C:\Users\anreinhardt\Desktop\Logo_FAPS.wmfParametric Tool for Automated Slot Insulation

Insertion in Small-Scale Electric Motor Stator

Production

Project Thesis in study program Electromobility ACES

Friedrich-Alexander-Universität Erlangen-Nürnberg  
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ABSTRACT

The customer specific manufacturing of stators for electric motors in small-scale production is based on a time-consuming and expensive process chain. For this reason, the Institute for Factory Automation and Production Systems (FAPS) from Friedrich-Alexander University Erlangen-Nuremberg (FAU) is researching on solutions centered on the flexible automation of these processes. This paper presents a parametric mechanical tool designed for the robotic-based insertion of slot insulation paper in electric motors. While this task is predominantly performed manually in small-scale production, the proposed tool offers a flexible solution for automation. The tool enables rapid adaptation to different stator configurations by generating customized insertion tools. Given the limited profit margin, the cost-efficiency of the solution is a key factor in its development. The main goal is to improve flexibility in assembling different variants, small batch sizes and customer specifications

Table Of Contents

[ABSTRACT 4](#_Toc203557565)

[Table Of Contents I](#_Toc203557566)

[1 Introduction and objectives 6](#_Toc203557567)

[1.1 Motivation 6](#_Toc203557568)

[1.2 Vision 8](#_Toc203557569)

[1.3 Problem Statement 8](#_Toc203557570)

[1.4 Structure of the thesis 8](#_Toc203557571)

[2 State of the Art 9](#_Toc203557572)

[2.1 Fundamentals of Stator Assembly 9](#_Toc203557573)

[2.1.1 Slot liner function and Importance 10](#_Toc203557574)

[2.1.2 Common Challenges in the Insertion Process 11](#_Toc203557575)

[2.2 Automation of Slot Liner insertion in Motor Manufacturing 12](#_Toc203557576)

[2.2.1 Large Scale vs Small Scale Production Strategies 12](#_Toc203557577)

[2.2.2 Automation Principles 14](#_Toc203557578)

[2.2.3 Design for flexible automation 14](#_Toc203557579)

[2.3 Variety in Stator Design for Slot Liner insertion 15](#_Toc203557580)

[2.3.1 Influence on Insertion tooling and strategies 16](#_Toc203557581)

[2.4 Robotic Systems for Insertion Tasks 17](#_Toc203557582)

[2.4.1 Suitable Robot Types 18](#_Toc203557583)

[2.4.2 Kinematics and Motion Control Principles 19](#_Toc203557584)

[2.4.3 End Effector Requirements 20](#_Toc203557585)

[2.5 Sensors and Actuators in Robotic Insertion Tasks 21](#_Toc203557586)

[2.5.1 Overview of Robotic Actuators 21](#_Toc203557587)

[2.5.2 Electric Grippers for Precision Handling 21](#_Toc203557588)

[2.5.3 Role of actuators in Slot Liner Insertion 21](#_Toc203557589)

[2.5.4 Overview of Sensors in Automation 21](#_Toc203557590)

[2.5.5 Force-Torque Sensors for compliant control 21](#_Toc203557591)

[2.5.6 Safety and Human Robot Interaction 21](#_Toc203557592)

[2.6 Programming Methods in Robotic Automation 21](#_Toc203557593)

[2.6.1 Overview of Robotic Programming 21](#_Toc203557594)

[2.6.2 Implementation of UR Script 21](#_Toc203557595)

[2.6.3 Integration of Sensor Feedback 21](#_Toc203557596)

[3 Hardware setup for flexible slot liner insertion 22](#_Toc203557597)

[3.1 Robotic Module 22](#_Toc203557598)

[3.2 Rotating Clamp for Stator Alignment 22](#_Toc203557599)

[3.3 Tool and Slot Liner Placement Platform 22](#_Toc203557600)

[4 Parametric tool for flexible slot liner insertion 25](#_Toc203557601)

[4.1 Selection of Required Adjustable Parameters 26](#_Toc203557602)

[4.2 Fundamental Tool design 27](#_Toc203557603)

[4.2.1 Initial Tool Concept and Design Considerations 27](#_Toc203557604)

[4.2.2 Final Tool Configuration 27](#_Toc203557605)

[4.3 Fitting Adjustable Parameters for Specific Use Cases 28](#_Toc203557606)

[5 PARAMETRIC SLOT LINER INSERTION PIPELINE 29](#_Toc203557607)

[5.1 Funnel Application 29](#_Toc203557608)

[5.2 Slot Liner Positioning and Partial Insertion 29](#_Toc203557609)

[5.3 Final Liner Insertion 29](#_Toc203557610)

[5.4 UR Script Based Insertion Control 30](#_Toc203557611)

[6 Tool Process Testing and Validation 31](#_Toc203557612)

[6.1 Testing results 31](#_Toc203557613)

[6.2 Stator A 32](#_Toc203557614)

[6.3 Stator B 33](#_Toc203557615)

[7 Result Discussion 35](#_Toc203557616)

[8 Outlook 36](#_Toc203557617)

[9 Bibliography 37](#_Toc203557618)

[10 References 38](#_Toc203557619)

Table of Figures

**No table of figures entries found.**

List of Tables

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Table of Abbreviations

ICE Internal Combustion Engines

PLDV Passenger Light Duty Vehicle

CLDV Commercial Light Duty Vehicle  
ASM Asynchronous Motor

PMSM Permanent Magnet Synchronous Motor

Cobot Collaborative Robot

# Introduction and objectives

The continued evolution of electric motor technologies is closely tied to advancements in manufacturing, automation and process optimization. As industries gradually transition towards electrification, particularly in the transportation sector, there is a growing need for adaptable systems that support efficient and scalable motor production. This thesis addresses on one such area by focusing on the development of a parametric tool for automated slot insulation insertion in small scale electric motor production. The goal is to enhance flexibility, precision and repeatability in a process that is often manual and time consuming.

## Motivation

For over a century, internal combustion engines (ICEs) shaped the course of transportation and industrial growth, powering everything from personal vehicles to heavy machinery and global logistics. Their dominance was built on several key advantages: mechanical simplicity, robust performance, relatively low production costs, and a well-established global refueling infrastructure. These engines enabled rapid mobility, supported economic expansion, and became a critical driver of technological innovation in the automotive and energy sectors. From long-haul freight to aviation and agriculture, ICEs provided the flexibility and power density necessary for a wide range of demanding applications, earning their place as the backbone of modern industry and everyday life. However, as their usage proliferated worldwide, the long-term environmental consequences proved to be far greater than initially anticipated. In particular, the extensive combustion of fossil fuels in ICEs has led to the dramatic rise in greenhouse gases, especially CO2, which is widely recongnized as the primary driver of human induced climatic change.

About 23% of global CO₂ emissions are attributed to the transportation sector, making it one of the largest contributors to climate change. Within this sector, freight transportation plays a particularly significant role, often generating more emissions than passenger transport on a per-vehicle or per-kilometer basis. The majority of these emissions come from diesel-fueled heavy-duty trucks, which dominate freight transport and contribute heavily to environmental pollution [1]. As shown in Fig. 1, in the past few decades, global CO₂ emissions from on-road vehicles increased from 1.7 Gt to 5.4 Gt, driven largely by the expansion of the vehicle fleet, especially in emerging economies. ICE vehicles emitted approximately 3.2 Gt of CO₂ globally in 2020 alone, underscoring the sector’s significant environmental impact. Passenger Light-Duty Vehicles (PLDVs), mostly gasoline-powered, were the top contributors in absolute terms, accounting for almost half of on-road emissions, largely due to their sheer number. Diesel-powered trucks, made up a significantly less portion of the fleet but produced 22% of emissions, making them the second-largest contributors and highlighting their disproportionately high emissions relative to fleet size. Commercial Light-Duty Vehicles (CLDVs), often used for urban goods transport, also contributed notably, particularly as part of the broader dieselization trend, although their emissions are often aggregated with PLDVs. [2]

A graph of different types of fuel

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Fig. 1 Global CO2 emissions from 1970 to 2020 by vehicle and fuel type. The panels are organized by fuel type (rows) and vehicle type (columns). [2]

In addition to contributing significantly to climate change, ICE vehicles are also major sources of air pollutants such as fine particulate matter (PM2.5), which poses serious risks to human health. Despite individuals spending only a fraction of their time in traffic, their exposure to harmful emissions during this period is disproportionately high, especially in congested urban environments. These health impacts translate into substantial societal costs in the form of healthcare expenses. While many regions are implementing stricter emission policies, the continued reliance on ICEs remains a significant barrier to improving air quality and public health. [3] This further underscores the urgency of developing cleaner, more efficient alternatives, such as electric vehicles-supported by scalable manufacturing technologies.

## Vision

The shift to electrification is not only about changing the energy source, it demands a complete rethinking of how these systems are designed and built. The manufacturing of electric motors, though less complex in moving parts than combustion engines, introduces new challenges in precision, scalability, and material handling. One such challenge is the insulation of stator slots, a critical step that influences motor performance, reliability and safety. To meet the increasing demand for high-quality motors at scale, automation of this process is essential. This project contributes to the broader vision of smart manufacturing by addressing one such bottleneck.

## Problem Statement

The goal of this project is to automate a specific step in the assembly of a pre-manufactured stator, namely, the robot-assisted insertion of slot liners into the stator slots. Currently this process is done manually, especially for small batch sizes. The core focus of this thesis is the development of a tool that enables reliable and repeatable insertion of the slot liners. Furthermore, the functionality and performance of the system will be optimized and validated within an automated robotic setup.

## Structure of the thesis

This thesis consists of six chapters. The first chapter outlines the motivation, vision, and the specific problem addressed in this work. Chapter two presents the theoretical background and the current state of the art in motor manufacture, slot liner insertion and robotics. Chapter three provides an overview of stator manufacturing, with a focus on the challenges related to slot insulation. The fourth chapter discusses the need for automation in stator assembly and defines the requirements for developing a suitable solution. Chapter five details the implementation process carried out during the course of this thesis, including the applied methodology, the resulting outcomes, and a critical discussion of each step. Finally, chapter six summarizes the overall findings, reflects on their significance within the context of ongoing research, and offers an outlook on potential future developments.

# State of the Art

Electric motors are fundamental components in a wide range of applications, and their production is undergoing a profound transformation to meet growing demand. While highly standardized and automated processes dominate large-scale production, such as in the automotive sector [4], small-scale and custom manufacturing remains prevalent in industries like marine propulsion, where motors are tailored to specific operational requirements [5].

## Fundamentals of Stator Assembly

A diagram of a section of a machine

AI-generated content may be incorrect.An electric motor generally comprises two main components: the **stator** and the **rotor**, both enclosed in a housing. The stator core is built from laminated electrical steel sheets, cut via punching or laser processes. These laminations are then stacked and bonded through riveting, welding, or adhesive techniques, to form the magnetic core essential for motor function.The **motor housing** is typically produced using **pressure die-casting** and subsequently machined to ensure surface quality and dimensional precision.

Fig. 2 Overview of insulating and supporting parts in a low-voltage insulation system: 1 turn insulation, 2 slot liner, 3 slot separator, 4 wedge, 5 phase separator, 6 lead sleeving, 7 coil-nose tape, 8 connection tape, 9 cable, 10 tie cord, and 11 bracing.

Once the stator core is assembled, several key sub-processes follow. One of the first is the insertion of slot insulation to electrically isolate the windings from the core. This is followed by the winding process, in which copper wire is inserted into the stator slots. Depending on the motor design and production requirements, different winding techniques may be employed, such as linear winding, needle winding, flyer winding, or the pull-in method using preformed coils. After winding, the wire ends are insulated, the winding head is formed, and the conductors are interconnected using methods such as crimping, soldering, or suitable welding techniques. The stator is then mechanically stabilized using bandaging and impregnated with resin through processes like trickling, dipping, or vacuum pressure impregnation, to enhance insulation and thermal dissipation. Electrical tests are carried out to verify winding resistance, insulation quality, and overall functionality. Meanwhile, the rotor shaft is formed and machined, joined with its laminated core, and completed depending on the motor type. In asynchronous motors (ASM), a rotor cage is manufactured by pressure die-casting, while permanent magnet synchronous motors (PMSM) incorporate embedded or surface-mounted permanent magnets. The rotor is subsequently balanced before final motor assembly and end-of-line testing, which ensures mechanical and electrical compliance with design specifications [4]. Figure 1 shows typical insulation elements in a stator, including slot liner, interphase insulation and wedges. [6]

### Slot liner function and Importance

One of the most critical and delicate steps in stator manufacturing is the **insertion of slot insulation**, often in the form of **slot liners**. These components serve two essential functions: they electrically isolate the stator windings from the core and contribute to **thermal management** by enabling heat dissipation from the windings. Especially in low-voltage electric motors, the slot liner must balance **high dielectric strength** with **thermal conductivity**. Material selection is therefore crucial, as improved thermal performance can directly enhance motor efficiency and longevity. [7]

In particular, the thermal management role of the slot liner is heavily influenced by how heat flows through the stator slot. Fig 2. illustrates the direction of the heat flow, which is from the middle of the slot to the laminate, passing through several layers of winding and the slot liner. A major challenge in this path is the interface air gap between the liner and the laminate, particularly at the rounded corners of the slot, where geometric mismatches increase thermal resistance. This interface gap acts as a thermal barrier, impeding effective heat dissipation. However, proper impregnation techniques can mitigate this issue by filling the gaps, thereby improving thermal contact and overall heat transfer. Consequently, key factors influencing slot thermal performance include the air gap at the liner-laminate interface, the thermal properties of the slot liner A diagram of a cross section of a log

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Fig. 3 Stator slot in (a) detail model (motor-cad) and the (b) actual stator slot

Due to the **precision and repeatability** required in the insertion process, manual insertion is often inconsistent and time-consuming. Errors in this step can negatively affect motor performance or lead to failure, which makes **automation** of slot liner insertion an attractive and increasingly necessary solution.

### Common Challenges in the Insertion Process

While large-scale production of electric motors typically involves fully automated processes, it is not economically feasible to implement dedicated machinery for each stator variant in customized small-scale production. Consequently, slot insulation insertion is often performed manually, which introduces several challenges. Quality variations arise due to differences in operator skill and fatigue, leading to inconsistent placement of insulation materials that can compromise motor performance and reliability. Furthermore, the repetitive and physically demanding nature of this task increases the risk of physical strain and injuries among workers, especially when performed over extended periods. These factors, combined with high labor costs in many regions, result in a process that is not only expensive but also inefficient and prone to human error.

To overcome these limitations, this paper proposes a flexible automation approach that combines a parametric mechanical tool with a general-purpose industrial robot or collaborative robot (Cobot). When equipped with the parametric tool, the robot system can perform slot insulation insertion for a variety of stator geometries without requiring

extensive hardware changes for each variant. This enables a consistent and repeatable process, improving operational efficiency and providing the flexibility required in high-variety, low-volume production environments. At the same time, the system is designed to minimize programming effort and allow for quick reconfiguration between different stator types to ensure overall cost efficiency, especially in high labour cost environments. Potential application scenarios, advantages and limitations of robot-assisted automation solutions have been explored and discussed in previous research work, e.g. Kühl et al. [9], Mahr et al. [10] or Henrich et al. [11]

## Automation of Slot Liner insertion in Motor Manufacturing

The process of inserting slot liners into stator slots varies widely across different manufacturing scales, from fully automated systems in mass production to manual operations in smaller workshops. This variation reflects the diverse requirements and constraints manufacturers face in balancing cost, flexibility, and quality. In the following sections, different automation solutions are reviewed, along with the fundamental principles guiding their development and implementation in modern electric motor production.

### Large Scale vs Small Scale Production Strategies

In the context of large-scale electric motor production, the slot liner insertion process is carried out using specialized automation systems designed for precision, speed, and adaptability. Slot insulation machines from manufacturers such as ELMOTEC STATOMAT, NIDE, and Delta Automation Technologies are designed to automate and optimize this process for various stator designs. These machines insert specially shaped insulation paper into the stator slots using a coordinated sequence of creasing, folding, cutting, and inserting. The process guarantees precise alignment and paper overhang, which protects the copper windings from the sharp edges of the laminated core while maintaining a shape conducive to winding insertion. High-speed insertion rates, such as three sleeves per second, are achieved alongside consistent quality, even in small series production. Advanced features like servo-driven feeding, automatic paper forming, programmable interfaces, robotic loading/unloading, and computer-controlled moulds further enhance productivity and flexibility. The machines are engineered for durability, using tempered steel components and stable tubular frameworks, allowing for fast changeovers between stator types and reliable operation with minimal noise and user effort. The technical data-sheet for NIDE slot liner insulation machine is shown in Fig.4. [12–14].

A screenshot of a computer

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Fig. 4 Technical specifications of a slot liner insertion machine, detailing operational limits, dimensions, power requirements, and efficiency. [13]

Despite significant advancements in automation, manual insertion of slot liners remains the standard practice in the small-scale manufacture of electric motors. In such setups, operators typically cut, fold, and insert the slot liners entirely by hand, or use machines for cutting and folding as shown in figure 5, while performing the insertion manually with simple jigs. This process relies heavily on visual inspection and tactile feedback to ensure proper alignment However, with the growing demand for electric motors, the need for scalable and streamlined production is increasing. In this context, automation becomes a promising alternative, not because manual methods are ineffective, but because they are difficult to integrate into digital workflows, challenging to scale, and not easily documented for consistent reproduction. [6, 15, 16]

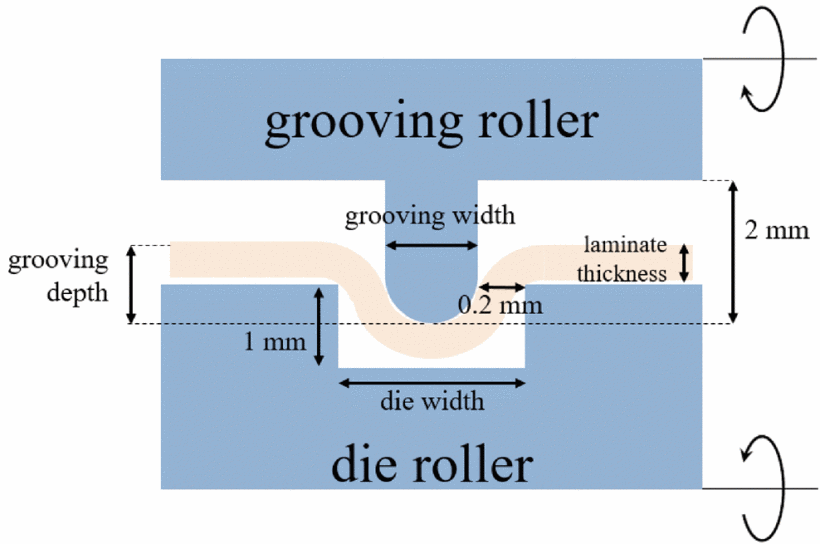


Fig. 5 Adjustable grooving module with two gear-coupled rotating shafts; Process principle: groove depth and width are controlled by roller spacing and track design, forming precise grooves on 0.2 mm thick slot liners.

### Automation Principles

In modern manufacturing, especially for small batch sizes with a high number of variants, automation solutions must be both flexible and economical. A key principle is to transfer repetitive and physically demanding tasks from human operators to automated tools to improve consistency and reduce workload. To remain cost-effective in low-volume environments, such systems should allow easy configuration for new product variants, minimizing programming and set-up efforts. In addition, a modular system architecture-in both hardware and software-allows for incremental expansion and integration of advanced features, such as real-time process adjustments or data-driven optimizations. Stable processes form the basis for reliable production results, while scalability ensures that automation can grow with evolving production requirements. Together, these principles create a framework for the transition from purely manual assembly to flexible and economically sustainable automation in a high variety product field. [17]

### Design for flexible automation

Flexible automation in small batch production requires process designs that can efficiently accommodate frequent changes in product geometries and batch sizes. A key element in achieving this flexibility is parametric tool design, where CAD-based models are defined using parameterized design principles. This approach enables rapid adaptation to different shapes and sizes of stator slots with minimal lead times and low costs, so that tool changes do not become a bottleneck in production .Robots and standard end effectors further contribute to process flexibility, allowing automated systems to perform different tasks without extensive retooling. Modular system architectures create a foundation for future enhancements, such as vision feedback systems or sensor-based adaptations that can improve process reliability and adaptability in real time. Intelligent systems that use digital models, environment-specific knowledge and trajectory-based movement commands support stable and responsive adaptation to variable production scenarios. Finally, scalability remains a key aspect of flexible automation. Even with increasing batch sizes, modular upgrades and reconfigurable system components help to maintain efficiency and make production processes economical. [18]

## Variety in Stator Design for Slot Liner insertion

Electric motor stators exhibit a considerable variety of geometric and structural designs, driven by application-specific performance requirements and space constraints. Key variations include the stator diameter, axial length (stack length), the number of slots, and, crucially, the geometry of the slots and teeth themselves. The majority of stator designs used in low to medium power AC electrical motors feature a parallel-sided tooth, resulting in a trapezoidal slot profile. This configuration enables effective utilization of the stator core material and facilitates the accommodation of windings made from many stranded circular conductors, which can be efficiently fitted into the irregular slot profile. In contrast, an alternative approach, using a parallel-sided slot with a trapezoidal-shaped tooth, is more commonly found in larger distributed wound machines and aircraft generators. The specific configuration of stator slots and teeth has a significant impact on electromagnetic performance, including magnetic flux distribution, core losses, and winding arrangement. Optimizing these shapes is crucial for minimizing losses and improving the magnetic circuit, especially in high-speed or high-frequency applications. Furthermore, the choice of slot liner material and its thickness plays a vital role in electrical insulation and thermal management, though it may also affect the available slot area and winding fill factor. Modern design practices often rely on advanced simulation and modeling techniques to balance requirements such as efficiency, torque ripple, noise, and manufacturability, ensuring that the stator slot and tooth geometry is well-matched to the intended application and winding configuration. [19, 20] . Different Topologies of the stator are shown in Fig 6.

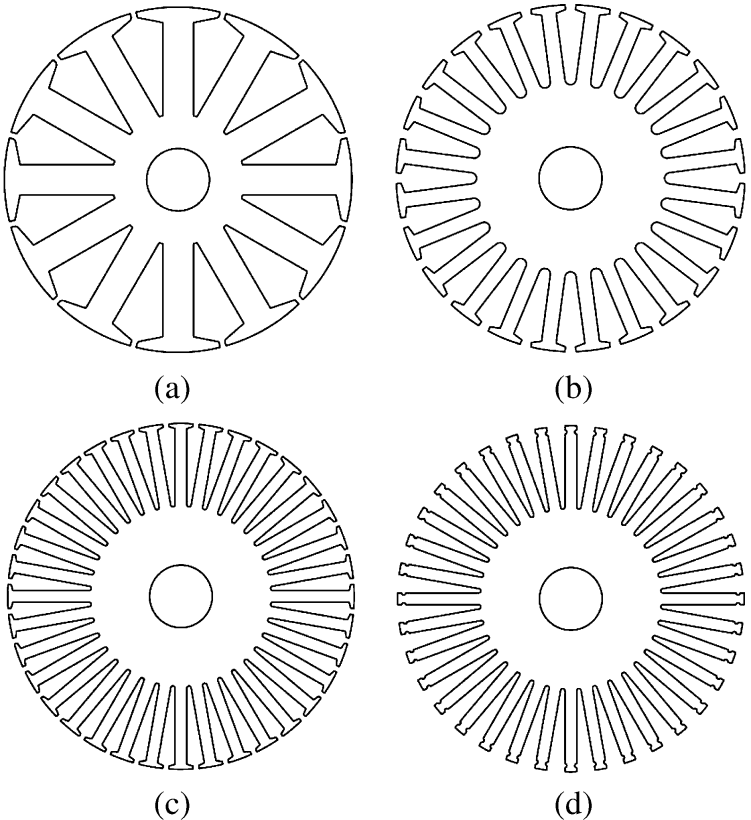


Fig. 6 Four typical stator configurations. (a) 12 stator slots. (b) 24 stator slots.(c) 36 stator slots. (d) 36 open stator slots

In view of this wide range of geometries, this paper focuses specifically on medium-sized stators, which are often used in industrial applications and are equipped with U-shaped slot liners. This slot liner shape is widely used in these stators as it provides a reliable balance between mechanical protection of the windings and simple insertion processes. In addition to the U-shaped liners, other common forms of slot liners such as L-shaped configurations are also adapted to specific stator geometries and winding techniques. By focusing on this segment, a clear scope for the analysis and optimization of insertion techniques for slot liners is ensured, while at the same time taking into account the practical challenges of variant management in low-volume production. [21]

### Influence on Insertion tooling and strategies

The geometry of slot liners, particularly the distinction between U-shaped and L-shaped configurations, exerts a significant influence on both insertion tooling and assembly strategies in stator manufacturing. U-shaped liners are often favored for their ease of handling, as their single-piece design is compatible with standard insertion tools, allowing for straightforward and efficient placement into the stator slots. This simplicity supports both automated and manual insertion processes, making U-shaped liners especially suitable for medium-sized stators in industrial applications. In contrast, L-shaped liners, as showin in Fig 7 which are typically inserted in pairs to form a complete insulation barrier, may require more precise alignment and specialized tooling to ensure both halves are properly positioned and retained during coil insertion. The presence of features such as reinforced cuffs at the slot edges further affects tooling requirements, as these areas may need additional support or guiding mechanisms to prevent damage or displacement during high-force insertion processes. Moreover, the choice of liner material and thickness also impacts insertion strategies, with thicker or stiffer liners demanding more robust tooling and careful handling to avoid folding or snagging. Ultimately, the selection of slot liner geometry not only shapes the design of insertion tools but also dictates whether fully automated, semi-automated, or manual strategies are most appropriate, particularly in low-volume or highly customized production environments where flexibility and precision are significant. [21]

A diagram of a wall with text

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Fig. 7 Cutaway view of a stator slot showing the arrangement of insulation materials and components, including the steel wedge, creepage block, turn-to-turn insulation strips, 'L' shaped slot liner, and subslot insulation. [21]

## Robotic Systems for Insertion Tasks

In industrial automation, robots are programmable machines capable of executing a wide variety of tasks with high speed, precision, and repeatability. Their adoption has transformed manufacturing environments by automating repetitive or complex processes, thus enhancing productivity, improving safety, and ensuring consistent product quality. The flexibility of modern robots allows them to adapt to diverse product designs and fluctuating production volumes, which is particularly valuable in applications such as stator assembly, where tasks like slot liner and winding insertion demand both accuracy and adaptability.

### Suitable Robot Types

Modern industrial automation relies on a diverse array of robotic systems, each tailored to specific tasks and operational environments. Among the most prevailent are Articulated robots, SCARA robots, Cartesian and Delta robots. Articulated robots are described as robotic arms with multiple rotary joints, often resembling a human arm, which allows them to perform a wide range of movements and tasks such as welding, assembly, and material handling. Selective Compliance Assembly Robot Arm (SCARA) robots, characterized by three revolute and one prismatic degree of freedom, have become a mainstay in packaging and assembly line automation.These robots are now commercially availabe in a wide range of sizes, linear speeds, and payload capacities to suit diverse industrial needs. While their control systems are typically optimized for standard industrial operations, these configurations often lack the flexibility required for advanced research applications. Cartesian robots, also known as gantry robots, move linearly along three perpendicular X, Y and Z axes, and are commonly used in applications that require straight-line movements such as CNC machine operations and automated drawing or cutting. Delta robots are constructed with lightweight, parallel arms connected to a fixed base, enabling extremely fast and precise movements; they are especially suited for high-speed sorting and packaging tasks. Fig 8 illustrates the different robot configurations. [22, 23]

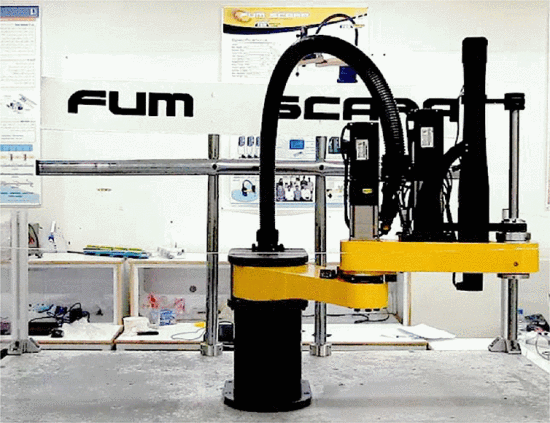


Fig.8 (a) SCARA Robot

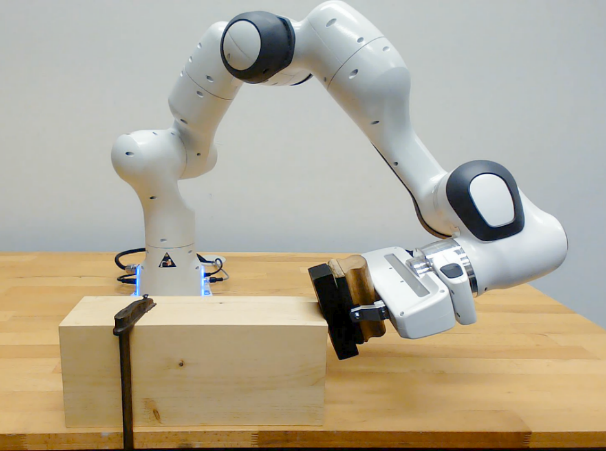


Fig 8 (b) Articulated robot

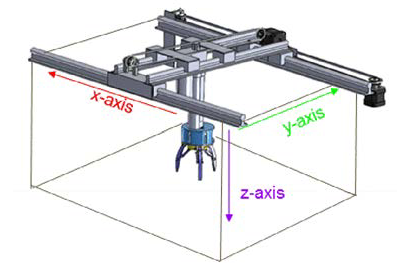


Fig 8 (c) Cartesian Robot

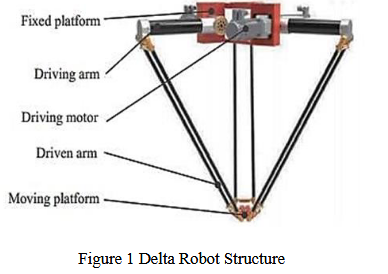


Fig 8 (d) Delta Robot

Fig. 8 Examples of common industrial robot configurations used in manufacturing and automation.

Collaborative robots, or cobots, which are designed with advanced sensors and safety features to work alongside humans without the need for safety cages, are increasingly used for flexible automation in environments where human-robot collaboration is beneficial. Each robot type is engineered with specific kinematic structures and control systems, allowing them to excel in particular industrial roles and adapt to the evolving demands of modern manufacturing. In this project, a UR10e robot is utilized as the collaborative robot of choice. As a cobot, the UR10e offers several distinct advantages in flexible automation settings. Its advanced safety features, including integrated sensors and force-limiting technology, enable it to work safely alongside human operators without the need for traditional safety cages. This not only enhances workplace safety but also allows for more efficient use of floor space. Additionally, the UR10e is designed for ease of use, featuring an intuitive programming interface that enables quick setup and redeployment for a variety of tasks. Its flexibility and adaptability make it ideal for environments with evolving production requirements, while its ability to automate repetitive or ergonomically challenging tasks helps improve overall productivity. By integrating the UR10e cobot, the project benefits from increased efficiency, enhanced safety, and the ability to quickly adapt to changing manufacturing demands.

### Kinematics and Motion Control Principles

Kinematics and motion control are foundational to the operation and effectiveness of collaborative robots such as the UR10e. Kinematics refers to the mathematical and geometric study of a robot's movement, focusing on the relationship between joint parameters and the position and orientation of the end-effector, without regard to the forces involved. In the context of the UR10e and similar cobots, both forward and inverse kinematics are essential: forward kinematics calculate the end-effector's position from given joint angles, while inverse kinematics determine the necessary joint angles to reach a desired position and orientation in space. [24]

Building upon the understanding of forward and inverse kinematics, Universal Robots' UR10e utilizes the Denavit–Hartenberg (D-H) convention to systematically model each of its six revolute joints. This modeling framework enables the formulation of transformation matrices that map joint space coordinates to Cartesian space, which is crucial for precise motion planning and real-time control. The D-H parameters define the spatial relationship between links, allowing for calculated transitions between various positions and orientations required during collaborative tasks [25]. The calculation of DH parameters in a UR robot is illustrated in Fig 9

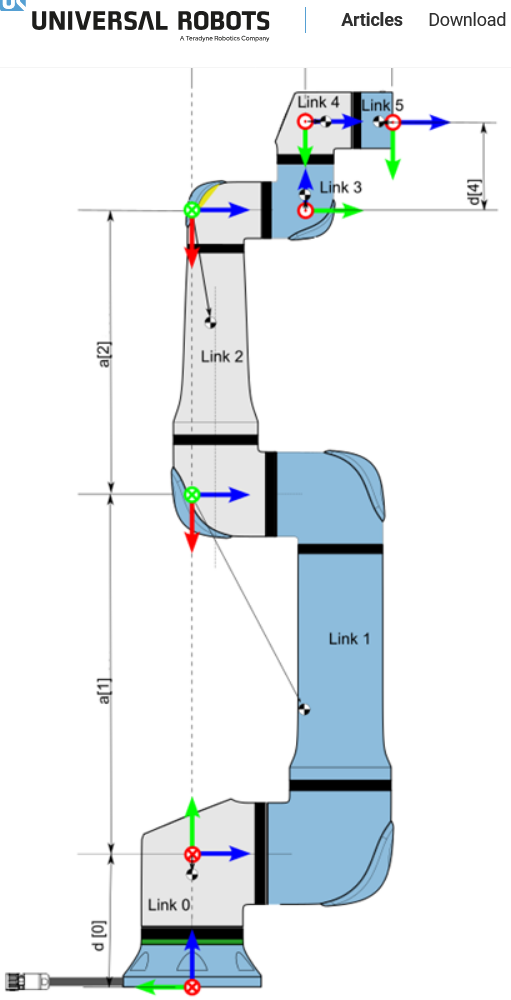


Fig. 9 DH parameter calculation in a Universal Robot

Motion control in the UR10e combines these kinematic models with robust feedback mechanisms and trajectory planning algorithms. Typically, users command the robot via waypoints and trajectory definitions within the programming environment, with the robot’s low-level controller executing the appropriate joint movements to interpolate smoothly between points. The UR10e is fundamentally a position-controlled robot, its built-in controllers accept position and velocity setpoints, rather than torque commands, which means the system emphasizes accuracy and safety, making it well-suited for collaborative environments.The effectiveness of these kinematic and control principles is further enhanced by the UR10e’s modular design, extensive joint ranges, and safety features like collision detection and force limits. The combination of precise kinematic modeling and advanced motion control forms the foundation of the UR10e’s reliability, flexibility, and user-friendly operation in diverse collaborative applications. [26]

### End Effector Requirements

The requirements for end effectors in robotic insertion tasks are shaped by the need for precision, adaptability, and safe handling of often delicate or varied components. For such tasks, the end effector must ensure positional accuracy and repeatability, minimizing insertion forces to protect both the components and the robot. Research highlights the importance of compliance, either through mechanical design or sensor feedback, to accommodate minor misalignments or uncertain tolerances, which is especially significant in operations like slot liner insertions for small-batch, high-variant manufacturing. The end effector design can thus incorporate passive compliance or active sensing (vision, tactile, and force/torque sensors) to enhance performance and reduce the risk of damage or failure during automated assembly. Additionally, modularity and flexibility are crucial: end effectors must often be quickly reconfigurable or compatible with a range of tools to support the diversity encountered in low-volume, customized production environments. Sensors integrated within or attached to the end effector should also support real-time monitoring and adaptive control, key factors in boosting insertion success rates and advancing automation reliability for sensitive handling tasks. [27, 28]

## Sensors and Actuators in Robotic Insertion Tasks

From the requirements described in the previous sections, flexibility and ease of configuration are crucial to meet the current state of the art in low volume, high variance production environments. The choice of actuator is crucial: industrial robots and Cobots are well suited for these tasks due to their inherent flexibility in terms of size and motion, their cost efficiency compared to specialized machines and their ability to work with standard end effectors such as grippers. This section provides an overview of the typical actuators and sensors used in robotic insertion tasks. It introduces various types of electric grippers suited for precision handling, discusses the role of actuators and compliant control, and explains the importance of sensor integration, especially force-torque sensors, for achieving consistent and reliable insertion. Safety and human-robot interaction considerations in such systems are also addressed.

### Electric Grippers for Precision Handling

Electric grippers are among the most versatile and widely adopted end effectors in modern robotics, especially valued for their ability to deliver precise, repeatable, and programmable manipulation of objects in automated tasks. These devices come in numerous configurations, each tailored to address the diverse requirements of precision handling and insertion processes encountered in industrial and collaborative environments. The most common type, the parallel jaw gripper, employs two jaws that move synchronously to grasp objects with consistent force control and high positional accuracy, making them ideal for handling components with uniform geometry such as circuit boards or machined parts. [29]



Fig 10 (a) Parallel jaw grippers



Fig 10 (b) Three Finger Grippers



Fig 10 (a) RG2 Gripper



Fig 10 (c) Soft Electric Gripper

Fig. 10 Different Gripper congigurations provided by On Robot

Another prevalent design, the three-finger or centric gripper, uses a radial jaw arrangement to offer self-centering and secure grasping of round or cylindrical items like pipes, bearings, or fasteners, ensuring stability during manipulation. Some electric grippers include built-in rotary axes, allowing them not only to grip but also rotate workpieces for orientation adjustments without additional arm movement, which improves operational efficiency in complex assemblies. For delicate or variably shaped parts, adaptive and soft electric grippers have emerged. These models use fingers with flexible or compliant material, sometimes powered by unique mechanisms such as tendon drives or shape-memory alloys to conform gently to irregular geometries, thus preventing damage during handling and adapting seamlessly to high-mix, low-volume production setups. Wide-stroke grippers extend this versatility further by accommodating larger or differently sized parts, supporting applications where component variability is high and downtime for changeover must be minimized. In collaborative workspaces, electric grippers designed for safety integrate features like force and speed limitation, smooth profiles, and compliance with international safety standards, allowing them to operate safely in proximity to human workers. [30, 31]

### Role of actuators in Slot Liner Insertion

### Overview of Sensors in Automation

### Force-Torque Sensors for compliant control

### Safety and Human Robot Interaction

## Programming Methods in Robotic Automation

### Overview of Robotic Programming

### Implementation of UR Script

### Integration of Sensor Feedback

# Hardware setup for flexible slot liner insertion

## Robotic Module

## Rotating Clamp for Stator Alignment

## Tool and Slot Liner Placement Platform

The hardware setup is centered around a modular robotic cell designed to support flexible and precise stator production for electric motors. This cell integrates a Universal Robots UR10e Cobot, an OnRobot RG2 Gripper and a HEX Force-Torque (FT) sensor as shown in Fig.3, all coordinated through a central compute box that enables real-time control and adaptability. The stator is mounted vertically in a motor-driven clamp to enable accurate angular positioning of the slots. To support the insertion process, the system also includes dedicated platforms for positioning both the insertion tool and slot liner. Together, these components improve the overall accuracy and consistency of the insertion process.

A close up of a robot arm

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Fig. 11 OnRobot RG2 gripper with OnRobot HEX FT sensor mounted at the wrist, used for precise insertion and force monitoring

The Cobot provides programmable motion control, enabling repeatable execution of the insertion tasks. The FT-sensor is mounted on the wrist of the robot for measuring interaction forces during operation. The gripper is attached to the FT-sensor, which allows for secure and flexible handling of the slot liners and funnels of varying sizes and geometries. The robot in combination with the FT-sensor and gripper forms a versatile platform for implementing advanced control strategies, improving insertion accuracy, and handling different stator geometries, typically encountered in small-batch electric motor production.

To address the variation in stator designs, the hardware setup incorporates modular and interchangeable tools. Customized tools for guiding slot liners were created using parametric CAD models, whereby rapid adaptation to different motor designs can be achieved by changing just a few core variables. These tools are easily fabricated through 3D printing, which significantly reduces lead time and cost for new configurations.

Sensor-assisted modularity further enhances system performance. The integrated FT-sensor enables real-time monitoring of contact forces during the insertion process, providing valuable force-based feedback to ensure proper positioning and to avoid excessive forces or potential misalignment. This capability enhances the robustness of the system, especially during the initial setup phase Moreover, the presence of the FT-sensor opens possibilities for future development, such as closed-loop feedback control, which could further refine insertion precision under varying mechanical tolerances.

A machine in a factory

AI-generated content may be incorrect.Customized 3D-printed platforms, shown in figure 5, were also designed for the parametric tool and slot liners to ensure secure and repeatable positioning. The tool platform enables reliable and consistent gripping by the robot during each insertion cycle, minimizing alignment errors and improving process stability. Similarly, the slot liner platform held a single pre-folded slot liner in a predefined orientation, enabling precise and repeatable pickup. Although manual reloading was required after each cycle, the secure positioning significantly improved the repeatability and consistency of the entire process.

Fig. 12 Tool and slot liner placement platforms: These platforms enable the robot to consistently and securely grip both the insertion tool and the slot liners for each cycle, ensuring repeatable and reliable operation

The stator itself was mounted on a mechanical rotary clamp that could rotate through an angle specified by the user. This rotary mechanism made it possible to adjust the stator incrementally so that each slot was aligned with the funnel after every successful insertion. The rotation step size was configured based on the number of slots in the stator, ensuring the system to perform fully automatic insertions across multiple slots without the need for manual repositioning.

# Parametric tool for flexible slot liner insertion

A close-up of several objects

AI-generated content may be incorrect.Although general design principles exist for stator slot configurations, the specific geometry is often customized to meet targeted performance requirements such as electromagnetic efficiency, torque output, thermal management and harmonic mitigation. As a result, slot dimensions and shapes can vary depending on the motor’s intended application [15]. For instance, [16] reports stator slots with a height of 30 mm and a slot width of 20 mm. In contrast the stators used in the present study feature smaller dimensions: The first stator has a slot height of 20 mm and a slot width of 8 mm, while the second has a slightly larger slot height of 22 mm. This variation highlights the need for adaptable solutions that can rapidly conform to different geometries to support flexible and efficient insertion of slot liners without requiring extensive manual reconfiguration. To address this problem, a parametric tool designed in the form of a “Funnel” was developed to guide the slot liners into the stator slot. Its design and various views are shown in figure 2.

Fig. 13 Different views of the parametric funnel. The funnel features a tapered internal geometry that guides the slot liner smoothly toward the outlet. The rear view shows the slot profile corresponding to the stator geometry, while the side view highlights the sloped design for insertion. The top view shows the rectangular inlet aligned precisely with the outlet channel.

## Selection of Required Adjustable Parameters

A diagram of a slot angle

AI-generated content may be incorrect.The parameters selected for adjusting the funnel to specific stator configurations, as shown in figure 6, are the slot width, the slot height, and the slot angle. These parameters have a direct influence on the geometry of the funnel, and therefore on the success of the insertion of the slot liner. By determining and adjusting these key dimensions, the insertion tool can be effectively adapted to a wide range of stator topologies. The slot-width governs the base opening and determines the maximum liner width that can be inserted. The slot-height dictates the depth of the slot liner that can be inserted and impacts the structural dimensions of the funnel. Lastly, the slot-angle affects the taper or curvature at the slot entrance, which is critical for guiding the liner during insertion without mechanical interference.

Fig. 14 Key parameters of the funnel design, including slot width, slot height, slot angle, and slot thickness. These parameters define the funnel geometry and limit the allowable dimensions and travel path of the slot liner during insertion

## Fundamental Tool design

### Initial Tool Concept and Design Considerations

### Final Tool Configuration

The funnel serves as a mechanically guided insertion aid positioned between the stator and the gripper during slot liner insertion. It helps shape and align the slot liner, simplifying the process and enhancing insertion accuracy.

The body of the funnel is rectangular in shape with an internal tapered channel that converges towards the stator slot. The inner surface is shaped with two gently curved guiding walls, which direct the slot liner into the correct slot while maintaining central alignment. At the core of the design is a central opening that allows the slot liner to pass through, effectively preventing twisting during insertion. A tapered profile along the insertion path provides slight compression of the slot liner, which helps it retain its shape and improves positioning accuracy as it enters the stator. To ensure vertical alignment, the front face of the funnel includes an inner guiderail that extends towards the stator’s slot profile. This rail serves as a continuous reference surface and guides the liner along the internal geometry of the slot, ensuring consistent insertion height and repeatability. The ends of the rail are tapered to minimize the chance of the slot liner being pulled back with the funnel during retraction.

A close-up of a grey object

AI-generated content may be incorrect.The rear of the tool also features an external guide rail that helps maintain proper alignment between the funnel and the stator during setup and operation. The grooves on the guide rail, as shown in figure 5, enhance positional locking, ensuring a firm fit and preventing unintentional movement or misalignment during insertion. The funnel inlet is widened to introduce a tolerance margin, accommodating minor misalignments and improving ease of use in practical conditions. The dimensions of the inlet are also parametrically linked to the slot height - as the slot height increases, the funnel inlet automatically scales in size. This preserves insertion reliability across various configurations.

Fig. 15 Grooves on the back of the funnel for proper alignment and locking to the stator slot.

The funnel is lightweight, and 3D printed using Poly Lactic Acid (PLA), a cost-effective material that supports rapid design iterations and economical production for small-scale applications. Design considerations were also made for robotic handling: the side faces are flat with a standard width of 20 mm to facilitate secure gripping. Additionally, the tail of the tool is extended to 50 mm, intentionally shifting the center of gravity rearward, to prevent forward tilting during handling, which could otherwise cause misalignment. To enhance the insertion process, a 1 mm clearance is maintained between the bottom opening of the funnel and the end of the inner-guide rail. This gap allows for smoother slot liner insertion.

The process begins with the robot picking up the funnel from the funnel platform and inserting it into the stator slot. Once positioned, the robot retrieves the slot liner from the platform and inserts it through the funnel into the stator slot. This procedure ensures accurate alignment and reliable slot liner placement.

## Fitting Adjustable Parameters for Specific Use Cases

To validate the adaptability of the parametric funnel design, two stators, both with an outer diameter of 240 mm but different slot geometries, were selected as representative use cases. The first stator has a slot height of 20 mm, while the second has a slot height of 22 mm. The funnel geometry was modified in CAD by adjusting predefined parameters, particularly the slot height. In both cases, the slot height of the funnel was deliberately set slightly lower than the actual stator slot height, to avoid possible interference during insertion. For example, the funnel slot height was parameterized to 19.50 mm for the first stator and 21.50 mm for the second. After the adjustments, the customized funnels were 3D printed and prepared for integration with the robot. These configurations were then used in the validation phase to evaluate the repeatability of the insertion process and the alignment accuracy across both the stators.

# PARAMETRIC SLOT LINER INSERTION PIPELINE

Reliable and flexible slot liner insertion is essential for small-batch electric motor production. To meet this need, a modular automation pipeline was developed. The pipeline was designed with scalability and adaptability in mind. Its parametric nature and sensor feedback implementation allows for quick adjustments to accommodate various stator geometries with minimal hardware or software modifications. By combining mechanical guidance with sensor-assisted control, the setup balances process flexibility, insertion accuracy, and operator safety. The following sub-chapters detail the pipeline architecture, key components, and parametric adaptability.

## Funnel Application

The robot picks up the funnel from the designated funnel platform and starts the insertion process. With the help of the FT sensor, it lowers the funnel until its end touches the stator, thus ensuring precise vertical alignment through force feedback. Subsequently, the robot continues with horizontal insertion, bringing slot profiles of the funnel and stator into perfect alignment and positioning the rear end of the funnel firmly against the stator to ensure correct axial placement. The insertion force is continuously monitored, and when a predefined threshold is reached, signaling that the funnel is fully seated, the gripper releases it, completing the process and preparing for the insertion of the slot liner. This method enables repeatable and precise placement of the funnel on a wide variety of stator designs irrespective of the height or width.

## Slot Liner Positioning and Partial Insertion

With the funnel in place, the robot moves to the slot liner platform to pick up a slot liner. It then aligns the slot liner precisely with the funnel inlet and initiates the insertion. The slot liner is pushed in until the gripper contacts the front opening of the funnel, achieving almost three-quarters of the total insertion depth. At this point, the gripper releases the slot liner, which remains partially inserted in the stator slot, with a portion protruding slightly from the funnel’s opening. The robot then retracts to initiate the funnel removal process.

## Final Liner Insertion

Once the partial insertion is completed, the robot regrasps the funnel and retracts it from the stator. After the funnel is fully removed, the robot repurposes it as a pushing tool to complete the liner insertion. By applying gentle forward pressure with the funnel, the robot ensures that the slot liner is fully seated and flush with the stator surface. This final step confirms proper alignment and secure placement of the liner, completing the automated insertion process. The motor-driven clamp then rotates the stator to align the next slot for insertion, enabling continuous and automated processing of all stator slots. The complete slot liner insertion procedure is illustrated in figure 8.A diagram of a flowchart

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Fig. 16. Process Pipeline: The slot liner insertion process follows a structured pipeline divided into two main phases. The first focuses on inserting the funnel and the second handles slot liner insertion. The pipeline is repeated in coordination with clamp rotation to insert slot liners into each stator slot.

## UR Script Based Insertion Control

# Tool Process Testing and Validation

To evaluate the effectiveness of the proposed funnel design and automated insertion process, a series of insertion tests were performed on two stators with different geometries - namely, slot height and number of slots. One had a height of 20 mm with 36 slots, while the other had a slot height of 22 mm with 48 slots. For ease of reference, the stator with the slot height of 20 mm is referred to as stator A and the one with the slot height of 22 mm as stator B. The tests used polyester fleece slot liners which were impregnated on both sides. For each stator, the funnel design was parametrically adapted to the respective slot configuration. These customized funnel variants were then produced using 3D printing and integrated into the test setup. The slot angle (85°) and slot width (8 mm) remained the same for both stators, as the inner diameter of the stator changes. After each insertion cycle, the motorized clamp rotates the stator to align the next slot for insertion. For the stator with 36 slots, the clamp rotates in 10° increments, while for the one with 48 slots, it rotates in 7.5° increments.

## A group of green and orange pie charts AI-generated content may be incorrect.Testing results

Fig. 17 Preliminary and optimized trials for stator A and B. Each stator underwent 40 Preliminary trials and 60 Optimized trials.

The reliability and repeatability of the slot liner insertion process were evaluated through a total of 200 insertion tests on the two stators. Both the Stators underwent 100 trials each, which includes 40 preliminary trials and 60 optimized trials. During all tests, the success rates, the occurrence of defects, and the corresponding failure modes were documented. The average process cycle time was measured at 39.8 seconds at 30% speed, despite the lack of path planning or motion optimization.

## Stator A

For stator A, results summarized in figure 9 indicate an improvement in success rate from 80% in the preliminary phase to 97% following the applied process optimizations. A total of eight errors were identified during the preliminary tests. Six of these were caused by the slot liner being pulled back together with the funnel during funnel extraction. The two remaining errors were caused by the improper placement of the slot liner on the insertion platform, which led to misalignment during insertion. An overview of the error distribution can be seen in figure 10.A graph of a bar chart

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Fig. 18 Error Frequency and causes in the preliminary trials for stator A. The slot liner being pulled back with the funnel accounted for 6 errors whereas slot liner misplacement caused 2 errors.

To improve insertion reliability and eliminate the observed failure modes, several corrective measures were implemented. Firstly, the insertion procedure was standardized to ensure precise gripping and consistent alignment of the slot liners. Next, the insertion depth was increased by using the inner finger of the gripper to push the slot liner deeper into the funnel before pulling the funnel out. This technique reduced friction when retracting the funnel and improved the overall quality of the insertion. Finally, the funnel removal motion was changed from a continuous pull to a start-stop sequence. Continuous retraction often caused the funnel to become stuck or dislodge the partially inserted liner. In contrast, withdrawing the funnel in small increments reduced the likelihood of the liner being pulled back, thereby improving consistency and success rates.

After implementing these changes, the optimized test runs were carried out, which led to an increase in the success rate from 80 % to 97 %. Although the error of the slot liner being pulled back with the funnel was significantly reduced, it was not eliminated, resulting in a residual 3% error.

## Stator B

Stator B, which has a slightly larger slot height of 22 mm, was also subjected to a total of 100 insertion attempts. The increased slot height results in a slight narrowing at the upper end of the slot, making the insertion process more sensitive to the profile of the slot liner and its alignment. A total of 10 errors were identified in the preliminary tests. Of these, 9 were attributed to improper insertion. During the initial runs, the slot liners often failed to enter the slot correctly, primarily due to the slot liners not conforming to the required slot profile. One additional error occurred due to misalignment of the funnel on the platform; the graphical representation of the errors can be seen in figure 11. Care was taken to ensure that the slot liners remained consistently aligned during each test. A success rate of 77% was achieved in the preliminary tests. A graph with blue bars

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Fig. 19 Fig. 11. Error frequency and causes in the preliminary trials for stator B. Poor slot liner profile accounted for the most number of errors.

In the optimized phase, the same improvements as for Stator A, such as discontinuous retraction and deeper insertion with the gripper were applied. Interestingly, the problem observed in earlier tests with Stator A, where the slot liner was pulled back with the funnel during retraction, did not occur at all with Stator B. This may be explained not only by the optimizations made, but possibly also due to the narrower upper part of the slot, which allowed the slot liner to sit more securely and resist displacement when the funnel was retracted. In addition, repeated trials and controlled folding techniques resulted in improved profiles of the slot liner, which played a crucial role in improving insertion performance. The improved geometry and consistent alignment significantly increased the insertion success rate to 97 %, confirming the effectiveness of the optimizations made for the more geometrically constrained slots of stator B.

# Result Discussion

The process for inserting the slot liners was validated on two stators with different configurations: Stator A with 36 slots and Stator B with 42 slots. This means that for each complete stator, either 36 or 42 successful insertions are required to achieve complete slot lining. One of the most important results of this validation was the 97 % success rate in the optimized tests for both the stators, demonstrating a high degree of repeatability and process reliability. Compared to conventional, fully manual insertion methods, the robot-assisted approach offers several advantages.

The robot-assisted assembly significantly reduces labor and associated costs. Once optimized, the automated process also ensures consistent placement performance, thus minimizing the variability and human error that occur with manual operations. Furthermore, the system has demonstrated high flexibility and can be effectively adapted to different stator types without the need for specialized machines for each variant. This adaptability simplifies logistics and reduces investment costs, creating a scalable solution for diverse manufacturing requirements. By minimizing or eliminating manual intervention during placement, this approach increases workplace safety and reduces the risk of operator injury and fatigue. However, a key drawback to the process is the sensitivity of the process to the slot liner’s profile and condition. During the preliminary trials with Stator B, the slot liners were insufficiently pre-folded, leading to several insertion errors due to improper profiles. This highlights the need for either precisely preformed slot liners or a pre-treatment step to ensure uniform geometry prior to robot-assisted insertion.

In terms of cycle time, the process currently runs at a constant duration of 39.8 seconds per insertion operation. It should be noted that no specific optimization of the process, path planning or timing has been carried out. With appropriate motion planning and trajectory optimization, significant reductions in cycle time can be achieved, thereby improving throughput and production efficiency.

In summary, robot-assisted insertion of slot liners using a parametric funnel has great potential as a scalable, flexible, and cost-effective solution. With minor improvements in the preparation of the slot liners and optimization of cycle times, it can serve as a robust alternative to conventional manual methods in stator assembly.

# Outlook

The Parametric slot liner insertion process has proven to be very promising, as it has a high success rate and can be adapted to different Stator types. However, the current system does not automate the entire preparation cycle for slot liners – in particular, grooving, folding, and cutting. By integrating pre-folding tools and a slot lining dispenser mechanism, robustness and consistency could be significantly improved and a fully automated workflow enabled. These additions would reduce dependence on manual preparation steps and improve process reliability, especially when working with non-pre-folded inserts.

To further reduce errors, a simple image-based quality control system could be introduced to verify the alignment and profile of each slot liner before insertion. This could be enhanced by AI-powered vision systems and machine learning, allowing real-time detection of profile deviations or misalignments and dynamic adjustment of insertion paths. Altogether, expanding the system with pre-processing automation, vision-based inspection, and intelligent feedback mechanisms would transform the current setup into a more autonomous, scalable, and efficient solution suitable for industrial applications.

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