Electrochemical Biosensors for Glucose Monitoring: Enzymatic and Non-Enzymatic Pathways Toward Next-Generation Biomedical Systems

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Abstract—Glucose monitoring is essential for managing diabetes and other metabolic disorders, driving advances in sensor technologies for integration into electronic and wearable devices. This paper presents a comparative analysis of enzymatic and nonenzymatic electrochemical biosensors. Enzymatic sensors rely on glucose oxidase or dehydrogenase and offer high specificity. They have been implemented in commercial self-monitoring and continuous glucose monitoring systems. However, limitations such as enzyme degradation and oxygen dependence have prompted interest in non-enzymatic alternatives. These fourth-generation sensors use metal-based catalysts, such as nickel and gold, to directly oxidize glucose. This in turn provides improved stability, miniaturization, and reagent-free operation. The paper examines mechanisms, materials, performance metrics, and integration considerations to highlight how design choices affect suitability for wearable biosensing platforms. The results indicate that no single architecture is universally optimal; sensor design must be tailored to application requirements. Future work should integrate electrochemical sensing with embedded electronics computational modeling to enable reliable, real-time monitoring. The analysis also demonstrates broader relevance across biomedical engineering, connecting principles of signal acquisition and noise reduction to neuroengineering, biophotonics, and medical imaging.

Index Terms—Electrochemical biosensors, glucose monitoring, enzymatic sensors, non-enzymatic sensors, glucose oxidase, nickel catalyst, wearable devices, continuous glucose monitoring (CGM), sensor integration, point-of-care diagnostics.

I. INTRODUCTION

HE global prevalence of diabetes and related metabolic disorders has underscored the critical need for continuous, accurate, and non-invasive glucose monitoring systems. Electrochemical biosensors have emerged as the dominant platform for this application due to their sensitivity, rapid response, and potential for miniaturization and integration into portable and wearable electronics [3]. Among these, enzymatic glucose sensors, pioneered in the 1960's, have served as the foundation for modern self-monitoring blood glucose (SMBG) meters and continuous glucose monitoring (CGM) systems. These sensors typically rely on enzymes such as glucose oxidase (GOx) or glucose dehydrogenase (GDH) to

catalyze specific reactions that generate electroactive species proportional to glucose concentration [2], [3].

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Despite their success, enzymatic sensors face key challenges. Enzymes are inherently sensitive to temperature, pH, and degradation over time. This necessitates frequent calibration and replacement [3]. Furthermore, early-generation enzymatic sensors exhibited dependence on oxygen as an electron acceptor. This limited reliability in low-oxygen conditions [2]. To address these issues, non-enzymatic glucose sensors have emerged as a compelling alternative. These fourthgeneration sensors use metal-based catalysts such as nickel, platinum, or copper to directly oxidize glucose at the electrode surface [1], [4]. This eliminates the need for biological components and external mediators.

While enzymatic sensors excel in selectivity and clinical maturity, non-enzymatic designs offer advantages in long-term stability, manufacturing scalability, and compatibility with flexible substrates. However, non-enzymatic sensors often require alkaline environments to function optimally and are prone to interference from other electroactive species. This trade-off between selectivity and stability presents a pivotal design consideration in modern biosensor development [1], [3].

This paper provides a comparative analysis of enzymatic and non-enzymatic electrochemical glucose sensors with a focus on their detection mechanisms, performance metrics, and potential for integration into next-generation electronic health monitoring systems. Drawing from recent literature, the discussion highlights how each approach meets the demands of modern sensing environments, and what innovations are required to overcome their respective limitations.

II. PRINCIPLES OF ELECTROCHEMICAL GLUCOSE SENSING

Enzymatic sensors utilize enzymes such as glucose oxidase (GOx) or glucose dehydrogenase (GDH) to catalyze glucose oxidation. The reaction typically involves either the reduction of oxygen (1st gen) or synthetic mediators (2nd gen), producing hydrogen peroxide or other electroactive species. These are measured at the electrode [2], [3].

Non-enzymatic sensors eliminate biological recognition

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elements and instead rely on direct electro-oxidation of glucose on catalytic materials such as nickel, platinum, copper, or metal oxides. These reactions often depend on surface redox couples (e.g., Ni(II)/Ni(III)) and are sensitive to pH and potential window. However, they avoid issues like enzyme degradation and oxygen dependence [1].

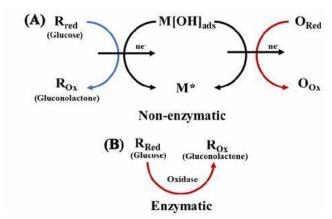


Fig. 1. Enzymatic vs. Non-Enzymatic Glucose Oxidation

We can analyze how glucose oxidation generates a measurable current in both enzymatic and non-enzymatic sensors through Faraday's Law of Electrolysis, where I = Faradaic current (A), n = Number of electrons transferred per glucose molecule, F = Faraday constant (\sim 96,485 C/mol), A = Electrode surface area (cm²), and J = Flux of electroactive species to the electrode (mol·cm²-·s²-¹).

$$I = nFAJ$$

Eq. 1. Faraday's Law of Electrolysis

This reinforces the idea that electrode design and surface area directly influence signal strength, which matters for electronics interface and signal conditioning.

III. SENSOR GENERATIONS AND DETECTION MECHANISMS

Glucose biosensors are often categorized by **generational design evolution**, particularly among enzymatic devices:

- 1. First-generation: $GOx + O_2 \rightarrow H_2O_2$
- 2. **Second-generation**: GOx + synthetic mediator
- Third-generation: Direct electron transfer from enzyme to electrode
- 4. **Fourth-generation**: Non-enzymatic, catalyst-based glucose oxidation (no biological elements) [2], [3].

Each generation improves stability, selectivity, and ease of integration. However, only the fourth-generation sensors offer the promise of a fully reagent-less, long-lifetime platform. This is ideal for implantable or wearable electronics [1], [4].

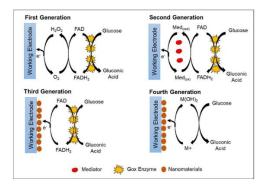


Fig. 2. Comparison of Four Generation Types [2]

IV. MATERIALS AND SENSOR ARCHITECTURES

Sensor performance is intimately linked to the materials and architecture of the sensing electrode. Enzymatic sensors typically use GOx immobilized on carbon or metal electrodes, with layered structures including membranes, mediators, and reference electrodes. These designs dominate commercial SMBG and CGM systems [2], [3].

Non-enzymatic sensors use advanced materials including Ni/NiO, Pt, Cu, and hybrid nanostructures. Nickel-based sensors in particular exploit the reversible formation of NiOOH, which oxidizes glucose. Enhancing sensitivity requires high-surface-area structures like nanowires, nanoporous foams, or bimetallic alloys. These not only improve electron transfer rates but also help mitigate surface fouling [1], [4].

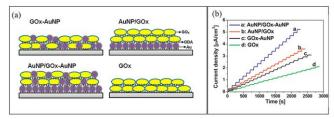


Fig. 3. Structural Designs of Electrodes and Responses [4]

V. PERFORMANCE METRICS AND INTERFERENCE

A glucose sensor's effectiveness is judged by its sensitivity, limit of detection (LOD), linear range, response time, selectivity, and stability.

We can use Michaelis Mention Kinetics for current response saturation in enzymatic sensors, where I = Measured current, Imax = Maximum current when enzyme is saturated, S = Glucose concentration, and Km = Michaelis constant (substrate concentration at half-max response). It allows us to measure nonlinear sensor output, which has to be linearized or calibrated in electronics/firmware for SMBG/CGM systems.

$$I = rac{I_{ ext{max}}[S]}{K_M + [S]}$$

Eq. 2. Michaelis Mention Kinetics

Equation 2 shares a structure with a classic saturating nonlinearity, where the sensor output (current) increases rapidly with glucose concentration but flattens as the enzyme sites become saturated. To evaluate the sensitivity of the sensor to glucose concentration, we differentiate Equation 2:

$$rac{dI}{d[S]} = rac{I_{
m max} K_M}{(K_M + [S])^2}$$

This expression defines the instantaneous sensitivity of the current with respect to glucose. In the limit where $[S] \ll Km$, the equation simplifies to:

$$rac{dI}{d[S]}pproxrac{I_{
m max}}{K_M}$$

indicating an approximately linear region where sensitivity is approximately constant and highest. Conversely, as $[S] \gg Km$, the sensor saturates and $dI/d[S] \rightarrow 0$, which diminishes resolution. This is a critical metric for design of analog-to-digital conversion and calibration in CGM electronics.

This nonlinear transfer function must be linearized or confined to its linear regime to ensure accurate readout. For glucose sensors, operating in this zone ensures that small changes in glucose concentration produce distinguishable changes in current. For reference, glucose oxidase-based biosensors typically exhibit Km values in the range of 1–5 mM [2], while the physiological glucose concentration in human blood ranges from approximately 3-10 mM. This overlap emphasizes the importance of carefully selecting the linear operating zone of the sensor. Calibrating the system to operate within the region where $[S] \approx Km$ ensures meaningful current variation and improves resolution within the range relevant to clinical monitoring. This is especially important given the finite bit resolution of ADCs in portable systems (often 10–12 bits). Understanding this nonlinear relationship enables engineers to map glucose concentration ranges onto the ADC input range efficiently, which minimizes quantization error while avoiding signal clipping or dead zones.

In real CGM systems, one of the major performance limitations of this kinetic behavior is drift in Imax over time due to enzyme degradation. This alters the sensor's gain and compresses the effective dynamic range, requiring recalibration or predictive filtering algorithms in the analog front-end. Some systems compensate for this using moving-average smoothing or polynomial fitting in the linear region, but these introduce their own latency and reduce real-time accuracy [2], [3].

A common implementation practice is to linearize the sensor's current response via piecewise approximations or log-transforms, especially for mapping to digital output formats like mg/dL in CGMs. Several commercial biosensor design guides

(e.g., Texas Instruments Blood Glucose Meter with the MSP430 MCU Smart Analog Combo) model this using a two-region response: an exponential rise below Km and a saturation-limited plateau above [8]. The TIA converts the current generated by the electrochemical reaction on the test strip into a voltage signal. This voltage is then processed by the analog-to-digital converter (ADC) within the microcontroller. Since the electrochemical reaction is temperature-dependent, ambient temperature measurements are essential for accurate glucose readings.

Enzymatic sensors offer high specificity due to the enzymesubstrate interaction but are limited by enzyme lifetime and environmental sensitivity. Non-enzymatic sensors exhibit higher stability and longer shelf-life but must contend with interference from electroactive species like uric acid or ascorbic acid. This is especially relevant since they often operate at higher potentials [1], [5].

Nickel-based systems perform exceptionally in alkaline media. They can achieve sensitivities $> 1000 \,\mu\text{A mM}^{-1}\,\text{cm}^{-2}$, but performance in neutral pH or whole blood remains challenging [4].

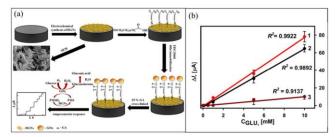


Fig. 4. GOx immobilization strategies on dendritic Au nanostructures with corresponding calibration plots [4]

Figure 4 highlights how different enzyme immobilization techniques directly impact the sensitivity and linearity of the glucose sensor. From a systems standpoint, these variations inform how interface engineering, specifically the arrangement of biomolecules and nanostructures, affects electron transfer and resulting current. For electronic integration, selecting the optimal configuration ensures consistent signal output across physiological glucose ranges. This reduces the need for complex calibration algorithms in the processing circuit.

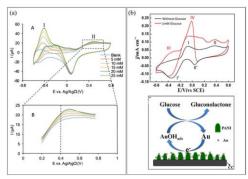


Fig. 5. CV of nanoporous Pt/SPCE-polyimide electrode with

and without glucose in PBS [4]

Cyclic voltammetry (CV) is an electrochemical technique where a linear voltage sweep is applied to the electrode, and the resulting current is measured. Peaks in the CV curve indicate redox reactions, allowing the identification of oxidation potentials for glucose and other analytes. This is useful for selecting appropriate bias voltages in the analog front-end. The voltammogram demonstrates a clear current increase in response to rising glucose concentrations, which validates the electrode's electrocatalytic activity in a physiologically relevant (neutral pH) environment. This is significant from a hardware integration perspective because it suggests that non-enzymatic sensors can be adapted for direct use in wearable or implantable systems, and eliminate external electrolytes and complex fluid handling modules. The low oxidation potential also reduces the load on analog front-end circuitry.

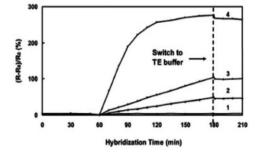
VI. INTEGRATION INTO ELECTRONIC SYSTEMS

Modern glucose biosensors must interface with embedded electronics to deliver real-time, reliable data. Enzymatic SMBG and CGM systems use potentiostats, analog signal conditioners, and digital processors to convert electrochemical signals into readable glucose values [3].

Non-enzymatic sensors, particularly those built on flexible substrates or in wearable formats (e.g., patches, tattoos), benefit from simpler architectures (no reagents or membranes) but often require compensation circuitry for pH drift, interference, or signal instability.

System-level integration involves not only sensor readout but also power management, data transmission, and biocompatible packaging. This is especially relevant for subcutaneous or sweat-based sensors.

Figures 6 and 7 both explore alternative electronic sensing modalities. While Fig. 6 illustrates a nanoscale field-effect architecture, Fig. 7 shows a potentiometric design based on membrane-bound DNA hybridization. Though based on different mechanisms, both highlight how sensor interfaces influence electrical readout, a critical concern for glucose monitoring system integration.



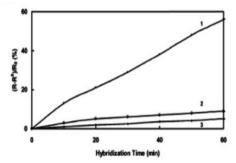


Fig. 6. Silicon Nanowire FET Biosensor Response [2]

Figure 6 shows how nanoscale devices can transduce biomolecular interactions into electrical resistance changes. This provides a label-free and highly sensitive platform. For glucose sensing systems, this kind of architecture supports miniaturization and low-power operation, which is critical for embedded or continuous monitoring devices [6]. The integration with CMOS-compatible platforms suggests future compatibility with standard microelectronic readout systems.

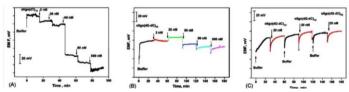


Fig. 7. Potentiometric Sensor at Solution Interface [2]

This sensor setup emphasizes how spatial configuration and molecular orientation at the sensor-electrolyte boundary influence signal output. From a systems design viewpoint, it underscores the importance of interface stability and reproducibility, which are essential for real-time monitoring applications. The observed regeneration and consistent signal response after repeated exposure indicate potential for long-term deployment with minimal drift, which can reduce the maintenance needs in electronic health platforms [7].

VI. Broader Connections Across Biomedical Engineering

The design trade-offs identified in glucose biosensors are not isolated to this application, and reflect broader themes across multiple branches of biomedical engineering. For example, biophotonics explores light-tissue interactions for sensing and imaging. Techniques such as near-infrared spectroscopy (NIRS) and optical coherence tomography (OCT) also confront issues of sensitivity and signal-to-noise optimization that parallel the challenges of electrochemical readout. Both require precise modeling of physical interactions to produce clinically meaningful signals.

Similarly, neuroengineering shares common ground with biosensor development through its reliance on electrode interfaces for recording and stimulation. Materials research on impedance reduction and biocompatibility in neural probes directly overlaps with strategies used in optimizing electrochemical glucose sensors. In both cases, system

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longevity and reliable signal acquisition are central design goals that demand advances in materials science and embedded electronics.

Medical imaging and diagnostic devices further illustrate this interconnectedness through the implementation of critical electrochemical and optical modalities. Biomedical devices must convert complex biological signals into quantifiable data that can be integrated into clinical decision-making. Lessons learned from calibrating glucose sensors, such as linearization of nonlinear transfer functions and compensation for drift, carry direct relevance to medical devices in the field today. We can consider tools such as imaging detectors, electrophysiological amplifiers, and wearable health monitors.

These connections emphasize that the engineering considerations in glucose biosensors are representative of challenges across biomedical engineering. Developing end-to-end platforms requires a shared foundation in disciplines such as physics-based modeling and signal acquisition. Expertise in one area provides a transferable technical toolkit that applies equally to other branches of biomedical engineering.

VII. CONCLUSION

Electrochemical biosensors remain one of the most impactful technologies in biomedical engineering, yet their future depends on overcoming trade-offs between stability and selectivity. Enzymatic biosensors deliver high specificity but are limited by enzyme degradation, oxygen dependence, and calibration requirements. Non-enzymatic biosensors, particularly those based on nickel and hybrid nanomaterials, offer promising improvements in long-term stability and manufacturability but must address interference and reduced selectivity under physiological conditions.

The comparative analysis presented here shows that sensor choice is application-dependent: enzymatic platforms remain best suited for mature clinical devices requiring high specificity, while non-enzymatic systems hold potential for next-generation wearables, implantables, and reagent-free monitoring. Future progress will rely on hybrid approaches that combine catalytic robustness with real-time computational calibration and low-power embedded hardware.

Beyond glucose monitoring, the design principles of electrode architecture, nonlinear transfer functions, and system-level signal processing apply broadly across biomedical engineering. These include neural interface design, where electrode stability dictates long-term recording fidelity; biophotonics, where sensor miniaturization and noise suppression are equally critical; and medical imaging, where signal acquisition and hardware integration define resolution and diagnostic accuracy. Situating glucose biosensors within this broader context emphasizes their role not only as clinical tools, but also as platforms for advancing core methodologies in biomedical engineering research.

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