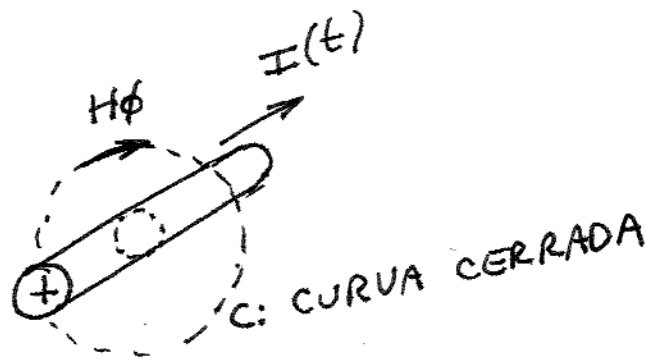
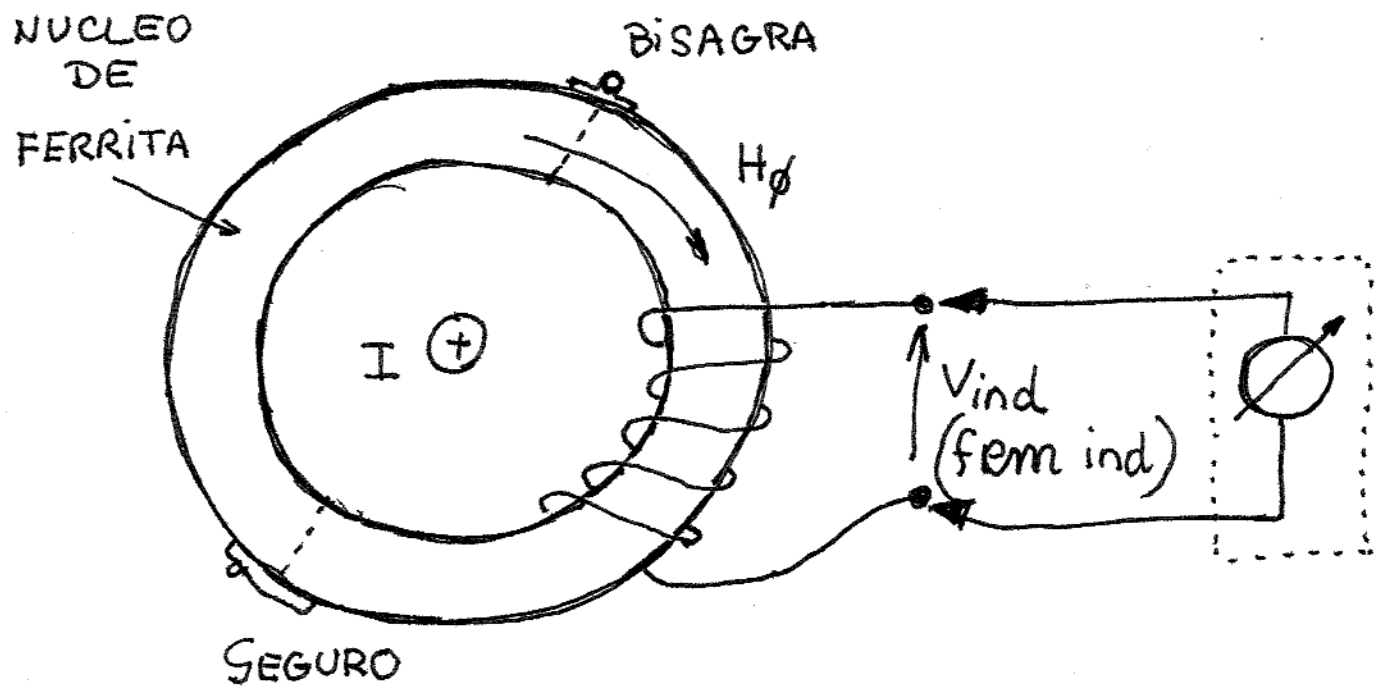


PUNTA DE CORRIENTE



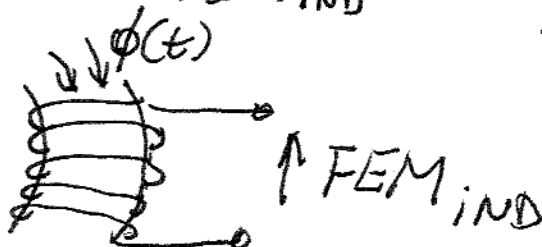
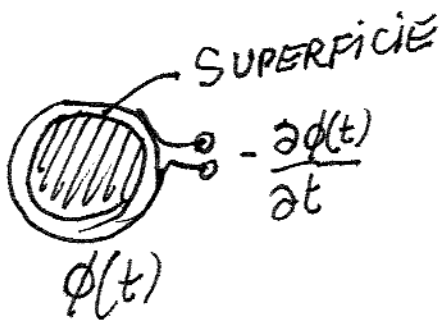
LEY DE AMPERE

$$\oint_C \vec{H} \cdot d\vec{l} = \int_S \vec{J} \cdot d\vec{S} + \int_S \frac{d\vec{D}}{dt} \cdot d\vec{S}$$

LEY DE FARADAY

~~XXXXXX~~

$$FEM_{ind} = - \frac{\partial \phi}{\partial t}$$



IMPEDANCIA DE TRANSFERENCIA

$$Z_T = \frac{V_{ind}}{I}$$

SE OBTIENE UNA
CURVA DE CALIBRACIÓN
 $Z_T(frec)$

I : CORRIENTE A MEDIR (CONOCIDA)

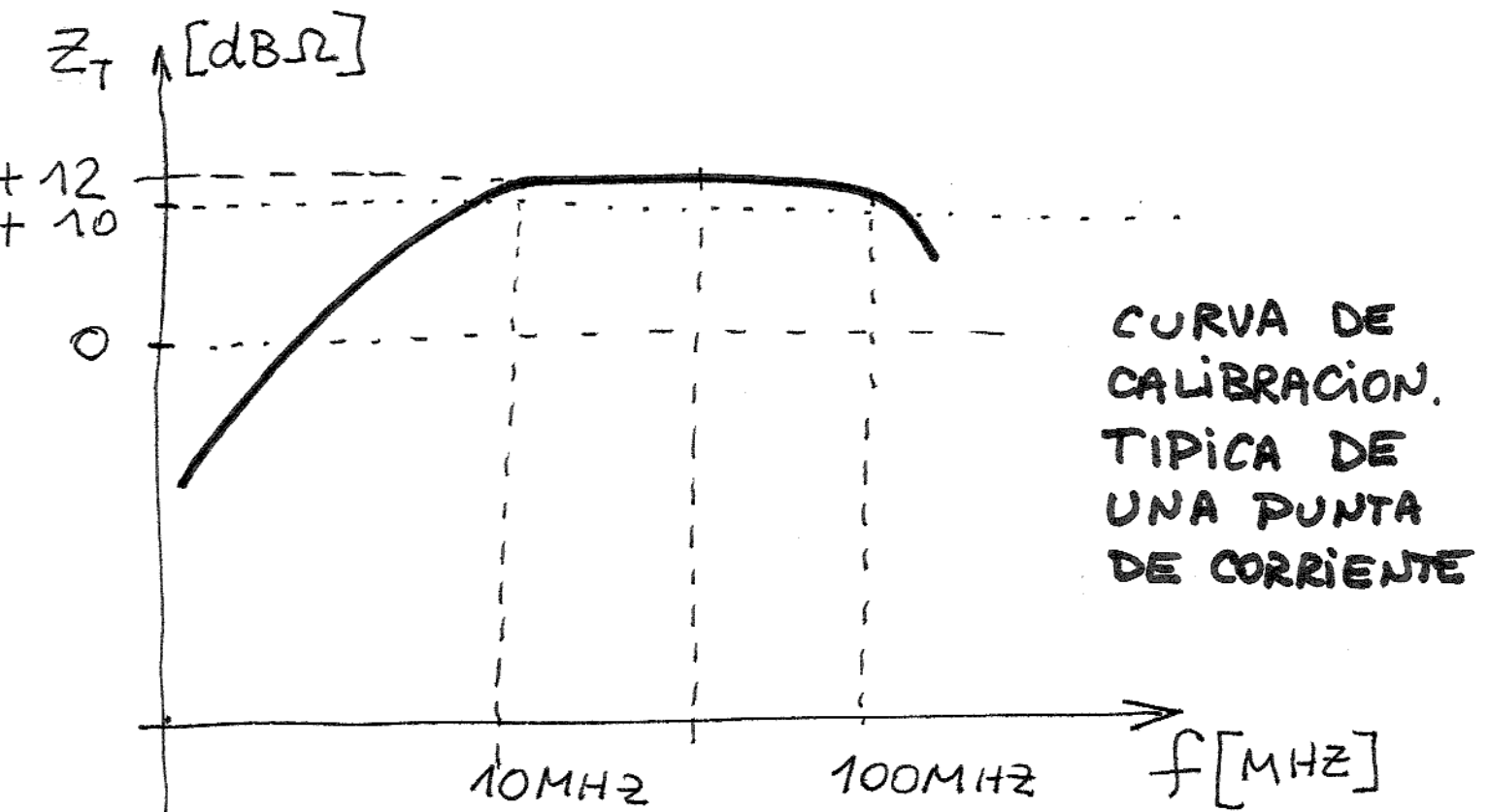
V_{ind} : TENSION EN EL ARROLLAMIENTO (MEDIDA)

GENERALMENTE SE DA:

$$|Z_T|_{dB\Omega} = |V|_{dB\mu V} - |I|_{dB\mu A}$$

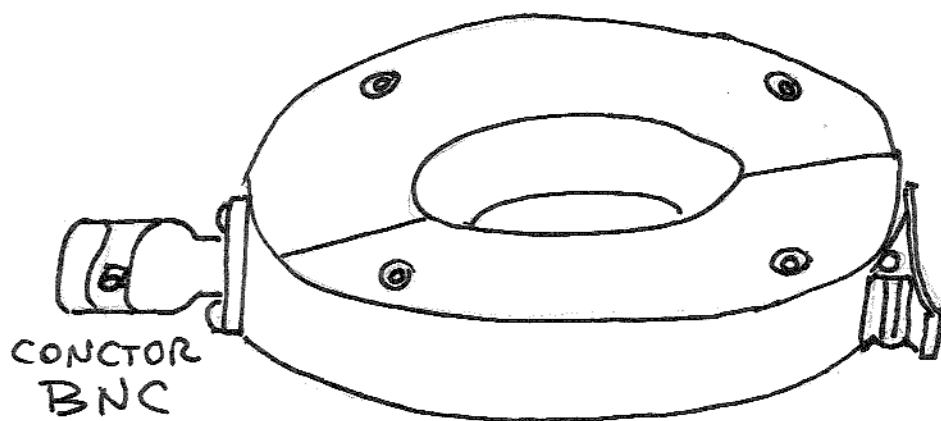
(dB RELATIVOS A 1Ω)

EJEMPLO $12dB\Omega$ DE 10 A 100 MHz

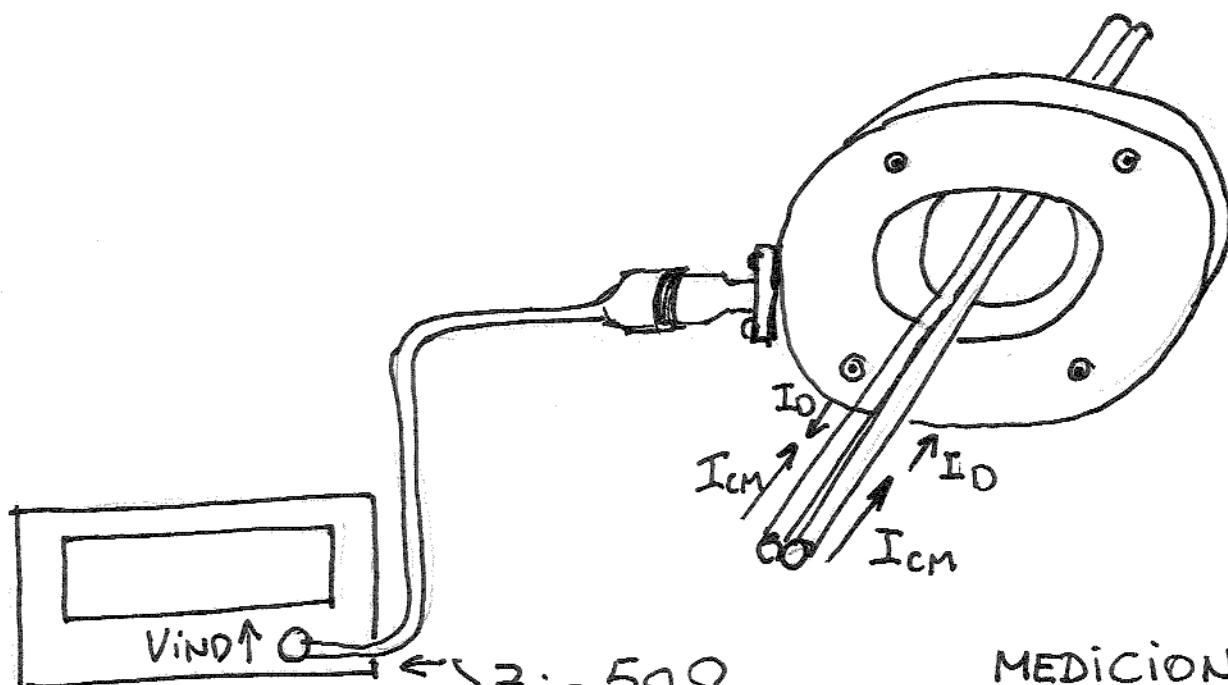


CURVA DE
CALIBRACION.
TIPICA DE
UNA PUNTA
DE CORRIENTE

SIRVE PARA MEDIR I_{MC} ENTRE 10 MHz Y 100 MHz



PUNTA DE
CORRIENTE
o
SENSOR DE
CORRIENTE



ANALIZADOR
DE ESPECTRO

MEDICION DE
VINDUCIDA

I_{CM} : CORRIENTE
DE MC A DETER
MINAR

EJEMPLO:

DEL EJEMPLO ANTERIOR

CISPR 22 DICE $E_{MAX} 100 \mu V/m$ $d = 10m$
($40 dB \mu V/m$) $f = 30 MHz$

$\Delta L = 1m$ CABLE

$$I_{MAX}|_{M.COMUN} = 26,5 \mu A. (28,46 dB \mu A)$$

$$|V|_{dB \mu V} = |I|_{dB \mu A} + |Z_T|_{dB \Omega}$$

$$|V|_{dB \mu V} = 28,5 dB \mu A + 12 dB \Omega$$

$$|V|_{dB \mu V} = 40,46 dB \mu V.$$

$$20 \log \frac{V}{1 \mu V} = 40,46 dB \mu V.$$

$$V = 10^{\frac{40,46}{20}} \cdot \mu V. = 105,5 \mu V.$$

$$\boxed{V = 105,5 \mu V}$$

TENSION MEDIDA MAXIMA EN LA Sonda
DE CORRIENTE PARA CUMPLIR LA NORMA.

SE HA VISTO PARA MODO COMÚN E_L/E_{MAX}

$$|E_{MAX}| = 1,256 \cdot 10^{-6} \frac{\Delta L \cdot I_0 \cdot f}{d} [V/m]$$

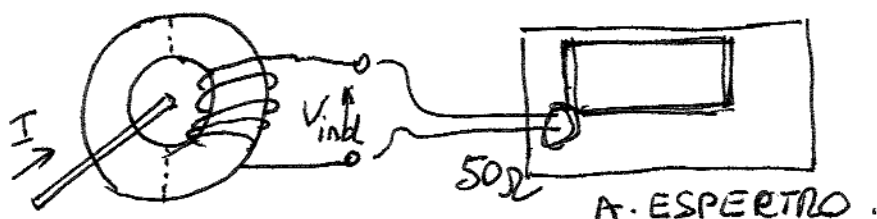
SI SE REEMPLAZA $Z_T = \frac{V_{ind}}{I}$

$$|E_{MAX}| = 1,256 \cdot 10^{-6} \frac{\Delta L \cdot |V_{ind}| \cdot f}{d \cdot |Z_T|}$$

$$|V_{ind}| = \frac{|E_{MAX}| d |Z_T|}{1,256 \cdot 10^{-6} \cdot \Delta L \cdot f} [\mu V]$$

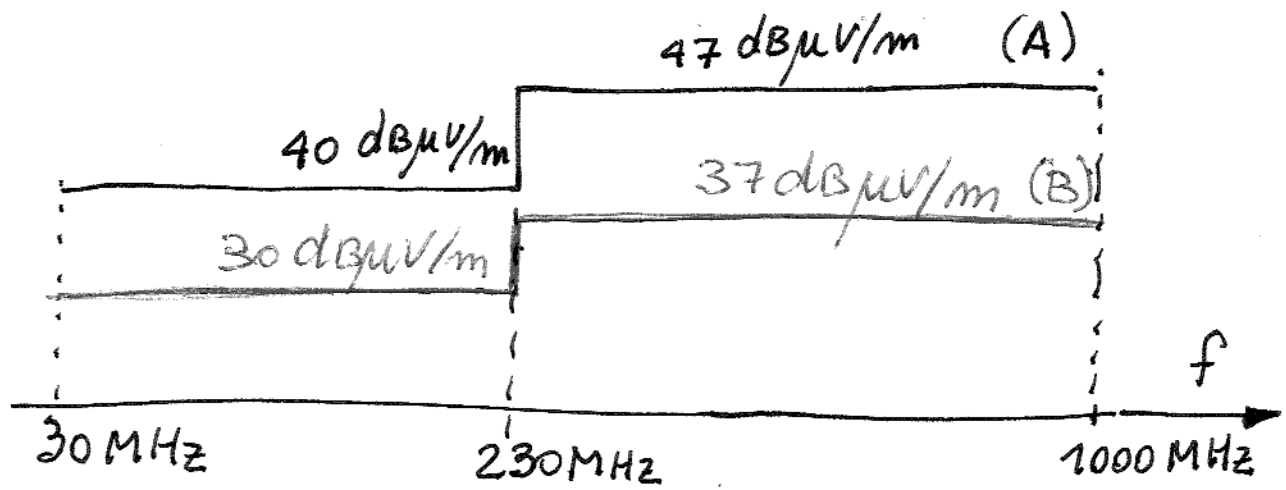
$$|V_{ind}|_{dB\mu V} = E_{MAX} (dB\mu V/m) + |Z_T|_{dB\Omega} + 20 \log d - 20 \log f (Hz) - 20 \log \Delta L - 20 \log (1,256 \cdot 10^{-6})$$

DADO UN CAMPO MAXIMO PARA LA I. DE M. COMUN Y LA PUNTA DE CORRIENTE CON SU Z_T , SE OBTIENE LA TENSION INDUCIDA MAXIMA QUE SE DEBE MEDIR EN EL ANALIZADOR DE ESPECTRO.

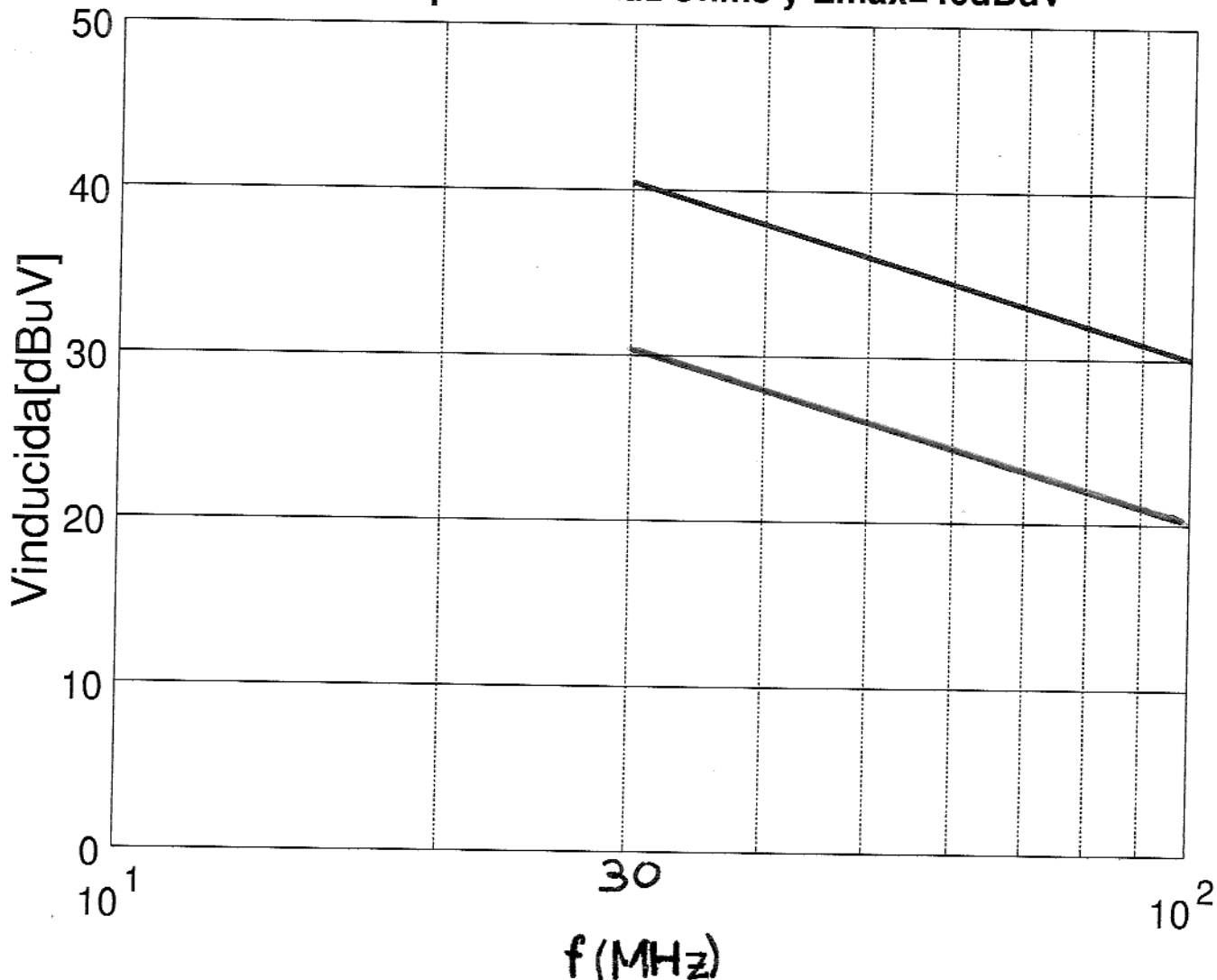


$$|V|_{ind.} = 40 dB\mu V/m + 12 dB\Omega + 20 \log 10 - 20 \log (30 \cdot 10^6) - 20 \log 1 - 20 \log (1,256 \cdot 10^{-6}) = 40 dB\mu V.$$

CISPR 22, $d=10\text{ m}$

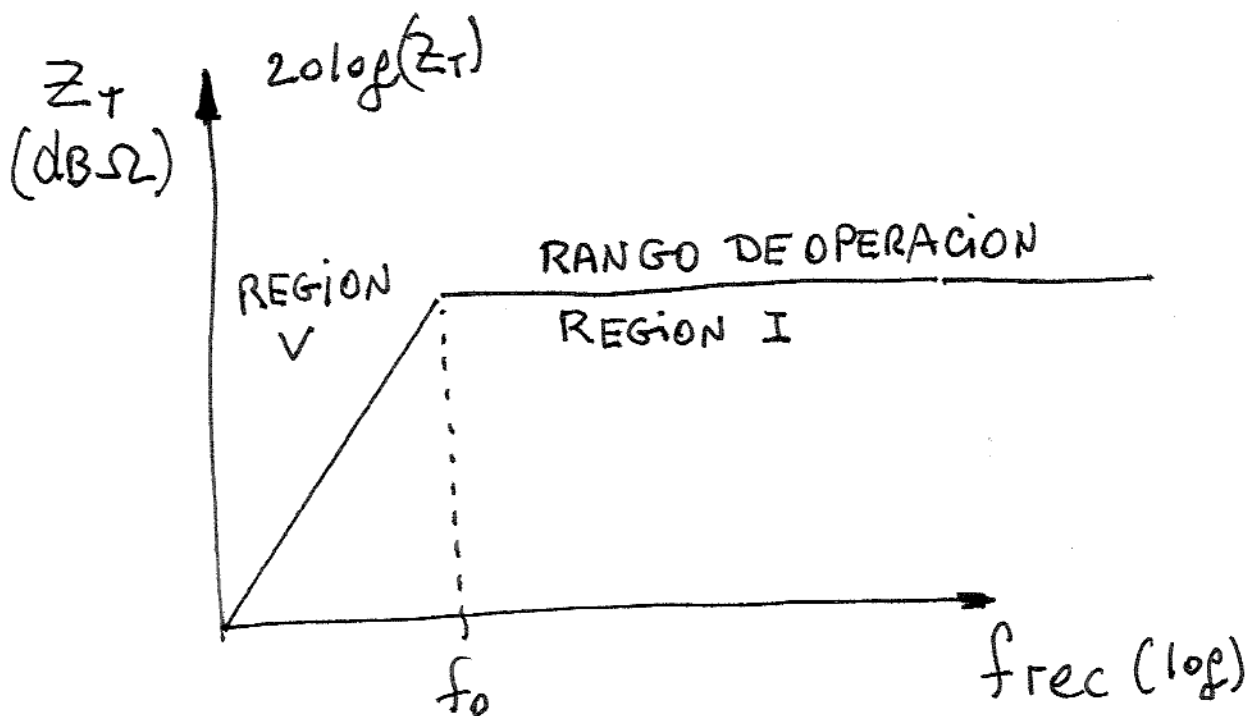
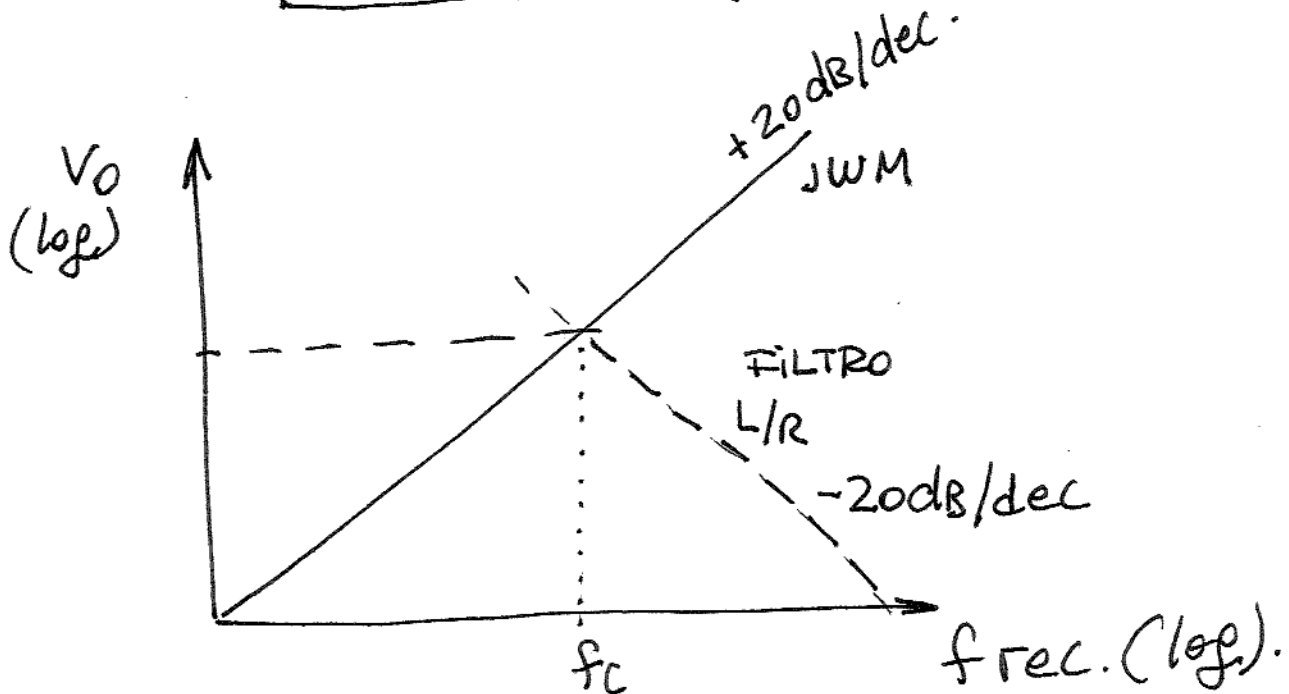
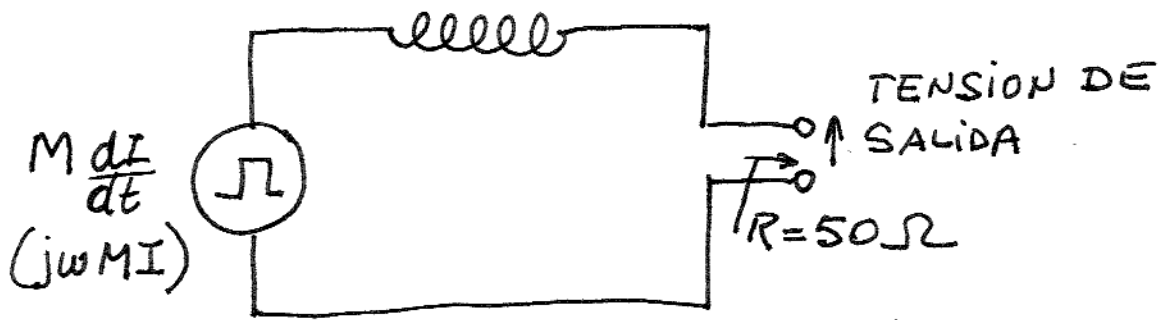


CISPR 22 para $Z_T=12\text{ dB}\Omega$ y $E_{\text{max}}=40\text{ dB}\mu\text{V}$



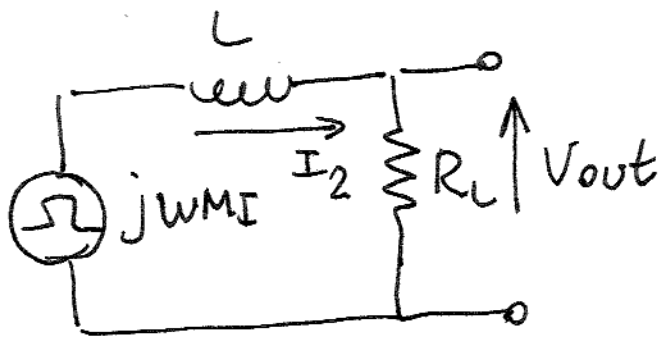
CIRCUITO EQUIVALENTE

L (AUTOINDUCTANCIA).



RESPUESTA TÍPICA

EN f_0, f_c ($X_L \equiv R_L$)



I : CORRIENTE EN EL PRIMARIO.

$$V_{out} = j\omega M I \frac{R_L}{R_L + j\omega L}$$

$$Z_t = \frac{V_{out}}{I} = \frac{j\omega M \cancel{I}}{\cancel{I}} \cdot \frac{R_L}{R_L + j\omega L}$$

$$Z_t = \frac{j\omega M R_L}{R_L + j\omega L}$$

$$Z_t \approx \frac{j\omega M R_L}{j\omega L} = \left(\frac{M}{L}\right) R_L \quad (Si \omega L \gg R_L)$$

PARA f_c : $X_L = R_L$
 $2\pi f_c L = R_L$

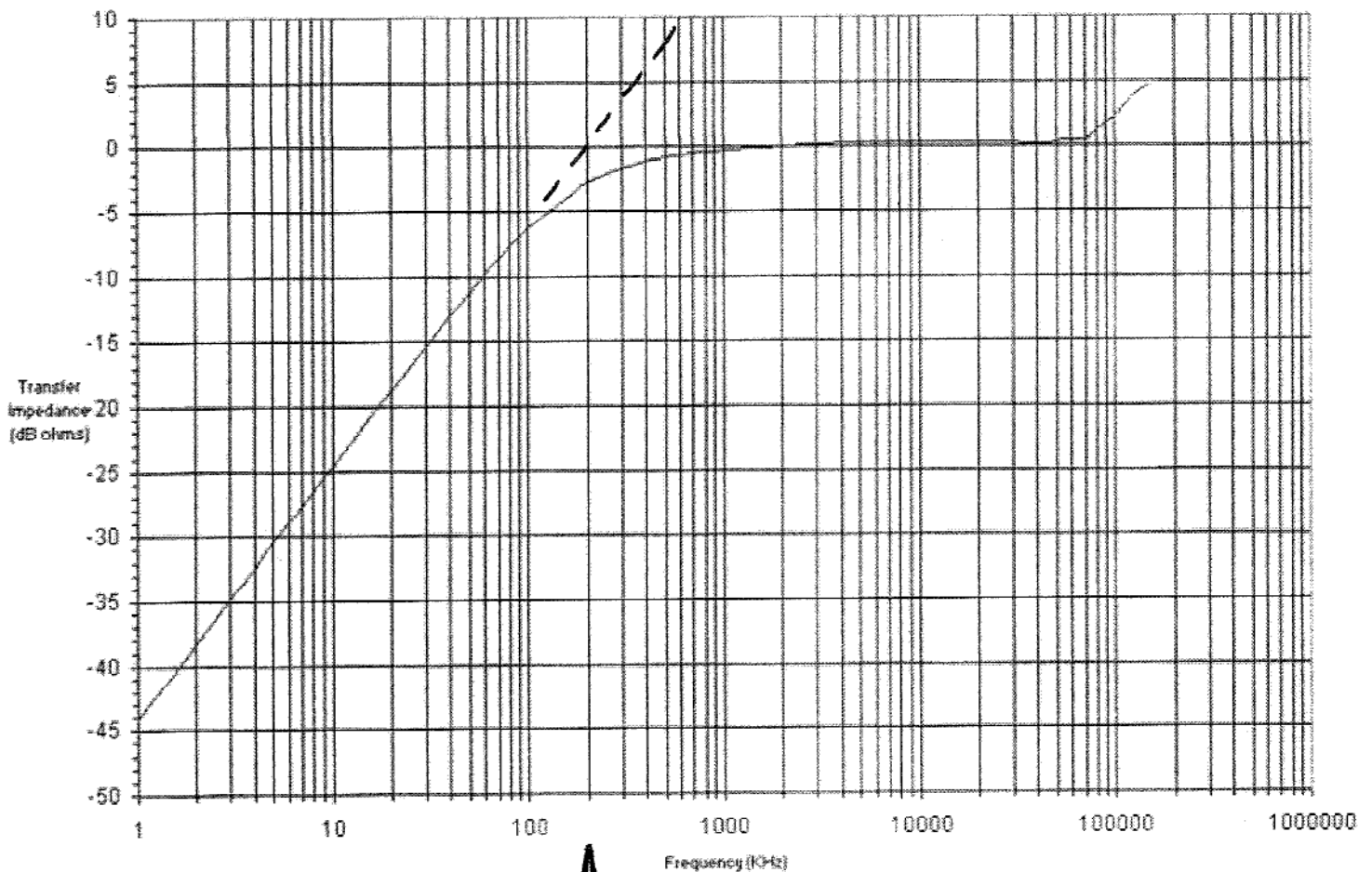
$$Z_t = \frac{M}{L} \cdot 2\pi f_c L$$

$$\boxed{M = \frac{Z_t}{2\pi f_c}}$$

SE PUEDE CALCULAR M CONOCIDA Z_t Y f_c . DE LA PUNTA

BROADBAND CURRENT PROBE BCP-611

10 KHz - 150 MHz



$$f_c = 200 \text{ KHz}$$

$$Z_t = 0 \text{ dB } \Omega \rightarrow Z_t = 1 \Omega$$

$$M = \frac{Z_t}{2\pi f_c} = \frac{1 \Omega}{2\pi \cdot 200 \cdot 10^3 \text{ Hz}} = 0,8 \cdot 10^{-6} \text{ H}$$

$$\text{COMO } Z_t = \frac{j\omega M R_L}{R_L + j\omega L}$$

$$\text{PARA } f = 10 \text{ MHz } \omega L \gg R_L. \quad Z_t \approx 1 \Omega.$$

$$Z_t = \frac{j\omega M R_L}{j\omega L} = \frac{M R_L}{L}$$

$$L = \frac{M R_L}{Z_t} = \frac{0,8 \cdot 10^{-6} 50 \Omega}{1 \Omega} =$$

$$\boxed{L = 40 \mu\text{H}}$$

EN RESONANCIA

$$\frac{\omega_c L}{R_L} = 1.$$

$$\omega_c = \frac{R_L}{L} =$$

$$f_c = \frac{R_L}{2\pi L} = \frac{50 \Omega}{2\pi \cdot 40 \cdot 10^{-6} \text{H}} = \boxed{200 \text{ kHz}}$$

Verifica o.k.