP
Scheme geogr. space : PROPSC      2 ICMAX      7
Scheme spectral space: CSS      0.5000E+00 CDD      0.5000E+00
Current is off
Quadruplets       : IQUAD      2
                  : LAMBDA    0.2500E+00 CNL4     0.3000E+08
                  : CSH1     0.5500E+01 CSH2     0.8330E+00
                  : CSH3     -0.1250E+01
Maximum Ursell nr for Snl4 : 0.1000E+02
Triads             : ITRIAD     1 TRFAC     0.8000E+00
                  : CUTFR     0.2500E+01 URCRI    0.2000E+00
Minimum Ursell nr for Snl3 : 0.1000E-01
JONSWAP ('73)      : GAMMA    0.3800E-01
Vegetation is off
Turbulence is off
Fluid mud is off
W-cap Komen ('84)  : EMPCOF (CDS2): 0.2360E-04
W-cap Komen ('84)  : APM (STPM) : 0.3020E-02
W-cap Komen ('84)  : POWST      : 0.2000E+01
W-cap Komen ('84)  : DELTA      : 0.1000E+01
W-cap Komen ('84)  : POWK       : 0.1000E+01
Wind drag is fit
Snyder/Komen wind input
Battjes&Janssen ('78): ALPHA    0.1000E+01 GAMMA    0.7300E+00
Set-up            : SUPCOR     0.0000E+00
Diffraction is off
Janssen ('89,'90) : ALPHA    0.1000E-01 KAPPA    0.4100E+00
Janssen ('89,'90) : RHOA     0.1280E+01 RHOW     0.1025E+04

1st and 2nd gen. wind: CF10     0.1880E+03 CF20     0.5900E+00
                   : CF30     0.1200E+00 CF40     0.2500E+03
                   : CF50     0.2300E-02 CF60     -0.2230E+00
                   : CF70     0.0000E+00 CF80     -0.5600E+00
                   : RHOAW    0.1249E-02 EDMMLPM  0.3600E-02
                   : CDRAG    0.1230E-02 UMIN     0.1000E+01
                   : LIM_PM    0.1300E+00

```

First guess by 2nd generation model flags for first iteration:

```

ITER      1 GRWMX      0.1000E+23 ALFA      0.0000E+00
IWIND      2 IWCAP      0 IQUAD      0
ITRIAD     1 IBOT      1 ISURF      1
IVEG       0 ITURBV     0 IMUD      0

```

```

iteration    1; sweep 1
iteration    1; sweep 2
iteration    1; sweep 3
iteration    1; sweep 4
not possible to compute, first iteration

```

Options given by user are activated for proceeding calculation:

```

ITER      2 GRWMX      0.1000E+00 ALFA      0.0000E+00
IWIND      3 IWCAP      1 IQUAD      2
ITRIAD     1 IBOT      1 ISURF      1
IVEG       0 ITURBV     0 IMUD      0

```

```

iteration    2; sweep 1
iteration    2; sweep 2
iteration    2; sweep 3
iteration    2; sweep 4
accuracy OK in 38.24 % of wet grid points ( 99.50 % required)

```

```

iteration    3; sweep 1
iteration    3; sweep 2
iteration    3; sweep 3
iteration    3; sweep 4
accuracy OK in 0.74 % of wet grid points ( 99.50 % required)

```

```

iteration    4; sweep 1
iteration    4; sweep 2
iteration    4; sweep 3
iteration    4; sweep 4
accuracy OK in 37.50 % of wet grid points ( 99.50 % required)

```

```

iteration    5; sweep 1
iteration    5; sweep 2
iteration    5; sweep 3
iteration    5; sweep 4
accuracy OK in 71.33 % of wet grid points ( 99.50 % required)

```

```

iteration    6; sweep 1
iteration    6; sweep 2
iteration    6; sweep 3

```


iteration 6; sweep 4
accuracy OK in 99.27 % of wet grid points (99.50 % required)

iteration 7; sweep 1
iteration 7; sweep 2
iteration 7; sweep 3
iteration 7; sweep 4
accuracy OK in 100.00 % of wet grid points (99.50 % required)

STOP

Run:1	Table:curve	SWAN version:41.20A								
Xp	Yp	Hsig	TPsmoo	RTpeak	Tm_10	Dir	Dspr	Depth	Setup	
[m]	[m]	[m]	[sec]	[sec]	[sec]	[degr]	[degr]	[m]	[m]	
0.	0.	1.78908	9.6469	10.0005	8.6896	0.000	31.7897	7.8797	-0.000347	
1.	0.	1.79043	9.6470	10.0005	8.6816	0.000	31.9430	7.9097	-0.000308	
2.	0.	1.79179	9.6471	10.0005	8.6738	0.000	32.0929	7.9397	-0.000269	
3.	0.	1.79264	9.6472	10.0005	8.6657	0.000	32.2211	7.9798	-0.000213	
4.	0.	1.79378	9.6473	10.0005	8.6584	0.000	32.3245	7.9998	-0.000186	
5.	0.	1.79469	9.6474	10.0005	8.6509	0.000	32.4325	8.0299	-0.000145	
6.	0.	1.79552	9.6474	10.0005	8.6436	0.000	32.5332	8.0599	-0.000103	
7.	0.	1.79615	9.6474	10.0005	8.6364	0.000	32.6160	8.0899	-0.000060	
8.	0.	1.79689	9.6475	10.0005	8.6296	0.000	32.6839	8.1100	-0.000032	
9.	0.	1.79644	9.6475	10.0005	8.6225	0.000	32.6402	8.1300	0.000000	
10.	0.	1.79679	9.6478	10.0005	8.6176	0.000	32.4729	8.0699	-0.000081	
11.	0.	1.79683	9.6481	10.0005	8.6125	0.000	32.2718	8.0098	-0.000162	
12.	0.	1.79642	9.6482	10.0005	8.6064	359.988	32.0494	7.9598	-0.000228	
13.	0.	1.79637	9.6485	10.0005	8.6010	359.993	31.8291	7.8997	-0.000312	
14.	0.	1.79625	9.6481	10.0005	8.5951	0.014	31.6006	7.8396	-0.000396	
15.	0.	1.79617	9.6483	10.0005	8.5890	359.995	31.3967	7.7895	-0.000469	
16.	0.	1.79654	9.6486	10.0005	8.5831	359.994	31.2196	7.7294	-0.000557	
17.	0.	1.79685	9.6490	10.0005	8.5767	359.994	31.0569	7.6794	-0.000632	
18.	0.	1.79730	9.6493	10.0005	8.5702	359.993	30.9165	7.6293	-0.000706	
19.	0.	1.79783	9.6497	10.0005	8.5634	359.993	30.7836	7.5792	-0.000781	
20.	0.	1.79843	9.6501	10.0005	8.5564	359.993	30.6531	7.5291	-0.000858	
21.	0.	1.79911	9.6505	10.0005	8.5491	359.993	30.5228	7.4791	-0.000937	
22.	0.	1.79975	9.6509	10.0005	8.5416	359.994	30.3836	7.4290	-0.001018	
23.	0.	1.80073	9.6514	10.0005	8.5342	359.994	30.2414	7.3689	-0.001119	
24.	0.	1.80157	9.6518	10.0005	8.5261	359.994	30.1083	7.3188	-0.001205	
25.	0.	1.80251	9.6523	10.0005	8.5178	359.994	29.9780	7.2687	-0.001294	
26.	0.	1.80352	9.6527	10.0005	8.5092	359.994	29.8487	7.2186	-0.001384	
27.	0.	1.80461	9.6532	10.0005	8.5004	359.994	29.7197	7.1685	-0.001477	
28.	0.	1.80576	9.6537	10.0005	8.4913	359.994	29.5912	7.1184	-0.001573	
29.	0.	1.80688	9.6542	10.0005	8.4819	359.994	29.4552	7.0683	-0.001671	
30.	0.	1.80838	9.6548	10.0005	8.4725	359.994	29.3162	7.0082	-0.001791	
31.	0.	1.80973	9.6553	10.0005	8.4623	359.994	29.1847	6.9581	-0.001895	
32.	0.	1.81119	9.6559	10.0005	8.4516	359.994	29.0555	6.9080	-0.002001	
33.	0.	1.81273	9.6565	10.0005	8.4405	359.994	28.9273	6.8579	-0.002109	
34.	0.	1.81418	9.6570	10.0005	8.4291	359.994	28.7828	6.8078	-0.002221	
35.	0.	1.81598	9.6577	10.0005	8.4179	359.994	28.5902	6.7376	-0.002381	
36.	0.	1.81870	9.6586	10.0005	8.4073	359.994	28.3713	6.6374	-0.002616	
37.	0.	1.82115	9.6594	10.0005	8.3954	359.995	28.1582	6.5472	-0.002832	
38.	0.	1.82404	9.6603	10.0005	8.3829	359.995	27.9365	6.4469	-0.003081	
39.	0.	1.82719	9.6612	10.0005	8.3692	359.995	27.7197	6.3467	-0.003340	
40.	0.	1.83019	9.6621	10.0005	8.3539	359.995	27.5039	6.2564	-0.003584	
41.	0.	1.83372	9.6631	10.0005	8.3378	359.995	27.2799	6.1561	-0.003866	
42.	0.	1.83744	9.6642	10.0005	8.3207	359.995	27.0517	6.0558	-0.004162	
43.	0.	1.84138	9.6654	10.0005	8.3023	359.995	26.8225	5.9555	-0.004471	
44.	0.	1.84553	9.6666	10.0005	8.2828	359.995	26.5924	5.8552	-0.004795	
45.	0.	1.84991	9.6678	10.0005	8.2620	359.996	26.3611	5.7549	-0.005134	
46.	0.	1.85459	9.6692	10.0005	8.2399	359.996	26.1386	5.6545	-0.005490	
47.	0.	1.85904	9.6705	10.0005	8.2162	359.997	25.9186	5.5642	-0.005825	
48.	0.	1.86413	9.6720	10.0005	8.1916	359.997	25.6908	5.4638	-0.006214	
49.	0.	1.86945	9.6735	10.0005	8.1657	359.998	25.4601	5.3634	-0.006622	
50.	0.	1.87500	9.6751	10.0005	8.1385	359.998	25.2288	5.2629	-0.007051	
51.	0.	1.88077	9.6767	10.0005	8.1098	359.999	24.9989	5.1625	-0.007499	
52.	0.	1.88676	9.6785	10.0005	8.0798	359.999	24.7810	5.0620	-0.007965	
53.	0.	1.89266	9.6803	10.0005	8.0495	359.998	24.5742	4.9616	-0.008435	
54.	0.	1.89868	9.6822	10.0005	8.0181	359.997	24.3697	4.8611	-0.008924	
55.	0.	1.90506	9.6841	10.0005	7.9857	359.993	24.2020	4.7606	-0.009428	
56.	0.	1.90953	9.6859	10.0005	7.9497	359.989	24.1529	4.7103	-0.009666	
57.	0.	1.90943	9.6872	10.0005	7.9079	359.987	24.2432	4.7606	-0.009359	

58.	0.	1.90967	9.6883	10.0005	7.8688	359.988	24.3702	4.8109	-0.009063
59.	0.	1.91061	9.6893	10.0005	7.8331	359.987	24.5128	4.8512	-0.008830
60.	0.	1.91116	9.6901	10.0005	7.7991	359.988	24.6741	4.9014	-0.008555
61.	0.	1.91169	9.6908	10.0005	7.7676	359.988	24.8318	4.9517	-0.008291
62.	0.	1.91270	9.6915	10.0005	7.7390	359.989	24.9891	4.9919	-0.008083
63.	0.	1.91330	9.6920	10.0005	7.7115	359.990	25.1592	5.0422	-0.007836
64.	0.	1.91385	9.6924	10.0005	7.6857	359.990	25.3216	5.0924	-0.007597
65.	0.	1.91485	9.6928	10.0005	7.6623	359.991	25.4811	5.1326	-0.007410
66.	0.	1.91537	9.6931	10.0005	7.6393	359.992	25.6394	5.1828	-0.007184
67.	0.	1.91634	9.6934	10.0005	7.6184	359.994	25.7955	5.2230	-0.007007
68.	0.	1.91694	9.6935	10.0005	7.5978	359.995	25.9634	5.2732	-0.006792
69.	0.	1.91713	9.6937	10.0005	7.5784	359.998	26.0852	5.3234	-0.006583
70.	0.	1.91795	9.6939	10.0005	7.5629	0.001	26.0846	5.3335	-0.006543
71.	0.	1.92037	9.6944	10.0005	7.5526	0.004	25.9815	5.2833	-0.006750
72.	0.	1.92282	9.6949	10.0005	7.5429	0.007	25.8328	5.2230	-0.007001
73.	0.	1.92516	9.6954	10.0005	7.5331	0.009	25.6719	5.1627	-0.007257
74.	0.	1.92752	9.6960	10.0005	7.5228	0.011	25.5094	5.1025	-0.007518
75.	0.	1.93002	9.6965	10.0005	7.5122	0.013	25.3580	5.0422	-0.007785
76.	0.	1.93214	9.6971	10.0005	7.5004	0.015	25.2129	4.9920	-0.008011
77.	0.	1.93466	9.6977	10.0005	7.4892	0.016	25.0671	4.9317	-0.008286
78.	0.	1.93729	9.6983	10.0005	7.4777	0.017	24.9278	4.8714	-0.008567
79.	0.	1.93962	9.6989	10.0005	7.4649	0.018	24.8086	4.8212	-0.008802
80.	0.	1.94142	9.6994	10.0005	7.4514	0.017	24.6968	4.7810	-0.008983
81.	0.	1.94368	9.7000	10.0005	7.4385	0.017	24.5765	4.7308	-0.009221
82.	0.	1.94598	9.7007	10.0005	7.4254	0.016	24.4609	4.6805	-0.009462
83.	0.	1.94775	9.7012	10.0005	7.4112	0.015	24.3460	4.6404	-0.009648
84.	0.	1.95008	9.7019	10.0005	7.3971	0.011	24.2296	4.5901	-0.009891
85.	0.	1.95202	9.7025	10.0005	7.3808	0.009	24.1125	4.5499	-0.010078
86.	0.	1.95436	9.7031	10.0005	7.3650	0.007	23.9846	4.4997	-0.010322
87.	0.	1.95681	9.7037	10.0005	7.3493	0.005	23.8869	4.4494	-0.010561
88.	0.	1.95737	9.7042	10.0005	7.3300	0.003	23.8440	4.4395	-0.010543
89.	0.	1.95743	9.7046	10.0005	7.3106	0.001	23.8281	4.4395	-0.010456
90.	0.	1.95735	9.7049	10.0005	7.2916	359.999	23.7947	4.4396	-0.010371
91.	0.	1.95829	9.7054	10.0005	7.2768	359.993	23.7118	4.4095	-0.010471
92.	0.	1.96017	9.7059	10.0005	7.2632	359.988	23.6014	4.3593	-0.010699
93.	0.	1.96110	9.7064	10.0005	7.2494	359.989	23.4838	4.3191	-0.010851
94.	0.	1.96232	9.7070	10.0005	7.2368	359.993	23.3611	4.2689	-0.011059
95.	0.	1.96238	9.7074	10.0005	7.2250	359.993	23.2386	4.2288	-0.011179
96.	0.	1.96303	9.7080	10.0005	7.2130	359.984	23.1125	4.1786	-0.011364
97.	0.	1.96265	9.7085	10.0005	7.2008	359.976	22.9883	4.1385	-0.011458
98.	0.	1.96231	9.7090	10.0005	7.1911	359.973	22.8621	4.0884	-0.011603
99.	0.	1.96105	9.7095	10.0005	7.1805	359.970	22.7359	4.0483	-0.011655
100.	0.	1.95994	9.7100	10.0005	7.1714	359.964	22.6021	3.9982	-0.011760
101.	0.	1.95792	9.7105	10.0005	7.1614	359.957	22.4787	3.9582	-0.011766
102.	0.	1.95611	9.7110	10.0005	7.1528	359.953	22.3528	3.9082	-0.011827
103.	0.	1.95387	9.7114	10.0005	7.1403	359.962	22.2271	3.8682	-0.011799
104.	0.	1.95208	9.7119	10.0005	7.1278	359.950	22.1021	3.8182	-0.011832
105.	0.	1.94940	9.7124	10.0005	7.1134	359.931	21.9763	3.7782	-0.011756
106.	0.	1.94703	9.7129	10.0005	7.0997	359.907	21.8471	3.7283	-0.011740
107.	0.	1.94363	9.7134	10.0005	7.0843	359.882	21.7183	3.6884	-0.011604
108.	0.	1.94032	9.7139	10.0005	7.0706	359.856	21.5908	3.6385	-0.011519
109.	0.	1.93579	9.7143	10.0005	7.0559	359.833	21.4638	3.5987	-0.011300
110.	0.	1.93153	9.7148	10.0005	7.0419	359.810	21.3341	3.5489	-0.011140
111.	0.	1.92624	9.7153	10.0005	7.0256	359.785	21.2056	3.5092	-0.010845
112.	0.	1.92178	9.7158	10.0005	7.0073	359.770	21.0767	3.4594	-0.010627
113.	0.	1.91633	9.7163	10.0005	6.9861	359.761	20.9487	3.4197	-0.010271
114.	0.	1.91117	9.7168	10.0005	6.9653	359.754	20.8196	3.3700	-0.009972
115.	0.	1.90473	9.7172	10.0005	6.9427	359.752	20.6911	3.3305	-0.009518
116.	0.	1.89832	9.7178	10.0005	6.9219	359.758	20.5601	3.2809	-0.009115
117.	0.	1.89021	9.7182	10.0005	6.9011	359.764	20.4324	3.2415	-0.008532
118.	0.	1.88235	9.7187	10.0005	6.8810	359.774	20.2988	3.1920	-0.008012
119.	0.	1.87333	9.7191	10.0005	6.8584	359.788	20.1628	3.1527	-0.007329
120.	0.	1.86546	9.7195	10.0005	6.8306	359.818	19.9975	3.1033	-0.006741
121.	0.	1.85716	9.7199	10.0005	6.8089	359.861	19.7548	3.0337	-0.006303
122.	0.	1.85153	9.7204	10.0005	6.7956	359.914	19.4396	2.9035	-0.006475

123.	0.	1.84153	9.7206	10.0005	6.7776	359.969	19.1222	2.7939	-0.006126
124.	0.	1.82808	9.7207	10.0005	6.7558	0.024	18.7906	2.6946	-0.005366
125.	0.	1.81573	9.7205	10.0005	6.7259	0.066	18.4242	2.5752	-0.004753
126.	0.	1.80032	9.7199	10.0005	6.6899	0.135	18.0929	2.4663	-0.003698
127.	0.	1.77916	9.7190	10.0005	6.6430	0.212	17.7766	2.3983	-0.001662
128.	0.	1.76102	9.7164	10.0005	6.5887	0.347	17.4364	2.3000	-0.000013
129.	0.	1.73827	9.7148	10.0005	6.5419	0.485	17.0927	2.2021	0.002124
130.	0.	1.71347	9.7149	10.0005	6.4866	0.664	16.7218	2.1046	0.004642
131.	0.	1.68625	9.7155	10.0005	6.4302	0.881	16.2321	1.9974	0.007387
132.	0.	1.66384	9.7161	10.0005	6.3917	1.147	15.4725	1.7985	0.008545
133.	0.	1.62453	9.7198	10.0005	6.3902	1.125	14.2885	1.4907	0.010662
134.	0.	1.50876	9.7350	10.0005	6.5137	0.565	12.6585	1.0255	0.025526
135.	0.	0.68625	9.9861	10.0005	7.9534	356.696	15.3298	0.4528	0.222755

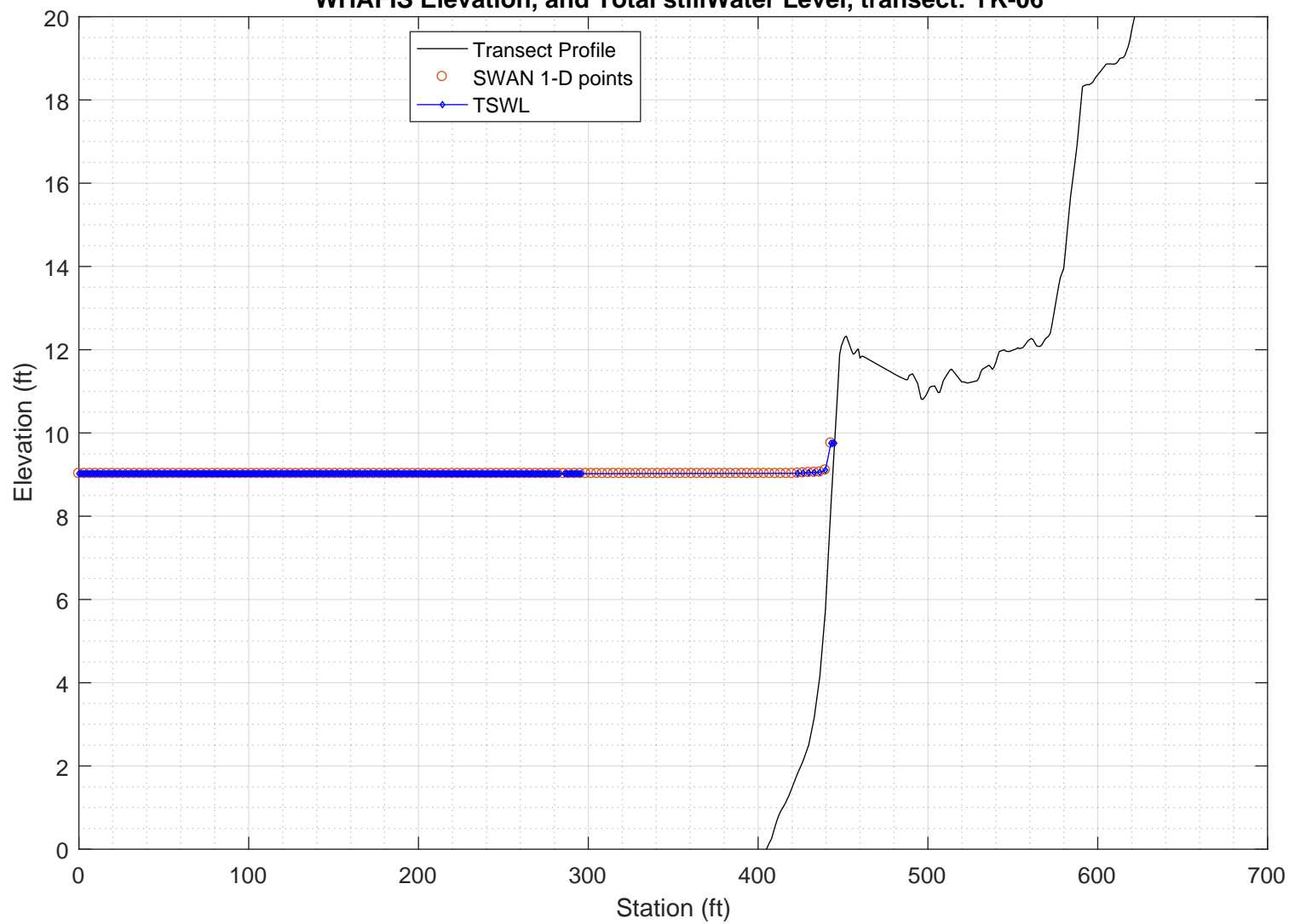
PART 3: WHAFIS

WHAFIS input: YK-06.dat

WHAFIS output: YK-06.out

PART 3 COMPLETE

WHAFIS Elevation, and Total stillWater Level, transect: YK-06



WAVE HEIGHT COMPUTATIONS FOR FLOOD INSURANCE STUDIES (WHAFIS VERSION 4.0G, 08_2007)

Executed on: Thu Feb 6 16:14:34 2020

Input file: C:\Users\shayward\Desktop\Kittery\T2\3_whafis\whafis4\YK-06.dat

Output file: C:\Users\shayward\Desktop\Kittery\T2\3_whafis\whafis4\YK-06.out

header

THIS IS A 100-YEAR CASE

THE FOLLOWING NON-DEFAULT WIND SPEEDS ARE BEING USED

WINDIF 56.14 WINDOF 56.14 WINDVH 60.00

PART1 INPUT

IE	0.000	-16.829	1.000	1.000	9.024	9.375	9.618	56.140	-0.033	0.000
OF	1.000	-16.862	0.000	9.024	0.000	0.000	0.000	0.000	-0.032	0.000
OF	2.000	-16.894	0.000	9.024	0.000	0.000	0.000	0.000	-0.032	0.000
OF	3.000	-16.927	0.000	9.024	0.000	0.000	0.000	0.000	-0.032	0.000
OF	4.000	-16.959	0.000	9.024	0.000	0.000	0.000	0.000	-0.032	0.000
OF	5.000	-16.992	0.000	9.024	0.000	0.000	0.000	0.000	-0.032	0.000
OF	6.000	-17.024	0.000	9.024	0.000	0.000	0.000	0.000	-0.032	0.000
OF	7.000	-17.056	0.000	9.024	0.000	0.000	0.000	0.000	-0.032	0.000
OF	8.000	-17.089	0.000	9.024	0.000	0.000	0.000	0.000	-0.032	0.000
OF	9.000	-17.120	0.000	9.024	0.000	0.000	0.000	0.000	-0.030	0.000
OF	10.000	-17.148	0.000	9.024	0.000	0.000	0.000	0.000	-0.027	0.000
OF	11.000	-17.175	0.000	9.024	0.000	0.000	0.000	0.000	-0.027	0.000
OF	12.000	-17.203	0.000	9.024	0.000	0.000	0.000	0.000	-0.027	0.000
OF	13.000	-17.230	0.000	9.024	0.000	0.000	0.000	0.000	-0.027	0.000
OF	14.000	-17.258	0.000	9.024	0.000	0.000	0.000	0.000	-0.027	0.000
OF	15.000	-17.285	0.000	9.024	0.000	0.000	0.000	0.000	-0.027	0.000
OF	16.000	-17.313	0.000	9.024	0.000	0.000	0.000	0.000	-0.027	0.000
OF	17.000	-17.340	0.000	9.024	0.000	0.000	0.000	0.000	-0.027	0.000
OF	18.000	-17.368	0.000	9.024	0.000	0.000	0.000	0.000	-0.027	0.000
OF	19.000	-17.395	0.000	9.024	0.000	0.000	0.000	0.000	-0.027	0.000
OF	20.000	-17.423	0.000	9.024	0.000	0.000	0.000	0.000	-0.027	0.000
OF	21.000	-17.450	0.000	9.024	0.000	0.000	0.000	0.000	-0.027	0.000
OF	22.000	-17.478	0.000	9.024	0.000	0.000	0.000	0.000	-0.027	0.000
OF	23.000	-17.505	0.000	9.024	0.000	0.000	0.000	0.000	-0.027	0.000
OF	24.000	-17.533	0.000	9.024	0.000	0.000	0.000	0.000	-0.027	0.000
OF	25.000	-17.560	0.000	9.024	0.000	0.000	0.000	0.000	-0.027	0.000
OF	26.000	-17.588	0.000	9.024	0.000	0.000	0.000	0.000	-0.027	0.000
OF	27.000	-17.615	0.000	9.024	0.000	0.000	0.000	0.000	-0.027	0.000
OF	28.000	-17.643	0.000	9.024	0.000	0.000	0.000	0.000	-0.027	0.000
OF	29.000	-17.670	0.000	9.024	0.000	0.000	0.000	0.000	0.011	0.000
OF	30.000	-17.621	0.000	9.024	0.000	0.000	0.000	0.000	0.053	0.000
OF	31.000	-17.564	0.000	9.024	0.000	0.000	0.000	0.000	0.058	0.000
OF	32.000	-17.506	0.000	9.024	0.000	0.000	0.000	0.000	0.058	0.000
OF	33.000	-17.449	0.000	9.024	0.000	0.000	0.000	0.000	0.057	0.000
OF	34.000	-17.392	0.000	9.024	0.000	0.000	0.000	0.000	0.058	0.000
OF	35.000	-17.334	0.000	9.024	0.000	0.000	0.000	0.000	0.058	0.000
OF	36.000	-17.277	0.000	9.024	0.000	0.000	0.000	0.000	0.058	0.000
OF	37.000	-17.219	0.000	9.024	0.000	0.000	0.000	0.000	0.058	0.000
OF	38.000	-17.162	0.000	9.024	0.000	0.000	0.000	0.000	0.057	0.000
OF	39.000	-17.105	0.000	9.024	0.000	0.000	0.000	0.000	0.058	0.000
OF	40.000	-17.047	0.000	9.024	0.000	0.000	0.000	0.000	0.058	0.000
OF	41.000	-16.990	0.000	9.024	0.000	0.000	0.000	0.000	0.058	0.000
OF	42.000	-16.932	0.000	9.024	0.000	0.000	0.000	0.000	0.058	0.000
OF	43.000	-16.875	0.000	9.024	0.000	0.000	0.000	0.000	0.057	0.000
OF	44.000	-16.818	0.000	9.024	0.000	0.000	0.000	0.000	0.058	0.000
OF	45.000	-16.760	0.000	9.024	0.000	0.000	0.000	0.000	0.058	0.000
OF	46.000	-16.703	0.000	9.024	0.000	0.000	0.000	0.000	0.058	0.000
OF	47.000	-16.645	0.000	9.024	0.000	0.000	0.000	0.000	0.058	0.000
OF	48.000	-16.588	0.000	9.024	0.000	0.000	0.000	0.000	0.056	0.000
OF	49.000	-16.533	0.000	9.024	0.000	0.000	0.000	0.000	0.054	0.000
OF	50.000	-16.481	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	51.000	-16.430	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	52.000	-16.378	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	53.000	-16.327	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	54.000	-16.275	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	55.000	-16.224	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	56.000	-16.172	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	57.000	-16.121	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	58.000	-16.069	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	59.000	-16.018	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	60.000	-15.966	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	61.000	-15.915	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	62.000	-15.863	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	63.000	-15.812	0.000	9.024	0.000	0.000	0.000	0.000	0.051	0.000
OF	64.000	-15.761	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	65.000	-15.709	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	66.000	-15.658	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	67.000	-15.606	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	68.000	-15.555	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	69.000	-15.503	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	70.000	-15.452	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	71.000	-15.400	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	72.000	-15.349	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	73.000	-15.297	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	74.000	-15.246	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	75.000	-15.194	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	76.000	-15.143	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	77.000	-15.091	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	78.000	-15.040	0.000	9.024	0.000	0.000	0.000	0.000	0.051	0.000
OF	79.000	-14.989	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	80.000	-14.937	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	81.000	-14.886	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	82.000	-14.834	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	83.000	-14.783	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	84.000	-14.731	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	85.000	-14.680	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	86.000	-14.628	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	87.000	-14.577	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	88.000	-14.525	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	89.000	-14.474	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	90.000	-14.422	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	91.000	-14.371	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	92.000	-14.319	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	93.000	-14.268	0.000	9.024	0.000	0.000	0.000	0.000	0.051	0.000
OF	94.000	-14.217	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	95.000	-14.165	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	96.000	-14.114	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	97.000	-14.062	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	98.000	-14.011	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	99.000	-13.959	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	100.000	-13.908	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000

OF	101.000	-13.856	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	102.000	-13.805	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	103.000	-13.753	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	104.000	-13.702	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	105.000	-13.650	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	106.000	-13.599	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	107.000	-13.547	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	108.000	-13.496	0.000	9.024	0.000	0.000	0.000	0.000	0.051	0.000
OF	109.000	-13.445	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	110.000	-13.393	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	111.000	-13.342	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	112.000	-13.290	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
OF	113.000	-13.239	0.000	9.024	0.000	0.000	0.000	0.000	0.062	0.000
OF	114.000	-13.167	0.000	9.024	0.000	0.000	0.000	0.000	0.084	0.000
OF	115.000	-13.071	0.000	9.024	0.000	0.000	0.000	0.000	0.097	0.000
OF	116.000	-12.974	0.000	9.024	0.000	0.000	0.000	0.000	0.097	0.000
OF	117.000	-12.877	0.000	9.024	0.000	0.000	0.000	0.000	0.097	0.000
OF	118.000	-12.780	0.000	9.024	0.000	0.000	0.000	0.000	0.097	0.000
OF	119.000	-12.684	0.000	9.024	0.000	0.000	0.000	0.000	0.097	0.000
OF	120.000	-12.587	0.000	9.024	0.000	0.000	0.000	0.000	0.097	0.000
OF	121.000	-12.490	0.000	9.024	0.000	0.000	0.000	0.000	0.097	0.000
OF	122.000	-12.393	0.000	9.024	0.000	0.000	0.000	0.000	0.097	0.000
OF	123.000	-12.297	0.000	9.024	0.000	0.000	0.000	0.000	0.097	0.000
OF	124.000	-12.200	0.000	9.024	0.000	0.000	0.000	0.000	0.097	0.000
OF	125.000	-12.103	0.000	9.024	0.000	0.000	0.000	0.000	0.097	0.000
OF	126.000	-12.007	0.000	9.024	0.000	0.000	0.000	0.000	0.097	0.000
OF	127.000	-11.910	0.000	9.024	0.000	0.000	0.000	0.000	0.097	0.000
OF	128.000	-11.813	0.000	9.024	0.000	0.000	0.000	0.000	0.097	0.000
OF	129.000	-11.716	0.000	9.024	0.000	0.000	0.000	0.000	0.097	0.000
OF	130.000	-11.620	0.000	9.024	0.000	0.000	0.000	0.000	0.097	0.000
OF	131.000	-11.523	0.000	9.024	0.000	0.000	0.000	0.000	0.097	0.000
OF	132.000	-11.426	0.000	9.024	0.000	0.000	0.000	0.000	0.097	0.000
OF	133.000	-11.329	0.000	9.024	0.000	0.000	0.000	0.000	0.097	0.000
OF	134.000	-11.232	0.000	9.024	0.000	0.000	0.000	0.000	0.097	0.000
OF	135.000	-11.134	0.000	9.024	0.000	0.000	0.000	0.000	0.098	0.000
OF	136.000	-11.035	0.000	9.024	0.000	0.000	0.000	0.000	0.099	0.000
OF	137.000	-10.936	0.000	9.024	0.000	0.000	0.000	0.000	0.099	0.000
OF	138.000	-10.837	0.000	9.024	0.000	0.000	0.000	0.000	0.099	0.000
OF	139.000	-10.738	0.000	9.024	0.000	0.000	0.000	0.000	0.099	0.000
OF	140.000	-10.639	0.000	9.024	0.000	0.000	0.000	0.000	0.099	0.000
OF	141.000	-10.540	0.000	9.024	0.000	0.000	0.000	0.000	0.099	0.000
OF	142.000	-10.441	0.000	9.024	0.000	0.000	0.000	0.000	0.099	0.000
OF	143.000	-10.342	0.000	9.024	0.000	0.000	0.000	0.000	0.099	0.000
OF	144.000	-10.243	0.000	9.024	0.000	0.000	0.000	0.000	0.099	0.000
OF	145.000	-10.144	0.000	9.024	0.000	0.000	0.000	0.000	0.099	0.000
OF	146.000	-10.045	0.000	9.024	0.000	0.000	0.000	0.000	0.098	0.000
OF	147.000	-9.947	0.000	9.024	0.000	0.000	0.000	0.000	0.098	0.000
OF	148.000	-9.848	0.000	9.024	0.000	0.000	0.000	0.000	0.099	0.000
OF	149.000	-9.749	0.000	9.024	0.000	0.000	0.000	0.000	0.099	0.000
OF	150.000	-9.650	0.000	9.024	0.000	0.000	0.000	0.000	0.099	0.000
OF	151.000	-9.551	0.000	9.024	0.000	0.000	0.000	0.000	0.099	0.000
OF	152.000	-9.452	0.000	9.024	0.000	0.000	0.000	0.000	0.099	0.000
OF	153.000	-9.353	0.000	9.024	0.000	0.000	0.000	0.000	0.099	0.000
OF	154.000	-9.254	0.000	9.024	0.000	0.000	0.000	0.000	0.099	0.000
OF	155.000	-9.156	0.000	9.024	0.000	0.000	0.000	0.000	0.099	0.000
OF	156.000	-9.057	0.000	9.024	0.000	0.000	0.000	0.000	0.099	0.000
OF	157.000	-8.958	0.000	9.024	0.000	0.000	0.000	0.000	0.099	0.000
OF	158.000	-8.859	0.000	9.024	0.000	0.000	0.000	0.000	0.099	0.000
OF	159.000	-8.760	0.000	9.024	0.000	0.000	0.000	0.000	0.099	0.000
OF	160.000	-8.661	0.000	9.024	0.000	0.000	0.000	0.000	0.099	0.000
OF	161.000	-8.562	0.000	9.024	0.000	0.000	0.000	0.000	0.099	0.000
OF	162.000	-8.463	0.000	9.024	0.000	0.000	0.000	0.000	0.099	0.000
OF	163.000	-8.364	0.000	9.023	0.000	0.000	0.000	0.000	0.099	0.000
OF	164.000	-8.265	0.000	9.023	0.000	0.000	0.000	0.000	0.099	0.000
OF	165.000	-8.166	0.000	9.023	0.000	0.000	0.000	0.000	0.099	0.000
OF	166.000	-8.067	0.000	9.023	0.000	0.000	0.000	0.000	0.099	0.000
OF	167.000	-7.968	0.000	9.023	0.000	0.000	0.000	0.000	0.099	0.000
OF	168.000	-7.870	0.000	9.023	0.000	0.000	0.000	0.000	0.099	0.000
OF	169.000	-7.771	0.000	9.023	0.000	0.000	0.000	0.000	0.099	0.000
OF	170.000	-7.672	0.000	9.023	0.000	0.000	0.000	0.000	0.099	0.000
OF	171.000	-7.573	0.000	9.023	0.000	0.000	0.000	0.000	0.099	0.000
OF	172.000	-7.474	0.000	9.023	0.000	0.000	0.000	0.000	0.099	0.000
OF	173.000	-7.375	0.000	9.023	0.000	0.000	0.000	0.000	0.099	0.000
OF	174.000	-7.276	0.000	9.023	0.000	0.000	0.000	0.000	0.099	0.000
OF	175.000	-7.177	0.000	9.023	0.000	0.000	0.000	0.000	0.099	0.000
OF	176.000	-7.078	0.000	9.023	0.000	0.000	0.000	0.000	0.099	0.000
OF	177.000	-6.979	0.000	9.023	0.000	0.000	0.000	0.000	0.099	0.000
OF	178.000	-6.880	0.000	9.023	0.000	0.000	0.000	0.000	0.099	0.000
OF	179.000	-6.781	0.000	9.023	0.000	0.000	0.000	0.000	0.099	0.000
OF	180.000	-6.682	0.000	9.023	0.000	0.000	0.000	0.000	0.099	0.000
OF	181.000	-6.583	0.000	9.023	0.000	0.000	0.000	0.000	0.099	0.000
OF	182.000	-6.485	0.000	9.023	0.000	0.000	0.000	0.000	0.073	0.000
OF	183.000	-6.437	0.000	9.023	0.000	0.000	0.000	0.000	0.001	0.000
OF	184.000	-6.483	0.000	9.023	0.000	0.000	0.000	0.000	-0.047	0.000
OF	185.000	-6.530	0.000	9.023	0.000	0.000	0.000	0.000	-0.047	0.000
OF	186.000	-6.576	0.000	9.023	0.000	0.000	0.000	0.000	-0.047	0.000
OF	187.000	-6.623	0.000	9.023	0.000	0.000	0.000	0.000	-0.047	0.000
OF	188.000	-6.669	0.000	9.023	0.000	0.000	0.000	0.000	-0.047	0.000
OF	189.000	-6.716	0.000	9.023	0.000	0.000	0.000	0.000	-0.047	0.000
OF	190.000	-6.763	0.000	9.023	0.000	0.000	0.000	0.000	-0.047	0.000
OF	191.000	-6.809	0.000	9.023	0.000	0.000	0.000	0.000	-0.047	0.000
OF	192.000	-6.856	0.000	9.023	0.000	0.000	0.000	0.000	-0.047	0.000
OF	193.000	-6.902	0.000	9.023	0.000	0.000	0.000	0.000	-0.047	0.000
OF	194.000	-6.949	0.000	9.023	0.000	0.000	0.000	0.000	-0.047	0.000
OF	195.000	-6.995	0.000	9.023	0.000	0.000	0.000	0.000	-0.047	0.000
OF	196.000	-7.042	0.000	9.023	0.000	0.000	0.000	0.000	-0.047	0.000
OF	197.000	-7.089	0.000	9.023	0.000	0.000	0.000	0.000	-0.047	0.000
OF	198.000	-7.135	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	199.000	-7.182	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	200.000	-7.228	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	201.000	-7.275	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	202.000	-7.321	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	203.000	-7.368	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	204.000	-7.414	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	205.000	-7.461	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	206.000	-7.508	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	207.000	-7.554	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	208.000	-7.601	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	209.000	-7.647	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	210.000	-7.694	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000

OF	211.000	-7.740	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	212.000	-7.787	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	213.000	-7.833	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	214.000	-7.880	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	215.000	-7.926	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	216.000	-7.973	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	217.000	-8.020	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	218.000	-8.066	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	219.000	-8.113	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	220.000	-8.159	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	221.000	-8.206	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	222.000	-8.252	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	223.000	-8.299	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	224.000	-8.345	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	225.000	-8.392	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	226.000	-8.439	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	227.000	-8.485	0.000	9.022	0.000	0.000	0.000	0.000	-0.047	0.000
OF	228.000	-8.532	0.000	9.022	0.000	0.000	0.000	0.000	-0.030	0.000
OF	229.000	-8.545	0.000	9.022	0.000	0.000	0.000	0.000	0.022	0.000
OF	230.000	-8.488	0.000	9.021	0.000	0.000	0.000	0.000	0.058	0.000
OF	231.000	-8.430	0.000	9.021	0.000	0.000	0.000	0.000	0.058	0.000
OF	232.000	-8.372	0.000	9.021	0.000	0.000	0.000	0.000	0.058	0.000
OF	233.000	-8.314	0.000	9.021	0.000	0.000	0.000	0.000	0.058	0.000
OF	234.000	-8.257	0.000	9.021	0.000	0.000	0.000	0.000	0.058	0.000
OF	235.000	-8.199	0.000	9.021	0.000	0.000	0.000	0.000	0.058	0.000
OF	236.000	-8.141	0.000	9.021	0.000	0.000	0.000	0.000	0.058	0.000
OF	237.000	-8.083	0.000	9.021	0.000	0.000	0.000	0.000	0.058	0.000
OF	238.000	-8.025	0.000	9.021	0.000	0.000	0.000	0.000	0.058	0.000
OF	239.000	-7.968	0.000	9.021	0.000	0.000	0.000	0.000	0.058	0.000
OF	240.000	-7.910	0.000	9.021	0.000	0.000	0.000	0.000	0.058	0.000
OF	241.000	-7.852	0.000	9.021	0.000	0.000	0.000	0.000	0.058	0.000
OF	242.000	-7.794	0.000	9.021	0.000	0.000	0.000	0.000	0.058	0.000
OF	243.000	-7.736	0.000	9.021	0.000	0.000	0.000	0.000	0.058	0.000
OF	244.000	-7.678	0.000	9.021	0.000	0.000	0.000	0.000	0.058	0.000
OF	245.000	-7.621	0.000	9.021	0.000	0.000	0.000	0.000	0.058	0.000
OF	246.000	-7.563	0.000	9.021	0.000	0.000	0.000	0.000	0.058	0.000
OF	247.000	-7.505	0.000	9.021	0.000	0.000	0.000	0.000	0.058	0.000
OF	248.000	-7.447	0.000	9.021	0.000	0.000	0.000	0.000	0.058	0.000
OF	249.000	-7.389	0.000	9.021	0.000	0.000	0.000	0.000	0.058	0.000
OF	250.000	-7.332	0.000	9.021	0.000	0.000	0.000	0.000	0.058	0.000
OF	251.000	-7.274	0.000	9.021	0.000	0.000	0.000	0.000	0.058	0.000
OF	252.000	-7.216	0.000	9.021	0.000	0.000	0.000	0.000	0.058	0.000
OF	253.000	-7.158	0.000	9.021	0.000	0.000	0.000	0.000	0.058	0.000
OF	254.000	-7.100	0.000	9.021	0.000	0.000	0.000	0.000	0.058	0.000
OF	255.000	-7.043	0.000	9.021	0.000	0.000	0.000	0.000	0.058	0.000
OF	256.000	-6.985	0.000	9.021	0.000	0.000	0.000	0.000	0.057	0.000
OF	257.000	-6.928	0.000	9.021	0.000	0.000	0.000	0.000	0.051	0.000
OF	258.000	-6.882	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	259.000	-6.836	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	260.000	-6.790	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	261.000	-6.745	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	262.000	-6.699	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	263.000	-6.653	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	264.000	-6.607	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	265.000	-6.561	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	266.000	-6.515	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	267.000	-6.470	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	268.000	-6.424	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	269.000	-6.378	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	270.000	-6.332	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	271.000	-6.286	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	272.000	-6.240	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	273.000	-6.194	0.000	9.020	0.000	0.000	0.000	0.000	0.046	0.000
OF	274.000	-6.149	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	275.000	-6.103	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	276.000	-6.057	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	277.000	-6.011	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	278.000	-5.965	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	279.000	-5.920	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	280.000	-5.874	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	281.000	-5.828	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	282.000	-5.782	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	283.000	-5.736	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	286.000	-5.599	0.000	9.021	0.000	0.000	0.000	0.000	0.037	0.000
OF	287.000	-5.588	0.000	9.021	0.000	0.000	0.000	0.000	0.005	0.000
OF	288.000	-5.588	0.000	9.022	0.000	0.000	0.000	0.000	0.001	0.000
OF	289.000	-5.587	0.000	9.022	0.000	0.000	0.000	0.000	0.001	0.000
OF	290.000	-5.587	0.000	9.022	0.000	0.000	0.000	0.000	0.001	0.000
OF	291.000	-5.586	0.000	9.022	0.000	0.000	0.000	0.000	0.001	0.000
OF	292.000	-5.586	0.000	9.022	0.000	0.000	0.000	0.000	0.001	0.000
OF	293.000	-5.585	0.000	9.022	0.000	0.000	0.000	0.000	0.001	0.000
OF	294.000	-5.584	0.000	9.022	0.000	0.000	0.000	0.000	0.001	0.000
OF	295.000	-5.584	0.000	9.022	0.000	0.000	0.000	0.000	0.001	0.000
OF	296.000	-5.583	0.000	9.022	0.000	0.000	0.000	0.000	0.058	0.000
IF	423.200	1.818	0.000	9.031	0.000	0.000	0.000	0.000	0.059	0.000
IF	426.500	2.124	0.000	9.039	0.000	0.000	0.000	0.000	0.103	0.000
IF	429.800	2.501	0.000	9.048	0.000	0.000	0.000	0.000	0.158	0.000
IF	433.100	3.166	0.000	9.052	0.000	0.000	0.000	0.000	0.250	0.000
IF	436.400	4.152	0.000	9.059	0.000	0.000	0.000	0.000	0.396	0.000
IF	439.600	5.739	0.000	9.107	0.000	0.000	0.000	0.000	0.634	0.000
IF	442.900	8.273	0.000	9.754	0.000	0.000	0.000	0.000	0.748	0.000
IF	444.000	9.031	0.000	9.754	0.000	0.000	0.000	0.000	0.705	0.000
IF	445.000	9.754	0.000	9.754	0.000	0.000	0.000	0.000	0.723	0.000
ET	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000

	END	END	FETCH	SURGE ELEV	SURGE ELEV	INITIAL	INITIAL		BOTTOM	AVERAGE
IE	STATION	ELEVATION	LENGTH	10-YEAR	100-YEAR	WAVE	HEIGHT	W. PERIOD	SLOPE	A-ZONES
	0.000	-16.829	1.000	1.000	9.024	9.375	9.618	56.140	-0.033	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
	1.000	-16.862	0.000	9.024	0.000	0.000	0.000	0.000	-0.032	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	2.000	-16.894	0.000	9.024	0.000	0.000	0.000	0.000	-0.032	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	3.000	-16.927	0.000	9.024	0.000	0.000	0.000	0.000	-0.032	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	4.000	-16.959	0.000	9.024	0.000	0.000	0.000	0.000	-0.032	0.000

	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	5.000	-16.992	0.000	9.024	0.000	0.000	0.000	0.000		-0.032	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	6.000	-17.024	0.000	9.024	0.000	0.000	0.000	0.000		-0.032	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	7.000	-17.056	0.000	9.024	0.000	0.000	0.000	0.000		-0.032	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	8.000	-17.089	0.000	9.024	0.000	0.000	0.000	0.000		-0.032	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	9.000	-17.120	0.000	9.024	0.000	0.000	0.000	0.000		-0.030	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	10.000	-17.148	0.000	9.024	0.000	0.000	0.000	0.000		-0.027	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	11.000	-17.175	0.000	9.024	0.000	0.000	0.000	0.000		-0.027	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	12.000	-17.203	0.000	9.024	0.000	0.000	0.000	0.000		-0.027	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	13.000	-17.230	0.000	9.024	0.000	0.000	0.000	0.000		-0.027	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	14.000	-17.258	0.000	9.024	0.000	0.000	0.000	0.000		-0.027	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	15.000	-17.285	0.000	9.024	0.000	0.000	0.000	0.000		-0.027	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	16.000	-17.313	0.000	9.024	0.000	0.000	0.000	0.000		-0.027	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	17.000	-17.340	0.000	9.024	0.000	0.000	0.000	0.000		-0.027	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	18.000	-17.368	0.000	9.024	0.000	0.000	0.000	0.000		-0.027	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	19.000	-17.395	0.000	9.024	0.000	0.000	0.000	0.000		-0.027	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	20.000	-17.423	0.000	9.024	0.000	0.000	0.000	0.000		-0.027	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	21.000	-17.450	0.000	9.024	0.000	0.000	0.000	0.000		-0.027	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	22.000	-17.478	0.000	9.024	0.000	0.000	0.000	0.000		-0.027	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	23.000	-17.505	0.000	9.024	0.000	0.000	0.000	0.000		-0.027	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	24.000	-17.533	0.000	9.024	0.000	0.000	0.000	0.000		-0.027	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	25.000	-17.560	0.000	9.024	0.000	0.000	0.000	0.000		-0.027	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	26.000	-17.588	0.000	9.024	0.000	0.000	0.000	0.000		-0.027	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	27.000	-17.615	0.000	9.024	0.000	0.000	0.000	0.000		-0.027	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	28.000	-17.643	0.000	9.024	0.000	0.000	0.000	0.000		-0.027	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	29.000	-17.670	0.000	9.024	0.000	0.000	0.000	0.000		0.011	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	30.000	-17.621	0.000	9.024	0.000	0.000	0.000	0.000		0.053	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	31.000	-17.564	0.000	9.024	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	32.000	-17.506	0.000	9.024	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	33.000	-17.449	0.000	9.024	0.000	0.000	0.000	0.000		0.057	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	34.000	-17.392	0.000	9.024	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	35.000	-17.334	0.000	9.024	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	36.000	-17.277	0.000	9.024	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	37.000	-17.219	0.000	9.024	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	38.000	-17.162	0.000	9.024	0.000	0.000	0.000	0.000		0.057	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	39.000	-17.105	0.000	9.024	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	40.000	-17.047	0.000	9.024	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES

OF	41.000	-16.990	0.000	9.024	0.000	0.000	0.000	0.000	0.058	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	42.000	-16.932	0.000	9.024	0.000	0.000	0.000	0.000	0.058	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	43.000	-16.875	0.000	9.024	0.000	0.000	0.000	0.000	0.057	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	44.000	-16.818	0.000	9.024	0.000	0.000	0.000	0.000	0.058	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	45.000	-16.760	0.000	9.024	0.000	0.000	0.000	0.000	0.058	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	46.000	-16.703	0.000	9.024	0.000	0.000	0.000	0.000	0.058	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	47.000	-16.645	0.000	9.024	0.000	0.000	0.000	0.000	0.058	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	48.000	-16.588	0.000	9.024	0.000	0.000	0.000	0.000	0.056	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	49.000	-16.533	0.000	9.024	0.000	0.000	0.000	0.000	0.054	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	50.000	-16.481	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	51.000	-16.430	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	52.000	-16.378	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	53.000	-16.327	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	54.000	-16.275	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	55.000	-16.224	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	56.000	-16.172	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	57.000	-16.121	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	58.000	-16.069	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	59.000	-16.018	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	60.000	-15.966	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	61.000	-15.915	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	62.000	-15.863	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	63.000	-15.812	0.000	9.024	0.000	0.000	0.000	0.000	0.051	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	64.000	-15.761	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	65.000	-15.709	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	66.000	-15.658	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	67.000	-15.606	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	68.000	-15.555	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	69.000	-15.503	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	70.000	-15.452	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	71.000	-15.400	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	72.000	-15.349	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	73.000	-15.297	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	74.000	-15.246	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	75.000	-15.194	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	76.000	-15.143	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	77.000	-15.091	0.000	9.024	0.000	0.000	0.000	0.000	0.052	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE

	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	115.000	-13.071	0.000	9.024	0.000	0.000	0.000	0.000		0.097	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	116.000	-12.974	0.000	9.024	0.000	0.000	0.000	0.000		0.097	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	117.000	-12.877	0.000	9.024	0.000	0.000	0.000	0.000		0.097	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	118.000	-12.780	0.000	9.024	0.000	0.000	0.000	0.000		0.097	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	119.000	-12.684	0.000	9.024	0.000	0.000	0.000	0.000		0.097	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	120.000	-12.587	0.000	9.024	0.000	0.000	0.000	0.000		0.097	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	121.000	-12.490	0.000	9.024	0.000	0.000	0.000	0.000		0.097	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	122.000	-12.393	0.000	9.024	0.000	0.000	0.000	0.000		0.097	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	123.000	-12.297	0.000	9.024	0.000	0.000	0.000	0.000		0.097	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	124.000	-12.200	0.000	9.024	0.000	0.000	0.000	0.000		0.097	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	125.000	-12.103	0.000	9.024	0.000	0.000	0.000	0.000		0.097	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	126.000	-12.007	0.000	9.024	0.000	0.000	0.000	0.000		0.097	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	127.000	-11.910	0.000	9.024	0.000	0.000	0.000	0.000		0.097	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	128.000	-11.813	0.000	9.024	0.000	0.000	0.000	0.000		0.097	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	129.000	-11.716	0.000	9.024	0.000	0.000	0.000	0.000		0.097	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	130.000	-11.620	0.000	9.024	0.000	0.000	0.000	0.000		0.097	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	131.000	-11.523	0.000	9.024	0.000	0.000	0.000	0.000		0.097	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	132.000	-11.426	0.000	9.024	0.000	0.000	0.000	0.000		0.097	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	133.000	-11.329	0.000	9.024	0.000	0.000	0.000	0.000		0.097	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	134.000	-11.232	0.000	9.024	0.000	0.000	0.000	0.000		0.097	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	135.000	-11.134	0.000	9.024	0.000	0.000	0.000	0.000		0.098	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	136.000	-11.035	0.000	9.024	0.000	0.000	0.000	0.000		0.099	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	137.000	-10.936	0.000	9.024	0.000	0.000	0.000	0.000		0.099	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	138.000	-10.837	0.000	9.024	0.000	0.000	0.000	0.000		0.099	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	139.000	-10.738	0.000	9.024	0.000	0.000	0.000	0.000		0.099	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	140.000	-10.639	0.000	9.024	0.000	0.000	0.000	0.000		0.099	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	141.000	-10.540	0.000	9.024	0.000	0.000	0.000	0.000		0.099	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	142.000	-10.441	0.000	9.024	0.000	0.000	0.000	0.000		0.099	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	143.000	-10.342	0.000	9.024	0.000	0.000	0.000	0.000		0.099	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	144.000	-10.243	0.000	9.024	0.000	0.000	0.000	0.000		0.099	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	145.000	-10.144	0.000	9.024	0.000	0.000	0.000	0.000		0.099	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	146.000	-10.045	0.000	9.024	0.000	0.000	0.000	0.000		0.098	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	147.000	-9.947	0.000	9.024	0.000	0.000	0.000	0.000		0.098	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	148.000	-9.848	0.000	9.024	0.000	0.000	0.000	0.000		0.099	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	149.000	-9.749	0.000	9.024	0.000	0.000	0.000	0.000		0.099	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
OF	150.000	-9.650	0.000	9.024	0.000	0.000	0.000	0.000		0.099	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES

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	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	225.000	-8.392	0.000	9.022	0.000	0.000	0.000	0.000		-0.047	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	226.000	-8.439	0.000	9.022	0.000	0.000	0.000	0.000		-0.047	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	227.000	-8.485	0.000	9.022	0.000	0.000	0.000	0.000		-0.047	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	228.000	-8.532	0.000	9.022	0.000	0.000	0.000	0.000		-0.030	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	229.000	-8.545	0.000	9.022	0.000	0.000	0.000	0.000		0.022	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	230.000	-8.488	0.000	9.021	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	231.000	-8.430	0.000	9.021	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	232.000	-8.372	0.000	9.021	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	233.000	-8.314	0.000	9.021	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	234.000	-8.257	0.000	9.021	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	235.000	-8.199	0.000	9.021	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	236.000	-8.141	0.000	9.021	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	237.000	-8.083	0.000	9.021	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	238.000	-8.025	0.000	9.021	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	239.000	-7.968	0.000	9.021	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	240.000	-7.910	0.000	9.021	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	241.000	-7.852	0.000	9.021	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	242.000	-7.794	0.000	9.021	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	243.000	-7.736	0.000	9.021	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	244.000	-7.678	0.000	9.021	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	245.000	-7.621	0.000	9.021	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	246.000	-7.563	0.000	9.021	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	247.000	-7.505	0.000	9.021	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	248.000	-7.447	0.000	9.021	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	249.000	-7.389	0.000	9.021	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	250.000	-7.332	0.000	9.021	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	251.000	-7.274	0.000	9.021	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	252.000	-7.216	0.000	9.021	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	253.000	-7.158	0.000	9.021	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	254.000	-7.100	0.000	9.021	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	255.000	-7.043	0.000	9.021	0.000	0.000	0.000	0.000		0.058	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	256.000	-6.985	0.000	9.021	0.000	0.000	0.000	0.000		0.057	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	257.000	-6.928	0.000	9.021	0.000	0.000	0.000	0.000		0.051	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	258.000	-6.882	0.000	9.021	0.000	0.000	0.000	0.000		0.046	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	259.000	-6.836	0.000	9.021	0.000	0.000	0.000	0.000		0.046	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES
	260.000	-6.790	0.000	9.021	0.000	0.000	0.000	0.000		0.046	0.000
	END	END	NEW SURGE	NEW SURGE						BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR						SLOPE	A-ZONES

OF	261.000	-6.745	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
	262.000	-6.699	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	263.000	-6.653	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
	264.000	-6.607	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	265.000	-6.561	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
	266.000	-6.515	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	267.000	-6.470	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
	268.000	-6.424	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	269.000	-6.378	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
	270.000	-6.332	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	271.000	-6.286	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
	272.000	-6.240	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	273.000	-6.194	0.000	9.020	0.000	0.000	0.000	0.000	0.046	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
	274.000	-6.149	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	275.000	-6.103	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
	276.000	-6.057	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	277.000	-6.011	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
	278.000	-5.965	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	279.000	-5.920	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
	280.000	-5.874	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	281.000	-5.828	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
	282.000	-5.782	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
OF	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	283.000	-5.736	0.000	9.021	0.000	0.000	0.000	0.000	0.046	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
	286.000	-5.599	0.000	9.021	0.000	0.000	0.000	0.000	0.037	0.000
OF	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	287.000	-5.588	0.000	9.021	0.000	0.000	0.000	0.000	0.005	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
	288.000	-5.588	0.000	9.022	0.000	0.000	0.000	0.000	0.001	0.000
OF	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	289.000	-5.587	0.000	9.022	0.000	0.000	0.000	0.000	0.001	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
	290.000	-5.587	0.000	9.022	0.000	0.000	0.000	0.000	0.001	0.000
OF	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	291.000	-5.586	0.000	9.022	0.000	0.000	0.000	0.000	0.001	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
	292.000	-5.586	0.000	9.022	0.000	0.000	0.000	0.000	0.001	0.000
OF	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	293.000	-5.585	0.000	9.022	0.000	0.000	0.000	0.000	0.001	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
	294.000	-5.584	0.000	9.022	0.000	0.000	0.000	0.000	0.001	0.000
OF	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	295.000	-5.584	0.000	9.022	0.000	0.000	0.000	0.000	0.001	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
	296.000	-5.583	0.000	9.022	0.000	0.000	0.000	0.000	0.058	0.000
IF	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
IF	423.200	1.818	0.000	9.031	0.000	0.000	0.000	0.000	0.059	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
IF	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
	426.500	2.124	0.000	9.039	0.000	0.000	0.000	0.000	0.103	0.000
IF	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
IF	429.800	2.501	0.000	9.048	0.000	0.000	0.000	0.000	0.158	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE

	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
IF	433.100	3.166	0.000	9.052	0.000	0.000	0.000	0.000	0.250	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
IF	436.400	4.152	0.000	9.059	0.000	0.000	0.000	0.000	0.396	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
IF	439.600	5.739	0.000	9.107	0.000	0.000	0.000	0.000	0.634	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
IF	442.900	8.273	0.000	9.754	0.000	0.000	0.000	0.000	0.748	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
IF	444.000	9.031	0.000	9.754	0.000	0.000	0.000	0.000	0.705	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
IF	445.000	9.754	0.000	9.754	0.000	0.000	0.000	0.000	0.723	0.000
-----END OF TRANSECT-----										

NOTE:

SURGE ELEVATION INCLUDES CONTRIBUTIONS FROM ASTRONOMICAL AND STORM TIDES.

1

PART2: CONTROLLING WAVE HEIGHTS, SPECTRAL PEAK WAVE PERIOD, AND WAVE CREST ELEVATIONS			
LOCATION	CONTROLLING WAVE HEIGHT	SPECTRAL PEAK WAVE PERIOD	WAVE CREST ELEVATION
IE	0.00	9.38	15.59
OF	1.00	9.37	15.58
OF	2.00	9.37	15.58
OF	3.00	9.37	15.58
OF	4.00	9.36	15.58
OF	5.00	9.36	15.58
OF	6.00	9.36	15.57
OF	7.00	9.35	15.57
OF	8.00	9.35	15.57
OF	9.00	9.35	15.57
OF	10.00	9.35	15.57
OF	11.00	9.34	15.57
OF	12.00	9.34	15.56
OF	13.00	9.34	15.56
OF	14.00	9.34	15.56
OF	15.00	9.34	15.56
OF	16.00	9.33	15.56
OF	17.00	9.33	15.56
OF	18.00	9.33	15.55
OF	19.00	9.33	15.55
OF	20.00	9.32	15.55
OF	21.00	9.32	15.55
OF	22.00	9.32	15.55
OF	23.00	9.32	15.55
OF	24.00	9.31	15.54
OF	25.00	9.31	15.54
OF	26.00	9.31	15.54
OF	27.00	9.31	15.54
OF	28.00	9.30	15.54
OF	29.00	9.30	15.54
OF	30.00	9.31	15.54
OF	31.00	9.31	15.54
OF	32.00	9.32	15.55
OF	33.00	9.32	15.55
OF	34.00	9.33	15.55
OF	35.00	9.33	15.56
OF	36.00	9.34	15.56
OF	37.00	9.34	15.56
OF	38.00	9.35	15.57
OF	39.00	9.35	15.57
OF	40.00	9.36	15.58
OF	41.00	9.36	15.58
OF	42.00	9.37	15.58
OF	43.00	9.38	15.59
OF	44.00	9.38	15.59
OF	45.00	9.39	15.59
OF	46.00	9.39	15.60
OF	47.00	9.40	15.60
OF	48.00	9.40	15.61
OF	49.00	9.41	15.61
OF	50.00	9.41	15.61
OF	51.00	9.42	15.62
OF	52.00	9.42	15.62
OF	53.00	9.43	15.62
OF	54.00	9.43	15.63
OF	55.00	9.44	15.63
OF	56.00	9.44	15.63
OF	57.00	9.45	15.64
OF	58.00	9.45	15.64
OF	59.00	9.46	15.65
OF	60.00	9.46	15.65
OF	61.00	9.47	15.65
OF	62.00	9.47	15.66
OF	63.00	9.48	15.66
OF	64.00	9.48	15.66
OF	65.00	9.49	15.67
OF	66.00	9.50	15.67
OF	67.00	9.50	15.67
OF	68.00	9.51	15.68
OF	69.00	9.51	15.68
OF	70.00	9.52	15.69
OF	71.00	9.52	15.69
OF	72.00	9.53	15.69
OF	73.00	9.53	15.70
OF	74.00	9.54	15.70
OF	75.00	9.54	15.70
OF	76.00	9.55	15.71
OF	77.00	9.56	15.71
OF	78.00	9.56	15.72
OF	79.00	9.57	15.72
OF	80.00	9.57	15.72
OF	81.00	9.58	15.73
OF	82.00	9.58	15.73
OF	83.00	9.59	15.74
OF	84.00	9.59	15.74

OF	85.00	9.60	9.62	15.74
OF	86.00	9.61	9.62	15.75
OF	87.00	9.61	9.62	15.75
OF	88.00	9.62	9.62	15.76
OF	89.00	9.62	9.62	15.76
OF	90.00	9.63	9.62	15.76
OF	91.00	9.63	9.62	15.77
OF	92.00	9.64	9.62	15.77
OF	93.00	9.65	9.62	15.78
OF	94.00	9.65	9.62	15.78
OF	95.00	9.66	9.62	15.78
OF	96.00	9.66	9.62	15.79
OF	97.00	9.67	9.62	15.79
OF	98.00	9.68	9.62	15.80
OF	99.00	9.68	9.62	15.80
OF	100.00	9.69	9.62	15.81
OF	101.00	9.69	9.62	15.81
OF	102.00	9.70	9.62	15.81
OF	103.00	9.71	9.62	15.82
OF	104.00	9.71	9.62	15.82
OF	105.00	9.72	9.62	15.83
OF	106.00	9.72	9.62	15.83
OF	107.00	9.73	9.62	15.84
OF	108.00	9.74	9.62	15.84
OF	109.00	9.74	9.62	15.84
OF	110.00	9.75	9.62	15.85
OF	111.00	9.75	9.62	15.85
OF	112.00	9.76	9.62	15.86
OF	113.00	9.77	9.62	15.86
OF	114.00	9.78	9.62	15.87
OF	115.00	9.79	9.62	15.88
OF	116.00	9.80	9.62	15.88
OF	117.00	9.81	9.62	15.89
OF	118.00	9.82	9.62	15.90
OF	119.00	9.84	9.62	15.91
OF	120.00	9.85	9.62	15.92
OF	121.00	9.86	9.62	15.93
OF	122.00	9.87	9.62	15.94
OF	123.00	9.89	9.62	15.94
OF	124.00	9.90	9.62	15.95
OF	125.00	9.91	9.62	15.96
OF	126.00	9.93	9.62	15.97
OF	127.00	9.94	9.62	15.98
OF	128.00	9.95	9.62	15.99
OF	129.00	9.97	9.62	16.00
OF	130.00	9.98	9.62	16.01
OF	131.00	9.99	9.62	16.02
OF	132.00	10.01	9.62	16.03
OF	133.00	10.02	9.62	16.04
OF	134.00	10.03	9.62	16.05
OF	135.00	10.05	9.62	16.06
OF	136.00	10.06	9.62	16.07
OF	137.00	10.08	9.62	16.08
OF	138.00	10.09	9.62	16.09
OF	139.00	10.11	9.62	16.10
OF	140.00	10.12	9.62	16.11
OF	141.00	10.14	9.62	16.12
OF	142.00	10.15	9.62	16.13
OF	143.00	10.17	9.62	16.14
OF	144.00	10.18	9.62	16.15
OF	145.00	10.20	9.62	16.16
OF	146.00	10.21	9.62	16.17
OF	147.00	10.23	9.62	16.18
OF	148.00	10.25	9.62	16.20
OF	149.00	10.26	9.62	16.21
OF	150.00	10.28	9.62	16.22
OF	151.00	10.29	9.62	16.23
OF	152.00	10.31	9.62	16.24
OF	153.00	10.33	9.62	16.25
OF	154.00	10.34	9.62	16.27
OF	155.00	10.36	9.62	16.28
OF	156.00	10.38	9.62	16.29
OF	157.00	10.40	9.62	16.30
OF	158.00	10.41	9.62	16.31
OF	159.00	10.43	9.62	16.33
OF	160.00	10.45	9.62	16.34
OF	161.00	10.47	9.62	16.35
OF	162.00	10.46	9.62	16.34
OF	163.00	10.45	9.62	16.34
OF	164.00	10.43	9.62	16.33
OF	165.00	10.42	9.62	16.32
OF	166.00	10.41	9.62	16.31
OF	167.00	10.40	9.62	16.30
OF	168.00	10.39	9.62	16.29
OF	169.00	10.38	9.62	16.29
OF	170.00	10.36	9.62	16.28
OF	171.00	10.35	9.62	16.27
OF	172.00	10.34	9.62	16.26
OF	173.00	10.33	9.62	16.25
OF	174.00	10.31	9.62	16.24
OF	175.00	10.30	9.62	16.23
OF	176.00	10.29	9.62	16.22
OF	177.00	10.27	9.62	16.21
OF	178.00	10.26	9.62	16.21
OF	179.00	10.25	9.62	16.20
OF	180.00	10.23	9.62	16.19
OF	181.00	10.22	9.62	16.18
OF	182.00	10.20	9.62	16.17
OF	183.00	10.20	9.62	16.16
OF	184.00	10.21	9.62	16.17
OF	185.00	10.22	9.62	16.18
OF	186.00	10.23	9.62	16.18
OF	187.00	10.24	9.62	16.19
OF	188.00	10.25	9.62	16.20
OF	189.00	10.26	9.62	16.20
OF	190.00	10.27	9.62	16.21
OF	191.00	10.28	9.62	16.22
OF	192.00	10.29	9.62	16.22
OF	193.00	10.30	9.62	16.23
OF	194.00	10.30	9.62	16.24

OF	195.00	10.31	9.62	16.24
OF	196.00	10.32	9.62	16.25
OF	197.00	10.33	9.62	16.26
OF	198.00	10.34	9.62	16.26
OF	199.00	10.35	9.62	16.27
OF	200.00	10.36	9.62	16.27
OF	201.00	10.37	9.62	16.28
OF	202.00	10.38	9.62	16.29
OF	203.00	10.39	9.62	16.29
OF	204.00	10.40	9.62	16.30
OF	205.00	10.41	9.62	16.31
OF	206.00	10.42	9.62	16.31
OF	207.00	10.42	9.62	16.32
OF	208.00	10.43	9.62	16.33
OF	209.00	10.44	9.62	16.33
OF	210.00	10.45	9.62	16.34
OF	211.00	10.46	9.62	16.34
OF	212.00	10.47	9.62	16.35
OF	213.00	10.48	9.62	16.36
OF	214.00	10.49	9.62	16.36
OF	215.00	10.50	9.62	16.37
OF	216.00	10.51	9.62	16.38
OF	217.00	10.51	9.62	16.38
OF	218.00	10.52	9.62	16.39
OF	219.00	10.53	9.62	16.39
OF	220.00	10.54	9.62	16.40
OF	221.00	10.55	9.62	16.41
OF	222.00	10.56	9.62	16.41
OF	223.00	10.57	9.62	16.42
OF	224.00	10.58	9.62	16.42
OF	225.00	10.58	9.62	16.43
OF	226.00	10.59	9.62	16.44
OF	227.00	10.60	9.62	16.44
OF	228.00	10.61	9.62	16.45
OF	229.00	10.61	9.62	16.45
OF	230.00	10.61	9.62	16.45
OF	231.00	10.60	9.62	16.44
OF	232.00	10.60	9.62	16.44
OF	233.00	10.59	9.62	16.43
OF	234.00	10.58	9.62	16.43
OF	235.00	10.58	9.62	16.43
OF	236.00	10.57	9.62	16.42
OF	237.00	10.57	9.62	16.42
OF	238.00	10.56	9.62	16.41
OF	239.00	10.55	9.62	16.41
OF	240.00	10.55	9.62	16.40
OF	241.00	10.54	9.62	16.40
OF	242.00	10.53	9.62	16.39
OF	243.00	10.53	9.62	16.39
OF	244.00	10.52	9.62	16.39
OF	245.00	10.51	9.62	16.38
OF	246.00	10.51	9.62	16.38
OF	247.00	10.50	9.62	16.37
OF	248.00	10.49	9.62	16.37
OF	249.00	10.49	9.62	16.36
OF	250.00	10.48	9.62	16.36
OF	251.00	10.47	9.62	16.35
OF	252.00	10.47	9.62	16.35
OF	253.00	10.46	9.62	16.34
OF	254.00	10.45	9.62	16.34
OF	255.00	10.45	9.62	16.33
OF	256.00	10.44	9.62	16.33
OF	257.00	10.43	9.62	16.32
OF	258.00	10.43	9.62	16.32
OF	259.00	10.42	9.62	16.32
OF	260.00	10.41	9.62	16.31
OF	261.00	10.41	9.62	16.31
OF	262.00	10.40	9.62	16.30
OF	263.00	10.40	9.62	16.30
OF	264.00	10.39	9.62	16.30
OF	265.00	10.39	9.62	16.29
OF	266.00	10.38	9.62	16.29
OF	267.00	10.38	9.62	16.28
OF	268.00	10.37	9.62	16.28
OF	269.00	10.36	9.62	16.28
OF	270.00	10.36	9.62	16.27
OF	271.00	10.35	9.62	16.27
OF	272.00	10.35	9.62	16.26
OF	273.00	10.34	9.62	16.26
OF	274.00	10.34	9.62	16.26
OF	275.00	10.33	9.62	16.25
OF	276.00	10.32	9.62	16.25
OF	277.00	10.32	9.62	16.24
OF	278.00	10.31	9.62	16.24
OF	279.00	10.30	9.62	16.23
OF	280.00	10.30	9.62	16.23
OF	281.00	10.29	9.62	16.23
OF	282.00	10.29	9.62	16.22
OF	283.00	10.28	9.62	16.22
OF	286.00	10.26	9.62	16.20
OF	287.00	10.26	9.62	16.20
OF	288.00	10.26	9.62	16.20
OF	289.00	10.26	9.62	16.20
OF	290.00	10.26	9.62	16.21
OF	291.00	10.26	9.62	16.21
OF	292.00	10.27	9.62	16.21
OF	293.00	10.27	9.62	16.21
OF	294.00	10.27	9.62	16.21
OF	295.00	10.27	9.62	16.21
OF	296.00	10.28	9.62	16.21
	397.76	6.59	9.62	13.64
IF	423.20	5.49	9.62	12.88
IF	426.50	5.27	9.62	12.73
IF	429.80	5.00	9.62	12.55
IF	433.10	4.50	9.62	12.20
IF	436.40	3.77	9.62	11.70
IF	439.60	2.60	9.62	10.93
IF	442.90	1.15	9.62	10.56
IF	444.00	0.56	9.62	10.15
IF	445.00	0.01	9.62	9.76

PART3 LOCATION OF AREAS ABOVE 100-YEAR SURGE
 NO AREAS ABOVE 100-YEAR SURGE IN THIS TRANSECT
 PART4 LOCATION OF SURGE CHANGES

STATION	10-YEAR SURGE	100-YEAR SURGE
163.00	1.00	9.02
198.00	1.00	9.02
230.00	1.00	9.02
273.00	1.00	9.02
274.00	1.00	9.02
288.00	1.00	9.02
423.20	1.00	9.03
426.50	1.00	9.04
429.80	1.00	9.05
433.10	1.00	9.05
436.40	1.00	9.06
439.60	1.00	9.11
442.90	1.00	9.75

PART5 LOCATION OF V ZONES
 STATION OF GUTTER LOCATION OF ZONE
 438.50 WINDWARD

PART6 NUMBERED A ZONES AND V ZONES

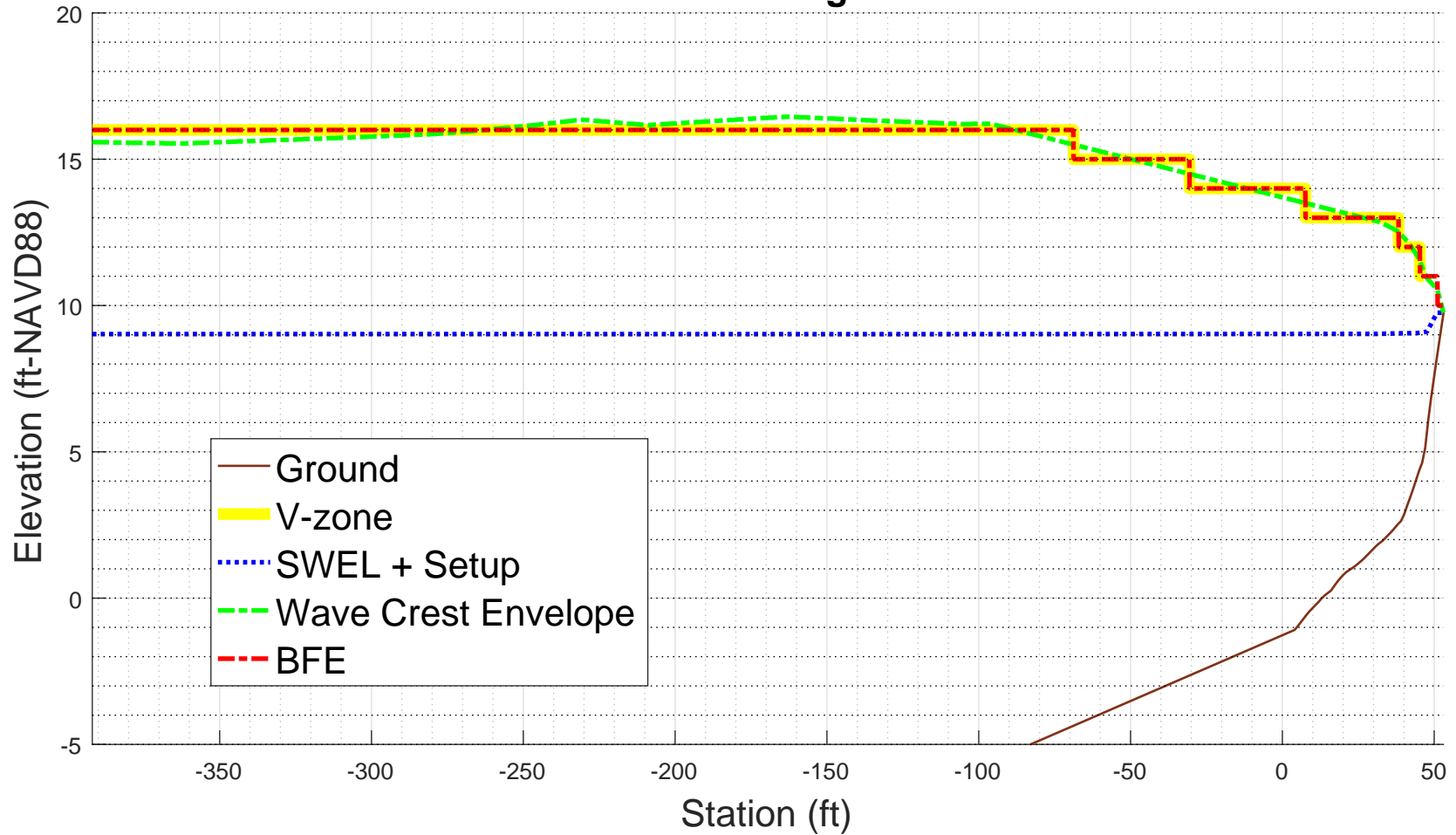
STATION OF GUTTER	ELEVATION	ZONE DESIGNATION	FHF
0.00	15.59		
162.00	16.34	V22 EL=16	120
163.00	16.34	V22 EL=16	120
197.00	16.26	V22 EL=16	120
198.00	16.26	V22 EL=16	120
229.00	16.45	V22 EL=16	120
230.00	16.45	V22 EL=16	120
272.00	16.26	V22 EL=16	120
273.00	16.26	V22 EL=16	120
274.00	16.26	V22 EL=16	120
287.00	16.20	V22 EL=16	120
288.00	16.20	V22 EL=16	120
296.00	16.21	V22 EL=16	120
324.26	15.50	V22 EL=15	120
363.80	14.50	V22 EL=14	120
402.46	13.50	V22 EL=13	120
423.20	12.88	V22 EL=13	120
426.50	12.73	V22 EL=13	120
429.80	12.55	V22 EL=13	120
430.25	12.50	V22 EL=12	120
433.10	12.20	V23 EL=12	130
436.40	11.70	V23 EL=12	130
437.21	11.50	V23 EL=11	130
438.50	11.18	A19 EL=11	95
439.60	10.93	A19 EL=11	95
442.90	10.56	A19 EL=11	95
443.06	10.50	A19 EL=10	95
445.00	9.76		

ZONE TERMINATED AT END OF TRANSECT
 PART 7 POSTSCRIPT NOTES

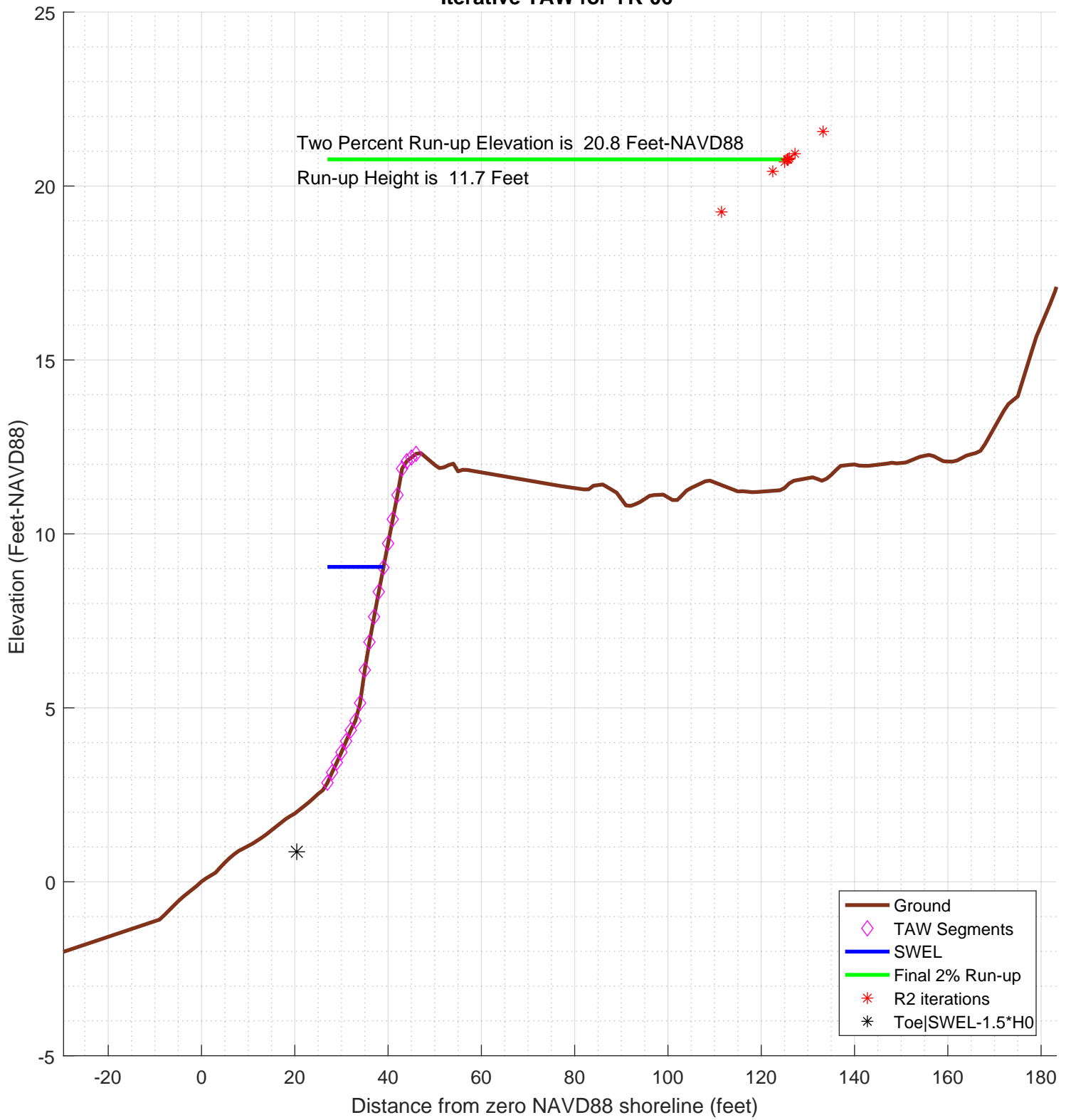
PS# 1 START(361191.8955,4771276.21)
 PS# 2 END(361217.8661,4771469.8232)

-1.000000e+00

YK-06
100-year WHAFIS Output
Zero Station: -70.70506513, 43.08256716
Onshore Dir: 82.4 deg CCW from E



Iterative TAW for YK-06



```

diary on          % begin recording

% FEMA appeal for The Town of Harpswell, Cumberland county, Maine
% TRANSECT ID: YK-06
% calculation by SJH, Ransom Consulting, Inc. 06-Feb-2020
% 100-year wave runup using TAW methodology
% including berm and weighted average with foreshore if necessary
%
% chk nld 20181015
%
% This script assumes that the incident wave conditions provided
% as input in the configuration section below are the
% appropriate values located at the end of the foreshore
% or toe of the slope on which the run-up is being calculated
% the script does not attempt to apply a depth limit or any other
% transformation to the incident wave conditions other than
% conversion of the peak wave period to the spectral mean wave
% as recommended in the references below
%
%
% references:
%
% Van der Meer, J.W., 2002. Technical Report Wave Run-up and
% Wave Overtopping at Dikes. TAW Technical Advisory Committee on
% Flood Defence, The Netherlands.
%
% FEMA. 2007, Atlantic Ocean and Gulf of Mexico Coastal Guidelines Update
%
%
%-----
% CONFIG
%-----
fname='infiles/YK-06sta_ele_include.csv'; % file with station, elevation, include
% third column is 0 for excluded points
imgname='logfiles/YK-06-runup';
SWEL=9.0235; % 100-yr still water level including wave setup.
H0=5.4588; % significant wave height at toe of structure
Tp=9.7161; % peak period, 1/fma,
T0=Tp/1.1;

gamma_berm=1; % this may get changed automatically below
gamma_rough=0.75;
gamma_beta=1;
gamma_perm=1;

setupAtToe=0.028035;
maxSetup=0.73082; % only used in case of berm/shallow foreshore weighted average

plotTitle='Iterative TAW for YK-06'

plotTitle =

Iterative TAW for YK-06

% END CONFIG
%-----

SWEL=SWEL+setupAtToe

SWEL =

          9.051535

SWEL_fore=SWEL+maxSetup

SWEL_fore =

          9.782355

% FIND WAVELENGTH USING DEEPWATER DISPERSION RELATION
% using English units
L0=32.15/(2*pi)*T0^2

L0 =

          399.208418021136

% Find Hb (Munk, 1949)
%Hb=H0/(3.3*(H0/L0)^(1/3))
%Db=-Hb/.78+SWEL; % depth at breaking

% The toe elevation here is only used to determine the average
% structure slope, it is not used to depth limit the wave height.
% Any depth limiting or other modification of the wave height
% to make it consistent with TAW guidance should be performed
% prior to the input of the significant wave height given above.
Ztoe=SWEL-1.5*H0

Ztoe =

```


0.8633349999999999

```
% read the transect
[sta,dep,inc] = textread(fname,'%n%n%n%*[\n]', 'delimiter',' ','headerlines',0);
```

```
% remove unselected points
k=find(inc==0);
sta(k)=[];
dep(k)=[];
```

```
sta_org=sta; % used for plotting purposes
dep_org=dep;
```

```
% initial guess at maximum run-up elevation to estimate slope
Z2=SWEL+1.5*H0
```

```
Z2 =
```

17.239735

```
% determine station at the max runup and -1.5*H0 (i.e. the toe)
top_sta=-999;
toe_sta=-999;
for kk=1:length(sta)-1
    if ((Z2 > dep(kk)) & (Z2 <= dep(kk+1))) % here is the intersection of z2 with profile
        top_sta=interp1(dep(kk:kk+1),sta(kk:kk+1),Z2)
    end
    if ((Ztoe > dep(kk)) & (Ztoe <= dep(kk+1))) % here is the intersection of Ztoe with profile
        toe_sta=interp1(dep(kk:kk+1),sta(kk:kk+1),Ztoe)
    end
end
% check to make sure we got them, if not extend the end slopes outward
S=diff(dep)./diff(sta);
if toe_sta== -999
    dy=dep(1)-Ztoe;
    toe_sta=sta(1)-dy/S(1)
end
```

```
toe_sta =
```

20.4222867573847

```
if top_sta== -999
    dy=Z2-dep(end);
    top_sta=sta(end)+dy/S(end)
end
```

```
top_sta =
```

92.4937382297555

```
% just so the reader can tell the values aren't -999 anymore
top_sta
```

```
top_sta =
```

92.4937382297555

```
toe_sta
```

```
toe_sta =
```

20.4222867573847

```
% check for case where the toe of slope is below SWL-1.5*H0
% in this case interpolate setup from the setupAtToe(really setup as first station), and the max setup
% also un-include points seaward of SWL-1.5*H0
```

```
if Ztoe > dep(1)
    dd=SWEL_fore-dep;
    k=find(dd<0,1); % k is index of first land point
    staAtSWL=interp1(dep(k-1:k),sta(k-1:k),SWEL_fore);
    dsta=staAtSWL-sta(1);
    dsetup=maxSetup-setupAtToe;
    dsetdsta=dsetup/dsta;
    setup=setupAtToe+dsetdsta*(toe_sta-sta(1));
    sprintf('-!!- Location of SWEL-1.5*H0 is %4.1f ft landward of toe of slope',dsta)
    sprintf('-!!- Setup is interpolated between setup at toe of slope and max setup')
    sprintf('-!!- setup is adjusted to %4.2f feet',setup)
    SWEL=SWEL-setupAtToe+setup;
    sprintf('-!!- SWEL is adjusted to %4.2f feet',SWEL)
    k=find(dep < SWEL-1.5*H0)
    sta(k)=[];
    dep(k)=[];
else
```

```
    sprintf('-!!- The User has selected a starting point that is %4.2f feet above the elevation of SWEL-1.5H0\n',de
    sprintf('-!!- This may be reasonable for some cases. However the user may want to consider:\n')
    sprintf('-!!- 1) Selecting a starting point that is at or below %4.2f feet elevation, or\n', Ztoe)
    sprintf('-!!- 2) Reducing the incident wave height to a depth limited condition.\n')
```

```

end

ans =

-!!- The User has selected a starting point that is 1.98 feet above the elevation of SWEL-1.5H0

ans =

-!!- This may be reasonable for some cases. However the user may want to consider:

ans =

-!!- 1) Selecting a starting point that is at or below 0.86 feet elevation, or

ans =

-!!- 2) Reducing the incident wave height to a depth limited condition.

% now iterate converge on a runup elevation
tol=0.001; % convergence criteria
R2del=999;
R2_new=3*H0; %initial guess
R2=R2_new;
iter=0;
R2_all=[];
topStaAll=[];
Berm_Segs=[];
TAW_ALWAYS_VALID=1;
while(abs(R2del) > tol && iter <= 25)
    iter=iter+1;
    sprintf('!----- STARTING ITERATION %d -----!',iter)
    % elevation of toe of slope
    Ztoe
    % station of toe slope (relative to 0-NAVD88 shoreline)
    toe_sta
    % station of top of slope/extent of 2% run-up
    top_sta
    % elevation of top of slope/extent of 2% run-up
    Z2
    % incident significant wave height
    H0
    % incident spectral peak wave period
    Tp
    % incident spectral mean wave period
    T0

    R2=R2_new
    Z2=R2+SWEL
    % determine slope for this iteration
    top_sta=-999;
    for kk=1:length(sta)-1
        if ((Z2 > dep(kk)) & (Z2 <= dep(kk+1))) % here is the intersection of z2 with profile
            top_sta=interp1(dep(kk:kk+1),sta(kk:kk+1),Z2)
            break;
        end
    end
    if top_sta== -999
        dy=Z2-dep(end);
        top_sta=sta(end)+dy/S(end)
    end

    % get the length of the slope (not accounting for berm)
    Lslope=top_sta-toe_sta

    % loop over profile segments to determine berm factor
    % re-calculate influence of depth of berm based on this run-up elevation
    % check for berm, berm width, berm height
    berm_width=0;
    rdh_sum=0;
    Berm_Segs=[];
    Berm_Heights=[];
    for kk=1:length(sta)-1
        ddep=dep(kk+1)-dep(kk);
        dsta=sta(kk+1)-sta(kk);
        s=ddep/dsta;
        if (s < 1/15) % count it as a berm if slope is flatter than 1:15 (see TAW manual)
            sprintf('Berm Factor Calculation: Iteration %d, Profile Segment: %d',iter, kk)
            berm_width=berm_width+dsta; % tally the width of all berm segments
            % compute the rdh for this segment and weight it by the segment length
            dh=SWEL-(dep(kk)+dep(kk+1))/2
            if dh < 0
                chi=R2;
            else
                chi=2* H0;
            end
            if (dh <= R2 & dh >=-2*H0)

```

```

        rdh=(0.5-0.5*cos(3.14159*dh/chi)) ;
    else
        rdh=1;
    end
    rdh_sum=rdh_sum + rdh * dsta
    Berm_Segs=[Berm_Segs, kk];
    Berm_Heights=[Berm_Heights, (dep(kk)+dep(kk+1))/2];
end
if dep(kk) >= Z2 % jump out of loop if we reached limit of run-up for this iteration
    break
end
end
sprintf('!----- End Berm Factor Calculation, Iter: %d -----!', iter)
berm_width
rB=berm_width/Lslope
if (berm_width > 0)
    rdh_mean=rdh_sum/berm_width
else
    rdh_mean=1
end
gamma_berm=1- rB * (1-rdh_mean)
if gamma_berm > 1
    gamma_berm=1
end
if gamma_berm < 0.6
    gamma_berm =0.6
end
% Iribarren number
slope=(Z2-Ztoe)/(Lslope-berm_width)
Irb=(slope/(sqrt(H0/L0)))
% runup height
gamma_berm
gamma_perm
gamma_beta
gamma_rough
gamma=gamma_berm*gamma_perm*gamma_beta*gamma_rough

% check validity
TAW_VALID=1;
if (Irb*gamma_berm < 0.5 | Irb*gamma_berm > 10 )
    sprintf('!!! - - Iribarren number: %6.2f is outside the valid range (0.5-10), TAW NOT VALID - - !!!\n', Irb)
    TAW_VALID=0;
else
    sprintf('!!! - - Iribarren number: %6.2f is in the valid range (0.5-10), TAW RECOMMENDED - - !!!\n', Irb*gamma_berm)
end
islope=1/slope;
if (slope < 1/8 | slope > 1)
    sprintf('!!! - - slope: 1:%3.1f V:H is outside the valid range (1:8 - 1:1), TAW NOT VALID - - !!!\n', islope)
    TAW_VALID=0;
else
    sprintf('!!! - - slope: 1:%3.1f V:H is in the valid range (1:8 - 1:1), TAW RECOMMENDED - - !!!\n', islope)
end
if TAW_VALID == 0
    TAW_ALWAYS_VALID=0;
end

if (Irb*gamma_berm < 1.8)
    R2_new=gamma*H0*1.77*Irb
else
    R2_new=gamma*H0*(4.3-(1.6/sqrt(Irb)))
end

% check to see if we need to evaluate a shallow foreshore
if berm_width > 0.25 * L0;
    disp('! Berm_width is greater than 1/4 wave length')
    disp('! Runup will be weighted average with foreshore calculation assuming depth limited wave height on
    % do the foreshore calculation
    fore_H0=0.78*(SWEL_fore-min(Berm_Heights))
    % get upper slope
    fore_toe_sta=-999;
    fore_toe_dep=-999;
    for kk=length(dep)-1:-1:1
        ddep=dep(kk+1)-dep(kk);
        dsta=sta(kk+1)-sta(kk);
        s=ddep/dsta;
        if s < 1/15
            break
        end
        fore_toe_sta=sta(kk);
        fore_toe_dep=dep(kk);
        upper_slope=(Z2-fore_toe_dep)/(top_sta-fore_toe_sta)
    end
    fore_Irb=upper_slope/(sqrt(fore_H0/L0));
    fore_gamma=gamma_perm*gamma_beta*gamma_rough;
    if (fore_Irb < 1.8)
        fore_R2=fore_gamma*fore_H0*1.77*fore_Irb;
    else
        fore_R2=fore_gamma*fore_H0*(4.3-(1.6/sqrt(fore_Irb)));
    end
    if berm_width >= L0
        R2_new=fore_R2
        disp('berm is wider than one wavelength, use full shallow foreshore solution');
    else
        w2=(berm_width-0.25*L0)/(0.75*L0)
        w1=1-w2
    end
end

```

```

        R2_new=w2*fore_R2 + w1*R2_new
    end
end % end berm width check

% convergence criterion
R2del=abs(R2-R2_new)
R2_all(iter)=R2_new;

% get the new top station (for plot purposes)
Z2=R2_new+SWEL
top_sta=-999;
for kk=1:length(sta)-1
    if ((Z2 > dep(kk)) & (Z2 <= dep(kk+1))) % here is the intersection of z2 with profile
        top_sta=interp1(dep(kk:kk+1),sta(kk:kk+1),Z2)
        break;
    end
end
if top_sta== -999
    dy=Z2-dep(end);
    top_sta=sta(end)+dy/S(end);
end
topStaAll(iter)=top_sta;

end

ans =

!----- STARTING ITERATION 1 -----!

Ztoe =

    0.863334999999999

toe_sta =

    20.4222867573847

top_sta =

    92.4937382297555

Z2 =

    17.239735

H0 =

    5.4588

Tp =

    9.7161

T0 =

    8.83281818181818

R2 =

    16.3764

Z2 =

    25.427935

top_sta =

    169.59543314501

Lslope =

    149.173146387625

ans =

!----- End Berm Factor Calculation, Iter: 1 -----!

berm_width =

    0

rB =

```

```

0

rdh_mean =
    1

gamma_berm =
    1

slope =
    0.164671729428895

Irb =
    1.40821932699039

gamma_berm =
    1

gamma_perm =
    1

gamma_beta =
    1

gamma_rough =
    0.75

gamma =
    0.75

ans =
!!! - - Iribaren number: 1.41 is in the valid range (0.5-10), TAW RECOMMENDED - - !!!

ans =
!!! - - slope: 1:6.1 V:H is in the valid range (1:8 - 1:1), TAW RECOMMENDED - - !!!

R2_new =
    10.2047416215375

R2del =
    6.17165837846249

Z2 =
    19.2562766215375

ans =
!----- STARTING ITERATION 2 -----!

Ztoe =
    0.863334999999999

toe_sta =
    20.4222867573847

top_sta =
    111.481889091691

```

```

Z2 =
    19.2562766215375

H0 =
    5.4588

Tp =
    9.7161

T0 =
    8.83281818181818

R2 =
    10.2047416215375

Z2 =
    19.2562766215375

top_sta =
    111.481889091691

Lslope =
    91.059602334306

ans =
!----- End Berm Factor Calculation, Iter: 2 -----!

berm_width =
    0

rB =
    0

rdh_mean =
    1

gamma_berm =
    1

slope =
    0.201987941414588

Irb =
    1.72733549289557

gamma_berm =
    1

gamma_perm =
    1

gamma_beta =
    1

gamma_rough =
    0.75

gamma =

```

0.75

ans =

!!! - - Iribaren number: 1.73 is in the valid range (0.5-10), TAW RECOMMENDED - - !!!

ans =

!!! - - slope: 1:5.0 V:H is in the valid range (1:8 - 1:1), TAW RECOMMENDED - - !!!

R2_new =

12.5172351073908

R2del =

2.31249348585333

Z2 =

21.5687701073908

ans =

!----- STARTING ITERATION 3 -----!

Ztoe =

0.863334999999999

toe_sta =

20.4222867573847

top_sta =

133.256780672231

Z2 =

21.5687701073908

H0 =

5.4588

Tp =

9.7161

T0 =

8.83281818181818

R2 =

12.5172351073908

Z2 =

21.5687701073908

top_sta =

133.256780672231

Lslope =

112.834493914846

ans =

!----- End Berm Factor Calculation, Iter: 3 -----!

```

berm_width =
    0

rB =
    0

rdh_mean =
    1

gamma_berm =
    1

slope =
    0.183502707275107

Irb =
    1.56925575407555

gamma_berm =
    1

gamma_perm =
    1

gamma_beta =
    1

gamma_rough =
    0.75

gamma =
    0.75

ans =
!!! - - Iribaren number: 1.57 is in the valid range (0.5-10), TAW RECOMMENDED - - !!!

ans =
!!! - - slope: 1:5.4 V:H is in the valid range (1:8 - 1:1), TAW RECOMMENDED - - !!!

R2_new =
    11.3717012694865

R2del =
    1.14553383790435

Z2 =
    20.4232362694865

ans =
!----- STARTING ITERATION 4 -----!

Ztoe =
    0.863334999999999

toe_sta =
    20.4222867573847

```



```
top_sta =
    122.470209693847

Z2 =
    20.4232362694865

H0 =
    5.4588

Tp =
    9.7161

T0 =
    8.83281818181818

R2 =
    11.3717012694865

Z2 =
    20.4232362694865

top_sta =
    122.470209693847

Lslope =
    102.047922936462

ans =
!----- End Berm Factor Calculation, Iter: 4 -----!

berm_width =
    0

rB =
    0

rdh_mean =
    1

gamma_berm =
    1

slope =
    0.191673683369969

Irb =
    1.63913129675108

gamma_berm =
    1

gamma_perm =
    1

gamma_beta =
    1
```

```

gamma_rough =
                                0.75

gamma =
                                0.75

ans =
!!! - - Iribaren number:  1.64 is in the valid range (0.5-10), TAW RECOMMENDED - - !!!

ans =
!!! - - slope: 1:5.2 V:H is in the valid range (1:8 - 1:1), TAW RECOMMENDED - - !!!

R2_new =
                                11.8780583723906

R2del =
                                0.506357102904133

Z2 =
                                20.9295933723906

ans =
!----- STARTING ITERATION 5 -----!

Ztoe =
                                0.8633349999999999

toe_sta =
                                20.4222867573847

top_sta =
                                127.238167348311

Z2 =
                                20.9295933723906

H0 =
                                5.4588

Tp =
                                9.7161

T0 =
                                8.83281818181818

R2 =
                                11.8780583723906

Z2 =
                                20.9295933723906

top_sta =
                                127.238167348311

Lslope =
                                106.815880590927

```

```

ans =
!----- End Berm Factor Calculation, Iter: 5 -----!

berm_width =
    0

rB =
    0

rdh_mean =
    1

gamma_berm =
    1

slope =
    0.187858380807986

Irb =
    1.60650406422771

gamma_berm =
    1

gamma_perm =
    1

gamma_beta =
    1

gamma_rough =
    0.75

gamma =
    0.75

ans =
!!! - - Iribaren number: 1.61 is in the valid range (0.5-10), TAW RECOMMENDED - - !!!

ans =
!!! - - slope: 1:5.3 V:H is in the valid range (1:8 - 1:1), TAW RECOMMENDED - - !!!

R2_new =
    11.6416232721578

R2del =
    0.236435100232841

Z2 =
    20.6931582721578

ans =
!----- STARTING ITERATION 6 -----!

Ztoe =
    0.863334999999999

```

```
toe_sta =
    20.4222867573847

top_sta =
    125.011848137079

z2 =
    20.6931582721578

H0 =
    5.4588

Tp =
    9.7161

T0 =
    8.83281818181818

R2 =
    11.6416232721578

z2 =
    20.6931582721578

top_sta =
    125.011848137079

Lslope =
    104.589561379695

ans =
!----- End Berm Factor Calculation, Iter: 6 -----!

berm_width =
    0

rB =
    0

rdh_mean =
    1

gamma_berm =
    1

slope =
    0.189596581251249

Irb =
    1.62136859177519

gamma_berm =
    1

gamma_perm =
    1
```

```

gamma_beta =
    1

gamma_rough =
    0.75

gamma =
    0.75

ans =
!!! - - Iribaren number: 1.62 is in the valid range (0.5-10), TAW RECOMMENDED - - !!!

ans =
!!! - - slope: 1:5.3 V:H is in the valid range (1:8 - 1:1), TAW RECOMMENDED - - !!!

R2_new =
    11.7493399183087

R2del =
    0.10771664615088

Z2 =
    20.8008749183087

ans =
!----- STARTING ITERATION 7 -----!

Ztoe =
    0.863334999999999

toe_sta =
    20.4222867573847

top_sta =
    126.026129174282

Z2 =
    20.8008749183087

H0 =
    5.4588

Tp =
    9.7161

T0 =
    8.83281818181818

R2 =
    11.7493399183087

Z2 =
    20.8008749183087

top_sta =
    126.026129174282

```

```

Lslope =
    105.603842416897

ans =
!----- End Berm Factor Calculation, Iter: 7 -----!

berm_width =
    0

rB =
    0

rdh_mean =
    1

gamma_berm =
    1

slope =
    0.188795591732357

Irb =
    1.61451878868433

gamma_berm =
    1

gamma_perm =
    1

gamma_beta =
    1

gamma_rough =
    0.75

gamma =
    0.75

ans =
!!! - - Iribaren number: 1.61 is in the valid range (0.5-10), TAW RECOMMENDED - - !!!

ans =
!!! - - slope: 1:5.3 V:H is in the valid range (1:8 - 1:1), TAW RECOMMENDED - - !!!

R2_new =
    11.6997024297719

R2del =
    0.0496374885367334

Z2 =
    20.7512374297719

ans =

```

!----- STARTING ITERATION 8 -----!

Ztoe =
0.863334999999999

toe_sta =
20.4222867573847

top_sta =
125.558732860376

Z2 =
20.7512374297719

H0 =
5.4588

Tp =
9.7161

T0 =
8.83281818181818

R2 =
11.6997024297719

Z2 =
20.7512374297719

top_sta =
125.558732860376

Lslope =
105.136446102992

ans =
!----- End Berm Factor Calculation, Iter: 8 -----!

berm_width =
0

rB =
0

rdh_mean =
1

gamma_berm =
1

slope =
0.189162780053358

Irb =
1.61765886434924

gamma_berm =
1

```

gamma_perm =
    1

gamma_beta =
    1

gamma_rough =
    0.75

gamma =
    0.75

ans =
!!! - - Iribaren number: 1.62 is in the valid range (0.5-10), TAW RECOMMENDED - - !!!

ans =
!!! - - slope: 1:5.3 V:H is in the valid range (1:8 - 1:1), TAW RECOMMENDED - - !!!

R2_new =
    11.722457167062

R2del =
    0.0227547372900769

Z2 =
    20.773992167062

ans =
!----- STARTING ITERATION 9 -----!

Ztoe =
    0.8633349999999999

toe_sta =
    20.4222867573847

top_sta =
    125.772995923372

Z2 =
    20.773992167062

H0 =
    5.4588

Tp =
    9.7161

T0 =
    8.83281818181818

R2 =
    11.722457167062

Z2 =

```



```

20.773992167062

top_sta =
    125.772995923372

Lslope =
    105.350709165987

ans =
!----- End Berm Factor Calculation, Iter: 9 -----!

berm_width =
    0

rB =
    0

rdh_mean =
    1

gamma_berm =
    1

slope =
    0.188994049728621

Irb =
    1.61621593722891

gamma_berm =
    1

gamma_perm =
    1

gamma_beta =
    1

gamma_rough =
    0.75

gamma =
    0.75

ans =
!!! - - Iribaren number: 1.62 is in the valid range (0.5-10), TAW RECOMMENDED - - !!!

ans =
!!! - - slope: 1:5.3 V:H is in the valid range (1:8 - 1:1), TAW RECOMMENDED - - !!!

R2_new =
    11.7120009134377

R2del =
    0.0104562536242749

Z2 =

```

```

20.7635359134377

ans =
!----- STARTING ITERATION 10 -----!

Ztoe =
0.8633349999999999

toe_sta =
20.4222867573847

top_sta =
125.674537791316

Z2 =
20.7635359134377

H0 =
5.4588

Tp =
9.7161

T0 =
8.83281818181818

R2 =
11.7120009134377

Z2 =
20.7635359134377

top_sta =
125.674537791316

Lslope =
105.252251033931

ans =
!----- End Berm Factor Calculation, Iter: 10 -----!

berm_width =
0

rB =
0

rdh_mean =
1

gamma_berm =
1

slope =
0.189071499354653

Irb =

```

```

1.61687826136083

gamma_berm =
    1

gamma_perm =
    1

gamma_beta =
    1

gamma_rough =
    0.75

gamma =
    0.75

ans =
!!! - - Iribaren number: 1.62 is in the valid range (0.5-10), TAW RECOMMENDED - - !!!

ans =
!!! - - slope: 1:5.3 V:H is in the valid range (1:8 - 1:1), TAW RECOMMENDED - - !!!

R2_new =
    11.7168004830122

R2del =
    0.00479956957445182

Z2 =
    20.7683354830122

ans =
!----- STARTING ITERATION 11 -----!

Ztoe =
    0.863334999999999

toe_sta =
    20.4222867573847

top_sta =
    125.719731478458

Z2 =
    20.7683354830122

H0 =
    5.4588

Tp =
    9.7161

T0 =
    8.83281818181818

R2 =

```

```

11.7168004830122

Z2 =
20.7683354830122

top_sta =
125.719731478458

Lslope =
105.297444721073

ans =
!----- End Berm Factor Calculation, Iter: 11 -----!

berm_width =
0

rB =
0

rdh_mean =
1

gamma_berm =
1

slope =
0.189035930888346

Irb =
1.61657409135024

gamma_berm =
1

gamma_perm =
1

gamma_beta =
1

gamma_rough =
0.75

gamma =
0.75

ans =
!!! - - Iribaren number: 1.62 is in the valid range (0.5-10), TAW RECOMMENDED - - !!!

ans =
!!! - - slope: 1:5.3 V:H is in the valid range (1:8 - 1:1), TAW RECOMMENDED - - !!!

R2_new =
11.7145962976927

```

```
R2del =
    0.00220418531947786

Z2 =
    20.7661312976927

ans =
!----- STARTING ITERATION 12 -----!

Ztoe =
    0.863334999999999

toe_sta =
    20.4222867573847

top_sta =
    125.698976437785

Z2 =
    20.7661312976927

H0 =
    5.4588

Tp =
    9.7161

T0 =
    8.83281818181818

R2 =
    11.7145962976927

Z2 =
    20.7661312976927

top_sta =
    125.698976437785

Lslope =
    105.2766896804

ans =
!----- End Berm Factor Calculation, Iter: 12 -----!

berm_width =
    0

rB =
    0

rdh_mean =
    1

gamma_berm =
    1

slope =
```

```

0.189052261788567

Irb =
    1.61671374792273

gamma_berm =
    1

gamma_perm =
    1

gamma_beta =
    1

gamma_rough =
    0.75

gamma =
    0.75

ans =
!!! - - Iribaren number: 1.62 is in the valid range (0.5-10), TAW RECOMMENDED - - !!!

ans =
!!! - - slope: 1:5.3 V:H is in the valid range (1:8 - 1:1), TAW RECOMMENDED - - !!!

R2_new =
    11.7156083270057

R2del =
    0.00101202931299405

Z2 =
    20.7671433270057

ans =
!----- STARTING ITERATION 13 -----!

Ztoe =
    0.863334999999999

toe_sta =
    20.4222867573847

top_sta =
    125.708505904009

Z2 =
    20.7671433270057

H0 =
    5.4588

Tp =
    9.7161

```

```

T0 =
    8.83281818181818

R2 =
    11.7156083270057

Z2 =
    20.7671433270057

top_sta =
    125.708505904009

Lslope =
    105.286219146624

ans =
!----- End Berm Factor Calculation, Iter: 13 -----!

berm_width =
    0

rB =
    0

rdh_mean =
    1

gamma_berm =
    1

slope =
    0.189044762822067

Irb =
    1.61664961918858

gamma_berm =
    1

gamma_perm =
    1

gamma_beta =
    1

gamma_rough =
    0.75

gamma =
    0.75

ans =
!!! - - Iribaren number: 1.62 is in the valid range (0.5-10), TAW RECOMMENDED - - !!!

ans =
!!! - - slope: 1:5.3 V:H is in the valid range (1:8 - 1:1), TAW RECOMMENDED - - !!!

```

```
R2_new =  
11.7151436144784
```

```
R2del =  
0.000464712527325162
```

```
Z2 =  
20.7666786144784
```

```
% final 2% runup elevation  
Z2=R2_new+SWEL
```

```
Z2 =  
20.7666786144784
```

```
diary off
```

PART 5: RUNUP2

for transect: YK-06

Station locations shifted by: -0.06 feet from their
original location to set the shoreline to
elevation 0 for RUNUP2 input

RUNUP2 INPUT CONVERSIONS

for transect: YK-06

Incident significant wave height: 5.86 feet

Peak wave period: 9.62 seconds

Mean wave height: 3.67 feet

Local Depth below SWEL: 25.85 feet

Mean wave height deshoaled using Hunt approximation for
celerity assuming constant wave energy flux.

References: R.G. Dean and R.A. Dalrymple. 2000. Water

Wave Mechanics for Engineers and Scientists. World
Scientific Publishing Company, River Edge New Jersey

USACE (1985), Direct Methods for Calculating Wavelength, CETN-1-17
US Army Engineer Waterways Experiment Station Coastal Engineering
Research Center, Vicksburg, MS

also see Coastal Engineering Manual Part II-3
for discussion of shoaling coefficient

Deep water wavelength, L_0 (m)

$$L_0 = gT^2 / 2\pi$$

$$L_0 = 32.17 \times 8.17^2 / 6.28 = 342.20$$

Deep water wave celerity, C_0 (ft/s)

$$C_0 = L_0 / T$$

$$C_0 = 342.20 / 8.17 = 41.86$$

Angular frequency, σ (rad/s)

$$\sigma = 2\pi / T$$

$$\sigma = 6.28 / 8.17 = 0.77$$

Hunts (1979) approximation for Celerity C_{1H} (ft/s) at Depth D (ft)

$$y = \sigma \cdot \sigma \cdot D / g$$

$$y = 0.77 \times 0.77 \times 25.85 / 32.17 = 0.47$$

$$C_{1H} = \sqrt{g \cdot D / (y + 1 / (1 + 0.6522 \cdot y + 0.4622 \cdot y^2 + 0.0864 \cdot y^4 + 0.0675 \cdot y^5))}$$

$$C_{1H} = 26.56$$

Shoaling Coefficient K_{sH}

$$K_{sH} = \sqrt{C_0 / C_{1H}}$$

$$K_{sH} = \sqrt{41.86 / 26.56} = 1.26$$

Deepwater Wave Height H_{0_H} (ft)

$$H_{0_H} = H / K_{sH}$$

$$H_{0_H} = 3.67 / 1.26 = 2.92$$

Deepwater mean wave height: 2.92 feet

END RUNUP2 CONVERSIONS

RUNUP2 RESULTS

for transect: YK-06

RUNUP2 SWEL:

9.00
9.00
9.00
9.00
9.00
9.00
9.00
9.00
9.00

RUNUP2 deepwater mean wave heights:
2.78

2.78
2.78
2.92
2.92
2.92
3.07
3.07
3.07

RUNUP2 mean wave periods:

7.77
8.17
8.58
7.77
8.17
8.58
7.77
8.17
8.58

RUNUP2 runup above SWEL:

8.03
8.25
8.34
8.21
8.31
8.41
8.30
8.46
8.64

RUNUP2 Mean runup height above SWEL: 8.33 feet

RUNUP2 2-percent runup height above SWEL: 18.32 feet

RUNUP2 2-percent runup elevation: 27.32 feet-NAVD88

RUNUP2 Messages:

No Messages

_____END RUNUP2 RESULTS_____

_____ACES BEACH RUNUP_____

Incident significant wave height: 5.86 feet

Significant wave height deshoaled using Hunt equation

Deepwater significant wave height: 4.09 feet

Peak wave period: 9.62 seconds

Average beach Slope: 1:15.48 (H:V)

ACES RUNUP CALCULATED USING 'Aces_Beach_Runup.m'

ACES Beach 2-percent runup height above SWEL: 5.88 feet

ACES Beach 2-percent runup elevation: 14.88 feet-NAVD88

ACES BEACH RUNUP is valid

_____END ACES BEACH RESULTS_____

PART 5 COMPLETE_____

FEMA
RUNUP2 transect: YK-06
9.00
-16.83 -404.9 1.0
-16.83 -361.9 1.0
-16.53 -355.9 1.0
-13.24 -291.9 1.0
-11.23 -270.9 1.0
-6.48 -222.9 1.0
-6.44 -221.9 1.0
-6.44 -137.9 1.0
-5.60 -118.9 1.0
-5.58 -108.9 1.0
-1.09 -8.9 1.0
-0.44 -3.9 1.0
0.26 3.1 1.0
0.89 8.1 1.0
1.37 14.1 1.0
2.63 26.1 1.0
4.63 33.1 1.0
6.89 36.1 1.0
11.88 43.1 1.0
1 12.30 46.1 1.0
9.0 2.78 7.77
9.0 2.78 8.17
9.0 2.78 8.58
9.0 2.92 7.77
9.0 2.92 8.17
9.0 2.92 8.58
9.0 3.07 7.77
9.0 3.07 8.17
9.0 3.07 8.58

sjh

job 2
1

CROSS SECTION PROFILE

	LENGTH	ELEV.	SLOPE	ROUGHNESS
1	-404.0	-16.8		
2	-361.0	-16.8	.00	1.00
3	-355.0	-16.5	20.00	1.00
4	-291.0	-13.2	19.39	1.00
5	-270.0	-11.2	10.50	1.00
6	-222.9	-6.5	9.98	1.00
7	-221.9	-6.4	25.00	1.00
8	-137.9	-6.4	FLAT	1.00
9	-118.9	-5.6	22.62	1.00
10	-108.9	-5.6	500.00	1.00
11	-8.9	-1.1	22.27	1.00
12	-3.9	-.4	7.69	1.00
13	3.1	.3	10.00	1.00
14	8.1	.9	7.94	1.00
15	14.1	1.4	12.50	1.00
16	26.1	2.6	9.52	1.00
17	33.1	4.6	3.50	1.00
18	36.1	6.9	1.33	1.00
19	43.1	11.9	1.40	1.00
20	46.1	12.3	7.14	1.00
	LAST SLOPE	9.00	LAST ROUGHNESS	1.00

OUTPUT TABLE

INPUT PARAMETERS -----			RUNUP RESULTS -----			
WATER LEVEL ABOVE DATUM (FT.)	DEEP WATER WAVE HEIGHT (FT.)	WAVE PERIOD (SEC.)	BREAKING SLOPE NUMBER	RUNUP SLOPE NUMBER	RUNUP ABOVE WATER LEVEL (FT.)	BREAKER DEPTH (FT.)
9.00	2.78	7.77	11	20	8.03	5.03
9.00	2.78	8.17	11	20	8.25	5.13
9.00	2.78	8.58	11	20	8.34	5.23
9.00	2.92	7.77	11	20	8.21	5.24
9.00	2.92	8.17	11	20	8.31	5.34
9.00	2.92	8.58	11	20	8.41	5.44
9.00	3.07	7.77	11	20	8.30	5.46
9.00	3.07	8.17	11	20	8.46	5.56
9.00	3.07	8.58	11	20	8.64	5.66

Runup2 2% runup elevation for Transect: YK-06

