

DATA LOG FOR TRANSECT ID: CM-139

PART 1: USER INPUT

## SWAN 1-D / WHAFIS input

station: -396 ft

-69.9975 deg E LON: LAT: 43.73 deg N

Bottom ELEV: -24.08 ft-NAVD88

8.804 ft-NAVD88

5.611 ft HS: 10.4458 sec TP:

Wave Direction bin: 45 deg CCW from East (90 deg sector)
Transect Direction: 50.4934 deg CCW from East

#### TAW/RUNUP input

-48 ft toe sta:

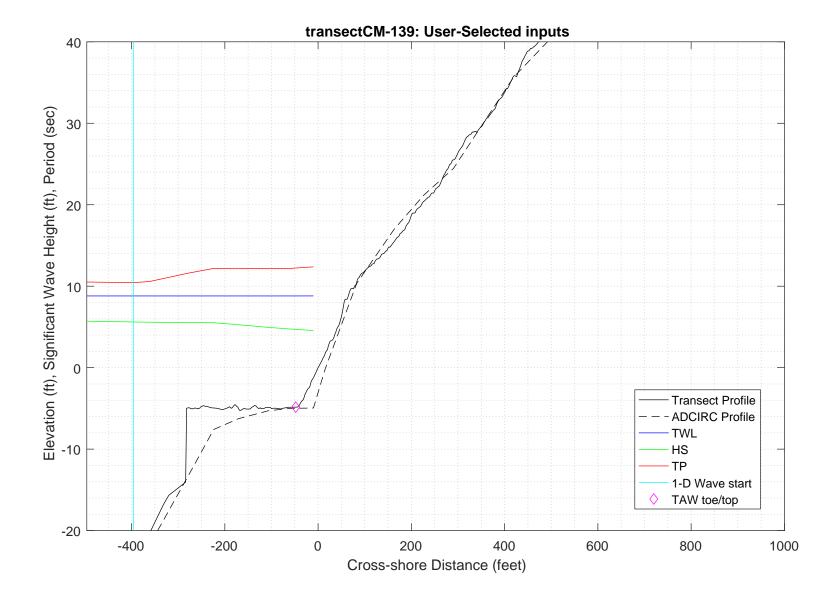
toe elev: -4.8444 ft-NAVD88

top sta: 500 ft

top elev: 41.9542 ft-NAVD88

\*Wave and water level conditions at toe to be calculated in SWAN 1-D\*

PART 1 COMPLETE\_



DADE O. GUAN 1 D

### PART 2: SWAN 1-D

swan input grid name: 2\_swan/gridfiles/CM-139zmeters\_xmeters.grd

swan file name: 2\_swan/swanfiles/CM-139.swn
swan output name: 2\_swan/swanfiles/CM-139.dat

Boundary Conditions:

TWL- 2.6835 meters HS- 1.7103 meters PER- 10.4458 seconds

Batch File: 2\_swan/swanfiles/runswan.dat

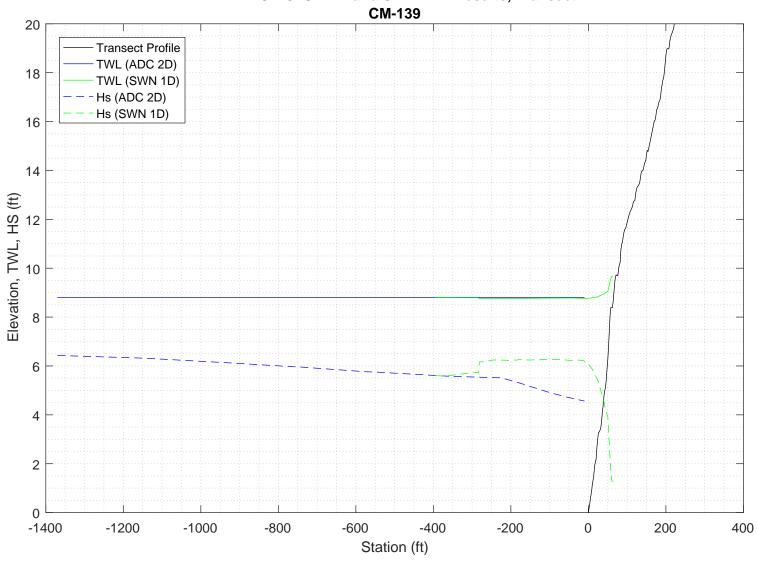
SWAN maximum additional wave setup: 0.87295 feet

SWAN output at toe:

SETUP- -0.023839 feet HS- 6.2267 feet PER- 10.2103 seconds

PART 2 COMPLETE\_\_\_\_\_

# 2-D ADCIRC+SWAN and SWAN 1-D results, Transect:



SWAN
SIMULATION OF WAVES IN NEAR SHORE AREAS
VERSION NUMBER 41.20A

```
PROJECT '2018FemaAppeal' '1'
  '100-year Wind and Wave conditions'
! -- SET commands ------
SET DEPMIN=0.01 MAXMES=999 MAXERR=3 PWTAIL=4
SET LEVEL 0
SET CARTESIAN
! -- MODE commands -----
MODE STATIONARY ONED
!-- COORDINATES commands-----
COORDINATES CART
! -- computational (CGRID) grid commands ------
                              xlenc=length of grid in meters
! mxc = number of mesh cells (one less than number of grid points)
!CGRID REGular [xpc] [ypc] [alpc] [xlenc] [ylenc] [mxc] [myc] &
     [ CIRcle | SECtor[dir1] [dir2] ] [mdc] [flow] [fhigh] [msc]
             0 0 0
                              140
CGRID REGULAR
                                        0.
                                 36
                                      0.03
                                            0.8
                                                    30
Resolution in sigma-space: df/f = 0.1157
! -- READgrid --- not used in 1-D mode -----
! -- INPgrid commands ------
!INPgrid BOTtom REGular [xpinp] [ypinp] [alpinp] [mxinp] [myinp] [dxinp] [dyinp]
INPGRID BOTTOM REGULAR 0
                           0
                                   0 140 0
!READinp BOTtom [fac] 'fname1' [idla] [nhedf] [FREe|FORmat[form]|UNFormatted]
       BOTTOM -1. '../gridfiles/CM-139zmeters xmeters.grd' 1
! -- WIND [vel] [dir]
      25.1 0
WIND
! -- BOUnd SHAPespec
BOUND SHAPE JONSWAP 3.3 PEAK DSPR POWER
! -- BOUndspec
! BOU SIDE W CCW CON FILE 'swanspec.txt' 1
BOUN SIDE W CCW CONSTANT PAR 1.7103 10.4458
!-- \ {\tt BOUndnest1} \ - \ {\tt optional} \ {\tt for} \ {\tt boundary} \ {\tt from} \ {\tt parent} \ {\tt run}
!-- BOUndnest2
!-- BOUndnest3
!-- INITial -- usest to specify initial values
```

```
!----- P H Y S I C S -----
!-- GEN1 [cf10] [cf20] [cf30] [cf40] [edm1pm] [cdrag] [umin] [cfpm]
!-- GEN2 [cf10] [cf20] [cf30] [cf40] [cf50] [cf60] [edm1pm] [cdrag] [umin] [cfpm]
   GEN3 KOMEN
  whitecapping ( on by default)
!-- WCAPping KOMen [cds2] [stpm] [powst] [delta] [powk]
   WCAP KOM
  quadruplet wave interactions
!-- QUADrupl [iquad] [lambda] [Cn14] [Csh1] [Csh2]
! -- BREaking CONstant [alpha] [gamma]
    BREAK
           CON
                    1.
!-- FRICtion JONswap CONstant [cfjon]
   FRIC
          JONSWAP CON
                          0.038
!-- TRIad [itriad] [trfac] [cutfr] [a] [b] [urcrit] [urslim]
! TRIAD
           1 0.65
                          2.5
                              0.95 -0.75 0.2 0.01
 TRIAD
!-- VEGEtation [height] [diamtr] [nstems] [drag]
!-- MUD [layer] [rhom] [viscm]
!- LIMiter [ursell] [qb] deactivates quadruplets with Ursell number exceeds ursell
!-- OBSTacle -- not in 1-D
!-- SETUP [supcor]
  SETUP
         Ω
! ----- N U M E R I C S -----
!-- PROP can use BBST or GSE instead of default
! -- NUMeric -- lots of options
    NUM ACCUR npnts=100. stat 30
    NUMeric STOPC
! -----O U T P U T ------
!OUTPut OPTIons "comment' (TABLE [field]) (BLOck [ndec] [len]) (SPEC [ndec])
OUTPUT OPTIONS '%' TABLE 16
$BLOCK 9 1000 SPEC 8
!CURve 'sname' [xp1] [yp1] <[int] [xp] [yp] >
CURVE 'curve' 0
                 0
                       140 140 0
!TABLe 'sname' < HEADer NOHEADer INDexed > 'fname' <output parameters> (output time)
Table 'curve'
              HEADER 'CM-139.dat' XP YP HSIGN TPS RTP TMM10 DIR &
DSPR DEPTH SETUP
!QUANTITY XP hexp=99999
!-----
COMPUTE STATIONARY
              COMPUTATIONAL PART OF SWAN
```

\_\_\_\_\_

```
One-dimensional mode of SWAN is activated
                                   141 MYC
Gridresolution
                    : MXC
                                                          1
                     : MCGRD
                                      142
                                       31 MDC
                    : MSC
                                                         36
                    : MTC
                    : NSTATC
                                        O TTERMX
                                                          50
Propagation flags
                    : ITFRE
                                        1 IREFR
                                                           1
                    : IBOT
Source term flags
                                        1 ISURF
                                                           1
                    : IWCAP
                                        1 IWIND
                                                           3
                    : ITRIAD
                                        1 IOUAD
                                                           2
                    : IVEG
                                        0 ITURBV
                    : IMUD
                              0.1000E+01 DY
Spatial step
                    : DX
                                                 0.1000E+01
Spectral bin
                    : df/f
                               0.1157E+00 DDIR
                                                 0.1000E+02
Physical constants : GRAV
                               0.9810E+01 RHO
                                                 0.1025E+04
                    : WSPEED 0.2510E+02 DIR
Wind input : WSPEED Tail parameters : E(f)
                                                 0.0000E+00
                               0.4000E+01 E(k)
                                                 0.2500E+01
                    : A(f)
                               0.5000E+01 A(k)
                                                 0.3000E+01
Accuracy parameters : DREL
                               0.1000E-01 NPNTS 0.9950E+02
                    : DHABS
                               0.0000E+00 CURVAT 0.5000E-02
                    : GRWMX
                               0.1000E+00
                    : LEVEL
                               0.0000E+00 DEPMIN 0.1000E-01
Drying/flooding
The Cartesian convention for wind and wave directions is used
Scheme for geographic propagation is SORDUP
Scheme geogr. space : PROPSC
                                  2 ICMAX
                               0.5000E+00 CDD
Scheme spectral space: CSS
                                                 0.5000E+00
Current is off
Quadruplets
                    : IQUAD
                    : LAMBDA 0.2500E+00 CNL4
                                                 0.3000E+08
                               0.5500E+01 CSH2
                    : CSH1
                                                 0.8330E+00
                    : CSH3
                              -0.1250E+01
                              0.1000E+01
Maximum Ursell nr for Snl4:
                                       1 TRFAC
                                                0.8000E+00
Triads
                    : ITRIAD
                    : CUTFR
                               0.2500E+01 URCRI 0.2000E+00
                               0.1000E-01
Minimum Ursell nr for Snl3 :
JONSWAP ('73)
                    : GAMMA
                             0.3800E-01
Vegetation is off
Turbulence is off
Fluid mud is off
                   : EMPCOF (CDS2):
: APM (STPM) :
: POWST :
W-cap Komen ('84)
                                      0.2360E-04
W-cap Komen ('84)
                                      0.3020E-02
                    : POWST
W-cap Komen ('84)
                                       0.2000E+01
W-cap Komen ('84)
                    : DELTA
                                       0.1000E+01
W-cap Komen ('84)
                    : POWK
                                  : 0.1000E+01
Wind drag is fit
Snyder/Komen wind input
Battjes&Janssen ('78): ALPHA
                               0.1000E+01 GAMMA 0.7300E+00
                   : SUPCOR 0.0000E+00
Set-up
Diffraction is off
Janssen ('89,'90)
Janssen ('89,'90)
                    : ALPHA
                               0.1000E-01 KAPPA 0.4100E+00
                    : RHOA
                               0.1280E+01 RHOW
                                                  0.1025E+04
1st and 2nd gen. wind: CF10
                               0.1880E+03 CF20
                                                 0.5900E+00
                    : CF30
                               0.1200E+00 CF40
                                                 0.2500E+03
                    : CF50
                               0.2300E-02 CF60
                                                 -0.2230E+00
                               0.0000E+00 CF80
                                               -0.5600E+00
                    : CF70
                               0.1249E-02 EDMLPM 0.3600E-02
                    : RHOAW
                    : CDRAG
                               0.1230E-02 UMIN
                    : LIM_PM
                              0.1300E+00
 First guess by 2nd generation model flags for first iteration:
                        0.1000E+23 ALFA
0 IQUAD 0
 ITER 1 GRWMX
 IWIND
           2 IWCAP
        1 IBOT 1 ISURF
0 ITURBV 0 IMUD
 ITRIAD
                        1 ISURF
                                     1
                                     0
 IVEG
 -----
iteration 1; sweep 1
          1; sweep 2
1; sweep 3
iteration
iteration
          1; sweep 4
iteration
not possible to compute, first iteration
 Options given by user are activated for proceeding calculation:
       2 GRWMX 0.1000E+00 ALFA
                                        0.0000E+00
 ITER
           3 IWCAP
 IWIND
                        1 IQUAD
                                     2
 ITRIAD
           1 IBOT
                        1 ISURF
                                     1
                       0 IMUD
 IVEG
          0 ITURBV
                                     0
 _____
iteration 2; sweep 1
iteration
            2; sweep 2
iteration
            2; sweep 3
            2; sweep 4
iteration
accuracy OK in 33.34 % of wet grid points (99.50 % required)
iteration
            3; sweep 1
            3; sweep 2
iteration
iteration
            3; sweep 3
```

```
3; sweep 4
iteration
accuracy OK in 0.71 % of wet grid points (99.50 % required)
iteration
             4; sweep 1
             4; sweep 2
iteration
iteration
             4; sweep 3
iteration
             4; sweep
accuracy OK in 29.79 % of wet grid points (99.50 % required)
iteration
             5; sweep 1
iteration
             5; sweep 2
iteration
             5; sweep 3
iteration
             5; sweep
accuracy OK in 90.79 % of wet grid points (99.50 % required)
iteration
             6; sweep 1
iteration
             6; sweep 2
iteration
             6; sweep 3
             6; sweep
iteration
accuracy OK in 97.88 % of wet grid points (99.50 % required)
iteration
             7; sweep 1
iteration
             7; sweep 2
             7; sweep 3
iteration
            7; sweep 4
iteration
accuracy OK in 99.30 % of wet grid points (99.50 % required)
iteration
             8; sweep 1
iteration
             8; sweep 2
             8; sweep 3
iteration
             8; sweep 4
iteration
accuracy OK in 99.30 % of wet grid points (99.50 % required)
             9; sweep 1
iteration
iteration
            9; sweep 2
            9; sweep 3
iteration
            9; sweep 4
iteration
accuracy OK in 99.30 % of wet grid points ( 99.50 % required)
           10; sweep 1
iteration
iteration
           10; sweep 2
iteration
            10; sweep 3
iteration
           10; sweep 4
accuracy OK in 99.30 % of wet grid points (99.50 % required)
iteration
           11; sweep 1
iteration
           11; sweep 2
iteration
            11; sweep
iteration
           11; sweep 4
accuracy OK in 98.59 % of wet grid points (99.50 % required)
            12; sweep 1
iteration
iteration
           12; sweep 2
           12; sweep 3
iteration
           12; sweep 4
iteration
accuracy OK in 98.59 % of wet grid points (99.50 % required)
iteration
            13; sweep 1
iteration
           13; sweep 2
iteration
           13; sweep 3
iteration
            13; sweep 4
accuracy OK in 98.59 % of wet grid points (99.50 % required)
iteration
            14; sweep 1
iteration
           14; sweep 2
iteration
           14; sweep 3
            14; sweep
iteration
accuracy OK in 99.30 % of wet grid points ( 99.50 % required)
            15; sweep 1
iteration
iteration
            15; sweep 2
iteration
           15; sweep 3
iteration
            15; sweep
accuracy OK in 98.59 % of wet grid points (99.50 % required)
iteration
            16; sweep 1
iteration
            16; sweep 2
iteration
           16; sweep 3
            16; sweep
iteration
accuracy OK in 100.00 % of wet grid points ( 99.50 % required)
```

% % Run:1	Table:c	urve	SWAN vers	sion:41.20A						
% Xp % [m]	]	Yp [m]	Hsig [m]	TPsmoo [sec]	RTpeak [sec]	Tm_10 [sec]	Dir [degr]	Dspr [degr]	Depth [m]	Setup [m]
6	0.	0.	1.70739	10.1810	10.0005	9.4246	0.000	31.5063	10.0200	0.00000
	1.	0.	1.70663	10.1811	10.0005	9.4233	0.000	31.3287	9.9800	-0.000032
	2.	0.	1.70626	10.1814	10.0005	9.4232	0.000	31.0840	9.8899	-0.000107
	3.	0.	1.70619	10.1817	10.0005	9.4236	0.000	30.8480	9.7698	-0.000203
	4.	0.	1.70612	10.1821	10.0005	9.4240	0.000	30.6108	9.6497	-0.000302
	5.	0.	1.70616	10.1825	10.0005	9.4242	0.000	30.3693	9.5296	-0.000406
	6.	0.	1.70643	10.1828	10.0005	9.4244	0.000	30.1331	9.4095	-0.000515
	7.	0.	1.70664	10.1832	10.0005	9.4241	0.000	29.8985	9.2994	-0.000619
	8. 9.	0. 0.	1.70718 1.70787	10.1836 10.1841	10.0005	9.4239 9.4236	0.000	29.6576 29.4147	9.1793 9.0591	-0.000738 -0.000863
1	10.	0.	1.70872	10.1845	10.0005 10.0005	9.4230	0.000	29.1711	8.9390	-0.000863
	11.	0.	1.70981	10.1849	10.0005	9.4221	0.000	28.9342	8.8189	-0.001130
	12.	0.	1.71082	10.1854	10.0005	9.4207	0.000	28.6997	8.7087	-0.001261
	13.	0.	1.71220	10.1859	10.0005	9.4192	0.000	28.4602	8.5886	-0.001410
	14.	0.	1.71374	10.1863	10.0005	9.4173	0.000	28.2359	8.4684	-0.001562
	15.	0.	1.71543	10.1868	10.0005	9.4149	0.000	28.0242	8.3483	-0.001718
1	16.	0.	1.71733	10.1873	10.0005	9.4120	0.000	27.8191	8.2281	-0.001880
	17.	0.	1.71909	10.1878	10.0005	9.4082	0.000	27.6154	8.1180	-0.002035
	18.	0.	1.72124	10.1884	10.0005	9.4041	0.000	27.4053	7.9978	-0.002210
	19.	0.	1.72359	10.1889	10.0005	9.3993	0.000	27.1972	7.8776	-0.002392
	20.	0.	1.72589	10.1895	10.0005	9.3936	0.000	27.0013	7.7674	-0.002566
	21.	0.	1.72810	10.1900	10.0005	9.3867	360.000	26.8133	7.6673	-0.002730
	22.	0.	1.73048 1.73326	10.1905 10.1911	10.0005	9.3792 9.3711	360.000	26.6287	7.5671	-0.002901 -0.003077
	23. 24.	0. 0.	1.73480	10.1911	10.0005 10.0005	9.3606	360.000 0.000	26.4748 26.3615	7.4669 7.4168	-0.003077
	25.	0.	1.73655	10.1919	10.0005	9.3499	0.000	26.2686	7.3667	-0.003103
	26.	0.	1.73806	10.1923	10.0005	9.3385	0.000	26.1823	7.3267	-0.003338
	27.	0.	1.73996	10.1927	10.0005	9.3272	0.000	26.0978	7.2766	-0.003434
	28.	0.	1.74161	10.1931	10.0005	9.3153	0.000	26.0202	7.2365	-0.003513
	29.	0.	1.74324	10.1935	10.0005	9.3033	0.000	25.9385	7.1964	-0.003593
3	30.	0.	1.74526	10.1940	10.0005	9.2913	0.000	25.8551	7.1463	-0.003694
	31.	0.	1.74694	10.1944	10.0005	9.2787	0.000	25.7714	7.1062	-0.003777
	32.	0.	1.74901	10.1949	10.0005	9.2663	0.000	25.6872	7.0561	-0.003882
	33.	0.	1.75076	10.1953	10.0005	9.2531	0.000	25.6028	7.0160	-0.003967
	34.	0.	1.74008	10.1958	10.0005	9.2404	0.000	23.7793	6.9659	-0.004135
	35. 36.	0. 0.	1.88037 1.88014	10.2091 10.2126	10.0005 10.0005	9.2783 9.1662	0.000 0.000	21.2789 20.4124	4.1851 4.1650	-0.014897 -0.015030
	37.	0.	1.88052	10.2120	10.0005	9.0564	0.000	20.1945	4.1852	-0.013030
	38.	0.	1.88191	10.2189	10.0005	8.9572	0.000	20.1343	4.2054	-0.014797
	39.	0.	1.88465	10.2215	10.0005	8.8692	0.000	20.1152	4.2055	-0.014509
	40.	0.	1.88859	10.2238	10.0005	8.7906	0.000	20.0874	4.1854	-0.014587
	41.	0.	1.89084	10.2258	10.0005	8.7180	0.000	20.0980	4.1855	-0.014509
4	42.	0.	1.89121	10.2274	10.0005	8.6513	0.000	20.1008	4.2057	-0.014281
	43.	0.	1.89397	10.2289	10.0005	8.5931	0.000	20.0450	4.1856	-0.014354
	14.	0.	1.89875	10.2304	10.0005	8.5390	0.000	19.9734	4.1354	-0.014647
	45.	0.	1.90113	10.2316	10.0005	8.4856	0.000	19.9211	4.1153	-0.014702
	46.	0.	1.90347	10.2326	10.0005	8.4353	0.000	19.9017	4.0953	-0.014747
	47.	0. 0.	1.90281	10.2333 10.2338	10.0005	8.3858	0.000	19.9155	4.1155	-0.014476
	18. 19.	0.	1.90355 1.90284	10.2342	10.0005 10.0005	8.3417 8.2994	0.000	19.9390 19.9872	4.1156 4.1359	-0.014360 -0.014091
	50.	0.	1.90207	10.2342	10.0005	8.2603	0.000	20.0327	4.1562	-0.014091
	51.	0.	1.90187	10.2345	10.0005	8.2250	0.001	20.0327	4.1664	-0.013647
	52.	0.	1.90150	10.2345	10.0005	8.1922	0.001	20.0868	4.1765	-0.013470
	53.	0.	1.90171	10.2344	10.0005	8.1624	0.002	20.1022	4.1766	-0.013367
	54.	0.	1.90121	10.2343	10.0005	8.1335	0.002	20.1266	4.1868	-0.013191
	55.	0.	1.90068	10.2340	10.0005	8.1064	0.003	20.1536	4.1970	-0.013018
	56.	0.	1.90019	10.2337	10.0005	8.0808	0.003	20.1914	4.2072	-0.012847
	57.	0.	1.89904	10.2334	10.0005	8.0558	0.003	20.2333	4.2274	-0.012608
	58.	0.	1.89836	10.2330	10.0005	8.0332	0.003	20.2459	4.2376	-0.012447
5	59.	0.	1.89875	10.2327	10.0005	8.0135	0.004	20.2261	4.2276	-0.012430

ماه ماه ماه ماه ماه

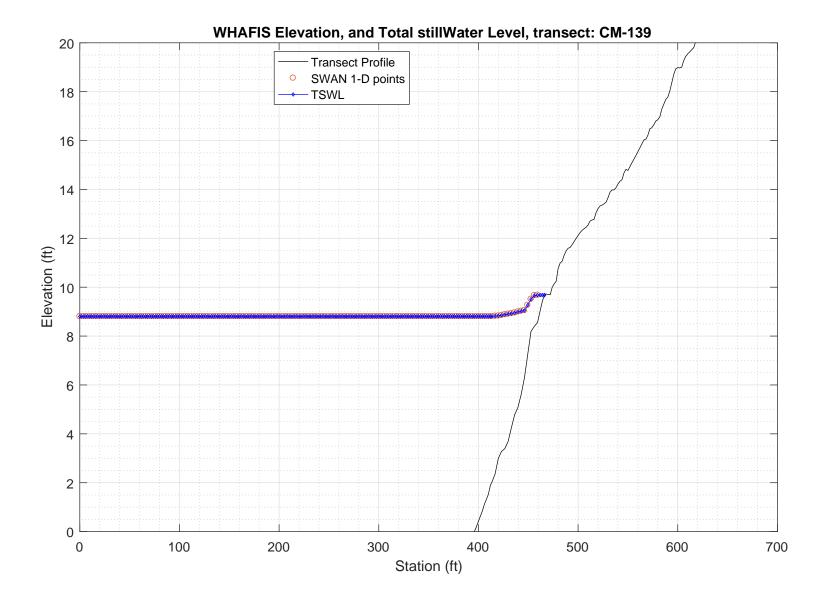
60.	0.	1.89962	10.2323	10.0005	7.9953	0.004	20.1881	4.2075	-0.012483
61.	0.	1.90032	10.2320	10.0005	7.9776	0.005	20.1367	4.1875	-0.012532
62.	0.	1.90163	10.2316	10.0005	7.9611	0.005	20.0876	4.1573	-0.012651
63.	0.	1.90294	10.2312	10.0005	7.9349	0.006	20.1001	4.1474	-0.012620
64.	0.	1.90094	10.2305	10.0005	7.9034	0.006	20.0984	4.1878	-0.012224
65.	0.	1.90428	10.2301	10.0005	7.8811	0.007	20.0071	4.1375	-0.012488
	0.	1.90897		10.0005	7.8602	0.007	19.9387	4.0671	-0.012892
66.		1.90897	10.2298		7.8602				
67.	0.	1.90819	10.2291	10.0005	7.8304	0.008	19.9881	4.0874	-0.012597
			10 0000						
68.	0.	1.90619	10.2283	10.0005	7.7991	0.009	20.1562	4.1379	-0.012082
69.	0.	1.90140	10.2274	10.0005	7.7649	0.010	20.3451	4.2387	-0.011250
			10 2067		7 7410				
70.	0.	1.90017	10.2267	10.0005	7.7412	0.010	20.4104	4.2691	-0.010942
71.	0.	1.90197	10.2262	10.0005	7.7251	0.010	20.3916	4.2390	-0.011050
72.	0.	1.90372	10.2257	10.0005	7.7087	0.010	20.3670	4.2088	-0.011155
73.	0.	1.90381	10.2251	10.0005	7.6889	0.011	20.3737	4.2090	-0.011048
			10 0044						
74.	0.	1.90328	10.2244	10.0005	7.6686	0.011	20.3915	4.2191	-0.010869
75.	0.	1.90329	10.2238	10.0005	7.6500	0.011	20.4034	4.2192	-0.010761
		1 00011	10.2230		7.6314				
76.	0.	1.90311	10.2232	10.0005	7.6314	0.011	20.3846	4.2193	-0.010655
77.	0.	1.90503	10.2227	10.0005	7.6172	0.013	20.3273	4.1792	-0.010824
78.	0.	1.90680	10.2222	10.0005	7.6024	0.015	20.2588	4.1390	-0.010988
79.	0.	1.90862	10.2217	10.0005	7.5871	0.017	20.2169	4.0989	-0.011141
			10 0011		7 5621				
80.	0.	1.90903	10.2211	10.0005	7.5631	0.020	20.2761	4.0990	-0.010992
81.	0.	1.90654	10.2202	10.0005	7.5312	0.025	20.4123	4.1596	-0.010421
	0.	1.90520	10.2195		7.5022	0.033			
82.		1.90520		10.0005			20.4971	4.2000	-0.010021
83.	0.	1.90726	10.2190	10.0005	7.4806	0.043	20.5585	4.1800	-0.010041
84.	0.	1.90657	10.2184	10.0005	7.4524	0.057	20.6305	4.2103	-0.009723
85.	0.	1.90798	10.2179	10.0005	7.4290	0.074	20.6698	4.2003	-0.009682
			10.0175						
86.	0.	1.90978	10.2175	10.0005	7.4070	0.093	20.6990	4.1803	-0.009706
87.	0.	1.91150	10.2171	10.0005	7.3851	0.115	20.7440	4.1603	-0.009723
	0.		10.2166		7.3619	0.136			
88.		1.91197		10.0005			20.8093	4.1604	-0.009596
89.	0.	1.91248	10.2162	10.0005	7.3400	0.153	20.9057	4.1605	-0.009465
90.	0.	1.91131	10.2156	10.0005	7.3153	0.165	21.0046	4.1909	-0.009135
			10.2136		7.3133				
91.	0.	1.91157	10.2152	10.0005	7.2958	0.170	21.0667	4.1910	-0.009013
92.	0.	1.91150	10.2148	10.0005	7.2780	0.168	21.1138	4.1911	-0.008889
		1.91130							
93.	0.	1.91138	10.2144	10.0005	7.2610	0.164	21.1650	4.1912	-0.008762
94.	0.	1.91081	10.2140	10.0005	7.2429	0.160	21.2269	4.2014	-0.008572
					1.2423				
95.	0.	1.91026	10.2136	10.0005	7.2253	0.157	21.2907	4.2116	-0.008386
96.	0.	1.90948	10.2133	10.0005	7.2089	0.153	21.3360	4.2218	-0.008203
		1.30340	10.2133		7.2009				
97.	0.	1.90941	10.2129	10.0005	7.1964	0.148	21.3493	4.2118	-0.008151
98.	0.	1.90950	10.2127	10.0005	7.1869	0.142	21.3463	4.1918	-0.008158
					7.1009				
99.	0.	1.90876	10.2124	10.0005	7.1776	0.133	21.3389	4.1819	-0.008092
100.	0.	1.90776	10.2121	10.0005	7.1698	0.122	21.3240	4.1720	-0.008021
					7.1090				
101.	0.	1.90656	10.2118	10.0005	7.1629	0.109	21.3032	4.1621	-0.007945
102.	0.	1.90524	10.2115	10.0005	7.1569	0.096	21.2852	4.1521	-0.007864
		1.90324	10.2113		7.1309				
103.	0.	1.90339	10.2112	10.0005	7.1497	0.084	21.2763	4.1523	-0.007714
104.	0.	1.90154	10.2109	10.0005	7.1427	0.072	21.2708	4.1524	-0.007564
								4.1324	
105.	0.	1.89971	10.2106	10.0005	7.1358	0.061	21.2673	4.1526	-0.007415
106.	0.	1.89790	10.2103	10.0005	7.1289	0.051	21.2657	4.1527	-0.007266
								1.1527	
107.	0.	1.89594	10.2100	10.0005	7.1219	0.042	21.2389	4.1529	-0.007121
108.	0.	1.89554	10.2099	10.0005	7.1203	0.034	21.1399	4.1128	-0.007238
			10.2000		7.1203				
109.	0.	1.89718	10.2099	10.0005	7.1257	0.025	20.9765	4.0223	-0.007687
110.	0.	1.89842	10.2099	10.0005	7.1306	0.015	20.8031	3.9319	-0.008126
		1.00012			7.1300			2.0515	
111.	0.	1.89779	10.2099	10.0005	7.1318	0.005	20.5786	3.8616	-0.008402
112.	0.	1.90140	10.2101	10.0005	7.1464	359.993	20.2814	3.7006	-0.009364
113.	0.	1.90182	10.2102	10.0005	7.1531	359.981	19.9928	3.5800	-0.009964
114.	0.	1.90125	10.2103	10.0005	7.1549	359.973	19.7481	3.4696	-0.010419
	0.								
115.		1.89564	10.2102	10.0005	7.1445	359.969	19.4710	3.4198	-0.010233
116.	0.	1.89780	10.2106	10.0005	7.1567	359.965	19.1036	3.2286	-0.011377
117.	0.	1.89298	10.2108	10.0005	7.1537	359.962	18.7822	3.1084	-0.011589
118.	0.	1.88448	10.2111	10.0005	7.1453	359.960	18.4724	3.0086	-0.011362
119.		1.87511	10.2114	10.0005	7.1387		18.1300	2.8888	-0.011172
	0.					359.956			
120.	0.	1.86373	10.2120	10.0005	7.1306	359.954	17.7657	2.7592	-0.010838
121.	0.	1.84829	10.2126	10.0005	7.1176	359.954	17.4110	2.6400	-0.009995
122.	0.	1.82783	10.2133	10.0005	7.0984	359.956	17.0681	2.5416	-0.008444
123.	0.	1.80495	10.2142	10.0005	7.0799	359.959	16.7059	2.4333	-0.006665
124.	0.	1.77941	10.2153	10.0005	7.0608	359.963	16.3291	2.3154	-0.004591
125.	0.	1.74963	10.2165	10.0005	7.0331	359.965	15.9374	2.2082	-0.001822
126.	0.	1.72155	10.2178	10.0005	6.9976	0.014	15.5361	2.0707	0.000682

	_								
127.	0.	1.68586	10.2189	10.0005	6.9408	0.093	15.0958	1.9747	0.004683
128.	0.	1.65893	10.2199	10.0005	6.8865	0.242	14.6090	1.7768	0.006826
129.	0.	1.60494	10.2201	10.0005	6.8220	0.317	14.2997	1.6942	0.014224
130.	0.	1.54911	10.2197	10.0005	6.7209	0.498	14.0632	1.6727	0.022668
131.	0.	1.49332	10.2192	10.0005	6.6811	0.560	13.7041	1.5900	0.030017
132.	0.	1.43913	10.2188	10.0005	6.6809	0.560	13.1883	1.4264	0.036399
133.	0.	1.37789	10.2187	10.0005	6.6754	0.526	12.6799	1.2747	0.044722
134.	0.	1.30403	10.2188	10.0005	6.6469	0.486	12.1687	1.1866	0.056625
135.	0.	1.24338	10.2186	10.0005	6.6271	0.424	11.5309	1.0361	0.066064
136.	0.	1.19186	10.2194	10.0005	6.6047	0.361	10.7415	0.8444	0.074396
137.	0.	0.90260	10.4342	10.0005	7.4537	359.019	10.8241	0.6106	0.140650
138.	0.	0.60724	11.0171	11.1572	8.4479	358.102	10.8320	0.4055	0.215470
139.	0.	0.40672	13.5028	13.8874	9.0559	357.195	10.5605	0.3907	0.260743
140.	0.	0.37907	13.6772	13.8874	8.4273	356.790	10.4531	0.3361	0.266076

PART 3: WHAFIS

WHAFIS input: CM-139.dat WHAFIS output: CM-139.out

PART 3 COMPLETE\_\_\_



WAVE HEIGHT COMPUTATIONS FOR FLOOD INSURANCE STUDIES (WHAFIS VERSION 4.0G, 08\_2007)

Executed on: Thu Feb 20 14:57:37 2020

Input file: C:\FEMA-TransectAnalysis\LOMR-TransectAnalysis-Harpswell\3\_whafis\whafis4\CM-139.dat
Output file: C:\FEMA-TransectAnalysis\LOMR-TransectAnalysis-Harpswell\3\_whafis\whafis4\CM-139.out
header

THIS IS A 100-YEAR CASE

THE FOLLOWING NON-DEFAULT WIND SPEEDS ARE BEING USED
WINDLE 56 14 WIN

			THE FOLLO			SPEEDS ARE				
					PART1 INE	PUT				
IE	0.000	-24.080	1.000	1.000	8.804 0.000	8.978	10.446	56.140	0.045	0.000
OF OF	2.000 4.000	-23.989 -23.898	0.000	8.804 8.804	0.000	0.000	0.000	0.000	0.045	0.000
OF	6.000	-23.699	0.000	8.804	0.000	0.000	0.000	0.000	0.109	0.000
OF	8.000	-23.463	0.000	8.804	0.000	0.000	0.000	0.000	0.118	0.000
OF	10.000	-23.226	0.000	8.804	0.000	0.000	0.000	0.000	0.118	0.000
OF	12.000	-22.990	0.000	8.804	0.000	0.000	0.000	0.000	0.118	0.000
OF OF	14.000 16.000	-22.754 -22.518	0.000	8.804 8.804	0.000	0.000	0.000	0.000	0.118 0.118	0.000
OF	18.000	-22.316	0.000	8.804	0.000	0.000	0.000	0.000	0.118	0.000
OF	20.000	-22.045	0.000	8.804	0.000	0.000	0.000	0.000	0.118	0.000
OF	22.000	-21.809	0.000	8.804	0.000	0.000	0.000	0.000	0.118	0.000
OF	24.000	-21.573	0.000	8.804	0.000	0.000	0.000	0.000	0.118	0.000
OF OF	26.000 28.000	-21.336 -21.100	0.000	8.804 8.804	0.000	0.000	0.000	0.000	0.118 0.118	0.000
OF	30.000	-20.864	0.000	8.804	0.000	0.000	0.000	0.000	0.118	0.000
OF	32.000	-20.628	0.000	8.804	0.000	0.000	0.000	0.000	0.118	0.000
OF	34.000	-20.392	0.000	8.804	0.000	0.000	0.000	0.000	0.118	0.000
OF	36.000 38.000	-20.155 -19.919	0.000	8.804 8.804	0.000	0.000	0.000	0.000	0.118 0.118	0.000
OF OF	40.000	-19.683	0.000	8.804	0.000	0.000	0.000	0.000	0.118	0.000
OF	42.000	-19.447	0.000	8.804	0.000	0.000	0.000	0.000	0.118	0.000
OF	44.000	-19.210	0.000	8.804	0.000	0.000	0.000	0.000	0.118	0.000
OF	46.000	-18.974	0.000	8.804	0.000	0.000	0.000	0.000	0.118	0.000
OF OF	48.000 50.000	-18.738 -18.502	0.000	8.804 8.804	0.000	0.000	0.000	0.000	0.118 0.118	0.000
OF	52.000	-18.265	0.000	8.804	0.000	0.000	0.000	0.000	0.118	0.000
OF	54.000	-18.029	0.000	8.804	0.000	0.000	0.000	0.000	0.118	0.000
OF	56.000	-17.793	0.000	8.804	0.000	0.000	0.000	0.000	0.118	0.000
OF OF	58.000 60.000	-17.557 -17.320	0.000	8.804 8.804	0.000	0.000	0.000	0.000	0.118 0.118	0.000
OF	62.000	-17.084	0.000	8.804	0.000	0.000	0.000	0.000	0.118	0.000
OF	64.000	-16.848	0.000	8.804	0.000	0.000	0.000	0.000	0.112	0.000
OF	66.000	-16.635	0.000	8.804	0.000	0.000	0.000	0.000	0.102	0.000
OF	68.000 70.000	-16.440	0.000	8.804	0.000	0.000	0.000	0.000	0.098	0.000
OF OF	70.000	-16.244 -16.048	0.000	8.804 8.804	0.000	0.000	0.000	0.000	0.098 0.098	0.000
OF	74.000	-15.852	0.000	8.804	0.000	0.000	0.000	0.000	0.098	0.000
OF	76.000	-15.657	0.000	8.804	0.000	0.000	0.000	0.000	0.071	0.000
OF	78.000	-15.568	0.000	8.804	0.000	0.000	0.000	0.000	0.045	0.000
OF OF	80.000 82.000	-15.479 -15.390	0.000	8.804 8.804	0.000	0.000	0.000	0.000	0.045	0.000
OF	84.000	-15.390	0.000	8.804	0.000	0.000	0.000	0.000	0.045	0.000
OF	86.000	-15.211	0.000	8.804	0.000	0.000	0.000	0.000	0.045	0.000
OF	88.000	-15.122	0.000	8.804	0.000	0.000	0.000	0.000	0.045	0.000
OF	90.000	-15.033	0.000	8.804	0.000	0.000	0.000	0.000	0.045	0.000
OF OF	92.000 94.000	-14.943 -14.854	0.000	8.804 8.804	0.000	0.000	0.000	0.000	0.045	0.000
OF	96.000	-14.765	0.000	8.804	0.000	0.000	0.000	0.000	0.045	0.000
OF	98.000	-14.676	0.000	8.804	0.000	0.000	0.000	0.000	0.045	0.000
OF	100.000	-14.586	0.000	8.804	0.000	0.000	0.000	0.000	0.045	0.000
OF OF	102.000 104.000	-14.497 -14.408	0.000	8.804 8.804	0.000	0.000	0.000	0.000	0.045	0.000
OF	106.000	-14.318	0.000	8.804	0.000	0.000	0.000	0.000	0.045	0.000
OF	108.000	-14.229	0.000	8.804	0.000	0.000	0.000	0.000	0.045	0.000
OF	110.000	-14.140	0.000	8.804	0.000	0.000	0.000	0.000	0.045	0.000
OF OF	112.000 114.000	-14.051 -4.981	0.000	8.804 8.804	0.000	0.000	0.000	0.000	2.290 2.275	0.000
OF	116.000	-4.950	0.000	8.804	0.000	0.000	0.000	0.000	0.015	0.000
OF	118.000	-4.920	0.000	8.804	0.000	0.000	0.000	0.000	0.005	0.000
OF	120.000	-4.928	0.000	8.804	0.000	0.000	0.000	0.000	-0.017	0.000
OF	122.000	-4.990	0.000	8.804	0.000	0.000	0.000	0.000	-0.024	0.000
OF OF	124.000 126.000	-5.025 -5.060	0.000	8.804 8.804	0.000	0.000	0.000	0.000	-0.018 -0.003	0.000
OF	128.000	-5.036	0.000	8.804	0.000	0.000	0.000	0.000	0.017	0.000
OF	130.000	-4.992	0.000	8.804	0.000	0.000	0.000	0.000	0.023	0.000
OF	132.000	-4.945	0.000	8.804	0.000	0.000	0.000	0.000	0.002	0.000
OF OF	134.000 136.000	-4.984 -4.986	0.000	8.804 8.804	0.000	0.000	0.000	0.000	-0.010 -0.017	0.000
OF	138.000	-5.054	0.000	8.804	0.000	0.000	0.000	0.000	-0.017	0.000
OF	140.000	-5.001	0.000	8.804	0.000	0.000	0.000	0.000	0.019	0.000
OF	142.000	-4.977	0.000	8.804	0.000	0.000	0.000	0.000	0.042	0.000
OF	144.000	-4.834	0.000	8.804	0.000	0.000	0.000	0.000	0.049	0.000
OF OF	146.000 148.000	-4.781 -4.720	0.000	8.804 8.804	0.000	0.000	0.000	0.000	0.029 0.029	0.000
OF	150.000	-4.666	0.000	8.804	0.000	0.000	0.000	0.000	0.006	0.000
OF	152.000	-4.694	0.000	8.804	0.000	0.000	0.000	0.000	-0.021	0.000
OF	154.000	-4.748	0.000	8.804	0.000	0.000	0.000	0.000	-0.012	0.000
OF OF	156.000 158.000	-4.743 -4.759	0.000	8.804 8.804	0.000	0.000	0.000	0.000	-0.003 -0.014	0.000
OF	160.000	-4.798	0.000	8.804	0.000	0.000	0.000	0.000	-0.014	0.000
OF	162.000	-4.836	0.000	8.804	0.000	0.000	0.000	0.000	-0.019	0.000
OF	164.000	-4.874	0.000	8.804	0.000	0.000	0.000	0.000	-0.019	0.000
OF	166.000	-4.913	0.000	8.804	0.000	0.000	0.000	0.000	-0.014	0.000
OF OF	168.000 170.000	-4.931 -4.940	0.000	8.804 8.804	0.000	0.000	0.000	0.000	-0.007 -0.005	0.000
OF	172.000	-4.949	0.000	8.804	0.000	0.000	0.000	0.000	-0.005	0.000
OF	174.000	-4.958	0.000	8.804	0.000	0.000	0.000	0.000	-0.005	0.000
OF	176.000	-4.968	0.000	8.804	0.000	0.000	0.000	0.000	-0.004	0.000
OF	178.000	-4.976	0.000	8.804	0.000	0.000	0.000	0.000	-0.009	0.000
OF OF	180.000 182.000	-5.003 -5.031	0.000	8.804 8.804	0.000	0.000	0.000	0.000	-0.014 -0.014	0.000
OF	184.000	-5.058	0.000	8.804	0.000	0.000	0.000	0.000	-0.014	0.000

OF 282.000	OF         246.000         -5.089         0.000         8.803         0.000 <td< th=""><th>0.004 0.000 0.029 0.000 0.053 0.000 0.035 0.000 0.035 0.000 0.035 0.000 0.035 0.000 0.035 0.000 0.014 0.000 0.057 0.000 0.057 0.000 0.022 0.000 0.021 0.000 0.021 0.000 0.021 0.000 0.026 0.000 0.007 0.000 0.007 0.000</th></td<>	0.004 0.000 0.029 0.000 0.053 0.000 0.035 0.000 0.035 0.000 0.035 0.000 0.035 0.000 0.035 0.000 0.014 0.000 0.057 0.000 0.057 0.000 0.022 0.000 0.021 0.000 0.021 0.000 0.021 0.000 0.026 0.000 0.007 0.000 0.007 0.000
OF         300.000         -4.979         0.000         8.803         0.000 <td< td=""><td>OF         282.000         -4.947         0.000         8.803         0.000         <th< td=""><td>0.029 0.000 0.020 0.000 0.003 0.000 -0.003 0.000 -0.003 0.000 -0.003 0.000 -0.003 0.000 -0.036 0.000 -0.026 0.000</td></th<></td></td<>	OF         282.000         -4.947         0.000         8.803         0.000 <th< td=""><td>0.029 0.000 0.020 0.000 0.003 0.000 -0.003 0.000 -0.003 0.000 -0.003 0.000 -0.003 0.000 -0.036 0.000 -0.026 0.000</td></th<>	0.029 0.000 0.020 0.000 0.003 0.000 -0.003 0.000 -0.003 0.000 -0.003 0.000 -0.003 0.000 -0.036 0.000 -0.026 0.000
OF         320.000         -4.997         0.000         8.804         0.000 <th< td=""><td>OF         300.000         -4.979         0.000         8.803         0.000         <th< td=""><td>0.004 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.005 0.000 0.009 0.000 0.009 0.000 0.009 0.000 0.009 0.000</td></th<></td></th<>	OF         300.000         -4.979         0.000         8.803         0.000 <th< td=""><td>0.004 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.005 0.000 0.009 0.000 0.009 0.000 0.009 0.000 0.009 0.000</td></th<>	0.004 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.005 0.000 0.009 0.000 0.009 0.000 0.009 0.000 0.009 0.000
OF         344.000         -4.850         0.000         8.805         0.000         0.000         0.000         0.000         0.000         0.000         0.001         0.000           OF         346.000         -4.848         0.000         8.805         0.000         0.000         0.000         0.000         0.001         0.000           OF         350.000         -4.839         0.000         8.805         0.000         0.000         0.000         0.001         0.001         0.001           OF         352.000         -4.839         0.000         8.805         0.000         0.000         0.000         0.000         0.001         0.002         0.001           OF         354.000         -4.726         0.000         8.805         0.000         0.000         0.000         0.000         0.000         0.064         0.000           OF         356.000         -4.364         0.000         8.805         0.000         0.000         0.000         0.000         0.001         0.000           OF         350.000         -4.364         0.000         8.805         0.000         0.000         0.000         0.000         0.000         0.000         0.000         0.000	OF         320.000         -4.997         0.000         8.804         0.000 <th< td=""><td>0.015 0.000 0.012 0.000 0.012 0.000 0.012 0.000 0.012 0.000 0.012 0.000 0.001 0.000 0.004 0.000 0.001 0.000 0.001 0.000 0.001 0.000</td></th<>	0.015 0.000 0.012 0.000 0.012 0.000 0.012 0.000 0.012 0.000 0.012 0.000 0.001 0.000 0.004 0.000 0.001 0.000 0.001 0.000 0.001 0.000
	OF         342,000         -4.851         0.000         8.804         0.000 <td< td=""><td>0.001 0.000 0.001 0.000 0.001 0.000 0.002 0.000 0.001 0.000 0.001 0.000 0.064 0.000 0.091 0.000 0.091 0.000 0.000 0.000</td></td<>	0.001 0.000 0.001 0.000 0.001 0.000 0.002 0.000 0.001 0.000 0.001 0.000 0.064 0.000 0.091 0.000 0.091 0.000 0.000 0.000

	OF OF OF IF	390.000 392.000 394.000 396.000 398.000 400.000 402.000 404.000 406.000 412.000 413.400 416.700 413.200 423.200 426.500 429.800 433.100 436.400 449.500 449.500 449.500 449.500 449.500 440.000 459.300 466.000 466.000 466.000 466.000	-0.766 -0.512 -0.245 0.005 0.202 0.420 0.641 0.845 1.123 1.317 1.532 1.891 2.011 2.347 2.995 3.284 3.394 3.394 4.250 4.783 5.082 5.614 6.293 7.251 8.192 8.393 8.561 9.045 9.403 9.668 9.677 0.000	0.000 0.000	8.806 8.806 8.806 8.806 8.806 8.806 8.806 8.806 8.806 8.806 8.806 8.806 8.806 8.806 9.801 9.801 9.021 9.048 9.021 9.048 9.021 9.048 9.021 9.048 9.021 9.048 9.0677 9.677 9.677 9.677 9.677 9.677	0.000 0.0000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.0000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.124 0.130 0.129 0.112 0.104 0.110 0.106 0.120 0.118 0.102 0.144 0.041 0.097 0.151 0.166 0.128 0.128 0.128 0.128 0.128 0.128 0.128 0.196 0.197 0.157 0.109 0.179 0.156 0.119 0.031 0.000
1 IE	END STATION 0.000 END	END ELEVATION -24.080 END	FETCH LENGTH 1.000 NEW SURGE	SURGE ELEV 10-YEAR 1.000 NEW SURGE	SURGE ELEV 100-YEAR 8.804	INITIAL WAVE HEIGHT 8.978	INITIAL W. PERIOD 10.446	56.140	BOTTOM SLOPE 0.045 BOTTOM	AVERAGE A-ZONES 0.000 AVERAGE
OF	STATION 2.000	ELEVATION -23.989	10-YEAR 0.000	100-YEAR 8.804	0.000	0.000	0.000	0.000	SLOPE 0.045 BOTTOM	A-ZONES 0.000 AVERAGE
OF	END STATION 4.000	END ELEVATION -23.898	NEW SURGE 10-YEAR 0.000	NEW SURGE 100-YEAR 8.804	0.000	0.000	0.000	0.000	SLOPE 0.072	A-ZONES 0.000
OF	END STATION 6.000	END ELEVATION -23.699	NEW SURGE 10-YEAR 0.000	NEW SURGE 100-YEAR 8.804	0.000	0.000	0.000	0.000	BOTTOM SLOPE 0.109	AVERAGE A-ZONES 0.000
OF	END STATION 8.000	END ELEVATION -23.463	NEW SURGE 10-YEAR 0.000	NEW SURGE 100-YEAR 8.804	0.000	0.000	0.000	0.000	BOTTOM SLOPE 0.118	AVERAGE A-ZONES 0.000
OF	END STATION 10.000	END ELEVATION -23.226	NEW SURGE 10-YEAR 0.000	NEW SURGE 100-YEAR 8.804	0.000	0.000	0.000	0.000	BOTTOM SLOPE 0.118	AVERAGE A-ZONES 0.000
OF	END STATION 12.000	END ELEVATION -22.990	NEW SURGE 10-YEAR 0.000	NEW SURGE 100-YEAR 8.804	0.000	0.000	0.000	0.000	BOTTOM SLOPE 0.118	AVERAGE A-ZONES 0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	14.000 END STATION	-22.754 END ELEVATION	0.000 NEW SURGE 10-YEAR	8.804 NEW SURGE 100-YEAR	0.000	0.000	0.000	0.000	0.118 BOTTOM SLOPE	0.000 AVERAGE A-ZONES
OF	16.000 END STATION	-22.518 END ELEVATION	0.000 NEW SURGE 10-YEAR	8.804 NEW SURGE 100-YEAR	0.000	0.000	0.000	0.000	0.118 BOTTOM SLOPE	0.000 AVERAGE A-ZONES
OF	18.000 END	-22.281 END	0.000 NEW SURGE	8.804 NEW SURGE	0.000	0.000	0.000	0.000	0.118 BOTTOM	0.000 AVERAGE
OF	20.000 END			100-YEAR 8.804 NEW SURGE	0.000	0.000	0.000	0.000	SLOPE 0.118 BOTTOM	A-ZONES 0.000 AVERAGE
OF	STATION 22.000 END	ELEVATION -21.809 END	10-YEAR 0.000 NEW SURGE	100-YEAR 8.804 NEW SURGE	0.000	0.000	0.000	0.000	SLOPE 0.118 BOTTOM	A-ZONES 0.000 AVERAGE
OF	STATION 24.000 END	ELEVATION -21.573 END	10-YEAR 0.000 NEW SURGE	100-YEAR 8.804 NEW SURGE	0.000	0.000	0.000	0.000	SLOPE 0.118 BOTTOM	A-ZONES 0.000 AVERAGE
OF		ELEVATION -21.336	10-YEAR 0.000 NEW SURGE	100-YEAR 8.804	0.000	0.000	0.000	0.000	SLOPE 0.118 BOTTOM	A-ZONES 0.000 AVERAGE
OF	STATION 28.000	ELEVATION -21.100	10-YEAR 0.000	100-YEAR 8.804	0.000	0.000	0.000	0.000	SLOPE 0.118	A-ZONES 0.000
OF	END STATION 30.000	END ELEVATION -20.864	NEW SURGE 10-YEAR 0.000	NEW SURGE 100-YEAR 8.804	0.000	0.000	0.000	0.000	BOTTOM SLOPE 0.118	AVERAGE A-ZONES 0.000
OF	END STATION 32.000	END ELEVATION -20.628	NEW SURGE 10-YEAR 0.000	NEW SURGE 100-YEAR 8.804	0.000	0.000	0.000	0.000	BOTTOM SLOPE 0.118	AVERAGE A-ZONES 0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	34.000 END STATION	-20.392 END ELEVATION	0.000 NEW SURGE 10-YEAR	100-YEAR	0.000	0.000	0.000	0.000	0.118 BOTTOM SLOPE	0.000 AVERAGE A-ZONES
OF	36.000 END	-20.155	0.000 NEW SURGE 10-YEAR	8.804 NEW SURGE 100-YEAR	0.000	0.000	0.000	0.000	0.118 BOTTOM SLOPE	0.000 AVERAGE A-ZONES
OF	38.000 END	-19.919 END	0.000 NEW SURGE	8.804 NEW SURGE	0.000	0.000	0.000	0.000	0.118 BOTTOM	0.000 AVERAGE
OF	40.000 END	ELEVATION -19.683 END	10-YEAR 0.000 NEW SURGE		0.000	0.000	0.000	0.000	SLOPE 0.118 BOTTOM	A-ZONES 0.000 AVERAGE
OF	STATION 42.000 END	-19.447 END	10-YEAR 0.000 NEW SURGE	100-YEAR 8.804 NEW SURGE	0.000	0.000	0.000	0.000	SLOPE 0.118 BOTTOM	A-ZONES 0.000 AVERAGE
OF	STATION 44.000	ELEVATION -19.210	10-YEAR 0.000	100-YEAR 8.804	0.000	0.000	0.000	0.000	SLOPE 0.118	A-ZONES 0.000

0.000 0.000

	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	46.000	-18.974	0.000	8.804	0.000	0.000	0.000	0.000	0.118	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 48.000	ELEVATION -18.738	10-YEAR 0.000	100-YEAR 8.804	0.000	0.000	0.000	0.000	SLOPE 0.118	A-ZONES 0.000
01	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	50.000 END	-18.502 END	0.000 NEW SURGE	8.804 NEW SURGE	0.000	0.000	0.000	0.000	0.118 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	52.000	-18.265	0.000	8.804	0.000	0.000	0.000	0.000	0.118	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	54.000	-18.029	0.000	8.804	0.000	0.000	0.000	0.000	0.118	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	56.000	-17.793	0.000	8.804	0.000	0.000	0.000	0.000	0.118	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 58.000	ELEVATION -17.557	10-YEAR 0.000	100-YEAR 8.804	0.000	0.000	0.000	0.000	SLOPE 0.118	A-ZONES 0.000
OF	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	60.000 END	-17.320 END	0.000 NEW SURGE	8.804 NEW SURGE	0.000	0.000	0.000	0.000	0.118 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	62.000	-17.084	0.000	8.804	0.000	0.000	0.000	0.000	0.118	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	64.000	-16.848	0.000	8.804	0.000	0.000	0.000	0.000	0.112	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	66.000	-16.635	0.000	8.804	0.000	0.000	0.000	0.000	0.102	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 68.000	ELEVATION -16.440	10-YEAR 0.000	100-YEAR 8.804	0.000	0.000	0.000	0.000	SLOPE 0.098	A-ZONES 0.000
OF	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR	0.000				SLOPE	A-ZONES
OF	70.000 END	-16.244 END	0.000 NEW SURGE	8.804 NEW SURGE	0.000	0.000	0.000	0.000	0.098 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	72.000	-16.048	0.000	8.804	0.000	0.000	0.000	0.000	0.098	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	74.000	-15.852	0.000	8.804	0.000	0.000	0.000	0.000	0.098	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	76.000	-15.657	0.000	8.804	0.000	0.000	0.000	0.000	0.071	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 78.000	ELEVATION -15.568	10-YEAR 0.000	100-YEAR 8.804	0.000	0.000	0.000	0.000	SLOPE 0.045	A-ZONES 0.000
OF	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	80.000 END	-15.479 END	0.000 NEW SURGE	8.804 NEW SURGE	0.000	0.000	0.000	0.000	0.045 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	82.000 END	-15.390 END	0.000 NEW SURGE	8.804	0.000	0.000	0.000	0.000	0.045	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	A-ZONES
OF	84.000	-15.300	0.000	8.804	0.000	0.000	0.000	0.000	0.045	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	86.000	-15.211	0.000	8.804	0.000	0.000	0.000	0.000	0.045	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 88.000	ELEVATION -15.122	10-YEAR 0.000	100-YEAR 8.804	0.000	0.000	0.000	0.000	SLOPE 0.045	A-ZONES 0.000
01	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
OF	STATION 90.000	ELEVATION -15.033	10-YEAR 0.000	100-YEAR 8.804	0.000	0.000	0.000	0.000	SLOPE 0.045	A-ZONES 0.000
Or	END	-15.033 END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	92.000 END	-14.943 END	0.000 NEW SURGE	8.804 NEW SURGE	0.000	0.000	0.000	0.000	0.045 BOTTOM	0.000 AVERAGE
		ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	94.000	-14.854	0.000 NEW SURGE	8.804	0.000	0.000	0.000	0.000	0.045	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	96.000	-14.765	0.000	8.804	0.000	0.000	0.000	0.000	0.045	0.000
	END	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	98.000	-14.676	0.000	8.804	0.000	0.000	0.000	0.000	0.045	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 100.000	ELEVATION -14.586	10-YEAR 0.000	100-YEAR 8.804	0.000	0.000	0.000	0.000	SLOPE 0.045	A-ZONES 0.000
01	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
O.E.		ELEVATION -14.497	10-YEAR 0.000	100-YEAR	0.000	0.000	0.000	0.000	SLOPE	A-ZONES 0.000
OF	102.000 END	-14.497 END	NEW SURGE	8.804 NEW SURGE	0.000	0.000	0.000	0.000	0.045 BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	104.000 END	-14.408 END	0.000 NEW SURGE	8.804 NEW SURGE	0.000	0.000	0.000	0.000	0.045 BOTTOM	0.000 AVERAGE
		ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	106.000	-14.318	0.000	8.804	0.000	0.000	0.000	0.000	0.045	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	108.000	-14.229	0.000	8.804	0.000	0.000	0.000	0.000	0.045	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 110.000	ELEVATION -14.140	10-YEAR 0.000	100-YEAR 8.804	0.000	0.000	0.000	0.000	SLOPE 0.045	A-ZONES 0.000
	END	END	NEW SURGE	NEW SURGE			<del>-</del>		BOTTOM	AVERAGE
OF	STATION 112.000	ELEVATION -14.051	10-YEAR 0.000	100-YEAR 8.804	0.000	0.000	0.000	0.000	SLOPE 2.290	A-ZONES 0.000
91	000	11.031	0.000	2.004	3.000	3.000	0.000	0.000	2.270	5.000

	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	114.000	-4.981	0.000	8.804	0.000	0.000	0.000	0.000	2.275	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 116.000	ELEVATION -4.950	10-YEAR 0.000	100-YEAR 8.804	0.000	0.000	0.000	0.000	SLOPE 0.015	A-ZONES 0.000
O1	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR	0.000				SLOPE	A-ZONES
OF	118.000 END	-4.920 END	0.000 NEW SURGE	8.804 NEW SURGE	0.000	0.000	0.000	0.000	0.005 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	120.000	-4.928	0.000	8.804	0.000	0.000	0.000	0.000	-0.017	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	122.000	-4.990	0.000	8.804	0.000	0.000	0.000	0.000	-0.024	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 124.000	ELEVATION -5.025	10-YEAR 0.000	100-YEAR 8.804	0.000	0.000	0.000	0.000	SLOPE -0.018	A-ZONES 0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 126.000	ELEVATION	10-YEAR 0.000	100-YEAR 8.804	0.000	0.000	0.000	0.000	SLOPE -0.003	A-ZONES 0.000
OF	END	-5.060 END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	128.000 END	-5.036 END	0.000 NEW SURGE	8.804 NEW SURGE	0.000	0.000	0.000	0.000	0.017 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	130.000	-4.992	0.000	8.804	0.000	0.000	0.000	0.000	0.023	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	132.000	-4.945	0.000	8.804	0.000	0.000	0.000	0.000	0.002	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 134.000	ELEVATION -4.984	10-YEAR 0.000	100-YEAR 8.804	0.000	0.000	0.000	0.000	SLOPE -0.010	A-ZONES 0.000
O1	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	136.000 END	-4.986 END	0.000 NEW SURGE	8.804 NEW SURGE	0.000	0.000	0.000	0.000	-0.017 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	138.000 END	-5.054 END	0.000 NEW SURGE	8.804	0.000	0.000	0.000	0.000	-0.004	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	A-ZONES
OF	140.000	-5.001	0.000	8.804	0.000	0.000	0.000	0.000	0.019	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	142.000	-4.977	0.000	8.804	0.000	0.000	0.000	0.000	0.042	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 144.000	ELEVATION -4.834	10-YEAR 0.000	100-YEAR 8.804	0.000	0.000	0.000	0.000	SLOPE 0.049	A-ZONES 0.000
OF	END	-4.634 END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	146.000 END	-4.781 END	0.000 NEW SURGE	8.804 NEW SURGE	0.000	0.000	0.000	0.000	0.029 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	148.000	-4.720	0.000	8.804	0.000	0.000	0.000	0.000	0.029	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	150.000	-4.666	0.000	8.804	0.000	0.000	0.000	0.000	0.006	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 152.000	ELEVATION -4.694	10-YEAR 0.000	100-YEAR 8.804	0.000	0.000	0.000	0.000	SLOPE -0.021	A-ZONES 0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR	0.000	0 000	0.000	0 000	SLOPE	A-ZONES
OF	154.000 END	-4.748 END	0.000 NEW SURGE	8.804 NEW SURGE	0.000	0.000	0.000	0.000	-0.012 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	156.000 END	-4.743 END	0.000 NEW SURGE	8.804 NEW SURGE	0.000	0.000	0.000	0.000	-0.003 BOTTOM	0.000 AVERAGE
		ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	158.000	-4.759	0.000	8.804	0.000	0.000	0.000	0.000	-0.014	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	160.000	-4.798	0.000	8.804	0.000	0.000	0.000	0.000	-0.019	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 162.000	ELEVATION -4.836	10-YEAR 0.000	100-YEAR 8.804	0.000	0.000	0.000	0.000	SLOPE -0.019	A-ZONES 0.000
01	END	END	NEW SURGE	NEW SURGE	3.000	0.000	0.000	3.000	BOTTOM	AVERAGE
0.7	STATION	ELEVATION	10-YEAR	100-YEAR	0.000	0.000	0.000	0 000	SLOPE	A-ZONES
OF	164.000 END	-4.874 END	0.000 NEW SURGE	8.804 NEW SURGE	0.000	0.000	0.000	0.000	-0.019 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	166.000 END	-4.913 END	0.000 NEW SURGE	8.804 NEW SURGE	0.000	0.000	0.000	0.000	-0.014 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	168.000	-4.931	0.000	8.804	0.000	0.000	0.000	0.000	-0.007	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	170.000	-4.940	0.000	8.804	0.000	0.000	0.000	0.000	-0.005	0.000
	END	END	NEW SURGE	NEW SURGE		-	-		BOTTOM	AVERAGE
OF	STATION 172.000	ELEVATION -4.949	10-YEAR 0.000	100-YEAR 8.804	0.000	0.000	0.000	0.000	SLOPE -0.005	A-ZONES 0.000
Or.	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
0=	STATION	ELEVATION	10-YEAR	100-YEAR	0.000	0.000	0.000	0.000	SLOPE	A-ZONES
OF	174.000 END	-4.958 END	0.000 NEW SURGE	8.804 NEW SURGE	0.000	0.000	0.000	0.000	-0.005 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	176.000	-4.968	0.000	8.804	0.000	0.000	0.000	0.000	-0.004	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	178.000	-4.976	0.000	8.804	0.000	0.000	0.000	0.000	-0.009	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	180.000	-5.003	0.000	8.804	0.000	0.000	0.000	0.000	-0.014	0.000
		<del>-</del>	<del>-</del>			-	-			

	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	182.000	-5.031	0.000	8.804	0.000	0.000	0.000	0.000	-0.014	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 184.000	ELEVATION -5.058	10-YEAR 0.000	100-YEAR 8.804	0.000	0.000	0.000	0.000	SLOPE -0.014	A-ZONES 0.000
OF	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR	0.000				SLOPE	A-ZONES
OF	186.000 END	-5.086 END	0.000 NEW SURGE	8.804 NEW SURGE	0.000	0.000	0.000	0.000	-0.014 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	188.000	-5.113	0.000	8.804	0.000	0.000	0.000	0.000	-0.011	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	190.000	-5.131	0.000	8.804	0.000	0.000	0.000	0.000	-0.007	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 192.000	ELEVATION -5.141	10-YEAR 0.000	100-YEAR 8.804	0.000	0.000	0.000	0.000	SLOPE 0.008	A-ZONES 0.000
OF	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	194.000 END	-5.098 END	0.000 NEW SURGE	8.804 NEW SURGE	0.000	0.000	0.000	0.000	0.020 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	196.000	-5.063	0.000	8.804	0.000	0.000	0.000	0.000	0.018	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	198.000	-5.027	0.000	8.804	0.000	0.000	0.000	0.000	0.021	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 200.000	ELEVATION -4.979	10-YEAR 0.000	100-YEAR 8.804	0.000	0.000	0.000	0.000	SLOPE 0.027	A-ZONES 0.000
OF	END	-4.979 END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	202.000 END	-4.920 END	0.000 NEW SURGE	8.804 NEW SURGE	0.000	0.000	0.000	0.000	0.030 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	204.000	-4.861	0.000	8.804	0.000	0.000	0.000	0.000	0.030	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM	AVERAGE A-ZONES
OF	206.000	-4.802	0.000	8.804	0.000	0.000	0.000	0.000	SLOPE -0.007	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 208.000	ELEVATION -4.888	10-YEAR 0.000	100-YEAR 8.804	0.000	0.000	0 000	0.000	SLOPE -0.047	A-ZONES 0.000
OF	208.000 END	-4.888 END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	210.000 END	-4.988 END	0.000 NEW SURGE	8.804	0.000	0.000	0.000	0.000	-0.008	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	A-ZONES
OF	212.000	-4.918	0.000	8.804	0.000	0.000	0.000	0.000	0.055	0.000
	END STATION	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	214.000	ELEVATION -4.769	10-YEAR 0.000	100-YEAR 8.804	0.000	0.000	0.000	0.000	SLOPE 0.075	A-ZONES 0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR	100-YEAR	0.000	0.000	0.000	0 000	SLOPE	A-ZONES
OF	216.000 END	-4.620 END	0.000 NEW SURGE	8.804 NEW SURGE	0.000	0.000	0.000	0.000	0.059 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	218.000	-4.532	0.000	8.804	0.000	0.000	0.000	0.000	-0.007	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	220.000	-4.645	0.000	8.803	0.000	0.000	0.000	0.000	-0.061	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 222.000	ELEVATION -4.777	10-YEAR 0.000	100-YEAR 8.803	0.000	0.000	0.000	0.000	SLOPE -0.047	A-ZONES 0.000
01	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
0.17		ELEVATION	10-YEAR	100-YEAR	0.000	0.000	0.000	0.000	SLOPE	A-ZONES
OF	224.000 END	-4.834 END	0.000 NEW SURGE	8.803 NEW SURGE	0.000	0.000	0.000	0.000	-0.083 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	226.000	-5.109	0.000	8.803	0.000	0.000	0.000	0.000	-0.106	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	228.000	-5.258	0.000	8.803	0.000	0.000	0.000	0.000	-0.035	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 230.000	ELEVATION -5.248	10-YEAR 0.000	100-YEAR 8.803	0.000	0.000	0.000	0.000	SLOPE 0.021	A-ZONES 0.000
<b>01</b>	END	END	NEW SURGE	NEW SURGE	3.000	0.000	3.000	0.000	BOTTOM	AVERAGE
0-	STATION	ELEVATION	10-YEAR	100-YEAR	0.000	0 000	0.000	0.000	SLOPE	A-ZONES
OF	232.000 END	-5.175 END	0.000 NEW SURGE	8.803 NEW SURGE	0.000	0.000	0.000	0.000	0.036 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	234.000	-5.102	0.000	8.803	0.000	0.000	0.000	0.000	0.036	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	236.000	-5.029	0.000	8.803	0.000	0.000	0.000	0.000	0.020	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 238.000	ELEVATION -5.021	10-YEAR 0.000	100-YEAR 8.803	0.000	0.000	0.000	0.000	SLOPE -0.008	A-ZONES 0.000
OI.	END	END	NEW SURGE	NEW SURGE	3.000	0.000	0.000	0.000	BOTTOM	AVERAGE
0-	STATION	ELEVATION	10-YEAR	100-YEAR	0.000	0 000	0.000	0.000	SLOPE	A-ZONES
OF	240.000 END	-5.060 END	0.000 NEW SURGE	8.803 NEW SURGE	0.000	0.000	0.000	0.000	-0.012 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	242.000	-5.068	0.000	8.803	0.000	0.000	0.000	0.000	-0.007	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	244.000	-5.089	0.000	8.803	0.000	0.000	0.000	0.000	-0.005	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 246.000	ELEVATION -5.089	10-YEAR 0.000	100-YEAR 8.803	0.000	0.000	0.000	0.000	SLOPE 0.002	A-ZONES 0.000
01	END	END	NEW SURGE	NEW SURGE	5.000	0.000	0.000	0.000	BOTTOM	AVERAGE
0.7	STATION	ELEVATION	10-YEAR	100-YEAR	0.000	0.000	0.000	0 000	SLOPE	A-ZONES
OF	248.000	-5.082	0.000	8.803	0.000	0.000	0.000	0.000	0.004	0.000

	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 250.000	ELEVATION -5.075	10-YEAR 0.000	100-YEAR 8.803	0.000	0.000	0.000	0.000	SLOPE 0.029	A-ZONES 0.000
OF	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	252.000	-4.968	0.000	8.803	0.000	0.000	0.000	0.000	0.053	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	254.000	-4.862	0.000	8.803	0.000	0.000	0.000	0.000	0.044	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR	0 000		0.000		SLOPE	A-ZONES
OF	256.000 END	-4.792 END	0.000 NEW SURGE	8.803 NEW SURGE	0.000	0.000	0.000	0.000	0.035 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	258.000	-4.722	0.000	8.803	0.000	0.000	0.000	0.000	0.035	0.000
	END	END ELEVATION	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 260.000	-4.651	10-YEAR 0.000	100-YEAR 8.803	0.000	0.000	0.000	0.000	SLOPE 0.014	A-ZONES 0.000
01	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	262.000 END	-4.668 END	0.000 NEW SURGE	8.803 NEW SURGE	0.000	0.000	0.000	0.000	-0.033 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	264.000	-4.782	0.000	8.803	0.000	0.000	0.000	0.000	-0.057	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 266.000	ELEVATION -4.895	10-YEAR 0.000	100-YEAR 8.803	0.000	0.000	0.000	0.000	SLOPE -0.057	A-ZONES 0.000
01	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	268.000 END	-5.009 END	0.000 NEW SURGE	8.803 NEW SURGE	0.000	0.000	0.000	0.000	-0.022 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	270.000	-4.984	0.000	8.803	0.000	0.000	0.000	0.000	0.021	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 272.000	ELEVATION -4.925	10-YEAR 0.000	100-YEAR 8.803	0.000	0.000	0.000	0.000	SLOPE -0.014	A-ZONES 0.000
01	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	274.000 END	-5.042 END	0.000 NEW SURGE	8.803 NEW SURGE	0.000	0.000	0.000	0.000	-0.026 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	276.000	-5.028	0.000	8.803	0.000	0.000	0.000	0.000	0.007	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 278.000	ELEVATION -5.015	10-YEAR 0.000	100-YEAR 8.803	0.000	0.000	0.000	0.000	SLOPE 0.007	A-ZONES 0.000
OF	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	280.000 END	-5.001 END	0.000 NEW SURGE	8.803 NEW SURGE	0.000	0.000	0.000	0.000	0.017 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	282.000	-4.947	0.000	8.803	0.000	0.000	0.000	0.000	0.029	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 284.000	ELEVATION -4.885	10-YEAR 0.000	100-YEAR 8.803	0.000	0.000	0.000	0.000	SLOPE 0.020	A-ZONES 0.000
OF	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	286.000 END	-4.866 END	0.000 NEW SURGE	8.803	0.000	0.000	0.000	0.000	0.003	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	A-ZONES
OF	288.000	-4.872	0.000	8.803	0.000	0.000	0.000	0.000	-0.003	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 290.000	ELEVATION -4.878	10-YEAR 0.000	100-YEAR 8.803	0.000	0.000	0.000	0.000	SLOPE -0.003	A-ZONES 0.000
01	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
		ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	292.000 END	-4.884 END	0.000 NEW SURGE	8.803 NEW SURGE	0.000	0.000	0.000	0.000	-0.003 BOTTOM	0.000 AVERAGE
		ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	294.000	-4.890	0.000	8.803	0.000	0.000	0.000	0.000	-0.036	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 296.000	ELEVATION -5.027	10-YEAR 0.000	100-YEAR 8.803	0.000	0.000	0.000	0.000	SLOPE -0.026	A-ZONES 0.000
01	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
0-	STATION	ELEVATION	10-YEAR	100-YEAR	0.000	0 000	0.000	0.000	SLOPE	A-ZONES
OF	298.000 END	-4.993 END	0.000 NEW SURGE	8.803 NEW SURGE	0.000	0.000	0.000	0.000	0.012 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	300.000	-4.979	0.000	8.803	0.000	0.000	0.000	0.000	0.004	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 302.000	ELEVATION -4.978	10-YEAR 0.000	100-YEAR 8.803	0.000	0.000	0.000	0.000	SLOPE 0.000	A-ZONES 0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR	0.000		0.000		SLOPE	A-ZONES
OF	304.000 END	-4.977 END	0.000 NEW SURGE	8.803 NEW SURGE	0.000	0.000	0.000	0.000	0.000 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	306.000	-4.979	0.000	8.803	0.000	0.000	0.000	0.000	-0.005	0.000
	END	END	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM	AVERAGE
OF	STATION 308.000	ELEVATION -4.998	0.000	8.804	0.000	0.000	0.000	0.000	SLOPE -0.009	A-ZONES 0.000
	END	END	NEW SURGE	NEW SURGE	3.330	000	2.000	000	BOTTOM	AVERAGE
0-	STATION	ELEVATION	10-YEAR	100-YEAR	0.000	0 000	0.000	0.000	SLOPE	A-ZONES
OF	310.000 END	-5.016 END	0.000 NEW SURGE	8.804 NEW SURGE	0.000	0.000	0.000	0.000	-0.009 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	312.000	-5.035	0.000	8.804	0.000	0.000	0.000	0.000	-0.009	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	314.000	-5.053	0.000	8.804	0.000	0.000	0.000	0.000	-0.009	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
O.E.	STATION	ELEVATION	10-YEAR	100-YEAR	0.000	0 000	0.000	0 000	SLOPE	A-ZONES
OF	316.000	-5.071	0.000	8.804	0.000	0.000	0.000	0.000	0.005	0.000

	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 318.000	ELEVATION -5.034	10-YEAR 0.000	100-YEAR 8.804	0.000	0.000	0.000	0.000	SLOPE 0.018	A-ZONES 0.000
01	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	320.000	-4.997	0.000 NEW SURGE	8.804 NEW SURGE	0.000	0.000	0.000	0.000	0.015	0.000
	END STATION	END ELEVATION	10-YEAR	100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	322.000	-4.973	0.000	8.804	0.000	0.000	0.000	0.000	0.012	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 324.000	ELEVATION -4.949	10-YEAR 0.000	100-YEAR 8.804	0 000	0.000	0 000	0 000	SLOPE 0.012	A-ZONES 0.000
OF	324.000 END	-4.949 END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	326.000	-4.925	0.000	8.804	0.000	0.000	0.000	0.000	0.012	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	328.000	-4.902	0.000	8.804	0.000	0.000	0.000	0.000	0.012	0.000
01	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	330.000 END	-4.878 END	0.000 NEW SURGE	8.804 NEW SURGE	0.000	0.000	0.000	0.000	0.009 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	332.000	-4.864	0.000	8.804	0.000	0.000	0.000	0.000	0.004	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 334.000	ELEVATION -4.861	10-YEAR 0.000	100-YEAR 8.804	0.000	0.000	0.000	0.000	SLOPE 0.001	A-ZONES 0.000
OF	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	336.000	-4.859	0.000 NEW SURGE	8.804	0.000	0.000	0.000	0.000	0.001 BOTTOM	0.000
	END STATION	END ELEVATION	10-YEAR	NEW SURGE 100-YEAR					SLOPE	AVERAGE A-ZONES
OF	338.000	-4.856	0.000	8.804	0.000	0.000	0.000	0.000	0.001	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION	ELEVATION	10-YEAR 0.000	100-YEAR	0.000	0 000	0 000	0 000	SLOPE	A-ZONES 0.000
OF	340.000 END	-4.853 END	NEW SURGE	8.804 NEW SURGE	0.000	0.000	0.000	0.000	0.001 BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	342.000	-4.851	0.000	8.804	0.000	0.000	0.000	0.000	0.001	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	344.000	-4.850	0.000	8.805	0.000	0.000	0.000	0.000	0.001	0.000
01	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	346.000 END	-4.848 END	0.000 NEW SURGE	8.805 NEW SURGE	0.000	0.000	0.000	0.000	0.001 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	348.000	-4.844	0.000	8.805	0.000	0.000	0.000	0.000	0.002	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 350.000	ELEVATION -4.839	10-YEAR 0.000	100-YEAR 8.805	0.000	0.000	0.000	0.000	SLOPE 0.001	A-ZONES 0.000
OF	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	352.000	-4.839	0.000 NEW SURGE	8.805	0.000	0.000	0.000	0.000	0.028	0.000
	END STATION	END ELEVATION	10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	354.000	-4.726	0.000	8.805	0.000	0.000	0.000	0.000	0.064	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 356.000	ELEVATION -4.583	10-YEAR 0.000	100-YEAR 8.805	0.000	0.000	0.000	0.000	SLOPE 0.091	A-ZONES 0.000
OF	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	358.000	-4.364	0.000	8.805	0.000	0.000	0.000	0.000	0.100	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	360.000	-4.182	0.000	8.805	0.000	0.000	0.000	0.000	0.080	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
0.11		ELEVATION	10-YEAR	100-YEAR	0.000	0.000	0.000	0 000	SLOPE	A-ZONES
OF	362.000 END	-4.045 END	0.000 NEW SURGE	8.805 NEW SURGE	0.000	0.000	0.000	0.000	0.064 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	364.000	-3.928	0.000	8.805	0.000	0.000	0.000	0.000	0.096	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	366.000	-3.661	0.000	8.806	0.000	0.000	0.000	0.000	0.167	0.000
	END	END	NEW SURGE	NEW SURGE		<del>.</del>	<del>-</del>		BOTTOM	AVERAGE
0.7	STATION	ELEVATION	10-YEAR	100-YEAR	0.000	0.000	0.000	0.000	SLOPE	A-ZONES
OF	368.000 END	-3.259 END	0.000 NEW SURGE	8.806 NEW SURGE	0.000	0.000	0.000	0.000	0.154 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	370.000	-3.043	0.000	8.806	0.000	0.000	0.000	0.000	0.111	0.000
	END STATION	END ELEVATION	NEW SURGE 10-YEAR	NEW SURGE 100-YEAR					BOTTOM SLOPE	AVERAGE A-ZONES
OF	372.000	-2.814	0.000	8.806	0.000	0.000	0.000	0.000	0.106	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
0-	STATION	ELEVATION	10-YEAR	100-YEAR	0.000	0 000	0 000	0 000	SLOPE	A-ZONES
OF	374.000 END	-2.617 END	0.000 NEW SURGE	8.806 NEW SURGE	0.000	0.000	0.000	0.000	0.077 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	376.000	-2.507	0.000	8.806	0.000	0.000	0.000	0.000	0.053	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
OF	378.000	ELEVATION -2.404	10-YEAR 0.000	100-YEAR 8.806	0.000	0.000	0.000	0.000	SLOPE 0.143	A-ZONES 0.000
01	END	END	NEW SURGE	NEW SURGE	3.000	0.000	0.000	5.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR		0 00-	0.00-	0.00-	SLOPE	A-ZONES
OF	380.000 END	-1.935 END	0.000 NEW SURGE	8.806 NEW SURGE	0.000	0.000	0.000	0.000	0.203 BOTTOM	0.000 AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	382.000	-1.592	0.000	8.806	0.000	0.000	0.000	0.000	0.128	0.000
	END	END	NEW SURGE 10-YEAR	NEW SURGE					BOTTOM	AVERAGE
OF	STATION 384.000	ELEVATION -1.424	0.000	100-YEAR 8.806	0.000	0.000	0.000	0.000	SLOPE 0.089	A-ZONES 0.000
	1.000	2.121	3.000	0.000	3.550	000	2.000	000	5.505	0.000

	FILTE	FILE	MEN CHECK	MENT CITE OF					DOMMON	311003.00
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	386.000	-1.235	0.000	8.806	0.000	0.000	0.000	0.000	0.104	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	388.000	-1.008	0.000	8.806	0.000	0.000	0.000	0.000	0.117	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF		-0.766	0.000		0 000	0 000	0.000	0 000		0.000
OF	390.000			8.806	0.000	0.000	0.000	0.000	0.124	
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	392.000	-0.512	0.000	8.806	0.000	0.000	0.000	0.000	0.130	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
OF	394.000	-0.245	0.000	8.806	0.000	0.000	0.000	0.000	0.129	0.000
OF	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
IF	396.000	0.005	0.000	8.806	0.000	0.000	0.000	0.000	0.112	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
IF	398.000	0.202	0.000	8.806	0.000	0.000	0.000	0.000	0.104	0.000
	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
					0.000	0 000	0 000	0 000		
IF	400.000	0.420	0.000	8.806	0.000	0.000	0.000	0.000	0.110	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
IF	402.000	0.641	0.000	8.806	0.000	0.000	0.000	0.000	0.106	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
IF	404.000	0.845	0.000	8.806	0.000	0.000	0.000	0.000	0.120	0.000
TL					0.000	0.000	0.000	0.000	BOTTOM	
	END	END	NEW SURGE	NEW SURGE						AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
IF	406.000	1.123	0.000	8.806	0.000	0.000	0.000	0.000	0.118	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
IF	408.000	1.317	0.000	8.806	0.000	0.000	0.000	0.000	0.102	0.000
IF	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
IF	410.000	1.532	0.000	8.806	0.000	0.000	0.000	0.000	0.144	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
IF	412.000	1.891	0.000	8.806	0.000	0.000	0.000	0.000	0.141	0.000
	END	END	NEW SURGE	NEW SURGE	0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
IF	413.400	2.011	0.000	8.806	0.000	0.000	0.000	0.000	0.097	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
IF	416.700	2.347	0.000	8.819	0.000	0.000	0.000	0.000	0.151	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
					0 000	0 000	0 000	0 000		
IF	419.900	2.995	0.000	8.826	0.000	0.000	0.000	0.000	0.144	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
IF	423.200	3.284	0.000	8.851	0.000	0.000	0.000	0.000	0.061	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
IF	426.500	3.394	0.000	8.878	0.000	0.000	0.000	0.000	0.061	0.000
1P					0.000	0.000	0.000	0.000	0.001	
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
IF	429.800	3.689	0.000	8.903	0.000	0.000	0.000	0.000	0.130	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
IF	433.100	4.250	0.000	8.923	0.000	0.000	0.000	0.000	0.166	0.000
	END		NEW SURGE		0.000	0.000	0.000	0.000	BOTTOM	AVERAGE
		DI DIZADION	10-YEAR	100 VEND					SLOPE	A-ZONES
		ELEVATION	IU-YEAR	IUU-YEAR	0.000	0 000	0 000	0 000	SLOPE	A-ZUNES
IF		4.783	0.000	8.951	0.000	0.000	0.000	0.000	0.128 BOTTOM SLOPE	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
							0.000		SLOPE	A-ZONES
IF		5.082	0.000	8.990	0.000	0.000	0.000	0.000	0.128	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
		ELEVATION		100-YEAR					SIODE	A-ZONEC
IF	442.900			9.021	0.000	0 000	0.000	0.000	0 104	77 7014179
TL				NEW CIPCE	0.000	0.000	0.000	0.000	U.184	0.00.0
	END		NEW SURGE	NEW SURGE					BOT.LOM	AVERAGE
			10-YEAR	100-YEAR	0.000				SLOPE	A-ZONES
IF	446.200		0.000	9.048	0.000	0.000	0.000	0.000	0.248	0.000
	END	END	NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
		ELEVATION	IU-YEAR	IUU-YEAR					SLOPE	A = ZONES
IF	449.500		0 000	9.266	0 000	0.000	0.000	0 000	0 288	0 000
TT		1.23.	MEM CITOCH	NEW SURGE	0.000			0.000	0.288 BOTTOM	ס.טט.ט
	END								POTIOM	AVERAGE
				100-YEAR			0.000		SLOPE	A-ZONES
IF		8.192		9.511	0.000	0.000	0.000	0.000	0.176	0.000
	END		NEW SURGE						BOTTOM	AVERAGE
		ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
IF	456.000		0.000	9.660	0.000	0.000	0.000	0.000	0.057	0.000
-	END	END	NEW SURGE	NEW SURGE					SLOPE 0.057 BOTTOM	AVERAGE
			10-425	100-0000					2011014	V = 4UMEG
	SIATION	PTFAULTON	10-YEAR	TUU-IEAR	0.000	0 000	0 000	0 000	PLOPE	A-ZUNES
IF	459.300	8.561	0.000	9.677	0.000	0.000	0.000	0.000	0.109	0.000
	END		NEW SURGE	NEW SURGE					BOTTOM	AVERAGE
		ELEVATION	IU-YEAR	TUU-YEAR					SLOPE	A-ZONES
IF	462.000		0.000	9.677	0.000	0.000	0.000	0.000	0.179	0.000
	EMD	FND	MEM CIIDCE	NEW CITECE					BOTTOM	AVERAGE
	STATION	ET.EMATTON	10-7575	100-7575					ST.ODE	A-70NEC
TE	DIMITON	U 4UJ	70-1FWK	TOO-IEAK	0 000	0 000	0.000	0 000	0 156	U 000
IF	404.000	9.403	U.UUU	9.6//	0.000	0.000	0.000	0.000	U.156	0.000
	END	END	NEW SURGE	NEW SURGE					RO.I.I.OW	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
IF	466.000	9.668	0.000	9.677	0.000	0.000	0.000	0.000	0.119	0.000
	END	END	NEW SURGE	NEW SURGE	0.000				BOTTOM	AVERAGE
	STATION	ELEVATION	10-YEAR	100-YEAR					SLOPE	A-ZONES
IF	466.300	9 677	0 000	9 677	0.000 -END OF TRANSE	0.000	0.000	0.000	0.031	0 000
		J.077			-END OF TRANSE	CT				
NOTE:					OL TENINGE					
							10			

PART2: CONTROLLING WAVE PERIORS   SPECTRAL					
RE	1.00	PART2:	PEAK WAVE PERIO	D, AND WAVE CRES	ST ELEVATIONS
OF 2.00 8.98 10.45 15.09 OF 6.00 9.00 10.45 15.11 OF 6.00 9.00 10.45 15.11 OF 8.00 9.02 10.45 15.11 OF 8.00 9.02 10.45 15.11 OF 10.00 9.04 10.45 15.12 OF 10.00 9.09 10.45 15.12 OF 110.00 9.09 10.45 15.13 OF 110.00 9.09 10.45 15.15 OF 16.00 9.09 10.45 15.15 OF 16.00 9.09 10.45 15.17 OF 16.00 9.09 10.45 15.17 OF 20.00 9.12 10.45 15.18 OF 20.00 9.12 10.45 15.18 OF 20.00 9.12 10.45 15.18 OF 20.00 9.12 10.45 15.20 OF 24.00 9.16 10.45 15.20 OF 28.00 9.18 10.45 15.22 OF 28.00 9.28 10.45 15.27 OF 38.00 9.26 10.45 15.27 OF 38.00 9.26 10.45 15.30 OF 38.00 9.30 10.45 15.30 OF 38.00 9.30 10.45 15.30 OF 38.00 9.30 10.45 15.30 OF 40.00 9.34 10.45 15.30 OF 40.00 9.34 10.45 15.30 OF 40.00 9.32 10.45 15.30 OF 40.00 9.34 10.45 15.30 OF 40.00 9.30 10.45 15.30 OF 60.00 9.34 10.45 15.30 OF 60.00 9.30 10.45 15.30 OF 60.00 9.43 10.45 15.50 OF 55.00 9.49 10.45 15.50 OF 60.00 9.47 10.45 15.50 OF 60.00 9.49 10.45 15.50 OF 60.00 9.50 10.45 15.50 OF 60.00 9.50 10.45 15.50 OF 60.00 9.50 10.45 15.50 OF 60.00 9.66 10.45 15.50 OF 60.00 9.70 10.45 15.50 OF 60.00 9.70 10.45 15.50 OF 60.00 9.70 10.45 15.50 OF 70.00 9.66 10.45 15.50 OF 70.00 9.68 10.45 15.50 OF 70.00 9.89 10.45 15.50 OF 70.00 9.80 10.45 1			WAVE HEIGHT	WAVE PERIOD	ELEVATION
OF 6.00 9.00 10.45 15.12 OF 10.00 9.04 10.45 15.12 OF 11.00 9.05 10.45 15.12 OF 11.00 9.05 10.45 15.13 OF 12.00 9.05 10.45 15.13 OF 12.00 9.05 10.45 15.14 OF 12.00 9.05 10.45 15.14 OF 12.00 9.05 10.45 15.14 OF 12.00 9.05 10.45 15.17 OF 18.00 9.11 10.45 15.18 OF 22.00 9.11 10.45 15.19 OF 24.00 9.16 10.45 15.20 OF 24.00 9.16 10.45 15.20 OF 26.00 9.18 10.45 15.20 OF 26.00 9.18 10.45 15.23 OF 30.00 9.22 10.45 15.26 OF 33.00 9.20 10.45 15.26 OF 33.00 9.22 10.45 15.26 OF 33.00 9.23 10.45 15.30 OF 33.00 9.23 10.45 15.30 OF 34.00 9.30 10.45 15.30 OF 44.00 9.34 10.45 15.33 OF 44.00 9.36 10.45 15.33 OF 48.00 9.30 10.45 15.33 OF 48.00 9.38 10.45 15.33 OF 48.00 9.36 10.45 15.33 OF 48.00 9.36 10.45 15.34 OF 55.00 9.43 10.45 15.36 OF 66.00 9.38 10.45 15.35 OF 67.00 9.43 10.45 15.30 OF 50.00 9.43 10.45 15.30 OF 50.00 9.43 10.45 15.30 OF 50.00 9.45 10.45 15.50 OF 68.00 9.57 10.45 15.50 OF 68.00 9.66 10.45 15.50 OF 68.00 9.66 10.45 15.50 OF 68.00 9.77 10.45 15.50 OF 68.00 9.78 10.45 15.50 OF 68.00 9.78 10.45 15.50 OF 772.00 9.66 10.45 15.50 OF 78.00 9.78 10.45 15.50 OF 68.00 9.78 10.45 15.50 OF 78.00 9.98 10.45 15.50 OF 79.00 9.98 10.45 15.50 OF 68.00 9.78 10.45 15.50 OF 68.00 9.78 10.45 15.50 OF 79.00 9.80 10.45 15.50 OF 68.00 9.79 10.45 15.50 OF 79.00 9.80 10.45 15.50 OF 79.00 9.98 10.45 15.50 OF 79.00 9.98 10.45 15.50 OF 79.00 9.99 10.45 15.50 OF 99.00 9.99 10.45 15.50 OF 108.00 9	OF	2.00	8.98	10.45	15.09
OF 10.00 9.04 10.45 15.13 OF 12.00 9.05 10.45 15.14 OF 14.00 9.07 10.45 15.15 OF 16.00 9.07 10.45 15.17 OF 18.00 9.11 10.45 15.17 OF 18.00 9.11 10.45 15.17 OF 18.00 9.11 10.45 15.17 OF 22.00 3.12 10.45 15.20 OF 22.00 3.12 10.45 15.20 OF 24.00 3.16 10.45 15.22 OF 26.00 9.18 10.45 15.23 OF 28.00 9.20 10.45 15.24 OF 30.00 9.22 10.45 15.26 OF 31.00 9.22 10.45 15.26 OF 32.00 9.24 10.45 15.26 OF 32.00 9.24 10.45 15.27 OF 34.00 9.28 10.45 15.27 OF 36.00 9.28 10.45 15.30 OF 40.00 9.38 10.45 15.30 OF 50.00 9.43 10.45 15.37 OF 50.00 9.45 10.45 15.30 OF 50.00 9.45 10.45 15.30 OF 50.00 9.45 10.45 15.30 OF 50.00 9.45 10.45 15.50 OF 60.00 9.56 10.45 15.50 OF 60.00 9.57 10.45 15.50 OF 60.00 9.66 10.45 15.50 OF 60.00 9.77 10.45 15.50 OF 60.00 9.78 10.45 15.50 OF 70.00 9.66 10.45 15.50 OF 60.00 9.78 10.45 15.50 OF 60.00 9.79 10.45 15.50 OF 70.00 9.66 10.45 15.50 OF 70.00 9.66 10.45 15.50 OF 70.00 9.66 10.45 15.50 OF 70.00 9.67 10.45 15.50 OF 70.00 9.68 10.45 15.50 OF 70.00 9.68 10.45 15.50 OF 70.00 9.68 10.45 15.50 OF 70.00 9.67 10.45 15.50 OF 70.00 9.68 10.45 15.50 OF 70.00 9.60 10.45 15.50 OF 70.00 9.80 10.45 15.50 OF 70.00 9.80 10.45 15.50 OF 100.00 9.90	OF	6.00	9.00	10.45	15.11
OF 14.00 9.07 10.45 15.15 OF 18.00 9.09 10.45 15.17 OF 18.00 9.11 10.45 15.17 OF 20.00 9.12 10.45 15.19 OF 22.00 9.14 10.45 15.20 OF 22.00 9.14 10.45 15.20 OF 24.00 9.16 10.45 15.20 OF 26.00 9.16 10.45 15.22 OF 26.00 9.16 10.45 15.22 OF 26.00 9.16 10.45 15.22 OF 30.00 9.22 11.45 15.23 OF 30.00 9.22 11.45 15.23 OF 30.00 9.22 11.45 15.23 OF 30.00 9.22 11.45 15.26 OF 31.00 9.26 10.45 15.27 OF 34.00 9.26 10.45 15.28 OF 38.00 9.28 10.45 15.30 OF 40.00 9.38 10.45 15.30 OF 40.00 9.38 10.45 15.31 OF 42.00 9.34 10.45 15.31 OF 44.00 9.36 10.45 15.33 OF 42.00 9.38 10.45 15.37 OF 44.00 9.36 10.45 15.36 OF 46.00 9.38 10.45 15.37 OF 55.00 9.49 10.45 15.39 OF 56.00 9.49 10.45 15.39 OF 56.00 9.45 10.45 15.40 OF 56.00 9.57 10.45 15.40 OF 56.00 9.57 10.45 15.40 OF 66.00 9.57 10.45 15.45 OF 66.00 9.57 10.45 15.50 OF 67 70.00 9.56 10.45 15.50 OF 68.00 9.59 10.45 15.50 OF 68.00 9.59 10.45 15.50 OF 69.00 9.57 10.45 15.50 OF 69.00 9.57 10.45 15.50 OF 60.00 9.57 10.45 15.50 OF 60.00 9.57 10.45 15.50 OF 60.00 9.66 10.45 15.50 OF 70.00 9.66 10.45 15.50 OF 70.00 9.66 10.45 15.50 OF 70.00 9.66 10.45 15.50 OF 71.00 9.66 10.45 15.50 OF 72.00 9.68 10.45 15.50 OF 74.00 9.76 10.45 15.50 OF 78.00 9.77 10.45 15.50 OF 78.00 9.78 10.45 15.50 OF 79.00 9.66 10.45 15.50 OF 70.00 9.66 10.45 15.50 OF 70.00 9.66 10.45 15.50 OF 71.00 9.70 9.80 10.45 15.50 OF 72.00 9.81 10.45 15.50 OF 72.00 9.81 10.45 15.50 OF 74.00 9.79 10.45 15.50 OF 76.00 9.79 10.45 15.50 OF 77.00 9.66 10.45 15.50 OF 78.00 9.79 10.45 15.50 OF 78.00 9.79 10.45 15.50 OF 79.00 9.67 10.45 15.50 OF 71.00 9.66 10.45 15.50 OF 71.00 9.60 10.45 15.50 OF 71.00 9.60 9.81 10.45 15.50 OF 71.00 9.60 10.45 15.50 OF 91.00 9.90 9.80 10.45 15.50 OF 188.00 9.90 10.45 15.80 OF 188.00 9.90 10.45 15.80 OF 188.00 9.90 10.45 15.80 OF 188.0		10.00	9.04	10.45	15.13
OF 16.00 9.09 10.45 15.17 OF 20.00 9.11 10.45 15.18 OF 20.00 9.12 10.45 15.18 OF 20.00 9.12 10.45 15.19 OF 22.00 9.14 10.45 15.20 OF 24.00 9.16 10.45 15.20 OF 24.00 9.16 10.45 15.20 OF 26.00 9.18 10.45 15.22 OF 28.00 9.20 10.45 15.33 OF 30.00 9.20 10.45 15.34 OF 31.00 9.24 10.45 15.34 OF 33.00 9.20 10.45 15.34 OF 33.00 9.20 10.45 15.35 OF 34.00 9.28 10.45 15.30 OF 34.00 9.32 10.45 15.30 OF 34.00 9.32 10.45 15.30 OF 34.00 9.32 10.45 15.30 OF 38.00 9.33 10.45 15.30 OF 44.00 9.34 10.45 15.30 OF 44.00 9.33 10.45 15.30 OF 44.00 9.34 10.45 15.30 OF 44.00 9.38 10.45 15.30 OF 48.00 9.30 10.45 15.30 OF 55.00 9.43 10.45 15.30 OF 55.00 9.43 10.45 15.30 OF 55.00 9.45 10.45 15.40 OF 56.00 9.47 10.45 15.40 OF 56.00 9.47 10.45 15.40 OF 56.00 9.47 10.45 15.40 OF 68.00 9.57 10.45 15.45 OF 68.00 9.66 10.45 15.50 OF 77.00 9.68 10.45 15.55 OF 78.00 9.73 10.45 15.55 OF 78.00 9.73 10.45 15.55 OF 78.00 9.73 10.45 15.55 OF 78.00 9.76 10.45 15.55 OF 78.00 9.77 10.45 15.55 OF 78.00 9.78 10.45 15.55 OF 78.00 9.78 10.45 15.55 OF 78.00 9.79 10.45 15.55 OF 78.00 9.79 10.45 15.55 OF 79.00 9.66 10.45 15.55 OF 78.00 9.79 10.45 15.55 OF 80.00 9.79 10.45 15.55 OF 80.00 9.79 10.45 15.56 OF 99.00 9.70 10.45 15.55 OF 99.00 9.81 10.45 15.55 OF 100.00 9.85 10.45 15.55 OF 100.00 9.86 10.45 15.56 OF 99.00 9.98 10.45 15.57 OF 100.00 9.87 10.45 15.58 OF 100.00 9.99 10.45 15.59 OF 100.00 9.98 10.45 15.59 OF 100.00 9.98 10.45 15.58 OF 100.00 9.99 10.45 15.80 OF 100.00 9.99 10.45 15.80 OF 100.00 10.00 10.45 15.80 OF 100.00 10.00 10.45 15.80 OF 100.00 10.00 10.45 15.80 OF 1					
OF 20.00 9.12 10.45 15.19 OF 22.00 9.16 10.45 15.20 OF 24.00 9.16 10.45 15.20 OF 26.00 9.18 10.45 15.22 OF 26.00 9.20 10.45 15.23 OF 30.00 9.20 10.45 15.24 OF 30.00 9.22 10.45 15.26 OF 32.00 9.24 10.45 15.26 OF 32.00 9.24 10.45 15.26 OF 33.00 9.23 10.45 15.26 OF 33.00 9.23 10.45 15.27 OF 34.00 9.28 10.45 15.27 OF 35.00 9.28 10.45 15.30 OF 40.00 9.32 10.45 15.31 OF 44.00 9.34 10.45 15.33 OF 44.00 9.38 10.45 15.39 OF 48.00 9.38 10.45 15.39 OF 48.00 9.38 10.45 15.39 OF 48.00 9.38 10.45 15.39 OF 50.00 9.43 10.45 15.39 OF 50.00 9.43 10.45 15.30 OF 50.00 9.43 10.45 15.30 OF 50.00 9.45 10.45 15.40 OF 50.00 9.47 10.45 15.40 OF 50.00 9.47 10.45 15.40 OF 50.00 9.47 10.45 15.40 OF 50.00 9.59 10.45 15.55 OF 60.00 9.70 10.45 15.55 OF 60.00 9.70 10.45 15.55 OF 77.00 9.66 10.45 15.55 OF 78.00 9.70 10.45 15.55 OF 88.00 9.70 10.45 15.56 OF 99.00 9.70 10.45 15.55 OF 99.00 9.70 10.45 15.58 OF 100.00 9.88 10.45 15.58 OF 100.00 9.88 10.45 15.58 OF 100.00 9.99 10.45 15.88 OF 100.00 9.99 10.45 15.88 OF 100.00 9.99 10.45 15.88 OF 100.00 9.9					
OF 24.00 9.16 10.45 15.23 OF 28.00 9.18 10.45 15.23 OF 28.00 9.20 10.45 15.23 OF 30.00 9.20 10.45 15.24 OF 30.00 9.22 10.45 15.26 OF 32.00 9.24 10.45 15.26 OF 32.00 9.24 10.45 15.26 OF 32.00 9.24 10.45 15.27 OF 34.00 9.26 10.45 15.27 OF 34.00 9.28 10.45 15.30 OF 36.00 9.28 10.45 15.30 OF 36.00 9.28 10.45 15.31 OF 40.00 9.32 10.45 15.31 OF 40.00 9.33 10.45 15.31 OF 42.00 9.34 10.45 15.33 OF 42.00 9.34 10.45 15.33 OF 42.00 9.34 10.45 15.34 OF 44.00 9.36 10.45 15.34 OF 44.00 9.36 10.45 15.35 OF 44.00 9.36 10.45 15.35 OF 46.00 9.30 10.45 15.35 OF 46.00 9.30 10.45 15.37 OF 46.00 9.30 10.45 15.37 OF 46.00 9.30 10.45 15.36 OF 46.00 9.30 10.45 15.36 OF 46.00 9.30 10.45 15.40 OF 56.00 9.49 10.45 15.40 OF 56.00 9.49 10.45 15.40 OF 56.00 9.52 00 9.52 00 9.54 10.45 15.45 OF 66.00 9.59 10.45 15.47 OF 66.00 9.57 10.45 15.40 OF 66.00 9.57 10.45 15.40 OF 66.00 9.57 10.45 15.50 OF 66.00 9.57 10.45 15.50 OF 66.00 9.59 10.45 15.50 OF 66.00 9.61 10.45 15.50 OF 66.00 9.61 10.45 15.55 OF 67.00 9.68 10.45 15.55 OF 67.00 9.72 10.45 15.55 OF 67.00 9.73 10.45 15.56 OF 72.00 9.68 10.45 15.55 OF 67.00 9.73 10.45 15.56 OF 73.00 9.73 10.45 15.57 OF	OF	20.00	9.12	10.45	15.19
OF 28.00 9.20 10.45 15.24 OF 30.00 9.22 10.45 15.26 OF 32.00 9.24 10.45 15.27 OF 34.00 9.26 10.45 15.27 OF 36.00 9.28 10.45 15.27 OF 36.00 9.28 10.45 15.30 OF 36.00 9.30 10.45 15.30 OF 38.00 9.30 10.45 15.31 OF 42.00 9.34 10.45 15.31 OF 42.00 9.34 10.45 15.33 OF 44.00 9.36 10.45 15.33 OF 44.00 9.38 10.45 15.34 OF 46.00 9.38 10.45 15.34 OF 46.00 9.39 10.45 15.34 OF 46.00 9.39 10.45 15.34 OF 46.00 9.40 10.45 15.34 OF 46.00 9.40 10.45 15.35 OF 46.00 9.40 10.45 15.37 OF 56.00 9.47 10.45 15.42 OF 56.00 9.49 10.45 15.43 OF 56.00 9.52 10.45 15.47 OF 66.00 9.54 10.45 15.40 OF 66.00 9.55 10.45 15.50 OF 66.00 9.57 10.45 15.50 OF 66.00 9.61 10.45 15.55 OF 66.00 9.66 10.45 15.55 OF 66.00 9.66 10.45 15.55 OF 70.00 9.66 10.45 15.55 OF 770.00 9.66 10.45 15.55 OF 78.00 9.72 10.45 15.55 OF 78.00 9.72 10.45 15.55 OF 78.00 9.73 10.45 15.56 OF 78.00 9.73 10.45 15.56 OF 78.00 9.73 10.45 15.56 OF 78.00 9.74 10.45 15.56 OF 79.00 9.68 10.45 15.55 OF 79.00 9.68 10.45 15.55 OF 80.00 9.74 10.45 15.56 OF 79.00 9.68 10.45 15.56 OF 79.00 9.70 10.45 15.56 OF 79.00 9.70 10.45 15.56 OF 79.00 9.70 10.45 15.56 OF 80.00 9.71 10.45 15.62 OF 80.00 9.73 10.45 15.62 OF 80.00 9.73 10.45 15.62 OF 80.00 9.78 10.45 15.65 OF 80.00 9.79 10.45 15.65 OF 90.00 9.88 10.45 15.57 OF 96.00 9.89 10.45 15.70 OF 100.00 9.86 10.45 15.58 OF 90.00 9.99 10.45 15.70 OF 112.00 9.99 10.45 15.70 OF 114.00 9.99 10.45 15.81 OF 114.00 10.00 10.01 10.45 15.80 OF 114.00 10.00 10.04 10.45 15.81 OF 114.00 10.00 10.04 10.45 15.80 OF 114.00 10.00 10.04 10.45 15.80 OF 114.00 10.00 10.04 10.45	OF	24.00	9.16	10.45	15.22
OF 32.00 9.24 10.45 15.27 OF 36.00 9.26 10.45 15.28 OF 36.00 9.28 10.45 15.30 OF 36.00 9.30 10.45 15.30 OF 36.00 9.30 10.45 15.30 OF 40.00 9.32 10.45 15.31 OF 42.00 9.34 10.45 15.33 OF 42.00 9.34 10.45 15.33 OF 42.00 9.36 10.45 15.33 OF 44.00 9.36 10.45 15.36 OF 46.00 9.38 10.45 15.36 OF 46.00 9.38 10.45 15.37 OF 48.00 9.40 10.45 15.39 OF 50.00 9.43 10.45 15.39 OF 50.00 9.43 10.45 15.42 OF 50.00 9.47 10.45 15.42 OF 50.00 9.47 10.45 15.45 OF 50.00 9.47 10.45 15.45 OF 50.00 9.47 10.45 15.45 OF 50.00 9.57 10.45 15.45 OF 60.00 9.57 10.45 15.45 OF 60.00 9.57 10.45 15.55 OF 60.00 9.57 10.45 15.55 OF 66.00 9.59 10.45 15.55 OF 66.00 9.64 10.45 15.55 OF 66.00 9.66 10.45 15.55 OF 66.00 9.66 10.45 15.55 OF 67 70.00 9.66 10.45 15.55 OF 77.00 9.66 10.45 15.55 OF 77.00 9.66 10.45 15.56 OF 77.00 9.66 10.45 15.56 OF 77.00 9.77 10.45 15.50 OF 76.00 9.78 10.45 15.56 OF 98.00 9.77 10.45 15.56 OF 98.00 9.78 10.45 15.66 OF 99.00 9.78 10.45 15.66 OF 99.00 9.78 10.45 15.65 OF 99.00 9.78 10.45 15.65 OF 99.00 9.81 10.45 15.65 OF 99.00 9.82 10.45 15.65 OF 99.00 9.83 10.45 15.66 OF 99.00 9.88 10.45 15.66 OF 99.00 9.89 10.45 15.66 OF 99.00 9.89 10.45 15.66 OF 99.00 9.89 10.45 15.66 OF 99.00 9.98 10.45 15.77 OF 110.00 9.99 10.45 15.77 OF 110.00 9.99 10.45 15.79 OF 110.00 9.99 10.45 15.80 OF 122.00 10.00 10.45 15.81 OF 138.00 10.01 10.45 15.83 OF 138.00 10.01 10.45 15.83 OF 138.00 10.01 10.04 10.45 15.88 OF 138.00 10.01 10.0	OF	28.00	9.20	10.45	15.24
OF 36.00 9.28 10.45 15.30 OF 38.00 9.30 10.45 15.31 OF 40.00 9.32 10.45 15.33 OF 42.00 9.34 10.45 15.33 OF 42.00 9.34 10.45 15.33 OF 42.00 9.36 10.45 15.33 OF 44.00 9.36 10.45 15.36 OF 46.00 9.38 10.45 15.36 OF 46.00 9.38 10.45 15.37 OF 48.00 9.40 10.45 15.39 OF 50.00 9.43 10.45 15.39 OF 52.00 9.45 10.45 15.42 OF 54.00 9.47 10.45 15.42 OF 56.00 9.49 10.45 15.45 OF 56.00 9.49 10.45 15.45 OF 66.00 9.57 10.45 15.45 OF 66.00 9.57 10.45 15.55 OF 66.00 9.57 10.45 15.50 OF 66.00 9.57 10.45 15.50 OF 66.00 9.61 10.45 15.55 OF 66.00 9.61 10.45 15.55 OF 68.00 9.66 10.45 15.55 OF 68.00 9.66 10.45 15.55 OF 70.00 9.66 10.45 15.55 OF 77.00 9.66 10.45 15.56 OF 77.00 9.70 10.45 15.56 OF 78.00 9.77 10.45 15.56 OF 78.00 9.77 10.45 15.56 OF 79.00 9.78 10.45 15.55 OF 98.00 9.77 10.45 15.56 OF 99.00 9.78 10.45 15.66 OF 99.00 9.78 10.45 15.66 OF 99.00 9.78 10.45 15.65 OF 99.00 9.88 10.45 15.66 OF 99.00 9.88 10.45 15.67 OF 110.00 9.89 10.45 15.67 OF 110.00 9.89 10.45 15.68 OF 99.00 9.88 10.45 15.69 OF 98.00 9.88 10.45 15.69 OF 99.00 9.88 10.45 15.69 OF 110.00 9.98 10.45 15.69 OF 110.00 9.98 10.45 15.69 OF 110.00 9.99 10.45 15.70 OF 110.00 9.99 10.45 15.70 OF 110.00 9.99 10.45 15.70 OF 110.00 9.99 10.45 15.80 OF 122.00 10.00 10.45 15.80 OF 122.00 10.00 10.45 15.81 OF 122.00 10.00 10.45 15.81 OF 124.00 10.01 10.45 15.81 OF 125.00 10.00 10.45 15.81 OF 126.00 10.00 10.04 10.45 15.82 OF 186.00 10.00 10.04 10.45 15.83 OF 186.00 10.00 10.0			9.24	10.45	15.27
OF 40.00 9.32 10.45 15.33 OF P 42.00 9.36 10.45 15.34 OF 44.00 9.36 10.45 15.36 OF 46.00 9.38 10.45 15.36 OF 46.00 9.38 10.45 15.37 OF 48.00 9.40 10.45 15.39 OF 50.00 9.43 10.45 15.39 OF 50.00 9.43 10.45 15.39 OF 52.00 9.45 10.45 15.42 OF 54.00 9.47 10.45 15.42 OF 56.00 9.47 10.45 15.45 OF 56.00 9.49 10.45 15.45 OF 56.00 9.49 10.45 15.45 OF 60.00 9.59 10.45 15.45 OF 60.00 9.59 10.45 15.45 OF 60.00 9.59 10.45 15.45 OF 66.00 9.59 10.45 15.50 OF 66.00 9.59 10.45 15.50 OF 66.00 9.64 10.45 15.55 OF 66.00 9.64 10.45 15.55 OF 66.00 9.66 10.45 15.55 OF 70.00 9.66 10.45 15.55 OF 70.00 9.66 10.45 15.55 OF 70.00 9.68 10.45 15.55 OF 70.00 9.68 10.45 15.55 OF 70.00 9.68 10.45 15.56 OF 74.00 9.70 10.45 15.56 OF 74.00 9.70 10.45 15.56 OF 76.00 9.73 10.45 15.60 OF 78.00 9.73 10.45 15.60 OF 79.00 9.68 10.45 15.60 OF 79.00 9.68 10.45 15.60 OF 79.00 9.75 10.45 15.60 OF 79.00 9.80 10.45 15.70 OF 104.00 9.80 10.45 15.60 OF 79.00 9.80 10.45 15.60 OF 79.00 9.80 10.45 15.60 OF 79.00 9.80 10.45 15.70 OF 104.00 9.90 10.45 15.70 OF 104.00 9.90 10.45 15.70 OF 104.00 9.90 10.45 15.80 OF 79.00 10.00 9.80 10.45 15.80 OF 79.00 10.00 10.45 15.80			9.28		
OF         42.00         9.34         10.45         15.36           OF         46.00         9.38         10.45         15.36           OF         46.00         9.38         10.45         15.37           OF         50.00         9.43         10.45         15.39           OF         50.00         9.43         10.45         15.40           OF         54.00         9.47         10.45         15.43           OF         56.00         9.47         10.45         15.43           OF         56.00         9.52         10.45         15.47           OF         60.00         9.54         10.45         15.47           OF         60.00         9.57         10.45         15.50           OF         64.00         9.59         10.45         15.50           OF         66.00         9.61         10.45         15.53           OF         70.00         9.68         10.45         15.55           OF         70.00         9.68         10.45         15.56           OF         72.00         9.68         10.45         15.59           OF         74.00         9.70         10.45 </td <td></td> <td></td> <td></td> <td></td> <td></td>					
OF 46.00 9.38 10.45 15.37 OF 50.00 9.43 10.45 15.39 OF 50.00 9.43 10.45 15.40 OF 50.00 9.45 10.45 15.40 OF 50.00 9.45 10.45 15.42 OF 54.00 9.47 10.45 15.42 OF 54.00 9.47 10.45 15.43 OF 56.00 9.49 10.45 15.43 OF 56.00 9.52 10.45 15.45 OF 60.00 9.52 10.45 15.48 OF 62.00 9.57 10.45 15.48 OF 62.00 9.57 10.45 15.50 OF 62.00 9.57 10.45 15.50 OF 66.00 9.61 10.45 15.50 OF 66.00 9.61 10.45 15.55 OF 66.00 9.61 10.45 15.55 OF 66.00 9.66 10.45 15.55 OF 70.00 9.66 10.45 15.55 OF 70.00 9.68 10.45 15.55 OF 70.00 9.68 10.45 15.55 OF 74.00 9.70 10.45 15.59 OF 74.00 9.70 10.45 15.59 OF 74.00 9.70 10.45 15.60 OF 78.00 9.73 10.45 15.62 OF 82.00 9.73 10.45 15.62 OF 82.00 9.75 10.45 15.62 OF 82.00 9.75 10.45 15.63 OF 82.00 9.76 10.45 15.65 OF 82.00 9.78 10.45 15.66 OF 99.00 9.80 10.45 15.66 OF 99.00 9.80 10.45 15.66 OF 99.00 9.80 10.45 15.66 OF 99.00 9.81 10.45 15.66 OF 99.00 9.81 10.45 15.66 OF 99.00 9.81 10.45 15.66 OF 99.00 9.83 10.45 15.66 OF 99.00 9.83 10.45 15.66 OF 99.00 9.81 10.45 15.66 OF 99.00 9.83 10.45 15.66 OF 99.00 9.88 10.45 15.67 OF 99.00 9.88 10.45 15.67 OF 99.00 9.88 10.45 15.68 OF 99.00 9.88 10.45 15.68 OF 99.00 9.88 10.45 15.68 OF 100.00 9.89 10.45 15.68 OF 100.00 9.89 10.45 15.68 OF 100.00 9.89 10.45 15.69 OF 100.00 9.89 10.45 15.72 OF 100.00 9.99 10.45 15.73 OF 110.00 9.99 10.45 15.77 OF 110.00 9.99 10.45 15.80 OF 110.00 9.99 10.45 15.80 OF 110.00 9.99 10.45 15.80 OF 110.00 10.00 10.00 10.00 10.45 15.80 OF 110.00 10.00 10.00 10.00 10.45 15.80 OF 110.00 10.00 10.00 10.00 10.45 15.80 OF	OF	42.00	9.34	10.45	15.34
OF 50.00 9.43 10.45 15.40 OF 52.00 9.45 10.45 15.42 OF 54.00 9.47 10.45 15.42 OF 56.00 9.49 10.45 15.43 OF 56.00 9.59 10.45 15.43 OF 56.00 9.52 10.45 15.45 OF 60.00 9.57 10.45 15.48 OF 62.00 9.57 10.45 15.50 OF 62.00 9.57 10.45 15.50 OF 64.00 9.59 10.45 15.50 OF 66.00 9.61 10.45 15.52 OF 66.00 9.61 10.45 15.53 OF 66.00 9.64 10.45 15.53 OF 66.00 9.64 10.45 15.55 OF 70.00 9.66 10.45 15.55 OF 70.00 9.66 10.45 15.55 OF 77.00 9.68 10.45 15.55 OF 77.00 9.72 10.45 15.65 OF 77.00 9.72 10.45 15.65 OF 78.00 9.73 10.45 15.65 OF 80.00 9.74 10.45 15.65 OF 80.00 9.74 10.45 15.65 OF 80.00 9.75 10.45 15.65 OF 80.00 9.75 10.45 15.65 OF 80.00 9.75 10.45 15.65 OF 80.00 9.76 10.45 15.65 OF 80.00 9.78 10.45 15.65 OF 90.00 9.81 10.45 15.66 OF 92.00 9.81 10.45 15.66 OF 92.00 9.81 10.45 15.66 OF 94.00 9.82 10.45 15.66 OF 94.00 9.82 10.45 15.66 OF 94.00 9.83 10.45 15.68 OF 96.00 9.83 10.45 15.68 OF 96.00 9.83 10.45 15.69 OF 100.00 9.85 10.45 15.70 OF 100.00 9.86 10.45 15.70 OF 100.00 9.87 10.45 15.70 OF 100.00 9.87 10.45 15.70 OF 100.00 9.87 10.45 15.70 OF 100.00 9.89 10.45 15.70 OF 100.00 9.89 10.45 15.70 OF 100.00 9.89 10.45 15.70 OF 100.00 9.99 10.45 15.70 OF 110.00 9.99 10.45 15.80 OF 110.00 10.00 10.00 10.00 10.00 10.0	OF	46.00	9.38	10.45	15.37
OF 56.00 9.47 10.45 15.43 OF 56.00 9.49 10.45 15.45 OF 6.00 9.52 10.45 15.47 OF 60.00 9.52 10.45 15.47 OF 60.00 9.54 10.45 15.48 OF 62.00 9.57 10.45 15.50 OF 62.00 9.57 10.45 15.50 OF 66.00 9.61 10.45 15.52 OF 66.00 9.61 10.45 15.53 OF 66.00 9.64 10.45 15.53 OF 68.00 9.64 10.45 15.55 OF 67.00 9.66 10.45 15.55 OF 67.00 9.66 10.45 15.55 OF 67.00 9.68 10.45 15.55 OF 67.00 9.68 10.45 15.55 OF 67.00 9.70 10.45 15.55 OF 67.00 9.72 10.45 15.60 OF 68.00 9.73 10.45 15.62 OF 78.00 9.73 10.45 15.62 OF 80.00 9.73 10.45 15.63 OF 80.00 9.74 10.45 15.63 OF 80.00 9.75 10.45 15.65 OF 80.00 9.75 10.45 15.65 OF 80.00 9.78 10.45 15.65 OF 90.00 9.81 10.45 15.65 OF 90.00 9.81 10.45 15.66 OF 92.00 9.81 10.45 15.66 OF 92.00 9.81 10.45 15.66 OF 94.00 9.82 10.45 15.68 OF 96.00 9.83 10.45 15.68 OF 96.00 9.83 10.45 15.68 OF 96.00 9.83 10.45 15.68 OF 96.00 9.88 10.45 15.69 OF 100.00 9.85 10.45 15.69 OF 100.00 9.85 10.45 15.69 OF 100.00 9.85 10.45 15.70 OF 104.00 9.87 10.45 15.70 OF 104.00 9.87 10.45 15.70 OF 104.00 9.87 10.45 15.70 OF 104.00 9.89 10.45 15.72 OF 104.00 9.98 10.45 15.72 OF 104.00 9.99 10.45 15.72 OF 104.00 9.99 10.45 15.72 OF 108.00 9.99 10.45 15.73 OF 118.00 9.99 10.45 15.79 OF 112.00 9.99 10.45 15.79 OF 114.00 9.99 10.45 15.79 OF 114.00 9.99 10.45 15.79 OF 116.00 9.99 10.45 15.80 OF 122.00 10.00 10.01 10.45 15.80 OF 122.00 10.00 10.04 10.	OF	50.00	9.43	10.45	15.40
OF 58.00 9.52 10.45 15.47 OF 60.00 9.54 10.45 15.48 OF 62.00 9.54 10.45 15.50 OF 62.00 9.57 10.45 15.50 OF 62.00 9.57 10.45 15.50 OF 66.00 9.61 10.45 15.52 OF 66.00 9.61 10.45 15.53 OF 66.00 9.61 10.45 15.53 OF 68.00 9.64 10.45 15.55 OF 70.00 9.66 10.45 15.55 OF 70.00 9.66 10.45 15.55 OF 72.00 9.68 10.45 15.55 OF 74.00 9.70 10.45 15.59 OF 74.00 9.70 10.45 15.59 OF 76.00 9.72 10.45 15.61 OF 78.00 9.73 10.45 15.62 OF 80.00 9.73 10.45 15.62 OF 80.00 9.73 10.45 15.62 OF 80.00 9.75 10.45 15.63 OF 84.00 9.76 10.45 15.65 OF 84.00 9.76 10.45 15.65 OF 84.00 9.78 10.45 15.65 OF 84.00 9.78 10.45 15.65 OF 88.00 9.79 10.45 15.65 OF 99.00 9.81 10.45 15.66 OF 92.00 9.81 10.45 15.66 OF 94.00 9.83 10.45 15.66 OF 94.00 9.83 10.45 15.68 OF 96.00 9.83 10.45 15.67 OF 100.00 9.85 10.45 15.67 OF 100.00 9.85 10.45 15.67 OF 102.00 9.86 10.45 15.67 OF 102.00 9.86 10.45 15.70 OF 102.00 9.87 10.45 15.70 OF 106.00 9.89 10.45 15.72 OF 106.00 9.98 10.45 15.72 OF 106.00 9.99 10.45 15.72 OF 110.00 9.91 10.45 15.73 OF 112.00 9.98 10.45 15.79 OF 112.00 9.98 10.45 15.79 OF 112.00 9.99 10.45 15.79 OF 112.00 9.99 10.45 15.79 OF 114.00 9.99 10.45 15.81 OF 128.00 10.01 10.45 15.83 OF 148.00 9.99 10.45 15.80 OF 148.00 9.99 10.45 15.83 OF 148.00 9.99 10.45 15.83 OF 148.0	OF	54.00	9.47	10.45	15.43
OF 62.00 9.57 10.45 15.50 OF 66.00 9.61 10.45 15.52 OF 68.00 9.61 10.45 15.52 OF 68.00 9.64 10.45 15.55 OF 70.00 9.66 10.45 15.55 OF 772.00 9.68 10.45 15.56 OF 772.00 9.86 10.45 15.58 OF 774.00 9.70 10.45 15.58 OF 774.00 9.70 10.45 15.58 OF 776.00 9.72 10.45 15.61 OF 78.00 9.73 10.45 15.61 OF 80.00 9.74 10.45 15.62 OF 80.00 9.74 10.45 15.63 OF 82.00 9.75 10.45 15.63 OF 84.00 9.76 10.45 15.63 OF 88.00 9.78 10.45 15.65 OF 88.00 9.78 10.45 15.65 OF 88.00 9.79 10.45 15.66 OF 90.00 9.80 10.45 15.66 OF 92.00 9.81 10.45 15.66 OF 92.00 9.81 10.45 15.66 OF 94.00 9.82 10.45 15.68 OF 96.00 9.83 10.45 15.68 OF 96.00 9.83 10.45 15.69 OF 9100.00 9.85 10.45 15.69 OF 102.00 9.86 10.45 15.70 OF 102.00 9.86 10.45 15.70 OF 104.00 9.87 10.45 15.70 OF 104.00 9.87 10.45 15.70 OF 106.00 9.89 10.45 15.77 OF 106.00 9.89 10.45 15.77 OF 110.00 9.99 10.45 15.77 OF 12.00 9.98 10.45 15.77 OF 12.00 9.98 10.45 15.77 OF 12.00 9.99 10.45 15.77 OF 13.00 10.01 10.45 15.81 OF 14.00 9.99 10.45 15.82 OF 140.00 9.99 10.45 15.83 OF 140.00 9.99 10.45 15.83 OF 150.00 9.99 10.45 15.83 OF 160.00 9.99 10.45 15.83 OF 160.00 10.01 10.45 15.83 OF 160.00 10.01 10.45 15.83 OF 150.00 9.99 10.45 15.88 OF 150.00 10.00 10.00 10.45 15.88 OF 150.00 10.00 10.00 10.45 15.88 OF 150.00 10.00 10.00 10.45 15.88 OF 160.00 10.00 10.00 10.45 15.88 OF 160.00 10.00 10.					
OF 64.00 9.59 10.45 15.52 OF 68.00 9.61 10.45 15.53 OF 68.00 9.64 10.45 15.55 OF 70.00 9.66 10.45 15.55 OF 72.00 9.68 10.45 15.56 OF 72.00 9.68 10.45 15.58 OF 74.00 9.70 10.45 15.59 OF 76.00 9.72 10.45 15.59 OF 776.00 9.72 10.45 15.61 OF 78.00 9.73 10.45 15.62 OF 80.00 9.74 10.45 15.62 OF 82.00 9.75 10.45 15.63 OF 80.00 9.76 10.45 15.63 OF 86.00 9.78 10.45 15.65 OF 86.00 9.78 10.45 15.65 OF 90.00 9.80 10.45 15.65 OF 90.00 9.80 10.45 15.66 OF 92.00 9.81 10.45 15.66 OF 92.00 9.81 10.45 15.66 OF 94.00 9.82 10.45 15.68 OF 94.00 9.83 10.45 15.68 OF 96.00 9.84 10.45 15.68 OF 96.00 9.84 10.45 15.69 OF 97.00 9.84 10.45 15.69 OF 98.00 9.84 10.45 15.69 OF 100.00 9.85 10.45 15.69 OF 100.00 9.86 10.45 15.69 OF 100.00 9.86 10.45 15.70 OF 104.00 9.87 10.45 15.70 OF 104.00 9.89 10.45 15.70 OF 104.00 9.89 10.45 15.72 OF 104.00 9.89 10.45 15.72 OF 104.00 9.99 10.45 15.73 OF 104.00 9.99 10.45 15.73 OF 12.00 9.99 10.45 15.79 OF 12.00 9.99 10.45 15.79 OF 122.00 10.00 10.45 15.80 OF 122.00 9.98 10.45 15.79 OF 122.00 10.00 10.45 15.81 OF 122.00 9.98 10.45 15.79 OF 122.00 10.00 10.45 15.81 OF 126.00 10.01 10.45 15.81 OF 126.00 10.01 10.45 15.81 OF 126.00 10.02 10.45 15.81 OF 126.00 10.01 10.45 15.81 OF 126.00 9.99 10.45 15.81 OF 126.00 10.01 10.45 15.81 OF 126.00 9.99 10.45 15.81 OF 126.00 10.01 10.45 15.81 OF 126.00 9.99 10.45 15.80 OF 126.00 10.01 10.45 15.81 OF 126.00 9.99 10.45 15.80 OF 126.00 10.01 10.45 15.81 OF 126.00 9.99 10.45 15.80 OF 126.00 9.99 10.45 15.80 OF 126.00 10.01 10.45 15.81 OF 126.00 10.01 10.45 15.83 OF 140.00 10.01 10.45 15.83 OF 140.00 10.01 10.45 15.83 OF 140.00 10.01 10.45 15.88 OF 140.00 10.01 10.45 15.88 OF 140.00 10.01 10.45 15.88 OF 140.00 10.01					
OF 68.00 9.64 10.45 15.55 OF 70.00 9.66 10.45 15.56 OF 72.00 9.68 10.45 15.56 OF 72.00 9.68 10.45 15.59 OF 74.00 9.70 10.45 15.59 OF 76.00 9.72 10.45 15.61 OF 78.00 9.72 10.45 15.62 OF 80.00 9.74 10.45 15.62 OF 82.00 9.75 10.45 15.63 OF 86.00 9.76 10.45 15.63 OF 86.00 9.76 10.45 15.63 OF 86.00 9.78 10.45 15.65 OF 86.00 9.78 10.45 15.65 OF 90.00 9.80 10.45 15.65 OF 90.00 9.80 10.45 15.66 OF 92.00 9.81 10.45 15.66 OF 92.00 9.83 10.45 15.66 OF 94.00 9.82 10.45 15.68 OF 96.00 9.83 10.45 15.68 OF 98.00 9.84 10.45 15.68 OF 98.00 9.88 10.45 15.69 OF 100.00 9.85 10.45 15.70 OF 100.00 9.86 10.45 15.70 OF 104.00 9.87 10.45 15.70 OF 104.00 9.89 10.45 15.72 OF 104.00 9.99 10.45 15.72 OF 108.00 9.90 10.45 15.72 OF 112.00 9.99 10.45 15.73 OF 112.00 9.99 10.45 15.79 OF 112.00 9.99 10.45 15.79 OF 122.00 9.98 10.45 15.79 OF 122.00 10.00 10.45 15.80 OF 122.00 10.00 10.45 15.81 OF 124.00 10.01 10.45 15.81 OF 125.00 9.99 10.45 15.79 OF 126.00 10.02 10.45 15.81 OF 126.00 10.02 10.45 15.81 OF 126.00 10.02 10.45 15.81 OF 126.00 10.01 10.45 15.81 OF 136.00 9.99 10.45 15.79 OF 126.00 10.02 10.45 15.81 OF 136.00 9.99 10.45 15.81 OF 126.00 10.01 10.45 15.81 OF 136.00 9.99 10.45 15.81 OF 126.00 10.02 10.45 15.81 OF 136.00 9.99 10.45 15.82 OF 146.00 9.99 10.45 15.83 OF 146.00 9.99 10.45 15.80 OF 146.00 10.01 10.45 15.81 OF 146.00 9.99 10.45 15.83 OF 146.00 10.01 10.45 15.83 OF 146.00 10.01 10.45 15.83 OF 146.00 10.01 10.45 15.83 OF 146.00 10.02 10.45 15.83 OF 146.00 10.01 10.45 15.83 OF 146.00 10.02 10.45 15.88 OF 146.00 10.00 10.05 10.45 15.88 OF 146.00 10.00 10.00 10.45 15.88 OF 146.0			9.59		
OF         72.00         9.68         10.45         15.58           OF         74.00         9.70         10.45         15.61           OF         76.00         9.73         10.45         15.62           OF         80.00         9.74         10.45         15.62           OF         82.00         9.75         10.45         15.63           OF         84.00         9.76         10.45         15.65           OF         86.00         9.78         10.45         15.65           OF         80.00         9.78         10.45         15.65           OF         90.00         9.80         10.45         15.66           OF         92.00         9.81         10.45         15.66           OF         92.00         9.81         10.45         15.68           OF         92.00         9.81         10.45         15.68           OF         92.00         9.81         10.45         15.68           OF         92.00         9.83         10.45         15.70           OF         92.00         9.85         10.45         15.70           OF         102.00         9.87         10.45 </td <td>OF</td> <td>68.00</td> <td>9.64</td> <td>10.45</td> <td>15.55</td>	OF	68.00	9.64	10.45	15.55
OF         76.00         9.72         10.45         15.61           OF         80.00         9.74         10.45         15.62           OF         80.00         9.75         10.45         15.62           OF         84.00         9.75         10.45         15.63           OF         86.00         9.78         10.45         15.65           OF         80.00         9.79         10.45         15.65           OF         90.00         9.80         10.45         15.66           OF         92.00         9.81         10.45         15.66           OF         92.00         9.81         10.45         15.68           OF         94.00         9.82         10.45         15.68           OF         94.00         9.83         10.45         15.68           OF         94.00         9.85         10.45         15.70           OF         90.00         9.85         10.45         15.70           OF         100.00         9.85         10.45         15.70           OF         104.00         9.87         10.45         15.72           OF         106.00         9.98         10.45	OF	72.00	9.68	10.45	15.58
OF         80.00         9.74         10.45         15.62           OF         82.00         9.75         10.45         15.63           OF         84.00         9.76         10.45         15.65           OF         86.00         9.78         10.45         15.65           OF         90.00         9.80         10.45         15.66           OF         92.00         9.81         10.45         15.66           OF         94.00         9.82         10.45         15.68           OF         94.00         9.83         10.45         15.68           OF         96.00         9.83         10.45         15.68           OF         96.00         9.83         10.45         15.68           OF         100.00         9.85         10.45         15.70           OF         102.00         9.86         10.45         15.77           OF         104.00         9.87         10.45         15.72           OF         104.00         9.87         10.45         15.72           OF         104.00         9.91         10.45         15.72           OF         104.00         9.91         10	OF	76.00	9.72	10.45	15.61
OF         84.00         9.76         10.45         15.64           OF         86.00         9.78         10.45         15.65           OF         98.00         9.79         10.45         15.65           OF         92.00         9.81         10.45         15.66           OF         94.00         9.82         10.45         15.68           OF         96.00         9.83         10.45         15.68           OF         98.00         9.84         10.45         15.68           OF         98.00         9.84         10.45         15.69           OF         100.00         9.85         10.45         15.69           OF         102.00         9.86         10.45         15.70           OF         104.00         9.87         10.45         15.72           OF         106.00         9.87         10.45         15.72           OF         108.00         9.90         10.45         15.72           OF         108.00         9.91         10.45         15.73           OF         106.00         9.99         10.45         15.74           OF         112.00         9.99	OF	80.00	9.74	10.45	15.62
OF         88.00         9.79         10.45         15.65           OF         90.00         9.80         10.45         15.66           OF         92.00         9.81         10.45         15.68           OF         94.00         9.82         10.45         15.68           OF         98.00         9.84         10.45         15.68           OF         100.00         9.85         10.45         15.70           OF         102.00         9.86         10.45         15.70           OF         102.00         9.86         10.45         15.71           OF         106.00         9.87         10.45         15.72           OF         106.00         9.87         10.45         15.72           OF         108.00         9.90         10.45         15.73           OF         110.00         9.91         10.45         15.73           OF         110.00         9.99         10.45         15.73           OF         112.00         9.99         10.45         15.75           OF         112.00         9.98         10.45         15.79           OF         112.00         9.98         <			9.76	10.45	15.64
OF         92.00         9.81         10.45         15.67           OF         94.00         9.82         10.45         15.68           OF         96.00         9.83         10.45         15.68           OF         100.00         9.85         10.45         15.70           OF         102.00         9.86         10.45         15.71           OF         102.00         9.87         10.45         15.72           OF         106.00         9.87         10.45         15.72           OF         108.00         9.90         10.45         15.72           OF         108.00         9.90         10.45         15.73           OF         110.00         9.91         10.45         15.73           OF         112.00         9.92         10.45         15.75           OF         116.00         9.98         10.45         15.79           OF         116.00         9.98         10.45         15.79           OF         118.00         9.98         10.45         15.79           OF         120.00         10.01         10.45         15.81           OF         120.00         10.01					
OF         94.00         9.82         10.45         15.68           OF         96.00         9.83         10.45         15.69           OF         100.00         9.85         10.45         15.70           OF         102.00         9.86         10.45         15.71           OF         104.00         9.87         10.45         15.72           OF         106.00         9.89         10.45         15.72           OF         106.00         9.89         10.45         15.72           OF         108.00         9.90         10.45         15.73           OF         110.00         9.91         10.45         15.73           OF         112.00         9.92         10.45         15.74           OF         112.00         9.98         10.45         15.79           OF         116.00         9.98         10.45         15.79           OF         118.00         9.98         10.45         15.79           OF         120.00         10.00         10.45         15.80           OF         124.00         10.01         10.45         15.81           OF         124.00         10.01					
OF         98.00         9.84         10.45         15.69           OF         100.00         9.85         10.45         15.71           OF         104.00         9.87         10.45         15.71           OF         106.00         9.87         10.45         15.72           OF         106.00         9.99         10.45         15.72           OF         110.00         9.91         10.45         15.73           OF         112.00         9.91         10.45         15.74           OF         114.00         9.99         10.45         15.75           OF         114.00         9.98         10.45         15.79           OF         114.00         9.98         10.45         15.79           OF         120.00         9.98         10.45         15.79           OF         120.00         9.98         10.45         15.79           OF         122.00         10.01         10.45         15.81           OF         122.00         10.01         10.45         15.81           OF         126.00         10.01         10.45         15.81           OF         130.00         10.01	OF	94.00	9.82	10.45	15.68
OF         102.00         9.86         10.45         15.71           OF         104.00         9.87         10.45         15.72           OF         106.00         9.89         10.45         15.72           OF         108.00         9.90         10.45         15.73           OF         110.00         9.91         10.45         15.74           OF         112.00         9.92         10.45         15.74           OF         114.00         9.99         10.45         15.79           OF         116.00         9.98         10.45         15.79           OF         118.00         9.98         10.45         15.79           OF         120.00         9.98         10.45         15.79           OF         120.00         10.01         10.45         15.81           OF         124.00         10.01         10.45         15.81           OF         124.00         10.01         10.45         15.81           OF         130.00         10.01         10.45         15.81           OF         132.00         10.01         10.45         15.81           OF         134.00         10.01 <td>OF</td> <td>98.00</td> <td>9.84</td> <td>10.45</td> <td>15.69</td>	OF	98.00	9.84	10.45	15.69
OF         106.00         9.89         10.45         15.72           OF         108.00         9.90         10.45         15.73           OF         110.00         9.91         10.45         15.74           OF         112.00         9.92         10.45         15.75           OF         114.00         9.99         10.45         15.79           OF         118.00         9.98         10.45         15.79           OF         120.00         9.98         10.45         15.79           OF         120.00         9.98         10.45         15.79           OF         120.00         10.00         10.45         15.80           OF         124.00         10.01         10.45         15.81           OF         124.00         10.01         10.45         15.81           OF         124.00         10.01         10.45         15.81           OF         126.00         10.01         10.45         15.81           OF         130.00         10.01         10.45         15.81           OF         134.00         10.01         10.45         15.81           OF         134.00         10.01 </td <td>OF</td> <td>102.00</td> <td>9.86</td> <td>10.45</td> <td>15.71</td>	OF	102.00	9.86	10.45	15.71
OF         110.00         9.91         10.45         15.74           OF         112.00         9.92         10.45         15.75           OF         116.00         9.98         10.45         15.80           OF         116.00         9.98         10.45         15.79           OF         118.00         9.98         10.45         15.79           OF         120.00         9.98         10.45         15.79           OF         122.00         10.00         10.45         15.79           OF         122.00         10.01         10.45         15.81           OF         124.00         10.01         10.45         15.81           OF         126.00         10.01         10.45         15.81           OF         128.00         10.01         10.45         15.81           OF         130.00         10.01         10.45         15.81           OF         132.00         10.01         10.45         15.81           OF         134.00         10.01         10.45         15.81           OF         136.00         10.01         10.45         15.81           OF         138.00         10.03	OF	106.00	9.89	10.45	15.72
OF         114.00         9.99         10.45         15.80           OF         116.00         9.98         10.45         15.79           OF         118.00         9.98         10.45         15.79           OF         120.00         9.98         10.45         15.79           OF         122.00         10.00         10.45         15.80           OF         122.00         10.01         10.45         15.81           OF         126.00         10.01         10.45         15.81           OF         128.00         10.01         10.45         15.81           OF         130.00         10.01         10.45         15.81           OF         132.00         10.00         10.45         15.81           OF         134.00         10.01         10.45         15.81           OF         136.00         10.01         10.45         15.81           OF         136.00         10.01         10.45         15.81           OF         138.00         10.03         10.45         15.82           OF         140.00         10.02         10.45         15.82           OF         140.00         10.	OF	110.00	9.91	10.45	15.74
OF         118.00         9.98         10.45         15.79           OF         120.00         9.98         10.45         15.79           OF         122.00         10.00         10.45         15.80           OF         124.00         10.01         10.45         15.81           OF         126.00         10.02         10.45         15.81           OF         128.00         10.01         10.45         15.81           OF         130.00         10.01         10.45         15.81           OF         132.00         10.00         10.45         15.81           OF         134.00         10.01         10.45         15.81           OF         136.00         10.01         10.45         15.81           OF         136.00         10.01         10.45         15.81           OF         138.00         10.03         10.45         15.81           OF         138.00         10.02         10.45         15.82           OF         140.00         10.02         10.45         15.82           OF         144.00         9.99         10.45         15.81           OF         146.00         9.		114.00	9.99	10.45	15.80
OF         122.00         10.00         10.45         15.80           OF         124.00         10.01         10.45         15.81           OF         126.00         10.02         10.45         15.81           OF         128.00         10.01         10.45         15.81           OF         130.00         10.01         10.45         15.81           OF         134.00         10.01         10.45         15.81           OF         134.00         10.01         10.45         15.81           OF         136.00         10.01         10.45         15.81           OF         138.00         10.01         10.45         15.81           OF         138.00         10.02         10.45         15.82           OF         140.00         10.02         10.45         15.82           OF         140.00         10.02         10.45         15.82           OF         144.00         9.99         10.45         15.81           OF         146.00         9.99         10.45         15.80           OF         148.00         9.97         10.45         15.78           OF         150.00         9.			9.98 9.98		
OF         124,00         10.01         10.45         15.81           OF         126.00         10.02         10.45         15.81           OF         128.00         10.01         10.45         15.81           OF         130.00         10.01         10.45         15.81           OF         132.00         10.00         10.45         15.81           OF         134.00         10.01         10.45         15.81           OF         136.00         10.01         10.45         15.81           OF         138.00         10.03         10.45         15.82           OF         140.00         10.02         10.45         15.82           OF         142.00         10.02         10.45         15.82           OF         144.00         9.99         10.45         15.80           OF         146.00         9.98         10.45         15.79           OF         148.00         9.97         10.45         15.78           OF         150.00         9.98         10.45         15.78           OF         154.00         9.98         10.45         15.78           OF         154.00         9.98					
OF         128.00         10.01         10.45         15.81           OF         130.00         10.01         10.45         15.81           OF         132.00         10.00         10.45         15.80           OF         134.00         10.01         10.45         15.81           OF         136.00         10.01         10.45         15.81           OF         138.00         10.03         10.45         15.82           OF         140.00         10.02         10.45         15.82           OF         142.00         10.02         10.45         15.82           OF         144.00         9.99         10.45         15.81           OF         146.00         9.99         10.45         15.80           OF         146.00         9.99         10.45         15.79           OF         148.00         9.97         10.45         15.78           OF         150.00         9.96         10.45         15.78           OF         152.00         9.97         10.45         15.78           OF         154.00         9.98         10.45         15.79           OF         156.00         9.98 </td <td>OF</td> <td>124.00</td> <td>10.01</td> <td>10.45</td> <td>15.81</td>	OF	124.00	10.01	10.45	15.81
OF         132.00         10.00         10.45         15.80           OF         134.00         10.01         10.45         15.81           OF         136.00         10.01         10.45         15.81           OF         138.00         10.03         10.45         15.82           OF         140.00         10.02         10.45         15.82           OF         142.00         10.02         10.45         15.81           OF         144.00         9.99         10.45         15.80           OF         146.00         9.98         10.45         15.78           OF         148.00         9.97         10.45         15.78           OF         150.00         9.96         10.45         15.78           OF         150.00         9.97         10.45         15.78           OF         150.00         9.97         10.45         15.78           OF         154.00         9.98         10.45         15.78           OF         156.00         9.98         10.45         15.79           OF         158.00         9.99         10.45         15.80           OF         160.00         10.01 <td>OF</td> <td>128.00</td> <td>10.01</td> <td>10.45</td> <td>15.81</td>	OF	128.00	10.01	10.45	15.81
OF         136.00         10.01         10.45         15.81           OF         138.00         10.03         10.45         15.82           OF         140.00         10.02         10.45         15.82           OF         142.00         10.02         10.45         15.81           OF         144.00         9.99         10.45         15.80           OF         146.00         9.98         10.45         15.79           OF         148.00         9.97         10.45         15.78           OF         150.00         9.96         10.45         15.78           OF         150.00         9.97         10.45         15.78           OF         154.00         9.98         10.45         15.78           OF         154.00         9.98         10.45         15.79           OF         156.00         9.98         10.45         15.79           OF         156.00         9.98         10.45         15.79           OF         160.00         10.00         10.45         15.80           OF         160.00         10.00         10.45         15.80           OF         160.00         10.01 <td>OF</td> <td>132.00</td> <td>10.00</td> <td>10.45</td> <td>15.80</td>	OF	132.00	10.00	10.45	15.80
OF         140.00         10.02         10.45         15.82           OF         142.00         10.02         10.45         15.81           OF         144.00         9.99         10.45         15.80           OF         146.00         9.98         10.45         15.79           OF         148.00         9.97         10.45         15.78           OF         150.00         9.96         10.45         15.78           OF         152.00         9.97         10.45         15.78           OF         154.00         9.98         10.45         15.79           OF         156.00         9.98         10.45         15.79           OF         158.00         9.99         10.45         15.80           OF         160.00         10.00         10.45         15.80           OF         160.00         10.01         10.45         15.80           OF         160.00         10.01         10.45         15.80           OF         166.00         10.01         10.45         15.81           OF         166.00         10.03         10.45         15.82           OF         168.00         10.03 </td <td>OF</td> <td>136.00</td> <td>10.01</td> <td>10.45</td> <td>15.81</td>	OF	136.00	10.01	10.45	15.81
OF         144.00         9.99         10.45         15.80           OF         146.00         9.98         10.45         15.79           OF         148.00         9.97         10.45         15.78           OF         150.00         9.96         10.45         15.78           OF         152.00         9.97         10.45         15.78           OF         154.00         9.98         10.45         15.79           OF         156.00         9.98         10.45         15.79           OF         158.00         9.99         10.45         15.80           OF         160.00         10.00         10.45         15.80           OF         162.00         10.01         10.45         15.81           OF         164.00         10.02         10.45         15.82           OF         166.00         10.03         10.45         15.82           OF         168.00         10.03         10.45         15.83           OF         170.00         10.04         10.45         15.83           OF         174.00         10.05         10.45         15.83           OF         178.00         10.05 </td <td>OF</td> <td>140.00</td> <td>10.02</td> <td>10.45</td> <td>15.82</td>	OF	140.00	10.02	10.45	15.82
OF         148.00         9.97         10.45         15.78           OF         150.00         9.96         10.45         15.78           OF         152.00         9.97         10.45         15.78           OF         154.00         9.98         10.45         15.79           OF         156.00         9.98         10.45         15.79           OF         160.00         9.99         10.45         15.80           OF         160.00         10.00         10.45         15.80           OF         162.00         10.01         10.45         15.81           OF         164.00         10.02         10.45         15.82           OF         166.00         10.03         10.45         15.82           OF         168.00         10.03         10.45         15.82           OF         170.00         10.04         10.45         15.83           OF         172.00         10.04         10.45         15.83           OF         174.00         10.05         10.45         15.84           OF         178.00         10.05         10.45         15.84           OF         180.00         10.06	OF	144.00	9.99	10.45	15.80
OF         152.00         9.97         10.45         15.78           OF         154.00         9.98         10.45         15.79           OF         156.00         9.98         10.45         15.79           OF         158.00         9.99         10.45         15.80           OF         160.00         10.01         10.45         15.80           OF         162.00         10.01         10.45         15.81           OF         164.00         10.02         10.45         15.82           OF         166.00         10.03         10.45         15.82           OF         168.00         10.03         10.45         15.83           OF         170.00         10.04         10.45         15.83           OF         172.00         10.04         10.45         15.83           OF         174.00         10.05         10.45         15.84           OF         178.00         10.05         10.45         15.84           OF         180.00         10.05         10.45         15.85           OF         184.00         10.06         10.45         15.85           OF         184.00         10.					
OF         154.00         9.98         10.45         15.79           OF         156.00         9.98         10.45         15.79           OF         158.00         9.99         10.45         15.80           OF         160.00         10.00         10.45         15.80           OF         162.00         10.01         10.45         15.81           OF         164.00         10.02         10.45         15.82           OF         166.00         10.03         10.45         15.82           OF         168.00         10.03         10.45         15.83           OF         170.00         10.04         10.45         15.83           OF         172.00         10.04         10.45         15.83           OF         174.00         10.05         10.45         15.84           OF         178.00         10.05         10.45         15.84           OF         180.00         10.06         10.45         15.85           OF         184.00         10.07         10.45         15.85           OF         184.00         10.08         10.45         15.86           OF         186.00         10	OF				15.78 15.78
OF         158.00         9.99         10.45         15.80           OF         160.00         10.00         10.45         15.80           OF         162.00         10.01         10.45         15.81           OF         164.00         10.02         10.45         15.82           OF         166.00         10.03         10.45         15.83           OF         170.00         10.04         10.45         15.83           OF         172.00         10.04         10.45         15.83           OF         174.00         10.05         10.45         15.84           OF         176.00         10.05         10.45         15.84           OF         178.00         10.05         10.45         15.84           OF         180.00         10.06         10.45         15.85           OF         184.00         10.06         10.45         15.85           OF         184.00         10.08         10.45         15.86           OF         186.00         10.08         10.45         15.86           OF         188.00         10.09         10.45         15.87           OF         190.00	OF	154.00	9.98	10.45	15.79
OF         162.00         10.01         10.45         15.81           OF         164.00         10.02         10.45         15.82           OF         166.00         10.03         10.45         15.82           OF         168.00         10.03         10.45         15.83           OF         170.00         10.04         10.45         15.83           OF         172.00         10.04         10.45         15.83           OF         174.00         10.05         10.45         15.84           OF         176.00         10.05         10.45         15.84           OF         178.00         10.05         10.45         15.84           OF         180.00         10.06         10.45         15.85           OF         182.00         10.07         10.45         15.85           OF         184.00         10.08         10.45         15.86           OF         186.00         10.08         10.45         15.86           OF         188.00         10.09         10.45         15.87           OF         190.00         10.10         10.45         15.87	OF	158.00	9.99	10.45	15.80
OF         166.00         10.03         10.45         15.82           OF         168.00         10.03         10.45         15.83           OF         170.00         10.04         10.45         15.83           OF         172.00         10.04         10.45         15.83           OF         174.00         10.05         10.45         15.84           OF         176.00         10.05         10.45         15.84           OF         178.00         10.05         10.45         15.84           OF         180.00         10.06         10.45         15.85           OF         182.00         10.07         10.45         15.85           OF         184.00         10.08         10.45         15.86           OF         186.00         10.08         10.45         15.86           OF         188.00         10.09         10.45         15.87           OF         190.00         10.10         10.45         15.87	OF	162.00	10.01	10.45	15.81
OF         170.00         10.04         10.45         15.83           OF         172.00         10.04         10.45         15.83           OF         174.00         10.05         10.45         15.84           OF         176.00         10.05         10.45         15.84           OF         178.00         10.05         10.45         15.84           OF         180.00         10.06         10.45         15.85           OF         182.00         10.07         10.45         15.85           OF         184.00         10.08         10.45         15.86           OF         186.00         10.09         10.45         15.86           OF         188.00         10.09         10.45         15.87           OF         190.00         10.10         10.45         15.87	OF	166.00	10.03	10.45	15.82
OF     174.00     10.05     10.45     15.84       OF     176.00     10.05     10.45     15.84       OF     178.00     10.05     10.45     15.84       OF     180.00     10.06     10.45     15.85       OF     182.00     10.07     10.45     15.85       OF     184.00     10.08     10.45     15.86       OF     186.00     10.08     10.45     15.86       OF     188.00     10.09     10.45     15.87       OF     190.00     10.10     10.45     15.87	OF	170.00	10.04	10.45	15.83
OF     178.00     10.05     10.45     15.84       OF     180.00     10.06     10.45     15.85       OF     182.00     10.07     10.45     15.85       OF     184.00     10.08     10.45     15.86       OF     186.00     10.08     10.45     15.86       OF     188.00     10.09     10.45     15.87       OF     190.00     10.10     10.45     15.87	OF	174.00	10.05	10.45	15.84
OF     180.00     10.06     10.45     15.85       OF     182.00     10.07     10.45     15.85       OF     184.00     10.08     10.45     15.86       OF     186.00     10.08     10.45     15.86       OF     188.00     10.09     10.45     15.87       OF     190.00     10.10     10.45     15.87					
OF     184.00     10.08     10.45     15.86       OF     186.00     10.08     10.45     15.86       OF     188.00     10.09     10.45     15.87       OF     190.00     10.10     10.45     15.87	OF	180.00	10.06	10.45	15.85
OF 188.00 10.09 10.45 15.87 OF 190.00 10.10 10.45 15.87	OF	184.00	10.08	10.45	15.86
	OF	188.00	10.09	10.45	15.87

OF	194.00	10.09	10.45	15.87
OF	196.00	10.09	10.45	15.87
OF	198.00	10.08	10.45	15.86
OF	200.00	10.08	10.45	15.86
OF	202.00	10.07	10.45	15.85
OF	204.00	10.06	10.45	15.84
OF	206.00	10.05	10.45	15.84
OF	208.00	10.07	10.45	15.85
OF	210.00	10.09	10.45	15.87
OF	212.00	10.08	10.45	15.86
OF	214.00	10.05	10.45	15.84
OF	216.00	10.06	10.45	15.85
OF	218.00	10.02	10.45	15.82
OF	220.00	10.01	10.45	15.81
OF	222.00	10.02	10.45 10.45	15.82
OF	224.00 226.00	10.04	10.45	15.83 15.87
OF OF	228.00	10.09 10.12	10.45	15.89
OF	230.00	10.12	10.45	15.89
OF	232.00	10.11	10.45	15.88
OF	234.00	10.10	10.45	15.87
OF	236.00	10.09	10.45	15.86
OF	238.00	10.09	10.45	15.86
OF	240.00	10.10	10.45	15.87
OF	242.00	10.10	10.45	15.87
OF	244.00	10.11	10.45	15.88
OF	246.00	10.11	10.45	15.88
OF	248.00	10.11	10.45	15.88
OF	250.00	10.11	10.45 10.45	15.88 15.87
OF OF	252.00 254.00	10.09 10.07	10.45	15.85
OF	256.00	10.06	10.45	15.84
OF	258.00	10.06	10.45	15.84
OF	260.00	10.07	10.45	15.85
OF	262.00	10.07	10.45	15.85
OF	264.00	10.06	10.45	15.84
OF	266.00	10.08	10.45	15.86
OF	268.00	10.11	10.45	15.88
OF	270.00	10.11	10.45	15.88
OF	272.00	10.10	10.45	15.87
OF	274.00	10.12	10.45	15.89
OF	276.00	10.12	10.45	15.89
OF	278.00	10.12 10.12	10.45 10.45	15.89 15.89
OF OF	280.00 282.00	10.12	10.45	15.88
OF	284.00	10.10	10.45	15.87
OF	286.00	10.10	10.45	15.87
OF	288.00	10.10	10.45	15.88
OF	290.00	10.11	10.45	15.88
OF	292.00	10.11	10.45	15.88
OF	294.00	10.11	10.45	15.88
OF	296.00	10.14	10.45	15.90
OF	298.00	10.14	10.45	15.90
OF	300.00	10.14	10.45	15.90
OF	302.00	10.14	10.45 10.45	15.90 15.90
OF OF	304.00 306.00	10.14 10.14	10.45	15.90
OF	308.00	10.15	10.45	15.91
OF	310.00	10.16	10.45	15.91
OF	312.00	10.16	10.45	15.92
OF	314.00	10.17	10.45	15.92
OF	316.00	10.17	10.45	15.93
OF	318.00	10.17	10.45	15.92
OF	320.00	10.16	10.45	15.92
OF OF	322.00 324.00	10.16 10.16	10.45 10.45	15.92 15.91
OF	326.00	10.15	10.45	15.91
OF	328.00	10.15	10.45	15.91
OF	330.00	10.16	10.45	15.91
OF	332.00	10.16	10.45	15.91
OF	334.00	10.16	10.45	15.91
OF	336.00	10.16	10.45	15.91
OF	338.00 340.00	10.16	10.45 10.45	15.91 15.91
OF OF	342.00	10.16 10.16	10.45	15.91
OF	344.00		10.45	15.92
OF		TO.TO		
	346.00	10.16 10.16	10.45	15.92
OF		10.16 10.16 10.16		15.92 15.92
OF	346.00 348.00 350.00	10.16 10.16 10.16	10.45 10.45 10.45	15.92 15.92
OF OF	346.00 348.00 350.00 352.00	10.16 10.16 10.16 10.16	10.45 10.45 10.45 10.45	15.92 15.92 15.92
OF OF OF	346.00 348.00 350.00 352.00 354.00	10.16 10.16 10.16 10.16 10.17	10.45 10.45 10.45 10.45 10.45	15.92 15.92 15.92 15.92
OF OF OF	346.00 348.00 350.00 352.00 354.00 356.00	10.16 10.16 10.16 10.16 10.17 10.06	10.45 10.45 10.45 10.45 10.45 10.45	15.92 15.92 15.92 15.92 15.85
OF OF OF OF	346.00 348.00 350.00 352.00 354.00 356.00 358.00	10.16 10.16 10.16 10.16 10.17 10.06 9.90	10.45 10.45 10.45 10.45 10.45 10.45	15.92 15.92 15.92 15.92 15.85 15.74
OF OF OF OF OF	346.00 348.00 350.00 352.00 354.00 356.00 358.00 360.00	10.16 10.16 10.16 10.16 10.17 10.06 9.90 9.77	10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45	15.92 15.92 15.92 15.92 15.85 15.74 15.64
OF OF OF OF OF	346.00 348.00 350.00 352.00 354.00 356.00 358.00 360.00 362.00	10.16 10.16 10.16 10.16 10.17 10.06 9.90 9.77 9.67	10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45	15.92 15.92 15.92 15.92 15.85 15.74 15.64
OF OF OF OF OF	346.00 348.00 350.00 352.00 354.00 356.00 358.00 360.00	10.16 10.16 10.16 10.16 10.17 10.06 9.90 9.77	10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45	15.92 15.92 15.92 15.92 15.85 15.74 15.64 15.58
OF OF OF OF OF OF OF	346.00 348.00 350.00 352.00 354.00 356.00 360.00 362.00 364.00	10.16 10.16 10.16 10.16 10.17 10.06 9.90 9.77 9.67 9.59 9.39 9.10	10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45	15.92 15.92 15.92 15.85 15.74 15.64 15.58 15.52 15.38
OF OF OF OF OF OF OF OF	346.00 348.00 350.00 352.00 354.00 356.00 360.00 362.00 364.00 366.00 368.00 370.00	10.16 10.16 10.16 10.17 10.06 9.90 9.77 9.67 9.59 9.39 9.10 8.94	10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45	15.92 15.92 15.92 15.92 15.85 15.74 15.64 15.58 15.52 15.38
OF OF OF OF OF OF OF OF OF	346.00 348.00 350.00 352.00 354.00 356.00 360.00 362.00 364.00 366.00 368.00 370.00	10.16 10.16 10.16 10.16 10.17 10.06 9.90 9.77 9.67 9.59 9.39 9.10 8.94	10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45	15.92 15.92 15.92 15.92 15.65 15.74 15.64 15.58 15.52 15.38 15.18
OF OF OF OF OF OF OF OF OF	346.00 348.00 350.00 352.00 354.00 356.00 360.00 362.00 364.00 366.00 368.00 370.00 372.00	10.16 10.16 10.16 10.16 10.17 10.06 9.90 9.77 9.67 9.59 9.39 9.10 8.94 8.78	10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45	15.92 15.92 15.92 15.85 15.74 15.64 15.58 15.52 15.38 15.18 15.07 14.95
OF	346.00 348.00 350.00 352.00 354.00 356.00 360.00 362.00 364.00 366.00 368.00 370.00 371.00 372.00 374.00 376.00	10.16 10.16 10.16 10.17 10.06 9.90 9.77 9.67 9.59 9.39 9.10 8.94 8.78 8.63 8.55	10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45	15.92 15.92 15.92 15.85 15.74 15.64 15.58 15.52 15.38 15.18 15.07 14.95
OF O	346.00 348.00 350.00 352.00 354.00 356.00 360.00 362.00 364.00 366.00 376.00 371.00 376.00 378.00	10.16 10.16 10.16 10.16 10.17 10.06 9.90 9.77 9.67 9.59 9.39 9.10 8.94 8.63 8.63 8.55 8.48	10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45	15.92 15.92 15.92 15.85 15.74 15.64 15.58 15.52 15.38 15.18 15.14 15.47 14.95 14.85
OF O	346.00 348.00 350.00 3552.00 354.00 356.00 360.00 362.00 364.00 366.00 368.00 370.00 372.00 374.00 378.00 380.00	10.16 10.16 10.16 10.16 10.17 10.06 9.90 9.77 9.59 9.39 9.10 8.94 8.63 8.55 8.48 8.13	10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45	15.92 15.92 15.92 15.85 15.74 15.64 15.58 15.52 15.38 15.18 15.07 14.95 14.85 14.79 14.74
OF O	346.00 348.00 350.00 352.00 354.00 356.00 360.00 362.00 364.00 366.00 368.00 370.00 372.00 374.00 374.00 378.00 380.00 380.00	10.16 10.16 10.16 10.17 10.06 9.90 9.77 9.67 9.59 9.39 9.10 8.94 8.78 8.63 8.55 8.48 8.13 7.88	10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45	15.92 15.92 15.92 15.85 15.74 15.64 15.58 15.52 15.38 15.18 15.07 14.95 14.79 14.74
OF O	346.00 348.00 350.00 350.00 352.00 354.00 356.00 360.00 362.00 364.00 366.00 370.00 371.00 374.00 376.00 378.00 388.00 388.00	10.16 10.16 10.16 10.16 10.17 10.06 9.90 9.77 9.67 9.59 9.39 9.10 8.94 8.63 8.63 8.55 8.48 8.13 7.88	10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45	15.92 15.92 15.92 15.85 15.74 15.64 15.58 15.52 15.38 15.18 15.14.95 14.85 14.85 14.79 14.74 14.50
OF O	346.00 348.00 350.00 352.00 354.00 356.00 360.00 362.00 364.00 366.00 368.00 370.00 372.00 374.00 374.00 378.00 380.00 380.00	10.16 10.16 10.16 10.17 10.06 9.90 9.77 9.67 9.59 9.39 9.10 8.94 8.78 8.63 8.55 8.48 8.13 7.88 7.76 7.62 7.45	10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45 10.45	15.92 15.92 15.92 15.85 15.74 15.64 15.58 15.52 15.38 15.18 15.07 14.95 14.79 14.74
OF O	346.00 348.00 350.00 350.00 352.00 354.00 356.00 360.00 362.00 364.00 368.00 370.00 372.00 374.00 376.00 380.00 382.00 384.00 388.00 389.00	10.16 10.16 10.16 10.16 10.17 10.06 9.90 9.77 9.67 9.59 9.39 9.10 8.94 8.78 8.63 8.55 8.48 8.13 7.88 7.76 7.62 7.45 7.27	10.45 10.45	15.92 15.92 15.92 15.85 15.74 15.64 15.58 15.71 14.95 14.85 14.85 14.79 14.74 14.50 14.32 14.23 14.14 14.02
OF O	346.00 348.00 350.00 3552.00 354.00 356.00 358.00 360.00 362.00 364.00 368.00 370.00 372.00 374.00 378.00 388.00 388.00 388.00 388.00 388.00 3892.00	10.16 10.16 10.16 10.16 10.17 10.06 9.90 9.77 9.67 9.59 9.39 9.10 8.94 8.63 8.63 8.55 8.48 8.13 7.88 8.13 7.88 7.76 7.62 7.45 7.27 7.08	10.45 10.45	15.92 15.92 15.92 15.85 15.74 15.64 15.58 15.52 15.38 15.18 15.07 14.95 14.85 14.79 14.74 14.50 14.32 14.23 14.14 14.02
OF O	346.00 348.00 350.00 350.00 352.00 354.00 358.00 360.00 362.00 364.00 368.00 370.00 372.00 374.00 376.00 378.00 388.00 388.00 388.00 3892.00 394.00	10.16 10.16 10.16 10.16 10.17 10.06 9.90 9.77 9.67 9.59 9.39 9.10 8.94 8.78 8.63 8.55 8.48 8.13 7.88 7.76 7.62 7.62 7.08 6.88	10.45 10.45	15.92 15.92 15.92 15.85 15.74 15.64 15.58 15.52 15.38 15.18 16.07 14.85 14.79 14.74 14.50 14.32 14.23 14.14 14.02 13.89 13.76
OF O	346.00 348.00 350.00 3552.00 354.00 356.00 358.00 360.00 362.00 364.00 368.00 370.00 372.00 374.00 378.00 388.00 388.00 388.00 388.00 388.00 3892.00	10.16 10.16 10.16 10.16 10.17 10.06 9.90 9.77 9.67 9.59 9.39 9.10 8.94 8.63 8.63 8.55 8.48 8.13 7.88 8.13 7.88 7.76 7.62 7.45 7.27 7.08	10.45 10.45	15.92 15.92 15.92 15.85 15.74 15.64 15.58 15.52 15.38 15.18 15.07 14.95 14.85 14.79 14.74 14.50 14.32 14.23 14.14 14.02

IF I	398.00 400.00 402.00 404.00 408.00 410.00 413.40 416.70 419.90 423.20 426.50 429.80 433.10 436.40 439.60 442.90 446.20 449.50 456.00 459.30 462.00 464.00	6.55 6.39 6.23 6.07 5.87 5.72 5.56 5.29 4.96 4.47 4.28 4.21 4.01 3.60 3.21 3.01 2.63 2.13 1.56 1.02 0.98 0.87 0.49 0.21	10.4 10.4 10.4 10.4 10.4 10.4 10.4 10.4	5 5 1 1 5 5 5 1 1 5 5 5 5 5 5 5 5 5 5 5	3.39 3.28 3.16 3.06 2.91 2.81 2.70 2.51 2.45 2.29 1.96 1.84 1.83 1.71 1.44 1.20 1.10 0.86 0.23 0.35 0.28 0.029 9.83
IF IF PART3 I	466.00 466.30 LOCATION OF AF	0.01 0.01 REAS ABOVE 100	10.4 10.4 -YEAR	5 5 SURGE	9.68 9.68
STATION		TION OF SURGE YEAR SURGE		GES 100-YEAR	
220.00 308.00 344.00 366.00 416.70 419.90 423.20 426.50 429.80 433.10 439.60 442.90 446.20 449.50 452.80 455.80	PARTS				
Si	FATION OF GUTT 439.73 PART6 NUM		WIN	ON OF ZONE DWARD V ZONES	
STATION				IGNATION EL=15	FHF 120
6	51.93	15.50	V22	EL=16	120
21	18.00	15.82	V22	EL=16	120
22	20.00	15.81	V22	EL=16	120
30	06.00	15.90	V22	EL=16	120
30	08.00	15.91	V22	EL=16	120
34	12.00	15.91	V22	EL=16	120
34	14.00	15.92	V22	EL=16	120
36	54.00	15.52	V22	EL=16	120
	54.23	15.50	V22	EL=15	120
36	56.00	15.38	V22	EL=15	120
37	79.98	14.50	V22	EL=14	120
39	95.92	13.50	V22	EL=13	120
41	12.21	12.50	V22	EL=12	120
41	13.40	12.45	V22	EL=12	120
41	16.70	12.29	V22		120
41	19.90	11.96	V22	EL=12	120
42	23.20	11.84	V22	EL=12	120
	26.50	11.83	V22	EL=12	120
	29.80	11.71	V22	EL=12	120
	32.37	11.50	V22	EL=11	120
	33.10	11.44	V22	EL=11	120
	36.40	11.20	V22	EL=11	120
43	39.60	11.10	V22	EL=11	120

439.73	11.11			
		A19	EL=11	95
442.90	10.86	-10	11	0.5
446.20	10.54	A19	EL=11	95
440.20	10.54	A19	EL=11	95
446.94	10.50			
449.50	10.36	A19	EL=10	95
449.50	10.30	A19	EL=10	95
452.80	10.23			
456.00	10.25	A19	EL=10	95
456.00	10.35	A19	EL=10	95
459.30	10.28	1117	DD-10	,,,
		A19	EL=10	95
466.30	9.68			

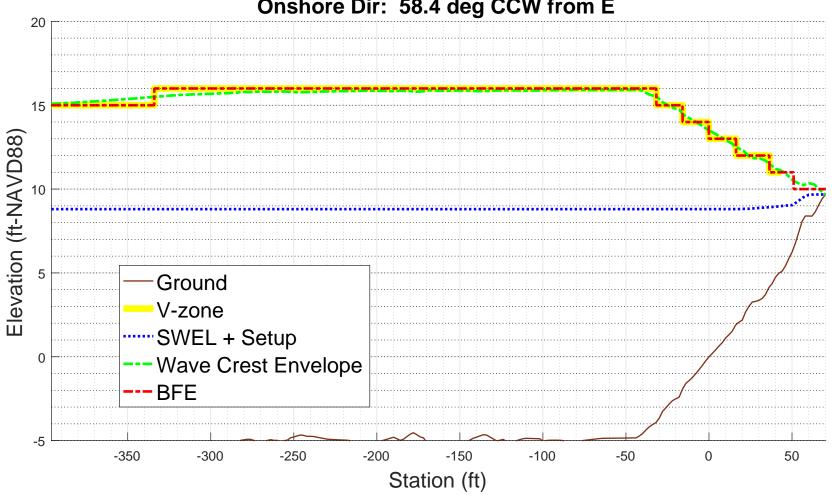
466.30 9.68

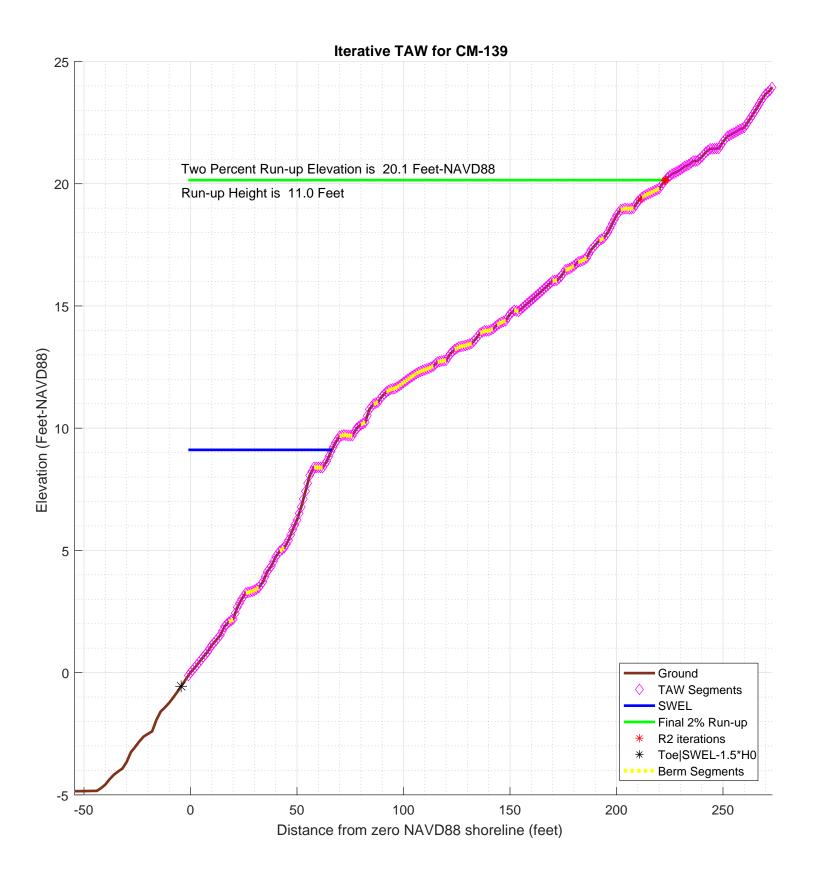
ZONE TERMINATED AT END OF TRANSECT
PART 7 POSTSCRIPT NOTES
PS# 1 START(419662.1474,4842368.952)
PS# 2 END(419770.6124,4842545.4995)

-1.000000e+00

**CM-139 100-year WHAFIS Output** Zero Station: -69.99675854, 43.73093497







```
% begin recording
diary on
% FEMA appeal for The Town of Harpswell, Cumberland county, Maine
% TRANSECT ID: CM-139
% TRANSECT ID. CM-13/9
% calculation by SJH, Ransom Consulting, Inc. 20-Feb-2020
% 100-year wave runup using TAW methodology
% including berm and weighted average with foreshore if necessary
% chk nld 20200220
% This script assumes that the incident wave conditions provided
% as input in the configuration section below are the
% appropriate values located at the end of the foreshore
% or toe of the slope on which the run-up is being calculated
% the script does not attempt to apply a depth limit or any other
\mbox{\ensuremath{\mbox{\$}}} transformation to the incident wave conditions other than
% conversion of the peak wave period to the spectral mean wave
\ensuremath{\text{\upshape 8}} as recommended in the references below
% references:
Van der Meer, J.W., 2002. Technical Report Wave Run-up and
% Wave Overtopping at Dikes. TAW Technical Advisory Committee on
% Flood Defence, The Netherlands.
% FEMA. 2007, Atlantic Ocean and Gulf of Mexico Coastal Guidelines Update
% CONFIG
fname='inpfiles/CM-139sta_ele_include.csv'; % file with station, elevation, include
                                             % third column is 0 for excluded points
imgname='logfiles/CM-139-runup';
SWEL=8.804; % 100-yr still water level including wave setup. H0=6.2267; % significant wave height at toe of structure
Tp=10.2103;
                 % peak period, 1/fma,
T0=Tp/1.1;
gamma_berm=0.7549; % this may get changed automatically below
gamma_rough=1;
gamma_beta=1;
gamma_perm=1;
setupAtToe=-0.023839;
maxSetup=0.87295;
                      % only used in case of berm/shallow foreshore weighted average
plotTitle='Iterative TAW for CM-139'
plotTitle =
Iterative TAW for CM-139
% END CONFIG
              ______
SWEL=SWEL+setupAtToe
SWEL =
                     8.780161
SWEL_fore=SWEL+maxSetup
SWEL fore =
                     9.653111
% FIND WAVELENGTH USING DEEPWATER DISPERSION RELATION
% using English units
L0=32.15/(2*pi)*T0^2
T<sub>1</sub>O =
            440.851927637668
% Find Hb (Munk, 1949)
%Hb=H0/(3.3*(H0/L0)^(1/3))
%Db=-Hb/.78+SWEL; % depth at breaking
% The toe elevation here is only used to determine the average
% structure slope, it is not used to depth limit the wave height.
% Any depth limiting or other modification of the wave height
```

```
% to make it consitent with TAW guidance should be performed
% prior to the input of the significant wave height given above.
Ztoe=SWEL-1.5*H0
Ztoe =
                 -0.559889
% read the transect
[sta,dep,inc] = textread(fname,'%n%n%n%*[^n]','delimiter',',','headerlines',0);
% remove unselected points
k=find(inc==0);
sta(k)=[];
dep(k)=[];
sta_org=sta; % used for plotting purposes
dep_org=dep;
% initial guess at maximum run-up elevation to estimate slope
Z2 =
                 18.120211
% determine station at the max runup and -1.5*H0 (i.e. the toe)
top_sta=-999;
toe_sta=-999;
for kk=1:length(sta)-1
    if ((Z2 > dep(kk)) & (Z2 <= dep(kk+1)))
                                                % here is the intersection of z2 with profile
       top_sta=interp1(dep(kk:kk+1),sta(kk:kk+1),Z2)
                                                    % here is the intersection of Ztoe with profile
    i f
       ((Ztoe > dep(kk)) & (Ztoe <= dep(kk+1)))
       toe_sta=interp1(dep(kk:kk+1),sta(kk:kk+1),Ztoe)
    end
end
toe_sta =
         -4.37839811542992
top_sta =
           196.59710472875
% check to make sure we got them, if not extend the end slopes outward
S=diff(dep)./diff(sta);
if toe_sta==-999
   dy=dep(1)-Ztoe;
   toe_sta=sta(1)-dy/S(1)
end
if top_sta==-999
   dy=Z2-dep(end);
   top_sta=sta(end)+dy/S(end)
% just so the reader can tell the values aren't -999 anymore
top sta
top sta =
           196.59710472875
toe_sta
toe sta =
         -4.37839811542992
% check for case where the toe of slope is below SWL-1.5*H0 \,
% in this case interpolate setup from the setupAtToe(really setup as first station), and the max setup
% also un-include points seaward of SWL-1.5*H0
if Ztoe > dep(1)
   dd=SWEL_fore-dep;
   k=find(dd<0,1); % k is index of first land point
   staAtSWL=interpl(dep(k-1:k),sta(k-1:k),SWEL_fore);
   dsta=staAtSWL-sta(1);
   dsetup=maxSetup-setupAtToe;
   dsetdsta=dsetup/dsta;
   setup=setupAtToe+dsetdsta*(toe_sta-sta(1));
   sprintf('-!!- Location of SWEL-1.5*HO is %4.1f ft landward of toe of slope', dsta)
   sprintf('-!!- Setup is interpolated between setup at toe of slope and max setup')
```

```
sprintf('-!!-
                              setup is adjusted to %4.2f feet', setup)
    SWEL=SWEL-setupAtToe+setup;
    sprintf('-!!-
                             SWEL is adjusted to %4.2f feet', SWEL)
    k=find(dep < SWEL-1.5*H0)
    sta(k)=[];
    dep(k) = [];
else
   sprintf('-!!- The User has selected a starting point that is %4.2f feet above the elevation of SWEL-1.5H0\n',dep(1 sprintf('-!!- This may be reasonable for some cases. However the user may want to consider:\n') sprintf('-!!- 1) Selecting a starting point that is at or below %4.2f feet elevation, or\n', Ztoe)
    sprintf('-!!-
                         2) Reducing the incident wave height to a depth limited condition. 
 \n')
end
ans =
-!!- Location of SWEL-1.5*H0 is 117.9 ft landward of toe of slope
-!!- Setup is interpolated between setup at toe of slope and max setup
ans =
-!!-
              setup is adjusted to 0.31 feet
ans =
              SWEL is adjusted to 9.11 feet
-!!-
k =
      1
       2
       3
      4
5
      6
7
8
9
     10
     11
     12
     13
     14
     15
     16
     17
     18
     19
     20
     21
     23
     25
     26
     27
     28
     29
```

```
R2=R2_new;
iter=\overline{0};
R2 all=[];
topStaAll=[];
Berm Segs=[];
TAW_ALWAYS_VALID=1;
while(abs(R2del) > tol && iter <= 25)</pre>
    iter=iter+1;
    sprintf ('!-----', starting iteration %d -----!',iter)
    % elevation of toe of slope
    Ztoe
    % station of toe slope (relative to 0-NAVD88 shoreline
    toe_sta
    % station of top of slope/extent of 2% run-up
    top sta
    % elevation of top of slope/extent of 2% run-up
    Z_2
    % incident significant wave height
    H0
    % incident spectral peak wave period
    Тp
    % incident spectral mean wave period
   Т0
   R2=R2_new
    Z2=R2+SWEL
    % determine slope for this iteration
    top_sta=-999;
    for kk=1:length(sta)-1
       if ((Z2 > dep(kk)) & (Z2 <= dep(kk+1)))
                                                % here is the intersection of z2 with profile
          top_sta=interp1(dep(kk:kk+1),sta(kk:kk+1),Z2)
          break;
       end
    end
    if top_sta==-999
       dy=Z2-dep(end);
       top_sta=sta(end)+dy/S(end)
    end
    % get the length of the slope (not accounting for berm)
   Lslope=top_sta-toe_sta
    % loop over profile segments to determine berm factor
    % re-calculate influence of depth of berm based on this run-up elevation
    % check for berm, berm width, berm height
   berm_width=0;
    rdh_sum=0;
    Berm_Segs=[];
    Berm_Heights=[];
    for kk=1:length(sta)-1
       ddep=dep(kk+1)-dep(kk);
       dsta=sta(kk+1)-sta(kk);
       s=ddep/dsta;
                          % count it as a berm if slope is flatter than 1:15 (see TAW manual)
       if (s < 1/15)
          sprintf ('Berm Factor Calculation: Iteration %d, Profile Segment: %d',iter,kk)
          berm_width=berm_width+dsta; % tally the width of all berm segments
          % compute the rdh for this segment and weight it by the segment length
          dh=SWEL-(dep(kk)+dep(kk+1))/2
          if dh < 0
              chi=R2;
          else
              chi=2* H0;
          end
          if (dh <= R2 \& dh >= -2*H0)
             rdh=(0.5-0.5*cos(3.14159*dh/chi));
          else
            rdh=1;
          end
          rdh_sum=rdh_sum + rdh * dsta
          Berm_Segs=[Berm_Segs, kk];
          Berm_Heights=[Berm_Heights, (dep(kk)+dep(kk+1))/2];
       end
       if dep(kk) >= Z2 % jump out of loop if we reached limit of run-up for this iteration
          break
       end
    end
    sprintf ('!----- End Berm Factor Calculation, Iter: %d -----!',iter)
    berm_width
    rB=berm_width/Lslope
    if (berm_width > 0)
       rdh_mean=rdh_sum/berm_width
    else
       rdh_mean=1
    end
    gamma_berm=1- rB * (1-rdh_mean)
    if gamma_berm > 1
       gamma_berm=1
    end
    if gamma_berm < 0.6
       gamma_berm = 0.6
```

```
end
% Iribarren number
slope=(Z2-Ztoe)/(Lslope-berm_width)
Irb=(slope/(sqrt(H0/L0)))
% runup height
gamma_berm
gamma_perm
gamma_beta
gamma_rough
gamma=gamma_berm*gamma_perm*gamma_beta*gamma_rough
% check validity
TAW_VALID=1;
if (Irb*gamma_berm < 0.5 | Irb*gamma_berm > 10 )
   sprintf('!!! - - Iribaren number: %6.2f is outside the valid range (0.5-10), TAW NOT VALID - - !!!\n', Irb*gam
   TAW_VALID=0;
   sprintf('!!! - - Iribaren number: %6.2f is in the valid range (0.5-10), TAW RECOMMENDED - - !!!\n', Irb*gamma_
end
islope=1/slope;
if (slope < 1/8 | slope > 1)
sprintf('!!! - - slope: 1
                  - slope: 1:%3.1f V:H is outside the valid range (1:8 - 1:1), TAW NOT VALID - - !!!\n', islope)
   TAW_VALID=0;
else
   sprintf('!!! - - slope: 1:%3.1f V:H is in the valid range (1:8 - 1:1), TAW RECOMMENDED - - !!!\n', islope)
end
if TAW_VALID == 0
   TAW_ALWAYS_VALID=0;
if (Irb*gamma_berm < 1.8)
   R2_new=gamma*H0*1.77*Irb
else
   R2_new=gamma*H0*(4.3-(1.6/sqrt(Irb)))
end
% check to see if we need to evaluate a shallow foreshore
if berm_width > 0.25 * L0;
   disp ('!
disp ('!
             Berm_width is greater than 1/4 wave length')
              Runup will be weighted average with foreshore calculation assuming depth limited wave height on ber
   % do the foreshore calculation
   fore_H0=0.78*(SWEL_fore-min(Berm_Heights))
   % get upper slope
   fore_toe_sta=-999;
   fore_toe_dep=-999;
   for kk=length(dep)-1:-1:1
      ddep=dep(kk+1)-dep(kk);
      dsta=sta(kk+1)-sta(kk);
      s=ddep/dsta;
      if s < 1/15
         break
      end
      fore_toe_sta=sta(kk);
      fore_toe_dep=dep(kk);
      upper_slope=(Z2-fore_toe_dep)/(top_sta-fore_toe_sta)
   end
   fore_Irb=upper_slope/(sqrt(fore_H0/L0));
   fore_gamma=gamma_perm*gamma_beta*gamma_rough;
   if (fore Irb < 1.8)
      fore_R2=fore_gamma*fore_H0*1.77*fore_Irb;
   else
      fore_R2=fore_gamma*fore_H0*(4.3-(1.6/sqrt(fore_Irb)));
   end
   if berm width >= L0
      R2 new=fore R2
      disp ('berm is wider than one wavelength, use full shallow foreshore solution');
   else
      w2=(berm_width-0.25*L0)/(0.75*L0)
      w1 = 1 - w2
      R2_new=w2*fore_R2 + w1*R2_new
   end
end % end berm width check
% convergence criterion
R2del=abs(R2-R2_new)
R2_all(iter)=R2_new;
% get the new top station (for plot purposes)
Z2=R2_new+SWEL
top_sta=-999;
for kk=1:length(sta)-1
   if ((Z2 > dep(kk)) & (Z2 <= dep(kk+1)))
                                               % here is the intersection of z2 with profile
      top_sta=interp1(dep(kk:kk+1),sta(kk:kk+1),Z2)
   end
end
if top_sta==-999
   dy=Z2-dep(end);
   top_sta=sta(end)+dy/S(end);
topStaAll(iter)=top_sta;
```

```
end
ans =
       -----! STARTING ITERATION 1 -----!
7toe =
                 -0.559889
toe_sta =
         -4.37839811542992
top_sta =
           196.59710472875
7.2 =
                 18.120211
H0 =
                    6.2267
Tp =
                   10.2103
T0 =
          9.28209090909091
R2 =
                   18.6801
Z2 =
          27.7920895455134
top_sta =
           313.97001027602
Lslope =
           318.34840839145
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 20
          7.01733954551342
rdh sum =
         0.599065845823981
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 21
dh =
          6.95683954551342
rdh_sum =
          1.19064063116286
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 28
dh =
          5.84106454551342
rdh_sum =
          1.6420749834842
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 29
dh =
          5.82241454551342
rdh_sum =
          2.09116860919536
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 30
dh =
          5.79601454551342
rdh_sum =
          2.53695075903407
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 31
dh =
          5.76186454551342
rdh_sum =
          2.97845290273617
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 32
dh =
          5.71803954551342
rdh_sum =
          3.41446888099168
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 33
dh =
          5.66453954551342
rdh_sum =
          3.84379821136296
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 44
dh =
          4.10266454551342
rdh_sum =
          4.08852215773557
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 45
          4.03861454551342
rdh_sum =
          4.32633313641215
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 60
         0.716464545513425
rdh_sum =
```

```
4.33447774023632
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 61
dh =
         0.718214545513424
rdh_sum =
          4.34266207081192
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 62
dh =
         0.719939545513425
rdh_sum =
          4.35088565442187
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 63
dh =
         0.721639545513424
rdh_sum =
          4.35914801329253
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 72
        -0.569610454486575
rdh_sum =
          4.36144048709367
Berm Factor Calculation: Iteration 1, Profile Segment: 73
        -0.597610454486576
rdh sum =
          4.36396368543612
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 74
dh =
        -0.605235454486575
rdh_sum =
          4.36655162630951
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 75
dh =
        -0.592485454486576
rdh_sum =
          4.36903176888756
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 76
dh =
        -0.584710454486576
rdh_sum =
           4.3714472984164
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 77
dh =
        -0.581910454486575
rdh_sum =
          4.37383976729215
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 82
dh =
         -1.05048545448658
rdh_sum =
          4.38162247682359
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 83
dh =
         -1.10383545448657
rdh_sum =
          4.39021343688658
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 88
dh =
         -1.89333545448658
rdh_sum =
          4.41534753029256
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 89
dh =
         -1.93178545448658
rdh_sum =
          4.44150375509001
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 94
         -2.39768545448658
rdh_sum =
           4.4816063336612
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 95
         -2.45383545448658
rdh_sum =
```

```
4.52358214779857
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 96
dh =
         -2.48993545448658
rdh_sum =
          4.56678388555495
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 97
dh =
         -2.50598545448658
rdh_sum =
          4.61053607670744
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 98
dh =
         -2.54166045448657
rdh_sum =
          4.65552368380569
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 99
         -2.59696045448658
rdh_sum =
          4.70245867193533
Berm Factor Calculation: Iteration 1, Profile Segment: 100
dh =
         -2.65703545448658
rdh sum =
          4.75155359566805
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 101
dh =
         -2.72188545448658
rdh_sum =
          4.80303178825642
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 102
dh =
        -2.78673545448658
rdh_sum =
           4.8569466003655
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 103
dh =
         -2.85158545448658
rdh_sum =
           4.9133510928299
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 104
dh =
         -2.91396045448658
rdh_sum =
          4.97220003309272
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 105
dh =
         -2.97386045448658
rdh_sum =
          5.03344212435562
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 106
dh =
         -3.03341045448658
rdh_sum =
          5.09710752043771
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 107
dh =
         -3.09261045448658
rdh_sum =
          5.16322535829537
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 108
dh =
         -3.14551045448658
rdh_sum =
           5.2315710456004
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 109
         -3.19211045448658
rdh_sum =
          5.30190757209896
Berm Factor Calculation: Iteration 1, Profile Segment: 110
         -3.23113545448658
rdh_sum =
```

```
5.37393162870342
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 111
dh =
         -3.26258545448658
rdh_sum =
          5.44732907336501
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 112
dh =
         -3.29383545448658
rdh_sum =
          5.52210299327982
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 113
dh =
         -3.32488545448658
rdh_sum =
          5.59825621175062
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 114
         -3.36333545448658
rdh_sum =
          5.67613346400767
Berm Factor Calculation: Iteration 1, Profile Segment: 115
dh =
         -3.40918545448658
rdh sum =
          5.75608962116676
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 118
dh =
         -3.60403545448658
rdh_sum =
          5.84515763480688
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 119
dh =
        -3.62728545448658
rdh_sum =
          5.93534256115743
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 120
dh =
         -3.64426045448658
rdh_sum =
          6.02634691220303
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 121
dh =
         -3.65496045448658
rdh_sum =
          6.11786949157243
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 126
dh =
         -4.12838545448658
rdh_sum =
          6.23362033016775
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 127
dh =
         -4.18293545448658
rdh_sum =
         6.35232234057193
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 128
dh =
         -4.21903545448658
rdh_sum =
          6.47299503364288
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 129
dh =
         -4.23668545448658
rdh_sum =
          6.59463632591779
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 130
         -4.25831045448658
rdh_sum =
           6.7174689016373
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 131
         -4.28391045448658
rdh_sum =
```

```
6.84171818381369
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 132
dh =
         -4.31266045448658
rdh_sum =
           6.9675667956922
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 133
dh =
         -4.34456045448658
rdh_sum =
          7.09520020371398
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 138
dh =
         -4.79738545448658
rdh_sum =
          7.24929995385892
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 139
         -4.84253545448658
rdh_sum =
          7.40615115174649
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 140
dh =
         -4.86608545448658
rdh sum =
          7.56444535148319
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 141
dh =
         -4.86803545448658
rdh_sum =
          7.72285927605111
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 142
dh =
        -4.89063545448658
rdh_sum =
           7.8826634576163
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 143
dh =
         -4.93388545448658
rdh_sum =
          8.04514188216504
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 146
dh =
         -5.13698545448658
rdh_sum =
          8.22041489208975
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 147
dh =
         -5.19413545448658
rdh_sum =
          8.39935710230119
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 148
dh =
         -5.23781045448658
rdh_sum =
          8.58112338933707
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 149
dh =
         -5.26801045448657
rdh_sum =
          8.76485249365481
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 154
dh =
         -5.69873545448658
rdh_sum =
          8.97743932112012
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 155
         -5.67618545448657
rdh_sum =
         9.18847659558763
Berm Factor Calculation: Iteration 1, Profile Segment: 172
         -6.91756045448658
rdh_sum =
```

```
9.49035943034023
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 173
dh =
         -6.93326045448658
rdh_sum =
          9.79345509581798
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 178
dh =
         -7.37643545448658
rdh_sum =
          10.1313205579696
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 179
dh =
         -7.40228545448657
rdh_sum =
          10.4712437956307
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 180
         -7.44433545448658
rdh_sum =
           10.814520847403
Berm Factor Calculation: Iteration 1, Profile Segment: 181
         -7.50258545448658
rdh sum =
            11.16245670252
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 184
dh =
         -7.70038545448658
rdh_sum =
           11.526318732635
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 185
dh =
         -7.72573545448657
rdh_sum =
          11.8922331195691
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 186
dh =
        -7.76693545448658
rdh_sum =
          12.2614882749465
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 187
dh =
         -7.82398545448658
rdh_sum =
          12.6353797514282
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 194
dh =
         -8.59431045448657
rdh_sum =
          13.0728347048123
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 195
dh =
         -8.64211045448658
rdh_sum =
         13.5142795294783
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 204
dh =
         -9.83591045448658
rdh_sum =
          14.0559270739797
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 205
dh =
         -9.86051045448658
rdh_sum =
          14.5996356624158
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 206
         -9.86938545448658
rdh_sum =
         15.1440876367368
Berm Factor Calculation: Iteration 1, Profile Segment: 207
         -9.86253545448658
rdh_sum =
```

```
15.6879658514312
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 208
dh =
         -9.86646045448658
rdh_sum =
          16.2321728333765
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 209
dh =
         -9.88116045448658
rdh_sum =
          16.7776109496387
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 214
dh =
         -10.3572104544866
rdh_sum =
          17.3627259773918
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 215
         -10.4098104544866
rdh_sum =
          17.9521961529196
Berm Factor Calculation: Iteration 1, Profile Segment: 216
dh =
         -10.4557854544866
rdh sum =
          18.5454672203581
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 217
dh =
         -10.4951354544866
rdh_sum =
          19.1419870509342
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 218
dh =
         -10.5365604544866
rdh_sum =
          19.7419223880212
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 219
dh =
         -10.5800604544866
rdh_sum =
          20.3454390921685
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 220
dh =
         -10.6233604544866
rdh_sum =
           20.952515195534
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 221
dh =
         -10.6664604544866
rdh_sum =
          21.5631286188907
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 228
dh =
         -11.2982604544866
rdh_sum =
          22.2248319635042
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 229
dh =
         -11.3397604544866
rdh_sum =
          22.8898335090317
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 230
dh =
         -11.3860854544866
rdh_sum =
          23.5585072200711
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 231
         -11.4372354544866
rdh_sum =
          24.2312236705167
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 232
         -11.4944104544866
```

```
24.9084439162284
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 233
dh =
         -11.5576104544866
rdh_sum =
          25.5906234755512
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 234
dh =
         -11.6099604544866
rdh_sum =
          26.2768953870441
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 235
dh =
         -11.6514604544866
rdh_sum =
          26.9664012303305
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 238
         -11.8127354544866
rdh_sum =
          27.6683855252169
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 239
dh =
         -11.8211854544866
rdh sum =
           28.371019611339
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 244
dh =
         -12.2150604544866
rdh_sum =
          29.1034659701403
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 245
dh =
         -12.2813604544866
rdh_sum =
          29.8408338001472
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 246
dh =
         -12.3164354544866
rdh_sum =
          30.5807933619185
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 247
dh =
         -12.3202854544866
rdh_sum =
          31.3210368976555
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 248
dh =
         -12.3250104544866
rdh_sum =
          32.0616288092266
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 249
dh =
         -12.3306104544866
rdh_sum =
          32.8026334139279
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 254
dh =
         -12.8425354544866
rdh_sum =
          33.8026334139279
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 255
dh =
         -12.8881854544866
rdh_sum =
          34.8026334139279
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 256
dh =
         -12.9345104544866
rdh_sum =
          35.8026334139279
Berm Factor Calculation: Iteration 1, Profile Segment: 257
         -12.9815104544866
```

```
36.8026334139279
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 258
dh =
         -13.0322354544866
rdh_sum =
          37.8026334139279
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 259
dh =
         -13.0866854544866
rdh_sum =
          38.8026334139279
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 260
dh =
         -13.1325604544866
rdh_sum =
          39.8026334139279
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 261
         -13.1698604544866
rdh_sum =
          40.8026334139279
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 278
         -15.1985854544866
rdh sum =
          41.8026334139279
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 279
dh =
         -15.2425354544866
rdh_sum =
          42.8026334139279
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 284
dh =
         -15.8273854544866
rdh_sum =
          43.8026334139279
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 285
dh =
         -15.8577354544866
rdh_sum =
          44.8026334139279
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 290
dh =
         -16.3686354544866
rdh_sum =
          45.8026334139279
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 291
dh =
         -16.3826854544866
rdh_sum =
          46.8026334139279
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 292
dh =
         -16.3988104544866
rdh_sum =
          47.8026334139279
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 293
dh =
         -16.4170104544866
rdh_sum =
          48.8026334139279
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 294
dh =
         -16.4539854544866
rdh_sum =
          49.8026334139279
ans =
Berm Factor Calculation: Iteration 1, Profile Segment: 295
dh =
         -16.5097354544866
rdh_sum =
         50.8026334139279
 ----- End Berm Factor Calculation, Iter: 1 -----!
berm_width =
  130
rB =
```

```
0.408357625083988
rdh_mean =
         0.390789487799445
gamma_berm =
         0.751224242061582
slope =
         0.150529429941286
Irb =
          1.26659805841667
gamma_berm = 0.751224242061582
gamma_perm =
gamma_beta =
gamma_rough =
gamma =
         0.751224242061582
!!! - - Iribaren number: 0.95 is in the valid range (0.5-10), TAW RECOMMENDED - - !!!
!!! - - slope: 1:6.6 V:H is in the valid range (1:8 - 1:1), TAW RECOMMENDED - - !!!
R2\_new =
          10.4867187515172
    Berm_width is greater than 1/4 wave length
    Runup will be weighted average with foreshore calculation assuming depth limited wave height on berm
fore_H0 =
                5.89559958
upper_slope =
        0.0760215167036978
upper_slope =
        0.0759137707687769
upper_slope =
         0.075804847475598
upper_slope =
        0.0756947274203544
upper_slope =
        0.0755833907704967
upper_slope =
        0.0754708172528257
upper_slope =
        0.0754223383205499
upper_slope =
        0.0753733147729274
upper_slope =
        0.0753539582490276
upper_slope =
         0.075334381802103
w2 =
        0.0598447894485056
w1 =
         0.940155210551494
R2\_new =
           10.265964123278
R2del =
          8.41413587672201
Z2 =
          19.3779536687914
top_sta =
          211.236374706542
ans =
          ----- STARTING ITERATION 2 -----!
Ztoe =
                 -0.559889
toe_sta =
         -4.37839811542992
top_sta =
          211.236374706542
Z2 =
          19.3779536687914
H0 =
                    6.2267
Tp =
                   10.2103
T0 =
          9.28209090909091
R2 =
           10.265964123278
7.2 =
          19.3779536687914
top_sta =
          211.236374706542
Lslope =
          215.614772821972
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 20
          7.01733954551342
rdh_sum =
```

```
0.599065845823981
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 21
dh =
          6.95683954551342
rdh_sum =
          1.19064063116286
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 28
dh =
          5.84106454551342
rdh_sum =
           1.6420749834842
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 29
dh =
          5.82241454551342
rdh_sum =
          2.09116860919536
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 30
          5.79601454551342
rdh_sum =
          2.53695075903407
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 31
dh =
          5.76186454551342
rdh sum =
          2.97845290273617
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 32
dh =
          5.71803954551342
rdh_sum =
          3.41446888099168
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 33
dh =
          5.66453954551342
rdh_sum =
          3.84379821136296
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 44
dh =
          4.10266454551342
rdh_sum =
          4.08852215773557
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 45
dh =
          4.03861454551342
rdh_sum =
          4.32633313641215
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 60
dh =
         0.716464545513425
rdh_sum =
          4.33447774023632
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 61
dh =
         0.718214545513424
rdh_sum =
          4.34266207081192
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 62
dh =
         0.719939545513425
rdh_sum =
          4.35088565442187
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 63
dh =
         0.721639545513424
rdh_sum =
          4.35914801329253
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 72
dh =
        -0.569610454486575
rdh_sum =
          4.36672498212041
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 73
        -0.597610454486576
rdh_sum =
```

```
4.37506304456257
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 74
dh =
        -0.605235454486575
rdh_sum =
          4.38361462508888
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 75
dh =
        -0.592485454486576
rdh_sum =
          4.39181067962445
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 76
dh =
        -0.584710454486576
rdh_sum =
          4.39979360756762
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 77
        -0.581910454486575
rdh_sum =
          4.40770046462582
Berm Factor Calculation: Iteration 2, Profile Segment: 82
         -1.05048545448658
rdh sum =
          4.43331439950748
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 83
dh =
        -1.10383545448657
rdh_sum =
          4.46157065763506
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 88
dh =
        -1.89333545448658
rdh_sum =
          4.54317457725032
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 89
dh =
         -1.93178545448658
rdh_sum =
          4.62802857774397
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 94
dh =
         -2.39768545448658
rdh_sum =
          4.75669089949592
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 95
dh =
         -2.45383545448658
rdh_sum =
          4.89116107578002
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 96
dh =
         -2.48993545448658
rdh_sum =
          5.02942234879217
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 97
dh =
         -2.50598545448658
rdh_sum =
          5.16938334197964
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 98
dh =
         -2.54166045448657
rdh_sum =
          5.31315342220386
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 99
         -2.59696045448658
rdh_sum =
          5.46291173718541
Berm Factor Calculation: Iteration 2, Profile Segment: 100
         -2.65703545448658
rdh_sum =
```

```
5.61928896405186
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 101
dh =
         -2.72188545448658
rdh_sum =
           5.7829414790897
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 102
dh =
         -2.78673545448658
rdh_sum =
          5.95400174494285
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 103
dh =
         -2.85158545448658
rdh_sum =
          6.13259930688464
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 104
         -2.91396045448658
rdh_sum =
           6.3185659629714
Berm Factor Calculation: Iteration 2, Profile Segment: 105
         -2.97386045448658
rdh sum =
          6.51171704134807
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 106
dh =
         -3.03341045448658
rdh_sum =
          6.71211276739417
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 107
dh =
        -3.09261045448658
rdh_sum =
          6.91980918509293
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 108
dh =
         -3.14551045448658
rdh_sum =
          7.13411059738993
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 109
dh =
         -3.19211045448658
rdh_sum =
          7.35429248199598
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 110
dh =
         -3.23113545448658
rdh_sum =
          7.57944277746044
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 111
dh =
         -3.26258545448658
rdh_sum =
         7.80862564159852
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 112
dh =
         -3.29383545448658
rdh_sum =
          8.04184027707684
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 113
dh =
         -3.32488545448658
rdh_sum =
          8.27908504584482
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 114
         -3.36333545448658
rdh_sum =
          8.52135326780243
Berm Factor Calculation: Iteration 2, Profile Segment: 115
         -3.40918545448658
rdh_sum =
```

```
8.769658331117
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 118
dh =
         -3.60403545448658
rdh_sum =
          9.04415651201236
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 119
dh =
         -3.62728545448658
rdh_sum =
          9.32183550529751
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 120
dh =
         -3.64426045448658
rdh_sum =
          9.60184395092967
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 121
         -3.65496045448658
rdh_sum =
          9.88332379491445
Berm Factor Calculation: Iteration 2, Profile Segment: 126
         -4.12838545448658
rdh sum =
          10.2320197060058
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 127
dh =
         -4.18293545448658
rdh_sum =
          10.5886916892261
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 128
dh =
        -4.21903545448658
rdh_sum =
         10.9506641629155
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 129
dh =
         -4.23668545448658
rdh_sum =
          11.3152343221553
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 130
dh =
         -4.25831045448658
rdh_sum =
          11.6829925762071
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 131
dh =
         -4.28391045448658
rdh_sum =
          12.0545324197132
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 132
dh =
         -4.31266045448658
rdh_sum =
         12.4303285528878
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 133
dh =
         -4.34456045448658
rdh_sum =
          12.8108585547613
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 138
dh =
         -4.79738545448658
rdh_sum =
          13.2595984812618
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 139
         -4.84253545448658
rdh_sum =
         13.7152150818047
Berm Factor Calculation: Iteration 2, Profile Segment: 140
         -4.86608545448658
```

```
14.1744219643721
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 141
dh =
         -4.86803545448658
rdh_sum =
          14.6339262289742
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 142
dh =
         -4.89063545448658
rdh_sum =
          15.0968780998871
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 143
dh =
         -4.93388545448658
rdh_sum =
          15.5664325134237
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 146
         -5.13698545448658
rdh_sum =
          16.0670444089466
Berm Factor Calculation: Iteration 2, Profile Segment: 147
dh =
         -5.19413545448658
rdh sum =
          16.5764002791265
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 148
dh =
         -5.23781045448658
rdh_sum =
          17.0924366557703
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 149
dh =
         -5.26801045448657
rdh_sum =
          17.6130908060481
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 154
dh =
         -5.69873545448658
rdh_sum =
          18.1992242539089
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 155
dh =
         -5.67618545448657
rdh_sum =
          18.7819568848075
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 172
dh =
         -6.91756045448658
rdh_sum =
           19.541642627791
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 173
         -6.93326045448658
rdh_sum =
          20.3033782107369
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 178
dh =
         -7.37643545448658
rdh_sum =
          21.1203107234644
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 179
dh =
         -7.40228545448657
rdh_sum =
          21.9402924958984
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 180
         -7.44433545448658
rdh_sum =
          22.7651916126735
Berm Factor Calculation: Iteration 2, Profile Segment: 181
         -7.50258545448658
```

```
23.5968134563169
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 184
dh =
         -7.70038545448658
rdh_sum =
          24.4504648421444
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 185
dh =
         -7.72573545448657
rdh_sum =
          25.3068475266138
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 186
dh =
         -7.76693545448658
rdh_sum =
          26.1676234181942
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 187
         -7.82398545448658
rdh_sum =
          27.0343877890093
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 194
         -8.59431045448657
rdh sum =
          27.9703782310523
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 195
dh =
         -8.64211045448658
rdh_sum =
          28.9099023364405
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 204
dh =
         -9.83591045448658
rdh_sum =
           29.905578438641
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 205
dh =
         -9.86051045448658
rdh_sum =
          30.9017344391704
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 206
dh =
         -9.86938545448658
rdh_sum =
          31.8980566731293
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 207
dh =
         -9.86253545448658
rdh_sum =
          32.8942509252786
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 208
dh =
         -9.86646045448658
rdh_sum =
          33.890518776846
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 209
dh =
         -9.88116045448658
rdh_sum =
          34.8870559117084
ans =
Berm Factor Calculation: Iteration 2, Profile Segment: 214
dh =
         -10.3572104544866
rdh_sum =
          35.8868610351513
ans =
!---- End Berm Factor Calculation, Iter: 2 -----!
berm_width =
    89
rB =
         0.412773201182672
rdh_mean =
         0.403223157698329
gamma_berm =
         0.753666512411453
```

slope =

```
0.157468534077182
Irb =
         1.32498568287725
gamma_berm =
         0.753666512411453
gamma_perm =
gamma beta =
gamma_rough =
gamma =
         0.753666512411453
ans =
!!! - - Iribaren number: 1.00 is in the valid range (0.5-10), TAW RECOMMENDED - - !!!
ans =
!!! - - slope: 1:6.4 V:H is in the valid range (1:8 - 1:1), TAW RECOMMENDED - - !!!
R2\_new =
          11.0057999055228
R2del =
         0.739835782244787
Z2 =
          20.1177894510362
top_sta =
          222.698821613257
ans =
      -----! STARTING ITERATION 3 -----!
Ztoe =
                 -0.559889
toe_sta =
         -4.37839811542992
top_sta =
          222.698821613257
Z2 =
          20.1177894510362
H0 =
                    6.2267
Tp =
                   10.2103
T0 =
          9.28209090909091
R2 =
          11.0057999055228
Z_{2} =
          20.1177894510362
top_sta =
          222.698821613257
Lslope =
          227.077219728687
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 20
dh =
          7.01733954551342
rdh_sum =
         0.599065845823981
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 21
dh =
          6.95683954551342
rdh_sum =
          1.19064063116286
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 28
dh =
          5.84106454551342
rdh_sum =
          1.6420749834842
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 29
dh =
          5.82241454551342
rdh_sum =
          2.09116860919536
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 30
dh =
          5.79601454551342
rdh_sum =
          2.53695075903407
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 31
          5.76186454551342
rdh_sum =
          2.97845290273617
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 32
          5.71803954551342
rdh_sum =
```

```
3.41446888099168
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 33
dh =
          5.66453954551342
rdh_sum =
          3.84379821136296
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 44
dh =
          4.10266454551342
rdh_sum =
          4.08852215773557
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 45
dh =
          4.03861454551342
rdh_sum =
          4.32633313641215
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 60
         0.716464545513425
rdh_sum =
          4.33447774023632
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 61
dh =
         0.718214545513424
rdh sum =
          4.34266207081192
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 62
dh =
         0.719939545513425
rdh_sum =
          4.35088565442187
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 63
dh =
         0.721639545513424
rdh_sum =
          4.35914801329253
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 72
dh =
        -0.569610454486575
rdh_sum =
          4.36574270809429
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 73
dh =
        -0.597610454486576
rdh_sum =
          4.37300006948653
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 74
dh =
        -0.605235454486575
rdh_sum =
          4.38044334405394
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 75
dh =
        -0.592485454486576
rdh_sum =
          4.38757705910298
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 76
dh =
        -0.584710454486576
rdh_sum =
          4.39452520762113
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 77
dh =
        -0.581910454486575
rdh_sum =
          4.40140712305405
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 82
         -1.05048545448658
rdh_sum =
          4.42371813555522
Berm Factor Calculation: Iteration 3, Profile Segment: 83
         -1.10383545448657
rdh_sum =
```

```
4.44833362132377
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 88
dh =
         -1.89333545448658
rdh_sum =
          4.51959498529184
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 89
dh =
         -1.93178545448658
rdh_sum =
          4.59370568232418
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 94
dh =
         -2.39768545448658
rdh_sum =
          4.70631145841565
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 95
         -2.45383545448658
rdh_sum =
          4.82403337241888
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 96
dh =
         -2.48993545448658
rdh sum =
          4.94509650571875
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 97
dh =
         -2.50598545448658
rdh_sum =
          5.06765808246897
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 98
dh =
         -2.54166045448657
rdh_sum =
          5.19357864037501
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 99
dh =
         -2.59696045448658
rdh_sum =
          5.32478251596152
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 100
dh =
         -2.65703545448658
rdh_sum =
          5.46183000323624
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 101
dh =
         -2.72188545448658
rdh_sum =
          5.60530531491284
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 102
dh =
         -2.78673545448658
rdh_sum =
          5.75533061772272
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 103
dh =
         -2.85158545448658
rdh_sum =
          5.91202583397765
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 104
dh =
         -2.91396045448658
rdh_sum =
           6.0752474223091
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 105
         -2.97386045448658
rdh_sum =
          6.24483693657685
Berm Factor Calculation: Iteration 3, Profile Segment: 106
         -3.03341045448658
rdh_sum =
```

```
6.42085292176391
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 107
dh =
         -3.09261045448658
rdh_sum =
          6.60335039900445
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 108
dh =
         -3.14551045448658
rdh_sum =
           6.7917163760749
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 109
dh =
         -3.19211045448658
rdh_sum =
          6.98531086923436
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 110
         -3.23113545448658
rdh_sum =
          7.18332571482023
Berm Factor Calculation: Iteration 3, Profile Segment: 111
dh =
         -3.26258545448658
rdh sum =
          7.38493018895868
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 112
dh =
         -3.29383545448658
rdh_sum =
          7.59012528423923
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 113
dh =
         -3.32488545448658
rdh_sum =
         7.79891125439882
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 114
dh =
        -3.36333545448658
rdh_sum =
          8.01217556865805
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 115
dh =
         -3.40918545448658
rdh_sum =
          8.23082522475304
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 118
dh =
         -3.60403545448658
rdh_sum =
          8.47288739509683
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 119
dh =
         -3.62728545448658
rdh_sum =
           8.7177979255399
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 120
dh =
         -3.64426045448658
rdh_sum =
          8.96479516842474
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 121
dh =
         -3.65496045448658
rdh_sum =
          9.21311080235554
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 126
         -4.12838545448658
rdh_sum =
         9.52192825311554
Berm Factor Calculation: Iteration 3, Profile Segment: 127
         -4.18293545448658
rdh_sum =
```

```
9.83796258198087
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 128
dh =
         -4.21903545448658
rdh_sum =
          10.1587975183832
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 129
dh =
         -4.23668545448658
rdh_sum =
          10.4819865225741
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 130
dh =
         -4.25831045448658
rdh_sum =
          10.8080658717953
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 131
         -4.28391045448658
rdh_sum =
          11.1375754123495
Berm Factor Calculation: Iteration 3, Profile Segment: 132
         -4.31266045448658
rdh sum =
          11.4709480628741
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 133
dh =
         -4.34456045448658
rdh_sum =
          11.8086202085289
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 138
dh =
        -4.79738545448658
rdh_sum =
          12.2086047666992
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 139
dh =
         -4.84253545448658
rdh_sum =
          12.6149112221677
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 140
dh =
         -4.86608545448658
rdh_sum =
          13.0245213877872
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 141
dh =
         -4.86803545448658
rdh_sum =
          13.4344052941846
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 142
dh =
         -4.89063545448658
rdh_sum =
         13.8474638011439
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 143
dh =
         -4.93388545448658
rdh_sum =
          14.2666075699897
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 146
dh =
         -5.13698545448658
rdh_sum =
            14.71447693083
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 147
         -5.19413545448658
rdh_sum =
         15.1704651072159
Berm Factor Calculation: Iteration 3, Profile Segment: 148
         -5.23781045448658
rdh_sum =
```

```
15.6326658304612
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 149
dh =
         -5.26801045448657
rdh_sum =
          16.0991658440298
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 154
dh =
         -5.69873545448658
rdh_sum =
          16.6271011101238
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 155
dh =
         -5.67618545448657
rdh_sum =
          17.1518224140215
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 172
         -6.91756045448658
rdh_sum =
          17.8482854833836
Berm Factor Calculation: Iteration 3, Profile Segment: 173
dh =
         -6.93326045448658
rdh sum =
          18.5468071191688
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 178
dh =
         -7.37643545448658
rdh_sum =
          19.3016401999774
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 179
dh =
         -7.40228545448657
rdh_sum =
          20.0596405916311
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 180
dh =
        -7.44433545448658
rdh_sum =
          20.8227631363251
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 181
dh =
         -7.50258545448658
rdh_sum =
          21.5929183878569
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 184
dh =
         -7.70038545448658
rdh_sum =
          22.3863858216431
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 185
dh =
         -7.72573545448657
rdh_sum =
          23.1827748523011
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 186
dh =
         -7.76693545448658
rdh_sum =
          23.9838790226263
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 187
dh =
         -7.82398545448658
rdh_sum =
           24.791443392604
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 194
         -8.59431045448657
rdh_sum =
          25.6775881902255
Berm Factor Calculation: Iteration 3, Profile Segment: 195
         -8.64211045448658
rdh_sum =
```

```
26.5680308662617
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 204
dh =
         -9.83591045448658
rdh_sum =
          27.5404090297858
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 205
dh =
         -9.86051045448658
rdh_sum =
          28.5139263562617
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 206
dh =
         -9.86938545448658
rdh_sum =
          29.4878489329007
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 207
         -9.86253545448658
rdh_sum =
          30.4614589925952
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 208
dh =
         -9.86646045448658
rdh sum =
          31.4352483438142
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 209
dh =
         -9.88116045448658
rdh_sum =
          32.4097038951878
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 214
dh =
         -10.3572104544866
rdh_sum =
          33.4011589927084
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 215
dh =
         -10.4098104544866
rdh_sum =
          34.3939406292343
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 216
dh =
         -10.4557854544866
rdh_sum =
          35.3877907529978
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 217
dh =
         -10.4951354544866
rdh_sum =
           36.382487849933
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 218
         -10.5365604544866
rdh_sum =
          37.3780091433394
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 219
dh =
         -10.5800604544866
rdh_sum =
          38.3743213382053
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 220
dh =
         -10.6233604544866
rdh_sum =
          39.3713448037664
ans =
Berm Factor Calculation: Iteration 3, Profile Segment: 221
dh =
         -10.6664604544866
rdh_sum =
         40.3690008519398
!----- End Berm Factor Calculation, Iter: 3 -----!
berm_width =
    96
rB =
```

```
0.422763675346656
rdh_mean =
         0.42051042554104
gamma_berm =
          0.75501285767666
slope =
         0.157751884681689
Irb =
         1.32736987662368
gamma_berm =
          0.75501285767666
gamma_perm =
gamma_beta =
gamma_rough =
gamma =
          0.75501285767666
!!! - - Iribaren number: 1.00 is in the valid range (0.5-10), TAW RECOMMENDED - - !!!
!!! - - slope: 1:6.3 V:H is in the valid range (1:8 - 1:1), TAW RECOMMENDED - - !!!
R2\_new =
         11.0452999339406
R2del =
        0.0395000284178515
Z2 =
         20.1572894794541
top_sta =
          223.084941148133
ans =
!----- STARTING ITERATION 4 -----!
Ztoe =
                 -0.559889
toe_sta =
         -4.37839811542992
top_sta =
         223.084941148133
72 =
          20.1572894794541
H0 =
                    6.2267
Tp =
                   10.2103
T0 =
         9.28209090909091
R2 =
          11.0452999339406
Z_{2} =
          20.1572894794541
top_sta =
          223.084941148133
Lslope =
          227.463339263563
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 20
dh =
          7.01733954551342
rdh_sum =
         0.599065845823981
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 21
dh =
         6.95683954551342
rdh_sum =
         1.19064063116286
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 28
dh =
          5.84106454551342
rdh_sum =
           1.6420749834842
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 29
dh =
          5.82241454551342
rdh_sum =
          2.09116860919536
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 30
          5.79601454551342
rdh_sum =
         2.53695075903407
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 31
          5.76186454551342
rdh_sum =
```

```
2.97845290273617
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 32
dh =
          5.71803954551342
rdh_sum =
          3.41446888099168
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 33
dh =
          5.66453954551342
rdh_sum =
          3.84379821136296
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 44
dh =
          4.10266454551342
rdh_sum =
          4.08852215773557
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 45
          4.03861454551342
rdh_sum =
          4.32633313641215
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 60
dh =
         0.716464545513425
rdh sum =
          4.33447774023632
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 61
dh =
         0.718214545513424
rdh_sum =
          4.34266207081192
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 62
dh =
         0.719939545513425
rdh_sum =
          4.35088565442187
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 63
dh =
         0.721639545513424
rdh_sum =
          4.35914801329253
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 72
dh =
        -0.569610454486575
rdh_sum =
          4.36569572778009
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 73
dh =
        -0.597610454486576
rdh_sum =
          4.37290139947767
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 74
dh =
        -0.605235454486575
rdh_sum =
          4.38029166349505
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 75
dh =
        -0.592485454486576
rdh_sum =
          4.38737456740953
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 76
dh =
        -0.584710454486576
rdh_sum =
          4.39427322345938
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 77
dh =
        -0.581910454486575
rdh_sum =
          4.40110611712692
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 82
         -1.05048545448658
rdh_sum =
```

```
4.42325902522953
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 83
dh =
         -1.10383545448657
rdh_sum =
          4.44770021282661
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 88
dh =
         -1.89333545448658
rdh_sum =
           4.5184651572114
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 89
dh =
         -1.93178545448658
rdh_sum =
          4.59206011566953
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 94
         -2.39768545448658
rdh_sum =
          4.70389334217407
Berm Factor Calculation: Iteration 4, Profile Segment: 95
dh =
         -2.45383545448658
rdh sum =
           4.8208091755344
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 96
dh =
         -2.48993545448658
rdh_sum =
          4.94104440753902
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 97
dh =
        -2.50598545448658
rdh_sum =
          5.06276831705426
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 98
dh =
         -2.54166045448657
rdh_sum =
          5.18782936113373
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 99
dh =
         -2.59696045448658
rdh_sum =
          5.31813948762408
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 100
dh =
         -2.65703545448658
rdh_sum =
          5.45425554208633
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 101
dh =
         -2.72188545448658
rdh_sum =
          5.59675819266703
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 102
dh =
         -2.78673545448658
rdh_sum =
          5.74576906481571
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 103
dh =
         -2.85158545448658
rdh_sum =
          5.90140756979662
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 104
         -2.91396045448658
rdh_sum =
          6.06353132631094
Berm Factor Calculation: Iteration 4, Profile Segment: 105
         -2.97386045448658
rdh_sum =
```

```
6.23198312730808
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 106
dh =
         -3.03341045448658
rdh_sum =
          6.40682139450134
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 107
dh =
         -3.09261045448658
rdh_sum =
          6.58810105653411
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 108
dh =
         -3.14551045448658
rdh_sum =
          6.77521313202248
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 109
         -3.19211045448658
rdh_sum =
          6.96752174915066
Berm Factor Calculation: Iteration 4, Profile Segment: 110
dh =
         -3.23113545448658
rdh sum =
          7.16422381730647
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 111
dh =
         -3.26258545448658
rdh_sum =
          7.36449375701655
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 112
dh =
         -3.29383545448658
rdh_sum =
         7.56833263493058
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 113
dh =
         -3.32488545448658
rdh_sum =
          7.77574078379305
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 114
dh =
         -3.36333545448658
rdh_sum =
          7.98760044704861
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 115
dh =
         -3.40918545448658
rdh_sum =
          8.20481335669187
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 118
dh =
         -3.60403545448658
rdh_sum =
          8.44530141819106
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 119
dh =
         -3.62728545448658
rdh_sum =
          8.68862137326608
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 120
dh =
         -3.64426045448658
rdh_sum =
          8.93401601162604
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 121
         -3.65496045448658
rdh_sum =
         9.18072145595269
Berm Factor Calculation: Iteration 4, Profile Segment: 126
         -4.12838545448658
rdh_sum =
```

```
9.48759356819826
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 127
dh =
         -4.18293545448658
rdh_sum =
          9.80164433922863
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 128
dh =
         -4.21903545448658
rdh_sum =
          10.1204705111922
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 129
dh =
         -4.23668545448658
rdh_sum =
          10.4416384541943
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 130
         -4.25831045448658
rdh_sum =
          10.7656817019238
Berm Factor Calculation: Iteration 4, Profile Segment: 131
dh =
         -4.28391045448658
rdh sum =
          11.0931373745673
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 132
dh =
         -4.31266045448658
rdh_sum =
          11.4244362570965
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 133
dh =
        -4.34456045448658
rdh_sum =
          11.7600126229715
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 138
dh =
         -4.79738545448658
rdh_sum =
          12.1575992520768
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 139
dh =
         -4.84253545448658
rdh_sum =
          12.5614789743605
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 140
dh =
         -4.86608545448658
rdh_sum =
          12.9686474966653
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 141
dh =
         -4.86803545448658
rdh_sum =
          13.376088528731
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 142
dh =
         -4.89063545448658
rdh_sum =
          13.7866899347235
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 143
dh =
         -4.93388545448658
rdh_sum =
          14.2033495891876
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 146
         -5.13698545448658
rdh_sum =
         14.6486120081791
Berm Factor Calculation: Iteration 4, Profile Segment: 147
         -5.19413545448658
rdh_sum =
```

```
15.1019599760397
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 148
dh =
         -5.23781045448658
rdh_sum =
          15.5614954804189
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 149
dh =
         -5.26801045448657
rdh_sum =
          16.0253131965372
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 154
dh =
         -5.69873545448658
rdh_sum =
          16.5503438673183
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 155
         -5.67618545448657
rdh_sum =
          17.0721711431519
Berm Factor Calculation: Iteration 4, Profile Segment: 172
dh =
         -6.91756045448658
rdh sum =
          17.7653825409224
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 173
dh =
         -6.93326045448658
rdh_sum =
          18.4606513267108
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 178
dh =
         -7.37643545448658
rdh_sum =
          19.2122379168318
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 179
dh =
        -7.40228545448657
rdh_sum =
          19.9669946222166
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 180
dh =
         -7.44433545448658
rdh_sum =
          20.7268786319228
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 181
dh =
         -7.50258545448658
rdh_sum =
          21.4938036977231
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 184
dh =
         -7.70038545448658
rdh_sum =
          22.2840799591124
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 185
dh =
         -7.72573545448657
rdh_sum =
          23.0772840222052
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 186
dh =
         -7.76693545448658
rdh_sum =
          23.8752138992894
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 187
         -7.82398545448658
rdh_sum =
          24.6796199680946
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 194
         -8.59431045448657
rdh_sum =
```

```
25.5629632576319
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 195
dh =
         -8.64211045448658
rdh_sum =
          26.4506353337351
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 204
dh =
         -9.83591045448658
rdh_sum =
           27.421344182127
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 205
dh =
         -9.86051045448658
rdh_sum =
          28.3932213297462
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 206
         -9.86938545448658
rdh_sum =
          29.3655142997744
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 207
dh =
         -9.86253545448658
rdh sum =
          30.3374865900422
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 208
dh =
         -9.86646045448658
rdh_sum =
          31.3096428467276
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 209
dh =
         -9.88116045448658
rdh_sum =
          32.2824828678676
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 214
dh =
         -10.3572104544866
rdh_sum =
          33.2729373632931
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 215
dh =
         -10.4098104544866
rdh_sum =
          34.2647916199884
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 216
dh =
         -10.4557854544866
rdh_sum =
          35.2577791838701
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 217
dh =
         -10.4951354544866
rdh_sum =
          36.2516698001199
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 218
dh =
         -10.5365604544866
rdh_sum =
          37.2464442397028
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 219
dh =
         -10.5800604544866
rdh_sum =
          38.2420728382586
ans =
Berm Factor Calculation: Iteration 4, Profile Segment: 220
dh =
         -10.6233604544866
rdh_sum =
          39.2384763206842
Berm Factor Calculation: Iteration 4, Profile Segment: 221
         -10.6664604544866
```

```
40.2355763368092
ans =
!----- End Berm Factor Calculation, Iter: 4 -----!
berm_width =
   96
rB =
        0.422046033047832
rdh_mean =
        0.419120586841762
gamma_berm =
         0.754842147997413
slope =
        0.157589017558115
Irb =
         1.32599946565103
gamma_berm =
        0.754842147997413
gamma_perm =
gamma_beta =
gamma_rough =
gamma =
        0.754842147997413
ans =
!!! - - Iribaren number: 1.00 is in the valid range (0.5-10), TAW RECOMMENDED - - !!!
!!! - - slope: 1:6.3 V:H is in the valid range (1:8 - 1:1), TAW RECOMMENDED - - !!!
R2\_new =
         11.0314016981865
R2del =
       0.0138982357541675
Z2 =
         20.1433912436999
top_sta =
         222.949083516128
ans =
!----- STARTING ITERATION 5 -----!
Ztoe =
                -0.559889
toe_sta =
         -4.37839811542992
top_sta =
         222.949083516128
7.2 =
          20.1433912436999
H0 =
                   6.2267
Tp =
                  10.2103
T0 =
          9.28209090909091
R2 =
         11.0314016981865
Z2 =
          20.1433912436999
top_sta =
          222.949083516128
Lslope =
          227.327481631558
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 20
         7.01733954551342
rdh_sum =
        0.599065845823981
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 21
dh =
          6.95683954551342
rdh_sum =
         1.19064063116286
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 28
dh =
          5.84106454551342
rdh_sum =
          1.6420749834842
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 29
         5.82241454551342
rdh_sum =
         2.09116860919536
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 30
         5.79601454551342
```

```
2.53695075903407
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 31
dh =
          5.76186454551342
rdh_sum =
          2.97845290273617
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 32
dh =
          5.71803954551342
rdh_sum =
          3.41446888099168
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 33
dh =
          5.66453954551342
rdh_sum =
          3.84379821136296
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 44
          4.10266454551342
rdh_sum =
          4.08852215773557
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 45
dh =
          4.03861454551342
rdh sum =
          4.32633313641215
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 60
dh =
         0.716464545513425
rdh_sum =
          4.33447774023632
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 61
dh =
         0.718214545513424
rdh_sum =
          4.34266207081192
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 62
dh =
         0.719939545513425
rdh_sum =
          4.35088565442187
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 63
dh =
         0.721639545513424
rdh_sum =
          4.35914801329253
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 72
dh =
        -0.569610454486575
rdh_sum =
          4.36571220061653
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 73
dh =
        -0.597610454486576
rdh_sum =
          4.37293599643225
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 74
dh =
        -0.605235454486575
rdh_sum =
          4.38034484770878
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 75
dh =
        -0.592485454486576
rdh_sum =
          4.38744556768572
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 76
dh =
        -0.584710454486576
rdh_sum =
          4.39436157742504
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 77
        -0.581910454486575
rdh_sum =
```

```
4.40121165973634
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 82
dh =
         -1.05048545448658
rdh_sum =
           4.4234200057881
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 83
dh =
         -1.10383545448657
rdh_sum =
          4.44792230976563
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 88
dh =
         -1.89333545448658
rdh_sum =
          4.51886133336414
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 89
         -1.93178545448658
rdh_sum =
          4.59263714648905
Berm Factor Calculation: Iteration 5, Profile Segment: 94
dh =
         -2.39768545448658
rdh sum =
          4.70474130202309
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 95
dh =
         -2.45383545448658
rdh_sum =
          4.82193982616538
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 96
dh =
        -2.48993545448658
rdh_sum =
          4.94246540315579
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 97
dh =
         -2.50598545448658
rdh_sum =
          5.06448308336729
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 98
dh =
         -2.54166045448657
rdh_sum =
          5.18984556159912
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 99
dh =
         -2.59696045448658
rdh_sum =
          5.32046913167688
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 100
dh =
         -2.65703545448658
rdh_sum =
          5.45691184915817
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 101
dh =
         -2.72188545448658
rdh_sum =
          5.59975562600399
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 102
dh =
         -2.78673545448658
rdh_sum =
          5.74912227796662
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 103
         -2.85158545448658
rdh_sum =
          5.90513139603257
Berm Factor Calculation: Iteration 5, Profile Segment: 104
         -2.91396045448658
rdh_sum =
```

```
6.06764019234921
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 105
dh =
         -2.97386045448658
rdh_sum =
          6.23649102556178
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 106
dh =
         -3.03341045448658
rdh_sum =
           6.4117423610563
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 107
dh =
         -3.09261045448658
rdh_sum =
          6.59344916036403
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 108
         -3.14551045448658
rdh_sum =
          6.78100103519435
Berm Factor Calculation: Iteration 5, Profile Segment: 109
dh =
         -3.19211045448658
rdh sum =
          6.97376067124052
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 110
dh =
         -3.23113545448658
rdh_sum =
          7.17092319802868
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 111
dh =
         -3.26258545448658
rdh_sum =
         7.37166123106984
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 112
dh =
         -3.29383545448658
rdh_sum =
          7.57597581116739
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 113
dh =
         -3.32488545448658
rdh_sum =
          7.78386724348411
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 114
dh =
         -3.36333545448658
rdh_sum =
          7.99621960550084
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 115
dh =
         -3.40918545448658
rdh_sum =
          8.21393647741063
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 118
dh =
         -3.60403545448658
rdh_sum =
          8.45497671070661
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 119
dh =
         -3.62728545448658
rdh_sum =
          8.69885461721066
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 120
         -3.64426045448658
rdh_sum =
         8.94481142921035
Berm Factor Calculation: Iteration 5, Profile Segment: 121
         -3.65496045448658
rdh_sum =
```

```
9.19208170955222
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 126
dh =
         -4.12838545448658
rdh_sum =
          9.49963631911347
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 127
dh =
         -4.18293545448658
rdh_sum =
          9.81438300846251
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 128
dh =
         -4.21903545448658
rdh_sum =
          10.1339139506523
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 129
         -4.23668545448658
rdh_sum =
          10.4557909823054
Berm Factor Calculation: Iteration 5, Profile Segment: 130
dh =
         -4.25831045448658
rdh sum =
          10.7805486007158
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 131
dh =
         -4.28391045448658
rdh_sum =
           11.108724883622
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 132
dh =
        -4.31266045448658
rdh_sum =
          11.4407513655541
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 133
dh =
         -4.34456045448658
rdh_sum =
          11.7770630618941
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 138
dh =
         -4.79738545448658
rdh_sum =
          12.1754911765547
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 139
dh =
         -4.84253545448658
rdh_sum =
          12.5802225080298
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 140
dh =
         -4.86608545448658
rdh_sum =
         12.9882478802201
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 141
dh =
         -4.86803545448658
rdh_sum =
          13.3965461948655
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 142
dh =
         -4.89063545448658
rdh_sum =
          13.8080098841127
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 143
         -4.93388545448658
rdh_sum =
           14.225541317633
Berm Factor Calculation: Iteration 5, Profile Segment: 146
         -5.13698545448658
rdh_sum =
```

```
14.6717187024969
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 147
dh =
         -5.19413545448658
rdh_sum =
          15.1259933362586
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 148
dh =
         -5.23781045448658
rdh_sum =
          15.5864643038269
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 149
dh =
         -5.26801045448657
rdh_sum =
          16.0512234910058
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 154
         -5.69873545448658
rdh_sum =
          16.5772738844109
Berm Factor Calculation: Iteration 5, Profile Segment: 155
dh =
         -5.67618545448657
rdh sum =
          17.1001171602999
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 172
dh =
         -6.91756045448658
rdh_sum =
          17.7944711216148
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 173
dh =
        -6.93326045448658
rdh_sum =
          18.4908829013787
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 178
dh =
        -7.37643545448658
rdh_sum =
          19.2436107649237
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 179
dh =
         -7.40228545448657
rdh_sum =
          19.9995077913618
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 180
dh =
         -7.44433545448658
rdh_sum =
          20.7605303665284
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 181
dh =
         -7.50258545448658
rdh_sum =
          21.5285911409164
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 184
dh =
         -7.70038545448658
rdh_sum =
          22.3199896757852
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 185
dh =
         -7.72573545448657
rdh_sum =
          23.1143138684938
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 186
         -7.76693545448658
rdh_sum =
          23.9133601842364
Berm Factor Calculation: Iteration 5, Profile Segment: 187
         -7.82398545448658
```

```
24.7188771564981
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 194
dh =
         -8.59431045448657
rdh_sum =
          25.6032072516073
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 195
dh =
         -8.64211045448658
rdh_sum =
           26.491855359235
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 204
dh =
         -9.83591045448658
rdh_sum =
          27.4631556133794
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 205
         -9.86051045448658
rdh_sum =
          28.4356139792809
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 206
dh =
         -9.86938545448658
rdh sum =
          29.4084844709152
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 207
dh =
         -9.86253545448658
rdh_sum =
          30.3810371369921
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 208
dh =
         -9.86646045448658
rdh_sum =
          31.3537721348715
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 209
dh =
         -9.88116045448658
rdh_sum =
          32.3271847556094
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 214
dh =
         -10.3572104544866
rdh_sum =
          33.3179967502946
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 215
dh =
         -10.4098104544866
rdh_sum =
          34.3101828837403
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 216
dh =
         -10.4557854544866
rdh_sum =
          35.3034796405385
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 217
dh =
         -10.4951354544866
rdh_sum =
          36.2976598235765
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 218
dh =
         -10.5365604544866
rdh_sum =
          37.2927029611055
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 219
         -10.5800604544866
rdh_sum =
          38.2885781168196
Berm Factor Calculation: Iteration 5, Profile Segment: 220
         -10.6233604544866
rdh_sum =
```

```
39.2852058898539
ans =
Berm Factor Calculation: Iteration 5, Profile Segment: 221
dh =
         -10.6664604544866
rdh_sum =
          40.2825078104902
ans =
!----- End Berm Factor Calculation, Iter: 5 -----!
berm_width =
rB =
         0.422298260249909
rdh_mean =
         0.419609456359273
gamma_berm =
         0.754902083155022
slope =
         0.157646213774078
Irb =
          1.32648073111597
gamma_berm =
         0.754902083155022
gamma_perm =
gamma_beta =
gamma_rough =
gamma =
         0.754902083155022
ans =
!!! - - Iribaren number: 1.00 is in the valid range (0.5-10), TAW RECOMMENDED - - !!!
ans = !!! - slope: 1:6.3 \text{ V:H} is in the valid range (1:8 - 1:1), TAW RECOMMENDED - - !!!
R2\_new =
          11.0362817164741
R2del =
       0.00488001828766471
          20.1482712619876
top_sta =
222.996786529693
% final 2% runup elevation
Z2=R2_new+SWEL
Z2 =
20.1482712619876
diary off
-1.000000e+00
-1.000000e+00
```

```
PART 5: RUNUP2
        for transect: CM-139
Station locations shifted by: -0.04 feet from their
original location to set the shoreline to
elevation 0 for RUNUP2 input
              RUNUP2 INPUT CONVERSIONS_
        for transect: CM-139
Incident significant wave height: 5.61 feet
Peak wave period: 10.45 seconds
Mean wave height: 3.51 feet
Local Depth below SWEL: 32.88 feet
Mean wave height deshoaled using Hunt approximation for
celerity assuming constant wave energy flux.
 References: R.G. Dean and R.A. Dalrymple. 2000. Water
             Wave Mechanics for Engineers and Scientists. World
              Scientific Publishing Company, River Edge New Jersy
             USACE (1985), Direct Methods for Calculating Wavelength, CETN-1-17
             US Army Engineer Waterways Experiment Station Coastel Engineering
             Research Center, Vicksburg, MS
             also see Coastal Engineering Manual Part II-3
             for discussion of shoaling coefficient
    Depth, D = 32.88
    Period, T = 8.88
    Waveheight, H = 3.51
Deep water wavelength, L0 (ft)
    L0 = g*T*T/twopi
    L0 = 32.17*8.88*8.88/6.28 = 403.69
Deep water wave celerity, CO (ft/s)
    C0 = L0/T
    C0 = 403.69/8.88 = 45.47
Angular frequency, sigma (rad/s)
    sigma = twopi/T
    sigma = 6.28/8.88 = 0.71
Hunts (1979) approximation for Celerity C1H (ft/s) at Depth D (ft)
    y = sigma.*sigma.*D./g
    y = 0.71*0.71*32.88/32.17 = 0.51
    \texttt{C1H} = \texttt{sqrt}( \texttt{g.*D.}/(\texttt{y+1.}/(\texttt{1} + \texttt{0.6522.*y} + \texttt{0.4622.*y.^2} + \texttt{0.0864.*y.^4} + \texttt{0.0675.*y.^5})) \ )
    C1H = 29.75
Shoaling Coefficient KsH
    KsH = sqrt(C0/C1H)
    KsH = sqrt(45.47/29.75) = 1.24
Deepwater Wave Height HO_H (ft)
    H0_H = H/KsH
    H0_H = 3.51/1.24 = 2.84
Deepwater mean wave height: 2.84 feet
              END RUNUP2 CONVERSIONS
              _RUNUP2 RESULTS
        for transect: CM-139
RUNUP2 SWEL:
8.80
```

8.80 8.80 8.80

```
8.80
8.80
8.80
8.80
RUNUP2 deepwater mean wave heights:
2.70
2.70
2.70
2.84
2.84
2.84
2.98
2.98
2.98
RUNUP2 mean wave periods:
8.43
8.88
9.32
8.43
8.88
9.32
8.43
8.88
9.32
RUNUP2 runup above SWEL:
3.59
3.69
3.87
3.67
3.83
3.94
3.75
3.92
4.06
RUNUP2 Mean runup height above SWEL: 3.81 feet
RUNUP2 2-percent runup height above SWEL: 8.39 feet
RUNUP2 2-percent runup elevation: 17.19 feet-NAVD88
RUNUP2 Messages:
Nonfatal Error, Check Output
             __END RUNUP2 RESULTS_
              ___ACES BEACH RUNUP_
Incident significant wave height: 5.61 feet
Significant wave height deshoaled using Hunt equation
Deepwater significant wave height: 3.98 feet
Peak wave period: 10.45 seconds
Average beach Slope: 1:13.57 (H:V)
ACES RUNUP CALCULATED USING 'Aces_Beach_Runup.m'
ACES Beach 2-percent runup height above SWEL: 6.72 feet
ACES Beach 2-percent runup elevation: 15.52 feet-NAVD88
ACES BEACH RUNUP is valid
```

8.80

RUNUP2 transect: C17.0
-24.08 -396.0 1.0
-23.70 -390.0 1.0
-15.66 -320.0 1.0
-14.05 -284.0 1.0
-4.98 -282.0 1.0
-4.53 -178.0 1.0
-4.53 -40.0 1.0
3.47 32.0 1.0
8.07 56.0 1.0
11.31 90.0 1.0
14.40 148.0 1.0
16.96 186.0 1.0
18.94 202.0 1.0
22.30 260.0 1.0
28.25 318.0 1.0 RUNUP2 transect: CM-139 28.25 318.0 29.04 342.0 29.04 342.0 1.0 31.83 380.0 1.0 35.84 426.0 1.0 38.75 448.0 1.0 1 41.95 500.0 1.0 8.8 2.70 8.43 8.8 2.70 8.88 2.70 9.32 2.84 8.43 2.84 8.88 8.8 8.8 2.84 9.32 2.98 8.43 2.98 8.88 2.98 9.32 8.8 8.8 8.8

FEMA

8.8

job 2 1 sjh

\*

## CROSS SECTION PROFILE

	LENGTH	ELEV.	SLOPE	ROUGHNESS
1	-396.0	-24.0	.00	1.00
2	-390.0	-23.7	8.64	1.00
3	-320.0	-15.6		
4	-284.0	-14.0	22.50	1.00
5	-282.0	-5.0	.22	1.00
6	-178.0	-4.5	231.11	1.00
7	-40.0	-4.5	FLAT	1.00
8	32.0	3.5	9.00	1.00
9	56.0	8.1	5.22	1.00
10	90.0	11.3	10.49	1.00
11	148.0	14.4	18.77	1.00
12	186.0	17.0	14.84	1.00
			8.08	1.00
13	202.0	19.0	17.26	1.00
14	260.0	22.3	9.75	1.00
15	318.0	28.3	30.38	1.00
16	342.0	29.0	13.62	1.00
17	380.0	31.8	11.47	1.00
18	426.0	35.8	7.56	1.00
19	448.0	38.8	16.25	1.00
20	500.0	42.0		

LAST SLOPE 17.00 LAST ROUGHNESS 1.00

\*

OUTPUT TABLE

## INPUT PARAMETERS RUNUP RESULTS

WATER LEVEL ABOVE DATUM (FT.)	DEEP WATER WAVE HEIGHT (FT.)	WAVE PERIOD (SEC.)	BREAKING SLOPE NUMBER	RUNUP SLOPE NUMBER	RUNUP ABOVE WATER LEVEL (FT.)	BREAKER DEPTH (FT.)
8.80	2.70	8.43	8	10	3.59	4.10
8.80 COMPOSITE SLOPE USED	2.70 BUT WAVE MAY	8.88 REFLECT, NOT BREAK	8	10	3.69	4.19
8.80 COMPOSITE SLOPE USED	2.70	9.32	8	10	3.87	4.27
8.80	2.84	8.43	8	10	3.67	4.27
8.80 COMPOSITE SLOPE USED	2.84 BUT WAVE MAY	8.88 REFLECT, NOT BREAK	8	10	3.83	4.36
8.80 COMPOSITE SLOPE USED	2.84 BUT WAVE MAY	9.32 REFLECT, NOT BREAK	8	10	3.94	4.45
8.80	2.98	8.43	8	10	3.75	4.45
8.80	2.98	8.88	8	10	3.92	4.53
8.80 COMPOSITE SLOPE USED	2.98 BUT WAVE MAY	9.32 REFLECT, NOT BREAK	8	10	4.06	4.62

