

Università degli studi di Bergamo  
Scuola di Ingegneria (Dalmine)  
CCS Ingegneria Edile

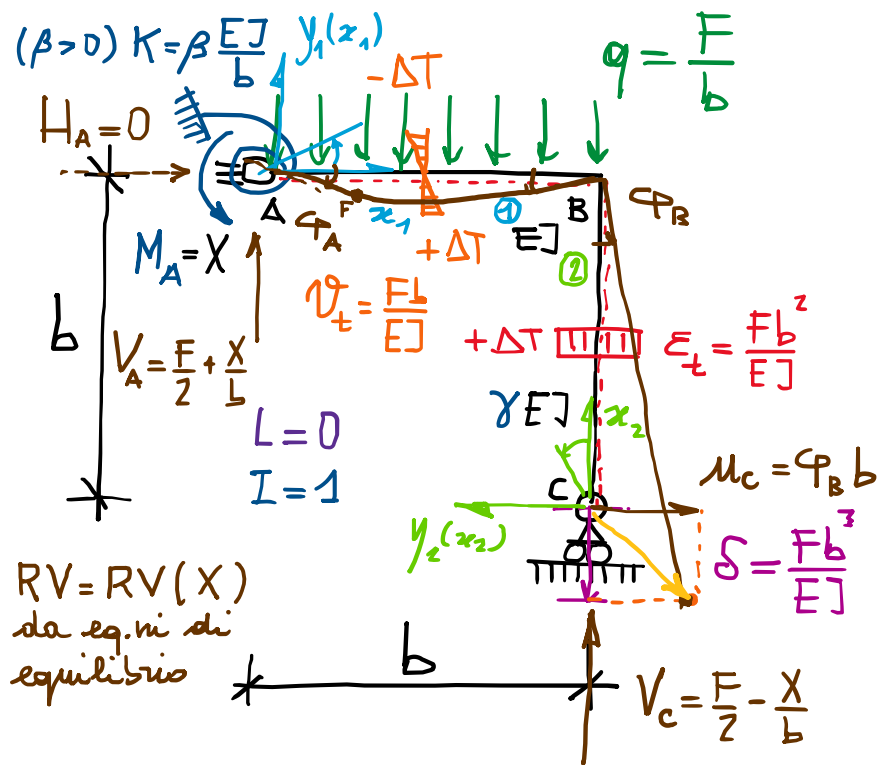
LM-24 Ingegneria delle Costruzioni Edili

Complementi di Scienza delle Costruzioni  
(ICAR/08 - SdC; 6 CFU)

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LEZIONE 09

# Soluzione tramite Metodo della Linea Elastica (LE)



Curvatura totale del generico campo i-esimo: (n campi di integrazione)

$$y_i''(x_i) \approx \chi_i(x_i) = \underbrace{\chi_{ie}(x_i)}_{\frac{M_i(x_i)}{EJ_i}} + \underbrace{\chi_{it}(x_i)}_{\frac{\vartheta_{it}(x_i)}{EJ_i}}$$

$|y_i'| \ll 1$

$\frac{M_i(x_i)}{EJ_i}$  Legge di B-E-N  
 $\frac{\vartheta_{it}(x_i)}{EJ_i}$  curvatura termica impressa

$$EJ_i(x_i) y_i''(x_i) = M_i(x_i) + EJ_i(x_i) \vartheta_{it}(x_i)$$

$$EJ \cdot y_i''(x_i) = \frac{M_i(x_i)}{\chi_i(x_i)} + EJ \cdot \vartheta_t(x_i)$$

eq. differenziale del 2° ordine

Tratto 1:

$$\begin{aligned}
 EJ y_1''(x_1) &= M_1(x_1) + EJ \frac{Fb}{EJ} = -\frac{F}{b} \frac{x_1^2}{2} + \left(\frac{F}{2} + \frac{X}{b}\right) x_1 - X + Fb \\
 EJ y_1'(x_1) &= -\frac{F}{b} \frac{x_1^3}{6} + \left(\frac{F}{2} + \frac{X}{b}\right) \frac{x_1^2}{2} + (Fb - X) x_1 + A_1 \\
 EJ y_1(x_1) &= -\frac{F}{b} \frac{x_1^4}{24} + \left(\frac{F}{2} + \frac{X}{b}\right) \frac{x_1^3}{6} + (Fb - X) \frac{x_1^2}{2} + \underbrace{A_1 x_1 + A_2}_{\text{comp. moto rigido rototranslatorio}}
 \end{aligned}$$

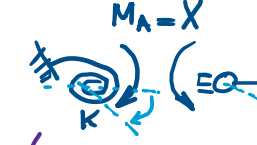
Tratto 2:

$$\begin{aligned}
 EJ y_2''(x_2) &= 0 + EJ 0 = 0 \\
 EJ y_2'(x_2) &= B_1 \\
 EJ y_2(x_2) &= \frac{B_1 x_2}{2} + B_2
 \end{aligned}$$

Incognite  $2n + I = 5$

$A_1, A_2, B_1, B_2; X$   
 costanti di inc. integrazione ipert.

Scrittura e imposizione delle condizioni al contorno (c.c.) [in numero pari a  $n_{cc} = 2n + 1 = 5$ ]

- $y_1(0) = 0$  cerniera in A
  - $y_1'(0) = -\frac{X}{K}$  molla elastica rotazionale in A   $\phi = \frac{X}{K}$  opposta a  $M_A = X$  sull'asta
  - $y_1(b) = -\delta + \varepsilon_t b = 0$  carrello in C con cedimento  $\delta + (\Delta l_{BC}^t = \varepsilon_t b)$
  - $y_1'(b) = y_2'(b)$  continuit  alla rotazione in B  $\rightarrow \phi_B$
  - $y_2(b) = 0$  cerniera in A + invest. assiale di AB ( $EA_{AB} \rightarrow \infty$ )
- spost. assoluti  
 $\downarrow$   
B   nodo fisso ( $u_B = v_B = 0$ )

$EJ y_1(0) = 0 \Rightarrow A_2 = 0$

$EJ y_1'(0) = A_1 = -\frac{X}{K} EJ = -\frac{X}{\beta \frac{EJ}{b}} = -\frac{b}{\beta} X \Rightarrow A_1 = A_1(X) = -\frac{b}{\beta} X \rightarrow A_1 = -\frac{b}{\beta} \frac{13}{8} \frac{Fb}{3+\beta} = -\frac{13}{8} \frac{1}{3+\beta} Fb^2 = A_1$

$EJ y_1(b) = -\frac{F}{b} \frac{b^4}{24} + \left(\frac{F}{2} + \frac{X}{b}\right) \frac{b^3}{6} + (Fb - X) \frac{b^2}{2} + A_1 b + A_2 = 0 \Rightarrow \left(\frac{1}{6} - \frac{3}{2} \frac{1}{\beta} - \frac{1}{\beta}\right) X b^2 = \left(\frac{1}{24} - \frac{1}{12} - \frac{1}{2}\right) Fb^3$

$EJ y_1'(b) = -\frac{F}{b} \frac{b^3}{6} + \left(\frac{F}{2} + \frac{X}{b}\right) \frac{b^2}{2} + (Fb - X)b + A_1 = EJ y_2'(b) = B_1 = \left(-\frac{1}{3} - \frac{1}{\beta}\right) X = \frac{1-2-12}{24} Fb = -\frac{13}{24} Fb$

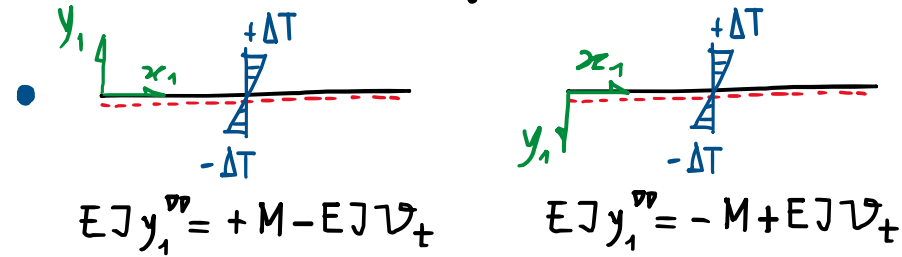
$EJ y_2(b) = B_1 b + B_2 = 0 \Rightarrow B_2 = -B_1 b \rightarrow u_c = \phi_B b$   
 $\phi_B \geq |\phi_A|$   
 $\phi_B = \frac{B_1}{EJ} = \frac{13}{8} \frac{1+\beta/6}{3+\beta} \frac{Fb^2}{EJ}$

$B_2 = -\frac{13}{48} \frac{6+\beta}{3+\beta} Fb^3$   $B_1 = \frac{13}{48} \frac{6+\beta}{3+\beta} Fb^2$

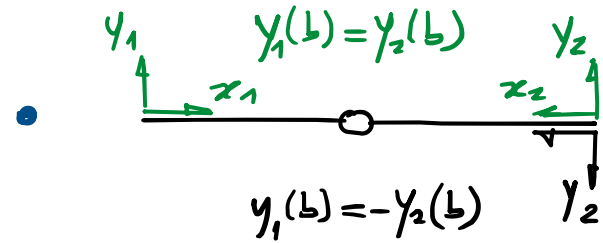
$X = \frac{13}{8} \frac{\beta}{3+\beta} Fb$   $\beta \rightarrow 0, X \rightarrow 0$   
 $\beta \rightarrow \infty, X \rightarrow \frac{13}{24} Fb$

- LE finali, sost.  $A_1, A_2, B_1, B_2$  e  $X$  e tracciamento della deformata qualitativa.

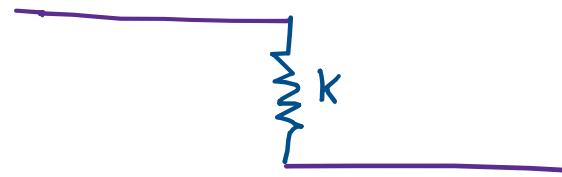
- Attenzione ai segni su LE e c.c.!



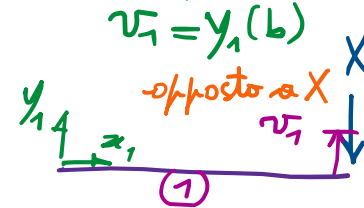
curvature elastiche e termiche



molla relativa  
elongazionale



letto nel riferim. locale

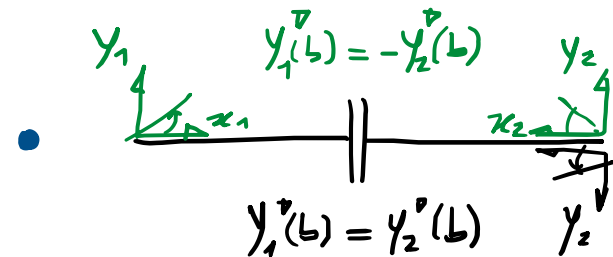
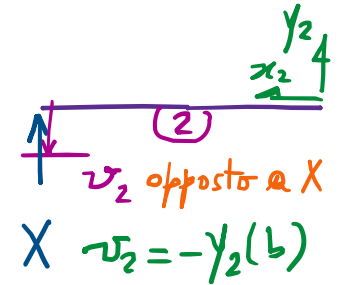


$$y_1(l) - y_2(l) = \frac{X}{K}$$

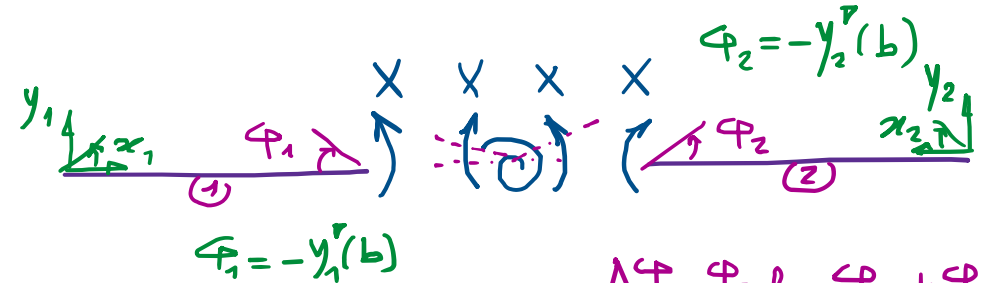
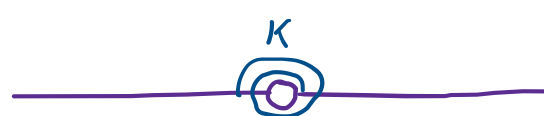


spost. relativo

$$\Delta l = v_{rel} = v_1 + v_2 = \frac{X}{K} \text{ legge di Hooke}$$



rotazionale



$$-y_1'(l) - y_2'(l) = \frac{X}{K}$$

$$\Delta \varphi = \varphi_{rel} = \varphi_1 + \varphi_2 = \frac{X}{K}$$