
ASEN 2004

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% Using thermodynamic and aerodynamic relations, and equations of
motion, determine
% the trajectory of a bottle rocket with specified initial properties

% wind (+/- 11.25 degrees from SW), (+/- .1 m/s wind speed)
% mass (+/- .5 gram), launchpad angle (+/- 1 degree)
% bottle diameter (+/- .1 cm), bottle throat (+/- .1 cm)
% pressure (+/- 3447.38 Pa)

% Assumptions
% Steady, uniform 1D flow, only 2D required, Ideal weather + Gas,
% Compressible within the bottle (two densities)

g = 9.81; % [m/s^2]
C_discharge = 0.8; % discharge coefficient
rho_amb = 0.961; % kg/m^3 ambient air density
Vol_bottle = 0.002; % m^3 volume of empty bottle
P_amb = 83426.56; % Pa atmospheric pressure
gamma = 1.4; % ratio of specific heats for air
rho_water = 1000; % kg/m^3 density of water
R = 287; % J/kgK gas constant of air
M_bottle = 0.160; % kg mass of empty 2 litre bottle with cones and
fins
T_airI = 290.372; % K initial temperature of air
v0 = 0.0; % m/s initial velocity of rocket
x0 = 0.0; % m initial horizontal displacement
y0 = 0.0; % m initial lateral displacement
z0 = 0.25; % m initial vertical displacement
l_s = 0.5; % m length of test stand
tspan = [0 5]; % integration time
windspeed = 3.57632; % m/s
windangle = deg2rad(45); % radians

% After meeting the verification requirements, I begin to try test
cases
% make 1 true and all others false to see associated graph
% Verification case on by default
verification = true;

if (verification == true)
    P_gage = 275790; % initial gage pressure of air in bottle
    Vol_waterI = .6/rho_water; % m^3 initial volume of water inside
    bottle
    C_drag = 0.30; % drag coefficient
    theta = deg2rad(45); % radians initial angle of rocket

    D_throat = 2.1; % cm diameter of the throat
    D_bottle = 10.5; % cm diameter of bottle
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A_t = pi * (D_throat/200)^2; % m^2 area of throat
A_B = pi * (D_bottle/200)^2; % m^2 cross sectional area of bottle

% determining rocket mass
P_airI = (P_gage + P_amb);
rho_air_bottleI = P_airI ./ (R .* T_airI);
M_waterI = (Vol_waterI .* rho_water);
Vol_airI = (Vol_bottle - Vol_waterI);
M_airI = (P_airI .* Vol_airI)./(R .* T_airI);
RMI = M_bottle + M_waterI + M_airI;

X0 = [x0,y0,z0,v0,v0,v0,RMI,M_airI,Vol_airI];

opt = odeset('Events', @stopEvent);
[t, X] = ode45(@(t,x)
odeFun(t,x,g,C_discharge,rho_amb,Vol_bottle,P_amb,gamma,rho_water,A_t,R,C_drag,T_
tspan, X0, opt);
figure
plot3(X(:,1),X(:,2),X(:,3))
grid on
title("Rocket Trajectory")
xlabel("Downrange [m]")
ylabel("Crossrange [m]")
zlabel("Height [m]")
hold off
endpoint = [X(end,1),X(end,2)]
simulationM(100, endpoint)
end

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Function propagation

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function [value, isterminal, direction] = stopEvent(t,X)
    value = (X(3) <= 0);
    isterminal = 1;
    direction = 0;
end
function dx =
odeFun(t,x,g,C_discharge,rho_amb,Vol_bottle,P_amb,gamma,rho_water,A_t,R,C_drag,T_
    % must split into three parts, as there are three sections of
    flight
    % Part 1 is powered (water exhaust), so drag + thrust(water) +
    gravity
    % Part 2 is also powered (air exhaust), so drag + thrust(air) +
    gravity
    % Part 3 is unpowered, so just drag + gravity
    xpos = x(1);
    ypos = x(2);
    zpos = x(3);
    Vx = x(4);
    Vy = x(5);
    Vz = x(6);
    RM = x(7);

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AM = x(8);
AV = x(9);

% Part 1
if (AV < Vol_bottle)
    % calculating change in volume of air over time
    AVdot = C_discharge .* A_t .* sqrt((2./rho_water) .*
((P_airI .* (Vol_airI./AV).^gamma) - P_amb));
    % calculating current pressure based on volume
    P_air = P_airI .* (Vol_airI./AV).^gamma;
    % calculating change in mass of the rocket over time
    RMDot = -C_discharge .* A_t .* sqrt(2 .* rho_water .* (P_air -
P_amb));
    % with P_air we can now calculate the force from thrust
    F_t = 2 .* C_discharge .* A_t .* (P_air - P_amb);
    % change in air mass is zero because of phase of flight
    AMdot = 0;
else
    % set pressure and temperature to fixed values after all water
is
    % expelled (AV >= Vol_bottle) && (P_air > P_amb)
    % calculating pressure at end of part 1
    P_air_end = P_airI .* (Vol_airI./Vol_bottle).^gamma;
    % calculating temperature at the end of part 1
    T_air_end = T_airI .* (Vol_airI./Vol_bottle).^(gamma-1);
    % Air pressure now changes (no water left in the bottle)
    % calculating new pressure
    P_air = P_air_end .* (AM./M_airI).^gamma;
end

% Part 2
if (AV >= Vol_bottle) && (P_air > P_amb)
    % Calculating air density/temperature
    rho_air_bottle = AM./Vol_bottle;
    T_air = P_air ./ (rho_air_bottle .* R);
    % determining whether choked flow, need critical pressure
    P_crit = P_air .* (2 ./ (gamma + 1)).^(gamma./(gamma-1));
    if (P_crit > P_amb)
        % flow is choked, determine exit velocity
        % need temperature at exit
        T_exit = T_air .* (2./(gamma+1));
        % calculating exit velocity
        V_exit = sqrt(gamma .* R .* T_exit);
        % air pressure at exit is just critical pressure
        P_exit = P_crit;
        % calculating air density at exit
        rho_air_exit = P_exit ./ (R .* T_exit);
    elseif (P_crit < P_amb)
        % solve for exit mach speed through pressure relation
        Mach_exit = sqrt((((P_air./P_amb).^(gamma-1))./(
gamma))-1)./((gamma-1)./2));
        % calculating temperature of air at exit
        T_exit = T_air ./ (1 + (((gamma-1)./2) .*
(Mach_exit.^2)));

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        % air pressure at exit is just ambient pressure
        P_exit = P_amb;
        % calculating density at exit
        rho_air_exit = P_exit ./ (R .* T_exit);
        % now we can calculate exit velocity
        V_exit = Mach_exit .* sqrt(gamma .* R .* T_exit);
    end
    % thrust, air mass, and rocket mass change by the same
functions
    % calculating change in air mass
    AMdot = -C_drag .* rho_air_exit .* A_t .* V_exit;
    % calculating thrust
    F_t = (-AMdot) .* V_exit + ((P_amb - P_exit) .* A_t);
    % Calculating change in rocket mass (same as change in air
mass)
    RMdot = AMdot;
    % Air volume is unchanging during this phase
    AVdot = 0;
end

% Part 3
if (AV >= Vol_bottle) && (P_air <= P_amb)
    % no water or air exhaust thrust
    F_t = 0;
    AVdot = 0;
    % Change in air mass is zero, as pressure has equalized
    AMdot = 0;
    % change in mass is zero (again no exhaust and pressure
equalized)
    RMdot = 0;
end

%     if (zpos < 5)
%
%     elseif (zpos <= 22 && zpos > 3)
%
%         windx = (zpos/22 * windspeed) * sin(abs(deg2rad(40) -
windangle));
%         windy = (zpos/22 * windspeed) * cos(abs(deg2rad(40) -
windangle));
%
%         Vx = Vx - windx;
%         Vy = Vy - windy;
%
%         hx = (Vx)./sqrt((Vx.^2) + (Vz.^2) + (Vy.^2));
%         hz = (Vz)./sqrt((Vx.^2) + (Vz.^2) + (Vy.^2));
%         hy = (Vy)./sqrt((Vx.^2) + (Vz.^2) + (Vy.^2));
%     else
%
%     end

    % initial heading is determined by test stand
    % so we have to check whether its cleared the stand yet (using
trig)

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    % if (sqrt(((zpos - z0)^2) + ((xpos - x0)^2)) <= l_s)
    if (xpos < (l_s .* cos(theta) + x0) && zpos < (l_s .* sin(theta) +
z0) && t < 2)
        % once it has cleared the stand, heading is determined by
velocity
        % components
        hx = cos(theta);
        hz = sin(theta);
        hy = 0;
    elseif (zpos <= 22 && zpos >= (l_s .* sin(theta) + z0))
        windx = (zpos./22)*windspeed * sin(abs(deg2rad(40) -
windangle));
        windy = (zpos./22)*windspeed * cos(abs(deg2rad(40) -
windangle));

        Vx = Vx - windx;
        Vy = Vy - windy;
        hx = (Vx)./sqrt((Vx.^2) + (Vz.^2) + (Vy.^2));
        hz = (Vz)./sqrt((Vx.^2) + (Vz.^2) + (Vy.^2));
        hy = (Vy)./sqrt((Vx.^2) + (Vz.^2) + (Vy.^2));
    else
        windx = windspeed * sin(abs(deg2rad(40) - windangle));
        windy = windspeed * cos(abs(deg2rad(40) - windangle));

        Vx = Vx - windx;
        Vy = Vy - windy;
        hx = (Vx)./sqrt((Vx.^2) + (Vz.^2) + (Vy.^2));
        hz = (Vz)./sqrt((Vx.^2) + (Vz.^2) + (Vy.^2));
        hy = (Vy)./sqrt((Vx.^2) + (Vz.^2) + (Vy.^2));
    end

    % velocity vector is just combination of components
V = sqrt((Vx.^2) + (Vz.^2) + (Vy.^2));

    % Since drag force is a simple function of area and velocity, it
can
    % be calculated outside of the individual parts

    % Calculating drag:
F_d = (1/2) .* rho_amb .* V^2 .* C_drag .* A_B;

    % Now, we have all forces responsible for motion
    % We can now determine the acceleration components which govern
    % trajectory:
accelX = ((F_t .* hx) - (F_d .* hx)) ./ RM;
accelZ = ((F_t .* hz) - (F_d .* hz) - (RM .* g)) ./ RM;
accelY = ((F_t .* hy) - (F_d .* hy)) ./ RM;

    % final outputs for state vector
dx = [Vx; Vy; Vz; accelX; accelY; accelZ; RMdot; AMdot; AVdot];
end
function [] = simulationM(N, endpoint)
    % constants

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g = 9.81; % [m/s^2]
C_discharge = 0.8; % discharge coefficient
rho_amb = 0.961; % kg/m^3 ambient air density
Vol_bottle = 0.002; % m^3 volume of empty bottle
P_amb = 83426.56; % Pa atmospheric pressure
gamma = 1.4; % ratio of specific heats for air
rho_water = 1000; % kg/m^3 density of water
R = 287; % J/kgK gas constant of air
M_bottle = 0.16; % kg mass of empty 2 litre bottle with cones and
fins
T_airI = 290.372; % K initial temperature of air
v0 = 0.0; % m/s initial velocity of rocket
x0 = 0.0; % m initial horizontal displacement
y0 = 0.0; % m initial lateral displacement
z0 = 0.25; % m initial vertical displacement
l_s = 0.5; % m length of test stand
tspan = [0 5]; % integration time

% mass
mp = .6 + 0.005*randn(N,1);
ms = M_bottle + 0.005*randn(N,1);

% bottle geometry
D_throat = 2.1 + 0.1 * randn(N,1); % cm diameter of the throat
D_bottle = 10.5 + 0.1 * randn(N,1); % cm diameter of bottle
A_t = pi .* (D_throat./200).^2; % m^2 area of throat
A_B = pi .* (D_bottle./200).^2; % m^2 cross sectional area of
bottle

% environment (wind)
windspeed = 3.57632 + 0.1*randn(N,1); % m/s
windangle = deg2rad(45 + 11.25*randn(N,1)); % radians

P_gage = 275790 + (3447 * randn(N,1)); % initial gage pressure of
air in bottle
Vol_waterI = mp./rho_water; % m^3 initial volume of water inside
bottle
C_drag = 0.30; % drag coefficient
theta = deg2rad(45 + randn(N,1)); % radians initial angle of
rocket

% determining rocket mass
P_airI = (P_gage + P_amb);
rho_air_bottleI = P_airI ./ (R .* T_airI);
M_waterI = (Vol_waterI .* rho_water);
Vol_airI = (Vol_bottle - Vol_waterI);
M_airI = (P_airI .* Vol_airI)./(R .* T_airI);
RMI = ms + M_waterI + M_airI;

opt = odeset('Events', @stopEvent);

% vectors to fill with final landing values

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Lx = zeros();
Ly = zeros();
figure
for i = 1:N
    X0 = [x0,y0,z0,v0,v0,v0,RMI(i),M_airI(i),Vol_airI(i)];
    [t, X] = ode45(@(t,x)
odeFun(t,x,g,C_discharge,rho_amb,Vol_bottle,P_amb,gamma,rho_water,A_t(i),R,C_drag
tspan, X0, opt);
    plot3(X(:,1),X(:,2),X(:,3))
    hold on
    title("Monte Carlo Analysis")
    xlabel('Downrange [m]')
    ylabel('Crossrange [m]')
    zlabel('Height [m]')
    zlim([0 30]);
    grid on;

    Lx(i) = X(end,1);
    Ly(i) = X(end,2);
end
hold off

% plotting error ellipses
figure; plot(Lx,Ly,'k.','markersize',6)
axis equal; grid on; xlabel('x [m]'); ylabel('y [m]'); hold on;
plot(endpoint(1),endpoint(2),'r','markersize',6)
title("Error Analysis")

% Calculate covariance matrix
P = cov(Lx,Ly);
mean_x = mean(Lx);
mean_y = mean(Ly);

% Calculate the define the error ellipses
n=100; % Number of points around ellipse
p=0:pi/n:2*pi; % angles around a circle

[eigvec,eigval] = eig(P); % Compute eigen-stuff
xy_vect = [cos(p'),sin(p')] * sqrt(eigval) * eigvec'; %
Transformation
x_vect = xy_vect(:,1);
y_vect = xy_vect(:,2);

% Plot the error ellipses overlaid on the same figure
plot(1*x_vect+mean_x, 1*y_vect+mean_y, 'b')
plot(2*x_vect+mean_x, 2*y_vect+mean_y, 'g')
plot(3*x_vect+mean_x, 3*y_vect+mean_y, 'r')
hold off
end

endpoint =

67.3407    -7.6032

```

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