

# EV Battery Cell. Technical data

## 31 Ah NMC Li-ion cell specifications

- Nominal Capacity = 31 Ah
- Nominal Voltage = 3.7 V
- Voltage range = 3.4 V - 4.2 V
- Nominal energy capacity = 114.7Wh
- Series resistance = 3.6 m $\Omega$

## Operating temperatures

- Charge = 0°C / +40°C
- Discharge = -20°C / + 60°C

## Dimensions

- Thickness = 8.4 mm
- Width = 215 mm
- Length = 220 mm
- Weight 1 kg

## EV Battery Pack. Technical data

### Configuration:

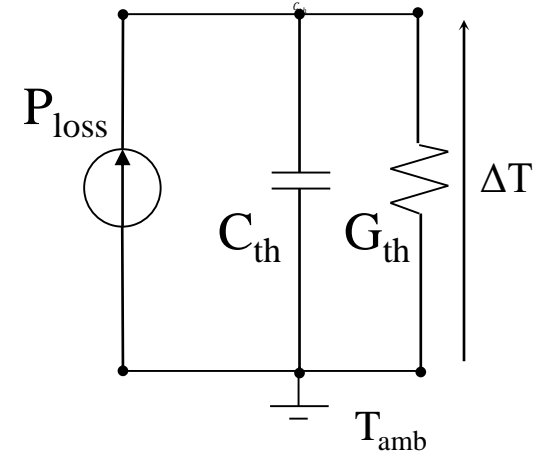
- 100 cells in series, 3 branches in parallel (100S-3P)
- Total number of cells: 300
- DC Round trip efficiency RTE = 94%

### First calculations

- Nominal Capacity = 93 Ah
- Nominal Voltage = 370 V
- Nominal energy capacity = 34,4kWh
- Equivalent series resistance = 120 m $\Omega$
- Net weight (only cells) = 300kg

# Thermal model of battery pack

- Cell specific heat
  - $C_p = 800 \text{ J/kg K}$
- Battery thermal capacity
  - $C_{th} = 800 \text{ J/kg K} \times 300\text{kg} = 240\text{kJ/K}$



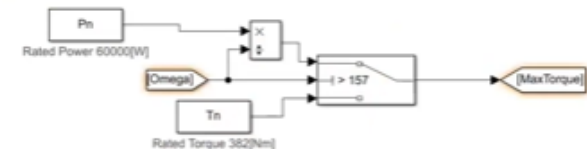
Two cooling methods are possible:

- air cooling and liquid cooling (more efficient)
- The same heat exchange area is chosen for both cooling methods =  $0.5\text{m}^2$
- Air convection coefficient  $K_{th-air} = 200 \text{ W/m}^2 \text{ K}$
- Glycol convection coefficient  $K_{th-glyc} = 2000 \text{ W/m}^2 \text{ K}$
- Air convection  $G_{th-a} = K_{th-air} \times 0.5\text{m}^2 = 100 \text{ W/K}$
- Glycol convection  $G_{th-g} = K_{th-glyc} \times 0.5\text{m}^2 = 1000 \text{ W/K}$

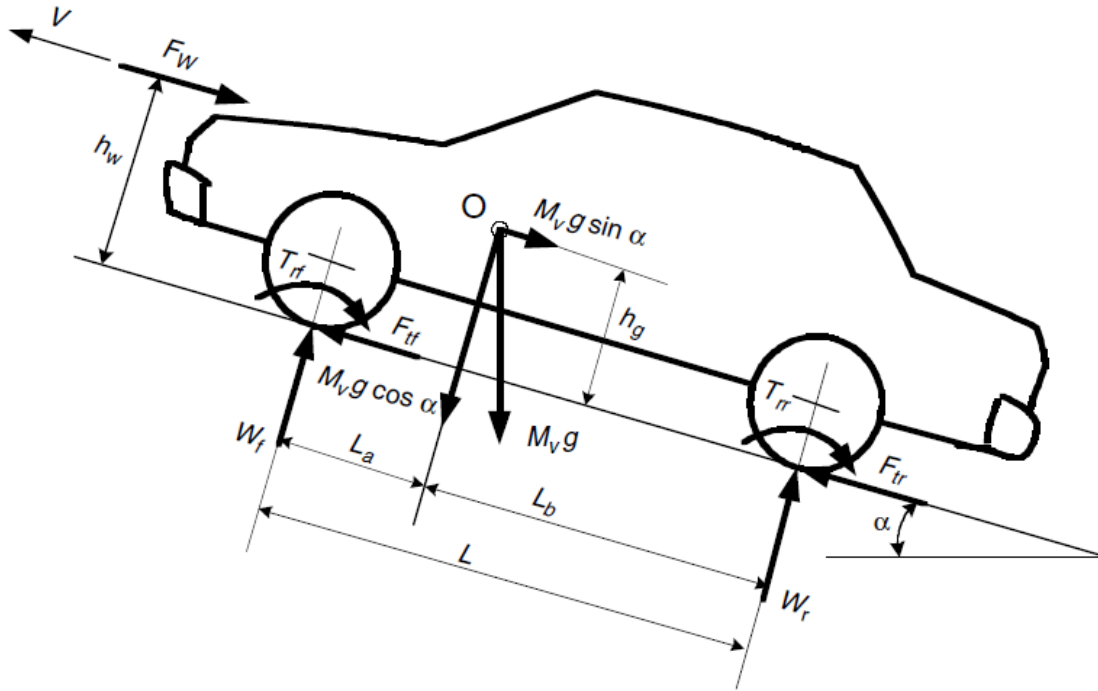
$$\Delta T = \frac{1}{C_{th}s + R_{th}} P_{loss}$$

# Vehicle data

- Average Kerb Weight = 1500 kg
- DC link battery voltage = 370 V
- Tank-to-Wheel efficiency = 80%
- Regenerative braking percentage = 50%
- Rolling resistance coefficient  $f_v$ , tire on road = 0.02
- Shape coefficient  $c_v$  = 0.29
- Vehicle frontal area = 2.38 m<sup>2</sup>
- Wheel radius = 0.35m
  
- The EV is equipped with a 60kW electric motor
  
- The kerb weight refers to the car loaded with all the fluids for its operation plus the weight of an average driver.
- The Tank-to-Wheel (T2W) efficiency takes into account the mechanical transmission, the electric motor and the inverters.
- Mechanical transmission has only one gear.
  - Transmission ratio  $k_t = N_{\text{motor}}/N_{\text{wheel}} = 5$

$$\text{Power} = 382\text{Nm} \times 157 \text{ rad/s} = 60\text{kW}$$


# Calculation of electric power $P_e$



## Forces acting on vehicle

In this exercise the grading resistance is neglected, assuming  $\alpha=0$

An additional constant load of **800W** has to be added to account for the power of the auxiliaries, such as heater or air conditioning

$$R_{rolling} = f_v \cdot m \cdot g$$

$$R_{aerodynamic} = \frac{1}{2} \rho_{air} \cdot A_{vehicle} \cdot v^2 \cdot c_v$$

$$P_r = F_T \cdot v = (R_{rolling} + R_{aerodynamic}) \cdot v$$

$$P_m = P_r + m \cdot a \cdot v$$

$$P_e = P_m / \eta_{T2W}$$

Mass  $m = 1500$  kg

Tank-to-Wheel efficiency  $\eta_{T2W} = 80\%$

Max Regenerative braking current = C2

Rolling resistance coefficient  $f_v = 0.02$  pu

Shape coefficient  $c_v = 0.29$  pu

Vehicle frontal area  $A_{vehicle} = 2.38$  m<sup>2</sup>

Gravity acceleration  $g = 9.81$  m/s<sup>2</sup>

Air density  $\rho_{air} = 1.2$  kg/m<sup>3</sup>

# Simulations required

## Slow charge

A 7.2kW single phase rectifier (OBC = on board battery charger) charge the battery at approximately C4, with a current equal to one quarter of capacity, up to a SoC = 90%, starting from SoC = 20%



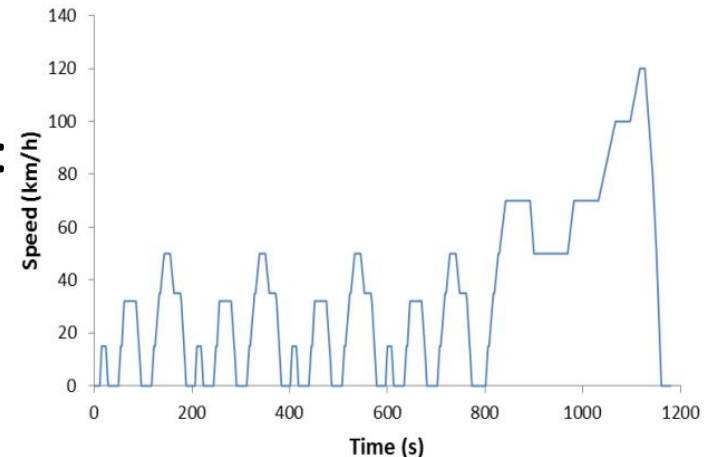
## Fast charge

A 50kW three phase rectifier (converter located in the external charger, EVSE = EV Supply Equipment) charge the battery at approximately 1.5C for 20 minutes, starting from SoC = 20%

## Driving session, two NEDC cycles

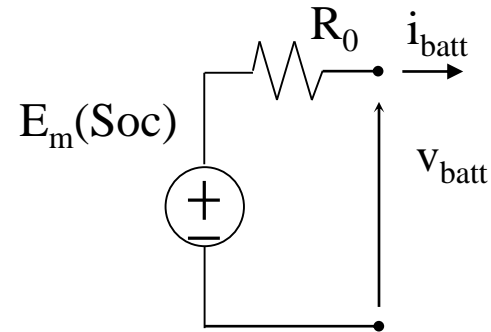
Calculate and draw the curves vs time of:

- Energy consumption
- Battery temperature
- SoC

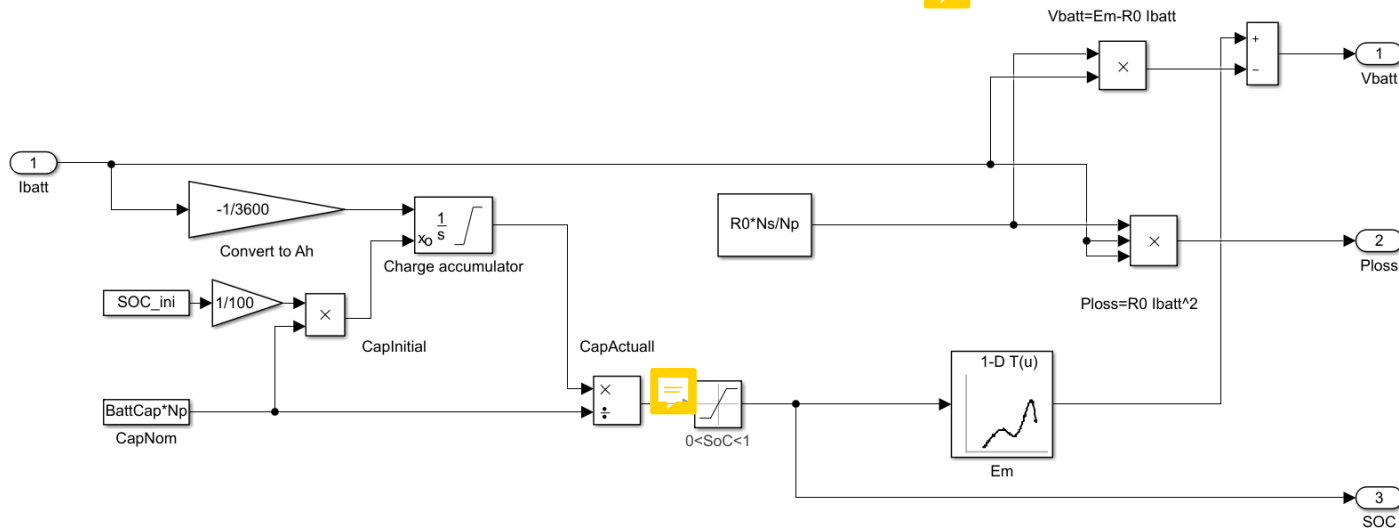
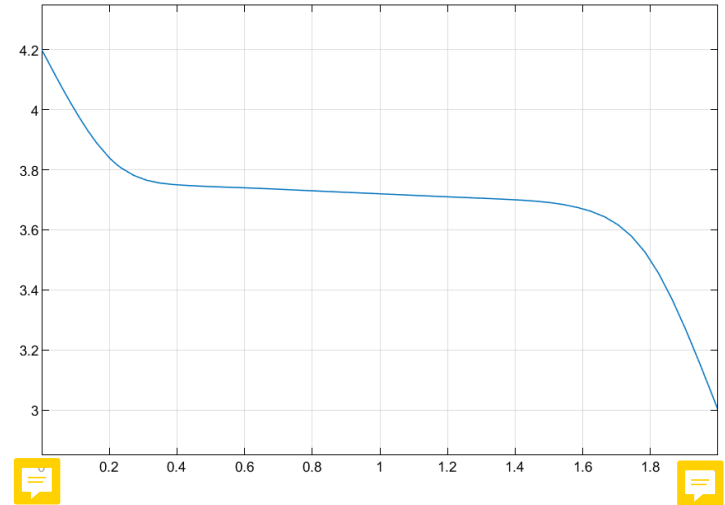


# Slow charge

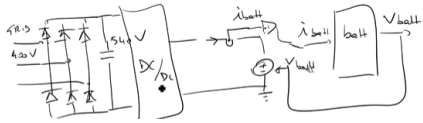
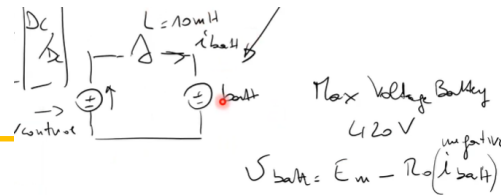
- Simple Battery model
  - No dependency on the temperature



$E_m(\text{SoC})$ : single module  
 $R_0 = 3.6 \text{ m}\Omega$



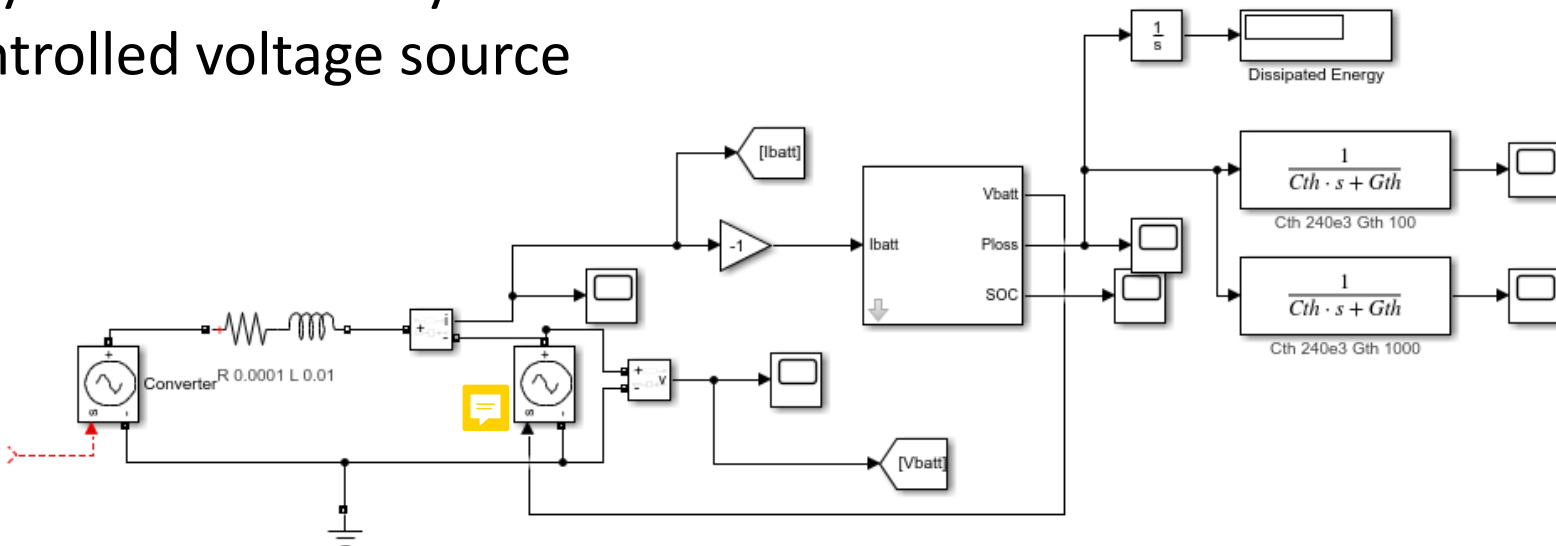
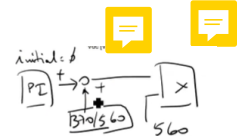
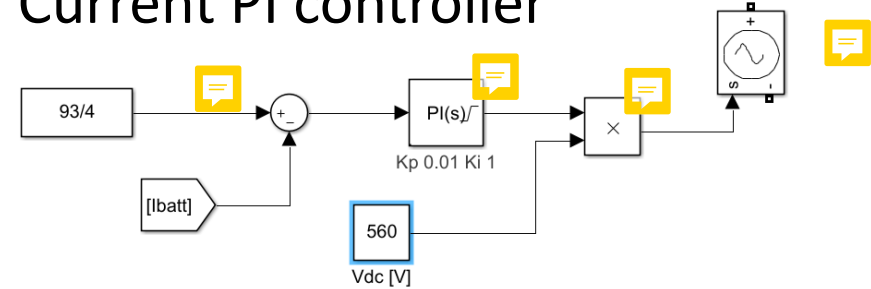
# Slow charge



Between the converter and the battery an de-coupling inductor is required (i.e. 10mH)

The converter and the battery may be simulated by means of a controlled voltage source

## Current PI controller

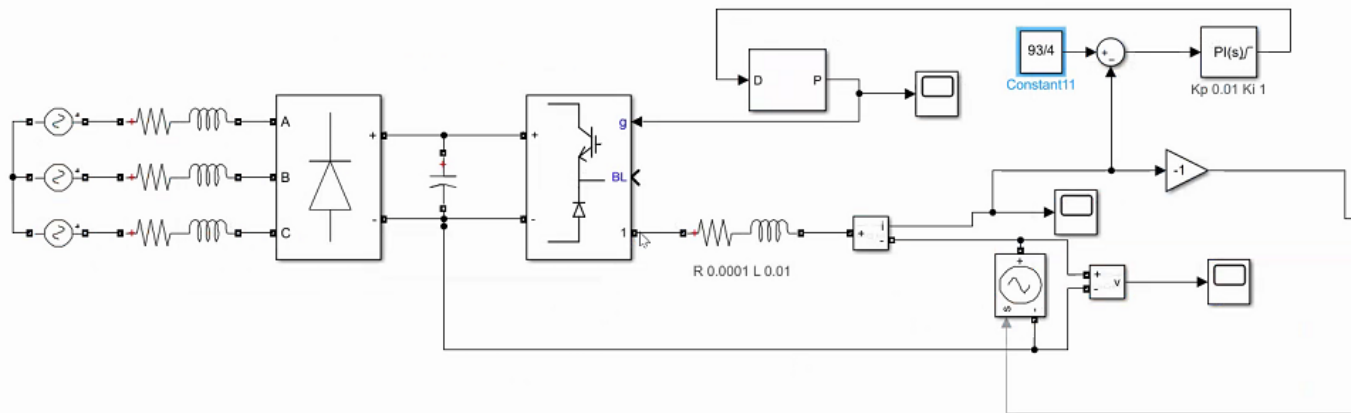




# Fast charge





- Similar to Slow charge




## Driving cycle

The speed controller requires a torque. In order to find the battery current, an energy balance may be applied, taking into account the Tank-to-Wheel ( $\eta_{T2W}$ ) efficiency = 80%.

$\eta_{T2W}$  is the product of the efficiency of the mechanical load  $\eta_{mech}$  and of the electrical devices (machine and converter)  $\eta_{el}$ . Suppose  $\eta_{el}=97\%$ . Therefore,  $\eta_{mech} = 82.5\%$  

The battery power  $P_{batt}$  is  $V_{batt} \times I_{batt}$  while the mechanical power at the motor shaft  $P_e$  is  $T_e \times \Omega_m$ . During motor operation, the  $P_{batt}=P_{aux}+P_e/\eta_{el}$ . During braking operation, the  $P_{batt}=P_e \times \eta_{el}-P_{aux}$  

Calculate and draw the curves vs time of: 

- Energy consumption
- Battery temperature
- SoC 

# Driving cycle: Open loop approach



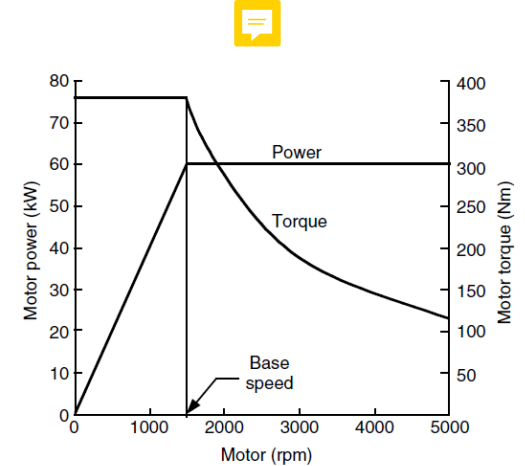
NEDC cycle gives speed  $v$  and acceleration  $a$

- $R_{rolling} = f_v \cdot m \cdot g$
- $R_{aerodynamic} = \frac{1}{2} \rho_{air} \cdot A_{vehicle} \cdot v^2 \cdot c_v$
- $P_r = F_T \cdot v = (R_{rolling} + R_{aerodynamic}) \cdot v$
- $P_m = P_r + m \cdot a \cdot v$
- If  $P_m > 0$  then  $P_e = P_m / \eta_{T2W}$  else  $P_e = P_m \cdot \eta_{T2W}$
- $P_{batt} = P_e + 800W$
- $I_{batt} = P_{batt} / V_{batt}$
- The battery model returns the new value of  $V_{batt}$ , SoC and Power Losses in the battery

# Driving cycle: Closed-loop approach

NEDC cycle gives speed reference  $v_{ref}$  ( $v$  is the actual speed)

- A linear speed controller (PI) asks for an electromagnetic torque reference
- It is limited to the maximum torque given by the operating regions (The curve of negative torque is mirrored from the positive one)
- $\Omega_m = v / \text{radius} \times \text{TransmissionRatio} = v \times k_{tr}$
- $T_e \times \Omega_m$  is the electromagnetic power  $P_{em}$
- If  $P_{em} > 0$  then  $P_e = P_{em} / \eta_{el}$  else  $P_e = P_{em} \cdot \eta_{el}$
- $P_{batt} = P_e + 800W$
- $I_{batt} = P_{batt} / V_{batt}$
- The battery model returns the new value of  $V_{batt}$ , SoC and Power Losses in the battery



# Driving cycle: Closed-loop approach

Towards the mechanical load:

- $R_{rolling} = f_v \cdot m \cdot g$
- $R_{aerodynamic} = \frac{1}{2} \rho_{air} \cdot A_{vehicle} \cdot v^2 \cdot c_v$
- $F_T = R_{rolling} + R_{aerodynamic}$

The electromagnetic force  $F_e$ , taking into account the mech. efficiency is:

- If  $T_e > 0$  then  $F_e = k_{tr} T_e \cdot \eta_{mech}$  else  $F_e = k_{tr} T_e / \eta_{mech}$
- $a = \frac{1}{m} (F_e - F_T)$
- $v = \int a \cdot dt$

I used, for the speed controller,  $K_p=1$  and  $K_i=100$ , saturation between -1 and 1, output gain=328Nm

# Some results

- Starting from 100% of SoC. Total distance 22km

