

Robotics with Contact

Fundamentals of Robotics, Lecture 12

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Assume the dynamics has to obey a certain equation, e.g.:

$$\mathbf{g}(\mathbf{q}) = 0 \quad (1)$$

This can happen, for example, if part of a robot is attached to the ground. Bolting the end-effector of a robot arm to the ground makes it into a parallel robot.

Equation (1) can be differentiated to find constraints on velocity or acceleration:

$$\mathbf{F}\dot{\mathbf{q}} = 0 \quad (2)$$

$$\mathbf{F}\ddot{\mathbf{q}} + \dot{\mathbf{F}}\dot{\mathbf{q}} = 0 \quad (3)$$

where $\mathbf{F} = \frac{\partial \mathbf{g}}{\partial \mathbf{q}}$.

Remember - without constraints the dynamics looks like $\mathbf{H}\ddot{\mathbf{q}} + \mathbf{C}\dot{\mathbf{q}} + \mathbf{g} = \boldsymbol{\tau}$. Presence of constraints adds reaction forces $\boldsymbol{\lambda}$:

$$\mathbf{H}\ddot{\mathbf{q}} + \mathbf{C}\dot{\mathbf{q}} + \mathbf{g} = \boldsymbol{\tau} + \mathbf{F}^\top \boldsymbol{\lambda} \quad (4)$$

Let us note that this equation is not solvable without the acceleration constraint equations. With constraints it has the following form:

$$\begin{cases} \mathbf{H}\ddot{\mathbf{q}} + \mathbf{C}\dot{\mathbf{q}} + \mathbf{g} = \boldsymbol{\tau} + \mathbf{F}^\top \boldsymbol{\lambda} \\ \mathbf{F}\ddot{\mathbf{q}} + \dot{\mathbf{F}}\dot{\mathbf{q}} = 0 \end{cases} \quad (5)$$

As long as \mathbf{F} has independent rows, it has only one solution.

We can re-write the equation in a block-matrix form:

$$\begin{bmatrix} \mathbf{H} & -\mathbf{F}^\top \\ -\mathbf{F} & 0 \end{bmatrix} \begin{bmatrix} \ddot{\mathbf{q}} \\ \lambda \end{bmatrix} = \begin{bmatrix} \tau - \mathbf{C}\dot{\mathbf{q}} - \mathbf{g} \\ \dot{\mathbf{F}}\dot{\mathbf{q}} \end{bmatrix} \quad (6)$$

The block matrix on the left-hand side is invertible (as long as \mathbf{F} has full row-rank).

Dynamics equations can be solved:

$$\mathbf{H}\ddot{\mathbf{q}} + \mathbf{C}\dot{\mathbf{q}} + \mathbf{g} = \boldsymbol{\tau} + \mathbf{F}^\top \boldsymbol{\lambda} \quad (7)$$

$$\ddot{\mathbf{q}} = \mathbf{H}^{-1}\mathbf{F}^\top \boldsymbol{\lambda} + \mathbf{H}^{-1}(\boldsymbol{\tau} - \mathbf{C}\dot{\mathbf{q}} - \mathbf{g}) \quad (8)$$

$$-\mathbf{F}\mathbf{H}^{-1}\mathbf{F}^\top \boldsymbol{\lambda} - \mathbf{F}\mathbf{H}^{-1}(\boldsymbol{\tau} - \mathbf{C}\dot{\mathbf{q}} - \mathbf{g}) = \dot{\mathbf{F}}\dot{\mathbf{q}} \quad (9)$$

$$-\mathbf{F}\mathbf{H}^{-1}\mathbf{F}^\top \boldsymbol{\lambda} = \mathbf{F}\mathbf{H}^{-1}(\boldsymbol{\tau} - \mathbf{C}\dot{\mathbf{q}} - \mathbf{g}) + \dot{\mathbf{F}}\dot{\mathbf{q}} \quad (10)$$

We define $\mathbf{f}_1 = \boldsymbol{\tau} - \mathbf{C}\dot{\mathbf{q}} - \mathbf{g}$ and $\mathbf{f}_2 = \dot{\mathbf{F}}\dot{\mathbf{q}}$:

$$-\mathbf{F}\mathbf{H}^{-1}\mathbf{F}^\top \boldsymbol{\lambda} = \mathbf{F}\mathbf{H}^{-1}\mathbf{f}_1 + \mathbf{f}_2 \quad (11)$$

$$\boldsymbol{\lambda} = -(\mathbf{F}\mathbf{H}^{-1}\mathbf{F}^\top)^{-1}(\mathbf{F}\mathbf{H}^{-1}\mathbf{f}_1 + \mathbf{f}_2) \quad (12)$$

$$\ddot{\mathbf{q}} = -\mathbf{H}^{-1}\mathbf{F}^\top (\mathbf{F}\mathbf{H}^{-1}\mathbf{F}^\top)^{-1}(\mathbf{F}\mathbf{H}^{-1}\mathbf{f}_1 + \mathbf{f}_2) + \mathbf{H}^{-1}\mathbf{f}_1 \quad (13)$$

$$\ddot{\mathbf{q}} = (\mathbf{I} - \mathbf{H}^{-1}\mathbf{F}^\top (\mathbf{F}\mathbf{H}^{-1}\mathbf{F}^\top)^{-1}\mathbf{F}\mathbf{H}^{-1})\mathbf{f}_1 - \quad (14)$$

$$-\mathbf{H}^{-1}\mathbf{F}^\top (\mathbf{F}\mathbf{H}^{-1}\mathbf{F}^\top)^{-1}\mathbf{F}\mathbf{H}^{-1}\mathbf{f}_2 \quad (15)$$

So, we have:

$$\begin{bmatrix} \ddot{\mathbf{q}} \\ \lambda \end{bmatrix} = \begin{bmatrix} \mathbf{I} - \mathbf{H}^{-1}\mathbf{F}^\top\mathbf{M}\mathbf{F}\mathbf{H}^{-1} & \mathbf{H}^{-1}\mathbf{F}^\top\mathbf{M}\mathbf{F}\mathbf{H}^{-1} \\ \mathbf{M}\mathbf{F}\mathbf{H}^{-1} & -\mathbf{M} \end{bmatrix} \begin{bmatrix} \mathbf{f}_1 \\ \mathbf{f}_2 \end{bmatrix} \quad (16)$$

where $\mathbf{M} = (\mathbf{F}\mathbf{H}^{-1}\mathbf{F}^\top)^{-1}$.

Note that reaction forces cannot assume arbitrary values. If \mathbf{f} is a reaction force acting at a contact point, then constraints on possible values of reaction forces are given as:

$$\|\mathbf{T}^\top \mathbf{f}\| \leq \mu \mathbf{n}^\top \mathbf{f} \quad (17)$$

where $\mathbf{T} \in \mathbb{R}^{3 \times 2}$ is a basis in a tangent plane on the supporting surface, \mathbf{n} is a normal to the supporting surface and μ is a friction coefficient.

For a horizontal surface with friction coefficient $\mu = 0.5$ and $\mathbf{f} = [f_x \ f_y \ f_z]$ the equation looks like:

$$\sqrt{f_x^2 + f_y^2} \leq 0.5 f_z \quad (18)$$

Alternatively, a linear approximation can be used:

$$\mathbf{A}\mathbf{f} \leq \mathbf{b} \quad (19)$$

For a horizontal surface with friction coefficient $\mu = 1$ approximation of the cone by a pyramid with 4 faces can look like:

$$\begin{bmatrix} \frac{\sqrt{2}}{2} & 0 & \frac{\sqrt{2}}{2} \\ -\frac{\sqrt{2}}{2} & 0 & \frac{\sqrt{2}}{2} \\ 0 & \frac{\sqrt{2}}{2} & \frac{\sqrt{2}}{2} \\ 0 & -\frac{\sqrt{2}}{2} & \frac{\sqrt{2}}{2} \end{bmatrix} \begin{bmatrix} f_x \\ f_y \\ f_z \end{bmatrix} \leq \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} \quad (20)$$

Constraints simulating physical contact can be written as inequalities:

$$\mathbf{g}(\mathbf{q}) \geq 0 \quad (21)$$

When $\mathbf{g}(\mathbf{q}) > 0$, the reaction force $\lambda = 0$, and conversely - if $\lambda > 0$, then $\mathbf{g}(\mathbf{q}) = 0$. This can be described via complimentary constraint:

$$\begin{cases} \mathbf{g}(\mathbf{q})^\top \lambda = 0 \\ \mathbf{g}(\mathbf{q}) \geq 0 \\ \lambda \geq 0 \end{cases} \quad (22)$$

Given nominal acceleration $\ddot{\mathbf{q}}^*$ and nominal reaction forces λ^* , we can formulate reactive control

$$\underset{\ddot{\mathbf{q}}, \lambda}{\text{minimize}} \quad \|\ddot{\mathbf{q}}\|_{\mathbf{Q}_1} + \|\lambda\|_{\mathbf{Q}_2} \quad (23)$$

$$\text{subject to: } \mathbf{H}(\ddot{\mathbf{q}}^* + \ddot{\mathbf{q}}) + \mathbf{C}\dot{\mathbf{q}} + \mathbf{g} = \tau + \mathbf{F}^\top(\lambda^* + \lambda) \quad (24)$$

$$\mathbf{F}(\ddot{\mathbf{q}}^* + \ddot{\mathbf{q}}) + \dot{\mathbf{F}}\dot{\mathbf{q}} = 0 \quad (25)$$

where $\|\cdot\|_{\mathbf{Q}_i}$ is a weighted norm with weight matrix \mathbf{Q}_i . This control law does not guarantee stability and requires solving a quadratic problem on each iteration.

For a constrained mechanical system we can solve inverse dynamics without the need for linearization. Consider the following dynamics:

$$\mathbf{H}\ddot{\mathbf{q}} + \mathbf{C}\dot{\mathbf{q}} + \mathbf{g} = \mathbf{B}\mathbf{u} + \mathbf{F}^\top \lambda \quad (26)$$

We can represent constraint Jacobian \mathbf{F}^\top as its QR decomposition: $\mathbf{F}^\top = \mathbf{Q} \begin{bmatrix} \mathbf{R} \\ \mathbf{0} \end{bmatrix}$, where $\mathbf{Q}^\top \mathbf{Q} = \mathbf{Q}\mathbf{Q}^\top = \mathbf{I}$ and \mathbf{R} is convertible.

$$\mathbf{H}\ddot{\mathbf{q}} + \mathbf{C}\dot{\mathbf{q}} + \mathbf{g} = \mathbf{B}\mathbf{u} + \mathbf{Q} \begin{bmatrix} \mathbf{R} \\ \mathbf{0} \end{bmatrix} \lambda \quad (27)$$

Let us multiply the equation by \mathbf{Q}^\top :

$$\mathbf{Q}^\top (\mathbf{H}\ddot{\mathbf{q}} + \mathbf{C}\dot{\mathbf{q}} + \mathbf{g}) = \mathbf{Q}^\top \mathbf{B}\mathbf{u} + \begin{bmatrix} \mathbf{R} \\ \mathbf{0} \end{bmatrix} \lambda \quad (28)$$

Introducing switching variables (to divide upper and lower part of the equations) $\mathbf{S}_1 = [\mathbf{I} \ \mathbf{0}]$ and $\mathbf{S}_2 = [\mathbf{0} \ \mathbf{I}]$ and multiplying equations by one and the other we get two systems:

$$\begin{cases} \mathbf{S}_1 \mathbf{Q}^\top (\mathbf{H}\ddot{\mathbf{q}} + \mathbf{C}\dot{\mathbf{q}} + \mathbf{g}) = \mathbf{S}_1 \mathbf{Q}^\top \mathbf{B}\mathbf{u} + \mathbf{R}\lambda \\ \mathbf{S}_2 \mathbf{Q}^\top (\mathbf{H}\ddot{\mathbf{q}} + \mathbf{C}\dot{\mathbf{q}} + \mathbf{g}) = \mathbf{S}_2 \mathbf{Q}^\top \mathbf{B}\mathbf{u} \end{cases} \quad (29)$$

The main advantage we achieved is that now we can calculate both \mathbf{u} and λ

Resulting expression for \mathbf{u} is:

$$\mathbf{u} = (\mathbf{S}_2 \mathbf{Q}^\top \mathbf{B})^+ \mathbf{S}_2 \mathbf{Q}^\top (\mathbf{H} \ddot{\mathbf{q}} + \mathbf{C} \dot{\mathbf{q}} + \mathbf{g}) \quad (30)$$

Expression for λ is:

$$\lambda = \mathbf{R}^{-1} \mathbf{S}_1 \mathbf{Q}^\top (\mathbf{H} \ddot{\mathbf{q}} + \mathbf{C} \dot{\mathbf{q}} + \mathbf{g} - \mathbf{B} \mathbf{u}) \quad (31)$$

We can notice a pseudo-inverse, implying that the no-residual solution does not have to exist.

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THANK YOU!

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Prove that $\mathbf{F}\mathbf{H}^{-1}\mathbf{F}^\top$ is full rank if \mathbf{F} is full row-rank and $\mathbf{H} > 0$ - positive-definite.

We can prove that $\mathbf{F}\mathbf{H}^{-1}\mathbf{F}^\top$ is positive-definite:

$$J = \mathbf{x}^\top \mathbf{F}\mathbf{H}^{-1}\mathbf{F}^\top \mathbf{x} \quad (32)$$

Defining $\mathbf{y} = \mathbf{F}^\top \mathbf{x}$. Since \mathbf{F} is full row-rank, then $\|\mathbf{x}\| \neq 0$ implies $\|\mathbf{y}\| \neq 0$ because \mathbf{F}^\top has trivial null space. We get: $J = \mathbf{y}^\top \mathbf{H}^{-1}\mathbf{y}$ which is positive for any non-zero \mathbf{y} (because \mathbf{H} is positive-definite), meaning $J > 0$ for any non-zero \mathbf{x} . Since $\mathbf{F}\mathbf{H}^{-1}\mathbf{F}^\top > 0$, it implies full-rank.

This is called *congruent transformation*, which leaves positive-definiteness in-tact.