

Digital Transmission Principles

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Digital Transmission

- Binary Transmission as a reference
- Additive white Gaussian noise channel
- Binary and ternary eye diagrams
- Eb/No and System SNR
- BER
- Multi-level signalling and choice of modulation

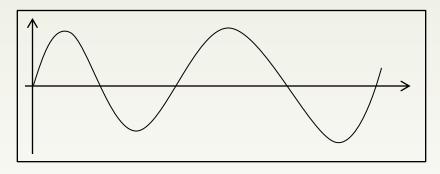


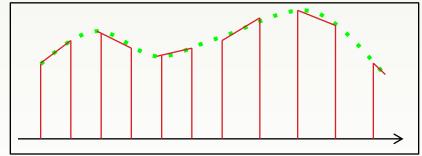
Signal types

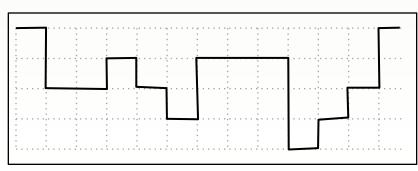
- Random Deterministic
- Discrete Time Continuous Time
- Discrete Amplitude Continuous Amplitude
- Lowpass, Bandpass, Highpass
- Periodic or non Periodic



Discrete-Continuous





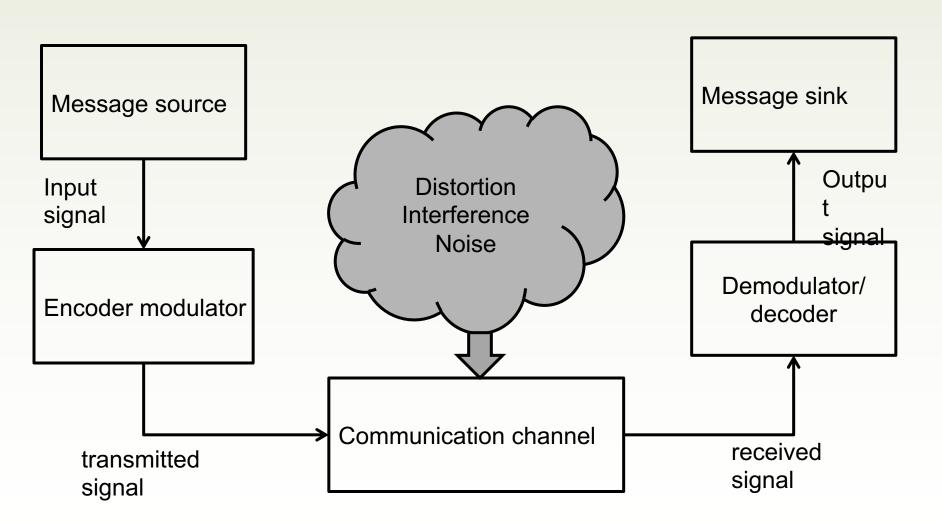


 Continuous time and amplitude

- Discrete time continuous amplitude – PAM signal
- Discrete time and amplitude, Multilevel signal.



Digital line system



Claude Shannon

- Shannon's Theorem predicts reliable digital communication in the presence of noise
 - "Given a discrete, memoryless channel with capacity C, and a source with a positive rate R (R<C), there exist a code such that the output of the source can be transmitted over the channel with an arbitrarily small probability of error."

B is the channel bandwidth in Hz and S/N is the signal to noise ratio

$$C_c = B \log_2 \left(1 + \frac{S}{N} \right)$$

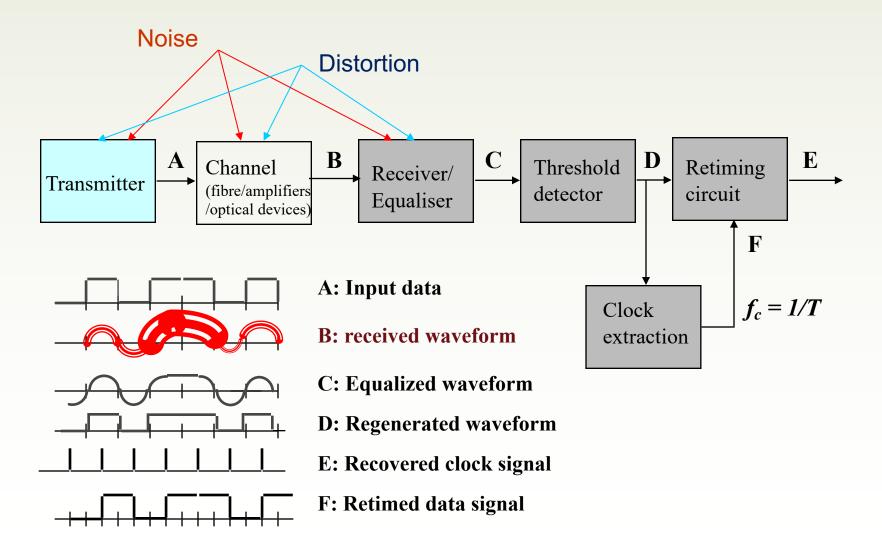


For a "good" digital system;

- We aim to transmit a "clean" signal and receive an "identical" one
- "Identical" means;-
 - 1- no added errors, all 1s received as 1s and all 0s received as 0s; <u>AND</u>
 - 2- Received data has the same timing as transmitted data



Binary transmission system





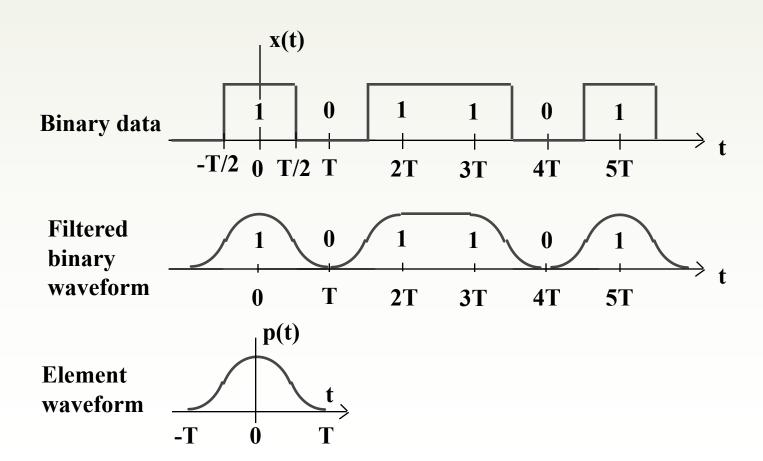
Effects of noise and Distortion

- Errors are introduced due to:
 - Noise on signal
 - Timing noise and jitter
 - Inter-Symbol-Interference (ISI)

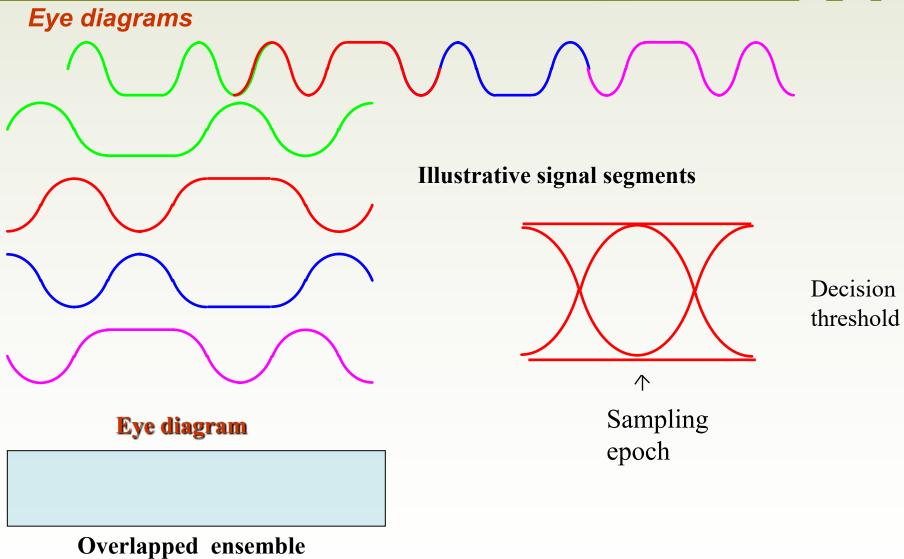
- Errors can be assessed by:
 - Considering the eye diagram
 - Measurement of Bit Error Rate (BER) or Pe



Binary signal waveforms



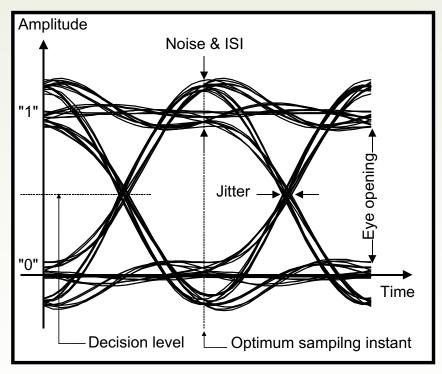




of possible waveforms



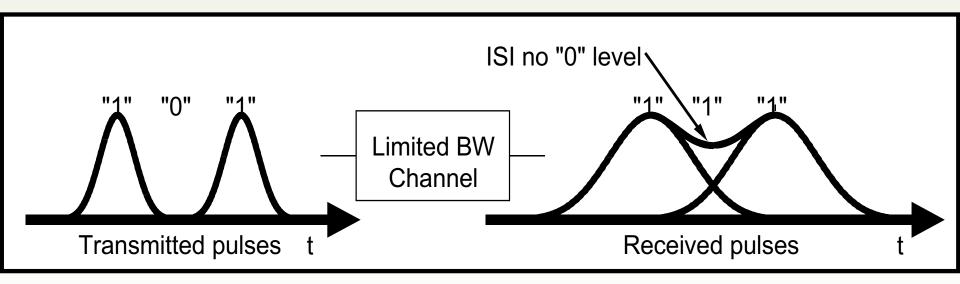
A more realistic eye...



- The eye diagram is a powerful diagnostic tool
 - Noise
 - Jitter
 - Telegraph Distortion
 - ISI
 - Patterning effects
 - Bit errors
- Normally displayed on a scope at the receiver



Concept of ISI in Binary signals

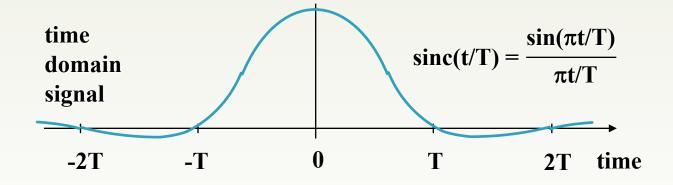


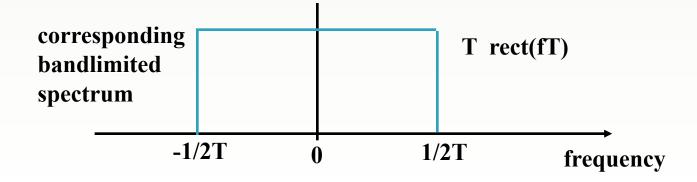
- •The signals can be "designed" so as to have no ISI
- •This is done at the signal shaping/equalisation stage in the receiver
- •Requires knowledge of received signal shape

(i.e transmitter, channel and receiver behaviour)

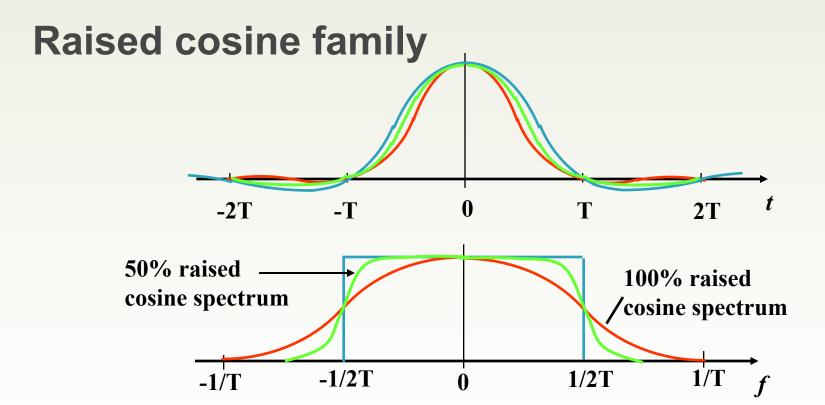


A zero isi signal





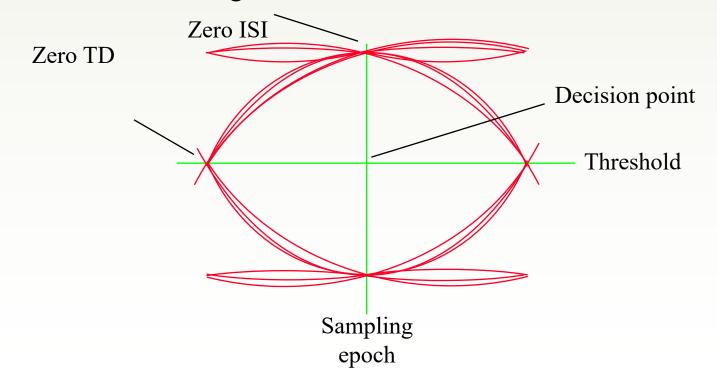






Eye diagram: 100% raised cosine signal

- The 100% raised cosine spectrum corresponds to the minimum bandwidth signal satisfying Nyquist Criteria
- This results in signals with zero ISI and zero TD





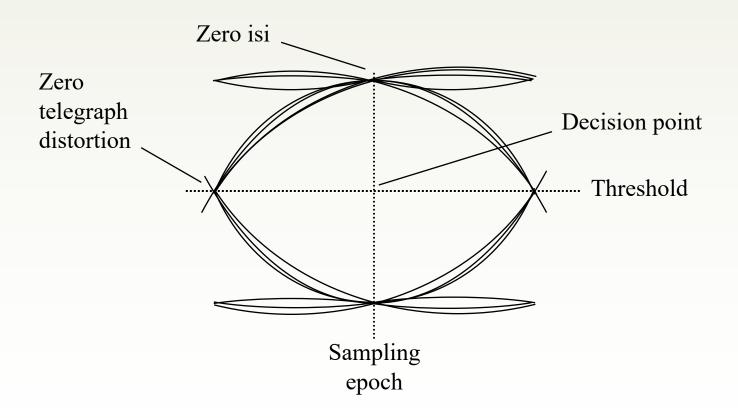
Raised Cosine Spectrum

$$X_r(f) = \begin{cases} T & 0 \le |f| \le \frac{1-\beta}{2T} \\ \frac{T}{2} \left\{ 1 + \cos\left[\frac{\pi T}{\beta} \left(|f| - \frac{1-\beta}{2T}\right)\right] \right\} & \frac{1-\beta}{2T} < |f| \le \frac{1+\beta}{2T} \\ 0 & f > \frac{1+\beta}{2T} \end{cases}$$

- Where β is the roll off factor 0< β<1
- Excess bandwidth (that above Nyquist) is usually referred to as a percentage of Nyquist
 - $-\beta$ =1/2 excess Bandwidth = 50%
 - $-\beta$ =1 excess Bandwidth = 100%

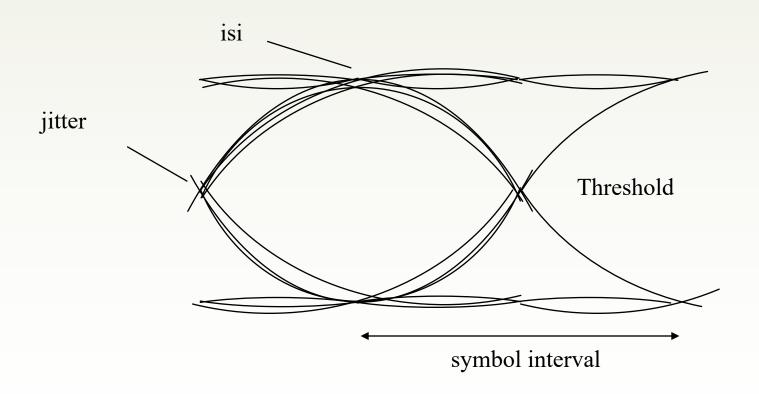


Eye diagram: 1



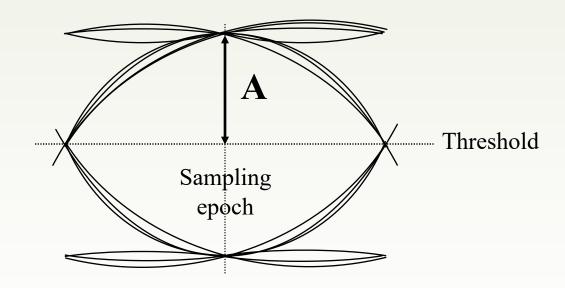


Eye diagram: 2





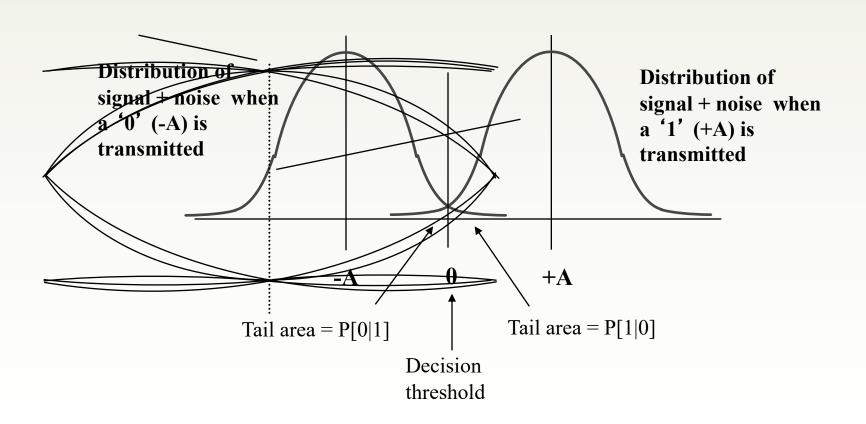
Signal to Noise Ratio (SNR)



- SNR defined in terms of half eye opening and rms noise voltage, σ
- SNR= A/σ
- Adjusted for multi-level systems for No. levels

https://en.wikipedia.org/wiki/Extinction ratio

Bit error rate (BER)



UCL

Noise and errors

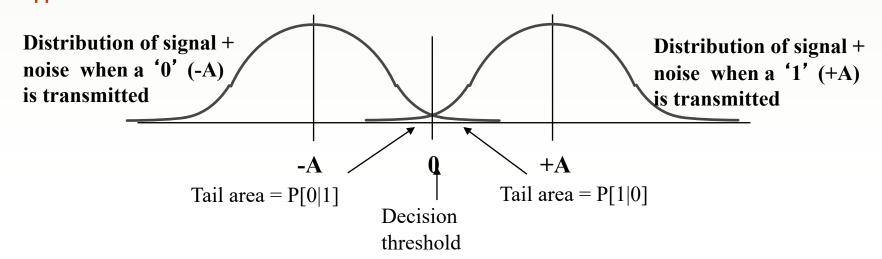
$$P_e = P(0)P[1|0] + P(1)P[0|1]$$

with $P(0) = P(1) = \frac{1}{2}$ and
 $P[1|0] = P[0|1]$ then with $\alpha = A/\sigma$
 $P[1|0] = P[1|0] = P[0|1] \approx \frac{1}{\sqrt{2\pi}\alpha}e^{-\frac{\alpha^2}{2}}$

Here α is the SNR and δ is the rms of noise

This applies for Gaussian noise and zero ISI

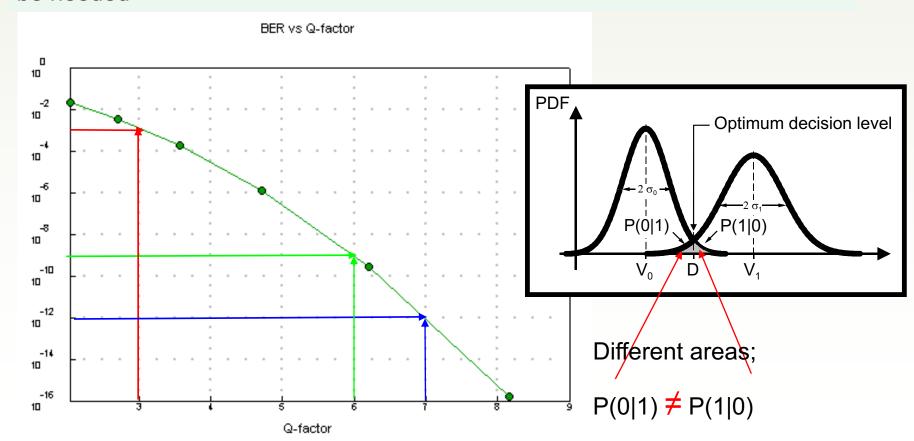
- •Probability of error (Pe) or Bit Error Rate (BER) taken as ratio of number of bits received in error to the total number of bits, in a given transmission period.
- •The primary measure of performance of a digital system
- •For optical systems BER is < 10⁻⁹,
- •This can be achieved for SNR value>6





Considerations for designers

- 1- The error rate deteriorates rapidly with SNR degradation (in the figure SNR is Q-Factor)
- 2- Noise may be different on the 1s and 0s. Different analysis and design will be needed



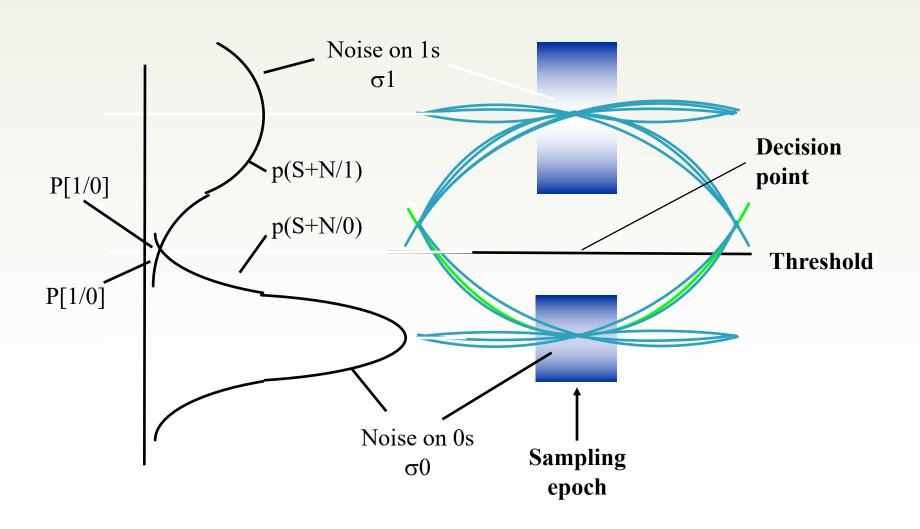


Q-based system design

- The operational system requirement is for a sufficiently low error rate at the end the system - which calls for a sufficiently large Q value at that point
- One can analyse a possible system arrangement and determine the signal and noise levels and hence the SNR
- From the SNR the corresponding Q can be found which allows the BER to be determined
- In design it is often convenient to work from a specified Q to the SNR
- Measuring Q can be effected by off-setting the threshold, necessary because systems are designed to operate error-free
- BER is measured and plotted versus threshold and then extrapolated to the region of practical interest



Noise on the Signal



Sources of Noise - 1

Thermal Noise

 Due to the random motion of electrons that is always present at a finite temperature

$$\sigma_{V_{thermal}}^2 = \frac{4 \ k \ T \ B_e}{R}$$

- R = Resistance (often 50Ω)
- Temperature T
- k_B = Boltzmann's Constant = 1.38x10⁻²³ J/ $^{\circ}$ K
- B_e= Electrical Bandwidth
- Signal Independent Noise

Sources of Noise - 2

- Shot Noise
 - Representation of the random nature of the arrival of photons

$$\sigma_{V_{shot}}^2 = 2 e I B_e$$

- e = Charge on an electron = 1.6x10⁻¹⁹ C
- B_e= Electrical Bandwidth
- \hat{I} = Average photocurrent generated = $\Re P_{rx}/2$
- \Re = Responsivity
- P_{rx} =Power at the Receiver
- Signal Dependent Noise

Sources of Noise - 3

- Signal Spontaneous Beat Noise
 - Due to ASE noise from an optical amplifier beating with the signal

$$\sigma_{V_{sig-spon}}^2 = 4 \Re G P_{opt} n_{sp} h f_c (G-1) B_e$$

 f_c = optical frequency

 $h = Planck's Constant = 6.63x10^{-34} J/Hz$

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G = Amplifier Gain
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- B_e= Electrical Bandwidth

- P = Power entering amplifier

- \mathcal{R} = Responsivity
- n_{sp} = spontaneous emission factor
- Signal Dependent Noise



Signal Dependent Noise

- Signal-spontaneous noise is signal dependent
- Hence EDFA cascades and optical preamplifier based receivers exhibit substantial variation in noise level between 1s (light present) and 0s (light absent), which we then indicate as σ1, σ0
- It is appropriate to position the decision threshold somewhat below half way in the eye in order to minimise the total error rate, corresponding to errors occurring approximately equally for 1s and 0s: P[0/1]=P[1/0]



Defining Q:

The root mean square value of a quantity is the square root of the mean value of the squared values of the quantity taken over an interval.

systems without amplifiers

- Additive noise, independent of signal level
- Bit error rate (BER) corresponds to 'Gaussian Tail' or complementary error function, erfc:
- BER = erfc(Q) with Q the ratio of signal s to rms noise, i.e. Q=s/σ
- $Q(dB)=20 log_{10}Q$
- BER of 10⁻⁹ corresponds to Q=6
- System operating margin may be expressed as an electrical Q margin: M_{elec}(dB)=20log₁₀(Q/6)

Decision Threshold

- The decision threshold is (nominally) set such that P[1/0] = P[0/1]
- If noise is equal on 1's and 0's then this will be in the middle – signal independent noise
- For signal dependent noise With perfect extinction for 0s and normalised decision threshold of this corresponds to equal 'margins' for 0s and 1s of D and (1-D) relative to the respective $\frac{1}{100}$ noise values $\frac{1}{100}$, such that:

$$\frac{D}{\sigma_0} = \frac{1 - D}{\sigma_1} \implies D = \frac{\sigma_0}{\sigma_0 + \sigma_1}$$



Defining Q:

systems with amplifiers

- Signal dependent noise requires a definition of Q which accommodates optimum threshold <0.5
- Peak signal level is 2s
- Threshold is optimally placed at $\sigma_0/(\sigma_0+\sigma_1)$

$$Q = \frac{2s}{\sigma_0 + \sigma_1}$$
; $BER_{opt} = erfc(Q)$



Q and SNR

- It is convenient to define a signal to noise ratio in terms of the mean number of signal photons per second, s, and the mean spontaneous noise in photons per second at any point in a system: SNR(dB)=10log(s/n)
- Note that optical dB calls for a factor of 10 multiplier while electrical Q uses a factor of 20
- In the beat noise limit SNR and Q are related by:

$$Q=rac{2~SNR}{1+\sqrt{1+4~SNR}}\sqrt{rac{\Delta v}{B_e}}$$
 , Δv being the optical bandwidth

$$SNR = Q \left(1 + Q \sqrt{\frac{B_e}{\Delta v}} \right) \sqrt{\frac{B_e}{\Delta v}}$$



Types of Coding

- Source Coding
 - Method of encoding the raw data
- Error Detection Coding
 - Detection of errors in the data sequence
- Error Correction Coding
 - Detection and Correction of Errors
- Line Coding
 - Formatting of the transmitted data stream to benefit transmission



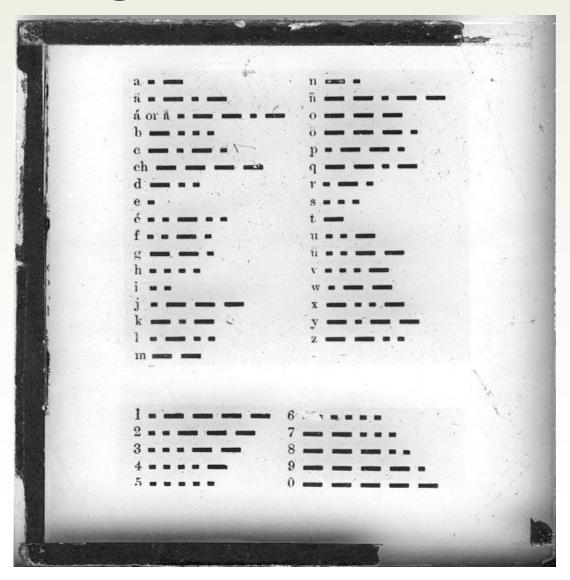
Source Coding

- We have seen already how the digitised voice is encoded against a code word for each level.
- ASCII is a common source coding scheme for transmitting text.

!	0100001	Α	1000001
1	0101111	Z	1011010
0	0110000	а	1100001
9	0111001	z	1111010
:	0111010	~	1111110
@	1000000		



Source Coding is not new





Error Detection/Correction

- We require a reliable channel, i.e. BER > x
- What can we do if this is not possible?
 - 1. Increase the power
 - 2. Diversity in space/frequency or time
 - 3. Full Duplex (echo information)
 - 4. Automatic repeat Request (ARQ)
 - Forward Error Correction

All of these introduce a certain amount of redundancy



prediction/error correction is also not new...

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According to a rscheearch at Cmabrigde Uinervtisy, it deosn't mttaer in waht oredr the Itteers in a wrod are, the olny iprmoatnt tihng is taht the frist and Isat Itteer be in the rghit pclae. The rset can be a taotl mses and you can sitll raed it wouthit porbelm. Tihs is bcuseae the huamn mnid deos not raed ervey Iteter by istlef, but the wrod as a wlohe.

Amzanig huh?



ARQ

- Three common ARQ techniques exist
 - Stop-and-wait: The sender(Tx) sends a frame and then waits for acknowledgement for the receiver (Rx).
 - Go-back-n: Sender sends frames in a sequence with acknowledgement from Rx. On error Rx discards current and further frames and notifies Tx of frame required. Tx starts again from this point
 - Selective repeat: Tx only repeats those frames for which negative acknowledgements are received.

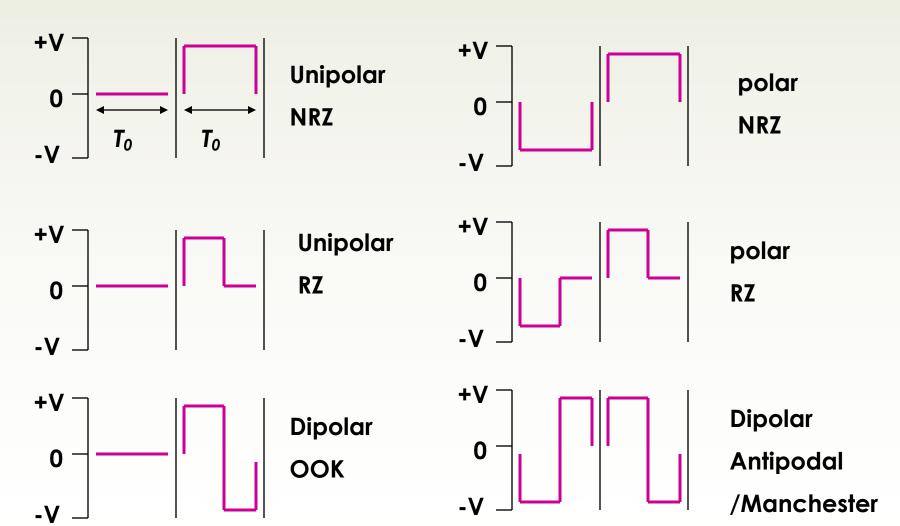


Line Coding

- We have considered so far only unipolar pulses to represent the binary bits in our system
- However, other pulse types can be used to represent these bits
- This is line coding, use for one or more of the following reasons
 - Presence or absence of a DC level
 - To shape the power spectral density
 - Bandwidth
 - Noise immunity
 - Ease of clock recovery

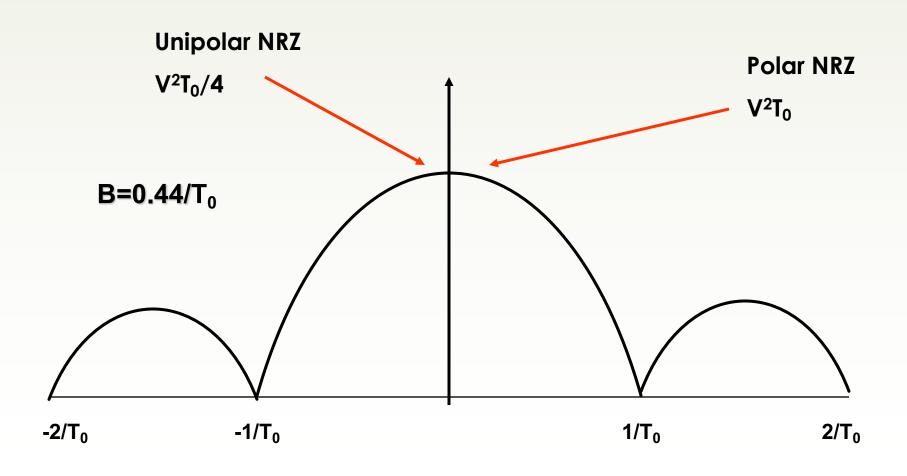


Example Line Codes



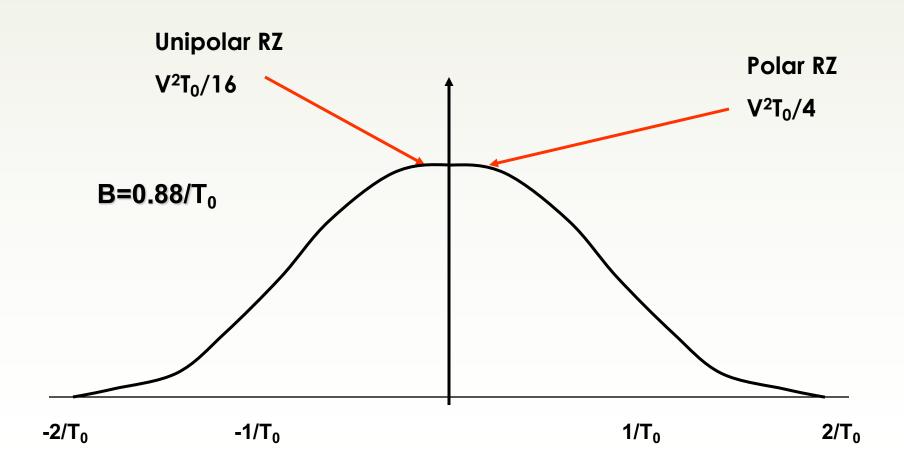


Line Code Spectrum



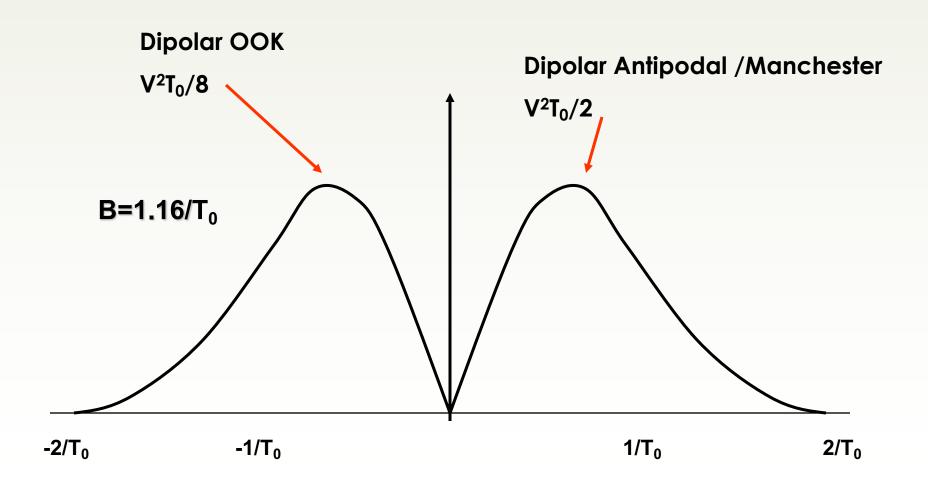


Line Code Spectrum





Line Code Spectrum





Example Line Codes

Coding Type	Comment
Unipolar NRZ	Usual format, DC term
Unipolar RZ	Simple timing extraction, DC term
Polar NRZ	Constant envelope, DC term
Polar RZ	Timing extraction by rectifying, DC term
Dipolar OOK	Simple timing extraction, no DC term
Manchester	Zero DC and Constant envelope
CMI	Simple timing extraction, no DC term
<i>n</i> B <i>m</i> T	Timing extraction by rectifying, no DC term



8B10B

- Maps 8-bit symbols to 10-bit symbols
 - The low 5 bit of data are encoded into a 6-bit group (the 5b/6b portion)
 - The top 3 bits are encoded into a 4-bit group (the 3b/4b portion).
- DC-balance
 - Difference between number of1s and 0s in a string of at
 least 20 bits is no more than 2
- enough state changes to allow clock recovery
- run-length limit of 5 consecutive equal bits
- Firewire, SerialATA, HDMI, USB3.0, some GE



Multi-level signalling

- For the same data rate the symbol rate (Baud rate) is reduced, which implies less noise at the output of the receiver filter
- For the same average transmit power the amplitude discrimination between adjacent signal levels is reduced, which implies reduced tolerance against noise
- Overall the BER/power performance is worse for m-ary than for binary - but the reduced bandwidth requirements may justify it use



m-ary baseband signalling

- Increasing the number of levels for the same symbol rate provides for increased data rate over a given bandwidth channel
- With the same average power this implies a reduction in margin against noise - or to maintain the noise margin and hence BER there must be an appropriate increase in received power.
- Alternatively, for a given information rate requirement increasing the number of levels can allow the symbol rate (Baud rate) to be reduced - which reduces the bandwidth and hence the noise - and so tends to ameliorate the increase compared with the binary case



Modulation

- Amplitude Modulation
 - Envelope AM
 - Double sideband suppressed carrier modulation, DSB-SC
 - Quadrature amplitude modulation (QAM)
- Angle Modulation
 - Frequency modulation (FM)
 - Phase Modulation (PM)
- Combined amplitude and phase modulation



AM schemes - analytic form

$$x_c(t) = a(t)\cos(\omega_c t) + b(t)\sin(\omega_c t)$$

Envelope AM: $a(t) = 1 + km(t), b(t) = 0$
DSBSC: $a(t) = m(t), b(t) = 0$
SSBSC: $a(t) = m(t), b(t) = \widehat{m}(t)$
VSB: $a(t) \equiv 1 + km(t), b \equiv \widehat{m}_{HF}(t)$

- Message bandwidth W
- Envelope AM, DSBSC and QAM require bandwidth of 2W
- SSBSC requires bandwidth of W
- VSB requires W<bandwidth<2W
- SSB and QAM are power and bandwidth efficient



How to choose a digital modulation scheme

- Power efficiency (E_b/N_o for a given BER)
- Bandwidth efficiency (bits/s/Hz)
- Performance in the presence of non-idealities (fading, noise, distortion, jitter, non-linearity)
- Cost and complexity

Not all of these can be satisfied simultaneously!!

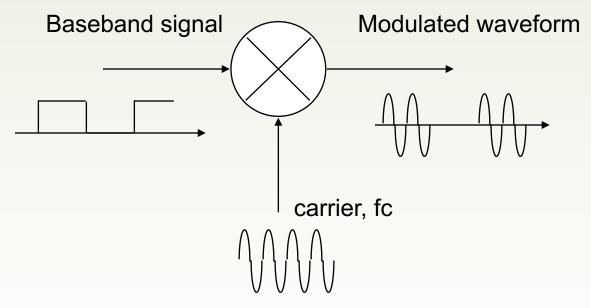


Angle Modulation

- Frequency and phase modulation are closely related frequency corresponds to rate of change of phase
- FM requires a bandwidth of W=2Fm(1+ β) Carson's rule β is the modulation index or peak deviation ratio
- FM and PM are tolerant to amplitude nonlinearity and so are compatible with high power amplifiers.
- FM offers an 'improvement factor' compared with AM of the order of $3\beta^2$
- FM systems have noise proportional to f²; preemphasis is employed to allow for this



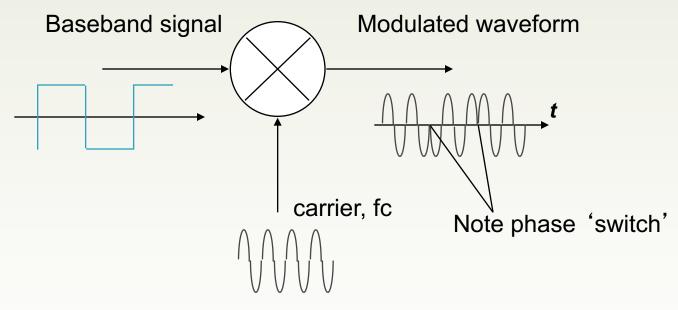
ASK schemes 1:



- The carrier is switched on and off by the unipolar binary signal, hence this form of ASK is sometimes referred to as <u>on-off keying (OOK)</u>
- In terms of analogue AM this is equivalent to binary envelope modulation with 100% modulation depth



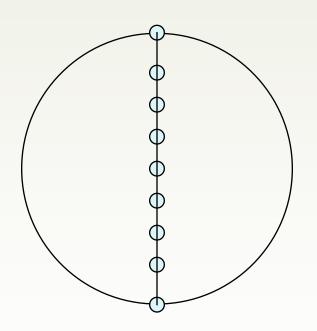
ASK Schemes 2:



- Note that this arrangement is equivalent to binary phase shift keying (BPSK) with 0 and π as the two phases
- In terms of analogue AM it is the equivalent of DSB-SC
- With an m-ary baseband input the modulated signal is multi-level ASK (m-ary ASK)



Amplitude Modulation



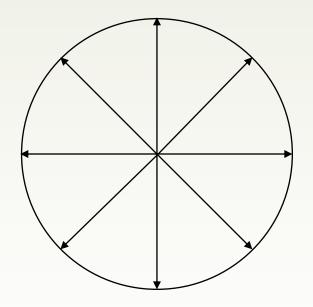
$$x(t) = A_m(t) \cos(\omega_c t)$$

 $A_m(t)$ conveys the data

- Can carry n-bits/symbol with 2ⁿ amplitudes
- Envelope varies with the data sensitive to amplitude distortion



Phase Modulation



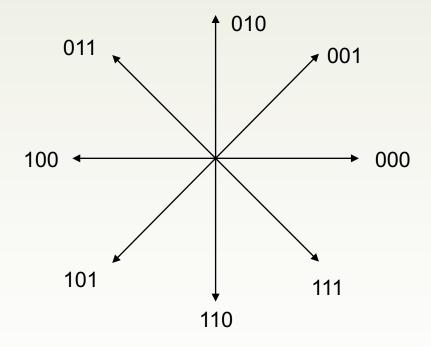
$$x(t) = \cos(\omega_c t + \phi_m(t))$$

 $\phi_m(t)$ conveys the data

- Can carry n-bits/symbol with 2ⁿ phases
- Constant envelope provides tolerance to amplitude distortion



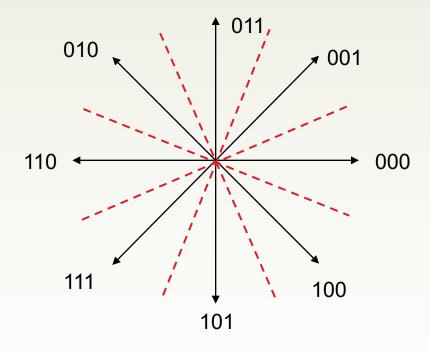
Phase-shift keying



- Possible signal phases for 8-phase PSK
- With 8=2³ phases there are 3 bits per symbol
- The phase coding shown is illustrative not necessarily the best choice!



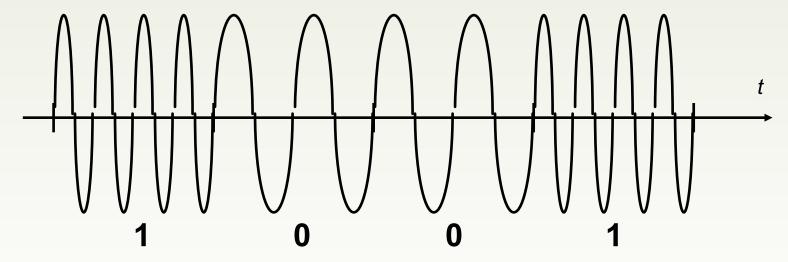
Phase-shift keying – Grey Code



- Grey Coding means that there will only be one bit in error if a decision is made in the wrong sector
- This form of coding is used with most angle modulation schemes



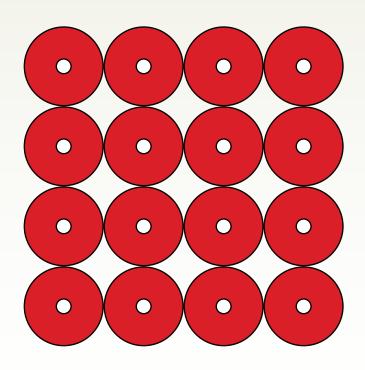
Frequency shift keying



- Binary FSK involves gating between two oscillators of different frequencies - with an obvious extension to m-ary FSK
- An alternative is to apply the baseband signal to drive a voltage controlled oscillator, which avoids phase discontinuities
- Again, the m-ary extension is straightforward



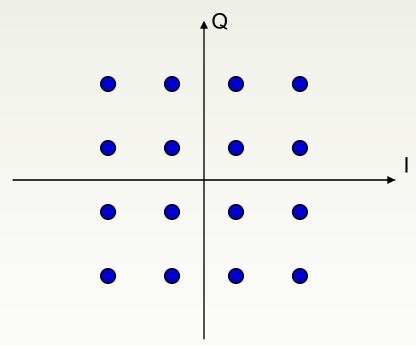
QAM Signals



- Signal space diagram or constellation
- 16 state QAM signal
- 4 bits per symbol
- Amplitude depends on state (data) being conveyed



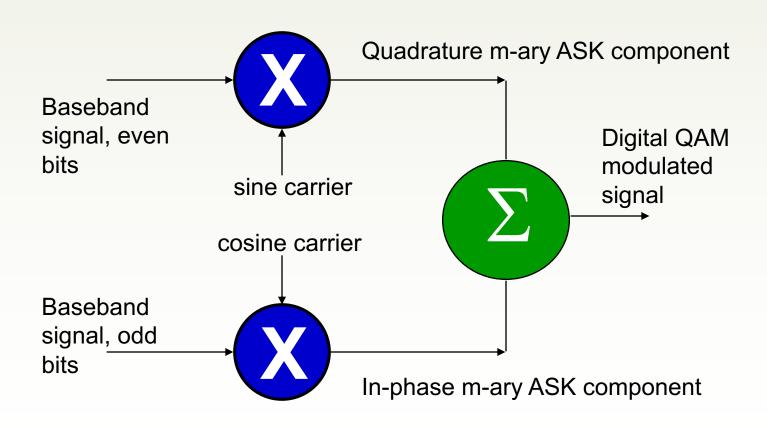
Quadrature amplitude modulation (QAM)



- 16-ary QAM has 4 in-phase and 4 quadrature signal levels, giving a total of 16 possible points in the signal constellation
- The capacity of this arrangement is 4 bits per symbol 2 each for the in-phase and quadrature components
- The above is only ONE example. There are many others...



QAM signal generation



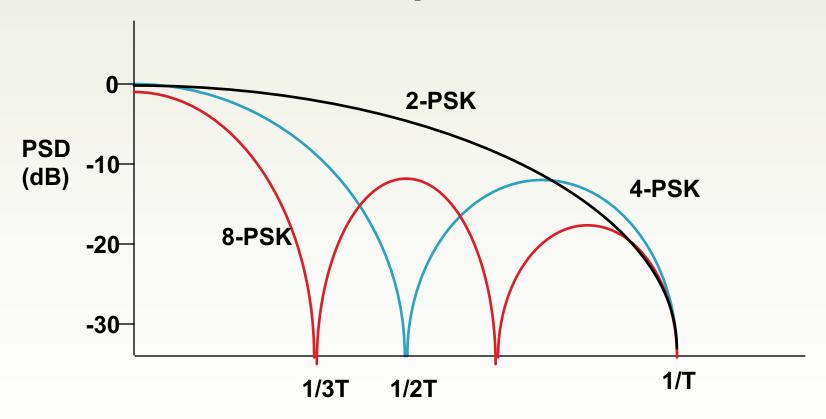


Phase Shift Keying

- From analogue modulation we know that DSB-SC provides the same SNR as does baseband transmission
- Hence 2 ϕ PSK (which corresponds to polar binary ASK) similarly provides the same SNR and hence BER as baseband binary transmission
- 4-f PSK(equivalent to 4 state QAM) similarly achieves the same performance as baseband transmission for the same data rate - or equivalently allows a factor of 2 increase in data rate over a given bandwidth channel at the expense of only a factor of 2 (3dB) increase in required received power
- m-ary PSK provides further increase in data rate for a given channel bandwidth at the expense of increased received power requirements for a given BER



Unfiltered PSK Power Spectra



Based on uncorrelated data and rectangular NRZ signalling



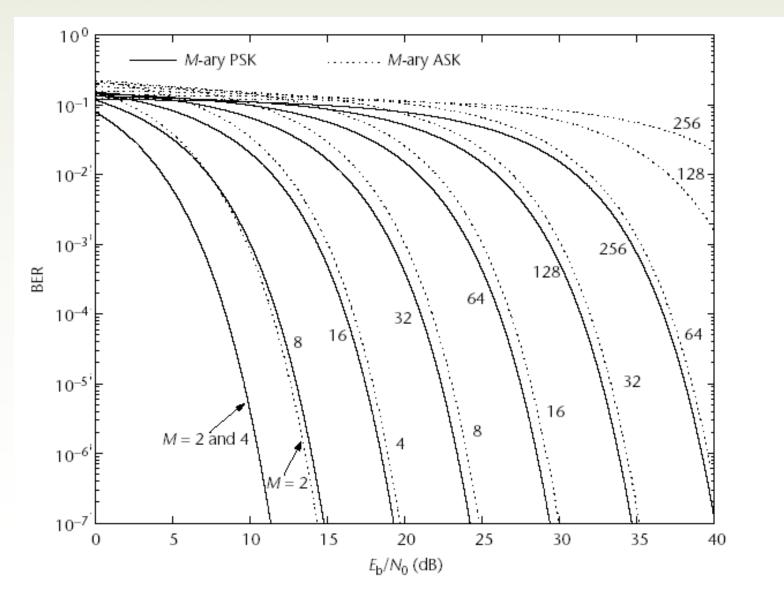
MSK - minimum shift keying

- A form of binary FSK (Continuous Phase FSK)
- Frequencies are such that exactly $\pi/2$ phase shift exists between the two signals in one symbol interval. This is achieved by fixing the frequency separation between carriers to be equal to the symbol rate (or its integer multiples)
- MSK produces the maximum phase difference using the minimum difference in signalling frequencies
- For MSK $\Delta \omega = \pi/T$ and $m_2(t)$ is a symmetric binary NRZ signal
- The result is bandwidth limitation

And there is Gaussian MSK (GMSK) used in GSM systems



Performance



Taken from Communication Engineering Principles, © Ifiok Otung, published 2001 by Palgrave



Summary

- Binary signalling
- Eye diagrams
- ISI and jitter considerations
- Noise and system performance
- Modulation and multi-level signalling