

# Frequency response, Bode

## Control Theory, Lecture 5

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Spring 2025

- Frequency response
- Partial-fraction expansion with sine input
- Amplitude and phase shift of a steady-state solution
- Bode plot

# SINE WAVE INPUT

Consider a sine wave with a phase shift. It can be presented in these two forms:

$$u(t) = A \sin(\omega t) + B \cos(\omega t) = \quad (1)$$

$$= M \sin(\omega t + \varphi) \quad (2)$$

where  $M = \sqrt{A^2 + B^2}$  is the amplitude of the signal and  $\varphi = -\tan^{-1} \left( \frac{B}{A} \right)$  is the phase shift.

Consider Laplace transforms:

$$\mathcal{L}(\sin(\omega t)) = \frac{\omega}{s^2 + \omega^2} \quad (3)$$

$$\mathcal{L}(\cos(\omega t)) = \frac{s}{s^2 + \omega^2} \quad (4)$$

$$\mathcal{L}(A \sin(\omega t) + B \cos(\omega t)) = \frac{A\omega + Bs}{s^2 + \omega^2} \quad (5)$$

# ODE WITH A SINE WAVE INPUT

Given an ODE with a sine input:

$$a_n y^{(n)} + \dots + a_1 \dot{y} + a_0 y = b_m u^{(m)} + \dots + b_1 \dot{u} + b_0 u \quad (6)$$

$$u(t) = A \sin(\omega t) \quad (7)$$

we can find its Laplace transform:

$$(a_n s^n + \dots + a_1 s + a_0)Y(s) = (b_m s^m + \dots + b_1 s + b_0)U(s) \quad (8)$$

$$U(s) = \frac{A\omega}{s^2 + \omega^2} \quad (9)$$

We can find its Laplace representation:

$$Y(s) = \frac{b_m s^m + \dots + b_1 s + b_0}{a_n s^n + \dots + a_1 s + a_0} \cdot \frac{A\omega}{s^2 + \omega^2} \quad (10)$$

## Frequency response

Frequency response is a steady-state output of the system, given a sine input.

Consider a system  $Y(s) = G(s)U(s)$ .

A sine input  $u(t) = A\sin(\omega t)$  in the time domain translates to  $U(s) = A\frac{\omega}{\omega^2 + s^2}$  in the Laplace domain. So, given a sine input, the system becomes:

$$Y(s) = G(s)\frac{A\omega}{\omega^2 + s^2} \quad (11)$$

# FRACTION EXPANSION, 1

Assuming negative real non-repeating poles we can expand the function  $Y(s) = G(s) \frac{A\omega}{\omega^2 + s^2}$ :

$$G(s) \frac{A\omega}{\omega^2 + s^2} = \frac{r_1}{s + p_1} + \frac{r_2}{s + p_2} + \dots + \frac{r_n}{s + p_n} + \frac{\alpha(s)}{s + j\omega} + \frac{\beta(s)}{s - j\omega}$$

Laplace function of the form  $\frac{r_i}{s + p_i}$  corresponds to the following time function:

$$y(t) = r_i e^{-p_i t} \quad (12)$$

So, for a stable transfer function  $G(s)$  as time goes to infinity,  $r_i e^{-p_i t}$  goes to zero. The only components of the function  $Y(s)$  that do not disappear are the last two:  $\frac{\alpha(s)}{s + j\omega} + \frac{\beta(s)}{s - j\omega}$ .

## FRACTION EXPANSION, 2

To find  $\alpha(s)$  we multiply the equation by  $s + j\omega$ :

$$\begin{aligned} G(s) \frac{A\omega(s + j\omega)}{(s + j\omega)(s - j\omega)} &= \\ &= \left( \frac{r_1}{s + p_1} + \dots + \frac{r_n}{s + p_n} \right) (s + j\omega) + \alpha(s) + \frac{\beta(s)(s + j\omega)}{s - j\omega} \end{aligned}$$

Considering  $s = -j\omega$  we get:

$$\alpha = G(-j\omega) \frac{A}{-2j} \quad (13)$$

To find  $\beta(s)$  we multiply the decomposition equation by  $s - j\omega$  and then consider  $s = j\omega$ :

$$\beta = G(j\omega) \frac{A}{2j} \quad (14)$$

Laplace image of the steady-state solution is:

$$Y_{ss}(s) = \frac{\alpha(s)}{s + j\omega} + \frac{\beta(s)}{s - j\omega} \quad (15)$$

$$Y_{ss}(s) = \frac{A}{2j} \left( G(j\omega) \frac{1}{s - j\omega} - G(-j\omega) \frac{1}{s + j\omega} \right) \quad (16)$$

Inverse Laplace transform gives us:

$$y_{ss}(t) = \frac{A}{2j} (G(j\omega)e^{j\omega t} - G(-j\omega)e^{-j\omega t}) \quad (17)$$



# FUNCTION OF COMPLEX VARIABLES

A complex function  $W(x)$  can be represented in a polar form:

$$W(x) = r(x)e^{\theta(x)i} \quad (18)$$

where

$$r(x) = |W(x)| = \text{amp}(W(x)) \quad (19)$$

$$\theta(x) = \text{phase}(W(x)) = \text{atan2}(\text{Im}(W(x)), \text{Re}(W(x))) \quad (20)$$

We observe the following conjugate identities:

$$|W(jx)| = |W(-jx)| \quad (21)$$

$$\text{phase}(W(-jx)) = -\text{phase}(W(jx)) \quad (22)$$

Finally, we can represent a sine function as a difference of exponentials:

$$\sin(x) = \frac{e^{ix} - e^{-ix}}{2i} \quad (23)$$

# AMPLITUDE AND PHASE, 1

We can define polar coordinates representation:

$$G(j\omega) = r(\omega)e^{j\theta(\omega)} \quad (24)$$

$$G(-j\omega) = r(\omega)e^{-j\theta(\omega)} \quad (25)$$

where  $r(\omega) = |G(j\omega)|$  and  
 $\theta(\omega) = \text{atan2}(\text{Im}(G(j\omega)), \text{Re}(G(j\omega)))$ .

We can re-write the steady-state solution

$y_{ss}(t) = \frac{A}{2j} (G(j\omega)e^{j\omega t} - G(-j\omega)e^{-j\omega t})$  as:

$$y_{ss}(t) = \frac{A}{2j} \left( r(\omega)e^{j\theta(\omega)}e^{j\omega t} - r(\omega)e^{-j\theta(\omega)}e^{-j\omega t} \right) \quad (26)$$

$$y_{ss}(t) = \frac{Ar(\omega)}{2j} \left( e^{j\theta(\omega)+j\omega t} - e^{-(j\theta(\omega)+j\omega t)} \right) \quad (27)$$

$$y_{ss}(t) = Ar(\omega) \sin(\omega t + \theta(\omega)) \quad (28)$$

Thus we found the steady-state output for the system:

$$y_{ss}(t) = Ar(\omega) \sin(\omega t + \theta(\omega)) \quad (29)$$

Let us find the ratio between amplitude of the input and the output systems:

$$\text{amplification}(\omega) = \frac{Ar(\omega)}{A} = r(\omega) = |G(j\omega)| \quad (30)$$

Let us find the phase shift between the input and the output systems:

$$\text{phase}(\omega) = \theta(\omega) = \text{atan2}(\text{Im}(G(j\omega)), \text{Re}(G(j\omega))) \quad (31)$$

# BODE PLOT

The first key idea of a Bode plot is substitution of purely complex variable  $j\omega$  in place of Laplace variable  $s$ , which can have non-zero real part.

Given a transfer function  $W(s)$ ,  $s = \sigma + j\omega$  we can analyse its behaviour when  $\sigma = 0$ . We can plot:

- its amplitude  $a(\omega) = |W(j\omega)|$ ,
- its phase  $\varphi(\omega) = \text{atan2}(\text{im}(W(j\omega)), \text{real}(W(j\omega)))$ .

Bode plot is actually two plots:

- 1  $20 \cdot \log(a(\omega))$ ,
- 2  $\frac{180}{\pi} \varphi(\omega)$ .

The 20 and  $\log()$  has to do with the vertical axis being in decibels.

## BODE PLOT - EXAMPLE

Consider  $W(s) = \frac{1}{1+s}$ . Then  $W(j\omega) = \frac{1}{1+j\omega}$ . We can transform it as:

$$W(j\omega) = \frac{1 - j\omega}{(1 + j\omega)(1 - j\omega)} = \frac{1 - j\omega}{1 + \omega^2} \quad (32)$$

Thus we have  $\text{real}(W(j\omega)) = \frac{1}{1+\omega^2}$  and  $\text{im}(W(j\omega)) = -\frac{\omega}{1+\omega^2}$ .

Bode plot is then given as:

$$a(\omega) = \sqrt{\frac{1 + \omega^2}{(1 + \omega^2)^2}} = \frac{1}{\sqrt{(1 + \omega^2)}} \quad (33)$$

$$\varphi(\omega) = \text{atan2} \left( -\frac{\omega}{1 + \omega^2}, \frac{1}{1 + \omega^2} \right) \quad (34)$$

## BODE PLOT - STABILITY MARGINS

Before we discuss the use of Bode plot, let us remember that closed-loop transfer function has form (when simple feedback is used):

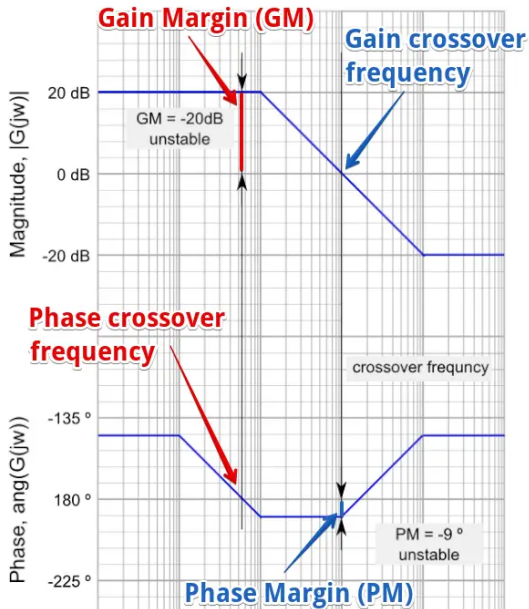
$$W(s) = \frac{G(s)}{1 + G(s)} \quad (35)$$

Substituting  $s \rightarrow j\omega$  we get:

$$W(\omega) = \frac{G(j\omega)}{1 + G(j\omega)} \quad (36)$$

From this we can see that  $W(\omega)$  becomes ill-defined if  $G(j\omega) = -1$ . Meaning, we want to avoid two things happening simultaneously: the amplitude of  $G(j\omega)$  being equal to 1, and its phase (argument) being equal to  $180^\circ$  (remember, phase of  $0^\circ$  is pure positive real number, phase of  $90^\circ$  is pure positive imaginary number,  $180^\circ$  is pure negative real number, etc.).

# STABILITY MARGINS - EXAMPLE



Consider a system with resonance:

$$\begin{cases} \dot{\mathbf{x}} = \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} \mathbf{u} \\ \mathbf{y} = \begin{bmatrix} 1 & 0 \end{bmatrix} \mathbf{x} \end{cases} \quad (37)$$

The state matrix of this system has eigenvalues  $\lambda_i = \pm j$  with resonance frequency  $\omega = 1$ .

The eigenvalues of the closed-loop system  $\mathbf{A} - \mathbf{BC}$  are  $\lambda_i = \pm\sqrt{2}j$  with resonance frequency  $\omega = \sqrt{2}$ .



# BODE PLOT WITH RESONANCE, 2

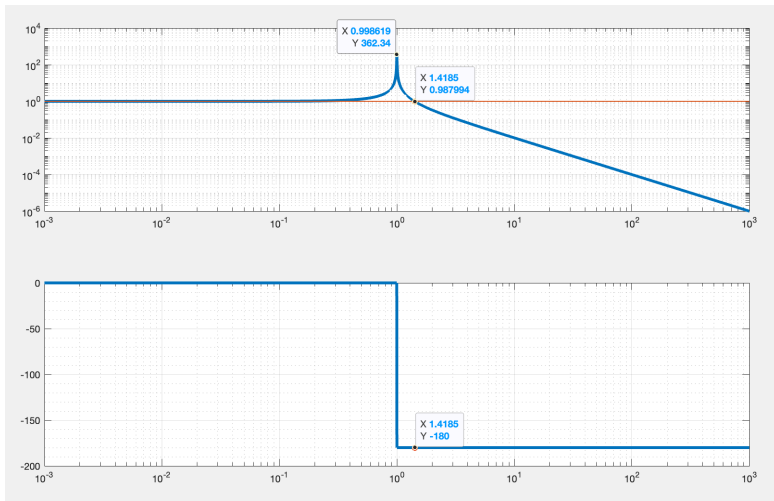


Figure 2: Bode plot of a system with resonance

- Nise, N.S. Control systems engineering. John Wiley & Sons. (Chapter 10 Frequency Response Techniques)
- Matthew M. Peet; Systems Analysis and Control - Lecture 18: The Frequency Response
- Control System Lectures - Bode Plots, Introduction
- Oxford University Press. s-Domain analysis: poles, zeros, and Bode plots

Lecture slides are available via Github:

[github.com/SergeiSa/Control-Theory-2025](https://github.com/SergeiSa/Control-Theory-2025)



# LAPLACE AND FOURIER TRANSFORMS

- *Fourier series* can be seen as representing a periodic function as a sum of harmonics (sines and cosines). These sines and cosines can be thought of as forming a basis in a linear space. The coefficients of the series can be thought of as a discrete spectrum of the function.
- *Fourier transform* gives a continuous spectrum of the function. The "basis" is still made of harmonic functions.
- *Laplace transform* also gives a continuous spectrum of the function, but in a different basis: the basis is given by complex exponentials. I like to think of this basis as solutions of second order ODEs.

# LAPLACE AND FOURIER TRANSFORMS

Let's compare. Fourier transform:

$$F(\omega) = \int_{-\infty}^{\infty} f(t)e^{-2\pi j t \omega} dt, \quad \omega \in \mathbb{R} \quad (38)$$

Laplace transform:

$$F(s) = \int_0^{\infty} f(t)e^{-st} dt, \quad s \in \mathbb{C} \quad (39)$$

We can see that Fourier looks like Laplace with purely imaginary number in the exponent.

# LAPLACE AND STEADY STATE SOLUTION

From analysing solutions of linear ODEs we know that, given harmonic input (sine, cosine, their combination) "after the transient process is over, the solution approaches a harmonic with the same frequency", but possibly different amplitude and phase.

Intuitively we can think of the imaginary part of  $s$  as having to do with this frequency response.

The kernel function of the Laplace transform is  $e^{-st}$  with  $s = \sigma + j\omega$  being a complex variable. If  $\sigma = 0$ , the kernel becomes  $e^{-j\omega t} = \cos(\omega t) - j\sin(\omega t)$ . You can see the similarity with Fourier transform kernel.