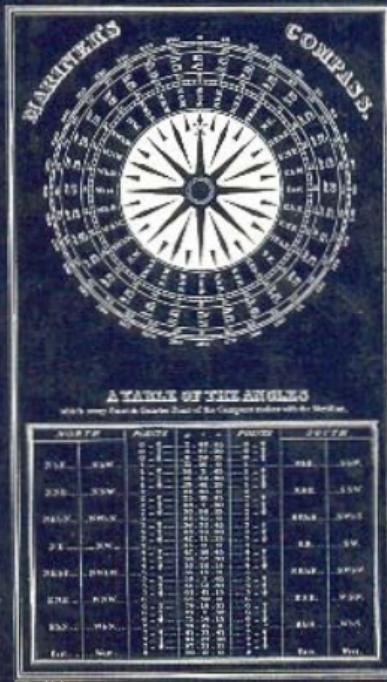


NORIE'S NAUTICAL TABLES



Edited by
Capt. A. G. Blance

Imray Laurie Norie & Wilson

NORIE'S NAUTICAL TABLES

WITH EXPLANATIONS OF THEIR USE

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PREFACE

One hundred and eighty years of publication involving many new editions and reprints afford a searching test of the usefulness and value of any publication designed to meet the exacting requirements of navigators and the shipping industry. Since J. W. Norie published the first edition of his **COMPLETE SET OF NAUTICAL TABLES AND EPITOME OF PRACTICAL NAVIGATION** in 1803, the tables have undergone a continuing process of change to maintain their usefulness to the modern practical navigator.

During these years many changes to the tables have been necessary in both content and presentation to conform with changing techniques of navigation, but the aim of the editors has always been to have user friendly navigational tables which could be used quickly and easily under shipboard conditions. This has resulted in many changes to the tables aimed at removing much of the tedium of interpolation, so enabling the navigator to obtain the answers to navigational problems quickly with the minimum of probability of error. Certain tables and data are also included which are not readily available on board ship or are only used in the examination room, but the physical dimensions of the book impose strict limits on what can be included with the result that it is impossible to include all the tables the editor would wish.

In the present edition, the Star's Total Correction Table inside the back cover, the Moon's Total Correction Table and the extended Star's Total Correction Table have been redesigned to reduce interpolation to a minimum.

The editor wishes to thank all those who have suggested improvements to the tables, and will welcome any further helpful criticism which users of the Tables may care to make.

A. G. BLANCE
London 1991

EXPLANATION AND
USE OF THE TABLES

I. COMPUTATION TABLES

TRAVERSE TABLE

(Pages 2 - 93)

These Tables afford an easy and expeditious means of solving all problems that resolve themselves into the solution of right-angled plane triangles. They can thus be applied to all the forms of Sailings except Great Circle Sailing; but they are specially useful in resolving a Traverse. On this account they are called Traverse Tables, and the terms *Course*, *Distance*, *Difference of Latitude* and *Departure* are used as names of the different parts involved.

The Traverse Table has now been brought into line with the requirements of the modern compass notation by the inclusion, at the top and foot of each page, of the number of degrees of the new (0-360) circular system of reckoning, corresponding to the value printed at centre of title in conformity with the older quadrantal notation, the latter form being retained for its application to the solution of certain problems in the Sailings and for its utility in the conversion of Departure to Difference of Longitude and vice versa, as explained later in this article.

The figures denoting the number of degrees under the new arrangement are placed in the appropriate quadrants of a small diagrammatic symbol, representing the cardinal points of the compass, and in these positions they introduce the equivalents in the new notation corresponding to the number of degrees of the old system, shown at centre of titles, when pertaining to the respective quadrants. The arrangement will be better understood by reference to an example; thus, on page 58 —'28 DEGREES'

For old	N28°E	S28°E	S28°W	N28°W
Read new	↑ 028°	↑ 152°	208° ↑	332° ↑

or vice versa, and, as examples of the reverse process, on page 38, but this time from the foot with caption '72 DEGREES'—

For new	↑ 072°	↑ 108°	↑ 252°	288° ↑
Read old	N72°E	S72°E	S72°W	N72°W

It will be observed that, in the new notation of the Traverse Table, the three-figure degrees corresponding to Easterly courses are placed in the symbol diagram towards the right-hand side of the page, in contradistinction to those for Westerly equivalents which are printed on the left.

The courses, in both the old and new notation, are displayed at the top and bottom of the pages, while the Distances are arranged in order in the columns marked Dist. The Difference of Latitude and Departure corresponding to any given Run on any given Course will be found in the columns marked D. Lat. and Dep., respectively, of the page for the given Course and opposite the given Distance. But it must most carefully be observed that when the required Course is found at the top of the page, the Difference of Latitude and Departure also are to be taken from the columns as named at the top of the page; and when the Course appears at the foot of the page, the relevant quantities too must be taken from the columns as named at the foot of the page.

When any of the given quantities (except the Course which is never to be changed) exceeds the limits of the tables, any aliquot part, as a half or a third, is to be taken, and the quantities found are to be doubled or trebled; that is, they are to be multiplied by the same figure as the given quantity was divided by. And since the Difference of Latitude and Departure corresponding to any given Course and Distance are to be found opposite the Distance on that page which contains the Course, it follows that if any two of the four parts be given, and these two be found in their proper places in the tables, the other two will be found in their respective places on the same page.

The following examples will illustrate the application of the tables to Plane Sailing:—

1 Example: Find the difference of latitude and departure made good by a ship in sailing 84 miles on a course 112° . (S 68° E., Old Style).

Course 112° is found in the Table at foot of page 46. Opposite 84 in the Distance column on that page we get:—D. Lat. 31·5, Dep. 77·9.

The D. Lat. is named S and Departure E, because it is noted that 112° is shown in the South and East quadrant of the compass symbol.

2 Example: Find the course and distance made good by a ship whose difference of latitude was found to be 431 miles S, and departure 132' W.

431 and 132 are not to be found alongside each other, but in the Table on page 37 we find 431·3 and 131·9, and these are sufficiently near to the desired value for all practical purposes. These give 197° , or 17° old style, as a course, and 451 as a distance. Hence—

Course $S17^\circ$ W, or 197° , and Distance 451 miles.

These tables may also, as has already been stated, be applied to solving problems in Parallel and Middle Latitude Sailings. In solving these problems the Course (old notation) at the top or bottom of page becomes the Latitude or Middle Latitude, the Distance column becomes a Diff. Longitude column, and the D. Lat. column becomes a Dep. column. To facilitate the taking out of these quantities the D. Long. and Dep. are bracketed together, and the words *D. Long.*, and *Dep.* are also printed in italics at the top of their respective columns when the Latitude or Middle Latitude, as course, is at the top; but at the bottom of their respective columns when Latitude or Middle Latitude, as course is at the bottom.

3 Example: In Latitude or Middle Latitude 47° the departure made good was 260·5; required the difference of Longitude.

With 47° as course at the bottom of the page, look in the column with *Dep.* printed in italics at the bottom, just over the end of the bracket; and opposite to 260·5 will be found 382 in the *D. Long.* column, which is the Difference of Longitude required. (Page 89)

4 Example: A ship, after sailing East 260·5, had changed her Longitude $6^\circ 22'$. Required the parallel of Latitude on which she sailed.

$6^\circ 22'$ equals 382'. Opposite 382 in *D. Long.* column is 260·5 in *Dep.* column entered from the bottom, and the parallel on which she sailed is Lat. 47° .

(Page 89)

MERIDIONAL PARTS (For the Spheroid)

(Pages 94 - 102)

This table is used in resolving problems by *Mercator's Sailing* and in constructing charts on Mercator's projection. The meridional parts are to be taken out for the degrees answering to the given latitude at the top or bottom, and for the minutes at either side column. Thus, the meridional parts corresponding to the latitude $49^\circ 57'$ are 3451·88.

(Page 98)

LOGARITHMS

(Pages 103 - 117)

This table gives correct to five significant figures the mantissae (or fractional parts) of the common logarithms of numbers. The operator must decide for himself the integral or whole number part of the logarithm (called the characteristic) according to the position of the decimal point in the natural number.

The rules for determining the characteristic can be demonstrated by the following:

10 000	=	10^4	$\therefore \log_{10} 10\ 000$	=	4
1 000	=	10^3	$\therefore \log_{10} 1\ 000$	=	3
100	=	10^2	$\therefore \log_{10} 100$	=	2
10	=	10^1	$\therefore \log_{10} 10$	=	1
1	=	10^0	$\therefore \log_{10} 1$	=	0
0.1	=	10^{-1}	$\therefore \log_{10} 0.1$	=	-1
0.01	=	10^{-2}	$\therefore \log_{10} 0.01$	=	-2
0.001	=	10^{-3}	$\therefore \log_{10} 0.001$	=	-3
0.0001	=	10^{-4}	$\therefore \log_{10} 0.0001$	=	-4

The above, which may be extended infinitely in both directions, shows that the log. of, say, 342 must lie between 2 and 3. Similarly, the log. of 29.64 must be between 1 and 2. From the table it will be found that $\log. 342 = 2.53403$ and $\log. 29.64 = 1.47188$. These statements could be expressed as follows:—

(pg 107)

(pg 106)

$$10^{2.53403} = 342$$

$$10^{1.47188} = 29.64$$

For numbers greater than 1 the rule for finding the characteristic is—The characteristic is the number which is 1 less than the number of figures before the decimal point. If there are five figures before the decimal point the characteristic is 4; if there is one figure before the decimal point the characteristic is 0, and so on. Thus:—

$\log. 5378$	=	3.73062
$\log. 537.8$	=	2.73062
$\log. 53.78$	=	1.73062
$\log. 5.378$	=	0.73062

(pg 110)

For numbers less than 1 the rule for finding the characteristic is—The negative characteristic of the log. of a number less than 1 is the number which is 1 more than the number of noughts between the decimal point and the first significant figure. Thus:—

$\log. 0.5378$	=	1.73062
$\log. 0.05378$	=	2.73062
$\log. 0.005378$	=	3.73062
$\log. 0.0005378$	=	4.73062

Tabular logarithms To avoid the negative characteristics, logarithms in tabular form are obtained by adding 10 to the characteristic.

Example: $\log. 0.5378 = 1.73062$ or in tabular form 9.73062

$\log. 0.005378 = 3.73062$ or in tabular form 7.73062

In the tables of logarithms of trigonometrical functions the characteristic is given in both forms at the top of each column of logarithms.

Example: $\log. \sin. 5^\circ 30' = 2.98157$ or 8.98157
 $\log. \cot. 5^\circ 30' = 1.01642$ or 11.01642

(pg 140)

Interpolation

When the number whose logarithm is required consists of four significant figures or less the mantissa is taken from the main part of the table. Where there are five significant figures the difference for the fifth figure is obtained from the relevant section of the D column.

Example: $\log. 140 \cdot 27 = 2 \cdot 14675 + 21 = 2 \cdot 14696$ (page 103)

If the number consists of more than six significant figures the approximate logarithm can be found by simple proportion.

Example: $\log. 140 \cdot 277 = 2 \cdot 14675$ (from main table) + 21 (from D column)
+ 2 (by simple proportion)
= 2.14698

To find the number, N, whose log. is known. If the number is required to four significant figures or less all that is necessary is to find the series of digits corresponding to the tabulated mantissa which is nearest to the one given. The characteristic of the log. will determine the position of the decimal point. Thus:—

Given $\log. N = 1 \cdot 87109$.

Nearest tabulated mantissa 87111 gives digits 7432. (pg 113)

The characteristic being 1, there are two figures before the decimal point.

The required number, N, is therefore 74.32.

The following examples will serve to illustrate the procedure when more than four significant figures are required. Suppose the number, N, correct to five significant figures is required when $\log. N$ is known to be 2.27104.

Example: $\log. N = 2 \cdot 27104$

The next less tabulated mantissa .27091 gives the digits 1866. (page 104)
But $.27104 - .27091 = 13$

∴ Entering the 180-189 section of the D column the fifth figure is 6 for a D value of 12 and by simple proportion the sixth figure is therefore 5.

∴ the digits of the number are 18665

The characteristic of the logarithm is 2.

∴ the number N is 186.665

LOGS. OF TRIG. FUNCTIONS

(Pages 118 - 241)

Whilst preserving the basic layout which has been a feature of 'Norie's', and 'Norie's' alone, since J. W. Norie produced the original edition, changes have been introduced which make the table a much more efficient instrument in conforming with the modern technique of astronomical navigation. For all angles from 0° to 90° the table is now completely downward reading and for that reason alone should be practically blunder-proof. In the main part of the table from 4° to 86° the log. functions of angles are tabulated for one minute intervals of the angles and proportional parts for fractions of one minute (from $0 \cdot 1$ to $0 \cdot 9$) are given. In the remainder of the table, where that system ceases to be practicable, log. functions are tabulated for intervals of $0 \cdot 1$ or $0 \cdot 2$ as necessary and differences between successive tabulations are given. This means that, except in special and rare cases, interpolation is reduced when taking out any log. function of an angle and there is no need to resort to the questionable practice of rounding off angles to the nearest minute in order to 'save trouble'. With this table it is no more of an effort to work accurately than it is to work roughly. How far a navigator is justified in working to tenths of a minute is a matter which can be argued about indefinitely,

but since the Nautical Almanac gives hour angles and declinations to tenths of a minute and a modern sextant with a decimal vernier enables readings to be taken to tenths of a minute as well, it would seem only logical to use navigation tables which, with the minimum of effort, provide for the same order of precision.

The characteristic of the logarithm is given at the top of each function's column in indicial form with the tabular form in brackets.

Example: log. sin. $5^{\circ} 09'$ = $\bar{2}.95310$ or 8.95310

Thus the navigator can use whichever form of characteristic is preferred though it must be appreciated that the two forms cannot be interchanged within a calculation.

Occasionally, it may be necessary to find the logs. of trigonometrical functions of angles greater than 90° . No difficulty should be experienced in such cases as the second, third and fourth quadrant equivalents of the first quadrant angles are plainly indicated. It should be noted, however, that the table is *upward* reading for angles between 90° and 180° and also for those between 270° and 360° , but *downward* reading for angles between 180° and 270° . In *all* cases, however, the name of the ratio being used appears at the *top* of the page. When applying proportional parts care should be taken to notice in which direction the log. function is increasing, i.e. upwards or downwards.

Examples:

(P9 127)	log. sin.	$1^{\circ} 38'7$	$= \bar{2} \cdot (45754 + \frac{86}{2})$	$= \bar{2}.45798$	or	8.45798
(P9 129)	-log. tan.	$177^{\circ} 57'5$	$= \bar{2} \cdot (55240 - \frac{70}{2})$	$= \bar{2}.55205$	or	8.55205
	log. cosec.	$26^{\circ} 04'4$	$= 0 \cdot (35712 - 10)$	$= 0.35702$	or	10.35702
	log. sec.	$333^{\circ} 25'3$	$= 0 \cdot (04852 - 2)$	$= 0.04850$	or	10.04850
	log. cos.	$138^{\circ} 17'6$	$= \bar{1} \cdot (87300 + 7)$	$= \bar{1}.87307$	or	9.87307
	log. sin.	$62^{\circ} 19'8$	$= \bar{1} \cdot (94720 + 5)$	$= \bar{1}.94725$	or	9.94725
	log. cot.	$117^{\circ} 53'0$		$= \bar{1}.72354$	or	9.72354
	log. cos.	$83^{\circ} 15'3$	$= \bar{1} \cdot (07018 - 32)$	$= \bar{1}.06986$	or	9.06986

To find the angle whose log. function is given is equally simple. For instance, to find θ when log. sin. $\theta = \bar{1}.66305$ or 9.66305 , notice that the next *less* tabulated log. sin. is $\bar{1}.66295$ or 9.66295 which gives the angle $27^{\circ} 24'0$. The excess 10 gives an additional $0'4$. Hence, $\theta = 27^{\circ} 24'4$.

In practice, the above processes will, of course, be performed mentally.

HAVERSINES

(Pages 242 - 348)

To make the tables clearer and to make interpolation almost completely unnecessary the tables are presented as follows:-

1. The Log. Haversines are printed in bold type and the Natural Haversines in light type.
2. In the range 0° to 90° and 270° to 360° (the range most frequently used) haversines are tabulated at $0.2'$ intervals and the proportional parts for $0.1'$ are given at the foot of each page.
3. In the remainder of the table haversines are tabulated at $1.0'$ intervals and the proportional parts for $0.2'$ are given at the top of each column.
4. The characteristic of the logarithms is given at the top of each column in the negative index form together with the tabular form in brackets.

ANGLE	LOG. HAVERSINE	NAT. HAV.
15° 33'·0	2·26249 or 8·26249	0·01830 — pg 258
15° 33'·6	2·26304 or 8·26304	0·01832 — //
15° 33'·7	2·26313 or 8·26313	0·01832 — //
344° 10'·0	2·27807 or 8·27807	0·01897 — //
344° 10'·4	2·27771 or 8·27771	0·01895 — //
344° 10'·5	2·27762 or 8·27762	0·01895 — //
95° 25'·0	1·73815 or 9·73815	0·54720 — pg 334
95° 25'·6	1·73822 or 9·73822	0·54729 — //
263° 37'·0	1·74475 or 9·74475	0·55559 — //
263° 37'·8	1·74466 or 9·74466	0·55547 — //

Derivation of Haversine Formulae:

$$\cos. A = \frac{\cos. a - \cos. b \cos. c}{\sin. b \sin. c}, \text{ (fundamental formula).}$$

$$\therefore 1 - \cos. A = 1 - \frac{\cos. a - \cos. b \cos. c}{\sin. b \sin. c}$$

$$\text{i.e. vers } A = \frac{\sin. b \sin. c - \cos. a + \cos. b \cos. c}{\sin. b \sin. c},$$

$$\therefore \cos. (b \sim c) - \cos. a = \sin. b \sin. c \text{ vers. } A,$$

or — cos. a = — cos. (b ~ c) + sin. b sin. c vers. A.

By adding unity to each side this becomes—

$$1 - \cos. a = 1 - \cos. (b \sim c) + \sin. b \sin. c \text{ vers. } A,$$

$$\therefore \text{vers. } a = \text{vers. } (b \sim c) + \sin. b \sin. c \text{ vers. } A,$$

$$\text{whence hav. } a = \text{hav. } (b \sim c) + \sin. b \sin. c \text{ hav. } A \dots \dots \dots (1)$$

By transposing we obtain—

$$\text{hav. } A = [\text{hav. } a - \text{hav. } (b \sim c)] \text{ cosec. } b \text{ cosec. } c. \dots \dots \dots (2)$$

$$\text{and hav. } (b \sim c) = \text{hav. } a - \text{hav. } A \sin. b \sin. c. \dots \dots \dots (3)$$

These three versions of the spherical haversine formula are frequently adapted for navigational purposes as follows.

$$(1) \text{Hav. } z = \text{hav. } (l \pm d)^* + \text{hav. } h \cos. l \cos. d.$$

$$(2) \text{Hav. } h = [\text{hav. } z - \text{hav. } (l \pm d)^*] \sec. l \sec. d.$$

$$(3) \text{Hav. mer. zen. dist.} = \text{hav. } z - \text{hav. } h \cos. l \cos. d.$$

where $\begin{cases} z = \text{zenith distance,} \\ l = \text{latitude,} \\ d = \text{declination,} \\ h = \text{hour angle.} \end{cases}$

* ($l \sim d$) when l and d have the same name,
 ($l + d$) when l and d have different names.

Examples

- (1) Find zenith distance when $h = 66^\circ 49' \cdot 3$, $l = 31^\circ 10' \cdot 2$ N., $d = 19^\circ 24' \cdot 7$ N.

$$\text{Hav. } z = \text{hav. } h \cos. l \cos. d + \text{hav. } (l \pm d).$$

h	..	$66^\circ 49' \cdot 3$	L. hav. $\bar{1} \cdot 48173$ or $9 \cdot 48173$	
l	..	$31^\circ 10' \cdot 2$	L. cos. $\bar{1} \cdot 93228$ or $9 \cdot 93228$	
d	..	$19^\circ 24' \cdot 7$	L. cos. $\bar{1} \cdot 97458$ or $9 \cdot 97458$	
			<hr/>	
			L. hav. $\bar{1} \cdot 38859$ or $9 \cdot 38859$	N. hav. $0 \cdot 24468$
$(l \sim d)$..	$11^\circ 45' \cdot 5$	N. hav. $0 \cdot 01049$
z	..	$60^\circ 40' \cdot 9$	N. hav. $0 \cdot 25517$
			<hr/>	

Calculated zenith distance = $60^\circ 40' \cdot 9$ and is used for comparing with the true zenith distance to find the intercept when establishing the position line by the Marc St. Hilaire or Intercept method.

- (2) Find the hour angle when $l = 41^\circ 21' \cdot 6$ N., $d = 9^\circ 34' \cdot 1$ S., $z = 63^\circ 45' \cdot 8$.

$$\text{Hav. } h = [\text{hav. } z - \text{hav. } (l \pm d)] \sec. l \sec. d.$$

z	..	$63^\circ 45' \cdot 8$	N. hav. $0 \cdot 27896$	
$(l + d)$..	$50^\circ 55' \cdot 7$	N. hav. $0 \cdot 18485$	
			<hr/>	
l	..	$41^\circ 21' \cdot 6$	N. hav. $0 \cdot 09411$	L. hav. $\bar{2} \cdot 97364$ or $8 \cdot 97364$
d	..	$9^\circ 34' \cdot 1$	L. sec. $0 \cdot 12461$ or $10 \cdot 12461$
				L. sec. $0 \cdot 00608$ or $10 \cdot 00608$
h	..	$41^\circ 46' \cdot 9$	L. hav. $\bar{1} \cdot 10433$ or $9 \cdot 10433$
			<hr/>	

Hour angle = $41^\circ 46' \cdot 9$ if body is W. of the meridian, or hour angle = $318^\circ 13' \cdot 1$ if body is E. of the meridian, and is used for finding the computed longitude when establishing the position line by the "chronometer method".

- (3) Find the mer. zen. dist. when $h = 355^\circ 57' \cdot 2$, $l = 48^\circ 12' \cdot 5$ N., $d = 12^\circ 13' \cdot 7$ S., $z = 60^\circ 21' \cdot 6$.

$$\text{Hav. mer. zen. dist.} = \text{hav. } z - \text{hav. } h \cos. l \cos. d.$$

h	..	$355^\circ 57' \cdot 2$	L. hav. $\bar{3} \cdot 09571$ or $7 \cdot 09571$	
l	..	$48^\circ 12' \cdot 5$	L. cos. $\bar{1} \cdot 82375$ or $9 \cdot 82375$	
d	..	$12^\circ 13' \cdot 7$	L. cos. $\bar{1} \cdot 99003$ or $9 \cdot 99003$	
			<hr/>	
			L. hav. $\bar{4} \cdot 90949$ or $6 \cdot 90949$	N. hav. $0 \cdot 00081$
z	..	$60^\circ 21' \cdot 6$	N. hav. $0 \cdot 25273$
mer. zen. dist.	..	$60^\circ 15' \cdot 2$	N. hav. $0 \cdot 25192$
			<hr/>	

The mer. zen. dist., $60^\circ 15' \cdot 2$, when combined with the declination gives the latitude of the point where the position line (at right angles to the direction of the body) cuts the meridian of D.R. longitude used to compute h . This method of working an ex-meridian sight is, of course, an alternative to using ex-meridian tables.

The haversine formulae and great circle sailing calculations

Formula (1) is used to find the great circle distance from one point to another and formula (2) is used to find the initial and final courses. The vertex of the track and the latitude of the point where the track cuts any specified meridian can then be found by right angled spherical trigonometry.

Example: Find the great circle distance and the initial course on the track from A ($17^{\circ} 22' N.$, $25^{\circ} 28' W.$) to B ($40^{\circ} 08' N.$, $73^{\circ} 17' W.$).

To find the great circle distance

Hav. AB =	hav. (PA ~ PB) + hav. P sin. PA sin. PB.		
P ..	$47^{\circ} 49' 0$	L. hav. $\overline{1.21550}$ or 9.21550	
PA ..	$72^{\circ} 38' 0$	L. sin. $\overline{1.97974}$ or 9.97974	
PB ..	$49^{\circ} 52' 0$	L. sin. $\overline{1.88340}$ or 9.88340	
(PA ~ PB) ..	$22^{\circ} 46' 0$	L. hav. $\overline{1.07864}$ or 9.07864	N. hav. $\overline{0.11985}$
AB ..	$46^{\circ} 58' 2$	N. hav. $\overline{0.03896}$
			N. hav. $\overline{0.15881}$
		∴ Great circle distance = 2818.2 miles.	

To find the initial course

Hav. A = [hav. PB - hav. (PA ~ AB)] cosec. PA cosec. AB.			
PB ..	$49^{\circ} 52' 0$	N. hav. $\overline{0.17772}$	
(PA ~ AB) ..	$25^{\circ} 39' 8$	N. hav. $\overline{0.04932}$	
PA ..	$72^{\circ} 38' 0$	N. hav. $\overline{0.12840}$	L. hav. $\overline{1.10856}$ or 9.10856
AB ..	$46^{\circ} 58' 2$	L. cosec. $\overline{0.02026}$ or 10.02026
A ..	$50^{\circ} 48' 5$	L. cosec. $\overline{0.13609}$ or 10.13609
			L. hav. $\overline{1.26491}$ or 9.26491
		∴ Initial course = N. $50^{\circ} 48' 5$ W. or $309^{\circ} 11' 5$.	

NATURAL FUNCTIONS OF ANGLES

(Pages 349-363)

In these tables, which are intended for use with simple pocket calculators, the natural trigonometric functions can be obtained to five decimal places.

Examples:

1. To find $\tan. 49^{\circ} 38'$:

$$\begin{array}{r} 1.17500 \quad (\tan. 49^{\circ} 36') \\ + 0.00138 \quad (2' \text{ from difference table against } 49^{\circ}) \\ \hline \end{array}$$

$$\tan. 49^{\circ} 38' = \underline{1.17638}$$

Page (354)

2. To find $\cos. 80^\circ 27'$:

$$\begin{array}{r} 0.16677 \quad (\cos. 80^\circ 24') \\ -0.00086 \quad (3' \text{ from difference table against } 80^\circ, \text{ subtracted}) \\ \hline \cos. 80^\circ 27' = 0.16591 \end{array}$$

(page 352)

3. To find $\sec. 76^\circ 44'$:

$$\begin{array}{r} 4.34689 \quad (\sec. 76^\circ 42') \\ +0.01078 \quad (\frac{1}{3}[\sec. 76^\circ 42' - \sec. 76^\circ 48']); \text{ difference must be} \\ \hline \text{obtained by this method because the mean} \\ \text{differences are not sufficiently accurate} \\ \sec. 76^\circ 44' = 4.35767 \end{array}$$

4. To convert $31^\circ 46'$ to radians:

$$\begin{array}{r} 31^\circ = 0.54105 \text{ radians} \\ 46' = 0.01338 \text{ radians} \\ \hline 31^\circ 46' = 0.55443 \text{ radians} \end{array}$$

(page 363)

5. To convert 1.648 radians to degrees:

$$\begin{array}{r} 1 \text{ radian} = 57^\circ 17.7' \\ 0.648 \text{ radians} = 37^\circ 07.7' \\ \hline 1.648 \text{ radians} = 94^\circ 25.4' \end{array}$$

(page 362)

SQUARES AND CUBES OF NUMBERS

(Pages 364 - 367)

These tables will give squares and cubes of numbers to four significant figures.

To obtain the square or cube of a number:

- (a) If the number is between 1 and 10 and consists of three significant figures (or less) the square or cube is taken from the main part of the tables, but if there are four significant figures the Mean Difference section is also used.

Example:

$$\begin{array}{ll} 2.824^2 & = 7.952 \text{ (from main table)} + 23 \text{ (from Mean Difference)} \\ & = 7.975 \\ 7.631^3 & = 58.22 \text{ (from main table)} + 2 \text{ (from Mean Difference)} \\ & = 58.24 \end{array}$$

- (b) All other numbers are converted into scientific notation and the square or cube obtained for the significant figures as before.

Example:

$$\begin{array}{ll} 463.8^2 & = (4.638 \times 10^2)^2 = 21.51 \times 10^4 \\ & = 2.151 \times 10^5 \text{ or } 215\ 100 \\ 0.000\ 07251^3 & = (7.251 \times 10^{-5})^3 = 381.3 \times 10^{-15} \\ & = 3.813 \times 10^{-13} \text{ or } 0.000\ 000\ 000\ 3813 \end{array}$$

SQUARE AND CUBE ROOTS OF NUMBERS

(Pages 368 - 377)

These tables, which give the square and cube roots of numbers to four significant figures, are in the following form:

(a) Square roots of numbers between 1 and 10 and between 10 and 100.

(b) Cube roots of numbers between 1 and 10, between 10 and 100 and between 100 and 1000.

The following examples illustrate the method of obtaining square or cube roots using the tables:

$$\sqrt{839.2}$$

$$\sqrt{4523}$$

$$\sqrt[3]{78\ 620\ 000}$$

$$\sqrt[3]{0.000\ 7247}$$

1. Change the number into scientific notation.

$$= \sqrt{8.392 \times 10^3} = \sqrt{4.523 \times 10^4} = \sqrt[3]{7.862 \times 10^7} = \sqrt[3]{7.247 \times 10^{-4}}$$

2. Adjust the position of the decimal point to make the index of 10 exactly divisible by the root being found.

$$= \sqrt{8.392 \times 10^3} = \sqrt{45.23 \times 10^2} = \sqrt[3]{78.62 \times 10^6} = \sqrt[3]{724.7 \times 10^{-6}}$$

3. Enter the tables shown below and extract the required root of the significant figures.

TABLE OF SQUARE
ROOTS 1-10

TABLE OF SQUARE
ROOTS 10-100

TABLE OF CUBE
ROOTS 10-100

TABLE OF CUBE
ROOTS 100-1000

$$= 2.897$$

$$= 6.725$$

$$= 4.284$$

$$= 8.982$$

4. Determine the square or cube root of the power of 10.

$$\begin{array}{lll} \sqrt{10^2} = 10 & \sqrt{10^2} = 10 & \sqrt[3]{10^6} = 10^2 \\ \therefore \sqrt{839.2} & \therefore \sqrt{45.23} & \therefore \sqrt[3]{78.620\ 000} \\ = 2.897 \times 10 & = 6.725 \times 10 & = 4.284 \times 10^2 \\ \text{or } 28.97 & \text{or } 67.25 & \text{or } 428.4 \end{array} \quad \begin{array}{lll} \sqrt[3]{10^{-6}} = 10^{-2} \\ \therefore \sqrt[3]{0.000\ 7247} \\ = 8.982 \times 10^{-2} \\ \text{or } 0.08982 \end{array}$$

Mean Difference columns are not required in the table of square roots of numbers between 5.5 and 9.9 nor in the tables of cube roots of numbers between 1.0 and 10.0 and between 55.0 and 100.0. When any of the above tables are being used to find the roots of numbers with four significant figures interpolation can be carried out mentally.

II. TABLES FOR CELESTIAL NAVIGATION

A, B & C AZIMUTH TABLES

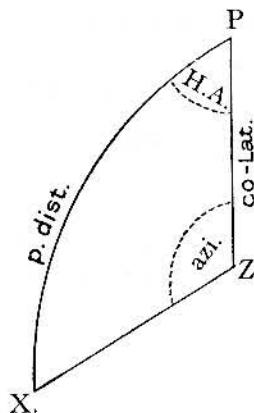
(Pages 380 - 428)

To conform with the method of presenting data in the Nautical Almanac the hour angles in Tables A and B are given in degrees and minutes of arc from $0^\circ 15'$ to $359^\circ 45'$.

If the H.A. is between 0° and 180° the body is west of the meridian and its hour angle will appear in the upper row of H.A.s at either the top or bottom of the page. If the H.A. is between 180° and 360° the body is east of the meridian and its hour angle will appear in the lower row.

The A, B and C values and the azimuth are derived by employing the well known formula which connects four adjacent parts of a spherical triangle. It can be shown, for instance, that in spherical triangle A B C:—

$$\begin{aligned}\cot. a \sin. b &= \cot. A \sin. C + \cos. b \cos. C. \\ \therefore \cot. a \sin. b &= \cos. C \cos. b = \sin. C \cot. A.\end{aligned}$$



The figure shows the astronomical triangle PZX with the four adjacent parts PX, P, PZ and Z representing, in that order, polar distance, hour angle, co-latitude and azimuth.

Applying the above formula to this particular case, we have:—

$$\cot. PX \sin. PZ - \cos. P. \cos. PZ = P. \cot. Z.$$

Dividing by $\sin. P. \sin. PZ$, this becomes—

$$\frac{\cot. PX}{\sin. P} \cdot \frac{\sin. PZ}{\sin. PZ} - \frac{\cos. P}{\sin. P} \cdot \frac{\cos. PZ}{\sin. PZ} = \frac{\sin. P}{\sin. P} \cdot \frac{\cot. Z}{\sin. PZ}$$

$$\begin{aligned} \text{i.e. } \cot. PX & \quad \frac{\sin. PZ}{\sin. PZ} - \frac{\cos. PZ}{\sin. PZ} = \frac{\cot. Z}{\sin. PZ}, \\ \text{or } \tan. \text{ decl.} & \quad \cot. P - \cot. P \quad \cot. PZ = \cot. Z \quad \cosec. PZ, \\ & \quad \cosec. H.A. - \cot. H.A. \tan. \text{ lat.} \\ & \qquad \qquad \qquad = \cot. \text{ azi. sec. lat.} \end{aligned}$$

In the tables:—

$\cot. H.A. \tan. \text{ lat.}$ is tabulated as A, and $\tan. \text{ decl. cosec. H. A.}$ is tabulated as B.
Hence $(A \pm B) \cos. \text{ lat.} = \cot. \text{ azimuth.}$

$(A \pm B)$, referred to for convenience as 'C', forms the primary argument in Table C with lat. as the secondary argument. With these two arguments the azimuth is found.

As an example, consider the case where hour angle = 48° , lat. = 52° N., and decl. = 15° N.

lat. 52° 00' N	L. tan. 0.10719		
H.A. 48° 00'	L. cot. 9.95444		
decl. 15° 00' N	+	+	
			L. cosec. 0.12893
			L. tan. 9.42805
	Log. A 0.06163	Log. B 9.55698	
(page 394-395)	$\therefore A = 1.153 S.$		$B = 0.361 N.$

(A is named opposite to lat.; B has the same name as decl.) $(A \pm B) = 'C' = 0.792 S.$ (Same name as A which is numerically greater than B).

'C' 0.792 S.	Log.	9.89873	if HA is between 0° and 180°
lat. 52° 00' N.	L. cos.	9.78934	
Azi. 64° 00'	HA < 180°	L. cot.	
		9.68807	
		$\therefore \text{Azimuth} = S. 64^\circ W.$ or $244^\circ.$	

(The azimuth takes the names of the 'C' factor and hour angle.) (page 394-395)

Reference to the tables will show that for the above data $A = 1.15 S.$ and $B = 0.36 N.$ The combination of these is $0.79 S.$, which in Table C with lat. 52° gives azimuth $S. 64^\circ 2' W.$

The rules for naming and combining A and B and for naming the azimuth are given on each page of the appropriate table. It is important that they should be applied correctly.

Longitude Correction

The quantity $(A \pm B)$ or 'C', besides being one of the arguments for finding the azimuth from table C, is also the 'longitude correction factor' or the error in longitude due to an error of 1' of latitude. This can often be very useful to those accustomed to working sights by the longitude method.

A simple sketch showing the direction of the position line will at once make it clear which way the longitude correction should be applied. It will easily be apparent that when working a sight by the longitude method:—

(a) when the position line lies N.E./S.W. (body in N.W. or S.E. quadrant), if the assumed latitude is too far north the computed longitude will be too far east, and if the latitude is too far south the longitude will be too far west;

(b) when the position line lies N.W./S.E. (body in N.E. or S.W. quadrant) the reverse holds good.

Example: Suppose a sight worked with lat. $49^\circ 06' N.$ gives longitude $179^\circ 46' 0 W.$ and azimuth $S. 70^\circ 5 E.$, the value of 'C' being 0.54 . If the correct latitude turned out to be $49^\circ 46' N.$, i.e. $40'$ error, the error in longitude would be 40×0.54 or 21.6 . We should therefore have:—

Computed long.	179° 46' 0 W.
Correction	21' 6 E.
Correct long.	179° 24' 4 W.

This is a case where the latitude being too far south, the computed longitude is too far west.

Examples on the use of the tables

In each of the following cases find the longitude correction factor and the true azimuth.

Example 1: H.A. 310° , lat. 48° N., decl. 20° N.

From Table A with H.A. 310° , lat. 48° N., $A = 0.93$ S.

From Table B with H.A. 310° , decl. 20° N., $B = 0.48$ N.

page 394 - 395

Long. corr'n. factor = $A - B = \underline{\underline{C}} = 0.45$ S.

From Table C with $C 0.45$ S., lat. 48° N., T. Azi. = $S. 73^\circ 2 E.$

A is named S. opposite to lat. because H.A. is *not* between 90° and 270° .

B is named N. because the decl. is N.

$C = A - B$ as A and B have different names, and is named S. as the greater quantity is S. The azimuth is named S. because C is S., and E. because H.A. is between 180° and 360° .

Example 2: H.A. 244° , lat. 41° S., decl. 5° S.

From Table A with H.A. 244° , lat. 41° S., $A = 0.42$ S.

From Table B with H.A. 244° , decl. 5° S., $B = 0.10$ S.

Long. corr'n. factor = $A + B = \underline{\underline{C}} = 0.52$ S.

From Table C with $C 0.52$ S., lat. 41° S., T. Azi. = $S. 68^\circ 6 E.$

A is named S. same as lat. because H.A. is between 90° and 270° .

B is named S. because the decl. is S.

$C = A + B$ as A and B have the same name (both S.).

The azimuth is named S. because C is S., and E. because H.A. is between 180° and 360° .

Example 3: H.A. 108° , lat. 61° N., decl. 20° N.

From Supplementary Table A with H.A. 108° , lat. 61° N., $A = 0.59$ N.

From Table B with H.A. 108° , decl. 20° N., $B = 0.38$ N.

Long. corr'n. factor = $A + B = \underline{\underline{C}} = 0.97$ N.

From Table C with $C 0.97$ N., lat. 61° N., T. Azi. = $N. 64^\circ 8 W.$

A is named N. same as lat. because H.A. is between 90° and 270° .

B is named N. because the decl. is N.

$C = A + B$ as A and B have the same name (both N.).

The azimuth is named N. because C is N., and W. because H.A. is between 0° and 180° .

Use of ABC Tables for Great Circle Sailing

These tables provide a ready means of finding the initial great circle course from one point to another. Suppose, for example, the initial course from P ($49^\circ 30' N.$, $5^\circ 00' W.$) to Q ($46^\circ 00' N.$, $53^\circ 00' W.$) is required. The procedure is simply to treat d. long. as hour angle, lat. of P. as latitude, and lat. of Q as declination. Thus:-

From Table A with H.A. 48° , lat. $49^\circ 30' N.$, $A = 1.06$ S. (pg 394)
From Table B with H.A. 48° , decl. $46^\circ 00' N.$, $B = 1.39$ N. (pg 395)

$A - B = \underline{\underline{C}} = 0.33$ N. (pg 412)

From Table C with $C 0.33$ N., lat. $49^\circ 30' N.$, T. Azi. = $N. 77^\circ 9 W.$

i.e. Initial G.C. Course = $N. 77^\circ 9 W.$ or $282^\circ 1$.

The final course, if required, may be obtained in a similar way by finding the initial course from Q to P and reversing it.

AMPLITUDES and CORRECTIONS

(Explanation with Table)
(Pages 429 - 431)

EX-MERIDIAN TABLE I

(Pages 432 - 443)

'A' is the change in the altitude of a body in seconds of arc during the minute of time immediately preceding or following meridian passage. It is tabulated for latitudes to 83° and declinations to 63° .

This table is in two sections:-

- (i) Latitude and Declination SAME NAME. On page 432 - 435 there are bands in which the value of 'A' is omitted. This is because 'A' changes too rapidly for accurate interpolation to be possible, when the body is near the zenith.
- (ii) Latitude and Declination DIFFERENT NAME. 'A' for Lower Transit observation is tabulated on the lower parts of pages 440 - 442 of this section and on page 443, although the latitude and declination are of the same name.

'A' is computed using the formula:-

$$A = \frac{1.9635 \times \cos \text{lat} \times \cos \text{dec}}{\sin (\text{lat} \pm \text{dec})}$$

In the denominator the latitude and declination are:-

- (a) subtracted at Upper Transit if of the same name;
- (b) added at Upper Transit if of different name;
- (c) subtracted at Lower Transit.

EX-MERIDIAN TABLE II

(Pages 444 - 447)

The Reduction is the product of 'A' from Table I and the square of the time in minutes that the body is East or West of the meridian. To obtain the True Meridian Altitude, the Reduction is added to the True Altitude of Upper Transit observations and subtracted from the True Altitude of Lower Transit observations of circumpolar bodies.

The table is entered with 'A' and the Local Hour Angle for Upper Transit observations or 'A' and $(180 - \text{LHA})$ for Lower Transit observations. If the interpolated value of 'A' from Table I is to one or two decimal places, the Reduction can be obtained to a corresponding accuracy by moving the decimal point the appropriate number of places as shown in the example below:

'A' = 2.45 ; Local Hour Angle = $354^{\circ} 00'$

From the column headed $354^{\circ} 00'$:-

Reduction for 2.0 = 19.2

0.4 = 3.84 (extract the value for 4" and move the decimal point one place)

0.05 = 0.48 (extract the value for 5" and move the decimal point two places)

Reduction for 2.45 = 23.52

Example 1: In D.R. Lat. $48^{\circ} 13' N.$, D.R. Long. $7^{\circ} 20' W.$, the True Altitude of the sun was $19^{\circ} 52'$. Sun's LHA $356^{\circ} 00'$. Declination $21^{\circ} 39' S.$ Determine the Position Line.

Table I (Different Name)	Table II LHA $356^{\circ} 00'$	T. Alt. Reduction	$19^{\circ} 52' \cdot 0 S.$ $5' \cdot 6$
Lat. $48^{\circ} 13' N.$	A = $1^{\circ} \cdot 3$	T. Mer. Alt.	$19^{\circ} 57' \cdot 6 S.$
Decl. $21^{\circ} 39' S.$	Red for. $1^{\circ} \cdot 0 = 4' \cdot 3$	T. Mer. Z. Dist.	$70^{\circ} 02' \cdot 4 N.$
A = $1^{\circ} \cdot 3$	" " $\cdot 3 = 1' \cdot 3$	Decl.	$21^{\circ} 39' \cdot 0 S.$
(page 433)	Reduction = $5' \cdot 6$	Lat.	$48^{\circ} 23' \cdot 4 N.$
	(page 444)	True Azimuth from Az. Tables 176°	

Position Line passes 086° and 266° through Lat. $48^{\circ} 23' \cdot 4 N.$, Long. $7^{\circ} 20' W.$

Example 2: D.R. Lat. $42^{\circ} 12' N.$, D.R. Long. $24^{\circ} 32' W.$, the True Altitude of Antares was $21^{\circ} 28'$. Star's LHA $357^{\circ} 00'$. Declination $26^{\circ} 18' \cdot 0 S.$ Determine the Position Line.

Table I (Different Name)	Table II LHA $357^{\circ} 00'$	T. Alt. Reduction	$21^{\circ} 28' \cdot 0 S.$ $3' \cdot 4$
Lat. $42^{\circ} 12' N.$	A = $1^{\circ} \cdot 4$	T. Mer. Alt.	$21^{\circ} 31' \cdot 4 S.$
Decl. $26^{\circ} 18' S.$	Red. for $1^{\circ} \cdot 0 = 2' \cdot 4$	T. Mer. Z. Dist.	$68^{\circ} 28' \cdot 6 N.$
A = $1^{\circ} \cdot 4$	" " $\cdot 4 = 0' \cdot 96$	Decl.	$26^{\circ} 18' \cdot 0 S.$
	Reduction = $3' \cdot 36$	Lat.	$42^{\circ} 10' \cdot 6 N.$
		True Azimuth from Az. Tables 177°	

Position Line passes 087° and 267° through Lat. $42^{\circ} 10' \cdot 6 N.$, Long. $24^{\circ} 32' W.$

Although the latitude and declination of a circumpolar body are always of the same name, 'A' for Lower Transit observations is tabulated in the lower part of the "Latitude and Declination Different Name" section of Table I.

When near its Lower Transit the Local Hour Angle is less than 180° when west of the meridian and more than 180° when east of it. The Hour Angle to use when entering Table II in this case is ($180^{\circ} - LHA$).

Example 3: D.R. Lat. $42^{\circ} 10' N.$, Long. $21^{\circ} 30' W.$, the True Altitude of Dubhe was $14^{\circ} 20'$. Star's LHA $176^{\circ} 30'$. Declination $62^{\circ} 01' N.$ Determine the Position Line.

Table I (Same Name)	Table II LHA $176^{\circ} 30'$	T. Alt. Reduction	$14^{\circ} 20' \cdot 0$ $-2' \cdot 3$
Lat. $42^{\circ} 10' N.$	A = $0^{\circ} \cdot 7$	T. Mer. Alt.	$14^{\circ} 17' \cdot 7$
Decl. $62^{\circ} 01' N.$	Reduction = $2' \cdot 29$	Polar Dist.	$27^{\circ} 59' \cdot 0$
A = $0^{\circ} \cdot 7$	For Lower Transit— $2' \cdot 3$	Lat.	$42^{\circ} 16' \cdot 7 N.$
		True Azimuth from Az. Tables 358°	

Position Line passes 088° and 268° through Lat. $42^{\circ} 16' \cdot 7 N.$, Long. $21^{\circ} 30' W.$

Example 4: D.R. Lat. $50^{\circ} 02'$ S., D.R. Long. $67^{\circ} 20'$ W., the True Altitude of Achernar was $17^{\circ} 20'$. Star's LHA $184^{\circ} 20'$. Declination $57^{\circ} 29'$ S. Determine the Position Line.

Table I (Same Name)	Table II	T. Alt.	$17^{\circ} 20' 0$
	LHA $184^{\circ} 20'$ = $4^{\circ} 20'$	Reduction	$-3' 5$
Lat. $50^{\circ} 02'$ S.	A = $0' 7$	T. Mer. Alt.	$17^{\circ} 16' 5$
Decl. $57^{\circ} 29'$ S.	Reduction = $3' 5$	Polar Dist.	$32^{\circ} 31' 0$
	For Lower Transit— $3' 5$		
A = $0'' 7$		Lat.	$49^{\circ} 47' 5$ S.
		True Azimuth from Az. Tables	177.5°

Position Line passes $087^{\circ} 5$ and $267^{\circ} 5$ through $49^{\circ} 47' 5$ S., Long. $67^{\circ} 20'$ W.

EX-MERIDIAN TABLE III

(Page 448)

This Table contains a Second Correction, which, when the amount of the Main Correction is considerable, enables the process of Reduction to Meridian to be applied with advantage on much larger hour angles than could otherwise be the case.

Example: D.R. Lat. $31^{\circ} 00'$ N., D.R. Long. $124^{\circ} 00'$ W., the True Altitude of the Sun was $55^{\circ} 01'$. Sun's LHA $347^{\circ} 30'$. Declination $2^{\circ} 00'$ S. Determine the Position Line.

Table I (Different Name)	Table II	T. Alt.	$55^{\circ} 01' 0$ S.
	LHA $347^{\circ} 30'$	1st Correction	$2^{\circ} 09' 2 +$
	A = $3' 1$	2nd Correction	$3' 6 -$
Lat. $31^{\circ} 00'$ N.	Red. for $3' 0 = 125' 0$		
Decl. $2^{\circ} 00'$ S.	" " $1 = 4' 2$	T. Mer. Alt.	$57^{\circ} 06' 6$ S.
A = $3'' 1$		T. Mer. Z. Dist.	$32^{\circ} 53' 4$ N.
	1st Correction = $129' 2$	Decl.	$2^{\circ} 00' 0$ S.
Entering Table III with $129'$ as First Correction and 56° as Altitude we have $3' 6'$ Subtractive for Second Correction.		Lat.	$30^{\circ} 53' 4$ N.
		True Azimuth from Az. Tables	158°

Position Line passes 068° and 248° through Lat. $30^{\circ} 53' 4$ N., Long. $124^{\circ} 00'$ W.

EX-MERIDIAN TABLE IV

(Page 448)

This Table gives the limits of Hour Angle or Time before or after the time of the Meridian Passage when an Ex-Meridian observation can be taken. When the observation is taken within the time limit prescribed by this Table the Second Correction from Table III is negligible. The Table is entered with 'A' taken from Table I.

Given Lat. 37° N., Declination 18° N., find the limits of Hour Angle for taking an Ex-Meridian observation.

For Lat. 37° and Declination 18° , 'Same Name', Table I gives $4'' 6$ for 'A'. Entering Table IV with $4'' 6$ as 'A', the time limit abreast is found to be 24 minutes.

CHANGE of HOUR ANGLE with ALTITUDE

(Pages 449 - 450)

The formula used in calculating the values tabulated is:—

Change of H.A. (in mins.) due to 1' change of Alt. = cosec. Az. sec. Lat.

The table gives in minutes of arc the error in hour angle resulting from an altitude 1' in error. This is of particular value to those navigators who work their sights by the 'Longitude by Chronometer' method. It will be seen that the error is least in the case of a body on the prime vertical and that it increases as the azimuth decreases—very rapidly as the azimuth becomes very small. From the table the observer can readily find the least azimuth on which the altitude of a body should be observed in order that the resulting longitude may not exceed a chosen limit of error. Another use to which this table can be put is to find the correct longitude when a sight has been worked using an altitude in error by a known amount.

Page 449
Example 1: In latitude 18° what should be the lowest value of azimuth in order that an error of 1' in the altitude may not produce more than 2' of error in the computed longitude?

Under lat. 18° and against azi. 32°, the error for 1' of alt. is found to be 1'.98. Accordingly, the observation should be taken on a bearing greater than 32°.

(In lat. 36°, it will be seen, an azimuth of about 39° would constitute the limit. In lat. 63° the error would exceed 2' even when the body was on the P.V.)

Example 2: A sight worked in lat. 54° by the 'Longitude Method' resulted in a deducted longitude of 64° 14'.5 W. and azimuth N. 65° E. Afterwards it was discovered that the sextant index error of 2' 30" off the arc had been applied the wrong way. Find the correct longitude.

Since the longitude is found by comparing the L.H.A. of the body with its G.H.A., it is evident that the error in the L.H.A. will be the error in the computed longitude. The index error of 2'.5, which should have been added, was subtracted, so that the altitude used was 5' too small.

The table shows that in lat. 54°, when the azi. is 65°, the error in H.A. is 1'.88 per 1' of alt. For 5', therefore, the error will be $5 \times 1'.88 = 9'.40$.

As the real altitude was greater than the value used, the observer must be *nearer* to the body than his computed longitude would lead him to suppose. With an *easterly* azimuth this means that the *Westerly* L.H.A. should be greater, and therefore the observer's west longitude should be smaller. Hence:—

Computed long.....	64° 14'.5W.
Error	9'.4 to subtract
Correct long.	<u>64° 05'.1W</u>

It will be appreciated that this is much quicker than re-working the sight.

CHANGE OF ALTITUDE IN ONE MINUTE OF TIME

(Pages 451 - 452)

This Table contains the change in the altitude of a celestial body in minutes and tenths of arc in one minute of time. It is useful for finding the correction to be applied to the computed altitude of a heavenly body when the time of observation differs from that used in the computation of the altitude. When the star is East of the Meridian the correction from the Table is subtractive from the computed altitude if the time of observation is earlier than that used in the computation of the

altitude; it is additive if the time of observation is later. When the star is West of the meridian the correction is additive if the time of observation is before that used when computing the altitude, it is subtractive if the time of observation is after.

Formula

Change of altitude in one minute of time = $15' \sin. Az. \cos. Lat.$

The change in 6 seconds of time is found by shifting the decimal point one place to the left.

The change in 1 second of time is found by calling the quantities in the Table seconds instead of minutes.

Example: In Lat. $51^{\circ} 30'$ N. on the Meridian of Greenwich on October 26th, 1925 at 8 h. 0 m. p.m. the computed altitude of the star *Altair* was $37^{\circ} 09' 2$. Find the true altitude at 8 h. 10 m. p.m., the Az. being $S.49^{\circ} 37' W.$ Opposite 52° in the Lat. Col. and under 50° in the Az. Col. is $7'1$ of arc which is the change of altitude in 1 min. of time, and $7'1 \times 10$ minutes gives $71'$ or $1^{\circ} 11'$, which is the correction to apply to the computed altitude.

<i>(Page 452)</i>	Computed Alt.	$37^{\circ} 09' 2$
	Corr. to Subt.	$1^{\circ} 11' 0$
	True Alt. required	$35^{\circ} 58' 2$

DIP of the SEA HORIZON

(Page 453)

The tabulated values are derived from the formula—Dip (in minutes) = $1.76\sqrt{h}$ where h = height of eye in metres. Thus, for example, when $h = 30$ m (98 ft), dip. = $9'6$.

Heights of eye are given in metres, ranging from 0.5 m to 50.0 m and also in the equivalent feet (1.5 ft to 164 ft).

MONTHLY MEAN OF THE SUN'S SEMIDIAMETER AND SUN'S PARALLAX IN ALTITUDE

(Page 453)

Correction for parallax is to be taken out opposite the Sun's Altitude and is always *additive*.

Example: The sun's parallax corresponding to 51° of altitude is $0'1$.

AUGMENTATION OF THE MOON'S SEMIDIAMETER

(Page 453)

REDUCTION OF THE MOON'S PARALLAX

(Page 453)

MEAN REFRACTION

(Page 454)

This table contains the Refraction of the heavenly bodies, in minutes and decimals at a mean state of the atmosphere, and corresponding to their apparent altitudes. This correction is always to be *subtracted* from the apparent altitude of the object.

Example: The mean refraction for the apparent altitude $10^{\circ} 50'$, is $4\cdot 9$.

Caution: For low altitudes all refraction tables are more or less inaccurate.

ADDITIONAL REFRACTION CORRECTIONS

(Page 454)

The mean refraction values given in the Mean Refraction table are for an atmospheric pressure of 1,000 mb (29·5 in) and an air temperature of 10°C (50°F). If the atmospheric pressure or temperature differ from these values additional corrections must be applied to the apparent altitude. These corrections are contained in the tables 'Additional Refraction Corrections for Atmospheric Pressure' and 'Additional Refraction Corrections for Air Temperature'.

Example: Find the true altitude of the sun when the observed altitude of the sun's lower limb was $6^{\circ} 00'$, height of eye 26 m (85 ft), atmospheric pressure 1020 mb (30·1 in), air temperature 0°C (32°F).

Observed altitude sun's lower limb	=	$6^{\circ} 00'$
Total correction	=	$0^{\circ}-01\cdot 5'$
		<hr/>
True altitude	=	$5^{\circ} 58\cdot 5'$
Correction for temperature	=	$-0\cdot 4'$
Correction for pressure	=	$-0\cdot 2'$
		<hr/>
Corrected altitude	=	$5^{\circ} 57\cdot 9'$

If the altitude is greater than $5^{\circ} 00'$ the error due to applying these corrections to the true altitude can be ignored in practice.

N.B.—To convert barometer readings from mercury inches to millibars, or vice-versa, see page 499. To convert temperatures from Fahrenheit to Celsius, or vice-versa, see page 494.

The adjustment of mean refraction as shown above is important only when the altitude is small. It should be borne in mind that on account of uncertain refraction position lines obtained from sights taken when the altitude of the body is less than 10° or so should not be relied upon implicitly. Moreover, due to the effect of atmospheric refraction on dip it is unwise to place too much reliance on sights taken, whatever the altitude, when there is cause for abnormal refraction to be suspected.

CORRECTION of MOON'S MERIDIAN PASSAGE

(Page 455)

The correction obtained from this table is to be applied to the time of meridian passage given in the Nautical Almanac (i.e. the time of transit at Greenwich) in order to find the time of the local transit according to the observer's longitude.

$$\text{Correction} = \frac{D \times \text{longitude}}{360} \quad \text{where } D \text{ is the difference between the times of successive transits.}$$

When the observer is in *East* longitude, D is the difference between the time of transit on the day of observation and the time of transit on the *preceding* day. When in *West* longitude it is the difference between the times on the day of observation and the *following* day.

Example: From Naut. Alm. L.M.T. of moon's upper transit at Greenwich is:—

	h. m.	
1st July	18 44	diff. 48m.
2nd July	19 32	diff. 53m.
3rd July	20 25	

Find G.M.T. of moon's upper transit on 2nd July (a) in longitude 156° E., (b) in longitude 63° W.

	July	h.	m.
(a) L.M.T. of transit at Greenwich	2	19	32
Corr'n. for D 48m., long. 156° E.			-20.8
L.M.T. of local transit	2	19	11.2
East longitude in time units		-10	24
G.M.T. of local transit (156° E.)	2	8	47.2
	July	h.	m.
(b) L.M.T. of transit at Greenwich	2	19	32
Corr'n. for D 53m., long. 63° W.			+9.2
L.M.T. of local transit	2	19	41.2
West longitude in time units		+4	12
G.M.T. of local transit (63° W.)	2	23	53.2

SUN'S TOTAL CORRECTION

(Pages 456–461 and Inside Front Cover)

This is a combined table for the correction of both Lower Limb and Upper Limb altitudes of the Sun. To simplify interpolation for intermediate altitudes and heights of eye, the tabulation is based on columnar and linear correction differences of 0.2.

The corrections in the main table give the combined effect of dip, refraction, parallax in altitude and an assumed semi-diameter of 16.0. Subsidiary corrections at the foot of the table give the monthly variations of the semi-diameter from the assumed value of 16.0. The corrections and subsidiary corrections are added to or subtracted from the observed altitude as shown in the table.

Example 1

Obs. Alt. Sun's L.L.	=	24 57.2
Corrn. for obs. alt. 25 and H.E. 12.0m	=	+ 8.0
		+ 0.1
True Alt. of Sun's centre	=	25 05.3

Example 2

Obs. Alt. Sun's U.L.	=	33 45.6
Corrn. for obs. alt. 34 and H.E. 19.7m	=	- 24.7
Subsidiary corrn. for June	=	+ 0.2
True Alt. of Sun's centre	=	33 20.7

(Page 458)

(Page 459)

STAR'S TOTAL CORRECTION

(Pages 462–465 and Inside Back Cover)

This table corrects the combined effects of dip and refraction. To simplify interpolation for intermediate altitudes and heights of eye, the table is based on columnar and linear correction differences of 0'.2.

This table can also be used for the correction of observed altitudes of the planets, but in the case of Venus and Mars the small additional correction given in the Nautical Almanac for parallax and phase may be necessary. The size of these corrections vary with the date and the altitude of the planet.

MOON'S TOTAL CORRECTION

(Lower Limb – pages 466–478; Upper Limb – pages 479–491)

This table corrects the combined effects of dip, atmospheric refraction, augmented semi-diameter and parallax in altitude. The dip component used in the main table is a constant 12'.3, therefore the subsidiary correction given at the foot of the pages must be added to the main correction. The argument for this subsidiary correction is the observer's height of eye.

No account has been taken of the reduction with latitude of the moon's horizontal parallax, but in general this is of no practical significance. In cases where a high degree of accuracy is required it will be necessary to apply the corrections separately together with the adjustment of the refraction correction for the prevailing atmospheric pressure and temperature.

The main corrections are ALWAYS added to both the lower limb and upper limb observed altitudes of the moon, the dip correction is then added and for upper limb observations 30' must be subtracted from the result.

Example 1

$$\text{Moon's Hor. Pax. (from N. Alm.)} = 57'.5$$

Obs. Alt. moon's lower limb	=	38°47'.4
Correction from main table	=	+ 47'.1
Correction for height of eye 13.5m	=	+ 5'.8
True altitude of moon	=	39°40'.3

Example 2

$$\text{Moon's Hor. Pax. (from N. Alm.)} = 59'0$$

Obs. Alt. moon's upper limb	=	69°36'.0
Correction from main table	=	+ 22'.0
Correction for height of eye 33m	=	+ 2'.2
		70°00'.2
		- 30'
True altitude of moon	=	69°30'.2

(Page 471)

III. TABLES FOR COASTAL NAVIGATION

DAY'S RUN - AVERAGE SPEED TABLE

(Pages 494-500)

This table provides a rapid means of finding the average speed directly from the arguments 'steaming time' and 'distance run'. It will be appreciated that there is no necessity to convert minutes into decimals of a day, and that no logarithms or co-logarithms are required. Simple addition is all that is needed.

The scope of the table has been made wide enough to cover cases of high speed vessels (up to 40 knots or so) on easterly or westerly courses in high latitudes where change of longitude between one local noon and the next may amount to some 30° , or 2 hours of time.

Distances are tabulated as multiples of 100 miles. Increments of speed for multiples of 10 miles and multiples of 1 mile are obtained simply by shifting the decimal point one or two places to the left, respectively.

Example: Given steaming time 23 h. 29 m., distance 582 miles, find the average speed.

Distance in miles	Speed in knots
500	21.291
80*	3.4066
2†	0.08517
582	24.78277

That is, average speed correct to two places of decimals, which are generally considered sufficient, is 24.78 knots.

* Enter with 800 miles and shift decimal point 1 place to the left

† Enter with 200 miles and shift decimal point 2 places to the left

RADAR RANGE TABLE

(Page 501)

RADAR PLOTTER'S SPEED AND DISTANCE TABLE

(Page 502)

MEASURED MILE SPEED TABLE

(Pages 503-509)

This table is arranged in 'critical table' form and gives speeds correct to the nearest hundredth of a knot without interpolation. If the time argument is an exact tabulated value, the speed immediately above it should be taken.

1. If the time recorded for the measured mile is 9 m. 16·2 s., the speed is 6·47 knots.
2. If the time is 4 m. 55·3 s., the speed is 12·19 knots.
3. If the time is 3 m. 52·3 s., the speed is 15·49 knots.
4. Suppose a ship on trials makes six runs over a measured mile, three against the tide and three with the tide, such that the timings by stop-watch are as follows:—

	m. s.
First run against tide	3 28·8
First run with tide.....	3 18·4
Second run against tide	3 30·0
Second run with tide	3 17·8
Third run against tide	3 31·1
Third run with tide	3 16·7
Then total time for 6 miles is	20 22·8
∴ Average time for 1 mile is	3 23·8

From the table the average speed for the six runs is 17·66 knots.

Strictly speaking, the average speed should be computed by finding the 'mean of means', in which case the work would be arranged as follows.

RUN	m.	SPEED KNOTS	1ST MEAN	2ND MEAN	3RD MEAN	4TH MEAN	MEAN OF MEANS
1st	3	28·8	17·24	17·690			
2nd	3	18·4	18·14	17·640	17·6650		
3rd	3	30·0	17·14	17·670	17·6550	17·655625	
4th	3	17·8	18·20	17·625	17·6475	17·650000	17·6528125
5th	3	31·1	17·05		17·6500		
6th	3	16·7	18·30	17·675			
			6) 106·07	4) 70·6175			
			17·68	17·6544			
			Ordinary mean speed	Ordinary mean of second means*			True mean speed

At speeds greater than about $19\frac{1}{2}$ knots it will be noticed that in certain cases a change of a tenth of a second in the time will make a difference of more than one hundredth of a knot in the tabulated speed. For example, if the time for one mile is between 2 m. 38·7 s. and 2 m. 38·8 s. the speed, correct to two places of decimals, could be either 22·68 or 22·67 knots.

In very high speed vessels the recorded time for a measured mile may be so small as to be beyond the scope of the table. Even so, a reasonably accurate speed is easily obtained by entering the table with double the recorded time, and then doubling the speed so obtained. For instance, if a mile is run in 1 m. 55·2 s., enter with 3 m. 50·4 s. This gives 15·62 knots which is half the required speed of 31·24 knots (and this will be correct within 0·02 of a knot). By calculation the correct speed is actually 31·250 knots.

* This is usually regarded as being sufficiently accurate

Besides its orthodox use for speed trial purposes, the table will be found useful to navigators for other purposes.

For example, suppose it is decided to alter course after the ship has run 6 miles on a certain heading from a position line obtained at 1432, the speed of the ship being 11·75 knots. The table shows that at this speed the ship will run one mile in a little over 5 m. 6 s., or 6 miles in about 30½ minutes. Therefore, the course should be altered at 1502½.

In certain circumstances it might be considered convenient to plot the radar target of another vessel at regular intervals corresponding to one mile runs of one's own vessel. Suppose the speed to be 9·70 knots, which the table shows to correspond to a mile in about 6 m. 11 s. Then, if the stop-watch is started from zero at the time of the first observation, successive observations should be taken as nearly as practicable when the watch shows 6 m. 11 s., 12 m. 22 s., 18 m. 33 s., 24 m. 44 s., and so on.

DISTANCE BY VERTICAL ANGLE

(Pages 510–515)

This table gives the distance of an observer from objects of known height when the angle between base and the summit is known. The tables are for distances up to 7 miles so that the whole object from base to summit will be in view when the height of eye is more than 12 metres (39 feet). Observers whose height of eye is less than this must apply a correction for Dip if their distance from the object exceeds the distance of the sea horizon given for their height of eye in the table Distance of the Sea Horizon (page 486).

The distances given are from the position of the observer to a point at the base vertically below the summit, and it is to this point that the angle should be measured. In places where there is a big rise and fall of tide it would be necessary to make an allowance for the state of the tide, as heights are always given above Mean High Water Springs or Mean Higher High Water. In the case of light-vessels there is no allowance for the state of the tide, as the water plane is always at the same distance with reference to any part of the vessel.

To find the Distance

Measure the angle from summit to base and note the angle; then under the given height find the observed angle, and opposite the angle will be found the distance off in Miles in the left hand column.

Example: The vertical angle between the base and summit of a light-house situated 61 m (200 feet) above sea level was 0° 57'. Required the distance.

Under 61 m (200 ft) and opposite the given angle is 2·0 miles, the distance. (page 512)

To find the Angle to place on the Sextant to pass at a given distance from a Point of Known Height

Opposite the given distance and under the known height will be found the required angle to place on the sextant.

Example: Wishing to pass a point situated 150 m (492 ft) above sea level at a distance of 4 miles, required the angle to place on the sextant.

Opposite 4 miles in the distance column at the *side*, and under 150 m (492 ft) at the *top*, is 1° 10', the angle required to place on the sextant.

EXTREME RANGE TABLE

(Pages 516-517)

This table has been compiled for the purpose of determining the maximum distance at which an object may be seen at sea according to its elevation and that of the observer's eye. Heights are given in metres with their equivalents in feet.

The arguments with which the table is ordinarily entered are the height of the observer's eye and the height of the distant object which last, however, need not be a terrestrial one but may be the masthead of a vessel, or some other easily defined detail thereof, provided always that the height of the feature or object observed be definitely known. The arguments, too, can be made interchangeable, thus, should the lookout, stationed at the masthead at an elevation exceeding 30 metres observe a low-lying rock having a height of less than that amount, then the terms can be substituted for each other and the 'Height of Eye' can be sought in the 'Height of Object' column, and vice versa.

The tables are computed on the basis of normal atmospheric conditions, refraction and visibility, and, in the case of lights, the quantity taken out as 'Extreme Range' presupposes that the light possesses sufficient power to be discernible at such a distance. It must be remembered also that the heights of lights and shore objects are referred to Mean High Water Springs or Mean Higher Water therefore due allowance should be made when the time of observation does not approximate thereto, particularly if the elevation or distance should be small.

Example 1: At what distance will a tower 60 m (197 ft) high be visible to an observer whose eye is elevated 20 m (66 ft) above the water?

Take 60 m (197 ft) as the 'Height of Object' in the marginal column and in the column under 20 m (66 ft) 'Height of Eye', at the top of the page, will be found the 25·6 miles distance.

Example 2: The officer of the watch, whose eye is elevated 16 m (52 ft) above the water, observes a shore light, with an elevation of 45 m (148 ft), just dipping. At what distance is the ship from the light?

In the column headed 16 m (52 ft) 'Height of Eye' and abreast of 45 m (148 ft) 'Height of Object' will be found the distance 22·4 miles.

DISTANCE of the SEA HORIZON

(Page 518)

The tabulations are derived from the formula—Distance of the sea horizon in nautical miles = $2.095 \sqrt{h}$, where h = height of eye in metres. Thus for example, when $h = 50$ m (164 ft) the distance of the sea horizon is 14·8 n. miles.

The following examples show how the table can be used.

Example 1: At what distance in good visibility should an observer whose height of eye is 16 m (52 ft) be able to sight a terrestrial object of height 170 m (558 ft)?

$$\begin{array}{ll} \text{Distance of horizon for height } 16 \text{ m (52 ft)} & = 8.4 \text{ miles} \\ " & " \\ & 170 \text{ m (558 ft)} = 27.3 \text{ miles} \end{array}$$

$$\text{Sum} = \underline{\underline{35.7 \text{ miles}}}$$

Hence, the object should be visible at a distance of 35·7 miles.

Example 2: The range of visibility of a light is stated on a chart to be 21 M. At what distance from the light will an observer be at the moment when the light has just dipped below the horizon if his height of eye is 50 feet?

Charted range, i.e. for 15 feet height of eye	21	miles
Subtracting distance of horizon for height 15 feet	4.55	"
Range of light at sea level	16.45	"
Adding distance of horizon for height 50 feet	8.30	"
Dipping distance, or maximum range to observer	24.75	"

N.B.—This method is applicable only in the case of a light of adequate power, and the accuracy of the result will probably be affected by the fact that the charted height of a light never includes a fraction of a mile. Abnormal refraction will also affect the accuracy of distances obtained by using this table.

DIP OF THE SHORE HORIZON

(Page 519)

When the part of the horizon immediately under the sun is obstructed by land and the observer is near the shore, the Dip for an observed altitude will be greater than that shown in the Dip of the Sea Horizon table. When correcting the altitude the dip should be taken from this table when obtaining the apparent altitude.

Example: The observed altitude of the sun's lower limb above the shore horizon (distance 1.6 miles) was $22^{\circ} 30'$, Height of Eye 12 m (39 ft).

$$\begin{aligned} \text{Observed altitude} &= 22^{\circ} 30' \\ \text{Dip of Shore Horizon} &= -14.7' \quad (\text{H.E.} = 12 \text{ m}, \\ &\qquad\qquad\qquad \text{distance} = 1.6 \text{ miles}) \\ \therefore \text{Apparent altitude} &= 22^{\circ} 15.3' \end{aligned}$$

If the refraction is believed to be abnormal the table should be used with caution.

The table can also be used to obtain the approximate range of a ship by measuring the angle between the ship's waterline and the sea horizon.

Example: The sextant angle between a ship's waterline and the sea horizon is $5.0'$. Height of Eye = 25 m (82 ft).

$$\begin{aligned} \text{From dip of sea horizon table.} \quad \text{Dip} &= 8.8' \\ \text{Observed angle} &= 5.0' \\ \therefore \text{Dip of the ship's waterline} &= 14.8' \\ \therefore \text{From the dip of the shore horizon table, Range} &= 3.5 \text{ miles} \end{aligned}$$

CORRECTION REQUIRED TO CONVERT A RADIO GREAT CIRCLE BEARING TO MERCATORIAL BEARING

(Page 520)

EXPLANATION OF THE TABLES

IV. PHYSICAL AND CONVERSION TABLES

TO CONVERT ARC TO TIME AND TIME TO ARC

(Pages 522-523)

HOURS AND MINUTES TO DECIMAL OF A DAY

(Page 524)

ATMOSPHERIC PRESSURE CONVERSION TABLE

(Page 525)

°FAHRENHEIT - °CELSIUS - °FAHRENHEIT

(Page 526)

SI - BRITISH UNITS

(Pages 527-528)

BRITISH GALLONS - U.S. GALLONS - LITRES

(Pages 529-531)

NAUTICAL MILES, STATUTE MILES, KILOMETRES

(Pages 532-534)

FATHOMS - METRES - FATHOMS

(Page 535)

DECIMAL FRACTIONS OF A DEGREE

(Page 536 and Inside Back Cover)

EXPLANATION OF THE TABLES

V. PORTS OF THE WORLD

PORTS OF THE WORLD. LATITUDES AND LONGITUDES

(Pages 538-595)

This section is an alphabetical list of all the ports of the world used by commercial shipping, the positions given to the nearest minute of latitude and longitude being those of the port area, not the centre of the towns or cities. Every effort has been made to ensure that the names and positions given are correct by checking with charts and reliable official sources and publications.

The user should note the following points:-

- 1 The order of listing is strictly alphabetical and if two or more ports have the same name they are listed in the sub-order of their countries, alphabetically.
- 2 A port which has several commonly used names or whose name has been changed recently is entered under each name with the alternative names in brackets.
- 3 Ports whose names consist of two or more words are entered under each word.
e.g. Port Chalmers is entered under P as Port Chalmers and under C as Chalmers, Port.
- 4 To assist in locating a port its country is given in Anglicised form and where it is considered useful the name of the bay, island, river etc. on which it is sited is given in the form used in its country.
- 5 Accents and diphthongs have been omitted.

TRAVERSE TABLE

17 Degrees

343°
197°017°
163°

1 h 08m

17°

D. Lon	Dep.	D. Lat.	D. Lon	Dep.	D. Lat.	D. Lon	Dep.	D. Lat.	D. Lon	Dep.	D. Lat.	D. Lon	Dep.		
Dist.	D.	Lat.	Dep.	Dist.	D.	Lat.	Dep.	Dist.	D.	Lat.	Dep.	Dist.	D.	Lat.	Dep.
301	287.8	88.0	361	345.2	105.5	421	402.6	123.1	481	460.0	140.6	541	517.4	158.2	
302	288.8	88.3	362	346.2	105.8	422	403.6	123.4	482	460.9	140.9	542	518.3	158.5	
303	289.8	88.6	363	347.1	106.1	423	404.5	123.7	483	461.9	141.2	543	519.3	158.8	
304	290.7	88.9	364	348.1	106.4	424	405.5	124.0	484	462.9	141.5	544	520.2	159.1	
305	291.7	89.2	365	349.1	106.7	425	406.4	124.3	485	463.8	141.8	545	521.2	159.3	
306	292.6	89.5	366	350.0	107.0	426	407.4	124.6	486	464.8	142.1	546	522.1	159.6	
307	293.6	89.8	367	351.0	107.3	427	408.3	124.8	487	465.7	142.4	547	523.1	159.9	
308	294.5	90.1	368	351.9	107.6	428	409.3	125.1	488	466.7	142.7	548	524.1	160.2	
309	295.5	90.3	369	352.9	107.9	429	410.3	125.4	489	467.6	143.0	549	525.0	160.5	
310	296.5	90.6	370	353.8	108.2	430	411.2	125.7	490	468.6	143.3	550	526.0	160.8	
311	297.4	90.9	371	354.8	108.5	431	412.2	126.0	491	469.5	143.6	551	526.9	161.1	
312	298.4	91.2	372	355.7	108.8	432	413.1	126.3	492	470.5	143.8	552	527.9	161.4	
313	299.3	91.5	373	356.7	109.1	433	414.1	126.6	493	471.5	144.1	553	528.8	161.7	
314	300.3	91.8	374	357.7	109.3	434	415.0	126.9	494	472.4	144.4	554	529.8	162.0	
315	301.2	92.1	375	358.6	109.6	435	416.0	127.2	495	473.4	144.7	555	530.7	162.3	
316	302.2	92.4	376	359.6	109.9	436	416.9	127.5	496	474.3	145.0	556	531.7	162.6	
317	303.1	92.7	377	360.5	110.2	437	417.9	127.8	497	475.3	145.3	557	532.7	162.9	
318	304.1	93.0	378	361.5	110.5	438	418.9	128.1	498	476.2	145.6	558	533.6	163.1	
319	305.1	93.3	379	362.4	110.8	439	419.8	128.4	499	477.2	145.9	559	534.6	163.4	
320	306.0	93.6	380	363.4	111.1	440	420.8	128.6	500	478.2	146.2	560	535.5	163.7	
321	307.0	93.9	381	364.4	111.4	441	421.7	128.9	501	479.1	146.5	561	536.5	164.0	
322	307.9	94.1	382	365.3	111.7	442	422.7	129.2	502	480.1	146.8	562	537.4	164.3	
323	308.9	94.4	383	366.3	112.0	443	423.6	129.5	503	481.0	147.1	563	538.4	164.6	
324	309.8	94.7	384	367.2	112.3	444	424.6	129.8	504	482.0	147.4	564	539.4	164.9	
325	310.8	95.0	385	368.2	112.6	445	425.6	130.1	505	482.9	147.6	565	540.3	165.2	
326	311.8	95.3	386	369.1	112.9	446	426.5	130.4	506	483.9	147.9	566	541.3	165.5	
327	312.7	95.6	387	370.1	113.1	447	427.5	130.7	507	484.8	148.2	567	542.2	165.8	
328	313.6	95.9	388	371.0	113.4	448	428.4	131.0	508	485.8	148.5	568	543.2	166.1	
329	314.6	96.2	389	372.0	113.7	449	429.4	131.3	509	486.8	148.8	569	544.1	166.4	
330	315.5	96.5	390	373.0	114.0	450	430.3	131.6	510	487.7	149.1	570	545.1	166.7	
331	316.5	96.8	391	373.9	114.3	451	431.3	131.9	511	488.7	149.4	571	546.1	166.9	
332	317.5	97.1	392	374.9	114.6	452	432.2	132.2	512	489.6	149.7	572	547.0	167.2	
333	318.4	97.4	393	375.8	114.9	453	433.2	132.4	513	490.6	150.0	573	548.0	167.5	
334	319.4	97.7	394	376.8	115.2	454	434.2	132.7	514	491.5	150.3	574	548.9	167.8	
335	320.4	97.9	395	377.7	115.5	455	435.1	133.0	515	492.5	150.6	575	549.9	168.1	
336	321.3	98.2	396	378.7	115.8	456	436.1	133.3	516	493.5	150.9	576	550.8	168.4	
337	322.3	98.5	397	379.7	116.1	457	437.0	133.6	517	494.4	151.2	577	551.8	168.7	
338	323.2	98.8	398	380.6	116.4	458	438.0	133.9	518	495.4	151.4	578	552.7	169.0	
339	324.2	99.1	399	381.6	116.7	459	438.9	134.2	519	496.3	151.7	579	553.7	169.3	
340	325.1	99.4	400	382.5	116.9	460	439.9	134.5	520	497.3	152.0	580	554.7	169.6	
341	326.1	99.7	401	383.5	117.2	461	440.9	134.8	521	498.2	152.3	581	555.6	169.9	
342	327.1	100.0	402	384.4	117.5	462	441.8	135.1	522	499.2	152.6	582	556.6	170.2	
343	328.0	100.3	403	385.4	117.8	463	442.8	135.4	523	500.1	152.9	583	557.5	170.5	
344	329.0	100.6	404	386.3	118.1	464	443.7	135.7	524	501.1	153.2	584	558.5	170.7	
345	329.9	100.9	405	387.3	118.4	465	444.7	136.0	525	502.1	153.5	585	559.4	171.0	
346	330.8	101.2	406	388.3	118.7	466	445.6	136.3	526	503.0	153.8	586	560.4	171.3	
347	331.8	101.5	407	389.2	119.0	467	446.6	136.5	527	504.0	154.1	587	561.4	171.6	
348	332.8	101.7	408	390.2	119.3	468	447.6	136.8	528	504.9	154.4	588	562.3	171.9	
349	333.8	102.0	409	391.1	119.6	469	448.5	137.1	529	505.9	154.7	589	563.3	172.2	
350	334.7	102.3	410	392.1	119.9	470	449.5	137.4	530	506.8	155.0	590	564.2	172.5	
351	335.7	102.6	411	393.0	120.2	471	450.4	137.7	531	507.8	155.2	591	565.2	172.8	
352	336.6	102.9	412	394.0	120.5	472	451.4	138.0	532	508.8	155.5	592	566.1	173.1	
353	337.6	103.2	413	394.9	120.7	473	452.3	138.3	533	509.7	155.8	593	567.1	173.4	
354	338.5	103.5	414	395.9	121.0	474	453.3	138.6	534	510.7	156.1	594	568.0	173.7	
355	339.5	103.8	415	396.8	121.3	475	454.2	138.9	535	511.6	156.4	595	569.0	174.0	
356	340.4	104.1	416	397.8	121.6	476	455.2	139.2	536	512.6	156.7	596	570.0	174.3	
357	341.4	104.4	417	398.7	121.9	477	456.2	139.5	537	513.5	157.0	597	570.9	174.5	
358	342.4	104.7	418	399.7	122.2	478	457.1	139.8	538	514.5	157.3	598	571.9	174.8	
359	343.3	105.0	419	400.7	122.5	479	458.1	140.0	539	515.4	157.6	599	572.8	175.1	
360	344.3	105.3	420	401.6	122.8	480	459.0	140.3	540	516.4	157.9	600	573.8	175.4	
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	
D. Lon	Dep.	D. Lat.	D. Lon	Dep.	D. Lat.	D. Lon	Dep.	D. Lat.	D. Lon	Dep.	D. Lat.	D. Lon	Dep.	D. Lat.	
287°			73 Degrees			073°			107°			4h 52m			
253°															

73°

22°

TRAVERSE TABLE 22 Degrees															
338° 202°				22 Degrees				022° 158°							
D. Lon Dep.				D. Lon Dep.				D. Lon Dep.							
Dist.	D.	Lat.	Dep.	Dist.	D.	Lat.	Dep.	Dist.	D.	Lat.	Dep.				
1	00	9	00	4	61	56	6	22	9	121	112	2	45	3	
2	01	9	00	7	62	57	5	23	2	122	113	1	45	7	
3	02	8	01	1	63	58	4	23	6	123	114	0	46	1	
4	03	7	01	5	64	59	3	24	0	124	115	0	46	5	
5	04	6	01	9	65	60	3	24	3	125	115	9	46	8	
6	05	6	02	2	66	61	2	24	7	126	116	8	47	2	
7	06	5	02	6	67	62	1	25	1	127	117	8	47	6	
8	07	4	03	0	68	63	0	25	5	128	118	7	47	9	
9	08	3	03	4	69	64	0	25	8	129	119	6	48	3	
10	09	3	03	7	70	64	9	26	2	130	120	5	48	7	
11	10	2	04	1	71	65	8	26	6	131	121	5	49	1	
12	11	1	04	5	72	66	8	27	0	132	122	4	49	4	
13	12	1	04	9	73	67	7	27	3	133	123	3	49	8	
14	13	0	05	2	74	68	6	27	7	134	124	2	50	2	
15	13	9	05	6	75	69	5	28	1	135	125	2	50	6	
16	14	8	06	0	76	70	5	28	5	136	126	1	50	9	
17	15	8	06	4	77	71	4	28	8	137	127	0	51	3	
18	16	7	06	7	78	72	3	29	2	138	128	0	51	7	
19	17	6	07	1	79	73	2	29	6	139	128	9	52	1	
20	18	5	07	5	80	74	2	30	0	140	129	8	52	4	
21	19	5	07	9	81	75	1	30	3	141	130	7	52	8	
22	20	4	08	2	82	76	0	30	7	142	131	7	53	2	
23	21	3	08	6	83	77	0	31	1	143	132	6	53	6	
24	22	3	09	0	84	77	9	31	5	144	133	5	53	9	
25	23	2	09	4	85	78	8	31	8	145	134	4	54	3	
26	24	1	09	7	86	79	7	32	2	146	135	4	54	7	
27	25	0	10	1	87	80	7	32	6	147	136	3	55	1	
28	26	0	10	5	88	81	6	33	0	148	137	2	55	4	
29	26	9	10	9	89	82	5	33	3	149	138	2	55	8	
30	27	8	11	2	90	83	4	33	7	150	139	1	56	2	
31	28	7	11	6	91	84	4	34	1	151	140	0	56	6	
32	29	7	12	0	92	85	3	34	5	152	140	9	56	9	
33	30	6	12	4	93	86	2	34	8	153	141	9	57	3	
34	31	5	12	7	94	87	2	35	2	154	142	8	57	7	
35	32	5	13	1	95	88	1	35	6	155	143	7	58	1	
36	33	4	13	5	96	89	0	36	0	156	144	6	58	4	
37	34	3	13	9	97	89	9	36	3	157	145	6	58	8	
38	35	2	14	2	98	90	9	36	7	158	146	5	59	2	
39	36	2	14	6	99	91	8	37	1	159	147	4	59	6	
40	37	1	15	0	100	92	7	37	5	160	148	3	59	9	
41	38	0	15	4	101	93	6	37	8	161	149	3	60	3	
42	38	9	15	7	102	94	6	38	2	162	150	2	60	7	
43	39	9	16	1	103	95	5	38	6	163	151	1	61	1	
44	40	8	16	5	104	96	4	39	0	164	152	1	61	4	
45	41	7	16	9	105	97	4	39	3	165	153	0	61	8	
46	42	7	17	2	106	98	3	39	7	166	153	9	62	2	
47	43	6	17	6	107	99	2	40	1	167	154	8	62	6	
48	44	5	18	0	108	100	1	40	5	168	155	8	62	9	
49	45	4	18	4	109	101	1	40	8	169	156	7	63	3	
50	46	4	18	7	110	102	0	41	2	170	157	6	63	7	
51	47	3	19	1	111	102	9	41	6	171	158	5	64	1	
52	48	2	19	5	112	103	8	42	0	172	159	5	64	4	
53	49	1	19	9	113	104	8	42	3	173	160	4	64	8	
54	50	1	20	2	114	105	7	42	7	174	161	3	65	2	
55	51	0	20	6	115	106	6	43	1	175	162	3	65	6	
56	51	9	21	0	116	107	6	43	5	176	163	2	65	9	
57	52	8	21	4	117	108	5	43	8	177	164	1	66	3	
58	53	8	21	7	118	109	4	44	2	178	165	0	66	7	
59	54	7	22	1	119	110	3	44	6	179	166	0	67	1	
60	55	6	22	5	120	111	3	45	0	180	166	9	67	4	
Dist.	Dep.	D.	Lat.	Dist.	Dep.	D.	Lat.	Dist.	Dep.	D.	Lat.	Dist.	Dep.	D.	Lat.
D. Lon	Dep.	D. Lon	Dep.	D. Lon	Dep.	D. Lon	Dep.	D. Lon	Dep.	D. Lon	Dep.	D. Lon	Dep.	D. Lat.	
292°														68 Degrees	
248°														068°	
														112°	
														4h 32m	

68°

TRAVERSE TABLE

43 Degrees

317°
223°

043°
137°

2 h 52m

43°

D. Lon	Dep.	D. Lat.	Dist.	Dep.	D. Lat.									
D. Lon	Dep.	D. Lat.	Dist.	Dep.	D. Lat.									
301	220.1	205.3	361	264.0	246.2	421	307.9	287.1	481	351.8	328.0	541	395.7	369.0
302	220.9	206.0	362	264.8	246.9	422	308.6	287.8	482	352.5	328.7	542	396.4	369.6
303	221.6	206.6	363	265.5	247.6	423	309.4	288.5	483	353.2	329.4	543	397.1	370.3
304	222.3	207.3	364	266.2	248.2	424	310.1	289.2	484	354.0	330.1	544	397.9	371.0
305	223.1	208.0	365	266.9	248.9	425	310.8	289.8	485	354.7	330.8	545	398.6	371.7
306	223.8	208.7	366	267.7	249.6	426	311.6	290.5	486	355.4	331.5	546	399.3	372.4
307	224.5	209.4	367	268.4	250.3	427	312.3	291.2	487	356.2	332.1	547	400.1	373.1
308	225.3	210.1	368	269.1	251.0	428	313.0	291.9	488	356.9	332.8	548	400.8	373.7
309	226.0	210.7	369	269.9	251.7	429	313.8	292.6	489	357.6	333.5	549	401.5	374.4
310	226.7	211.4	370	270.6	252.3	430	314.5	293.3	490	358.4	334.2	550	402.2	375.1
311	227.5	212.1	371	271.3	253.0	431	315.2	293.9	491	359.1	334.9	551	403.0	375.8
312	228.2	212.8	372	272.1	253.7	432	315.9	294.6	492	359.8	335.5	552	403.7	376.5
313	228.9	213.5	373	272.8	254.4	433	316.7	295.3	493	360.6	336.2	553	404.4	377.1
314	229.6	214.1	374	273.5	255.1	434	317.4	296.0	494	361.3	336.9	554	405.2	377.8
315	230.4	214.8	375	274.3	255.7	435	318.1	296.7	495	362.0	337.6	555	405.9	378.5
316	231.1	215.5	376	275.0	256.4	436	318.9	297.4	496	362.8	338.3	556	406.6	379.2
317	231.8	216.2	377	275.7	257.1	437	319.6	298.0	497	363.5	339.0	557	407.4	379.9
318	232.6	216.9	378	276.5	257.8	438	320.3	298.7	498	364.2	339.6	558	408.1	380.6
319	233.3	217.6	379	277.2	258.5	439	321.1	299.4	499	364.9	340.3	559	408.8	381.2
320	234.0	218.2	380	277.9	259.2	440	321.8	300.1	500	365.7	341.0	560	409.6	381.9
321	234.8	218.9	381	278.6	259.8	441	322.5	300.8	501	366.4	341.7	561	410.3	382.6
322	235.5	219.6	382	279.4	260.5	442	323.3	301.4	502	367.1	342.4	562	411.0	383.3
323	236.2	220.3	383	280.1	261.2	443	324.0	302.1	503	367.9	343.0	563	411.8	384.0
324	237.0	221.0	384	280.8	261.9	444	324.7	302.8	504	368.6	343.7	564	412.5	384.6
325	237.7	221.6	385	281.6	262.6	445	325.5	303.5	505	369.3	344.4	565	413.2	385.3
326	238.4	222.3	386	282.3	263.3	446	326.2	304.2	506	370.1	345.1	566	413.9	386.0
327	239.2	223.0	387	283.0	263.9	447	326.9	304.9	507	370.8	345.8	567	414.7	386.7
328	239.9	223.7	388	283.8	264.6	448	327.6	305.5	508	371.5	346.5	568	415.4	387.4
329	240.6	224.4	389	284.5	265.3	449	328.4	306.2	509	372.3	347.1	569	416.1	388.1
330	241.3	225.1	390	285.2	266.0	450	329.1	306.9	510	373.0	347.8	570	416.9	388.7
331	242.1	225.7	391	286.0	266.7	451	329.9	307.6	511	373.7	348.5	571	417.6	389.4
332	242.8	226.4	392	286.7	267.3	452	330.6	308.3	512	374.5	349.2	572	418.3	390.1
333	243.5	227.1	393	287.4	268.0	453	331.3	308.9	513	375.2	349.9	573	419.1	390.8
334	244.3	227.8	394	288.2	268.7	454	332.0	309.6	514	375.9	350.5	574	419.8	391.5
335	245.0	228.5	395	288.9	269.4	455	332.8	310.3	515	376.6	351.2	575	420.5	392.1
336	245.7	229.2	396	289.6	270.1	456	333.5	311.0	516	377.4	351.9	576	421.3	392.8
337	246.5	229.8	397	290.3	270.8	457	334.2	311.7	517	378.1	352.6	577	422.0	393.5
338	247.2	230.5	398	291.1	271.4	458	335.0	312.4	518	378.8	353.3	578	422.7	394.2
339	247.9	231.2	399	291.8	272.1	459	335.7	313.0	519	379.6	354.0	579	423.5	394.9
340	248.7	231.9	400	292.5	272.8	460	336.4	313.7	520	380.3	354.6	580	424.2	395.6
341	249.4	232.6	401	293.3	273.5	461	337.2	314.4	521	381.0	355.3	581	424.9	396.2
342	250.1	233.2	402	294.0	274.2	462	337.9	315.1	522	381.8	356.0	582	425.6	396.9
343	250.9	233.9	403	294.7	274.8	463	338.6	315.8	523	382.5	356.7	583	426.4	397.6
344	251.6	234.6	404	295.5	275.5	464	339.3	316.4	524	383.2	357.4	584	427.1	398.3
345	252.3	235.3	405	296.2	276.2	465	340.1	317.1	525	384.0	358.0	585	427.8	399.0
346	253.0	236.0	406	296.9	276.9	466	340.8	317.8	526	384.7	358.7	586	428.6	399.7
347	253.8	236.7	407	297.7	277.6	467	341.5	318.5	527	385.4	359.4	587	429.3	400.3
348	254.5	237.3	408	298.4	278.3	468	342.3	319.2	528	386.2	360.1	588	430.0	401.0
349	255.2	238.0	409	299.1	278.9	469	343.0	319.9	529	386.9	360.8	589	430.8	401.7
350	256.0	238.7	410	299.9	279.6	470	343.7	320.5	530	387.6	361.5	590	431.5	402.4
351	256.7	239.4	411	300.6	280.3	471	344.5	321.2	531	388.3	362.1	591	432.2	403.1
352	257.4	240.1	412	301.3	281.0	472	345.2	321.9	532	389.1	362.8	592	433.0	403.7
353	258.2	240.7	413	302.0	281.7	473	345.9	322.6	533	389.8	363.5	593	433.7	404.4
354	258.9	241.4	414	302.8	282.3	474	346.7	323.3	534	390.5	364.2	594	434.4	405.1
355	259.6	242.1	415	303.5	283.0	475	347.4	323.9	535	391.3	364.9	595	435.2	405.8
356	260.4	242.8	416	304.3	283.7	476	348.1	324.6	536	392.0	365.6	596	435.9	406.5
357	261.1	243.5	417	305.0	284.4	477	348.9	325.3	537	392.7	366.2	597	436.6	407.2
358	261.8	244.2	418	305.7	285.1	478	349.6	326.0	538	393.5	366.9	598	437.3	407.8
359	262.6	244.8	419	306.4	285.8	479	350.3	326.7	539	394.2	367.6	599	438.1	408.5
360	263.3	245.5	420	307.2	286.4	480	351.0	327.4	540	394.9	368.3	600	438.8	409.2

313°
227°

47 Degrees

047°
133°

3h 08m

47°

Terrestrial Spheroid

MERIDIONAL PARTS

Compression 293.465

1

M	41°	42°	43°	44°	45°	46°	47°	48°	49°	50°	M
0	2686-24	2766-05	2847-13	2929-55	3013-38	3098-70	3185-59	3274-13	3364-41	3456-53	0
1	2687-56	2767-39	2848-49	2930-93	3014-79	3100-14	3187-05	3275-62	3365-93	3458-08	1
2	2688-88	2768-73	2849-85	2932-32	3016-20	3101-57	3188-51	3277-11	3367-45	3459-64	2
3	2690-20	2770-07	2851-22	2933-71	3017-61	3103-01	3189-97	3278-60	3368-97	3461-19	3
4	2691-52	2771-41	2852-58	2935-09	3019-02	3104-44	3191-44	3280-09	3370-49	3462-74	4
5	2692-84	2772-75	2853-94	2936-48	3020-43	3105-88	3192-90	3281-58	3372-01	3464-29	5
6	2694-16	2774-10	2855-31	2937-87	3021-85	3107-32	3194-36	3283-07	3373-54	3465-85	6
7	2695-49	2775-44	2856-67	2939-26	3023-26	3108-76	3195-83	3284-57	3375-06	3467-40	7
8	2696-81	2776-78	2858-04	2940-64	3024-67	3110-19	3197-29	3286-06	3376-58	3468-96	8
9	2698-13	2778-13	2859-40	2942-03	3026-08	3111-63	3198-76	3287-55	3378-11	3470-52	9
10	2699-45	2779-47	2860-77	2943-42	3027-50	3113-07	3200-23	3289-05	3379-63	3472-07	10
11	2700-78	2780-81	2862-14	2944-81	3028-91	3114-51	3201-69	3290-54	3381-16	3473-63	11
12	2702-10	2782-16	2863-50	2946-20	3030-32	3115-95	3203-16	3292-04	3382-68	3475-19	12
13	2703-42	2783-50	2864-87	2947-59	3031-74	3117-39	3204-63	3293-54	3384-21	3476-75	13
14	2704-75	2784-85	2866-24	2948-98	3033-15	3118-83	3206-10	3295-03	3385-73	3478-30	14
15	2706-07	2786-19	2867-60	2950-37	3034-57	3120-27	3207-56	3296-53	3387-26	3479-86	15
16	2707-40	2787-54	2868-97	2951-76	3035-99	3121-71	3209-03	3298-03	3388-79	3481-42	16
17	2708-72	2788-89	2870-34	2953-15	3037-40	3123-16	3210-50	3299-52	3390-32	3482-98	17
18	2710-05	2790-23	2871-71	2954-55	3038-82	3124-60	3211-97	3301-02	3391-85	3484-54	18
19	2711-38	2791-58	2873-08	2955-94	3040-23	3126-04	3213-44	3302-52	3393-38	3486-11	19
20	2712-70	2792-93	2874-45	2957-33	3041-65	3127-49	3214-91	3304-02	3394-91	3487-67	20
21	2714-03	2794-28	2875-82	2958-73	3043-07	3128-93	3216-38	3305-52	3396-44	3489-23	21
22	2715-36	2795-62	2877-19	2960-12	3044-49	3130-37	3217-86	3307-02	3397-97	3490-79	22
23	2716-68	2796-97	2878-56	2961-51	3045-91	3131-82	3219-33	3308-52	3399-50	3492-36	23
24	2718-01	2798-32	2879-93	2962-91	3047-33	3133-26	3220-80	3310-02	3401-03	3493-92	24
25	2719-34	2799-67	2881-30	2964-30	3048-75	3134-71	3222-27	3311-53	3402-56	3495-49	25
26	2720-67	2801-02	2882-67	2965-70	3050-17	3136-15	3223-75	3313-03	3404-10	3497-05	26
27	2722-00	2802-37	2884-05	2967-09	3051-59	3137-60	3225-22	3314-53	3405-63	3498-62	27
28	2723-33	2803-72	2885-42	2968-49	3053-01	3139-05	3226-69	3316-03	3407-16	3500-18	28
29	2724-66	2805-07	2886-79	2969-89	3054-43	3140-49	3228-17	3317-54	3408-70	3501-75	29
30	2725-99	2806-42	2888-17	2971-28	3055-85	3141-94	3229-64	3319-04	3410-23	3503-32	30
31	2727-32	2807-77	2889-54	2972-68	3057-27	3143-39	3231-12	3320-55	3411-77	3504-89	31
32	2728-65	2809-13	2890-91	2974-08	3058-70	3144-84	3232-60	3322-05	3413-30	3506-45	32
33	2729-98	2810-48	2892-29	2975-48	3060-12	3146-29	3234-07	3323-56	3414-84	3508-02	33
34	2731-31	2811-83	2893-66	2976-88	3061-54	3147-74	3235-55	3325-07	3416-38	3509-59	34
35	2732-64	2813-18	2895-04	2978-28	3062-97	3149-19	3237-03	3326-57	3417-92	3511-16	35
36	2733-97	2814-54	2896-42	2979-68	3064-39	3150-64	3238-51	3328-08	3419-45	3512-73	36
37	2735-31	2815-89	2897-79	2981-08	3065-81	3152-09	3239-98	3329-59	3420-99	3514-31	37
38	2736-64	2817-25	2899-17	2982-48	3067-24	3153-54	3241-46	3331-10	3422-53	3515-88	38
39	2737-97	2818-60	2900-54	2983-88	3068-66	3154-99	3242-94	3332-60	3424-07	3517-45	39
40	2739-30	2819-95	2901-92	2985-28	3070-09	3156-45	3244-42	3344-11	3425-61	3519-02	40
41	2740-64	2821-31	2903-30	2986-68	3071-52	3157-90	3245-90	3335-62	3427-15	3520-60	41
42	2741-97	2822-67	2904-68	2988-08	3072-94	3159-35	3247-38	3337-13	3428-70	3522-17	42
43	2743-31	2824-02	2906-06	2989-48	3074-37	3160-81	3248-87	3338-65	3430-24	3523-75	43
44	2744-64	2825-38	2907-43	2990-88	3075-80	3162-26	3250-35	3340-16	3431-78	3525-32	44
45	2745-98	2826-73	2908-81	2992-29	3077-23	3163-71	3251-83	3341-67	3433-32	3526-90	45
46	2747-31	2828-09	2910-19	2993-69	3078-66	3165-17	3253-31	3343-18	3434-87	3528-47	46
47	2748-65	2829-45	2911-57	2995-09	3080-09	3166-62	3254-80	3344-69	3436-41	3530-05	47
48	2749-98	2830-81	2912-95	2996-50	3081-52	3168-08	3256-28	3346-21	3437-95	3531-63	48
49	2751-32	2832-16	2914-33	2997-90	3082-95	3169-54	3257-77	3347-72	3439-50	3533-21	49
50	2752-66	2833-52	2915-72	2999-31	3084-38	3170-99	3259-25	3349-82	3448-78	3542-69	50
51	2754-00	2834-88	2917-10	3000-71	3085-81	3172-45	3260-74	3350-75	3442-59	3536-37	51
52	2755-33	2836-24	2918-48	3002-12	3087-24	3173-91	3262-22	3352-27	3444-14	3537-95	52
53	2756-67	2837-60	2919-86	3003-53	3088-67	3175-37	3263-71	3353-78	3445-69	3539-53	53
54	2758-01	2838-96	2921-24	3004-93	3090-10	3176-83	3265-20	3355-30	3447-23	3541-11	54
55	2759-35	2840-32	2922-63	3006-34	3091-53	3178-28	3266-68	3356-82	3448-78	3542-69	55
56	2760-69	2841-68	2924-01	3007-75	3092-97	3179-74	3268-17	3358-33	3450-33	3544-27	56
57	2762-03	2843-04	2925-39	3009-16	3094-40	3181-20	3269-66	3359-85	3451-88	3545-85	57
58	2763-37	2844-40	2926-78	3010-56	3095-83	3182-66	3271-15	3361-37	3453-43	3547-44	58
59	2764-71	2845-77	2928-16	3011-97	3097-27	3184-13	3272-64	3362-89	3454-98	3549-02	59
60	2766-05	2847-13	2929-55	3013-38	3098-70	3185-59	3274-13	3364-41	3456-53	3550-60	60

LOGARITHMS

No. 1600—2199

20412—34223

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160	20412	20439	20466	20493	20520	20548	20575	20602	20629	20656	160	
161	20683	20710	20737	20763	20790	20817	20844	20871	20898	20925	161	1 3
162	20952	20978	21005	21032	21059	21085	21112	21139	21165	21192	162	2 5
163	21219	21245	21272	21299	21325	21352	21378	21405	21431	21458	163	3 8
164	21484	21511	21537	21564	21590	21617	21643	21669	21696	21722	164	4 11
165	21748	21775	21801	21827	21854	21880	21906	21932	21958	21985	165	5 13
166	22011	22037	22063	22089	22115	22141	22168	22194	22220	22246	166	6 16
167	22272	22298	22324	22350	22376	22402	22427	22453	22479	22505	167	7 18
168	22531	22557	22583	22608	22634	22660	22686	22712	22737	22763	168	8 21
169	22789	22814	22840	22866	22891	22917	22943	22968	22994	23019	169	9 24
170	23045	23070	23096	23122	23147	23172	23198	23223	23249	23274	170	
171	23300	23325	23350	23376	23401	23426	23452	23477	23502	23528	171	1 2
172	23553	23578	23603	23629	23654	23679	23704	23729	23754	23780	172	2 5
173	23805	23830	23855	23880	23905	23930	23955	23980	24005	24030	173	3 7
174	24055	24080	24105	24130	24155	24180	24204	24229	24254	24279	174	4 10
175	24304	24329	24353	24378	24403	24428	24452	24477	24502	24527	175	5 12
176	24551	24576	24601	24625	24650	24675	24699	24724	24748	24773	176	6 15
177	24797	24822	24846	24871	24895	24920	24944	24969	24993	25018	177	7 17
178	25042	25066	25091	25115	25140	25164	25188	25213	25237	25261	178	8 20
179	25285	25310	25334	25358	25382	25406	25431	25455	25479	25503	179	9 22
180	25527	25551	25576	25600	25624	25648	25672	25696	25720	25744	180	
181	25768	25792	25816	25840	25864	25888	25912	25936	25959	25983	181	1 2
182	26007	26031	26055	26079	26103	26126	26150	26174	26198	26221	182	2 5
183	26245	26269	26293	26316	26340	26364	26387	26411	26435	26458	183	3 7
184	26482	26505	26529	26553	26576	26600	26623	26647	26670	26694	184	4 9
185	26717	26741	26764	26788	26811	26834	26858	26881	26905	26928	185	5 12
186	26951	26975	26998	27021	27045	27068	27091	27114	27138	27161	186	6 14
187	27184	27207	27231	27254	27277	27300	27323	27346	27370	27393	187	7 16
188	27416	27439	27462	27485	27508	27531	27554	27577	27600	27623	188	8 19
189	27646	27669	27692	27715	27738	27761	27784	27807	27830	27853	189	9 21
190	27875	27898	27921	27944	27967	27990	28012	28035	28058	28081	190	
191	28103	28126	28149	28172	28194	28217	28240	28262	28285	28308	191	1 2
192	28330	28353	28375	28398	28421	28443	28466	28488	28511	28533	192	2 4
193	28556	28578	28601	28623	28646	28668	28691	28713	28735	28758	193	3 7
194	28780	28803	28825	28847	28870	28892	28914	28937	28959	28981	194	4 9
195	29004	29026	29048	29070	29093	29115	29137	29159	29181	29203	195	5 11
196	29226	29248	29270	29292	29314	29336	29358	29380	29403	29425	196	6 13
197	29447	29469	29491	29513	29535	29557	29579	29601	29623	29645	197	7 16
198	29667	29688	29710	29732	29754	29776	29798	29820	29842	29864	198	8 18
199	29885	29907	29929	29951	29973	29994	30016	30038	30060	30081	199	9 20
200	30103	30125	30146	30168	30190	30211	30233	30255	30276	30298	200	
201	30320	30341	30363	30384	30406	30428	30449	30471	30492	30514	201	1 2
202	30535	30557	30578	30600	30621	30643	30664	30685	30707	30728	202	2 4
203	30750	30771	30792	30814	30835	30856	30878	30899	30920	30942	203	3 6
204	30963	30984	31006	31027	31048	31069	31091	31112	31133	31154	204	4 8
205	31175	31197	31218	31239	31260	31281	31302	31323	31345	31366	205	5 11
206	31387	31408	31429	31450	31471	31492	31513	31534	31555	31576	206	6 13
207	31597	31618	31639	31660	31681	31702	31723	31744	31765	31785	207	7 15
208	31806	31827	31848	31869	31890	31911	31931	31952	31973	31994	208	8 17
209	32015	32035	32056	32077	32098	32118	32139	32160	32181	32201	209	9 19
210	32222	32243	32263	32284	32305	32325	32346	32367	32387	32408	210	
211	32428	32449	32469	32490	32511	32531	32552	32572	32593	32613	211	1 2
212	32634	32654	32675	32695	32716	32736	32756	32777	32797	32818	212	2 4
213	32838	32858	32879	32899	32919	32940	32960	32981	33001	33021	213	3 6
214	33041	33062	33082	33102	33123	33143	33163	33183	33203	33224	214	4 8
215	33244	33264	33284	33304	33325	33345	33365	33385	33405	33425	215	5 10
216	33445	33466	33486	33506	33526	33546	33566	33586	33606	33626	216	6 12
217	33646	33666	33686	33706	33726	33746	33766	33786	33806	33826	217	7 14
218	33846	33866	33886	33905	33925	33945	33965	33985	34005	34025	218	8 16
219	34044	34064	34084	34104	34124	34144	34163	34183	34203	34223	219	9 18

0 1 2 3 4 5 6 7 8 9

LOGARITHMS

No. 2800—3399

Log. 44716—53135

	0	1	2	3	4	5	6	7	8	9	5th fig.	D
280	44716	44731	44747	44762	44778	44793	44809	44824	44840	44855	280	
281	44871	44886	44902	44917	44932	44948	44963	44979	44994	45010	281	1 2
282	45025	45040	45056	45071	45087	45102	45117	45133	45148	45163	282	2 3
283	45179	45194	45209	45225	45240	45255	45271	45286	45301	45317	283	3 5
284	45332	45347	45362	45378	45393	45408	45424	45439	45454	45469	284	4 6
285	45485	45500	45515	45530	45545	45561	45576	45591	45606	45621	285	5 8
286	45637	45652	45667	45682	45697	45713	45728	45743	45758	45773	286	6 9
287	45788	45803	45818	45834	45849	45864	45879	45894	45909	45924	287	7 11
288	45939	45954	45969	45985	46000	46015	46030	46045	46060	46075	288	8 12
289	46090	46105	46120	46135	46150	46165	46180	46195	46210	46225	289	9 14
290	46240	46255	46270	46285	46300	46315	46330	46345	46359	46374	290	
291	46389	46404	46419	46434	46449	46464	46479	46494	46509	46523	291	1 1
292	46538	46553	46568	46583	46598	46613	46627	46642	46657	46672	292	2 3
293	46687	46702	46716	46731	46746	46761	46776	46790	46805	46820	293	3 4
294	46835	46850	46864	46879	46894	46909	46923	46938	46953	46968	294	4 6
295	46982	46997	47012	47026	47041	47056	47070	47085	47100	47115	295	5 7
296	47129	47144	47159	47173	47188	47203	47217	47232	47246	47261	296	6 9
297	47276	47290	47305	47320	47334	47349	47363	47378	47393	47407	297	7 10
298	47422	47436	47451	47465	47480	47494	47509	47524	47538	47553	298	8 12
299	47567	47582	47596	47611	47625	47640	47654	47669	47683	47698	299	9 13
300	47712	47727	47741	47756	47770	47784	47799	47813	47828	47842	300	
301	47857	47871	47886	47900	47914	47929	47943	47958	47972	47986	301	1 1
302	48001	48015	48029	48044	48058	48073	48087	48101	48116	48130	302	2 3
303	48144	48159	48173	48187	48202	48216	48230	48245	48259	48273	303	3 4
304	48287	48302	48316	48330	48345	48359	48373	48387	48402	48416	304	4 6
305	48430	48444	48458	48473	48487	48501	48515	48530	48544	48558	305	5 7
306	48572	48586	48601	48615	48629	48643	48657	48671	48686	48700	306	6 9
307	48714	48728	48742	48756	48770	48785	48799	48813	48827	48841	307	7 10
308	48855	48869	48883	48897	48911	48926	48940	48954	48968	48982	308	8 11
309	48996	49010	49024	49038	49052	49066	49080	49094	49108	49122	309	9 13
310	49136	49150	49164	49178	49192	49206	49220	49234	49248	49262	310	
311	49276	49290	49304	49318	49332	49346	49360	49374	49388	49402	311	1 1
312	49416	49429	49443	49457	49471	49485	49499	49513	49527	49541	312	2 3
313	49554	49568	49582	49596	49610	49624	49638	49651	49665	49679	313	3 4
314	49693	49707	49721	49734	49748	49762	49776	49790	49804	49817	314	4 6
315	49831	49845	49859	49872	49886	49900	49914	49928	49941	49955	315	5 7
316	49969	49982	49996	50010	50024	50037	50051	50065	50079	50092	316	6 8
317	50106	50120	50133	50147	50161	50174	50188	50202	50215	50229	317	7 10
318	50243	50256	50270	50284	50297	50311	50325	50338	50352	50365	318	8 11
319	50379	50393	50406	50420	50434	50447	50461	50474	50488	50501	319	9 12
320	50515	50529	50542	50556	50569	50583	50596	50610	50623	50637	320	
321	50651	50664	50678	50691	50705	50718	50732	50745	50759	50772	321	1 1
322	50786	50799	50813	50826	50840	50853	50866	50880	50893	50907	322	2 3
323	50920	50934	50947	50961	50974	50987	51001	51014	51028	51041	323	3 4
324	51055	51068	51081	51095	51108	51122	51135	51148	51162	51175	324	4 5
325	51188	51202	51215	51228	51242	51255	51268	51282	51295	51308	325	5 7
326	51322	51335	51348	51362	51375	51388	51402	51415	51428	51442	326	6 8
327	51455	51468	51481	51495	51508	51521	51534	51548	51561	51574	327	7 9
328	51587	51601	51614	51627	51640	51654	51667	51680	51693	51706	328	8 11
329	51720	51733	51746	51759	51772	51786	51799	51812	51825	51838	329	9 12
330	51851	51865	51878	51891	51904	51917	51930	51943	51957	51970	330	
331	51983	51996	52009	52022	52035	52048	52061	52075	52088	52101	331	1 1
332	52114	52127	52140	52153	52166	52179	52192	52205	52218	52231	332	2 3
333	52244	52258	52271	52284	52297	52310	52323	52336	52349	52362	333	3 4
334	52375	52388	52401	52414	52427	52440	52453	52466	52479	52492	334	4 5
335	52505	52517	52530	52543	52556	52569	52582	52595	52608	52621	335	5 6
336	52634	52647	52660	52673	52686	52699	52711	52724	52737	52750	336	6 8
337	52763	52776	52789	52802	52815	52827	52840	52853	52866	52879	337	7 9
338	52892	52905	52917	52930	52943	52956	52969	52982	52994	53007	338	8 10
339	53020	53033	53046	53058	53071	53084	53097	53110	53122	53135	339	9 12

0 1 2 3 4 5 6 7 8 9

LOGARITHMS

No. 3400—3999

Log. 53148—60195

0	1	2	3	4	5	6	7	8	9	5th fig.	D
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340	53148	53161	53173	53186	53199	53212	53225	53237	53250	53263	340
341	53275	53288	53301	53314	53326	53339	53352	53365	53377	53390	341 1 1
342	53403	53415	53428	53441	53453	53466	53479	53491	53504	53517	342 2 3
343	53529	53542	53555	53567	53580	53593	53605	53618	53631	53643	343 3 4
344	53656	53669	53681	53694	53706	53719	53732	53744	53757	53769	344 4 5
345	53782	53795	53807	53820	53832	53845	53857	53870	53883	53895	345 5 6
346	53908	53920	53933	53945	53958	53970	53983	53995	54008	54020	346 6 8
347	54033	54046	54058	54071	54083	54096	54108	54121	54133	54145	347 7 9
348	54158	54170	54183	54195	54208	54220	54233	54245	54258	54270	348 8 10
349	54283	54295	54307	54320	54332	54345	54357	54370	54382	54394	349 9 11
350	54407	54419	54432	54444	54456	54469	54481	54494	54506	54518	350
351	54531	54543	54555	54568	54580	54593	54605	54617	54630	54642	351 1 1
352	54654	54667	54679	54691	54704	54716	54728	54741	54753	54765	352 2 2
353	54778	54790	54802	54814	54827	54839	54851	54864	54876	54888	353 3 4
354	54900	54913	54925	54937	54949	54962	54974	54986	54998	55011	354 4 5
355	55023	55035	55047	55060	55072	55084	55096	55108	55121	55133	355 5 6
356	55145	55157	55169	55182	55194	55206	55218	55230	55243	55255	356 6 7
357	55267	55279	55291	55303	55315	55328	55340	55352	55364	55376	357 7 9
358	55388	55400	55413	55425	55437	55449	55461	55473	55485	55497	358 8 10
359	55509	55522	55534	55546	55558	55570	55582	55594	55606	55618	359 9 11
360	55630	55642	55654	55666	55679	55691	55703	55715	55727	55739	360
361	55751	55763	55775	55787	55799	55811	55823	55835	55847	55859	361 1 1
362	55871	55883	55895	55907	55919	55931	55943	55955	55967	55979	362 2 2
363	55991	56003	56015	56027	56039	56050	56062	56074	56086	56098	363 3 4
364	56110	56122	56134	56146	56158	56170	56182	56194	56206	56217	364 4 5
365	56229	56241	56253	56265	56277	56289	56301	56313	56324	56336	365 5 6
366	56348	56360	56372	56384	56396	56407	56419	56431	56443	56455	366 6 7
367	56467	56478	56490	56502	56514	56526	56538	56549	56561	56573	367 7 8
368	56585	56597	56608	56620	56632	56644	56656	56667	56679	56691	368 8 10
369	56703	56714	56726	56738	56750	56761	56773	56785	56797	56808	369 9 11
370	56820	56832	56844	56855	56867	56879	56891	56902	56914	56926	370
371	56937	56949	56961	56973	56984	56996	57008	57019	57031	57043	371 1 1
372	57054	57066	57078	57089	57101	57113	57124	57136	57148	57159	372 2 2
373	57171	57183	57194	57206	57217	57229	57241	57252	57264	57276	373 3 4
374	57287	57299	57310	57322	57334	57345	57357	57368	57380	57392	374 4 5
375	57403	57415	57426	57438	57449	57461	57473	57484	57496	57507	375 5 6
376	57519	57530	57542	57553	57565	57577	57588	57600	57611	57623	376 6 7
377	57634	57646	57657	57669	57680	57692	57703	57715	57726	57738	377 7 8
378	57749	57761	57772	57784	57795	57807	57818	57830	57841	57853	378 8 9
379	57864	57875	57887	57898	57910	57921	57933	57944	57956	57967	379 9 10
380	57978	57990	58001	58013	58024	58036	58047	58058	58070	58081	380
381	58093	58104	58115	58127	58138	58150	58161	58172	58184	58195	381 1 1
382	58206	58218	58229	58240	58252	58263	58275	58286	58297	58309	382 2 2
383	58320	58331	58343	58354	58365	58377	58388	58399	58411	58422	383 3 3
384	58433	58444	58456	58467	58478	58490	58501	58512	58524	58535	384 4 5
385	58546	58557	58569	58580	58591	58602	58614	58625	58636	58648	385 5 6
386	58659	58670	58681	58693	58704	58715	58726	58737	58749	58760	386 6 7
387	58771	58782	58794	58805	58816	58827	58838	58850	58861	58872	387 7 8
388	58883	58894	58906	58917	58928	58939	58950	58962	58973	58984	388 8 9
389	58995	59006	59017	59028	59040	59051	59062	59073	59084	59095	389 9 10
390	59107	59118	59129	59140	59151	59162	59173	59184	59196	59207	390
391	59218	59229	59240	59251	59262	59273	59284	59295	59306	59318	391 1 1
392	59329	59340	59351	59362	59373	59384	59395	59406	59417	59428	392 2 2
393	59439	59450	59461	59472	59483	59495	59506	59517	59528	59539	393 3 3
394	59550	59561	59572	59583	59594	59605	59616	59627	59638	59649	394 4 4
395	59660	59671	59682	59693	59704	59715	59726	59737	59748	59759	395 5 6
396	59770	59781	59791	59802	59813	59824	59835	59846	59857	59868	396 6 7
397	59879	59890	59901	59912	59923	59934	59945	59956	59967	59977	397 7 8
398	59988	59999	60010	60021	60032	60043	60054	60065	60076	60086	398 8 9
399	60097	60108	60119	60130	60141	60152	60163	60173	60184	60195	399 9 10

0	1	2	3	4	5	6	7	8	9
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LOGARITHMS

No. 5200—5799

Log. 71600—76335

	0	1	2	3	4	5	6	7	8	9	5th fig.	D
520	71600	71609	71617	71625	71634	71642	71650	71659	71667	71675	520	
521	71684	71692	71700	71709	71717	71725	71734	71742	71750	71759	521	1 1
522	71767	71775	71784	71792	71800	71809	71817	71825	71834	71842	522	2 2
523	71850	71859	71867	71875	71883	71892	71900	71908	71917	71925	523	3 3
524	71933	71941	71950	71958	71966	71975	71983	71991	71999	72008	524	4 3
525	72016	72024	72033	72041	72049	72057	72066	72074	72082	72090	525	5 4
526	72099	72107	72115	72123	72132	72140	72148	72156	72165	72173	526	6 5
527	72181	72189	72198	72206	72214	72222	72231	72239	72247	72255	527	7 6
528	72263	72272	72280	72288	72296	72305	72313	72321	72329	72337	528	8 7
529	72346	72354	72362	72370	72378	72387	72395	72403	72411	72419	529	9 8
530	72428	72436	72444	72452	72460	72469	72477	72485	72493	72501	530	
531	72510	72518	72526	72534	72542	72550	72559	72567	72575	72583	531	1 1
532	72591	72599	72608	72616	72624	72632	72640	72648	72656	72665	532	2 2
533	72673	72681	72689	72697	72705	72713	72722	72730	72738	72746	533	3 3
534	72754	72762	72770	72779	72787	72795	72803	72811	72819	72827	534	4 3
535	72835	72844	72852	72860	72868	72876	72884	72892	72900	72908	535	5 4
536	72917	72925	72933	72941	72949	72957	72965	72973	72981	72989	536	6 5
537	72997	73006	73014	73022	73030	73038	73046	73054	73062	73070	537	7 6
538	73078	73086	73094	73102	73111	73119	73127	73135	73143	73151	538	8 7
539	73159	73167	73175	73183	73191	73199	73207	73215	73223	73231	539	9 8
540	73239	73247	73256	73264	73272	73280	73288	73296	73304	73312	540	
541	73320	73328	73336	73344	73352	73360	73368	73376	73384	73392	541	1 1
542	73400	73408	73416	73424	73432	73440	73448	73456	73464	73472	542	2 2
543	73480	73488	73496	73504	73512	73520	73528	73536	73544	73552	543	3 2
544	73560	73568	73576	73584	73592	73600	73608	73616	73624	73632	544	4 3
545	73640	73648	73656	73664	73672	73680	73687	73695	73703	73711	545	5 4
546	73719	73727	73735	73743	73751	73759	73767	73775	73783	73791	546	6 5
547	73799	73807	73815	73823	73831	73838	73846	73854	73862	73870	547	7 6
548	73878	73886	73894	73902	73910	73918	73926	73934	73941	73949	548	8 6
549	73957	73965	73973	73981	73989	73997	74005	74013	74021	74028	549	9 7
550	74036	74044	74052	74060	74068	74076	74084	74092	74099	74107	550	
551	74115	74123	74131	74139	74147	74155	74162	74170	74178	74186	551	1 1
552	74194	74202	74210	74218	74225	74233	74241	74249	74257	74265	552	2 2
553	74273	74280	74288	74296	74304	74312	74320	74328	74335	74343	553	3 2
554	74351	74359	74367	74375	74382	74390	74398	74406	74414	74422	554	4 3
555	74429	74437	74445	74453	74461	74468	74476	74484	74492	74500	555	5 4
556	74508	74515	74523	74531	74539	74547	74554	74562	74570	74578	556	6 4
557	74586	74593	74601	74609	74617	74625	74632	74640	74648	74656	557	7 5
558	74663	74671	74679	74687	74695	74702	74710	74718	74726	74733	558	8 6
559	74741	74749	74757	74765	74772	74780	74788	74796	74803	74811	559	9 7
560	74819	74827	74834	74842	74850	74858	74865	74873	74881	74889	560	
561	74896	74904	74912	74920	74927	74935	74943	74950	74958	74966	561	1 1
562	74974	74981	74989	74997	75005	75012	75020	75028	75035	75043	562	2 2
563	75051	75059	75066	75074	75082	75089	75097	75105	75113	75120	563	3 2
564	75128	75136	75143	75151	75159	75166	75174	75182	75190	75197	564	4 3
565	75205	75213	75220	75228	75236	75243	75251	75259	75266	75274	565	5 4
566	75282	75289	75297	75305	75312	75320	75328	75335	75343	75351	566	6 5
567	75358	75366	75374	75381	75389	75397	75404	75412	75420	75427	567	7 5
568	75435	75443	75450	75458	75465	75473	75481	75488	75496	75504	568	8 6
569	75511	75519	75527	75534	75542	75549	75557	75565	75572	75580	569	9 7
570	75588	75595	75603	75610	75618	75626	75633	75641	75648	75656	570	
571	75664	75671	75679	75686	75694	75702	75709	75717	75724	75732	571	1 1
572	75740	75747	75755	75762	75770	75778	75785	75793	75800	75808	572	2 2
573	75816	75823	75831	75838	75846	75853	75861	75869	75876	75884	573	3 2
574	75891	75899	75906	75914	75921	75929	75937	75944	75952	75959	574	4 3
575	75967	75974	75982	75989	75997	76005	76012	76020	76027	76035	575	5 4
576	76042	76050	76057	76065	76072	76080	76088	76095	76103	76110	576	6 5
577	76118	76125	76133	76140	76148	76155	76163	76170	76178	76185	577	7 5
578	76193	76200	76208	76215	76223	76230	76238	76245	76253	76260	578	8 6
579	76268	76275	76283	76290	76298	76305	76313	76320	76328	76335	579	9 7

0 1 2 3 4 5 6 7 8 9

LOGARITHMS

No. 7000—7599

Log. 84510—88076

	0	1	2	3	4	5	6	7	8	9	5th fig.	D
700	84510	84516	84522	84528	84535	84541	84547	84553	84559	84566	700	
701	84572	84578	84584	84590	84597	84603	84609	84615	84621	84628	701	1 1
702	84634	84640	84646	84652	84658	84665	84671	84677	84683	84689	702	2 1
703	84696	84702	84708	84714	84720	84726	84733	84739	84745	84751	703	3 2
704	84757	84763	84770	84776	84782	84788	84794	84800	84807	84813	704	4 2
705	84819	84825	84831	84837	84844	84850	84856	84862	84868	84874	705	5 3
706	84881	84887	84893	84899	84905	84911	84917	84924	84930	84936	706	6 4
707	84942	84948	84954	84960	84967	84973	84979	84985	84991	84997	707	7 4
708	85003	85010	85016	85022	85028	85034	85040	85046	85052	85059	708	8 5
709	85065	85071	85077	85083	85089	85095	85101	85108	85114	85120	709	9 5
710	85126	85132	85138	85144	85150	85156	85163	85169	85175	85181	710	
711	85187	85193	85199	85205	85211	85218	85224	85230	85236	85242	711	1 1
712	85248	85254	85260	85266	85272	85279	85285	85291	85297	85303	712	2 1
713	85309	85315	85321	85327	85333	85339	85346	85352	85358	85364	713	3 2
714	85370	85376	85382	85388	85394	85400	85406	85412	85419	85425	714	4 2
715	85431	85437	85443	85449	85455	85461	85467	85473	85479	85485	715	5 3
716	85491	85497	85503	85510	85516	85522	85528	85534	85540	85546	716	6 4
717	85552	85558	85564	85570	85576	85582	85588	85594	85600	85606	717	7 4
718	85612	85619	85625	85631	85637	85643	85649	85655	85661	85667	718	8 5
719	85673	85679	85685	85691	85697	85703	85709	85715	85721	85727	719	9 5
720	85733	85739	85745	85751	85757	85763	85769	85775	85782	85788	720	
721	85794	85800	85806	85812	85818	85824	85830	85836	85842	85848	721	1 1
722	85854	85860	85866	85872	85878	85884	85890	85896	85902	85908	722	2 1
723	85914	85920	85926	85932	85938	85944	85950	85956	85962	85968	723	3 2
724	85974	85980	85986	85992	85998	86004	86010	86016	86022	86028	724	4 2
725	86034	86040	86046	86052	86058	86064	86070	86076	86082	86088	725	5 3
726	86094	86100	86106	86112	86118	86124	86130	86136	86142	86148	726	6 4
727	86153	86159	86165	86171	86177	86183	86189	86195	86201	86207	727	7 4
728	86213	86219	86225	86231	86237	86243	86249	86255	86261	86267	728	8 5
729	86273	86279	86285	86291	86297	86303	86309	86314	86320	86326	729	9 5
730	86332	86338	86344	86350	86356	86362	86368	86374	86380	86386	730	
731	86392	86398	86404	86410	86416	86421	86427	86433	86439	86445	731	1 1
732	86451	86457	86463	86469	86475	86481	86487	86493	86499	86505	732	2 1
733	86510	86516	86522	86528	86534	86540	86546	86552	86558	86564	733	3 2
734	86570	86576	86581	86587	86593	86599	86605	86611	86617	86623	734	4 2
735	86629	86635	86641	86647	86652	86658	86664	86670	86676	86682	735	5 3
736	86688	86694	86700	86706	86711	86717	86723	86729	86735	86741	736	6 4
737	86747	86753	86759	86764	86770	86776	86782	86788	86794	86800	737	7 4
738	86806	86812	86817	86823	86829	86835	86841	86847	86853	86859	738	8 5
739	86864	86870	86876	86882	86888	86894	86900	86906	86911	86917	739	9 5
740	86923	86929	86935	86941	86947	86953	86958	86964	86970	86976	740	
741	86982	86988	86994	86999	87005	87011	87017	87023	87029	87035	741	1 1
742	87040	87046	87052	87058	87064	87070	87076	87081	87087	87093	742	2 1
743	87099	87105	87111	87116	87122	87128	87134	87140	87146	87152	743	3 2
744	87157	87163	87169	87175	87181	87187	87192	87198	87204	87210	744	4 2
745	87216	87222	87227	87233	87239	87245	87251	87256	87262	87268	745	5 3
746	87274	87280	87286	87291	87297	87303	87309	87315	87320	87326	746	6 4
747	87332	87338	87344	87350	87355	87361	87367	87373	87379	87384	747	7 4
748	87390	87396	87402	87408	87413	87419	87425	87431	87437	87442	748	8 5
749	87448	87454	87460	87466	87471	87477	87483	87489	87495	87500	749	9 5
750	87506	87512	87518	87524	87529	87535	87541	87547	87552	87558	750	
751	87564	87570	87576	87581	87587	87593	87599	87605	87610	87616	751	1 1
752	87622	87628	87633	87639	87645	87651	87656	87662	87668	87674	752	2 1
753	87680	87685	87691	87697	87703	87708	87714	87720	87726	87731	753	3 2
754	87737	87743	87749	87754	87760	87766	87772	87777	87783	87789	754	4 2
755	87795	87800	87806	87812	87818	87823	87829	87835	87841	87846	755	5 3
756	87852	87858	87864	87869	87875	87881	87887	87892	87898	87904	756	6 4
757	87910	87915	87921	87927	87933	87938	87944	87950	87956	87961	757	7 4
758	87967	87973	87978	87984	87990	87996	88001	88007	88013	88019	758	8 5
759	88024	88030	88036	88041	88047	88053	88059	88064	88070	88076	759	9 5

0 1 2 3 4 5 6 7 8 9

LOGS. OF TRIG. FUNCTIONS

1°
181°

	Sine	Diff.	Cosec.	Tan.	Diff.	Cotan.	Secant	Diff.	Cosine	
36·0	2.(8) 44594	90	1.(11) 55406	2.(8) 44611	90	1.(11) 55389	0.(10) 00017	1.(9) 99983	99983	24'
·2	44684	91	55316	44701	91	55299	00017	99983	99983	
·4	44775	90	55225	44792	90	55208	00017	99983	99983	
·6	44865	89	55135	44882	89	55118	00017	99983	99983	
·8	44954	90	55046	44971	90	55029	00017	99983	99983	
37·0	45044	90	54956	45061	90	54939	00017	99983	99983	23'
·2	45134	89	54866	45151	89	54849	00017	99983	99983	
·4	45223	89	54777	45240	90	54760	00017	99983	99983	
·6	45312	89	54688	45330	89	54670	00018	99982	99982	
·8	45401	88	54599	45419	88	54581	00018	99982	99982	
38·0	45489	89	54511	45507	89	54493	00018	99982	99982	22'
·2	45578	88	54422	45596	88	54404	00018	99982	99982	
·4	45666	88	54334	45684	88	54316	00018	99982	99982	
·6	45754	88	54246	45772	88	54228	00018	99982	99982	
·8	45842	88	54158	45860	88	54140	00018	99982	99982	
39·0	45930	88	54070	45948	88	54052	00018	99982	99982	21'
·2	46018	87	53982	46036	87	53964	00018	99982	99982	
·4	46105	88	53895	46123	88	53877	00018	99982	99982	
·6	46193	87	53807	46211	87	53789	00018	99982	99982	
·8	46280	87	53720	46298	87	53702	00018	99982	99982	
40·0	46366	87	53634	46385	86	53615	00018	99982	99982	20'
·2	46453	87	53547	46471	88	53529	00018	99982	99982	
·4	46540	86	53460	46559	86	53441	00019	99981	99981	
·6	46626	86	53374	46645	86	53355	00019	99981	99981	
·8	46712	86	53288	46731	86	53269	00019	99981	99981	
41·0	46799	86	53202	46817	86	53183	00019	99981	99981	19'
·2	46884	86	53116	46903	86	53097	00019	99981	99981	
·4	46970	86	53030	46989	86	53011	00019	99981	99981	
·6	47056	85	52944	47075	85	52925	00019	99981	99981	
·8	47141	85	52859	47160	85	52840	00019	99981	99981	
42·0	47226	85	52774	47245	85	52755	00019	99981	99981	18'
·2	47311	85	52689	47330	85	52670	00019	99981	99981	
·4	47396	85	52604	47415	85	52585	00019	99981	99981	
·6	47481	85	52519	47500	85	52500	00019	99981	99981	
·8	47566	84	52434	47585	84	52415	00019	99981	99981	
43·0	47650	84	52350	47669	85	52331	00019	99981	99981	17'
·2	47734	84	52266	47754	84	52246	00020	99980	99980	
·4	47818	84	52182	47838	84	52162	00020	99980	99980	
·6	47902	84	52098	47922	84	52078	00020	99980	99980	
·8	47986	83	52014	48006	83	51994	00020	99980	99980	
44·0	48069	84	51931	48089	84	51911	00020	99980	99980	16'
·2	48153	83	51847	48173	83	51827	00020	99980	99980	
·4	48236	83	51764	48256	83	51744	00020	99980	99980	
·6	48319	83	51681	48339	83	51661	00020	99980	99980	
·8	48402	83	51598	48422	83	51578	00020	99980	99980	
45·0	48485	82	51515	48505	82	51495	00020	99980	99980	15'
·2	48567	83	51433	48587	83	51413	00020	99980	99980	
·4	48650	82	51350	48670	83	51330	00020	99980	99980	
·6	48732	82	51268	48753	82	51247	00021	99979	99979	
·8	48814	82	51186	48835	82	51165	00021	99979	99979	
46·0	48896	82	51104	48917	82	51083	00021	99979	99979	14'
·2	48978	82	51022	48999	82	51001	00021	99979	99979	
·4	49060	81	50940	49081	81	50919	00021	99979	99979	
·6	49141	82	50859	49162	82	50838	00021	99979	99979	
·8	49223	81	50777	49244	81	50756	00021	99979	99979	
47·0	49304	81	50696	49325	81	50675	00021	99979	99979	13'
·2	49385	81	50615	49406	81	50594	00021	99979	99979	
·4	49466	81	50534	49487	81	50513	00021	99979	99979	
·6	49547	80	50453	49568	80	50432	00021	99979	99979	
·8	49627	81	50373	49648	81	50352	00021	99979	99979	
48·0	49708	81	50292	49729		50271	00021	99979	99979	12'

178°

358°

2°
182°

LOGS. OF TRIG. FUNCTIONS

/	Sine	Diff.	Cosec.	Tan.	Diff.	Cotan.	Secant	Diff.	Cosine	
00-0	2.(8) 54282	72	1.(11) 45718	2.(8) 54308	73	1.(11) 45692	0.(10) 00027	1.(9) 99974	60'	
-2	54354	72	45646	54381	73	45619	00027	99973		
-4	54426	72	45574	54453	72	45547	00027	99973		
-6	54498	72	45502	54525	72	45475	00027	99973		
-8	54570	72	45430	54597	72	45403	00027	99973		
01-0	54642	72	45358	54669		45331	00027	99973		
-2	54714	72	45286	54741	72	45259	00027	99973		
-4	54786	72	45214	54813	72	45187	00027	99973		
-6	54857	71	45143	54884	71	45116	00027	99973		
-8	54928	71	45072	54955	71	45045	00027	99973		
02-0	55000	72	45001	55027	71	44973	00027	99973		
-2	55071	72	44929	55098	71	44902	00027	99973		
-4	55142	71	44858	55170	72	44830	00028	99972		
-6	55212	70	44788	55240	70	44760	00028	99972		
-8	55283	71	44717	55311	71	44689	00028	99972		
03-0	55354	70	44646	55382	70	44618	00028	99972		
-2	55424	70	44576	55452	71	44548	00028	99972		
-4	55495	71	44505	55523	71	44477	00028	99972		
-6	55565	70	44435	55593	70	44407	00028	99972		
-8	55635	70	44365	55663	70	44337	00028	99972		
04-0	55705	70	44295	55734		44266	00028	99972		
-2	55775	70	44225	55803	69	44197	00028	99972		
-4	55845	70	44155	55873	70	44127	00028	99972		
-6	55915	70	44085	55944	71	44056	00029	99971		
-8	55984	69	44016	56013	69	43987	00029	99971		
05-0	56054	69	43946	56083	69	43917	00029	99971		
-2	56123	69	43877	56152	69	43848	00029	99971		
-4	56193	70	43807	56222	70	43778	00029	99971		
-6	56262	69	43738	56291	69	43709	00029	99971		
-8	56331	69	43669	56360	69	43640	00029	99971		
06-0	56400	69	43600	56429		43571	00029	99971		
-2	56469	69	43531	56498	69	43502	00029	99971		
-4	56538	68	43462	56567	69	43433	00029	99971		
-6	56606	68	43394	56636		43364	00030	99970		
-8	56675	69	43325	56705	69	43295	00030	99970		
07-0	56743	68	43257	56773		43227	00030	99970		
-2	56811	68	43189	56841	68	43159	00030	99970		
-4	56880	68	43120	56910	68	43090	00030	99970		
-6	56948	68	43052	56978	68	43022	00030	99970		
-8	57016	68	42984	57046		42954	00030	99970		
08-0	57084	67	42916	57114		42886	00030	99970		
-2	57151	67	42849	57181	67	42819	00030	99970		
-4	57219	68	42781	57249	68	42751	00030	99970		
-6	57287	68	42713	57317	68	42683	00030	99970		
-8	57354	67	42646	57385	68	42615	00031	99969		
09-0	57421	68	42579	57452	68	42548	00031	99969		
-2	57489	68	42511	57520	67	42480	00031	99969		
-4	57556	67	42444	57587	67	42413	00031	99969		
-6	57623	67	42377	57654	67	42346	00031	99969		
-8	57690	67	42310	57721	67	42279	00031	99969		
10-0	57757	67	42243	57788	66	42212	00031	99969		
-2	57823	67	42177	57854	67	42146	00031	99969		
-4	57890	67	42110	57921	67	42079	00031	99969		
-6	57957	67	42043	57988	67	42012	00031	99969		
-8	58023	66	41977	58054	67	41946	00031	99969		
11-0	58089	66	41911	58121		41879	00032	99968		
-2	58155	66	41845	58187	66	41813	00032	99968		
-4	58222	67	41778	58254	67	41746	00032	99968		
-6	58288	66	41712	58320	66	41680	00032	99968		
-8	58353	66	41647	58385	66	41615	00032	99968		
12-0	58419	66	41581	58451		41549	00032	99968		

177°

357°

5°

185°

LOGS. OF TRIG. FUNCTIONS

	Sine	Parts	Cosec.	Tan.	Parts	Cotan.	Secant	Parts	Cosine	
00-0	2.(8) 94030	'	1.(11) 05970	2.(8) 94195	'	1.(11) 05805	0.(10) 00166	1.(9) 99834	60'	
01-0	94174	.1 14	05826	94340	.1 14	05660	00167	99833		
02-0	94317	.2 28	05683	94485	.2 29	05515	00168	99832		
03-0	94461	.3 43	05539	94630	.3 43	05371	00169	99831		
04-0	94603	.4 57	05397	94773	.4 57	05227	00170	99830		
05-0	94746	.5 71	05254	94917	.5 72	05083	00171	99829	55'	
06-0	94887	.6 85	05113	95060	.6 86	04940	00172	99828		
07-0	95029	.7 99	04971	95202	.7 100	04798	00173	99827		
08-0	95170	.8 114	04830	95344	.8 115	04656	00175	99826		
09-0	95310	.9 128	04690	95486	.9 129	04514	00176	99824		
10-0	95450	.1 14	04550	95627		04373	00177	99823	50'	
11-0	95589	.2 28	04411	95767	.1 14	04233	00178	99822		
12-0	95728	.3 41	04272	95908	.2 28	04093	00179	99821		
13-0	95867	.4 55	04133	96047	.3 42	03953	00180	99820		
14-0	96005	.5 69	03995	96187	.4 55	03813	00181	99819		
15-0	96143	.6 83	03857	96326	.5 69	03675	00183	99817	45'	
16-0	96280	.7 96	03720	96464	.6 83	03536	00184	99816		
17-0	96417	.8 110	03583	96602	.7 97	03398	00185	99815		
18-0	96553	.9 124	03447	96739	.8 111	03261	00186	99814		
19-0	96689		03311	96877	.9 125	03123	00187	99813		
20-0	96825	.1 13	03175	97013		02987	00188	99812	40'	
21-0	96960	.2 27	03040	97150	.1 13	02850	00190	99810		
22-0	97095	.3 40	02905	97286	.2 27	02715	00191	99809		
23-0	97229	.4 53	02771	97421	.3 40	02579	00192	99808		
24-0	97363	.5 67	02637	97556	.4 54	02444	00193	99807		
25-0	97496	.6 80	02504	97691	.5 67	02309	00194	99806	35'	
26-0	97629	.7 93	02371	97825	.6 81	02175	00196	99804		
27-0	97762	.8 107	02238	97959	.7 94	02041	00197	99803		
28-0	97894	.9 120	02106	98092	.8 108	01908	00198	99802		
29-0	98026		01974	98225	.9 121	01775	00199	99801		
30-0	98157	.1 13	01843	98358	.1 13	01642	00200	99800	30'	
31-0	98288	.2 26	01712	98490	.2 26	01510	00202	99798		
32-0	98419	.3 39	01581	98622	.3 39	01378	00203	99797		
33-0	98549	.4 52	01451	98753	.4 52	01247	00204	99796		
34-0	98679	.5 65	01321	98884	.5 65	01116	00205	99795		
35-0	98808	.6 78	01192	99015	.6 78	00985	00207	99794	25'	
36-0	98937	.7 91	01063	99145	.7 91	00855	00208	99792		
37-0	99066	.8 103	00934	99275	.8 104	00725	00209	99791		
38-0	99194	.9 116	00806	99405	.9 117	00596	00210	99790		
39-0	99322		00678	99534		00466	00212	99789		
40-0	99450		00550	99662		00338	00213	99787	20'	
41-0	99577	.1 13	00423	99791	.1 13	00209	00214	99786		
42-0	99704	.2 25	00296	99919	.2 25	00081	00215	99785		
43-0	99830	.3 38	00170		.3 38	0.(10) 99954	00217	99784		
44-0	99956	.4 50	00044		.4 51	99826	00218	99782		
45-0	1.(9) 00082	.5 63	0.(10) 99918	00174	.5 63	99700	00219	99781	15'	
46-0	00207	.6 75	99793	00301	.6 76	99573	00220	99780		
47-0	00332	.7 88	99668	00427	.7 89	99447	00222	99778		
48-0	00456	.8 100	99544	00553	.8 101	99321	00223	99777		
49-0	00581	.9 113	99420	00679	.9 114	99195	00224	99776		
50-0	00704		99296	00930		99070	00226	99775	10'	
51-0	00828	.1 12	99172	01055	.1 12	98945	00227	99773		
52-0	00951	.2 24	99049	01179	.2 25	98821	00228	99772		
53-0	01074	.3 37	98926	01303	.3 37	98697	00229	99771		
54-0	01196	.4 49	98804	01427	.4 49	98573	00231	99769		
55-0	01318	.5 61	98682	01550	.5 62	98450	00232	99768	5'	
56-0	01440	.6 73	98560	01673	.6 74	98327	00233	99767		
57-0	01561	.7 85	98439	01796	.7 86	98204	00235	99765		
58-0	01682	.8 98	98318	01918	.8 99	98082	00236	99764		
59-0	01803	.9 110	98197	02040	.9 111	97960	00237	99763		
60-0	01924		98077	02162		97838	00239	99761	0'	

174°

354°

15°

HAVERSINES

	.0	.2	.4	.6	.8								
	Log.	Nat.											
/	2.or(8.)	0.	/										
00	23140	01704	23159	01704	23178	01705	23197	01706	23216	01707	23235	01707	59
01	23235	01707	23255	01708	23274	01709	23293	01710	23312	01710	23331	01711	58
02	23331	01711	23350	01712	23370	01713	23389	01713	23408	01714	23427	01715	57
03	23427	01715	23446	01716	23465	01717	23484	01717	23503	01718	23523	01719	56
04	23523	01719	23542	01720	23561	01720	23580	01721	23599	01722	23618	01723	55
05	23618	01723	23637	01723	23656	01724	23675	01725	23694	01726	23713	01726	54
06	23713	01726	23732	01727	23751	01728	23771	01729	23790	01729	23809	01730	53
07	23809	01730	23828	01731	23847	01732	23866	01732	23885	01733	23904	01734	52
08	23904	01734	23923	01735	23942	01735	23961	01736	23980	01737	23999	01738	51
09	23999	01738	24018	01739	24037	01739	24056	01740	24075	01741	24094	01742	50
10	24094	01742	24113	01742	24132	01743	24151	01744	24170	01745	24189	01745	49
11	24189	01745	24208	01746	24227	01747	24245	01748	24264	01748	24283	01749	48
12	24283	01749	24302	01750	24321	01751	24340	01751	24359	01752	24378	01753	47
13	24378	01753	24397	01754	24416	01755	24435	01755	24454	01756	24472	01757	46
14	24472	01757	24491	01758	24510	01758	24529	01759	24548	01760	24567	01761	45
15	24567	01761	24586	01761	24605	01762	24624	01763	24642	01764	24661	01764	44
16	24661	01764	24680	01765	24699	01766	24718	01767	24737	01768	24755	01768	43
17	24755	01768	24774	01769	24793	01770	24812	01771	24831	01771	24850	01772	42
18	24850	01772	24868	01773	24887	01774	24906	01774	24925	01775	24944	01776	41
19	24944	01776	24962	01777	24981	01777	25000	01778	25019	01779	25037	01780	40
20	25037	01780	25056	01781	25075	01781	25094	01782	25112	01783	25131	01784	39
21	25131	01784	25150	01784	25169	01785	25187	01786	25206	01787	25225	01788	38
22	25225	01788	25244	01788	25262	01789	25281	01790	25300	01791	25319	01791	37
23	25319	01791	25337	01792	25356	01793	25375	01794	25393	01794	25412	01795	36
24	25412	01795	25431	01796	25449	01797	25468	01798	25487	01798	25505	01799	35
25	25505	01799	25524	01800	25543	01801	25561	01801	25580	01802	25599	01803	34
26	25599	01803	25617	01804	25636	01805	25655	01805	25673	01806	25692	01807	33
27	25692	01807	25710	01808	25729	01808	25748	01809	25766	01810	25785	01811	32
28	25785	01811	25804	01811	25822	01812	25841	01813	25859	01814	25878	01815	31
29	25878	01815	25897	01815	25915	01816	25934	01817	25952	01818	25971	01818	30
30	25971	01818	25989	01819	26008	01820	26026	01821	26045	01822	26064	01822	29
31	26064	01822	26082	01823	26101	01824	26119	01825	26138	01825	26156	01826	28
32	26156	01826	26175	01827	26193	01828	26212	01829	26230	01829	26249	01830	27
33	26249	01830	26267	01831	26286	01832	26304	01832	26323	01833	26341	01834	26
34	26341	01834	26360	01835	26378	01836	26397	01836	26415	01837	26434	01838	25
35	26434	01838	26452	01839	26471	01840	26489	01840	26508	01841	26526	01842	24
36	26526	01842	26544	01843	26563	01843	26581	01844	26600	01845	26618	01846	23
37	26618	01846	26637	01847	26655	01847	26673	01848	26692	01849	26710	01850	22
38	26710	01850	26729	01850	26747	01851	26765	01852	26784	01853	26802	01854	21
39	26802	01854	26821	01854	26839	01855	26857	01856	26876	01857	26894	01858	20
40	26894	01858	26912	01858	26931	01859	26949	01860	26967	01861	26986	01861	19
41	26986	01861	27004	01862	27022	01863	27041	01864	27059	01865	27077	01865	18
42	27077	01865	27096	01866	27114	01867	27132	01868	27151	01869	27169	01869	17
43	27169	01869	27187	01870	27206	01871	27224	01872	27242	01873	27261	01873	16
44	27261	01873	27279	01874	27297	01875	27315	01876	27334	01876	27352	01877	15
45	27352	01877	27370	01878	27388	01879	27407	01880	27425	01880	27443	01881	14
46	27443	01881	27461	01882	27480	01883	27498	01884	27516	01884	27534	01885	13
47	27534	01885	27553	01886	27571	01887	27589	01888	27607	01888	27626	01889	12
48	27626	01889	27644	01890	27662	01891	27680	01891	27698	01892	27717	01893	11
49	27717	01893	27735	01894	27753	01895	27771	01895	27789	01896	27807	01897	10
50	27807	01897	27826	01898	27844	01899	27862	01899	27880	01900	27898	01901	09
51	27898	01901	27916	01902	27934	01903	27953	01903	27971	01904	27989	01905	08
52	27989	01905	28007	01906	28025	01907	28043	01907	28061	01908	28080	01909	07
53	28080	01909	28098	01910	28116	01911	28134	01911	28152	01912	28170	01913	06
54	28170	01913	28188	01914	28206	01915	28224	01915	28242	01916	28260	01917	05
55	28260	01917	28278	01918	28297	01919	28315	01919	28333	01920	28351	01921	04
56	28351	01921	28369	01922	28387	01923	28405	01923	28423	01924	28441	01925	03
57	28441	01925	28459	01926	28477	01927	28495	01927	28513	01928	28531	01929	02
58	28531	01929	28549	01930	28567	01931	28585	01931	28603	01932	28621	01933	01
59	28621	01933	28639	01934	28657	01935	28675	01935	28693	01936	28711	01937	00

HAVERSINES

	91°		92°		93°		94°		95°		96°		Parts for 0° 2. etc.
	Log.	Nat.											
00	70648	50873	71387	51745	72112	52617	72825	53488	73526	54358	74215	55226	60
01	70661	50887	71399	51760	72124	52631	72837	53502	73538	54372	74226	55241	59
02	70673	50902	71411	51774	72136	52646	72849	53517	73549	54387	74237	55255	58
03	70686	50916	71423	51789	72148	52660	72861	53531	73561	54401	74249	55270	57
04	70698	50931	71436	51803	72160	52675	72873	53546	73572	54416	74260	55284	56
05	70710	50945	71448	51818	72172	52689	72884	53560	73584	54430	74272	55299	55
06	70723	50960	71460	51832	72184	52704	72896	53575	73596	54445	74283	55313	54
07	70735	50974	71472	51847	72196	52718	72908	53589	73607	54459	74294	55328	53
08	70748	50989	71484	51861	72208	52733	72920	53604	73619	54474	74306	55342	52
09	70760	51004	71496	51876	72220	52748	72931	53618	73630	54488	74317	55357	51
10	70772	51018	71509	51890	72232	52762	72943	53633	73642	54503	74328	55371	50
11	70785	51033	71521	51905	72244	52776	72955	53647	73653	54517	74340	55386	49
12	70797	51047	71533	51919	72256	52791	72967	53662	73665	54532	74351	55400	48
13	70809	51062	71545	51934	72268	52806	72978	53676	73676	54546	74362	55414	47
14	70822	51076	71557	51948	72280	52820	72990	53691	73688	54561	74374	55429	46
15	70834	51091	71569	51963	72292	52835	73002	53705	73699	54575	74385	55443	45
16	70847	51105	71582	51978	72304	52849	73014	53720	73711	54590	74396	55458	44
17	70859	51120	71594	51992	72316	52864	73025	53734	73722	54604	74408	55472	43
18	70871	51134	71606	52007	72328	52878	73037	53749	73734	54619	74419	55487	42
19	70884	51149	71618	52021	72340	52893	73049	53763	73746	54633	74430	55501	41
20	70896	51163	71630	52036	72352	52907	73060	53778	73757	54647	74442	55516	40
21	70908	51178	71642	52050	72363	52922	73072	53792	73769	54662	74453	55530	39
22	70921	51193	71654	52065	72375	52936	73084	53807	73780	54676	74464	55545	38
23	70933	51207	71666	52079	72387	52951	73096	53821	73792	54691	74475	55559	37
24	70945	51222	71679	52094	72399	52965	73107	53836	73803	54705	74487	55573	36
25	70958	51236	71691	52108	72411	52980	73119	53850	73815	54720	74498	55588	35
26	70970	51251	71703	52123	72423	52994	73131	53865	73826	54734	74509	55602	34
27	70982	51265	71715	52137	72435	53009	73142	53879	73838	54749	74521	55617	33
28	70995	51280	71727	52152	72447	53023	73154	53894	73849	54763	74532	55631	32
29	71007	51294	71739	52166	72459	53038	73166	53908	73860	54778	74543	55646	31
30	71019	51309	71751	52181	72471	53052	73177	53923	73872	54792	74554	55660	30
31	71032	51323	71763	52196	72482	53067	73189	53937	73883	54807	74566	55675	29
32	71044	51338	71775	52210	72494	53081	73201	53952	73895	54821	74577	55689	28
33	71056	51352	71787	52225	72506	53096	73212	53966	73906	54836	74588	55704	27
34	71068	51367	71800	52239	72518	53110	73224	53981	73918	54850	74600	55718	26
35	71081	51382	71812	52254	72530	53125	73236	53995	73929	54865	74611	55732	25
36	71093	51396	71824	52268	72542	53140	73247	54010	73941	54879	74622	55747	24
37	71105	51411	71836	52283	72554	53154	73259	54024	73952	54894	74633	55761	23
38	71118	51425	71848	52297	72565	53169	73271	54039	73964	54908	74645	55776	22
39	71130	51440	71860	52312	72577	53183	73282	54053	73975	54923	74656	55790	21
40	71142	51454	71872	52326	72589	53198	73294	54068	73987	54937	74667	55805	20
41	71154	51469	71884	52341	72601	53212	73306	54082	73998	54952	74678	55819	19
42	71167	51483	71896	52355	72613	53227	73317	54097	74009	54966	74690	55834	18
43	71179	51498	71908	52370	72625	53241	73329	54111	74021	54980	74701	55848	17
44	71191	51512	71920	52384	72637	53256	73341	54126	74032	54995	74712	55862	16
45	71203	51527	71932	52399	72648	53270	73352	54140	74044	55009	74723	55877	15
46	71216	51541	71944	52413	72660	53285	73364	54155	74055	55024	74734	55891	14
47	71228	51556	71956	52428	72672	53299	73375	54169	74067	55038	74746	55906	13
48	71240	51571	71968	52442	72684	53314	73387	54184	74078	55053	74757	55920	12
49	71252	51585	71980	52457	72696	53328	73399	54198	74089	55067	74768	55935	11
50	71265	51600	71992	52472	72708	53343	73410	54213	74101	55082	74779	55949	10
51	71277	51614	72004	52486	72719	53357	73422	54227	74112	55096	74791	55964	09
52	71289	51629	72016	52501	72731	53372	73433	54242	74124	55111	74802	55978	08
53	71301	51643	72028	52515	72743	53386	73445	54256	74135	55125	74813	55992	07
54	71314	51658	72040	52530	72755	53401	73457	54271	74146	55140	74824	56007	06
55	71326	51672	72052	52544	72767	53415	73468	54285	74158	55154	74835	56021	05
56	71338	51687	72064	52559	72778	53430	73480	54300	74169	55169	74846	56036	04
57	71350	51701	72076	52573	72790	53444	73491	54314	74181	55183	74858	56050	03
58	71362	51716	72088	52588	72802	53459	73503	54329	74192	55197	74869	56065	02
59	71375	51730	72100	52602	72814	53473	73515	54343	74203	55212	74880	56079	01
60	71387	51745	72112	52617	72825	53488	73526	54358	74215	55226	74891	56093	00
	268°	267°	266°	265°	264°	263°							

NATURAL FUNCTIONS OF ANGLES

NATURAL TANGENTS

Degrees	0'	6'	12'	18'	24'	30'	36'	42'	48'	54'	Add Mean Differences				
											1'	2'	3'	4'	5'
45	1.00000	0.0350	0.0701	0.1053	0.1406	0.1761	0.2117	0.2474	0.2832	0.3192	58	118	177	237	296
46	-0.0353	0.03915	0.04279	0.04644	0.05010	0.05378	0.05747	0.06117	0.06489	0.06862	61	123	184	245	307
47	-0.07237	0.07613	0.07990	0.08369	0.08749	0.09131	0.09514	0.09899	0.10285	0.10672	63	127	191	255	319
48	-0.11061	0.11452	0.11844	0.12238	0.12633	0.13029	0.13428	0.13828	0.14229	0.14632	66	132	199	265	331
49	-0.15037	0.15443	0.15851	0.16261	0.16672	0.17085	0.17500	0.17916	0.18334	0.18754	69	138	207	276	344
50	1.19175	1.19599	2.0024	2.0451	2.0879	2.1310	2.1742	2.2176	2.2612	2.3050	72	143	216	288	359
51	-0.23490	2.3931	2.4375	2.4820	2.5268	2.5717	2.6169	2.6622	2.7077	2.7535	75	150	225	300	375
52	-0.27994	2.8456	2.8919	2.9385	2.9853	3.0323	3.0795	3.1269	3.1745	3.2224	78	157	235	314	392
53	-0.32704	3.3187	3.3673	3.4160	3.4650	3.5142	3.5637	3.6134	3.6633	3.7134	82	164	247	329	411
54	-0.37638	3.8145	3.8653	3.9165	3.9679	4.0195	4.0714	4.1235	4.1759	4.2286	86	172	259	345	431
55	1.42815	4.3347	4.3881	4.4418	4.4958	4.5501	4.6046	4.6595	4.7146	4.7700	91	181	272	362	453
56	-0.48256	4.8816	4.9378	4.9944	5.0512	5.1084	5.1658	5.2235	5.2816	5.3400	95	191	286	382	477
57	-0.53987	5.4576	5.5170	5.5767	5.6366	5.6969	5.7575	5.8184	5.8797	5.9414	100	201	302	403	504
58	-0.60033	6.0657	6.1283	6.1914	6.2548	6.3185	6.3826	6.4471	6.5120	6.5772	106	213	319	426	533
59	-0.66428	6.7088	6.7752	6.8419	6.9091	6.9766	7.0446	7.1129	7.1817	7.2509	113	226	339	452	564
60	1.73205	1.73905	1.74610	1.75319	1.76032	1.76749	1.77471	1.78198	1.78929	1.79665	120	240	360	481	600
61	1.80405	1.81150	1.81900	1.82654	1.83413	1.84177	1.84946	1.85720	1.86500	1.87283	128	255	383	511	639
62	1.88073	1.88667	1.89667	1.90472	1.91282	1.92098	1.92920	1.93746	1.94579	1.95417	136	273	409	546	683
63	1.96261	1.97111	1.97967	1.98828	1.99695	2.00569	2.01449	2.02335	2.03227	2.04125	146	292	438	584	731
64	2.05030	2.05942	2.06860	2.07785	2.08716	2.09654	2.10600	2.11552	2.12511	2.13477	157	314	471	629	786
65	2.14451	2.15432	2.16420	2.17416	2.18419	2.19430	2.20449	2.21475	2.22510	2.23553	169	338	508	677	846
66	2.24604	2.25663	2.26730	2.27806	2.28891	2.29984	2.31086	2.32197	2.33317	2.34447	183	366	549	732	915
67	2.35585	2.36733	2.37891	2.39058	2.40235	2.41421	2.42618	2.43825	2.45043	2.46270	199	397	596	795	994
68	2.47509	2.48758	2.50018	2.51289	2.52571	2.53865	2.55170	2.56487	2.57815	2.59156	Mean differences no longer sufficiently accurate.				
69	2.60509	2.61874	2.63252	2.64642	2.66046	2.67462	2.68892	2.70335	2.71792	2.73263	Mean differences no longer sufficiently accurate.				
70	2.74748	2.76247	2.77761	2.79289	2.80833	2.82391	2.83965	2.85556	2.87161	2.88783	Mean differences no longer sufficiently accurate.				
71	2.90421	2.92076	2.93748	2.95437	2.97144	2.98868	3.00611	3.02372	3.04152	3.05950	Mean differences no longer sufficiently accurate.				
72	3.07768	3.09606	3.11464	3.13341	3.15240	3.17159	3.19100	3.21063	3.23048	3.25055	Mean differences no longer sufficiently accurate.				
73	3.27085	3.29139	3.31216	3.33317	3.35443	3.37594	3.39771	3.41973	3.44202	3.46458	Mean differences no longer sufficiently accurate.				
74	3.48741	3.51053	3.53393	3.55761	3.58160	3.60588	3.63048	3.65538	3.68061	3.70616	Mean differences no longer sufficiently accurate.				
75	3.73205	3.75828	3.78485	3.81177	3.83906	3.86671	3.89474	3.92316	3.95196	3.98117	Mean differences no longer sufficiently accurate.				
76	4.01078	4.04081	4.07127	4.10216	4.13350	4.16530	4.19756	4.23030	4.26352	4.29724	Mean differences no longer sufficiently accurate.				
77	4.33148	4.36623	4.40152	4.43735	4.47374	4.51071	4.54826	4.58641	4.62518	4.66458	Mean differences no longer sufficiently accurate.				
78	4.70463	4.74534	4.78673	4.82882	4.87162	4.91516	4.95945	5.00451	5.05037	5.09704	Mean differences no longer sufficiently accurate.				
79	5.14455	5.19293	5.24218	5.29235	5.34345	5.39552	5.44857	5.50264	5.55777	5.61397	Mean differences no longer sufficiently accurate.				
80	5.67128	5.72974	5.78938	5.85024	5.91236	5.97576	6.04051	6.10664	6.17419	6.24321	Mean differences no longer sufficiently accurate.				
81	6.31375	6.38587	6.45961	6.53503	6.61220	6.69116	6.77199	6.85475	6.93952	7.02637	Mean differences no longer sufficiently accurate.				
82	7.11537	7.20661	7.30018	7.39616	7.49465	7.59575	7.69957	7.80622	7.91582	8.02848	Mean differences no longer sufficiently accurate.				
83	8.14435	8.26356	8.38625	8.51259	8.64275	8.77689	8.91520	9.05789	9.20516	9.35724	Mean differences no longer sufficiently accurate.				
84	9.51436	9.6768	9.8448	10.019	10.199	10.385	10.579	10.780	10.988	11.205	Mean differences no longer sufficiently accurate.				
85	11.430	11.664	11.909	12.163	12.429	12.706	12.996	13.300	13.617	13.951	Mean differences no longer sufficiently accurate.				
86	14.301	14.669	15.056	15.464	15.895	16.350	16.832	17.343	17.886	18.464	Mean differences no longer sufficiently accurate.				
87	19.081	19.740	20.446	21.205	22.022	22.904	23.859	24.898	26.031	27.271	Mean differences no longer sufficiently accurate.				
88	28.636	30.145	31.821	33.694	35.801	38.188	40.917	44.066	47.740	52.081	Mean differences no longer sufficiently accurate.				
89	57.290	63.657	71.615	81.847	95.489	114.60	143.24	190.98	286.48	572.96	Mean differences no longer sufficiently accurate.				
90	∞										Mean differences no longer sufficiently accurate.				

NATURAL FUNCTIONS OF ANGLES

NATURAL COSINES

RADIAN S TO DEGREES

Radians	.000	.002	.004	.006	.008
.50	28 38.9	28 45.7	28 52.6	28 59.5	29 06.4
.51	29 13.3	29 20.1	29 27.0	29 33.9	29 40.8
.52	29 47.6	29 54.5	30 01.4	30 08.3	30 15.1
.53	30 22.0	30 28.9	30 35.8	30 42.6	30 49.5
.54	30 56.4	31 03.3	31 10.1	31 17.0	31 23.9
.55	31 30.8	31 37.6	31 44.5	31 51.4	31 58.3
.56	32 05.1	32 12.0	32 18.9	32 25.8	32 32.6
.57	32 39.5	32 46.4	32 53.3	33 00.1	33 07.0
.58	33 13.9	33 20.8	33 27.6	33 34.5	33 41.4
.59	33 48.3	33 55.1	34 02.0	34 08.9	34 15.8
.60	34 22.6	34 29.5	34 36.4	34 43.3	34 50.2
.61	34 57.0	35 03.9	35 10.8	35 17.7	35 24.5
.62	35 31.4	35 38.3	35 45.2	35 52.0	35 58.9
.63	36 05.8	36 12.7	36 19.5	36 26.4	36 33.3
.64	36 40.2	36 47.0	36 53.9	37 00.8	37 07.7
.65	37 14.5	37 21.4	37 28.3	37 35.2	37 42.0
.66	37 48.9	37 55.8	38 02.7	38 09.5	38 16.4
.67	38 23.3	38 30.2	38 37.0	38 43.9	38 50.8
.68	38 57.7	39 04.5	39 11.4	39 18.3	39 25.2
.69	39 32.0	39 38.9	39 45.8	39 52.7	39 59.5
.70	40 06.4	40 13.3	40 20.2	40 27.0	40 33.9
.71	40 40.8	40 47.7	40 54.6	41 01.4	41 08.3
.72	41 15.2	41 22.1	41 28.9	41 35.8	41 42.7
.73	41 49.6	41 56.4	42 03.3	42 10.2	42 17.1
.74	42 23.9	42 30.8	42 37.7	42 44.6	42 51.4
.75	42 58.3	43 05.2	43 12.1	43 18.9	43 25.8
.76	43 32.7	43 39.6	43 46.4	43 53.3	44 00.2
.77	44 07.1	44 13.9	44 20.8	44 27.7	44 34.6
.78	44 41.4	44 48.3	44 55.2	45 02.1	45 08.9
.79	45 15.8	45 22.7	45 29.6	45 36.4	45 43.3
.80	45 50.2	45 57.1	46 03.9	46 10.8	46 17.7
.81	46 24.6	46 31.5	46 38.3	46 45.2	46 52.1
.82	46 59.0	47 05.8	47 12.7	47 19.6	47 26.5
.83	47 33.3	47 40.2	47 47.1	47 54.0	48 00.8
.84	48 07.7	48 14.6	48 21.5	48 28.3	48 35.2
.85	48 42.1	48 49.0	48 55.8	49 02.7	49 09.6
.86	49 16.5	49 23.3	49 30.2	49 37.1	49 44.0
.87	49 50.8	49 57.7	50 04.6	50 11.5	50 18.3
.88	50 25.2	50 32.1	50 39.0	50 45.8	50 52.7
.89	50 59.6	51 06.5	51 13.3	51 20.2	51 27.1
.90	51 34.0	51 40.8	51 47.7	51 54.6	52 01.5
.91	52 08.3	52 15.2	52 22.1	52 29.0	52 35.9
.92	52 42.7	52 49.6	52 56.5	53 03.4	53 10.2
.93	53 17.1	53 24.0	53 30.9	53 37.7	53 44.6
.94	53 51.5	53 58.4	54 05.2	54 12.1	54 19.0
.95	54 25.9	54 32.7	54 39.6	54 46.5	54 53.4
.96	55 00.2	55 07.1	55 14.0	55 20.9	55 27.7
.97	55 34.6	55 41.5	55 48.4	55 55.2	56 02.1
.98	56 09.0	56 15.9	56 22.7	56 29.6	56 36.5
.99	56 43.4	56 50.2	56 57.1	57 04.0	57 10.9
1.00	57 17.7				

DEGREES TO RADIANS

MINUTES OF ARC TO RADIANS

TABLE A HOUR ANGLE

Lat.	45°	46°	47°	48°	49°	50°	51°	52°	53°	54°	55°	56°	57°	58°	59°	60°	Lat.
0	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	0
1	.02	.02	.02	.02	.02	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	1
2	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03	.02	.02	.02	.02	.02	.02	2
3	.05	.05	.05	.05	.05	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	3
4	.07	.07	.07	.06	.06	.06	.06	.05	.05	.05	.05	.05	.05	.05	.05	.05	4
5	.09	.08	.08	.08	.07	.07	.07	.07	.06	.06	.06	.06	.06	.05	.05	.05	5
6	.11	.10	.10	.09	.09	.09	.09	.08	.08	.08	.07	.07	.07	.07	.06	.06	6
7	.12	.12	.11	.11	.10	.10	.10	.10	.09	.09	.09	.08	.08	.08	.07	.07	7
8	.14	.14	.13	.13	.12	.12	.11	.11	.11	.10	.10	.09	.09	.09	.08	.08	8
9	.16	.15	.15	.14	.14	.13	.13	.12	.12	.12	.11	.11	.10	.10	.09	.09	9
10	.18	.17	.16	.16	.15	.15	.14	.14	.13	.13	.12	.12	.11	.11	.10	.10	10
11	.19	.19	.18	.18	.17	.16	.16	.15	.15	.14	.14	.13	.13	.12	.11	.11	11
12	.21	.21	.20	.19	.18	.18	.17	.17	.16	.15	.15	.14	.14	.13	.12	.12	12
13	.23	.22	.22	.21	.20	.19	.19	.18	.17	.17	.16	.16	.15	.14	.13	.13	13
14	.25	.24	.23	.22	.21	.20	.19	.19	.18	.17	.17	.16	.15	.14	.13	.13	14
15	.27	.26	.25	.24	.23	.22	.22	.21	.20	.19	.19	.18	.17	.16	.15	.15	15
16	.29	.28	.27	.26	.25	.24	.23	.22	.22	.21	.20	.19	.19	.18	.17	.17	16
17	.31	.30	.29	.28	.27	.26	.25	.24	.23	.22	.21	.21	.20	.19	.18	.18	17
18	.32	.31	.30	.29	.28	.27	.26	.25	.24	.24	.23	.22	.21	.20	.19	.19	18
19	.34	.33	.32	.31	.30	.29	.28	.27	.26	.25	.24	.23	.22	.21	.20	.20	19
20	.36	.35	.34	.33	.32	.31	.29	.28	.27	.26	.25	.24	.23	.22	.21	.20	20
21	.38	.37	.36	.35	.33	.32	.31	.30	.29	.28	.27	.26	.25	.24	.23	.22	21
22	.40	.39	.38	.36	.35	.34	.33	.32	.30	.29	.28	.27	.26	.25	.24	.23	22
23	.42	.41	.40	.38	.37	.36	.34	.33	.32	.31	.30	.29	.28	.27	.26	.25	23
24	.45	.43	.42	.40	.39	.37	.36	.35	.34	.32	.31	.30	.29	.28	.27	.26	24
25	.47	.45	.44	.42	.41	.39	.38	.36	.35	.34	.33	.31	.30	.29	.28	.27	25
26	.49	.47	.46	.44	.42	.41	.39	.38	.37	.35	.34	.33	.32	.30	.29	.28	26
27	.51	.49	.48	.46	.44	.43	.41	.40	.38	.37	.36	.34	.33	.32	.31	.29	27
28	.53	.51	.50	.48	.46	.45	.43	.42	.40	.39	.37	.36	.35	.33	.32	.31	28
29	.55	.54	.52	.50	.48	.47	.45	.43	.42	.40	.39	.37	.36	.35	.33	.32	29
30	.58	.56	.54	.52	.50	.48	.47	.45	.44	.42	.40	.39	.37	.36	.35	.33	30
31	.60	.58	.56	.54	.52	.50	.49	.47	.45	.44	.42	.40	.39	.38	.36	.35	31
32	.62	.60	.58	.56	.54	.52	.51	.49	.47	.45	.44	.42	.41	.39	.38	.36	32
33	.65	.63	.61	.58	.56	.55	.53	.51	.49	.47	.45	.44	.42	.41	.39	.37	33
34	.67	.65	.63	.61	.59	.57	.55	.53	.51	.49	.47	.46	.44	.42	.41	.39	34
35	.70	.68	.65	.63	.61	.59	.57	.55	.53	.51	.49	.47	.45	.44	.42	.40	35
36	.73	.70	.68	.65	.63	.61	.59	.57	.55	.53	.51	.49	.47	.45	.44	.42	36
37	.75	.73	.70	.68	.66	.63	.61	.59	.57	.55	.53	.51	.49	.47	.45	.44	37
38	.78	.75	.73	.70	.68	.66	.63	.61	.59	.57	.55	.53	.51	.49	.47	.45	38
39	.81	.78	.76	.73	.70	.68	.66	.63	.61	.59	.57	.55	.53	.51	.49	.47	39
40	.84	.81	.78	.76	.73	.70	.68	.66	.63	.61	.59	.57	.55	.52	.50	.48	40
41	.87	.84	.81	.78	.76	.73	.70	.68	.66	.63	.61	.59	.56	.54	.52	.50	41
42	.90	.87	.84	.81	.78	.76	.73	.70	.68	.65	.63	.61	.58	.56	.54	.52	42
43	.93	.90	.87	.84	.81	.78	.76	.73	.70	.68	.65	.63	.61	.58	.56	.54	43
44	.97	.93	.90	.87	.84	.81	.78	.75	.73	.70	.68	.65	.63	.60	.58	.56	44
45	1.00	.97	.93	.90	.87	.84	.81	.78	.75	.73	.70	.68	.65	.63	.60	.58	45
46	1.04	1.00	.97	.93	.90	.87	.84	.81	.78	.75	.73	.70	.67	.65	.62	.60	46
47	1.07	1.04	1.00	.97	.93	.90	.87	.84	.81	.78	.75	.72	.70	.67	.64	.62	47
48	1.11	1.07	1.04	1.00	.97	.93	.90	.87	.84	.81	.78	.75	.72	.69	.67	.64	48
49	1.15	1.11	1.07	1.04	1.00	.97	.93	.90	.87	.84	.81	.78	.75	.72	.69	.66	49
50	1.19	1.15	1.11	1.07	1.04	1.00	.97	.93	.90	.87	.83	.80	.77	.75	.72	.69	50
51	1.23	1.19	1.15	1.11	1.07	1.04	1.00	.97	.93	.90	.86	.83	.80	.77	.74	.71	51
52	1.28	1.24	1.19	1.15	1.11	1.07	1.04	1.00	.96	.93	.90	.86	.83	.80	.77	.74	52
53	1.33	1.28	1.24	1.19	1.15	1.11	1.07	1.04	1.00	.96	.93	.90	.86	.83	.80	.77	53
54	1.38	1.33	1.28	1.24	1.20	1.15	1.11	1.08	1.04	1.00	.96	.93	.89	.86	.83	.79	54
55	1.43	1.38	1.33	1.29	1.24	1.20	1.16	1.12	1.08	1.04	1.00	.96	.93	.89	.86	.82	55
56	1.48	1.43	1.38	1.34	1.29	1.24	1.20	1.16	1.12	1.08	1.04	1.00	.96	.93	.89	.86	56
57	1.54	1.49	1.44	1.39	1.34	1.29	1.25	1.20	1.16	1.12	1.08	1.04	1.00	.96	.93	.89	57
58	1.60	1.55	1.49	1.44	1.39	1.34	1.30	1.25	1.21	1.16	1.12	1.08	1.04	1.00	.96	.92	58
59	1.66	1.61	1.55	1.50	1.45	1.40	1.35	1.30	1.25	1.21	1.17	1.12	1.08	1.04	1.00	.96	59
60	1.73	1.67	1.62	1.56	1.51	1.45	1.40	1.35	1.31	1.26	1.21	1.17	1.12	1.08	1.04	1.00	60
	135°	134°	133°	132°	131°	130°	129°	128°	127°	126°	125°	124°	123°	122°	121°	120°	Lat.
	225°	226°	227°	228°	229°	230°	231°	232°	233°	234°	235°	236°	237°	238°	239°	240°	Lat.

HOUR ANGLE

A - Named opposite to Latitude, except when Hour Angle is between 90° and 270°.

A - Named opposite to Latitude, except when Hour Angle is between 90° and 270°.

A

TABLE B HOUR ANGLE

	45°	46°	47°	48°	49°	50°	51°	52°	53°	54°	55°	56°	57°	58°	59°	60°	
Dec.	315°	314°	313°	312°	311°	310°	309°	308°	307°	306°	305°	304°	303°	302°	301°	300°	Dec.
0	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	0
1	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	1
2	.05	.05	.05	.05	.05	.05	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	2
3	.07	.07	.07	.07	.07	.07	.07	.07	.07	.06	.06	.06	.06	.06	.06	.06	3
4	.10	.10	.10	.09	.09	.09	.09	.09	.09	.09	.09	.08	.08	.08	.08	.08	4
5	.12	.12	.12	.12	.12	.11	.11	.11	.11	.11	.11	.11	.10	.10	.10	.10	5
6	.15	.15	.14	.14	.14	.14	.14	.14	.13	.13	.13	.13	.13	.12	.12	.12	6
7	.17	.17	.17	.17	.16	.16	.16	.16	.15	.15	.15	.15	.14	.14	.14	.14	7
8	.20	.20	.19	.19	.19	.18	.18	.18	.17	.17	.17	.17	.16	.16	.16	.16	8
9	.22	.22	.22	.21	.21	.21	.20	.20	.20	.19	.19	.19	.18	.18	.18	.18	9
10	.25	.25	.24	.24	.23	.23	.23	.22	.22	.22	.21	.21	.21	.20	.20	.20	10
11	.27	.27	.27	.26	.26	.25	.25	.25	.24	.24	.24	.23	.23	.23	.22	.22	11
12	.30	.30	.29	.29	.28	.28	.27	.27	.27	.26	.26	.26	.25	.25	.25	.25	12
13	.33	.32	.32	.31	.31	.30	.30	.29	.29	.28	.28	.28	.27	.27	.27	.27	13
14	.35	.35	.34	.34	.33	.33	.32	.32	.31	.30	.30	.30	.29	.29	.29	.29	14
15	.38	.37	.37	.36	.36	.35	.34	.34	.33	.33	.32	.32	.31	.31	.31	.31	15
16	.41	.40	.39	.39	.38	.37	.37	.36	.36	.35	.35	.35	.34	.34	.33	.33	16
17	.43	.43	.42	.41	.41	.40	.39	.39	.38	.38	.37	.37	.36	.36	.35	.35	17
18	.46	.45	.44	.44	.43	.42	.42	.41	.41	.40	.40	.39	.39	.38	.38	.38	18
19	.49	.48	.47	.46	.46	.45	.44	.44	.43	.43	.42	.42	.41	.41	.40	.40	19
20	.51	.51	.50	.49	.48	.48	.47	.46	.46	.45	.44	.44	.43	.42	.42	.42	20
21	.54	.53	.52	.52	.51	.50	.49	.49	.48	.47	.47	.46	.45	.45	.44	.44	21
22	.57	.56	.55	.54	.54	.53	.52	.51	.51	.50	.49	.49	.48	.48	.47	.47	22
23	.60	.59	.58	.57	.56	.55	.55	.54	.53	.52	.52	.51	.51	.50	.49	.49	23
24	.63	.62	.61	.60	.59	.58	.57	.57	.56	.55	.54	.53	.53	.52	.51	.51	24
25	.66	.65	.64	.63	.62	.61	.60	.59	.58	.57	.56	.56	.55	.54	.54	.54	25
26	.69	.68	.67	.66	.65	.64	.63	.62	.61	.60	.60	.59	.58	.58	.57	.56	26
27	.72	.71	.70	.69	.68	.67	.66	.65	.64	.63	.62	.61	.61	.60	.59	.59	27
28	.75	.74	.73	.72	.70	.69	.68	.67	.67	.66	.65	.64	.63	.63	.62	.61	28
29	.78	.77	.76	.75	.73	.72	.71	.70	.69	.69	.68	.67	.66	.65	.65	.64	29
30	.82	.80	.79	.78	.76	.75	.74	.73	.72	.71	.70	.70	.69	.68	.67	.67	30
31	.85	.84	.82	.81	.80	.78	.77	.76	.75	.74	.73	.72	.72	.71	.70	.69	31
32	.88	.87	.85	.84	.83	.82	.80	.79	.78	.77	.76	.75	.75	.74	.73	.72	32
33	.92	.90	.89	.87	.86	.85	.84	.82	.81	.80	.79	.78	.77	.77	.76	.75	33
34	.96	.94	.92	.91	.89	.88	.87	.86	.84	.83	.82	.81	.80	.80	.79	.78	34
35	.99	.97	.96	.94	.93	.91	.90	.89	.88	.87	.85	.84	.83	.82	.81	.81	35
36	1.03	1.01	.99	.98	.96	.95	.93	.92	.91	.90	.89	.88	.87	.86	.85	.84	36
37	1.07	1.05	1.03	1.01	1.00	.98	.97	.96	.94	.93	.92	.91	.90	.89	.88	.87	37
38	1.11	1.09	1.07	1.05	1.04	1.02	1.00	.99	.98	.97	.95	.94	.93	.92	.91	.90	38
39	1.15	1.13	1.11	1.09	1.07	1.06	1.04	1.03	1.01	1.00	.99	.98	.97	.95	.94	.94	39
40	1.19	1.17	1.15	1.13	1.11	1.10	1.08	1.06	1.05	1.04	1.02	1.01	1.00	.99	.98	.97	40
41	1.23	1.21	1.19	1.17	1.15	1.13	1.12	1.10	1.09	1.07	1.06	1.05	1.04	1.03	1.01	1.00	41
42	1.28	1.25	1.23	1.21	1.19	1.18	1.16	1.14	1.13	1.11	1.10	1.09	1.07	1.06	1.05	1.04	42
43	1.32	1.30	1.28	1.25	1.24	1.22	1.20	1.18	1.17	1.15	1.14	1.12	1.11	1.10	1.09	1.08	43
44	1.37	1.34	1.32	1.30	1.28	1.26	1.24	1.23	1.21	1.19	1.18	1.16	1.15	1.14	1.13	1.12	44
45	1.41	1.39	1.37	1.35	1.33	1.31	1.29	1.27	1.25	1.24	1.22	1.21	1.19	1.18	1.17	1.15	45
46	1.47	1.44	1.42	1.39	1.37	1.35	1.33	1.31	1.30	1.28	1.26	1.25	1.23	1.22	1.21	1.20	46
47	1.52	1.49	1.47	1.44	1.42	1.40	1.38	1.36	1.34	1.33	1.31	1.29	1.28	1.26	1.25	1.24	47
48	1.57	1.54	1.52	1.49	1.47	1.45	1.43	1.41	1.39	1.37	1.36	1.34	1.32	1.31	1.30	1.28	48
49	1.63	1.60	1.57	1.55	1.52	1.50	1.48	1.46	1.44	1.42	1.40	1.39	1.37	1.36	1.34	1.33	49
50	1.69	1.66	1.63	1.60	1.58	1.56	1.53	1.51	1.49	1.47	1.45	1.44	1.42	1.41	1.39	1.38	50
51	1.75	1.72	1.69	1.66	1.64	1.61	1.59	1.57	1.55	1.53	1.51	1.49	1.47	1.46	1.44	1.43	51
52	1.81	1.78	1.75	1.72	1.70	1.67	1.65	1.62	1.60	1.58	1.56	1.54	1.53	1.51	1.49	1.48	52
53	1.88	1.84	1.81	1.79	1.76	1.73	1.71	1.68	1.66	1.64	1.62	1.60	1.58	1.56	1.55	1.53	53
54	1.95	1.91	1.88	1.85	1.82	1.80	1.77	1.75	1.72	1.70	1.68	1.66	1.64	1.62	1.61	1.59	54
55	2.02	1.99	1.95	1.92	1.89	1.86	1.84	1.81	1.79	1.77	1.74	1.72	1.70	1.68	1.67	1.65	55
56	2.10	2.06	2.03	2.00	1.96	1.94	1.91	1.88	1.86	1.83	1.81	1.79	1.77	1.75	1.73	1.71	56
57	2.18	2.14	2.11	2.07	2.04	2.01	1.98	1.95	1.93	1.90	1.88	1.86	1.84	1.82	1.80	1.78	57
58	2.27	2.22	2.19	2.15	2.12	2.09	2.06	2.03	2.00	1.98	1.95	1.93	1.91	1.89	1.87	1.85	58
59	2.36	2.31	2.28	2.24	2.21	2.17	2.14	2.11	2.08	2.06	2.03	2.01	1.98	1.96	1.94	1.92	59
60	2.45	2.41	2.37	2.33	2.29	2.26	2.23	2.20	2.17	2.14	2.11	2.09	2.07	2.04	2.02	2.00	60

HOUR ANGLE

B

B - Always named the same as Declination

B - Always named the same as Declination

TABLE C

Lat.	A. & B. CORRECTION.						Lat.			
	A \pm B = 30'	31'	32'	33'	34'	35'				
	36'	37'	38'	39'	40'	41'	42'	43'	44'	45' = A \pm B
AZIMUTHS										
0	73.3	72.8	72.3	71.7	71.2	70.7	70.2	69.7	69.2	68.7
5	73.4	72.8	72.3	71.8	71.3	70.8	70.3	69.8	69.3	68.8
10	73.5	73.0	72.5	72.0	71.5	71.0	70.5	70.0	69.5	69.0
14	73.7	73.2	72.7	72.2	71.7	71.2	70.7	70.2	69.7	69.3
18	74.1	73.6	73.1	72.6	72.1	71.6	71.1	70.6	70.1	69.6
20	74.3	73.8	73.3	72.8	72.3	71.8	71.3	70.8	70.3	69.9
22	74.5	74.0	73.5	73.0	72.5	72.0	71.5	71.1	70.6	69.7
24	74.7	74.2	73.7	73.2	72.7	72.3	71.8	71.3	70.9	70.4
26	74.9	74.4	74.0	73.5	73.0	72.5	72.1	71.6	71.1	70.7
28	75.2	74.7	74.2	73.8	73.3	72.8	72.4	71.9	71.5	71.0
30	75.4	75.0	74.5	74.1	73.6	73.1	72.7	72.2	71.8	71.3
31	75.6	75.1	74.7	74.2	73.8	73.3	72.9	72.4	72.0	71.5
32	75.7	75.3	74.8	74.4	73.9	73.5	73.0	72.6	72.1	71.7
33	75.9	75.4	75.0	74.5	74.1	73.6	73.2	72.8	72.3	71.9
34	76.0	75.6	75.1	74.7	74.3	73.8	73.4	72.9	72.5	72.1
35	76.2	75.8	75.3	74.9	74.4	74.0	73.6	73.1	72.7	72.3
36	76.4	75.9	75.5	75.1	74.6	74.2	73.8	73.3	72.9	72.5
37	76.5	76.1	75.7	75.2	74.8	74.4	74.0	73.5	73.1	72.7
38	76.7	76.3	75.8	75.4	75.0	74.6	74.2	73.7	73.3	72.9
39	76.9	76.5	76.0	75.6	75.2	74.8	74.4	74.0	73.5	73.1
40	77.1	76.6	76.2	75.8	75.4	75.0	74.6	74.2	73.8	73.4
41	77.2	76.8	76.4	76.0	75.6	75.2	74.8	74.4	74.0	73.6
42	77.4	77.0	76.6	76.2	75.8	75.4	75.0	74.6	74.2	73.8
43	77.6	77.2	76.8	76.4	76.0	75.6	75.2	74.9	74.5	74.1
44	77.8	77.4	77.0	76.6	76.3	75.9	75.5	75.1	74.7	74.3
45	78.0	77.6	77.3	76.9	76.5	76.1	75.7	75.3	75.0	74.6
46	78.2	77.8	77.5	77.1	76.7	76.3	76.0	75.6	75.2	74.8
47	78.4	78.1	77.7	77.3	76.9	76.6	76.2	75.8	75.5	75.1
48	78.6	78.3	77.9	77.5	77.2	76.8	76.5	76.1	75.7	75.3
49	78.9	78.5	78.1	77.8	77.4	77.1	76.7	76.4	76.0	75.6
50	79.1	78.7	78.4	78.0	77.7	77.3	77.0	76.6	76.3	75.9
51	79.3	79.0	78.6	78.3	77.9	77.6	77.2	76.9	76.6	76.2
52	79.5	79.2	78.9	78.5	78.2	77.8	77.5	77.2	76.9	76.5
53	79.8	79.4	79.1	78.8	78.4	78.1	77.8	77.4	77.1	76.8
54	80.0	79.7	79.3	79.0	78.7	78.4	78.1	77.7	77.4	77.0
55	80.2	79.9	79.6	79.3	79.0	78.6	78.3	78.0	77.7	77.3
56	80.5	80.2	79.9	79.5	79.2	78.9	78.6	78.3	78.0	77.6
57	80.7	80.4	80.1	79.8	79.5	79.2	78.9	78.6	78.3	77.9
58	81.0	80.7	80.4	80.1	79.8	79.5	79.2	78.9	78.6	78.2
59	81.2	80.9	80.6	80.4	80.1	79.8	79.5	79.2	78.9	78.5
60	81.5	81.2	80.9	80.6	80.4	80.1	79.8	79.5	79.2	78.9
61	81.7	81.5	81.2	80.9	80.6	80.4	80.1	79.8	79.6	79.3
62	82.0	81.7	81.5	81.2	80.9	80.7	80.4	80.1	79.9	79.6
63	82.2	82.0	81.7	81.5	81.2	81.0	80.7	80.5	80.2	80.9
64	82.5	82.3	82.0	81.8	81.5	81.3	81.0	80.8	80.5	80.2
65	82.8	82.5	82.3	82.1	81.8	81.6	81.3	81.1	80.9	80.6
66	83.0	82.8	82.6	82.4	82.1	81.9	81.7	81.4	81.2	80.9
67	83.3	83.1	82.9	82.7	82.4	82.2	82.0	81.8	81.6	81.3
68	83.6	83.4	83.2	83.0	82.7	82.5	82.3	82.1	81.9	81.7

A \pm B = 30' 31' 32' 33' 34' 35' 36' 37' 38' 39' 40' 41' 42' 43' 44' 45' = A \pm B

A & B Same Names } RULE TO FIND { A & B Different names
take Sum, (add). } C CORRECTION { take Difference (Sub.)

C CORRECTION, (A \pm B) is named the same as the greater of these quantities.

AZIMUTH takes combined names of C Correction and Hour Angle

TABLE C

Lat.	$A \pm B = 60'$	$62'$	$64'$	$66'$	$68'$	$70'$	A & B CORRECTION.				$-80'$	$-82'$	$-84'$	$-86'$	$-88'$	$-90' = A \pm B$	
							$-72'$	$-74'$	$-76'$	$-78'$							
0	59.0	58.2	57.4	56.6	55.8	55.0	54.2	53.5	52.8	52.0	51.3	50.6	50.0	49.3	48.7	48.0	
5	59.1	58.3	57.5	56.7	55.9	55.1	54.3	53.6	52.9	52.2	51.5	50.8	50.1	49.4	48.8	48.1	
10	59.4	58.6	57.8	57.0	56.2	55.4	54.7	53.9	53.2	52.5	51.8	51.1	50.4	49.7	49.1	48.4	
14	59.8	59.0	58.2	57.4	56.6	55.8	55.1	54.3	53.6	52.9	52.2	51.5	50.8	50.2	49.5	48.9	
18	60.3	59.5	58.7	57.9	57.1	56.3	55.6	54.9	54.1	53.4	52.7	52.1	51.4	50.7	50.1	49.4	
20	60.6	59.8	59.0	58.2	57.4	56.7	55.9	55.2	54.5	53.8	53.1	52.4	51.7	51.1	50.4	49.8	
22	60.9	60.1	59.3	58.5	57.8	57.0	56.3	55.5	54.8	54.1	53.4	52.8	52.1	51.4	50.8	50.2	
24	61.3	60.5	59.7	58.9	58.2	57.4	56.7	55.9	55.2	54.5	53.8	53.2	52.5	51.8	51.2	50.6	
26	61.7	60.9	60.1	59.3	58.6	57.8	57.1	56.4	55.7	55.0	54.3	53.6	52.9	52.3	51.7	51.0	
28	62.1	61.3	60.5	59.8	59.0	58.3	57.6	56.8	56.1	55.4	54.8	54.1	53.4	52.8	52.2	51.5	
30	62.5	61.8	61.0	60.2	59.5	58.8	58.1	57.3	56.6	56.0	55.3	54.6	54.0	53.3	52.7	52.1	
31	62.8	62.0	61.3	60.5	59.8	59.0	58.3	57.6	56.9	56.2	55.6	54.9	54.2	53.6	53.0	52.4	
32	63.0	62.3	61.5	60.8	60.0	59.3	58.6	57.9	57.2	56.5	55.8	55.2	54.5	53.9	53.3	52.7	
33	63.3	62.5	61.8	61.0	60.3	59.6	58.9	58.2	57.5	56.8	56.1	55.5	54.8	54.2	53.6	53.0	
34	63.6	62.8	62.1	61.3	60.6	59.9	59.2	58.5	57.8	57.1	56.4	55.8	55.1	54.5	53.9	53.3	
35	63.8	63.1	62.3	61.6	60.9	60.2	59.5	58.8	58.1	57.4	56.8	56.1	55.5	54.8	54.2	53.6	
36	64.1	63.4	62.6	61.9	61.2	60.5	59.8	59.1	58.4	57.7	57.1	56.4	55.8	55.2	54.6	53.9	
37	64.4	63.7	62.9	62.2	61.5	60.8	60.1	59.4	58.7	58.1	57.4	56.8	56.1	55.5	54.9	54.3	
38	64.7	64.0	63.2	62.5	61.8	61.1	60.4	59.8	59.1	58.4	57.8	57.1	56.5	55.9	55.3	54.7	
39	65.0	64.3	63.6	62.8	62.1	61.5	60.8	60.1	59.4	58.8	58.1	57.5	56.9	56.2	55.6	55.0	
40	65.3	64.6	63.9	63.2	62.5	61.8	61.1	60.5	59.8	59.1	58.5	57.9	57.2	56.6	56.0	55.4	
41	65.6	64.9	64.2	63.5	62.8	62.2	61.5	60.8	60.2	59.5	58.9	58.2	57.6	57.0	56.4	55.8	
42	66.0	65.3	64.6	63.9	63.2	62.5	61.9	61.2	60.5	59.9	59.3	58.6	58.0	57.4	56.8	56.2	
43	66.3	65.6	64.9	64.2	63.6	62.9	62.2	61.6	60.9	60.3	59.7	59.0	58.4	57.8	57.2	56.6	
44	66.7	66.0	65.3	64.6	63.9	63.3	62.6	62.0	61.3	60.7	60.1	59.5	58.9	58.3	57.7	57.1	
45	67.0	66.3	65.7	65.0	64.3	63.7	63.0	62.4	61.7	61.1	60.5	59.9	59.3	58.7	58.1	57.6	
46	67.4	66.7	66.0	65.4	64.7	64.1	63.4	62.8	62.2	61.5	60.9	60.3	59.7	59.1	58.6	58.0	
47	67.7	67.1	66.4	65.8	65.1	64.5	63.8	63.2	62.6	62.0	61.4	60.8	60.2	59.6	59.0	58.5	
48	68.1	67.5	66.8	66.2	65.5	64.9	64.3	63.7	63.0	62.4	61.8	61.2	60.7	60.1	59.5	58.9	
49	68.5	67.9	67.2	66.6	66.0	65.3	64.7	64.1	63.5	62.9	62.3	61.7	61.1	60.6	60.0	59.4	
50	68.9	68.3	67.6	67.0	66.4	65.8	65.2	64.6	64.0	63.4	62.8	62.2	61.6	61.1	60.5	60.0	
51	69.3	68.7	68.1	67.4	66.8	66.2	65.6	65.0	64.4	63.9	63.3	62.7	62.1	61.6	61.0	59.5	
52	69.7	69.1	68.5	67.9	67.3	66.7	66.1	65.5	64.9	64.4	63.8	63.2	62.7	62.1	61.6	59.0	
53	70.1	69.5	68.9	68.3	67.7	67.2	66.6	66.0	65.4	64.9	64.3	63.7	63.2	62.6	62.1	61.6	
54	70.6	70.0	69.4	68.8	68.2	67.6	67.1	66.5	65.9	65.4	64.8	64.3	63.7	63.2	62.6	62.1	
55	71.0	70.4	69.8	69.3	68.7	68.1	67.6	67.0	66.4	65.9	65.4	64.8	64.3	63.7	63.2	62.7	
56	71.5	70.9	70.3	69.7	69.2	68.6	68.1	67.5	67.0	66.4	65.9	65.4	64.9	64.3	63.8	63.3	
57	71.9	71.3	70.8	70.2	69.7	69.1	68.6	68.0	67.5	67.0	66.5	65.9	65.4	64.9	64.4	63.9	
58	72.4	71.8	71.3	70.7	70.2	69.6	69.1	68.6	68.1	67.5	67.0	66.5	66.0	65.5	65.0	64.5	
59	72.8	72.3	71.8	71.2	70.7	70.2	69.7	69.1	68.6	68.1	67.6	67.1	66.6	66.1	65.6	65.1	
60	73.3	72.8	72.3	71.7	71.2	70.7	70.2	69.7	69.2	68.7	68.2	67.7	67.2	66.7	66.3	65.8	
61	73.8	73.3	72.8	72.3	71.8	71.3	70.8	70.3	69.8	69.3	68.8	68.3	67.8	67.4	66.9	66.4	
62	74.3	73.8	73.3	72.8	72.3	71.8	71.3	70.8	70.4	69.9	69.4	68.9	68.5	68.0	67.6	67.1	
63	74.8	74.3	73.8	73.3	72.8	72.4	71.9	71.4	71.0	70.5	70.0	69.6	69.1	68.7	68.2	67.8	
64	75.3	74.8	74.3	73.9	73.4	72.9	72.5	72.0	71.6	71.1	70.7	70.2	69.8	69.3	68.9	68.5	
65	75.8	75.3	74.9	74.4	74.0	73.5	73.1	72.6	72.2	71.8	71.3	70.9	70.5	70.0	69.6	69.2	
66	76.3	75.8	75.4	75.0	74.5	74.1	73.7	73.2	72.8	72.4	72.0	71.6	71.1	70.7	70.3	69.9	
67	76.8	76.4	76.0	75.5	75.1	74.7	74.3	73.9	73.5	73.1	72.6	72.2	71.8	71.4	71.0	70.6	
68	77.3	76.9	76.5	76.1	75.7	75.3	74.9	74.5	74.1	73.7	73.3	72.9	72.5	72.1	71.8	71.4	

Lat. Lat.

$A \pm B = 60'$ $62'$ $64'$ $66'$ $68'$ $70'$ $72'$ $74'$ $76'$ $78'$ $80'$ $82'$ $84'$ $86'$ $88'$ $90' = A \pm B$

A & B Same Names } RULE TO FIND { A & B Different names
take Sum, (add) } C CORRECTION { take D difference (Sub.)

C CORRECTION, ($A \pm B$) is named the same as the greater of these quantities.

AZIMUTH takes combined names of C Correction and Hour Angle

TRUE AMPLITUDES

Lat.	Declination							
	25½°	26°	26½°	27°	27½°	28°	28½°	29°
5	◦	◦	◦	◦	◦	◦	◦	◦
2	25.5	26.0	26.5	27.0	27.5	28.0	28.5	29.0
4	25.6	26.1	26.6	27.1	27.6	28.1	28.6	29.1
6	25.7	26.2	26.7	27.2	27.7	28.2	28.7	29.2
8	25.8	26.3	26.8	27.3	27.8	28.3	28.8	29.3
10	25.9	26.4	26.9	27.5	28.0	28.5	29.0	29.5
12	26.1	26.6	27.1	27.7	28.2	28.7	29.2	29.7
14	26.3	26.9	27.4	27.9	28.4	28.9	29.5	30.0
16	26.6	27.1	27.7	28.2	28.7	29.2	29.8	30.3
18	26.9	27.5	28.0	28.5	29.0	29.6	30.1	30.7
20	27.3	27.8	28.3	28.9	29.4	30.0	30.5	31.1
22	27.7	28.2	28.8	29.3	29.9	30.4	31.0	31.5
24	28.1	28.7	29.2	29.8	30.4	30.9	31.5	32.1
26	28.6	29.2	29.8	30.3	30.9	31.5	32.1	32.6
28	29.2	29.8	30.4	30.9	31.5	32.1	32.7	33.3
30	29.8	30.4	31.0	31.6	32.2	32.8	33.4	34.1
31	30.1	30.8	31.4	32.0	32.6	33.2	33.8	34.5
32	30.5	31.1	31.7	32.4	33.0	33.6	34.2	34.9
33	30.9	31.5	32.1	32.8	33.4	34.0	34.7	35.3
34	31.3	31.9	32.6	33.2	33.8	34.5	35.1	35.8
35	31.7	32.4	33.0	33.7	34.3	35.0	35.6	36.3
36	32.2	32.8	33.5	34.1	34.8	35.5	36.1	36.8
37	32.6	33.3	34.0	34.6	35.3	36.0	36.7	37.4
38	33.1	33.8	34.5	35.2	35.9	36.6	37.3	38.0
39	33.6	34.3	35.0	35.8	36.5	37.2	37.9	38.6
40	34.2	34.9	35.6	36.4	37.1	37.8	38.5	39.3
41	34.8	35.5	36.2	37.0	37.7	38.5	39.2	40.0
42	35.4	36.2	36.9	37.7	38.4	39.2	39.9	40.7
43	36.1	36.8	37.6	38.4	39.2	39.9	40.7	41.5
44	36.8	37.5	38.3	39.2	39.9	40.7	41.6	42.4
45	37.5	38.3	39.1	39.9	40.8	41.6	42.4	43.3
46	38.3	39.1	40.0	40.8	41.7	42.5	43.4	44.3
47	39.1	40.0	40.9	41.7	42.6	43.5	44.4	45.3
48	40.0	40.9	41.8	42.7	43.6	44.5	45.5	46.4
49	41.0	41.9	42.9	43.8	44.7	45.7	46.7	47.7
50	42.0	43.0	44.0	44.9	45.9	46.9	47.9	49.0
50½	42.6	43.6	44.5	45.5	46.5	47.6	48.6	49.7
51	43.2	44.2	45.2	46.2	47.2	48.2	49.3	50.4
51½	43.8	44.8	45.8	46.8	47.9	49.0	50.0	51.2
52	44.4	45.4	46.4	47.5	48.6	49.7	50.8	52.0
52½	45.0	46.0	47.1	48.2	49.3	50.5	51.6	52.8
53	45.7	46.7	47.9	49.0	50.1	51.3	52.5	53.7
53½	46.4	47.5	48.6	49.8	50.9	52.1	53.3	54.6
54	47.1	48.2	49.4	50.6	51.8	53.0	54.3	55.6
54½	47.8	49.0	50.2	51.4	52.7	53.9	55.3	56.6
55	48.6	49.8	51.1	52.3	53.6	54.9	56.3	57.7
55½	49.5	50.7	52.0	53.3	54.6	56.0	57.4	58.9
56	50.3	51.6	52.9	54.3	55.7	57.1	58.6	60.1
56½	51.3	52.6	53.9	55.4	56.8	58.3	59.8	61.4
57	52.2	53.6	55.0	56.5	58.0	59.6	61.2	62.9
57½	53.2	54.7	56.1	57.7	59.2	60.7	62.6	65.0
58	54.3	55.8	57.4	58.9	60.6	62.4	64.2	66.2
58½	55.5	57.0	58.6	60.3	62.1	64.0	66.0	68.1
59	56.7	58.3	60.0	61.8	63.7	65.7	67.9	70.3
59½	58.0	59.7	61.5	63.4	65.5	67.7	70.1	72.8
60	59.4	61.2	63.2	65.2	67.4	69.9	72.6	75.8
60½	61.0	62.9	65.0	67.2	69.7	72.4	75.7	79.9
61	62.6	64.7	67.0	69.4	72.3	75.5	79.8	90.0
61½	64.5	66.7	69.3	72.1	75.4	79.7	90.0	—
62	66.2	69.0	71.9	75.2	79.6	90.0	—	—
62½	68.8	71.7	75.1	79.5	90.0	—	—	—

Amplitude Corrections

Lat.	Declination					
	0°	5°	10°	15°	20°	25°
◦	◦	◦	◦	◦	◦	◦
0	0.0	0.0	0.0	0.0	0.0	0.0
5	0.1	0.1	0.1	0.1	0.1	0.1
10	0.1	0.1	0.1	0.1	0.1	0.1
15	0.2	0.2	0.2	0.2	0.2	0.2
20	0.2	0.2	0.2	0.2	0.2	0.3
25	0.3	0.3	0.3	0.3	0.3	0.3
30	0.4	0.4	0.4	0.4	0.4	0.4
35	0.4	0.5	0.5	0.5	0.5	0.5
40	0.5	0.6	0.6	0.6	0.6	0.7
42	0.6	0.6	0.6	0.6	0.7	0.7
44	0.6	0.6	0.7	0.7	0.7	0.7
46	0.7	0.7	0.7	0.7	0.8	0.8
48	0.7	0.8	0.8	0.8	0.9	0.9
50	0.8	0.8	0.8	0.9	0.9	1.0
52	0.8	0.9	0.9	0.9	1.0	1.1
54	0.9	0.9	1.0	1.0	1.1	1.3
56	0.9	0.9	1.0	1.0	1.2	1.5
58	1.0	1.0	1.1	1.2	1.3	1.7
60	1.1	1.2	1.2	1.3	1.5	2.1
62	1.2	1.2	1.3	1.4	1.8	2.9

COMPASS ERROR BY AMPLITUDE

The true amplitudes given in the main table are calculated for the instant when the true altitude of the body is precisely 0° 00'. In the case of the sun (owing to the effects of dip, refraction and parallax) the lower limb at this instant will appear to be approximately half a diameter above the visible horizon. If the compass bearing is taken at that moment there will be no need to apply any correction.

However, should the bearing be observed when the sun's centre appears to be in the visible horizon, the correction obtained from the subsidiary table should be applied by being added to the observed azimuth reckoned from the elevated pole as shown in the example below. (Lat. 62° N., decl. 20° S.).

Obs'd. Azi.	S. 41°.5 E.
From elev. pole	N. 138°.5 E.
Corr'n.	+ 1°.8
Sum	N. 140°.3 E.
Corr'd. obs'd. Amp.	E. 50°.3 S.
T. Amp. from table	E. 46°.8 S.
Comp. Error	3°.5 W.

Observations of rising or setting stars and planets are seldom practicable but, if obtained, should be treated in the same way as those of the sun's centre.

In the case of the moon that body will be approximately one-third of a degree below the horizon at the moment when its true altitude is 0° 00'. If observed when its centre appears in the visible horizon, two-thirds of the correction from the subsidiary table should be subtracted from the observed azimuth reckoned from the elevated pole.

EX-MERIDIAN TABLE I
Latitude and Declination DIFFERENT NAME
 Change of Altitude in one minute from Meridian Passage = A

EX-MERIDIAN TABLE II

Reduction Plus to True Altitude at Upper Transit
HOUR ANGLE

A	0° 5'	0° 10'	0° 15'	0° 20'	0° 25'	0° 30'	0° 35'	0° 40'	0° 45'	0° 50'	0° 55'	1° 0'	A
	359° 55'	359° 50'	359° 45'	359° 40'	359° 35'	359° 30'	359° 25'	359° 20'	359° 15'	359° 10'	359° 5'	359° 0'	A
1	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.2	0.2	0.3	1
2	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.2	0.3	0.4	0.4	0.5	2
3	0.0	0.0	0.1	0.1	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	3
4	0.0	0.0	0.1	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.9	1.1	4
5	0.0	0.0	0.1	0.1	0.2	0.3	0.5	0.6	0.8	0.9	1.1	1.3	5
6	0.0	0.0	0.1	0.2	0.3	0.4	0.5	0.7	0.9	1.1	1.3	1.6	6
7	0.0	0.1	0.1	0.2	0.3	0.5	0.6	0.8	1.1	1.3	1.6	1.9	7
8	0.0	0.1	0.1	0.2	0.4	0.5	0.7	0.9	1.2	1.5	1.8	2.1	8
9	0.0	0.1	0.2	0.3	0.4	0.6	0.8	1.1	1.4	1.7	2.0	2.4	9
A	1° 5'	1° 10'	1° 15'	1° 20'	1° 25'	1° 30'	1° 35'	1° 40'	1° 45'	1° 50'	1° 55'	2° 0'	A
	358° 55'	358° 50'	358° 45'	358° 40'	358° 35'	358° 30'	358° 25'	358° 20'	358° 15'	358° 10'	358° 5'	358° 0'	A
1	0.3	0.4	0.4	0.5	0.5	0.6	0.7	0.7	0.8	0.9	1.0	1.1	1
2	0.6	0.7	0.8	0.9	1.0	1.2	1.3	1.5	1.6	1.8	1.9	2.1	2
3	0.9	1.1	1.3	1.5	1.7	1.8	2.0	2.2	2.5	2.7	3.0	3.2	3
4	1.2	1.4	1.7	1.9	2.2	2.4	2.7	3.0	3.3	3.6	3.9	4.3	4
5	1.6	1.8	2.1	2.4	2.7	3.0	3.4	3.7	4.1	4.5	4.9	5.3	5
6	1.9	2.2	2.5	2.9	3.2	3.6	4.0	4.4	4.9	5.4	5.9	6.4	6
7	2.2	2.5	2.9	3.3	3.7	4.2	4.7	5.2	5.7	6.3	6.9	7.5	7
8	2.5	2.9	3.3	3.8	4.3	4.8	5.4	5.9	6.5	7.1	7.8	8.5	8
9	2.8	3.3	3.8	4.3	4.9	5.4	6.0	6.7	7.4	8.1	8.8	9.6	9
A	2° 5'	2° 10'	2° 15'	2° 20'	2° 25'	2° 30'	2° 35'	2° 40'	2° 45'	2° 50'	2° 55'	3° 0'	A
	357° 55'	357° 50'	357° 45'	357° 40'	357° 35'	357° 30'	357° 25'	357° 20'	357° 15'	357° 10'	357° 5'	357° 0'	A
1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9	2.0	2.1	2.3	2.4	1
2	2.3	2.5	2.7	2.9	3.1	3.3	3.5	3.8	4.0	4.2	4.5	4.8	2
3	3.5	3.8	4.1	4.4	4.7	5.0	5.3	5.7	6.1	6.5	6.9	7.2	3
4	4.7	5.0	5.4	5.8	6.2	6.7	7.1	7.6	8.1	8.6	9.1	9.6	4
5	5.8	6.3	6.8	7.3	7.8	8.3	8.5	9.5	10.1	10.7	11.4	12.0	5
6	6.9	7.5	8.1	8.7	9.3	10.0	10.7	11.4	12.1	12.8	13.6	14.4	6
7	8.1	8.8	9.5	10.2	10.9	11.7	12.5	13.3	14.1	14.9	15.8	16.8	7
8	9.2	10.0	10.8	11.6	12.5	13.3	14.2	15.1	16.1	17.1	18.1	19.2	8
9	10.4	11.3	12.2	13.1	14.1	15.0	16.0	17.1	18.2	19.3	20.5	21.6	9
A	3° 5'	3° 10'	3° 15'	3° 20'	3° 25'	3° 30'	3° 35'	3° 40'	3° 45'	3° 50'	3° 55'	4° 0'	A
	356° 55'	356° 50'	356° 45'	356° 40'	356° 35'	356° 30'	356° 25'	356° 20'	356° 15'	356° 10'	356° 5'	356° 0'	A
1	2.5	2.7	2.8	2.9	3.1	3.3	3.5	3.6	3.8	4.0	4.1	4.3	1
2	5.1	5.3	5.6	5.9	6.2	6.5	6.8	7.1	7.5	7.8	8.2	8.5	2
3	7.6	8.0	8.5	8.9	9.4	9.8	10.3	10.8	11.3	11.8	12.3	12.8	3
4	10.1	10.7	11.3	11.9	12.5	13.1	13.7	14.4	15.0	15.7	16.4	17.1	4
5	12.7	13.4	14.1	14.8	15.6	16.3	17.1	17.9	18.8	19.6	20.5	21.3	5
6	15.2	16.0	16.9	17.8	18.7	19.6	20.5	21.5	22.5	23.5	24.5	25.6	6
7	17.7	18.7	19.7	20.7	21.8	22.9	24.0	25.1	26.3	27.5	28.7	29.9	7
8	20.3	21.4	22.5	23.7	24.9	26.1	27.4	28.7	30.0	31.3	32.7	34.1	8
9	22.8	24.1	25.4	26.7	28.0	29.4	30.8	32.3	33.8	35.3	36.9	38.4	9

Reduction Minus to True Altitude at Lower Transit

EX-MERIDIAN TABLE III
Second Correction Subtractive from First Correction

First Corr	Altitude																First Corr
	15°	30°	35°	40°	45°	50°	53°	56°	59°	62°	65°	68°	71°	74°	77°	80°	
15	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.2	15
30	0.0	0.1	0.1	0.1	0.1	0.2	0.2	0.2	0.2	0.2	0.3	0.3	0.4	0.5	0.6	0.7	30
35	0.1	0.1	0.1	0.2	0.2	0.2	0.2	0.3	0.3	0.3	0.4	0.4	0.5	0.6	0.8	1.0	35
40	0.1	0.1	0.2	0.2	0.2	0.3	0.3	0.3	0.4	0.4	0.5	0.6	0.7	0.8	1.0	1.3	40
45	0.1	0.2	0.2	0.3	0.3	0.4	0.4	0.4	0.5	0.6	0.6	0.7	0.9	1.0	1.3	1.7	45
50	0.1	0.2	0.3	0.3	0.4	0.4	0.5	0.5	0.6	0.7	0.8	0.9	1.1	1.3	1.6	2.1	50
55	0.1	0.3	0.3	0.4	0.4	0.5	0.6	0.7	0.7	0.8	0.9	1.1	1.3	1.5	1.9	2.5	55
60	0.1	0.3	0.4	0.4	0.5	0.6	0.7	0.7	0.9	1.0	1.1	1.3	1.5	1.8	2.3	3.0	60
65	0.2	0.4	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.2	1.3	1.5	1.8	2.1	2.7	3.5	65
70	0.2	0.4	0.5	0.6	0.7	0.9	0.9	1.1	1.2	1.3	1.5	1.8	2.1	2.5	3.1	4.0	70
75	0.2	0.5	0.6	0.7	0.8	1.0	1.1	1.2	1.4	1.5	1.8	2.0	2.4	2.9	3.5	4.6	75
80	0.3	0.5	0.7	0.8	0.9	1.1	1.2	1.4	1.6	1.8	2.0	2.3	2.7	3.3	4.0	5.3	80
85	0.3	0.6	0.7	0.9	1.1	1.3	1.4	1.6	1.8	2.0	2.3	2.6	3.1	3.7	4.5	6.0	85
90	0.3	0.7	0.8	1.0	1.2	1.4	1.6	1.8	2.0	2.2	2.5	2.9	3.4	4.1	5.1	6.7	90
93	0.3	0.7	0.9	1.1	1.3	1.5	1.7	1.9	2.1	2.4	2.7	3.1	3.7	4.4	5.5	7.1	93
96	0.4	0.8	0.9	1.1	1.3	1.6	1.8	2.0	2.2	2.5	2.9	3.3	3.9	4.7	5.8	7.6	96
99	0.4	0.8	1.0	1.2	1.4	1.7	1.9	2.1	2.4	2.7	3.1	3.5	4.1	5.0	6.2	8.1	99
102	0.4	0.9	1.1	1.3	1.5	1.8	2.0	2.2	2.5	2.9	3.2	3.7	4.4	5.3	6.6	8.6	102
105	0.4	0.9	1.1	1.4	1.6	1.9	2.1	2.4	2.7	3.0	3.4	4.0	4.7	5.6	7.0	9.1	105
108	0.5	1.0	1.2	1.4	1.7	2.0	2.3	2.5	2.8	3.2	3.6	4.2	4.9	5.9	7.3	9.6	108
111	0.5	1.0	1.3	1.5	1.8	2.1	2.4	2.7	3.0	3.4	3.8	4.4	5.2	6.3	7.8	10.2	111
114	0.5	1.1	1.3	1.6	1.9	2.3	2.5	2.8	3.2	3.6	4.1	4.7	5.5	6.6	8.2	10.7	114
117	0.5	1.1	1.4	1.7	2.0	2.4	2.6	3.0	3.3	3.7	4.3	4.9	5.8	6.9	8.6	11.3	117
120	0.6	1.2	1.5	1.8	2.1	2.5	2.8	3.1	3.5	3.9	4.5	5.2	6.1	7.3	9.1	11.9	120
123	0.6	1.3	1.5	1.8	2.2	2.6	2.9	3.3	3.7	4.1	4.7	5.5	6.4	7.6	9.5	12.5	123
126	0.6	1.3	1.6	1.9	2.3	2.8	3.1	3.4	3.8	4.3	5.0	5.7	6.7	8.0	10.0	13.1	126
129	0.7	1.4	1.7	2.0	2.4	2.9	3.2	3.6	4.0	4.6	5.2	6.0	7.0	8.4	10.5	13.7	129
132	0.7	1.5	1.8	2.1	2.5	3.0	3.4	3.8	4.2	4.8	5.4	6.3	7.4	8.8	11.0	14.4	132
135	0.7	1.5	1.9	2.2	2.6	3.2	3.5	3.9	4.4	5.0	5.7	6.6	7.7	9.2	11.5	15.0	135
138	0.7	1.6	1.9	2.3	2.8	3.3	3.7	4.1	4.6	5.2	5.9	6.9	8.0	9.7	12.0	15.7	138
141	0.8	1.7	2.0	2.4	2.9	3.5	3.8	4.3	4.8	5.4	6.2	7.2	8.4	1.0	12.5	16.4	141

EX-MERIDIAN TABLE IV

Limits of Hour Angle or Time 'before or after' Meridian Passage

A	Hour Angle								
"	m	"	m	"	m	"	m	"	m
52.2	4	7.54	17	3.37	30	1.92	43	1.21	56
40.2	5	6.94	18	3.20	31	1.85	44	1.17	57
31.4	6	6.44	19	3.05	32	1.78	45	1.13	58
25.4	7	6.00	20	2.92	33	1.72	46	1.09	59
21.2	8	5.64	21	2.79	34	1.66	47	1.06	60
18.0	9	5.26	22	2.67	35	1.60	48	1.02	61
15.7	10	4.94	23	2.55	36	1.54	49	0.99	62
13.8	11	4.60	24	2.45	37	1.49	50	0.96	63
12.2	12	4.40	25	2.35	38	1.43	51	0.93	64
10.9	13	4.17	26	2.25	39	1.38	52	0.90	65
9.90	14	3.94	27	2.16	40	1.34	53	0.87	66
9.02	15	3.73	28	2.08	41	1.29	54		
8.22	16	3.54	29	2.00	42	1.25	55		

AZIMUTH	CHANGE of HOUR ANGLE with ALTITUDE												
	LATITUDE												
	0°	3°	6°	9°	12°	15°	18°	21°	24°	27°	30°	33°	36°
0
1	57.30	57.38	57.61	58.01	58.58	59.32	60.25	61.38	62.72	64.31	66.16	68.32	70.83
2	28.65	28.69	28.81	29.01	29.29	29.66	30.13	30.69	31.37	32.16	33.09	34.17	35.42
3	19.11	19.13	19.21	19.35	19.53	19.78	20.09	20.47	20.92	21.44	22.06	22.78	23.62
4	14.34	14.36	14.41	14.51	14.66	14.84	15.07	15.36	15.69	16.09	16.55	17.09	17.72
5	11.47	11.49	11.54	11.62	11.73	11.88	12.06	12.29	12.56	12.88	13.25	13.68	14.18
6	9.57	9.58	9.62	9.69	9.78	9.90	10.06	10.25	10.47	10.74	11.05	11.41	11.83
7	8.21	8.22	8.25	8.31	8.39	8.50	8.63	8.79	8.98	9.21	9.48	9.78	10.14
8	7.19	7.20	7.23	7.28	7.35	7.44	7.56	7.70	7.87	8.06	8.30	8.57	8.88
9	6.39	6.40	6.43	6.47	6.54	6.62	6.72	6.85	7.00	7.17	7.38	7.62	7.90
10	5.76	5.77	5.79	5.83	5.89	5.96	6.06	6.17	6.30	6.46	6.65	6.87	7.12
11	5.24	5.25	5.27	5.31	5.36	5.43	5.51	5.61	5.74	5.88	6.05	6.25	6.48
12	4.81	4.82	4.84	4.87	4.92	4.98	5.06	5.15	5.27	5.40	5.55	5.74	5.95
13	4.45	4.45	4.47	4.50	4.55	4.60	4.67	4.76	4.87	4.99	5.13	5.30	5.50
14	4.13	4.14	4.16	4.19	4.23	4.28	4.35	4.43	4.53	4.64	4.77	4.93	5.11
15	3.86	3.87	3.89	3.91	3.95	4.00	4.06	4.14	4.23	4.34	4.46	4.61	4.78
16	3.63	3.63	3.65	3.67	3.71	3.76	3.82	3.89	3.97	4.07	4.19	4.33	4.48
17	3.42	3.43	3.44	3.46	3.50	3.54	3.60	3.66	3.74	3.84	3.95	4.08	4.23
18	3.24	3.24	3.25	3.28	3.31	3.35	3.40	3.47	3.54	3.63	3.74	3.86	4.00
19	3.07	3.08	3.09	3.11	3.14	3.18	3.23	3.29	3.36	3.45	3.55	3.66	3.80
20	2.92	2.93	2.94	2.96	2.99	3.03	3.07	3.13	3.20	3.28	3.38	3.49	3.61
21	2.79	2.79	2.81	2.83	2.85	2.89	2.93	2.99	3.06	3.13	3.22	3.33	3.45
22	2.67	2.67	2.68	2.70	2.73	2.76	2.81	2.86	2.92	3.00	3.08	3.18	3.30
24	2.46	2.46	2.47	2.49	2.51	2.55	2.59	2.63	2.69	2.76	2.84	2.93	3.04
26	2.28	2.28	2.29	2.31	2.33	2.36	2.40	2.44	2.50	2.56	2.63	2.72	2.82
28	2.13	2.13	2.14	2.16	2.18	2.21	2.24	2.28	2.33	2.39	2.46	2.54	2.63
30	2.00	2.00	2.01	2.03	2.05	2.07	2.10	2.14	2.19	2.25	2.31	2.39	2.47
32	1.89	1.89	1.90	1.91	1.93	1.95	1.98	2.02	2.07	2.12	2.18	2.25	2.33
34	1.79	1.79	1.80	1.81	1.83	1.85	1.88	1.92	1.96	2.01	2.07	2.13	2.21
36	1.70	1.70	1.71	1.72	1.74	1.76	1.79	1.82	1.86	1.91	1.96	2.03	2.10
38	1.62	1.63	1.63	1.65	1.66	1.68	1.71	1.74	1.78	1.82	1.88	1.94	2.01
40	1.56	1.56	1.56	1.58	1.59	1.61	1.64	1.67	1.70	1.75	1.80	1.86	1.92
42	1.49	1.50	1.50	1.51	1.53	1.55	1.57	1.60	1.64	1.68	1.73	1.78	1.85
44	1.44	1.44	1.45	1.46	1.47	1.49	1.51	1.54	1.58	1.62	1.66	1.72	1.78
46	1.39	1.39	1.40	1.41	1.42	1.44	1.46	1.49	1.52	1.56	1.61	1.66	1.72
48	1.35	1.35	1.35	1.36	1.38	1.40	1.42	1.44	1.47	1.51	1.55	1.60	1.66
50	1.31	1.31	1.31	1.32	1.34	1.35	1.37	1.40	1.43	1.47	1.51	1.56	1.61
52	1.27	1.27	1.28	1.29	1.30	1.31	1.33	1.36	1.39	1.42	1.47	1.51	1.57
55	1.22	1.22	1.23	1.24	1.25	1.26	1.28	1.31	1.34	1.37	1.41	1.46	1.51
60	1.16	1.16	1.16	1.17	1.18	1.20	1.21	1.24	1.26	1.30	1.33	1.38	1.43
65	1.10	1.11	1.11	1.12	1.13	1.14	1.16	1.18	1.21	1.24	1.27	1.32	1.36
70	1.06	1.07	1.07	1.08	1.09	1.10	1.12	1.14	1.17	1.19	1.23	1.27	1.32
75	1.04	1.04	1.04	1.05	1.06	1.07	1.09	1.11	1.13	1.16	1.19	1.23	1.28
80	1.02	1.02	1.02	1.03	1.04	1.05	1.07	1.09	1.11	1.14	1.17	1.21	1.26
85	1.00	1.01	1.01	1.02	1.03	1.04	1.06	1.08	1.10	1.13	1.16	1.20	1.24
90	1.00	1.00	1.01	1.01	1.02	1.04	1.05	1.07	1.09	1.12	1.15	1.19	1.24

AZIMUTH	CHANGE OF HOUR ANGLE with ALTITUDE											
	LATITUDE											
	39°	42°	45°	48°	51°	54°	57°	60°	63°	66°	69°	72°
0
1	73.73	77.10	81.03	85.63	91.05	97.48	105.20	114.60	126.21	140.88	159.89	185.43
2	36.87	38.56	40.52	42.82	45.53	48.75	52.61	57.31	63.11	70.45	79.96	92.73
3	24.59	25.71	27.02	28.56	30.36	32.51	35.08	38.21	42.09	46.98	53.32	61.83
4	18.45	19.29	20.27	21.42	22.78	24.39	26.32	28.67	31.58	35.25	40.00	46.39
5	14.76	15.44	16.23	17.15	18.23	19.52	21.07	22.95	25.27	28.21	32.02	37.13
6	12.31	12.87	13.53	14.30	15.20	16.28	17.57	19.13	21.04	23.48	26.65	30.91
7	10.56	11.04	11.60	12.26	13.04	13.96	15.07	16.41	18.07	20.17	22.90	26.55
8	9.25	9.67	10.16	10.74	11.42	12.22	13.19	14.37	15.83	17.67	20.05	23.25
9	8.23	8.60	9.04	9.55	10.16	10.88	11.74	12.78	14.08	15.72	17.84	20.69
10	7.41	7.75	8.14	8.61	9.15	9.80	10.57	11.52	12.68	14.16	16.07	18.64
11	6.74	7.05	7.41	7.83	8.33	8.92	9.62	10.48	11.54	12.89	14.63	16.96
12	6.19	6.47	6.80	7.19	7.64	8.18	8.83	9.62	10.59	11.83	13.42	15.56
13	5.72	5.98	6.29	6.64	7.06	7.56	8.16	8.89	9.79	10.93	12.40	14.39
14	5.32	5.56	5.85	6.18	6.57	7.03	7.59	8.27	9.11	10.16	11.53	13.38
15	4.97	5.20	5.46	5.77	6.14	6.57	7.09	7.73	8.51	9.50	10.78	12.50
16	4.67	4.88	5.13	5.42	5.77	6.17	6.66	7.26	7.99	8.92	10.12	11.74
17	4.40	4.60	4.84	5.11	5.44	5.82	6.28	6.84	7.53	8.41	9.54	11.07
18	4.16	4.36	4.58	4.84	5.14	5.51	5.94	6.47	7.13	7.96	9.03	10.47
19	3.95	4.13	4.34	4.59	4.88	5.23	5.64	6.14	6.77	7.55	8.57	9.94
20	3.76	3.93	4.14	4.37	4.65	4.97	5.37	5.85	6.44	7.19	8.16	9.46
21	3.59	3.76	3.95	4.17	4.43	4.75	5.12	5.58	6.15	6.86	7.79	9.03
22	3.44	3.59	3.78	3.99	4.24	4.54	4.90	5.34	5.88	6.56	7.45	8.64
24	3.16	3.31	3.48	3.67	3.91	4.18	4.51	4.92	5.42	6.04	6.86	7.96
26	2.94	3.07	3.23	3.41	3.63	3.88	4.19	4.56	5.02	5.61	6.37	7.38
28	2.74	2.87	3.01	3.18	3.39	3.62	3.91	4.26	4.69	5.24	5.94	6.89
30	2.57	2.69	2.83	2.99	3.18	3.40	3.67	4.00	4.41	4.92	5.58	6.47
32	2.43	2.54	2.67	2.82	3.00	3.21	3.47	3.77	4.16	4.64	5.27	6.11
34	2.30	2.41	2.53	2.67	2.84	3.04	3.28	3.58	3.94	4.40	4.99	5.79
36	2.19	2.29	2.41	2.54	2.70	2.89	3.12	3.40	3.75	4.18	4.75	5.51
38	2.09	2.19	2.30	2.43	2.58	2.76	2.98	3.25	3.58	3.99	4.53	5.26
40	2.00	2.09	2.20	2.33	2.47	2.65	2.86	3.11	3.43	3.82	4.34	5.03
42	1.92	2.01	2.11	2.23	2.38	2.54	2.74	2.99	3.29	3.67	4.17	4.84
44	1.85	1.94	2.04	2.15	2.29	2.45	2.64	2.88	3.17	3.54	4.02	4.66
46	1.79	1.87	1.97	2.08	2.21	2.37	2.55	2.78	3.06	3.42	3.88	4.50
48	1.73	1.81	1.90	2.01	2.14	2.29	2.47	2.69	2.96	3.31	3.75	4.35
50	1.68	1.76	1.85	1.95	2.07	2.22	2.40	2.61	2.88	3.21	3.64	4.22
52	1.63	1.71	1.80	1.90	2.02	2.16	2.33	2.54	2.80	3.12	3.54	4.11
55	1.57	1.64	1.73	1.82	1.94	2.08	2.24	2.44	2.69	3.00	3.41	3.95
60	1.49	1.55	1.63	1.73	1.84	1.96	2.12	2.31	2.54	2.84	3.22	3.74
65	1.42	1.49	1.56	1.65	1.75	1.88	2.03	2.21	2.43	2.71	3.08	3.57
70	1.37	1.43	1.51	1.59	1.69	1.81	1.95	2.13	2.34	2.62	2.97	3.44
75	1.33	1.39	1.46	1.55	1.65	1.76	1.90	2.07	2.28	2.55	2.89	3.35
80	1.31	1.37	1.44	1.52	1.61	1.73	1.86	2.03	2.24	2.50	2.83	3.29
85	1.29	1.35	1.42	1.50	1.60	1.71	1.84	2.01	2.21	2.47	2.80	3.25
90	1.29	1.35	1.41	1.49	1.59	1.70	1.84	2.00	2.20	2.46	2.79	3.24

CHANGE OF ALTITUDE IN ONE MINUTE OF TIME

AZIMUTH

Lat.	40°	42½°	45°	47½°	50°	52°	55°	57½°	60°	62½°	65°	67½°	70°	75°	80°	90°	Lat.
0°	9.6	10.1	10.6	11.0	11.5	11.9	12.3	12.7	13.0	13.3	13.6	13.8	14.1	14.5	14.8	15.0	0°
4°	9.6	10.1	10.6	11.0	11.5	11.9	12.3	12.6	13.0	13.3	13.6	13.8	14.1	14.5	14.7	15.0	4°
8°	9.5	10.0	10.5	11.0	11.4	11.8	12.2	12.5	12.9	13.2	13.5	13.7	14.0	14.4	14.6	14.9	8°
12°	9.4	9.9	10.4	10.8	11.2	11.6	12.0	12.3	12.7	13.0	13.3	13.5	13.8	14.2	14.4	14.7	12°
16°	9.3	9.8	10.2	10.6	11.0	11.4	11.8	12.1	12.5	12.8	13.1	13.3	13.5	13.9	14.2	14.4	16°
20°	9.1	9.5	10.0	10.4	10.8	11.1	11.5	11.8	12.2	12.5	12.8	13.0	13.2	13.6	13.9	14.1	20°
24°	8.8	9.2	9.7	10.2	10.5	10.8	11.2	11.5	11.9	12.2	12.4	12.6	12.9	13.2	13.5	13.7	24°
26°	8.7	9.1	9.5	9.9	10.3	10.6	11.0	11.3	11.7	12.0	12.2	12.5	12.7	13.0	13.3	13.5	26°
28°	8.5	9.0	9.4	9.7	10.1	10.4	10.8	11.1	11.5	11.7	12.0	12.2	12.4	12.8	13.1	13.2	28°
30°	8.3	8.8	9.2	9.6	9.9	10.2	10.6	10.9	11.2	11.5	11.8	12.0	12.2	12.5	12.8	13.0	30°
32°	8.2	8.6	9.0	9.4	9.7	10.0	10.4	10.7	11.0	11.3	11.5	11.8	12.0	12.3	12.5	12.7	32°
34°	8.0	8.4	8.8	9.2	9.5	9.8	10.2	10.5	10.8	11.0	11.3	11.5	11.7	12.0	12.3	12.4	34°
36°	7.8	8.2	8.6	9.0	9.3	9.6	9.9	10.2	10.5	10.7	11.0	11.2	11.4	11.7	12.0	12.1	36°
38°	7.6	8.0	8.4	8.7	9.1	9.4	9.7	10.0	10.2	10.5	10.7	10.9	11.1	11.4	11.6	11.8	38°
40°	7.4	7.7	8.1	8.5	8.8	9.1	9.4	9.7	10.0	10.2	10.4	10.6	10.8	11.1	11.3	11.5	40°
42°	7.2	7.5	7.9	8.2	8.5	8.8	9.1	9.4	9.7	9.9	10.1	10.3	10.5	10.8	11.0	11.1	42°
44°	6.9	7.2	7.6	8.0	8.3	8.6	8.8	9.0	9.3	9.6	9.8	10.0	10.1	10.4	10.6	10.8	44°
46°	6.7	7.0	7.4	7.7	8.0	8.3	8.5	8.7	9.0	9.2	9.4	9.6	9.8	10.1	10.3	10.4	46°
48°	6.5	6.8	7.1	7.4	7.7	8.0	8.2	8.5	8.7	8.9	9.1	9.3	9.4	9.7	9.9	10.0	48°
49°	6.3	6.6	6.9	7.2	7.6	7.8	8.0	8.3	8.5	8.7	8.9	9.1	9.2	9.5	9.7	9.8	49°
50°	6.2	6.5	6.8	7.1	7.4	7.6	7.9	8.1	8.3	8.5	8.7	8.9	9.1	9.3	9.5	9.6	50°
51°	6.0	6.3	6.6	6.8	7.2	7.5	7.7	7.9	8.1	8.3	8.5	8.7	8.9	9.1	9.3	9.4	51°
52°	5.9	6.2	6.5	6.8	7.1	7.4	7.6	7.8	8.0	8.2	8.4	8.6	8.7	8.9	9.1	9.2	52°
53°	5.8	6.1	6.4	6.7	7.0	7.3	7.5	7.7	7.9	8.1	8.3	8.4	8.5	8.7	8.9	9.0	53°
54°	5.7	6.0	6.2	6.5	6.8	7.0	7.2	7.4	7.6	7.8	8.0	8.2	8.3	8.5	8.7	8.8	54°
55°	5.5	5.8	6.1	6.3	6.6	6.8	7.0	7.2	7.5	7.6	7.8	8.0	8.1	8.3	8.5	8.6	55°
56°	5.4	5.7	5.9	6.2	6.4	6.7	6.9	7.1	7.3	7.4	7.6	7.8	7.9	8.1	8.3	8.4	56°
57°	5.2	5.5	5.8	6.0	6.3	6.5	6.7	6.9	7.1	7.2	7.4	7.6	7.7	7.9	8.0	8.2	57°
58°	5.1	5.3	5.6	5.8	6.1	6.3	6.5	6.7	6.9	7.0	7.2	7.4	7.5	7.7	7.8	8.0	58°
59°	5.0	5.2	5.5	5.7	5.9	6.1	6.3	6.5	6.7	6.9	7.0	7.2	7.3	7.5	7.6	7.7	59°
60°	4.8	5.1	5.3	5.5	5.7	5.9	6.1	6.3	6.5	6.7	6.8	6.9	7.0	7.2	7.4	7.5	60°
61°	4.8	5.1	5.3	5.5	5.7	5.9	6.1	6.3	6.5	6.6	6.7	6.8	6.9	7.0	7.2	7.3	61°
62°	4.5	4.7	5.0	5.2	5.4	5.6	5.8	5.9	6.1	6.2	6.4	6.5	6.6	6.7	6.9	7.0	62°
63°	4.3	4.5	4.8	5.0	5.2	5.4	5.6	5.7	5.9	6.0	6.2	6.3	6.4	6.5	6.7	6.8	63°
64°	4.2	4.4	4.7	4.9	5.1	5.2	5.4	5.5	5.7	5.8	6.0	6.1	6.2	6.3	6.4	6.5	64°
65°	4.1	4.3	4.5	4.7	4.9	5.0	5.2	5.3	5.5	5.6	5.8	5.9	6.0	6.1	6.2	6.3	65°
66°	4.0	4.1	4.3	4.5	4.7	4.9	5.0	5.1	5.3	5.4	5.5	5.6	5.7	5.9	6.0	6.1	66°
67°	3.8	4.0	4.1	4.3	4.5	4.7	4.8	5.0	5.1	5.2	5.3	5.4	5.5	5.7	5.8	5.9	67°
68°	3.6	3.8	4.0	4.1	4.3	4.5	4.6	4.8	4.9	5.0	5.1	5.2	5.4	5.5	5.6	5.8	68°
69°	3.5	3.6	3.8	4.0	4.1	4.3	4.4	4.6	4.7	4.8	4.9	5.0	5.1	5.3	5.4	5.6	69°
70°	3.3	3.5	3.6	3.7	3.9	4.1	4.2	4.3	4.5	4.6	4.7	4.7	4.8	4.9	5.0	5.1	70°
71°	3.1	3.3	3.5	3.6	3.7	3.9	4.0	4.1	4.2	4.3	4.4	4.5	4.6	4.7	4.8	4.9	71°
72°	2.9	3.1	3.3	3.4	3.5	3.7	3.8	3.9	4.0	4.1	4.2	4.2	4.3	4.4	4.5	4.6	72°
73°	2.8	3.0	3.1	3.3	3.4	3.5	3.6	3.7	3.8	3.9	4.0	4.1	4.1	4.2	4.3	4.4	73°
74°	2.6	2.8	2.9	3.1	3.2	3.3	3.4	3.5	3.6	3.7	3.8	3.9	3.9	3.9	4.0	4.1	74°
75°	2.5	2.6	2.7	2.9	3.0	3.1	3.2	3.3	3.4	3.4	3.5	3.5	3.6	3.7	3.8	3.9	75°
Lat.	40°	42½°	45°	47½°	50°	52°	55°	57½°	60°	62½°	65°	67½°	70°	75°	80°	90°	Lat.

AUGMENTATION OF THE MOON'S SEMI - DIAMETER

DIP OF THE SEA HORIZON

MEAN REFRACTION

ADDITIONAL REFRACTION CORRECTIONS
FOR AIR TEMPERATURE

Atmospheric Pressure 1000mbs (29.5ins) Temperature 10°C (50°F)						To be applied to the Apparent Altitude										
App. Alt.	Refr.	App. Alt.		Refr.		App. Alt.	Refr.	Air Temperature - °C								
		°	'	°	'			-5°	0°	5°	10°	15°	20°	25°	30°	35°
0 00	-33.9	4 00	-11.5	12 00	-4.4	0 00	-3.4	-2.0	-1.0	0.0	+1.0	+1.9	+2.8	+3.7	+4.7	
05	32.8	10 00	11.1	20 00	4.3	20	2.7	1.8	0.9	0.0	0.9	1.5	2.2	3.1	3.7	
10	31.8	20 00	10.8	40 00	4.2	40	2.4	1.6	0.8	0.0	0.8	1.3	2.0	2.7	3.3	
15	30.8	30 00	10.5	13 00	4.0	1 00	2.0	1.4	0.7	0.0	0.7	1.2	1.8	2.4	2.9	
20	29.9	40 00	10.2	20 00	3.9	20	1.8	1.2	0.6	0.0	0.6	1.0	1.5	2.0	2.6	
25	29.0	50 00	9.9	40 00	3.9	40	1.5	1.0	0.5	0.0	0.5	0.9	1.3	1.8	2.2	
0 30	-28.2	5 00	-9.7	14 00	-3.8	2 00	-1.3	-0.9	-0.4	0.0	+0.4	+0.8	+1.2	+1.5	+1.9	
35	27.4	10 00	9.4	20 00	3.7	20	1.2	0.8	0.4	0.0	0.4	0.7	1.1	1.4	1.7	
40	26.6	20 00	9.2	40 00	3.6	3 00	1.0	0.7	0.3	0.0	0.3	0.6	1.0	1.2	1.5	
45	25.9	30 00	8.9	15 00	3.5	20	1.0	0.6	0.3	0.0	0.3	0.6	0.9	1.1	1.4	
50	25.2	40 00	8.7	20 00	3.4	40	0.9	0.6	0.3	0.0	0.3	0.6	0.8	1.0	1.3	
55	24.6	50 00	8.5	40 00	3.4	4 00	-0.8	-0.6	-0.3	0.0	+0.3	+0.5	+0.8	+1.0	+1.2	
1 00	-23.9	6 00	-8.3	16 00	-3.3	5	0.7	0.5	0.2	0.0	0.2	0.4	0.7	0.8	1.0	
05	23.3	10 00	8.1	17 00	3.1	6	0.6	0.4	0.2	0.0	0.2	0.4	0.6	0.7	0.9	
10	22.7	20 00	7.9	18 00	2.9	7	0.5	0.4	0.2	0.0	0.2	0.3	0.5	0.6	0.8	
15	22.1	30 00	7.7	19 00	2.7	8	0.5	0.3	0.2	0.0	0.1	0.3	0.4	0.5	0.7	
20	21.5	40 00	7.5	20 00	2.6	9	0.4	0.3	0.1	0.0	0.1	0.3	0.4	0.5	0.6	
25	21.0	50 00	7.4	21 00	2.5	10 00	-0.4	-0.3	-0.1	0.0	+0.1	+0.2	+0.4	+0.4	+0.5	
1 30	-20.5	7 00	-7.2	22 00	-2.3	20	0.2	0.1	0.1	0.0	0.1	0.1	0.2	0.2	0.3	
35	20.1	10 00	7.0	23 00	2.2	30	0.1	0.1	0.0	0.0	0.0	0.1	0.1	0.1	0.2	
40	19.6	20 00	6.9	24 00	2.1	40	0.1	0.1	0.0	0.0	0.0	0.1	0.1	0.1	0.1	
45	19.1	30 00	6.8	25 00	2.0	50	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	
50	18.7	40 00	6.6	26 00	1.9	60	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
55	18.3	50 00	6.5	27 00	1.8											
2 00	-17.9	8 00	-6.4	28 00	-1.8											
05	17.5	10 00	6.3	29 00	1.7											
10	17.1	20 00	6.2	30 00	1.7											
15	16.8	30 00	6.1	31 00	1.6											
20	16.4	40 00	6.0	32 00	1.5											
25	16.1	50 00	5.9	33 00	1.5											
ADDITIONAL REFRACTION CORRECTIONS FOR ATMOSPHERIC PRESSURE																
To be applied to the Apparent Altitude																
App. Alt.						Atmospheric Pressure - millibars										
2 30	-15.8	9 00	-5.8	34 00	-1.4	0 00	960		980	1000		1020		1030		
							,	,		,	,	,	,	,		
35	15.5	10 00	5.7	35 00	1.4	0 00	+1.7		980	+0.8		0.0	-0.8	-1.7		
40	15.2	20 00	5.6	36 00	1.3	30	1.4			0.7		0.0	0.7	1.4		
45	14.8	30 00	5.5	37 00	1.2	1 00	1.2			0.6		0.0	0.6	1.2		
50	14.6	40 00	5.4	38 00	1.2	30	1.0			0.5		0.0	0.5	1.0		
55	14.4	50 00	5.3	39 00	1.2											
3 00	-14.1	10 00	-5.2	40 00	-1.1											
05	13.8	10 00	5.2	45 00	0.9	2 00	+0.9		45 00	+0.4		0.0	-0.4	-0.9		
10	13.6	20 00	5.1	50 00	0.8	4	0.6			0.3		0.0	0.3	0.6		
15	13.4	30 00	5.0	55 00	0.7	6	0.4			0.2		0.0	0.2	0.4		
20	13.1	40 00	4.9	60 00	0.5	8	0.3			0.2		0.0	0.2	0.3		
25	12.9	50 00	4.9	65 00	0.4	10	0.3			0.1		0.0	0.1	0.3		
3 30	-12.7	11 00	-4.8	70 00	-0.3	15 00	+0.2		70 00	+0.1		0.0	-0.1	-0.2		
35	12.4	10 00	4.7	75 00	0.3	20	0.1			0.1		0.0	0.1	0.1		
40	12.2	20 00	4.7	80 00	0.2	25	0.1			0.1		0.0	0.1	0.1		
45	12.1	30 00	4.6	85 00	0.1	30	0.1			0.0		0.0	0.0	0.1		
50	11.9	40 00	4.5	90 00	0.0	35	0.1			0.0		0.0	0.0	0.1		
55	11.7	50 00	4.5													
4 00	-11.5	12 00	-4.4			40 00	0.0			0.0		0.0	0.0	0.0	0.0	

CORRECTION OF MOON'S MER. PASS.

Corr. Plus to Mer. Pass. in West Long.

Long.	Difference between times of successive transits.										Long.
	39 m.	42 m.	45 m.	48 m.	51 m.	54 m.	57 m.	60 m.	63 m.	66 m.	
°	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	°
3	0.3	0.4	0.4	0.4	0.4	0.4	0.5	0.5	0.5	0.6	3
6	0.6	0.7	0.8	0.8	0.8	0.9	1.0	1.0	1.0	1.1	6
9	1.0	1.0	1.1	1.2	1.3	1.4	1.4	1.5	1.6	1.6	9
12	1.3	1.4	1.5	1.6	1.7	1.8	1.9	2.0	2.1	2.2	12
15	1.6	1.8	1.9	2.0	2.1	2.2	2.4	2.5	2.6	2.8	15
18	2.0	2.1	2.2	2.4	2.6	2.7	2.8	3.0	3.2	3.3	18
21	2.3	2.4	2.6	2.8	3.0	3.2	3.3	3.5	3.7	3.8	21
24	2.6	2.8	3.0	3.2	3.4	3.6	3.8	4.0	4.2	4.4	24
27	2.9	3.2	3.4	3.6	3.8	4.0	4.3	4.5	4.7	5.0	27
30	3.2	3.5	3.8	4.0	4.2	4.5	4.8	5.0	5.2	5.5	30
33	3.6	3.8	4.1	4.4	4.7	5.0	5.2	5.5	5.8	6.0	33
36	3.9	4.2	4.5	4.8	5.1	5.4	5.7	6.0	6.3	6.6	36
39	4.2	4.6	4.9	5.2	5.5	5.8	6.2	6.5	6.8	7.2	39
42	4.6	4.9	5.2	5.6	6.0	6.3	6.6	7.0	7.4	7.7	42
45	4.9	5.2	5.6	6.0	6.4	6.8	7.1	7.5	7.9	8.2	45
48	5.2	5.6	6.0	6.4	6.8	7.2	7.6	8.0	8.4	8.8	48
51	5.5	6.0	6.4	6.8	7.2	7.6	8.1	8.5	8.9	9.4	51
54	5.8	6.3	6.8	7.2	7.6	8.1	8.6	9.0	9.4	9.9	54
57	6.2	6.6	7.1	7.6	8.1	8.6	9.0	9.5	10.0	10.4	57
60	6.5	7.0	7.5	8.0	8.5	9.0	9.5	10.0	10.5	11.0	60
63	6.8	7.4	7.9	8.4	8.9	9.4	10.0	10.5	11.0	11.6	63
66	7.2	7.7	8.2	8.8	9.4	9.9	10.4	11.0	11.6	12.1	66
69	7.5	8.0	8.6	9.2	9.8	10.4	10.9	11.5	12.1	12.6	69
72	7.8	8.4	9.0	9.6	10.2	10.8	11.4	12.0	12.6	13.2	72
75	8.1	8.8	9.4	10.0	10.6	11.2	11.9	12.5	13.2	13.8	75
78	8.4	9.1	9.8	10.4	11.0	11.7	12.4	13.0	13.6	14.3	78
81	8.8	9.4	10.1	10.8	11.5	12.2	12.8	13.5	14.2	14.8	81
84	9.1	9.8	10.5	11.2	11.9	12.6	13.3	14.0	14.7	15.4	84
87	9.4	10.2	10.9	11.6	12.3	13.0	13.8	14.5	15.2	16.0	87
90	9.8	10.5	11.2	12.0	12.8	13.5	14.2	15.0	15.8	16.5	90
93	10.1	10.8	11.6	12.4	13.2	14.0	14.7	15.5	16.3	17.0	93
96	10.4	11.2	12.0	12.8	13.6	14.4	15.2	16.0	16.8	17.6	96
99	10.7	11.6	12.4	13.2	14.0	14.8	15.7	16.5	17.3	18.2	99
102	11.0	11.9	12.8	13.6	14.4	15.3	16.2	17.0	17.8	18.7	102
105	11.4	12.2	13.1	14.0	14.9	15.8	16.6	17.5	18.4	19.2	105
108	11.7	12.6	13.5	14.4	15.3	16.2	17.1	18.0	18.9	19.8	108
111	12.0	13.0	13.9	14.8	15.7	16.6	17.6	18.5	19.4	20.4	111
114	12.4	13.3	14.2	15.2	16.2	17.1	18.0	19.0	20.0	20.9	114
117	12.7	13.6	14.6	15.6	16.6	17.6	18.5	19.5	20.5	21.4	117
120	13.0	14.0	15.0	16.0	17.0	18.0	19.0	20.0	21.0	22.0	120
123	13.3	14.4	15.4	16.4	17.4	18.4	19.5	20.5	21.5	22.6	123
126	13.6	14.7	15.8	16.8	17.8	18.9	20.0	21.0	22.0	23.1	126
129	14.0	15.0	16.1	17.2	18.3	19.4	20.4	21.5	22.6	23.6	129
132	14.3	15.4	16.5	17.6	18.7	19.8	20.9	22.0	23.1	24.2	132
135	14.6	15.8	16.9	18.0	19.1	20.2	21.4	22.5	23.6	24.8	135
138	15.0	16.1	17.2	18.4	19.6	20.7	21.8	23.0	24.2	25.3	138
141	15.3	16.4	17.6	18.8	20.0	21.2	22.3	23.5	24.7	25.8	141
144	15.6	16.8	18.0	19.2	20.4	21.6	22.8	24.0	25.2	26.4	144
147	15.9	17.2	18.4	19.6	20.8	22.0	23.3	24.5	25.7	27.0	147
150	16.2	17.5	18.8	20.0	21.2	22.5	23.8	25.0	26.2	27.5	150
153	16.6	17.8	19.1	20.4	21.7	23.0	24.2	25.5	26.8	28.0	153
156	16.9	18.2	19.5	20.8	22.1	23.4	24.7	26.0	27.3	28.6	156
159	17.2	18.6	19.9	21.2	22.5	23.8	25.2	26.5	27.8	29.2	159
162	17.6	18.9	20.2	21.6	23.0	24.3	25.6	27.0	28.4	29.7	162
165	17.9	19.2	20.6	22.0	23.4	24.8	26.1	27.5	28.9	30.2	165
168	18.2	19.6	21.0	22.4	23.8	25.2	26.6	28.0	29.4	30.8	168
171	18.5	20.0	21.4	22.8	24.2	25.6	27.1	28.5	29.9	31.4	171
174	18.8	20.3	21.8	23.2	24.6	26.1	27.6	29.0	30.4	31.9	174
177	19.2	20.6	22.1	23.6	25.1	26.6	28.0	29.5	31.0	32.4	177
180	19.5	21.0	22.5	24.0	25.5	27.0	28.5	30.0	31.5	33.0	180

Corr. Minus to Mer. Pass. in East Long.

SUN'S TOTAL CORRECTION

To be applied to the Observed Altitude of the Sun's Lower (L) or Upper (U) Limb

Obs. Alt.	Height of Eye															
	10.5m (34ft)		11.2m (37ft)		12.0m (39ft)		12.8m (42ft)		13.6m (45ft)		14.5m (48ft)		15.4m (50ft)		16.3m (53ft)	
	L	U	L	U	L	U	L	U	L	U	L	U	L	U	L	U
06 00	+1.9	-30.1	+1.7	-30.3	+1.5	-30.5	+1.3	-30.7	+1.1	-30.9	+0.9	-31.1	+0.7	-31.3	+0.5	-31.5
10	2.1	29.9	1.9	30.1	1.7	30.3	1.5	30.5	1.3	30.7	1.1	30.9	0.9	31.1	0.7	31.3
20	2.3	29.7	2.1	29.9	1.9	30.1	1.7	30.3	1.5	30.5	1.3	30.7	1.1	30.9	0.9	31.1
30	2.5	29.5	2.3	29.7	2.1	29.9	1.9	30.1	1.7	30.3	1.5	30.5	1.3	30.7	1.1	30.9
40	2.7	29.3	2.5	29.5	2.3	29.7	2.1	29.9	1.9	30.1	1.7	30.3	1.5	30.5	1.3	30.7
50	2.9	29.1	2.7	29.3	2.5	29.5	2.3	29.7	2.1	29.9	1.9	30.1	1.7	30.3	1.5	30.5
07 00	+3.1	-28.9	+2.9	-29.1	+2.7	-29.3	+2.5	-29.5	+2.3	-29.7	+2.1	-29.9	+1.9	-30.1	+1.7	-30.3
15	3.3	28.7	3.1	28.9	2.9	29.1	2.7	29.3	2.5	29.5	2.3	29.7	2.1	29.9	1.9	30.1
30	3.5	28.5	3.3	28.7	3.1	28.9	2.9	29.1	2.7	29.3	2.5	29.5	2.3	29.7	2.1	29.9
45	3.7	28.3	3.5	28.5	3.3	28.7	3.1	28.9	2.9	29.1	2.7	29.3	2.5	29.5	2.3	29.7
08 00	3.9	28.1	3.7	28.3	3.5	28.5	3.3	28.7	3.1	28.9	2.9	29.1	2.7	29.3	2.5	29.5
15	4.1	27.9	3.9	28.1	3.7	28.3	3.5	28.5	3.3	28.7	3.1	28.9	2.9	29.1	2.7	29.3
30	4.3	27.7	4.1	27.9	3.9	28.1	3.7	28.3	3.5	28.5	3.3	28.7	3.1	28.9	2.9	29.1
45	4.5	27.5	4.3	27.7	4.1	27.9	3.9	28.1	3.7	28.3	3.5	28.5	3.3	28.7	3.1	28.9
09 00	+4.7	-27.3	+4.5	-27.5	+4.3	-27.7	+4.1	-27.9	+3.9	-28.1	+3.7	-28.3	+3.5	-28.5	+3.3	-28.7
20	4.9	27.1	4.7	27.3	4.5	27.5	4.3	27.7	4.1	27.9	3.9	28.1	3.7	28.3	3.5	28.5
40	5.1	26.9	4.9	27.1	4.7	27.3	4.5	27.5	4.3	27.7	4.1	27.9	3.9	28.1	3.7	28.3
10 00	5.3	26.7	5.1	26.9	4.9	27.1	4.7	27.3	4.5	27.5	4.3	27.7	4.1	27.9	3.9	28.1
30	5.5	26.5	5.3	26.7	5.1	26.9	4.9	27.1	4.7	27.3	4.5	27.5	4.3	27.7	4.1	27.9
11 00	5.7	26.3	5.5	26.5	5.3	26.7	5.1	26.9	4.9	27.1	4.7	27.3	4.5	27.5	4.3	27.7
30	5.9	26.1	5.7	26.3	5.5	26.5	5.3	26.7	5.1	26.9	4.9	27.1	4.7	27.3	4.5	27.5
12 00	6.1	25.9	5.9	26.1	5.7	26.3	5.5	26.5	5.3	26.7	5.1	26.9	4.9	27.1	4.7	27.3
30	6.3	25.7	6.1	25.9	5.9	26.1	5.7	26.3	5.5	26.5	5.3	26.7	5.1	26.9	4.9	27.1
13 00	+6.5	-25.5	+6.3	-25.7	+6.1	-25.9	+5.9	-26.1	+5.7	-26.3	+5.5	-26.5	+5.3	-26.7	+5.1	-26.9
14 00	6.7	25.3	6.5	25.5	6.3	25.7	6.1	25.9	5.9	26.1	5.7	26.3	5.5	26.5	5.3	26.7
15 00	6.9	25.1	6.7	25.3	6.5	25.5	6.3	25.7	6.1	25.9	5.9	26.1	5.7	26.3	5.5	26.5
16 00	7.1	24.9	6.9	25.1	6.7	25.3	6.5	25.5	6.3	25.7	6.1	25.9	5.9	26.1	5.7	26.3
17 00	7.3	24.7	7.1	24.9	6.9	25.1	6.7	25.3	6.5	25.5	6.3	25.7	6.1	25.9	5.9	26.1
18 00	7.5	24.5	7.3	24.7	7.1	24.9	6.9	25.1	6.7	25.3	6.5	25.5	6.3	25.7	6.1	25.9
19 00	7.7	24.3	7.5	24.5	7.3	24.7	7.1	24.9	6.9	25.1	6.7	25.3	6.5	25.5	6.3	25.7
20 00	+7.9	-24.1	+7.7	-24.3	+7.5	-24.5	+7.3	-24.7	+7.1	-24.9	+6.9	-25.1	+6.7	-25.3	+6.5	-25.5
22 00	8.1	23.9	7.9	24.1	7.7	24.3	7.5	24.5	7.3	24.7	7.1	24.9	6.9	25.1	6.7	25.3
24 00	8.3	23.7	8.1	23.9	7.9	24.1	7.7	24.3	7.5	24.5	7.3	24.7	7.1	24.9	6.9	25.1
26 00	8.5	23.5	8.3	23.7	8.1	23.9	7.9	24.1	7.7	24.3	7.5	24.5	7.3	24.7	7.1	24.9
29 00	8.7	23.3	8.5	23.5	8.3	23.7	8.1	23.9	7.9	24.1	7.7	24.3	7.5	24.5	7.3	24.7
32 00	8.9	23.1	8.7	23.3	8.5	23.5	8.3	23.7	8.1	23.9	7.9	24.1	7.7	24.3	7.5	24.5
36 00	9.1	22.9	8.9	23.1	8.7	23.3	8.5	23.5	8.3	23.7	8.1	23.9	7.9	24.1	7.7	24.3
40 00	+9.3	-22.7	+9.1	-22.9	+8.9	-23.1	+8.7	-23.3	+8.5	-23.5	+8.3	-23.7	+8.1	-23.9	+7.9	-24.1
45 00	9.5	22.5	9.3	22.7	9.1	22.9	8.9	23.1	8.7	23.3	8.5	23.5	8.3	23.7	8.1	23.9
52 00	9.7	22.3	9.5	22.5	9.3	22.7	9.1	22.9	8.9	23.1	8.7	23.3	8.5	23.5	8.3	23.7
60 00	9.9	22.1	9.7	22.3	9.5	22.5	9.3	22.7	9.1	22.9	8.9	23.1	8.7	23.3	8.5	23.5
75 00	10.1	21.9	9.9	22.1	9.7	22.3	9.5	22.5	9.3	22.7	9.1	22.9	8.9	23.1	8.7	23.3
90 00	10.3	21.7	10.1	21.9	9.9	22.1	9.7	22.3	9.5	22.5	9.3	22.7	9.1	22.9	8.9	23.1

ADDITIONAL MONTHLY CORRECTION

Jan	Feb	Mar	Apr	May	June	July	Aug	Sept	Oct	Nov	Dec
LL +0.2	+0.2	+0.1	0.0	-0.1	-0.2	-0.2	-0.2	-0.1	0.0	+0.2	+0.2
UL -0.2	-0.2	-0.1	0.0	+0.1	+0.2	+0.2	+0.2	+0.1	0.0	-0.2	-0.2

SUN'S TOTAL CORRECTION

To be applied to the Observed Altitude of the Sun's Lower (L) or Upper (U) Limb

Height of Eye

Obs. Alt	17.2m (56ft)		18.2m (60ft)		19.2m (63ft)		20.2m (66ft)		21.2m (70ft)		22.2m (73ft)		23.3m (77ft)		24.4m (80ft)	
	L	U	L	U	L	U	L	U	L	U	L	U	L	U	L	U
	,	,	,	,	,	,	,	,	,	,	,	,	,	,	,	,
06 00	+0.3	-31.7	+0.1	-31.9	-0.1	-32.1	-0.3	-32.3	-0.5	-32.5	-0.7	-32.7	-0.9	-32.9	-1.1	-33.1
10	0.5	31.5	0.3	31.7	+0.1	31.9	0.1	32.1	0.3	32.3	0.5	32.5	0.7	32.7	0.9	32.9
20	0.7	31.3	0.5	31.5	0.3	31.7	+0.1	31.9	0.1	32.1	0.3	32.3	0.5	32.5	0.7	32.7
30	0.9	31.1	0.7	31.3	0.5	31.5	0.3	31.7	+0.1	31.9	0.1	32.1	0.3	32.3	0.5	32.5
40	1.1	30.9	0.9	31.1	0.7	31.3	0.5	31.5	0.3	31.7	+0.1	31.9	0.1	32.1	0.3	32.3
50	1.3	30.7	1.1	20.9	0.9	31.1	0.7	31.3	0.5	31.5	0.3	31.7	+0.1	31.9	0.1	32.1
07 00	+1.5	-30.5	+1.3	-30.7	+1.1	-30.9	+0.9	-31.1	+0.7	-31.3	+0.5	-31.5	+0.3	-31.7	+0.1	-31.9
15	1.7	30.3	1.5	30.5	1.3	30.7	1.1	30.9	0.9	31.1	0.7	31.3	0.5	31.5	0.3	31.7
30	1.9	30.1	1.7	30.3	1.5	30.5	1.3	30.7	1.1	30.9	0.9	31.1	0.7	31.3	0.5	31.5
45	2.1	29.9	1.9	30.1	1.7	30.3	1.5	30.5	1.3	30.7	1.1	30.9	0.9	31.1	0.7	31.3
08 00	2.3	29.7	2.1	29.9	1.9	30.1	1.7	30.3	1.5	30.5	1.3	30.7	1.1	30.9	0.9	31.1
15	2.5	29.5	2.3	29.7	2.1	29.9	1.9	30.1	1.7	30.3	1.5	30.5	1.3	30.7	1.1	30.9
30	2.7	29.3	2.5	29.5	2.3	29.7	2.1	29.9	1.9	30.1	1.7	30.3	1.5	30.5	1.3	30.7
45	2.9	29.1	2.7	29.3	2.5	29.5	2.3	29.7	2.1	29.9	1.9	30.1	1.7	30.3	1.5	30.5
09 00	+3.1	-28.9	+2.9	-29.1	+2.7	-29.3	+2.5	-29.5	+2.3	-29.7	+2.1	-29.9	+1.9	-30.1	+1.7	-30.3
20	3.3	28.7	3.1	28.9	2.9	29.1	2.7	29.3	2.5	29.5	2.3	29.7	2.1	29.9	1.9	30.1
40	3.5	28.5	3.3	28.7	3.1	28.9	2.9	29.1	2.7	29.3	2.5	29.5	2.3	29.7	2.1	29.9
10 00	3.7	28.3	3.5	28.5	3.3	28.7	3.1	28.9	2.9	29.1	2.7	29.3	2.5	29.5	2.3	29.7
30	3.9	28.1	3.7	28.3	3.5	28.5	3.3	28.7	3.1	28.9	2.9	29.1	2.7	29.3	2.5	29.5
11 00	4.1	27.9	3.9	28.1	3.7	28.3	3.5	28.5	3.3	28.7	3.1	28.9	2.9	29.1	2.7	29.3
30	4.3	27.7	4.1	27.9	3.9	28.1	3.7	28.3	3.5	28.5	3.3	28.7	3.1	28.9	2.9	29.1
12 00	4.5	27.5	4.3	27.7	4.1	27.9	3.9	28.1	3.7	28.3	3.5	28.5	3.3	28.7	3.1	28.9
30	4.7	27.3	4.5	27.5	4.3	27.7	4.1	27.9	3.9	28.1	3.7	28.3	3.5	28.5	3.3	28.7
13 00	+4.9	-27.1	+4.7	-27.3	+4.5	-27.5	+4.3	-27.7	+4.1	-27.9	+3.9	-28.1	+3.7	-28.3	+3.5	-28.5
14 00	5.1	26.9	4.9	27.1	4.7	27.3	4.5	27.5	4.3	27.7	4.1	27.9	3.9	28.1	3.7	28.3
15 00	5.3	26.7	5.1	26.9	4.9	27.1	4.7	27.3	4.5	27.5	4.3	27.7	4.1	27.9	3.9	28.1
16 00	5.5	26.5	5.3	26.7	5.1	26.9	4.9	27.1	4.7	27.3	4.5	27.5	4.3	27.7	4.1	27.9
17 00	5.7	26.3	5.5	26.5	5.3	26.7	5.1	26.9	4.9	27.1	4.7	27.3	4.5	27.5	4.3	27.7
18 00	5.9	26.1	5.7	26.3	5.5	26.5	5.3	26.7	5.1	26.9	4.9	27.1	4.7	27.3	4.5	27.5
19 00	6.1	25.9	5.9	26.1	5.7	26.3	5.5	26.5	5.3	26.7	5.1	26.9	4.9	27.1	4.7	27.3
20 00	+6.3	-25.7	+6.1	-25.9	+5.9	-26.1	+5.7	-26.3	+5.5	-26.5	+5.3	-26.7	+5.1	-26.9	+4.9	-27.1
22 00	6.5	25.5	6.3	25.7	6.1	25.9	5.9	26.1	5.7	26.3	5.5	26.5	5.3	26.7	5.1	26.9
24 00	6.3	25.3	6.5	25.5	6.3	25.7	6.1	25.9	5.9	26.1	5.7	26.3	5.5	26.7		
26 00	6.9	25.1	6.7	25.3	6.5	25.5	6.3	25.7	6.1	25.9	5.9	26.1	5.7	26.3	5.5	26.5
29 00	7.1	24.9	6.9	25.1	6.7	25.3	6.5	25.5	6.3	25.7	6.1	25.9	5.9	26.1	5.7	26.3
32 00	7.3	24.7	7.1	24.9	6.9	25.1	6.7	25.3	6.5	25.5	6.3	25.7	6.1	25.9	5.9	26.1
36 00	7.5	24.5	7.3	24.7	7.1	24.9	6.9	25.1	6.7	25.3	6.5	25.5	6.3	25.7	6.1	25.9
40 00	+7.7	-24.3	+7.5	-24.7	+7.3	-24.7	+7.1	-24.9	+6.9	-25.1	+6.7	-25.3	6.5	-25.5	6.3	-25.7
45 00	7.9	24.1	7.7	24.3	7.5	24.5	7.3	24.7	7.1	24.9	6.9	25.1	6.7	25.3	6.5	25.5
52 00	8.1	23.9	7.9	24.1	7.7	24.3	7.5	24.5	7.3	24.7	7.1	24.9	6.9	25.1	6.7	25.3
60 00	8.3	23.7	8.1	23.9	7.9	24.1	7.7	24.3	7.5	24.5	7.3	24.7	7.1	24.9	6.9	25.1
75 00	8.5	23.5	8.3	23.7	8.1	23.9	7.9	24.1	7.7	24.3	7.5	24.5	7.3	24.7	7.1	24.9
90 00	8.7	23.3	8.5	23.5	8.3	23.7	8.1	23.9	7.9	24.1	7.7	24.3	7.5	24.5	7.3	24.7

ADDITIONAL MONTHLY CORRECTION

Jan	Feb	Mar	Apr	May	June	July	Aug	Sept	Oct	Nov	Dec
LL +0.2	+0.2	+0.1	0.0	-0.1	-0.2	-0.2	-0.2	-0.1	0.0	+0.2	+0.2
UL -0.2	-0.2	-0.1	0.0	+0.1	+0.2	+0.2	+0.2	+0.1	0.0	-0.2	-0.2

STAR'S TOTAL CORRECTION

*To be SUBTRACTED from the
Observed Altitude of the Star*

Height of Eye

Metres	9.1	9.8	10.5	11.2	12.0	12.8	13.6	14.5	15.4	16.3	17.2	18.2	19.2	20.2	21.2
Feet	30	32	34	37	39	42	45	48	51	53	56	60	63	66	70
Obs. Alt.	'	'	'	'	'	'	'	'	'	'	'	'	'	'	'
6° 00'	13.6	13.8	14.0	14.2	14.4	14.6	14.8	15.0	15.2	15.4	15.6	15.8	16.0	16.2	16.4
12	13.4	13.6	13.8	14.0	14.2	14.4	14.6	14.8	15.0	15.2	15.4	15.6	15.8	16.0	16.2
24	13.2	13.4	13.6	13.8	14.0	14.2	14.4	14.6	14.8	15.0	15.2	15.4	15.6	15.8	16.0
36	13.0	13.2	13.4	13.6	13.8	14.0	14.2	14.4	14.6	14.8	15.0	15.2	15.4	15.6	15.8
48	12.8	13.0	13.2	13.4	13.6	13.8	14.0	14.2	14.4	14.6	14.8	15.0	15.2	15.4	15.6
7 00	12.6	12.8	13.0	13.2	13.4	13.6	13.8	14.0	14.2	14.4	14.6	14.8	15.0	15.2	15.4
15	12.4	12.6	12.8	13.0	13.2	13.4	13.6	13.8	14.0	14.2	14.4	14.6	14.8	15.0	15.2
30	12.2	12.4	12.6	12.8	13.0	13.2	13.4	13.6	13.8	14.0	14.2	14.4	14.6	14.8	15.0
45	12.0	12.2	12.4	12.6	12.8	13.0	13.2	13.4	13.6	13.8	14.0	14.2	14.4	14.6	14.8
8 00	11.8	12.0	12.2	12.4	12.6	12.8	13.0	13.2	13.4	13.6	13.8	14.0	14.2	14.4	14.6
20	11.6	11.8	12.0	12.2	12.4	12.6	12.8	13.0	13.2	13.4	13.6	13.8	14.0	14.2	14.4
40	11.4	11.6	11.8	12.0	12.2	12.4	12.6	12.8	13.0	13.2	13.4	13.6	13.8	14.0	14.2
9 00	11.2	11.4	11.6	11.8	12.0	12.2	12.4	12.6	12.8	13.0	13.2	13.4	13.6	13.8	14.0
20	11.0	11.2	11.4	11.6	11.8	12.0	12.2	12.4	12.6	12.8	13.0	13.2	13.4	13.6	13.8
40	10.8	11.0	11.2	11.4	11.6	11.8	12.0	12.2	12.4	12.6	12.8	13.0	13.2	13.4	13.6
10 00	10.6	10.8	11.0	11.2	11.4	11.6	11.8	12.0	12.2	12.4	12.6	12.8	13.0	13.2	13.4
30	10.4	10.6	10.8	11.0	11.2	11.4	11.6	11.8	12.0	12.2	12.4	12.6	12.8	13.0	13.2
11 00	10.2	10.4	10.6	10.8	11.0	11.2	11.4	11.6	11.8	12.0	12.2	12.4	12.6	12.8	13.0
30	10.0	10.2	10.4	10.6	10.8	11.0	11.2	11.4	11.6	11.8	12.0	12.2	12.4	12.6	12.8
12 00	9.8	10.0	10.2	10.4	10.6	10.8	11.0	11.2	11.4	11.6	11.8	12.0	12.2	12.4	12.6
30	9.6	9.8	10.0	10.2	10.4	10.6	10.8	11.0	11.2	11.4	11.6	11.8	12.0	12.2	12.4
13 00	9.4	9.6	9.8	10.0	10.2	10.4	10.6	10.8	11.0	11.2	11.4	11.6	11.8	12.0	12.2
30	9.2	9.4	9.6	9.8	10.0	10.2	10.4	10.6	10.8	11.0	11.2	11.4	11.6	11.8	12.0
14 00	9.0	9.2	9.4	9.6	9.8	10.0	10.2	10.4	10.6	10.8	11.0	11.2	11.4	11.6	11.8
15 00	8.8	9.0	9.2	9.4	9.6	9.8	10.0	10.2	10.4	10.6	10.8	11.0	11.2	11.4	11.6
16 00	8.6	8.8	9.0	9.2	9.4	9.6	9.8	10.0	10.2	10.4	10.6	10.8	11.0	11.2	11.4
17 00	8.4	8.6	8.8	9.0	9.2	9.4	9.6	9.8	10.0	10.2	10.4	10.6	10.8	11.0	11.2
18 00	8.2	8.4	8.6	8.8	9.0	9.2	9.4	9.6	9.8	10.0	10.2	10.4	10.6	10.8	11.0
19 00	8.0	8.2	8.4	8.6	8.8	9.0	9.2	9.4	9.6	9.8	10.0	10.2	10.4	10.6	10.8
21 00	7.8	8.0	8.2	8.4	8.6	8.8	9.0	9.2	9.4	9.6	9.8	10.0	10.2	10.4	10.6
23 00	7.6	7.8	8.0	8.2	8.4	8.6	8.8	9.0	9.2	9.4	9.6	9.8	10.0	10.2	10.4
25 00	7.4	7.6	7.8	8.0	8.2	8.4	8.6	8.8	9.0	9.2	9.4	9.6	9.8	10.0	10.2
27 00	7.2	7.4	7.6	7.8	8.0	8.2	8.4	8.6	8.8	9.0	9.2	9.4	9.6	9.8	10.0
29 00	7.0	7.2	7.4	7.6	7.8	8.0	8.2	8.4	8.6	8.8	9.0	9.2	9.4	9.6	9.8
33 00	6.8	7.0	7.2	7.4	7.6	7.8	8.0	8.2	8.4	8.6	8.8	9.0	9.2	9.4	9.6
36 00	6.6	6.8	7.0	7.2	7.4	7.6	7.8	8.0	8.2	8.4	8.6	8.8	9.0	9.2	9.4
41 00	6.4	6.6	6.8	7.0	7.2	7.4	7.6	7.8	8.0	8.2	8.4	8.6	8.8	9.0	9.2
48 00	6.2	6.4	6.6	6.8	7.0	7.2	7.4	7.6	7.8	8.0	8.2	8.4	8.6	8.8	9.0
55 00	6.0	6.2	6.4	6.6	6.8	7.0	7.2	7.4	7.6	7.8	8.0	8.2	8.4	8.6	8.8
65 00	5.8	6.0	6.2	6.4	6.6	6.8	7.0	7.2	7.4	7.6	7.8	8.0	8.2	8.4	8.6
75 00	5.6	5.8	6.0	6.2	6.4	6.6	6.8	7.0	7.2	7.4	7.6	7.8	8.0	8.2	8.4
85 00	5.4	5.6	5.8	6.0	6.2	6.4	6.6	6.8	7.0	7.2	7.4	7.6	7.8	8.0	8.2
90 00	5.3	5.5	5.7	5.9	6.1	6.3	6.5	6.7	6.9	7.1	7.3	7.5	7.7	7.9	8.1

A shortened table of the Star's Total Correction is given inside the back cover

MOON'S TOTAL CORRECTION – LOWER LIMB

Add to the Observed Altitude of the Moon's Lower limb

Observed Altitude

H.P. ,	38°00'	30'	39°00'	30'	40°00'	30'	41°00'	30'	42°00'	30'	43°00'	30'	44°00'	30'	45°00'
54.0	43.7	43.5	43.2	42.9	42.6	42.3	42.1	41.8	41.5	41.2	40.9	40.6	40.3	39.9	39.6
54.2	43.9	43.7	43.4	43.1	42.8	42.6	42.3	42.0	41.7	41.4	41.1	40.8	40.5	40.1	39.8
54.4	44.2	43.9	43.6	43.3	43.0	42.8	42.5	42.2	41.9	41.6	41.3	41.0	40.6	40.3	40.0
54.6	44.4	44.1	43.8	43.5	43.2	43.0	42.7	42.4	42.1	41.8	41.5	41.2	40.8	40.5	40.2
54.8	44.6	44.3	44.0	43.7	43.5	43.2	42.9	42.6	42.3	42.0	41.7	41.4	41.0	40.7	40.4
55.0	44.8	44.5	44.2	43.9	43.7	43.4	43.1	42.8	42.5	42.2	41.9	41.6	41.2	40.9	40.6
55.2	45.0	44.7	44.4	44.2	43.9	43.6	43.3	43.0	42.7	42.4	42.1	41.8	41.4	41.1	40.8
55.4	45.2	44.9	44.6	44.4	44.1	43.8	43.5	43.2	42.9	42.6	42.3	41.9	41.6	41.3	41.0
55.6	45.4	45.1	44.9	44.6	44.3	44.0	43.7	43.4	43.1	42.8	42.5	42.1	41.8	41.5	41.2
55.8	45.6	45.3	45.1	44.8	44.5	44.2	43.9	43.6	43.3	43.0	42.7	42.3	42.0	41.7	41.4
56.0	45.8	45.6	45.3	45.0	44.7	44.4	44.1	43.8	43.5	43.2	42.9	42.5	42.2	41.9	41.6
56.2	46.0	45.8	45.5	45.2	44.9	44.6	44.3	44.0	43.7	43.4	43.1	42.7	42.4	42.1	41.8
56.4	46.3	46.0	45.7	45.4	45.1	44.8	44.5	44.2	43.9	43.6	43.3	42.9	42.6	42.3	42.0
56.6	46.5	46.2	45.9	45.6	45.3	45.0	44.7	44.4	44.1	43.8	43.5	43.1	42.8	42.5	42.2
56.8	46.7	46.4	46.1	45.8	45.5	45.2	44.9	44.6	44.3	44.0	43.7	43.3	43.0	42.7	42.3
57.0	46.9	46.6	46.3	46.0	45.7	45.4	45.1	44.8	44.5	44.2	43.9	43.5	43.2	42.9	42.5
57.2	47.1	46.8	46.5	46.2	45.9	45.6	45.3	45.0	44.7	44.4	44.1	43.7	43.4	43.1	42.7
57.4	47.3	47.0	46.7	46.4	46.1	45.8	45.5	45.2	44.9	44.6	44.3	43.9	43.6	43.3	42.9
57.6	47.5	47.2	46.9	46.6	46.3	46.0	45.7	45.4	45.1	44.8	44.5	44.1	43.8	43.5	43.1
57.8	47.7	47.4	47.1	46.8	46.5	46.2	45.9	45.6	45.3	45.0	44.6	44.3	44.0	43.7	43.3
58.0	47.9	47.6	47.4	47.1	46.7	46.4	46.1	45.8	45.5	45.2	44.8	44.5	44.2	43.9	43.5
58.2	48.1	47.9	47.6	47.3	47.0	46.6	46.3	46.0	45.7	45.4	45.0	44.7	44.4	44.0	43.7
58.4	48.4	48.1	47.8	47.5	47.2	46.8	46.5	46.2	45.9	45.6	45.2	44.9	44.6	44.2	43.9
58.6	48.6	48.3	48.0	47.7	47.4	47.1	46.7	46.4	46.1	45.8	45.4	45.1	44.8	44.4	44.1
58.8	48.8	48.5	48.2	47.9	47.6	47.3	46.9	46.6	46.3	46.0	45.6	45.3	45.0	44.6	44.3
59.0	49.0	48.7	48.4	48.1	47.8	47.5	47.1	46.8	46.5	46.2	45.8	45.5	45.2	44.8	44.5
59.2	49.2	48.9	48.6	48.3	48.0	47.7	47.4	47.0	46.7	46.4	46.0	45.7	45.4	45.0	44.7
59.4	49.4	49.1	48.8	48.5	48.2	47.9	47.6	47.2	46.9	46.6	46.2	45.9	45.6	45.2	44.9
59.6	49.6	49.3	49.0	48.7	48.4	48.1	47.8	47.4	47.1	46.8	46.4	46.1	45.8	45.4	45.1
59.8	49.8	49.5	49.2	48.9	48.6	48.3	48.0	47.6	47.3	47.0	46.6	46.3	46.0	45.6	45.3
60.0	50.0	49.7	49.4	49.1	48.8	48.5	48.2	47.8	47.5	47.2	46.8	46.5	46.2	45.8	45.5
60.2	50.3	49.9	49.6	49.3	49.0	48.7	48.4	48.0	47.7	47.4	47.0	46.7	46.3	46.0	45.6
60.4	50.5	50.2	49.8	49.5	49.2	48.9	48.6	48.2	47.9	47.6	47.2	46.9	46.5	46.2	45.8
60.6	50.7	50.4	50.1	49.7	49.4	49.1	48.8	48.4	48.1	47.8	47.4	47.1	46.7	46.4	46.0
60.8	50.9	50.6	50.3	49.9	49.6	49.3	49.0	48.6	48.3	48.0	47.6	47.3	46.9	46.6	46.2
61.0	51.1	50.8	50.5	50.2	49.8	49.5	49.2	48.9	48.5	48.2	47.8	47.5	47.1	46.8	46.4
61.2	51.3	51.0	50.7	50.4	50.0	49.7	49.4	49.1	48.7	48.4	48.0	47.7	47.3	47.0	46.6
61.4	51.5	51.2	50.9	50.6	50.2	49.9	49.6	49.3	48.9	48.6	48.2	47.9	47.5	47.2	46.8
61.5	51.6	51.3	51.0	50.7	50.4	50.0	49.7	49.4	49.0	48.7	48.4	48.0	47.7	47.3	46.9

Height of Eye Correction Always ADDED to the Observed Altitude

Metres	2	2.3	2.7	3.1	3.5	3.9	4.4	4.9	5.4	5.9	6.5
Feet	7	8	9	10	11	13	14	16	18	19	21
Corrn'	9.8	9.6	9.4	9.2	9.0	8.8	8.6	8.4	8.2	8.0	7.8

**RADAR PLOTTER'S
SPEED AND DISTANCE TABLE**

SPEED IN KNOTS	Miles in 1 min.	Miles in 2 min.	Miles in 2½ min.	Miles in 3 min.	Miles in 4 min.	Miles in 5 min.	Miles in 6 min.	SPEED IN KNOTS
4·0	0·07	0·13	0·17	0·20	0·27	0·33	0·40	4·0
4·5	0·08	0·15	0·19	0·23	0·30	0·38	0·45	4·5
5·0	0·08	0·17	0·21	0·25	0·33	0·42	0·50	5·0
5·5	0·10	0·18	0·23	0·28	0·37	0·46	0·55	5·5
6·0	0·10	0·20	0·25	0·30	0·40	0·50	0·60	6·0
6·5	0·11	0·22	0·27	0·33	0·43	0·54	0·65	6·5
7·0	0·12	0·23	0·29	0·35	0·47	0·58	0·70	7·0
7·5	0·13	0·25	0·31	0·38	0·50	0·63	0·75	7·5
8·0	0·13	0·27	0·33	0·40	0·53	0·67	0·80	8·0
8·5	0·14	0·28	0·35	0·43	0·57	0·71	0·85	8·5
9·0	0·15	0·30	0·38	0·45	0·60	0·75	0·90	9·0
9·5	0·16	0·32	0·40	0·48	0·63	0·80	0·95	9·5
10·0	0·17	0·33	0·42	0·50	0·67	0·83	1·00	10·0
10·5	0·18	0·35	0·44	0·53	0·70	0·88	1·05	10·5
11·0	0·18	0·37	0·46	0·55	0·73	0·91	1·10	11·0
11·5	0·19	0·38	0·48	0·58	0·77	0·96	1·15	11·5
12·0	0·20	0·40	0·50	0·60	0·80	1·00	1·20	12·0
12·5	0·21	0·42	0·52	0·63	0·83	1·04	1·25	12·5
13·0	0·22	0·43	0·54	0·65	0·87	1·08	1·30	13·0
13·5	0·23	0·45	0·56	0·68	0·90	1·13	1·35	13·5
14·0	0·23	0·47	0·58	0·70	0·93	1·17	1·40	14·0
14·5	0·24	0·48	0·60	0·73	0·97	1·21	1·45	14·5
15·0	0·25	0·50	0·63	0·75	1·00	1·25	1·50	15·0
15·5	0·26	0·52	0·65	0·78	1·03	1·29	1·55	15·5
16·0	0·27	0·53	0·67	0·80	1·07	1·33	1·60	16·0
16·5	0·28	0·55	0·69	0·83	1·10	1·38	1·65	16·5
17·0	0·28	0·57	0·71	0·85	1·13	1·42	1·70	17·0
17·5	0·29	0·58	0·73	0·88	1·17	1·46	1·75	17·5
18·0	0·30	0·60	0·75	0·90	1·20	1·50	1·80	18·0
18·5	0·31	0·62	0·77	0·93	1·23	1·54	1·85	18·5
19·0	0·32	0·63	0·79	0·95	1·27	1·58	1·90	19·0
19·5	0·33	0·65	0·81	0·98	1·30	1·63	1·95	19·5
20·0	0·33	0·67	0·83	1·00	1·33	1·67	2·00	20·0
20·5	0·34	0·68	0·85	1·03	1·37	1·71	2·05	20·5
21·0	0·35	0·70	0·88	1·05	1·40	1·75	2·10	21·0
21·5	0·36	0·72	0·90	1·08	1·43	1·79	2·15	21·5
22·0	0·37	0·73	0·92	1·10	1·47	1·83	2·20	22·0
22·5	0·38	0·75	0·94	1·13	1·50	1·88	2·25	22·5
23·0	0·38	0·77	0·96	1·15	1·53	1·92	2·30	23·0
23·5	0·39	0·78	0·98	1·18	1·57	1·96	2·35	23·5
24·0	0·40	0·80	1·00	1·20	1·60	2·00	2·40	24·0
24·5	0·41	0·82	1·02	1·23	1·63	2·04	2·45	24·5
25·0	0·42	0·83	1·04	1·25	1·67	2·08	2·50	25·0
25·5	0·43	0·85	1·06	1·28	1·70	2·13	2·55	25·5
26·0	0·43	0·87	1·08	1·30	1·73	2·17	2·60	26·0
26·5	0·44	0·88	1·10	1·33	1·77	2·21	2·65	26·5
27·0	0·45	0·90	1·13	1·35	1·80	2·25	2·70	27·0
27·5	0·46	0·92	1·15	1·38	1·83	2·29	2·75	27·5
28·0	0·47	0·93	1·17	1·40	1·87	2·33	2·80	28·0
28·5	0·48	0·95	1·19	1·43	1·90	2·38	2·85	28·5
29·0	0·48	0·97	1·21	1·45	1·93	2·42	2·90	29·0
29·5	0·49	0·98	1·23	1·48	1·97	2·46	2·95	29·5
30·0	0·50	1·00	1·25	1·50	2·00	2·50	3·00	30·0
30·5	0·51	1·02	1·27	1·53	2·03	2·54	3·05	30·5
31·0	0·52	1·03	1·29	1·55	2·07	2·58	3·10	31·0
31·5	0·53	1·05	1·31	1·58	2·10	2·63	3·15	31·5
32·0	0·53	1·07	1·33	1·60	2·13	2·67	3·20	32·0
32·5	0·54	1·08	1·35	1·63	2·17	2·71	3·25	32·5
33·0	0·55	1·10	1·38	1·65	2·20	2·75	3·30	33·0
33·5	0·56	1·12	1·40	1·68	2·23	2·79	3·35	33·5
34·0	0·57	1·13	1·42	1·70	2·27	2·83	3·40	34·0

RADAR RANGE TABLE

The accompanying table gives the approximate distance of the 'radar horizon' corresponding to different heights of the radar aerial or target from which an echo is returned, and is based on the formula:-

$$\text{horizon dist. in n.mls} = 2.21\sqrt{h}$$

where h = height of aerial or target in metres

In similar manner to light waves, radio waves are refracted in passing through the atmosphere. This has the effect of making the distance of the radar horizon for 3cm. waves, under certain standard conditions of the atmosphere, about 15 per cent. greater than the distance of the geometrical horizon. Hence, taking the latter in nautical miles to be $1.92\sqrt{h}$, the distance of the radar horizon becomes $2.21\sqrt{h}$. This will be correct only under the standard conditions, and every departure from such standard will cause the distances to vary somewhat. The standard referred to is as follows:-

Atmospheric pressure 1013mb. decreasing with height at the rate of approximately 100mb. per 1000m.

Air temperature at sea level 30°C . decreasing with height at the rate of 6.5°C per 1000m.

60 per cent. *relative humidity* remaining constant with height.

Apart from variations from the above standard, the range at which target echoes can be seen on the P.P.I. screen will depend to a considerable extent on the characteristics of the particular radar installation and on the echoing qualities of the target.

Used with discretion, however, the information given in the table can be of much value to the radar observer.

Note: — The sum of the radar horizon distances of aerial and target respectively gives the maximum distance from which that target can return an echo.

Examples:-

1. A target of height 120m (390ft) should begin to appear on the P.P.I. of an installation with an aerial mounted 10m (33ft) above sea level at a range of approximately $24 + 7 = 31$ miles

2. If an echo first appears on the P.P.I. (aerial 10m (33ft) above sea level) at a range of 26 miles, the probable height of the target is of the order of about 70m (230ft). This may assist in identifying it.

CAUTION: — TO BE USED WITH 3cm. WAVE RADAR ONLY.

m	ft.	Range Mls	m.	ft.	Range Mls
2	7	3.1	110	360	23
4	13	4.4	120	390	24
6	20	5.4	130	430	25
8	26	6.3	140	460	26
10	33	7.0	150	490	27
15	49	8.6	160	530	28
20	66	9.9	170	560	29
25	82	11.1	180	590	30
30	98	12.1	190	620	31
35	115	13.1	200	660	31
40	131	14.0	220	720	33
45	148	14.8	240	790	34
50	164	15.6	260	850	36
55	180	16.0	280	920	37
60	197	17.1	300	980	38
70	230	18.5	320	1050	40
80	262	19.8	340	1120	41
90	295	21.0	360	1180	42
100	328	22.1	380	1250	43
110	360	23.0	400	1310	44

DISTANCE BY VERTICAL ANGLE

Height of Object

Distance mls	m	46	47.5	49	50.5	52	53.5	55	56.5	58	59.5	61	62.5	64	65.5	
	ft	151	156	161	166	171	176	180	185	190	195	200	205	210	215	
0.1	13	57	14	23	14	49	15	15	15	41	16	07	16	32	16	58
.2	7	05	7	18	7	32	7	45	7	59	8	13	8	27	8	40
.3	4	44	4	53	5	02	5	12	5	21	5	30	5	39	5	48
.4	3	33	3	40	3	47	3	54	4	01	4	08	4	15	4	22
0.5	2	51	2	56	3	02	3	07	3	13	3	18	3	24	3	29
.6	2	22	2	27	2	31	2	36	2	41	2	45	2	50	2	55
.7	2	02	2	06	2	10	2	14	2	18	2	22	2	26	2	30
.8	1	47	1	51	1	54	1	57	2	01	2	04	2	08	2	11
.9	1	35	1	38	1	41	1	44	1	47	1	50	1	53	1	56
1.0	1	25	1	28	1	31	1	34	1	36	1	39	1	42	1	45
.1	1	18	1	20	1	23	1	25	1	28	1	30	1	33	1	35
.2	1	11	1	13	1	16	1	18	1	20	1	23	1	25	1	27
.3	1	06	1	08	1	10	1	12	1	14	1	16	1	18	1	20
.4	1	01	1	03	1	05	1	07	1	09	1	11	1	13	1	15
1.5	0	57	0	59	1	01	1	02	1	04	1	06	1	08	1	10
.6	0	53	0	55	0	57	0	59	1	00	1	02	1	04	1	06
.7	0	50	0	52	0	53	0	55	0	57	0	58	1	00	1	02
.8	0	47	0	49	0	50	0	52	0	54	0	55	0	56	0	58
.9	0	45	0	46	0	48	0	49	0	51	0	52	0	54	0	55
2.0	0	43	0	44	0	45	0	47	0	48	0	50	0	51	0	52
.1	0	41	0	42	0	43	0	45	0	46	0	47	0	49	0	50
.2	0	39	0	40	0	41	0	43	0	44	0	45	0	46	0	47
.3	0	37	0	38	0	39	0	41	0	42	0	43	0	44	0	45
.4	0	36	0	37	0	38	0	39	0	40	0	41	0	43	0	44
2.5	0	34	0	35	0	36	0	37	0	39	0	40	0	41	0	42
.6	0	33	0	34	0	35	0	36	0	37	0	38	0	39	0	40
.7	0	32	0	33	0	34	0	35	0	36	0	37	0	38	0	39
.8	0	30	0	31	0	32	0	33	0	34	0	35	0	36	0	37
.9	0	29	0	30	0	31	0	32	0	33	0	34	0	35	0	36
3.0	0	28	0	29	0	30	0	31	0	32	0	33	0	34	0	35
.2	0	27	0	28	0	29	0	30	0	31	0	32	0	33	0	34
.4	0	25	0	26	0	27	0	28	0	28	0	29	0	30	0	31
.6	0	24	0	24	0	25	0	26	0	27	0	28	0	29	0	30
.8	0	22	0	23	0	24	0	25	0	25	0	26	0	27	0	28
4.0	0	21	0	22	0	23	0	23	0	24	0	25	0	26	0	27
.2	0	20	0	21	0	22	0	23	0	24	0	24	0	25	0	26
.4	0	19	0	20	0	21	0	22	0	23	0	24	0	25	0	26
.6	0	19	0	19	0	20	0	21	0	22	0	23	0	24	0	25
.8	0	18	0	18	0	19	0	20	0	20	0	21	0	22	0	23
5.0	0	17	0	18	0	18	0	19	0	19	0	20	0	21	0	22
.2	0	16	0	17	0	17	0	18	0	19	0	20	0	21	0	22
.4	0	16	0	16	0	17	0	17	0	18	0	18	0	19	0	20
.6	0	15	0	16	0	16	0	17	0	17	0	18	0	18	0	19
.8	0	15	0	15	0	16	0	16	0	17	0	17	0	18	0	19
6.0	0	14	0	15	0	15	0	16	0	16	0	17	0	17	0	18

$$\text{Tan. } \theta = \frac{h}{d} \quad \text{Where } \theta = \text{vertical angle, } h = \text{height of object, and } d = \text{distance.}$$

EXTREME RANGE TABLE

Elevation		Height of Eye											
m		1.5	3	4.5	6	8	10	12	14	16	18	20	22
m	ft	5	10	15	20	26	33	39	46	52	59	66	72
0	0	2.6	3.6	4.4	5.1	5.9	6.6	7.3	7.8	8.4	8.9	9.4	9.8
2	7	5.5	6.6	7.4	8.1	8.9	9.6	10.2	10.8	11.3	11.9	12.3	12.8
4	13	6.8	7.8	8.6	9.3	10.1	10.8	11.4	12.0	12.6	13.1	13.6	14.0
6	20	7.7	8.8	9.6	10.3	11.1	11.8	12.4	13.0	13.5	14.0	14.5	15.0
8	26	8.5	9.6	10.4	11.1	11.9	12.6	13.2	13.8	14.3	14.8	15.3	15.8
10	33	9.2	10.3	11.1	11.8	12.6	13.3	13.9	14.5	15.0	15.5	16.0	16.5
12	39	9.8	10.9	11.7	12.4	13.2	13.9	14.5	15.1	15.6	16.1	16.6	17.1
14	46	10.4	11.5	12.3	13.0	13.8	14.5	15.1	15.7	16.2	16.7	17.2	17.7
16	52	10.9	12.0	12.8	13.5	14.3	15.0	15.6	16.2	16.8	17.3	17.7	18.2
18	59	11.4	12.5	13.3	14.0	14.8	15.5	16.1	16.7	17.3	17.8	18.3	18.7
20	66	11.9	13.0	13.8	14.5	15.3	16.0	16.6	17.2	17.7	18.3	18.7	19.2
22	72	12.4	13.5	14.3	15.0	15.8	16.5	17.1	17.7	18.2	18.7	19.2	19.7
24	79	12.8	13.9	14.7	15.4	16.2	16.9	17.5	18.1	18.6	19.2	19.6	20.1
26	85	13.2	14.3	15.1	15.8	16.6	17.3	17.9	18.5	19.1	19.6	20.1	20.5
28	92	13.7	14.7	15.5	16.2	17.0	17.7	18.3	18.9	19.5	20.0	20.5	20.9
30	98	14.0	15.1	15.9	16.6	17.4	18.1	18.7	19.3	19.9	20.4	20.8	21.3
35	115	15.0	16.0	16.8	17.5	18.3	19.0	19.7	20.2	20.8	21.3	21.8	22.2
40	131	15.8	16.9	17.7	18.4	19.2	19.9	20.5	21.1	21.6	22.1	22.6	23.1
45	148	16.6	17.7	18.5	19.2	20.0	20.7	21.3	21.9	22.4	22.9	23.4	23.9
50	164	17.4	18.4	19.2	19.9	20.7	21.4	22.1	22.7	23.2	23.7	24.2	24.6
55	180	18.1	19.2	20.0	20.7	21.5	22.2	22.8	23.4	23.9	24.4	24.9	25.4
60	197	18.8	19.9	20.7	21.4	22.2	22.9	23.5	24.1	24.6	25.1	25.6	26.1
65	213	19.5	20.5	21.3	22.0	22.8	23.5	24.1	24.7	25.3	25.8	26.3	26.7
70	230	20.1	21.1	21.9	22.7	23.5	24.2	24.8	25.4	25.9	26.4	26.9	27.4
75	246	20.7	21.7	22.5	23.3	24.1	24.8	25.4	26.0	26.5	27.0	27.5	28.0
80	262	21.3	22.4	23.2	23.9	24.7	25.4	26.0	26.6	27.1	27.6	28.1	28.6
85	279	21.9	22.9	23.7	24.4	25.2	25.9	26.6	27.2	27.7	28.2	28.7	29.1
90	295	22.4	23.5	24.3	25.0	25.8	26.5	27.1	27.7	28.3	28.8	29.2	29.7
95	312	23.0	24.0	24.8	25.6	26.3	27.0	27.7	28.3	28.8	29.3	29.8	30.2
100	328	23.5	24.6	25.4	26.1	26.9	27.6	28.2	28.8	29.3	29.8	30.3	30.8
110	361	24.5	25.6	26.4	27.1	27.9	28.6	29.2	29.8	30.4	30.9	31.3	31.8
120	394	25.5	26.6	27.4	28.1	28.9	29.6	30.2	30.8	31.3	31.8	32.3	32.8
130	427	26.5	27.5	28.3	29.0	29.8	30.5	31.1	31.7	32.3	32.8	33.3	33.7
140	459	27.4	28.4	29.2	29.9	30.7	31.4	32.0	32.6	33.2	33.7	34.2	34.6
150	492	28.2	29.3	30.1	30.8	31.6	32.3	32.9	33.5	34.0	34.5	35.0	35.5
160	525	29.1	30.1	30.9	31.6	32.4	33.1	33.8	34.3	34.9	35.4	35.9	36.3
170	558	29.9	30.9	31.7	32.4	33.2	33.9	34.6	35.2	35.7	36.2	36.7	37.1
180	591	30.7	31.7	32.5	33.2	34.0	34.7	35.4	35.9	36.5	37.0	37.5	37.9
190	623	31.4	32.5	33.3	34.0	34.8	35.5	36.1	36.7	37.3	37.8	38.2	38.7
200	656	32.2	33.3	34.1	34.8	35.6	36.3	36.9	37.5	38.0	38.5	39.0	39.5
210	689	32.9	34.0	34.8	35.5	36.3	37.0	37.6	38.2	38.7	39.2	39.7	40.2
220	722	33.6	34.7	35.5	36.2	37.0	37.7	38.3	38.9	39.5	40.0	40.4	40.9
230	755	34.3	35.4	36.2	36.9	37.7	38.4	39.0	39.6	40.1	40.7	41.1	41.6
240	787	35.0	36.1	36.9	37.6	38.4	39.1	39.7	40.3	40.8	41.3	41.8	42.3
250	820	35.7	36.8	37.6	38.3	39.1	39.8	40.4	41.0	41.5	42.0	42.5	43.0
260	853	36.3	37.4	38.2	38.9	39.7	40.4	41.0	41.6	42.2	42.7	43.2	43.6
270	886	37.0	38.1	38.9	39.6	40.4	41.0	41.7	42.3	42.8	43.3	43.8	44.3
280	919	37.6	38.7	39.5	40.2	41.0	41.7	42.3	42.9	43.4	43.9	44.4	44.9
290	951	38.2	39.3	40.1	40.8	41.6	42.3	42.9	43.5	44.1	44.6	45.0	45.5
300	984	38.9	39.9	40.7	41.4	42.2	42.9	43.5	44.1	44.7	45.2	45.7	46.1

DIP OF THE SHORE HORIZON or Dip at Different Ranges

Miles	Height of Eye													
	m ft	1.5 5	3 10	4.5 15	6 20	7.5 25	9 30	10.5 36	12 39	13.5 44	15 49	17.5 57	20 66	
0.1	° / °	° / °	° / °	° / °	° / °	° / °	° / °	° / °	° / °	° / °	° / °	° / °	° / °	° / °
.2	-27.9	-55.7	-1 23.5	-1 51.3	-2 19.1	-2 46.9	-3 14.7	-3 42.5	-4 10.3	-4 38.1	-5 24.5	-6 10.8		
.3	14.0	27.9	41.8	55.7	1 09.6	1 23.5	1 37.4	1 51.3	2 05.2	2 19.1	2 42.3	3 05.5		
.4	9.4	18.7	27.9	37.2	46.5	55.8	1 05.0	1 14.3	1 23.6	1 32.8	1 48.3	2 03.7		
.5	7.1	14.1	21.0	28.0	34.9	41.9	48.8	55.8	1 02.7	1 09.7	1 21.3	1 32.9		
.6	5.8	11.3	16.9	22.4	28.0	33.6	39.1	44.7	50.3	55.8	1 05.1	1 14.4		
.7	-4.9	-9.5	-14.2	-18.8	-23.4	-28.1	-32.7	-37.3	-42.0	-46.6	-54.3	-1 02.1		
.8	4.3	8.2	12.2	16.2	20.2	24.1	28.1	32.1	36.1	40.0	46.7	53.3		
.9	3.8	7.3	10.8	14.2	17.7	21.2	24.7	28.2	31.6	35.1	40.9	46.7		
1.0	3.5	6.6	9.7	12.7	15.8	18.9	22.0	25.1	28.2	31.3	36.4	41.6		
1.2	3.2	6.0	8.8	11.5	14.3	17.1	19.9	22.7	25.4	28.2	32.9	37.5		
.4	-2.8	-5.1	-7.5	-9.8	-12.1	-14.4	-16.7	-19.0	-21.4	-23.7	-27.6	-31.4		
.6	2.6	4.6	6.5	8.5	10.5	12.5	14.5	16.5	18.5	20.5	23.8	27.1		
.8	2.4	4.1	5.9	7.6	9.4	11.1	12.9	14.7	16.3	18.1	21.0	23.9		
2.0	2.2	3.6	5.0	6.4	7.8	9.2	10.6	12.0	13.4	14.8	17.1	19.4		
2.5	-3.3	-4.4	-5.5	-6.6	-7.7	-8.8	-10.0	-11.1	-12.2	-14.0	-15.9			
3.0	3.1	4.1	5.0	5.9	6.8	7.8	8.7	9.6	10.5	12.1	13.6			
.5		3.9	4.7	5.5	6.2	7.0	7.8	8.6	9.4	10.8	12.1			
4.0		3.8	4.5	5.2	5.9	6.6	7.3	7.9	8.6	9.8	11.0			
.5			4.4	5.0	5.6	6.2	6.8	7.5	8.1	9.1	10.1			
5.0					4.9	5.5	6.1	6.6	7.2	7.7	8.6	9.6		
6.0						5.3	5.8	6.2	6.7	7.2	7.9	8.7		
7.0							6.1	6.5	6.9	7.6	7.6	8.3		
8.0											7.4	8.0		
9.0												7.9		
Miles	Height of Eye													
m ft	20 66	22.5 74	25 82	27.5 90	30 98	32.5 107	35 115	37.5 123	40 131	42.5 139	45 148	47.5 156		
0.1	° / °	° / °	° / °	° / °	° / °	° / °	° / °	° / °	° / °	° / °	° / °	° / °	° / °	° / °
.2	-6 10.8	-6 57.2	-7 43.5	-8 29.9	-9 16.2	-10 02.6	-10 48.9	-11 35.3	-12 21.6	-13 08.0	-13 54.3	-14 40.7		
.3	3 05.5	3 28.6	3 51.8	4 15.0	4 38.2	5 01.4	5 24.5	5 47.7	6 10.9	6 34.0	6 57.2	7 20.4		
.4	2 03.7	2 19.2	2 34.6	2 50.1	3 05.5	3 21.0	3 36.3	3 51.9	4 07.3	4 22.8	4 38.2	4 53.7		
.5	1 32.9	1 44.5	1 56.0	2 07.6	2 19.2	2 30.8	2 42.4	2 54.0	3 05.6	3 17.2	3 28.7	3 40.3		
	1 14.4	1 23.6	1 32.9	1 42.2	1 51.4	2 00.7	2 10.0	2 19.3	2 28.5	2 37.8	2 47.1	2 56.3		
0.6	-1 02.1	-1 09.8	-1 17.5	-1 25.2	-1 33.0	-1 40.7	-1 48.4	-1 56.1	-2 03.9	-2 11.6	-2 19.3	-2 27.0		
.7	53.3	59.9	1 06.5	1 13.1	1 19.8	1 26.4	1 33.0	1 39.6	1 46.2	1 52.8	1 59.4	2 06.1		
.8	46.7	52.5	58.3	1 04.1	1 09.9	1 15.7	1 21.5	1 27.2	1 33.0	1 38.8	1 44.6	1 50.4		
.9	41.6	46.7	51.9	57.0	1 02.2	1 07.3	1 12.5	1 17.6	1 22.8	1 27.9	1 33.1	1 38.2		
1.0	37.5	42.1	46.8	51.4	56.0	1 00.7	1 05.3	1 09.9	1 14.6	1 19.2	1 23.9	1 28.5		
1.2	-31.4	-35.3	-39.1	-43.0	-46.9	-50.7	-54.6	-58.4	-1 02.3	-1 06.2	-1 10.0	-1 13.9		
.4	27.1	30.4	33.7	37.0	40.3	43.6	46.9	50.3	53.9	56.9	1 00.2	1 03.5		
.6	23.9	26.8	29.7	32.6	35.4	38.3	41.2	44.1	47.0	49.9	52.8	55.7		
.8	21.4	23.9	26.5	29.1	31.7	34.2	36.8	39.4	42.0	44.5	47.1	49.7		
2.0	19.4	21.7	24.0	26.3	28.7	31.0	33.3	35.6	37.9	40.2	42.6	44.9		
2.5	-15.9	-17.8	-19.6	-21.5	-23.3	-25.2	-27.0	-28.9	-30.7	-32.6	-34.4	-36.3		
3.0	13.6	15.2	16.7	18.3	19.8	21.4	22.9	24.4	26.0	27.5	29.1	30.6		
3.5	12.1	13.4	14.7	16.0	17.4	18.7	20.0	21.3	22.7	24.0	25.3	26.6		
4.0	11.0	12.1	13.3	14.4	15.6	16.8	17.9	19.1	20.2	21.4	22.5	23.7		
4.5	10.1	11.2	12.2	13.2	14.3	15.3	16.3	17.4	18.4	19.5	20.4	21.5		
5.0	-9.6	-10.5	-11.4	-12.4	-13.3	-14.2	-15.1	-16.1	-17.0	-17.9	-18.8	-19.8		
6.0	8.7	9.5	10.3	11.0	11.8	12.6	13.4	14.1	14.9	15.7	16.4	17.2		
7.0	8.3	8.9	9.6	10.2	10.9	11.6	12.2	12.9	13.6	14.2	14.9	15.5		
8.0	8.0	8.6	9.2	9.8	10.3	10.9	11.5	12.1	12.6	13.2	13.8	14.4		
9.0	7.9	8.4	9.0	9.5	10.0	10.5	11.0	11.5	12.1	12.6	13.1	13.6		
10.0			-8.9	-9.3	-9.8	-10.3	-10.7	-11.2	-11.6	-12.1	-12.6	-13.0		
11.0					9.7	10.1	10.5	11.0	11.4	11.8	12.2	12.7		
12.0								10.9	11.3	11.6	12.0	12.4		
13.0									11.2	11.6	11.9	12.3		
14.0											12.2	12.6		

DISTANCE OF THE SEA HORIZON

Height			Dist.		Height			Dist.		Height			Dist.	
m	ft	mls	m	ft	Miles	m	ft	Miles	m	ft	Miles	m	ft	
0.5	1.6	1.5	40	131	13.3	200	656	29.6						
1.0	3	2.1	42	138	13.6	205	673	30.0						
1.5	5	2.6	44	144	13.9	210	689	30.4						
2.0	7	3.0	46	151	14.2	215	705	30.7						
2.5	8	3.3	48	157	14.5	220	722	31.1						
			50	164	14.8	225	738	31.4						
3.0	10	3.6	52	171	15.1	230	755	31.8						
3.5	11	3.9	54	177	15.4	235	771	32.1						
4.0	13	4.2	56	184	15.7	240	787	32.5						
4.5	15	4.4	58	190	16.0	245	804	32.8						
5.0	16	4.7	60	197	16.2	250	820	33.1						
5.5	18	4.9	62	203	16.5	260	853	33.8						
6.0	20	5.1	64	210	16.8	270	886	34.4						
6.5	21	5.3	66	217	17.0	280	919	35.1						
7.0	23	5.5	68	223	17.3	290	951	35.7						
7.5	25	5.7	70	230	17.5	300	984	36.3						
8.0	26	5.9	72	236	17.8	310	1017	36.9						
8.5	28	6.1	74	243	18.0	320	1050	37.5						
9.0	30	6.3	76	249	18.3	330	1083	38.1						
9.5	31	6.5	78	256	18.5	340	1115	38.6						
10.0	33	6.6	80	262	18.7	350	1148	39.2						
11	36	6.9	82	269	19.0	360	1181	39.8						
12	39	7.3	84	276	19.2	370	1214	40.3						
13	43	7.6	86	282	19.4	380	1247	40.8						
14	46	7.8	88	289	19.7	390	1280	41.4						
15	49	8.1	90	295	19.9	400	1312	41.9						
16	52	8.4	92	302	20.1	410	1345	42.4						
17	56	8.6	94	308	20.3	420	1378	42.9						
18	59	8.9	96	315	20.5	430	1411	43.4						
19	62	9.1	98	322	20.7	440	1444	43.9						
20	66	9.4	100	328	21.0	450	1476	44.4						
21	69	9.6	105	344	21.5	460	1509	44.9						
22	72	9.8	110	361	22.0	470	1542	45.4						
23	75	10.0	115	377	22.5	480	1575	45.9						
24	79	10.3	120	394	23.0	490	1608	46.4						
25	82	10.5	125	410	23.4	500	1640	46.8						
26	85	10.7	130	427	23.9	510	1673	47.3						
27	89	10.9	135	443	24.3	520	1706	47.8						
28	92	11.1	140	459	24.8	530	1739	48.2						
29	95	11.3	145	476	25.2	540	1772	48.7						
30	98	11.5	150	492	25.7	550	1804	49.1						
31	102	11.7	155	509	26.1	560	1837	49.6						
32	105	11.9	160	525	26.5	570	1870	50.0						
33	108	12.0	165	541	26.9	580	1903	50.5						
34	112	12.2	170	558	27.3	590	1936	50.9						
35	115	12.4	175	574	27.7	600	1969	51.3						
36	118	12.6	180	591	28.1	610	2001	51.7						
37	121	12.7	185	607	28.5	620	2034	52.2						
38	125	12.9	190	623	28.9	630	2067	52.6						
39	128	13.1	195	640	29.3	640	2100	53.0						
40	131	13.3	200	656	29.6	650	2133	53.4						

**CORRECTION REQUIRED to CONVERT a
RADIO GREAT CIRCLE BEARING to
MERCATORIAL BEARING**

Mean Lat. Lat.	DIFFERENCE OF LONGITUDE OF SHIP AND RADIO STATION														Mean Lat. Lat.	
	2°	4°	6°	8°	10°	12°	14°	16°	18°	20°	22°	24°	26°	28°	30°	
0°	0°	0°	0°	0°	0°	0°	0°	0°	0°	0°	0°	0°	0°	0°	0°	0°
84	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	9.9	10.9	11.9	12.9	13.9	14.9	84
81	1.0	2.0	2.9	4.0	4.9	5.9	6.9	7.9	8.9	9.9	10.9	11.9	12.8	13.8	14.8	81
78	1.0	2.0	2.9	3.9	4.9	5.9	6.8	7.8	8.8	9.8	10.8	11.7	12.7	13.7	14.7	78
75	1.0	1.9	2.9	3.9	4.8	5.8	6.8	7.7	8.7	9.7	10.7	11.6	12.6	13.5	14.4	75
72	1.0	1.9	2.9	3.8	4.8	5.7	6.7	7.6	8.6	9.5	10.5	11.4	12.4	13.3	14.3	72
69	0.9	1.9	2.8	3.7	4.7	5.6	6.5	7.5	8.4	9.3	10.3	11.2	12.1	13.1	14.0	69
66	0.9	1.8	2.8	3.7	4.6	5.5	6.4	7.3	8.2	9.1	10.0	11.0	11.9	12.8	13.7	66
63	0.9	1.8	2.7	3.6	4.5	5.4	6.3	7.1	8.0	8.9	9.8	10.7	11.6	12.5	13.3	63
60	0.9	1.7	2.6	3.5	4.3	5.2	6.1	6.9	7.8	8.6	9.5	10.4	11.2	12.1	12.9	60
57	0.8	1.7	2.5	3.4	4.2	5.0	5.9	6.7	7.5	8.4	9.2	10.0	10.9	11.7	12.5	57
54	0.8	1.6	2.4	3.3	4.1	4.9	5.7	6.5	7.3	8.1	8.9	9.7	10.5	11.3	12.1	54
51	0.8	1.6	2.3	3.1	3.9	4.7	5.5	6.2	7.0	7.8	8.5	9.3	10.1	10.8	11.6	51
48	0.8	1.5	2.2	3.0	3.7	4.5	5.2	5.9	6.7	7.4	8.2	8.9	9.6	10.4	11.1	48
45	0.7	1.4	2.1	2.8	3.5	4.2	4.9	5.6	6.3	7.1	7.8	8.5	9.2	9.9	10.6	45
42	0.7	1.4	2.0	2.7	3.4	4.0	4.7	5.4	6.0	6.7	7.4	8.0	8.7	9.4	10.0	42
39	0.6	1.3	1.9	2.5	3.2	3.8	4.4	5.0	5.7	6.3	6.9	7.5	8.1	8.8	9.4	39
36	0.6	1.2	1.8	2.4	3.0	3.5	4.1	4.7	5.3	5.9	6.4	7.0	7.6	8.2	8.7	36
33	0.5	1.1	1.6	2.2	2.7	3.3	3.8	4.4	4.9	5.4	6.0	6.5	7.1	7.6	8.1	33
30	0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5	5.0	5.5	6.0	6.5	7.0	7.4	30
27	0.5	0.9	1.4	1.8	2.3	2.7	3.2	3.6	4.1	4.5	5.0	5.4	5.9	6.3	6.8	27
24	0.4	0.8	1.2	1.6	2.1	2.4	2.9	3.3	3.6	4.0	4.4	4.8	5.2	5.6	6.0	24
21	0.3	0.7	1.1	1.4	1.8	2.2	2.5	2.9	3.2	3.6	3.9	4.3	4.6	5.0	5.3	21
18	0.3	0.6	0.9	1.2	1.6	1.9	2.2	2.5	2.8	3.1	3.4	3.7	4.0	4.3	4.6	18
15	0.3	0.5	0.8	1.0	1.3	1.6	1.8	2.1	2.3	2.6	2.8	3.1	3.3	3.6	3.8	15
12	0.2	0.4	0.6	0.8	1.0	1.3	1.5	1.7	1.9	2.1	2.3	2.5	2.7	2.9	3.1	12
9	0.2	0.3	0.5	0.6	0.8	1.0	1.1	1.2	1.4	1.6	1.7	1.9	2.0	2.2	2.3	9
6	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1	1.2	1.3	1.5	1.6	6
3	0.1	0.1	0.2	0.2	0.3	0.3	0.4	0.4	0.5	0.5	0.6	0.6	0.7	0.7	0.8	3
	2°	4°	6°	8°	10°	12°	14°	16°	18°	20°	22°	24°	26°	28°	30°	

In both North and South latitudes always allow the above corrections towards the Equator from the Radio Great Circle bearing to obtain the corresponding Mercatorial line of bearing.

N.B.—The Bearings must always be laid off, on the chart, from the Radio Station.

EXAMPLE 1. A ship in D.R. position Lat. 39° 37' N., Long. 56° 25' W., receives from a Radio Station in Lat. 35° 14' N., Long. 75° 32' W., the Radio bearing 074°. Find the correction and the corresponding Mercatorial bearing.

Mean Lat. is $\frac{1}{2}(39^{\circ} 37' + 35^{\circ} 14')$ or $\frac{1}{2}(74^{\circ} 51') = 37^{\circ} 4$.

D. Long. is 75° 32' - 56° 25' = 19° 1.

For Mean Lat. 37° 4 and D. Long. 19° 1 the Table gives a correction of 6° (approx.).

Allowing this correction towards the Equator the corresponding Mercatorial bearing is found to be 074° + 6° = 080°.

EXAMPLE 2. A ship in D.R. position Lat. 37° 26' S., Long. 84° 35' W., finds, with her own apparatus, the Radio bearing of a station in Lat. 36° 37' S., Long. 73° 03' W., to be 089°. Find the correction and the corresponding Mercatorial bearing.

For Mean Lat. 37° and D. Long. 11° 5 the Table gives a correction of 3° 5 (approx.).

Allowing this correction towards the Equator the corresponding Mercatorial bearing is found to be 089° - 3° 5 = 085° 5.

CONVERSION OF ARC TO TIME

Arc	Time	Arc	Time	Arc	Time	Arc	Time	Arc	Time	Arc	Time	Arc	Time	Arc	Time	Arc	Time
°	h. m.	Parts of 1'	s.	"	s.												
'	m. s.																
0	0 00	60	4 00	120	8 00	180	12 00	240	16 00	300	20 00	0·1	0·4	0	0·00		
1	0 04	61	4 04	121	8 04	181	12 04	241	16 04	301	20 04	1	0·07				
2	0 08	62	4 08	122	8 08	182	12 08	242	16 08	302	20 08	2	0·13				
3	0 12	63	4 12	123	8 12	183	12 12	243	16 12	303	20 12	3	0·20				
4	0 16	64	4 16	124	8 16	184	12 16	244	16 16	304	20 16	4	0·27				
5	0 20	65	4 20	125	8 20	185	12 20	245	16 20	305	20 20	5	0·33				
6	0 24	66	4 24	126	8 24	186	12 24	246	16 24	306	20 24	6	0·40				
7	0 28	67	4 28	127	8 28	187	12 28	247	16 28	307	20 28	7	0·47				
8	0 32	68	4 32	128	8 32	188	12 32	248	16 32	308	20 32	8	0·53				
9	0 36	69	4 36	129	8 36	189	12 36	249	16 36	309	20 36	9	0·60				
10	0 40	70	4 40	130	8 40	190	12 40	250	16 40	310	20 40	10	0·67				
11	0 44	71	4 44	131	8 44	191	12 44	251	16 44	311	20 44	11	0·73				
12	0 48	72	4 48	132	8 48	192	12 48	252	16 48	312	20 48	12	0·80				
13	0 52	73	4 52	133	8 52	193	12 52	253	16 52	313	20 52	13	0·87				
14	0 56	74	4 56	134	8 56	194	12 56	254	16 56	314	20 56	14	0·93				
15	1 00	75	5 00	135	9 00	195	13 00	255	17 00	315	21 00	15	1·00				
16	1 04	76	5 04	136	9 04	196	13 04	256	17 04	316	21 04	16	1·07				
17	1 08	77	5 08	137	9 08	197	13 08	257	17 08	317	21 08	17	1·13				
18	1 12	78	5 12	138	9 12	198	13 12	258	17 12	318	21 12	18	1·20				
19	1 16	79	5 16	139	9 16	199	13 16	259	17 16	319	21 16	19	1·27				
20	1 20	80	5 20	140	9 20	200	13 20	260	17 20	320	21 20	20	1·33				
21	1 24	81	5 24	141	9 24	201	13 24	261	17 24	321	21 24	21	1·40				
22	1 28	82	5 28	142	9 28	202	13 28	262	17 28	322	21 28	22	1·47				
23	1 32	83	5 32	143	9 32	203	13 32	263	17 32	323	21 32	23	1·53				
24	1 36	84	5 36	144	9 36	204	13 36	264	17 36	324	21 36	24	1·60				
25	1 40	85	5 40	145	9 40	205	13 40	265	17 40	325	21 40	25	1·67				
26	1 44	86	5 44	146	9 44	206	13 44	266	17 44	326	21 44	26	1·73				
27	1 48	87	5 48	147	9 48	207	13 48	267	17 48	327	21 48	27	1·80				
28	1 52	88	5 52	148	9 52	208	13 52	268	17 52	328	21 52	28	1·87				
29	1 56	89	5 56	149	9 56	209	13 56	269	17 56	329	21 56	29	1·93				
30	2 00	90	6 00	150	10 00	210	14 00	270	18 00	330	22 00	30	2·00				
31	2 04	91	6 04	151	10 04	211	14 04	271	18 04	331	22 04	31	2·07				
32	2 08	92	6 08	152	10 08	212	14 08	272	18 08	332	22 08	32	2·13				
33	2 12	93	6 12	153	10 12	213	14 12	273	18 12	333	22 12	33	2·20				
34	2 16	94	6 16	154	10 16	214	14 16	274	18 16	334	22 16	34	2·27				
35	2 20	95	6 20	155	10 20	215	14 20	275	18 20	335	22 20	35	2·33				
36	2 24	96	6 24	156	10 24	216	14 24	276	18 24	336	22 24	36	2·40				
37	2 28	97	6 28	157	10 28	217	14 28	277	18 28	337	22 28	37	2·47				
38	2 32	98	6 32	158	10 32	218	14 32	278	18 32	338	22 32	38	2·53				
39	2 36	99	6 36	159	10 36	219	14 36	279	18 36	339	22 36	39	2·60				
40	2 40	100	6 40	160	10 40	220	14 40	280	18 40	340	22 40	40	2·67				
41	2 44	101	6 44	161	10 44	221	14 44	281	18 44	341	22 44	41	2·73				
42	2 48	102	6 48	162	10 48	222	14 48	282	18 48	342	22 48	42	2·80				
43	2 52	103	6 52	163	10 52	223	14 52	283	18 52	343	22 52	43	2·87				
44	2 56	104	6 56	164	10 56	224	14 56	284	18 56	344	22 56	44	2·93				
45	3 00	105	7 00	165	11 00	225	15 00	285	19 00	345	23 00	45	3·00				
46	3 04	106	7 04	166	11 04	226	15 04	286	19 04	346	23 04	46	3·07				
47	3 08	107	7 08	167	11 08	227	15 08	287	19 08	347	23 08	47	3·13				
48	3 12	108	7 12	168	11 12	228	15 12	288	19 12	348	23 12	48	3·20				
49	3 16	109	7 16	169	11 16	229	15 16	289	19 16	349	23 16	49	3·27				
50	3 20	110	7 20	170	11 20	230	15 20	290	19 20	350	23 20	50	3·33				
51	3 24	111	7 24	171	11 24	231	15 24	291	19 24	351	23 24	51	3·40				
52	3 28	112	7 28	172	11 28	232	15 28	292	19 28	352	23 28	52	3·47				
53	3 32	113	7 32	173	11 32	233	15 32	293	19 32	353	23 32	53	3·53				
54	3 36	114	7 36	174	11 36	234	15 36	294	19 36	354	23 36	54	3·60				
55	3 40	115	7 40	175	11 40	235	15 40	295	19 40	355	23 40	55	3·67				
56	3 44	116	7 44	176	11 44	236	15 44	296	19 44	356	23 44	56	3·73				
57	3 48	117	7 48	177	11 48	237	15 48	297	19 48	357	23 48	57	3·80				
58	3 52	118	7 52	178	11 52	238	15 52	298	19 52	358	23 52	58	3·87				
59	3 56	119	7 56	179	11 56	239	15 56	299	19 56	359	23 56	59	3·93				
60	4 00	120	8 00	180	12 00	240	16 00	300	20 00	360	24 00	60	4·00				

SUN'S TOTAL CORRECTION

To be applied to the Observed Altitude of the Sun's Lower (L) or Upper (U) Limb

Height of Eye

Obs. Alt.	2.0m (7ft)		2.3m (8ft)		2.7m (9ft)		3.1m (10ft)		3.5m (11ft)		3.9m (13ft)		4.4m (15ft)		4.9m (16ft)		5.4m (18ft)		5.9m (20ft)		6.5m (21ft)		7.1m (23ft)	
	L	U	L	U	L	U	L	U	L	U	L	U	L	U	L	U	L	U	L	U	L	U	L	U
10 00	+8.5	-23.5	+8.3	-23.7	+8.1	-23.9	+7.9	-24.1	+7.7	-24.3	+7.5	-24.5	+7.3	-24.7	+7.1	-24.9	+6.9	-25.1	+6.7	-25.3	+6.5	-25.5	+6.1	-25.7
30	8.7	-23.3	8.5	-23.5	8.3	-23.7	8.1	-23.9	7.9	-24.1	7.7	-24.3	7.5	-24.5	7.3	-24.7	7.1	-24.9	6.9	-25.1	6.7	-25.3	6.5	-25.5
11 00	8.9	-23.1	8.7	-23.3	8.5	-23.5	8.3	-23.7	8.1	-23.9	7.9	-24.1	7.7	-24.3	7.5	-24.5	7.3	-24.7	7.1	-24.9	6.9	-25.1	6.7	-25.3
30	9.1	-22.9	8.9	-23.1	8.7	-23.3	8.5	-23.5	8.3	-23.7	8.1	-23.9	7.9	-24.1	7.7	-24.3	7.5	-24.5	7.3	-24.7	7.1	-24.9	6.9	-25.1
12 00	9.3	-22.7	9.1	-22.9	8.9	-23.1	8.7	-23.3	8.5	-23.5	8.3	-23.7	8.1	-23.9	7.9	-24.1	7.7	-24.3	7.5	-24.5	7.3	-24.7	7.1	-24.9
30	9.5	-22.5	9.3	-22.7	9.1	-22.9	8.9	-23.1	8.7	-23.3	8.5	-23.5	8.3	-23.7	8.1	-23.9	7.9	-24.1	7.7	-24.3	7.5	-24.5	7.3	-24.7
13 00	+9.7	-22.3	+9.5	-22.5	+9.3	-22.7	+9.1	-22.9	+8.9	-23.1	+8.7	-23.3	+8.5	-23.5	+8.3	-23.7	+8.1	-23.9	+7.9	-24.1	+7.7	-24.3	+7.5	-24.5
14 00	9.9	-22.1	9.7	-22.3	9.5	-22.5	9.3	-22.7	9.1	-22.9	8.9	-23.1	8.7	-23.3	8.5	-23.5	8.3	-23.7	8.1	-23.9	7.9	-24.1	7.7	-24.3
15 00	10.1	-21.9	9.9	-22.1	9.7	-22.3	9.5	-22.5	9.3	-22.7	9.1	-22.9	8.9	-23.1	8.7	-23.3	8.5	-23.5	8.3	-23.7	8.1	-23.9	7.9	-24.1
16 00	10.3	-21.7	10.1	-21.9	9.9	-22.1	9.7	-22.3	9.5	-22.5	9.3	-22.7	9.1	-22.9	8.9	-23.1	8.7	-23.3	8.5	-23.5	8.3	-23.7	8.1	-23.9
17 00	10.5	-21.5	10.3	-21.7	10.1	-21.9	9.9	-22.1	9.7	-22.3	9.5	-22.5	9.3	-22.7	9.1	-22.9	8.9	-23.1	8.7	-23.3	8.5	-23.5	8.3	-23.7
18 00	10.7	-21.3	10.5	-21.5	10.3	-21.7	10.1	-21.9	9.9	-22.1	9.7	-22.3	9.5	-22.5	9.3	-22.7	9.1	-22.9	8.9	-23.1	8.7	-23.3	8.5	-23.5
19 00	10.9	-21.1	10.7	-21.3	10.5	-21.5	10.3	-21.7	10.1	-21.9	9.9	-22.1	9.7	-22.3	9.5	-22.5	9.3	-22.7	9.1	-22.9	8.9	-23.1	8.7	-23.3
20 00	+11.1	-20.9	+10.9	-21.1	+10.7	-21.3	+10.5	-21.5	+10.3	-21.7	+10.1	-21.9	+9.9	-22.1	+9.7	-22.3	+9.5	-22.5	+9.3	-22.7	+9.1	-22.9	+8.9	-23.1
22 00	11.3	-20.7	11.1	-20.9	10.9	-21.1	10.7	-21.3	10.5	-21.5	10.3	-21.7	10.1	-21.9	9.9	-22.1	9.7	-22.3	9.5	-22.5	9.3	-22.7	9.1	-22.9
24 00	11.5	-20.5	11.3	-20.7	11.1	-20.9	10.9	-21.1	10.7	-21.3	10.5	-21.5	10.3	-21.7	10.1	-21.9	9.9	-22.1	9.7	-22.3	9.5	-22.5	9.3	-22.7
26 00	11.7	-20.3	11.5	-20.5	11.3	-20.7	11.1	-20.9	10.9	-21.1	10.7	-21.3	10.5	-21.5	10.3	-21.7	10.1	-21.9	9.9	-22.1	9.7	-22.3	9.5	-22.5
29 00	11.9	-20.1	11.7	-20.3	11.5	-20.5	11.3	-20.7	11.1	-20.9	10.9	-21.1	10.7	-21.3	10.5	-21.5	10.3	-21.7	10.1	-21.9	9.9	-22.1	9.7	-22.3
32 00	12.1	-19.9	11.9	-20.1	11.7	-20.3	11.5	-20.5	11.3	-20.7	11.1	-20.9	10.9	-21.1	10.7	-21.3	10.5	-21.5	10.3	-21.7	10.1	-21.9	9.9	-22.1
36 00	12.3	-19.7	12.1	-19.9	11.9	-20.1	11.7	-20.3	11.5	-20.5	11.3	-20.7	11.1	-20.9	10.9	-21.1	10.7	-21.3	10.5	-21.5	10.3	-21.7	10.1	-21.9
40 00	+12.5	-19.5	+12.3	-19.7	+12.1	-19.9	+11.9	-20.1	+11.7	-20.3	+11.5	-20.5	+11.3	-20.7	+11.1	-20.9	+10.9	-21.1	+10.7	-21.3	+10.5	-21.5	+10.3	-21.7
45 00	12.7	-19.3	12.5	-19.5	12.3	-19.7	12.1	-19.9	11.9	-20.1	11.7	-20.3	11.5	-20.5	11.3	-20.7	11.1	-20.9	10.9	-21.1	10.7	-21.3	10.5	-21.5
52 00	12.9	-19.1	12.7	-19.3	12.5	-19.5	12.3	-19.7	12.1	-19.9	11.9	-20.1	11.7	-20.3	11.5	-20.5	11.3	-20.7	11.1	-20.9	10.9	-21.1	10.7	-21.3
60 00	13.1	-18.9	12.9	-19.1	12.7	-19.3	12.5	-19.5	12.3	-19.7	12.1	-19.9	11.9	-20.1	11.7	-20.3	11.5	-20.5	11.3	-20.7	11.1	-20.9	10.9	-21.1
75 00	13.3	-18.7	13.1	-18.9	12.9	-19.1	12.7	-19.3	12.5	-19.5	12.3	-19.7	12.1	-19.9	11.9	-20.1	11.7	-20.3	11.5	-20.5	11.3	-20.7	11.1	-20.9
90 00	13.5	-18.5	13.3	-18.7	13.1	-18.9	12.9	-19.1	12.7	-19.3	12.5	-19.5	12.3	-19.7	12.1	-19.9	11.9	-20.1	11.7	-20.3	11.5	-20.5	11.3	-20.7

Obs. Alt.	17.2m (56ft)		18.2m (60ft)		19.2m (63ft)		20.2m (66ft)		21.2m (70ft)		22.2m (73ft)		23.3m (77ft)		24.4m (80ft)		25.5m (84ft)		26.3m (88ft)		27.9m (92ft)		29.1m (96ft)	
	L	U	L	U	L	U	L	U	L	U	L	U	L	U	L	U	L	U	L	U	L	U	L	U
10 00	+3.7	-28.3	+3.5	-28.5	+3.3	-28.7	+3.1	-28.9	+2.9	-29.1	+2.7	-29.3	+2.5	-29.5	+2.3	-29.7	+2.1	-29.9	+1.9	-30.1	+1.7	-30.3	+1.5	-30.5
30	3.9	-28.1	3.7	-28.3	3.5	-28.5	3.3	-28.7	3.1	-28.9	2.9	-29.1	2.7	-29.3	2.5	-29.5	2.3	-29.7	2.1	-29.9	1.9	-30.1	1.7	-30.3
11 00	4.1	-27.9	3.9	-28.1	3.7	-28.3	3.5	-28.5	3.3	-28.7	3.1	-28.9	2.9	-29.1	2.7	-29.3	2.5	-29.5	2.3	-29.7	2.1	-29.9	1.9	-30.1
30	4.3	-27.7	4.1	-27.9	3.9	-28.1	3.7	-28.3	3.5	-28.5	3.3	-28.7	3.1	-28.9	2.9	-29.1	2.7	-29.3	2.5	-29.5	2.3	-29.7	2.1	-29.9
12 00	4.5	-27.5	4.3	-27.7	4.1	-27.9	3.9	-28.1	3.7	-28.3	3.5	-28.5	3.3	-28.7	3.1	-28.9	2.9	-29.1	2.7	-29.3	2.5	-29.5	2.3	-29.7
30	4.7	-27.3	4.5	-27.5	4.3	-27.7	4.1	-27.9	3.9	-28.1	3.7	-28.3	3.5	-28.5	3.3	-28.7	3.1	-28.9	2.9	-29.1	2.7	-29.3	2.5	-29.5
13 00	+4.9	-27.1	+4.7	-27.3	+4.5	-27.5	+4.3	-27.7	+4.1	-27.9	+3.9	-28.1	+3.7	-28.3	+3.5	-28.5	+3.3	-28.7	+3.1	-28.9	+2.9	-29.1	+2.7	-29.3
14 00	5.1	-26.9	4.9	-27.1	4.7	-27.3	4.5	-27.5	4.3	-27.7	4.1	-27.9	3.9	-28.1	3.7	-28.3	3.5	-28.5	3.3	-28.7	3.1	-28.9	2.9	-29.1
15 00	5.3	-26.7	5.1	-26.9	4.9	-27.1	4.7	-27.3	4.5	-27.5	4.3	-27.7	4.1	-27.9	3.9	-28.1	3.7	-28.3	3.5	-28.5	3.3	-28.7	3.1	-28.9
16 00	5.5	-26.5	5.3	-26.7	5.1	-26.9	4.9	-27.1	4.7	-27.3	4.5	-27.5	4.3	-27.7	4.1	-27.9	3.9	-28.1	3.7	-28.3	3.5	-28.5	3.3	-28.7
17 00	5.7	-26.3	5.5	-26.5	5.3	-26.7	5.1	-26.9	4.9	-27.1	4.7	-27.3	4.5	-27.5	4.3	-27.7	4.1	-27.9	3.9	-28.1	3.7	-28.3	3.5	-28.5
18 00	5.9	-26.1	5.7	-26.3	5.5	-26.5	5.3	-26.7	5.1	-26.9	4.9	-27.1	4.7	-27.3	4.5	-27.5	4.3	-27.7	4.1	-27.9	3.9	-28.1	3.7	-28.3
19 00	6.1	-25.9	5.9	-26.1	5.7	-26.3	5.5	-26.5	5.3	-26.7	5.1	-26.9	4.9	-27.1	4.7	-27.3	4.5	-27.5	4.3	-27.7	4.1	-27.9	3.9	-28.1
20 00	+6.3	-25.7	+6.1	-25.9	+5.9	-26.1	+5.7	-26.3	+5.5	-26.5	+5.3	-26.7	+5.1	-26.9	+4.9	-27.1	+4.7	-27.3	+4.5	-27.5	+4.3	-27.7	+4.1	-27.9
22 00	6.5	-25.5	6.3	-25.7	6.1	-25.9	5.9	-26.1	5.7	-26.3	5.5	-26.5	5.3	-26.7	5.1	-26.9	4.9	-27.1	4.7	-27.3	4.5	-27.5	4.3	-27.7
24 00	6.7	-25.3	6.5	-25.5	6.3	-25.7	6.1	-25.9	5.9	-26.1	5.7	-26.3	5.5	-26.5	5.3	-26.7	5.1	-26.9	4.9	-27.1	4.7	-27.3	4.5	-27.5
26 00	6.9	-25.1	6.7	-25.3	6.5	-25.5	6.3	-25.7	6.1	-25.9	5.9	-26.1	5.7	-26.3	5.5	-26.5	5.3	-26.7	5.1	-26.9	4.9	-27.1	4.7	-27.3
29 00	7.1	-24.9	6.9	-25.1	6.7	-25.3	6.5	-25.5	6.3	-25.7	6.1	-25.9	5.9	-26.1	5.7	-26.3	5.5	-26.5	5.3	-26.7	5.1	-26.9	4.9	-27.1
32 00	7.3	-24.7	7.1	-24.9	6.9	-25.1	6.7	-25.3	6.5	-25.5	6.3	-25.7	6.1	-25.9	5.9	-26.1	5.7							

DECIMALS OF THE DEGREE

	.0	.2	.4	.6	.8
0	0.000	0.003	0.007	0.010	0.013
1	.017	.020	.023	.027	.030
2	.033	.037	.040	.043	.047
3	.050	.053	.057	.060	.063
4	.067	.070	.073	.077	.080
5	0.083	0.087	0.090	0.093	0.097
6	.100	.103	.107	.110	.113
7	.117	.120	.123	.127	.130
8	.133	.137	.140	.143	.147
9	.150	.153	.157	.160	.163
10	0.167	0.170	0.173	0.177	0.180
11	.183	.187	.190	.193	.197
12	.200	.203	.207	.210	.213
13	.217	.220	.223	.227	.230
14	.233	.237	.240	.243	.247
15	0.250	0.253	0.257	0.260	0.263
16	.267	.270	.273	.277	.280
17	.283	.287	.290	.293	.297
18	.300	.303	.307	.310	.313
19	.317	.320	.323	.327	.330
20	0.333	0.337	0.340	0.343	0.347
21	.350	.353	.357	.360	.363
22	.367	.370	.373	.377	.380
23	.383	.387	.390	.393	.397
24	.400	.403	.407	.410	.413
25	0.417	0.420	0.423	0.427	0.430
26	.433	.437	.440	.443	.447
27	.450	.453	.457	.460	.463
28	.467	.470	.473	.477	.480
29	.483	.487	.490	.493	.497
30	0.500	0.503	0.507	0.510	0.513
31	.517	.520	.523	.527	.530
32	.533	.537	.540	.543	.547
33	.550	.553	.557	.560	.563
34	.567	.570	.573	.577	.580
35	0.583	0.587	0.590	0.593	0.597
36	.600	.603	.607	.610	.613
37	.617	.620	.623	.627	.630
38	.633	.637	.640	.643	.647
39	.650	.653	.657	.660	.663
40	0.667	0.670	0.673	0.677	0.680
41	.683	.687	.690	.693	.697
42	.700	.703	.707	.710	.713
43	.717	.720	.723	.727	.730
44	.733	.737	.740	.743	.747
45	0.750	0.753	0.757	0.760	0.763
46	.767	.770	.773	.777	.780
47	.783	.787	.790	.793	.797
48	.800	.803	.807	.810	.813
49	.817	.820	.823	.827	.830
50	0.833	0.837	0.840	0.843	0.847
51	.850	.853	.857	.860	.863
52	.867	.870	.873	.877	.880
53	.883	.887	.890	.893	.897
54	.900	.903	.907	.910	.913
55	0.917	0.920	0.923	0.927	0.930
56	.933	.937	.940	.943	.947
57	.950	.953	.957	.960	.963
58	.967	.970	.973	.977	.980
59	.983	.987	.990	.993	.997

STAR'S TOTAL CORRECTION

Metres	2.0	2.3	2.7	3.1	3.5	3.9	4.4	4.9	5.4	5.9	6.5	7.1
Feet	7	8	9	10	11	13	14	16	18	19	21	23
Obs. Alt.	/	/	/	/	/	/	/	/	/	/	/	/
10 00	7.8	8.0	8.2	8.4	8.6	8.8	9.0	9.2	9.4	9.6	9.8	10.0
11 00	7.4	7.6	7.8	8.0	8.2	8.4	8.6	8.8	9.0	9.2	9.4	9.6
12 00	7.0	7.2	7.4	7.6	7.8	8.0	8.2	8.4	8.6	8.8	9.0	9.2
13 00	6.6	6.8	7.0	7.2	7.4	7.6	7.8	8.0	8.2	8.4	8.6	8.8
14 00	6.2	6.4	6.6	6.8	7.0	7.2	7.4	7.6	7.8	8.0	8.2	8.4
15 00	6.0	6.2	6.4	6.6	6.8	7.0	7.2	7.4	7.6	7.8	8.0	8.2
16 00	5.8	6.0	6.2	6.4	6.6	6.8	7.0	7.2	7.4	7.6	7.8	8.0
17 00	5.6	5.8	6.0	6.2	6.4	6.6	6.8	7.0	7.2	7.4	7.6	7.8
18 00	5.4	5.6	5.8	6.0	6.2	6.4	6.6	6.8	7.0	7.2	7.4	7.6
19 00	5.2	5.4	5.6	5.8	6.0	6.2	6.4	6.6	6.8	7.0	7.2	7.4
21 00	5.0	5.2	5.4	5.6	5.8	6.0	6.2	6.4	6.6	6.8	7.0	7.2
23 00	4.8	5.0	5.2	5.4	5.6	5.8	6.0	6.2	6.4	6.6	6.8	7.0
25 00	4.6	4.8	5.0	5.2	5.4	5.6	5.8	6.0	6.2	6.4	6.6	6.8
27 00	4.4	4.6	4.8	5.0	5.2	5.4	5.6	5.8	6.0	6.2	6.4	6.6
29 00	4.2	4.4	4.6	4.8	5.0	5.2	5.4	5.6	5.8	6.0	6.2	6.4
33 00	4.0	4.2	4.4	4.6	4.8	5.0	5.2	5.4	5.6	5.8	6.0	6.2
36 00	3.8	4.0	4.2	4.4	4.6	4.8	5.0	5.2	5.4	5.6	5.8	6.0
41 00	3.6	3.8	4.0	4.2	4.4	4.6	4.8	5.0	5.2	5.4	5.6	5.8
48 00	3.4	3.6	3.8	4.0	4.2	4.4	4.6	4.8	5.0	5.2	5.4	5.6
55 00	3.2	3.4	3.6	3.8	4.0	4.2	4.4	4.6	4.8	5.0	5.2	5.4
65 00	3.0	3.2	3.4	3.6	3.8	4.0	4.2	4.4	4.6	4.8	5.0	5.2
75 00	2.8	3.0	3.2	3.4	3.6	3.8	4.0	4.2	4.4	4.6	4.8	5.0
85 00	2.6	2.8	3.0	3.2	3.4	3.6	3.8	4.0	4.2	4.4	4.6	4.8
90 00	2.5	2.7	2.9	3.1	3.3	3.5	3.7	3.9	4.1	4.3	4.5	4.7

Metres	22.2	23.3	24.4	25.5	26.7	27.9	29.1	30.3	31.6	32.9	34.0	35.5
Feet	73	76	80	84	88	92	95	99	104	108	112	116
Obs. Alt.	/	/	/	/	/	/	/	/	/	/	/	/
10 00	13.6	13.8	14.0	14.2	14.4	14.6	14.8	15.0	15.2	15.4	15.6	15.8
11 00	13.4	13.6	13.8	14.0	14.2	14.4	14.6	14.8	15.0	15.2	15.4	15.6
12 00	12.8	13.0	13.2	13.4	13.6	13.8	14.0	14.2	14.4	14.6	14.8	15.0
13 00	12.4	12.6	12.8	13.0	13.2	13.4	13.6	13.8	14.0	14.2	14.4	14.6
14 00	12.0	12.2	12.4	12.6	12.8	13.0	13.2	13.4	13.6	13.8	14.0	14.2
15 00	11.8	12.0	12.2	12.4	12.6	12.8	13.0	13.2	13.4	13.6	13.8	14.0
16 00	11.6	11.8	12.0	12.2	12.4	12.6	12.8	13.0	13.2	13.4	13.6	13.8
17 00	11.4	11.6	11.8	12.0	12.2	12.4	12.6	12.8	13.0	13.2	13.4	13.6
18 00	11.2	11.4	11.6	11.8	12.0	12.2	12.4	12.6	12.8	13.0	13.2	13.4
19 00	11.0	11.2	11.4	11.6	11.8	12.0	12.2	12.4	12.6	12.8	13.0	13.2
21 00	10.8	11.0	11.2	11.4	11.6	11.8	12.0	12.2	12.4	12.6	12.8	13.0
23 00	10.6	10.8	11.0	11.2	11.4	11.6	11.8	12.0	12.2	12.4	12.6	12.8
25 00	10.4	10.6	10.8	11.0	11.2	11.4	11.6	11.8	12.0	12.2	12.4	12.6
27 00	10.2	10.4	10.6	10.8	11.0	11.2	11.4	11.6	11.8	12.0	12.2	12.4
29 00	10.0	10.2	10.4	10.6	10.8	11.0	11.2	11.4	11.6	11.8	12.0	12.2
33 00	9.8	10.0	10.2	10.4	10.6	10.8	11.0	11.2	11.4	11.6	11.8	12.0
36 00	9.6	9.8	10.0	10.2	10.4	10.6	10.8	11.0	11.2	11.4	11.6	11.8
41 00	9.4	9.6	9.8	10.0	10.2	10.4	10.6	10.8	11.0	11.2	11.4	11.6
48 00	9.2	9.4	9.6	9.8	10.0	10.2	10.4	10.6	10.8	11.0	11.2	11.4
55 00	9.0	9.2	9.4	9.6	9.8	10.0	10.2	10.4	10.6	10.8	11.0	11.2
65 00	8.8	9.0	9.2	9.4	9.6	9.8	10.0	10.2	10.4	10.6	10.8	11.0
75 00	8.6	8.8	9.0	9.2	9.4	9.6	9.8	10.0	10.2	10.4	10.6	10.8
85 00	8.4	8.6	8.8	9.0	9.2	9.4	9.6	9.8	10.0	10.2	10.4	10.6
90 00	8.3	8.5	8.7	8.9	9.1	9.3	9.5	9.7	9.9	10.1	10.3	10.5

To be SUBTRACTED from the
Observed Altitude of the Star

Height of Eye

7.7	8.4	9.1	9.8	10.5	11.2	12.0	12.8	13.6	14.5	15.4	16.3	17.2	18.2	19.2	20.2	21.2
25	28	30	32	34	37	38	42	45	48	51	53	56	60	63	66	70
10.2	10.4	10.6	10.8	11.0	11.2	11.4	11.6	11.8	12.0	12.2	12.4	12.6	12.8	13.0	13.2	13.4
10.0	10.2	10.4	10.6	10.8	11.0	11.2	11.4	11.6	11.8	12.0	12.2	12.4	12.6	12.8	13.0	13.2
9.8	10.0	10.2	10.4	10.6	10.8	11.0	11.2	11.4	11.6	11.8	12.0	12.2	12.4	12.6	12.8	13.0
9.6	9.8	10.0	10.2	10.4	10.6	10.8	11.0	11.2	11.4	11.6	11.8	12.0	12.2	12.4	12.6	12.8
9.4	9.6	9.8	10.0	10.2	10.4	10.6	10.8	11.0	11.2	11.4	11.6	11.8	12.0	12.2	12.4	12.6
9.2	9.4	9.6	9.8	10.0	10.2	10.4	10.6	10.8	11.0	11.2	11.4	11.6	11.8	12.0	12.2	12.4
9.0	9.2	9.4	9.6	9.8	10.0	10.2	10.4	10.6	10.8	11.0	11.2	11.4	11.6	11.8	12.0	12.2
8.8	9.0	9.2	9.4	9.6	9.8	10.0	10.2	10.4	10.6	10.8	11.0	11.2	11.4	11.6	11.8	12.0
8.6	8.8	9.0	9.2	9.4	9.6	9.8	10.0	10.2	10.4	10.6	10.8	11.0	11.2	11.4	11.6	11.8
8.4	8.6	8.8	9.0	9.2	9.4	9.6	9.8	10.0	10.2	10.4	10.6	10.8	11.0	11.2	11.4	11.6
8.2	8.4	8.6	8.8	9.0	9.2	9.4	9.6	9.8	10.0	10.2	10.4	10.6	10.8	11.0	11.2	11.4
8.0	8.2	8.4	8.6	8.8	9.0	9.2	9.4	9.6	9.8	10.0	10.2	10.4	10.6	10.8	11.0	11.2
7.8	8.0	8.2	8.4	8.6	8.8	9.0	9.2	9.4	9.6	9.8	10.0	10.2	10.4	10.6	10.8	11.0
7.6	7.8	8.0	8.2	8.4	8.6	8.8	9.0	9.2	9.4	9.6	9.8	10.0	10.2	10.4	10.6	10.8
7.4	7.6	7.8	8.0	8.2	8.4	8.6	8.8	9.0	9.2	9.4	9.6	9.8	10.0	10.2	10.4	10.6
7.2	7.4	7.6	7.8	8.0	8.2	8.4	8.6	8.8	9.0	9.2	9.4	9.6	9.8	10.0	10.2	10.4
7.0	7.2	7.4	7.6	7.8	8.0	8.2	8.4	8.6	8.8	9.0	9.2	9.4	9.6	9.8	10.0	10.2
6.8	7.0	7.2	7.4	7.6	7.8	8.0	8.2	8.4	8.6	8.8	9.0	9.2	9.4	9.6	9.8	10.0
6.6	6.8	7.0	7.2	7.4	7.6	7.8	8.0	8.2	8.4	8.6	8.8	9.0	9.2	9.4	9.6	9.8
6.4	6.6	6.8	7.0	7.2	7.4	7.6	7.8	8.0	8.2	8.4	8.6	8.8	9.0	9.2	9.4	9.6
6.2	6.4	6.6	6.8	7.0	7.2	7.4	7.6	7.8	8.0	8.2	8.4	8.6	8.8	9.0	9.2	9.4
6.0	6.2	6.4	6.6	6.8	7.0	7.2	7.4	7.6	7.8	8.0	8.2	8.4	8.6	8.8	9.0	9.2
5.8	6.0	6.2	6.4	6.6	6.8	7.0	7.2	7.4	7.6	7.8	8.0	8.2	8.4	8.6	8.8	9.0
5.6	5.8	6.0	6.2	6.4	6.6	6.8	7.0	7.2	7.4	7.6	7.8	8.0	8.2	8.4	8.6	8.8
5.4	5.6	5.8	6.0	6.2	6.4	6.6	6.8	7.0	7.2	7.4	7.6	7.8	8.0	8.2	8.4	8.6
5.2	5.4	5.6	5.8	6.0	6.2	6.4	6.6	6.8	7.0	7.2	7.4	7.6	7.8	8.0	8.2	8.4
5.0	5.2	5.4	5.6	5.8	6.0	6.2	6.4	6.6	6.8	7.0	7.2	7.4	7.6	7.8	8.0	8.2
4.9	5.1	5.3	5.5	5.7	5.9	6.1	6.3	6.5	6.7	6.9	7.1	7.3	7.5	7.7	7.9	8.1

37.0	38.5	40.0	41.5	43.0	44.5	46.0	47.5	49.0
121	126	131	136	141	146	151	156	161
16.0	16.2	16.4	16.6	16.8	17.0	17.2	17.4	17.6
15.8	16.0	16.2	16.4	16.6	16.8	17.0	17.2	17.4
15.6	15.8	16.0	16.2	16.4	16.6	16.8	17.0	17.2
15.4	15.6	15.8	16.0	16.2	16.4	16.6	16.8	17.0
15.2	15.4	15.6	15.8	16.0	16.2	16.4	16.6	16.8
15.0	15.2	15.4	15.6	15.8	16.0	16.2	16.4	16.6
14.8	15.0	15.2	15.4	15.6	15.8	16.0	16.2	16.4
14.6	14.8	15.0	15.2	15.4	15.6	15.8	16.0	16.2
14.4	14.6	14.8	15.0	15.2	15.4	15.6	15.8	16.0
14.2	14.4	14.6	14.8	15.0	15.2	15.4	15.6	15.8
14.0	14.2	14.4	14.6	14.8	15.0	15.2	15.4	15.6
13.8	14.0	14.2	14.4	14.6	14.8	15.0	15.2	15.4
13.6	13.8	14.0	14.2	14.4	14.6	14.8	15.0	15.2
13.4	13.6	13.8	14.0	14.2	14.4	14.6	14.8	15.0
13.2	13.4	13.6	13.8	14.0	14.2	14.4	14.6	14.8
13.0	13.2	13.4	13.6	13.8	14.0	14.2	14.4	14.6
12.8	13.0	13.2	13.4	13.6	13.8	14.0	14.2	14.4
12.6	12.8	13.0	13.2	13.4	13.6	13.8	14.0	14.2
12.4	12.6	12.8	13.0	13.2	13.4	13.6	13.8	14.0
12.2	12.4	12.6	12.8	13.0	13.2	13.4	13.6	13.8
12.0	12.2	12.4	12.6	12.8	13.0	13.2	13.4	13.6
11.8	12.0	12.2	12.4	12.6	12.8	13.0	13.2	13.4
11.6	11.8	12.0	12.2	12.4	12.6	12.8	13.0	13.2
11.4	11.6	11.8	12.0	12.2	12.4	12.6	12.8	13.0
11.2	11.4	11.6	11.8	12.0	12.2	12.4	12.6	12.8
11.0	11.2	11.4	11.6	11.8	12.0	12.2	12.4	12.6
10.8	11.0	11.2	11.4	11.6	11.8	12.0	12.2	12.4
10.7	10.9	11.1	11.3	11.5	11.7	11.9	12.1	12.3