			1 0 4						
$d_1=0.4~\mathrm{m}$									
$\alpha_{19\Phi}$	0.03	0.04	$\frac{ ho}{0.05}$	0.06	0.07				
9.0	Нет	Нет	Нет	Нет	Нет				
10.0	Нет	Нет	Нет	Нет	Нет				
11.0	Нет	Нет	Нет	Нет	Нет				
12.0	Нет	Нет	Нет	Нет	Нет				
13.0	Нет	Нет	Нет	Нет	Нет				
14.0	71.31 0.7804	${ m Her}$	${ m Her}$	Нет	Нет				
15.0	62.33 0.5123	$69.01 \mid 0.6376$	Нет	Нет	Нет				
16.0	58.14 0.4034	$61.73 \mid 0.4506$	67.43 0.5396	Нет	Нет				
17.0	55.0 0.3305	57.68 0.359	Нет	66.17 0.4659	Нет				
18.0	52.72 0.2845	54.81 0.3017	57.41 0.326	60.62 0.358	65.16 0.4092				
19.0	50.7 0.2477	52.48 0.2601	54.64 0.2775	57.17 0.2986	$60.09 \mid\! 0.3225$				
			$d_1 = 0.5 \text{ M}$						
$\alpha_{19\Phi}$	0.09	0.04	ρ	0.06	0.07				
	0.03	0.04	0.05	$\frac{0.06}{44.6 0.5556}$	0.07 Нет				
$ \begin{array}{c c} 9.0 \\ 10.0 \end{array} $	37.48 0.406 $35.34 0.3133$	39.26 0.4397 36.59 0.3289	41.47 0.484 $38.1 0.351$	$\frac{44.6}{0.3778}$	41.93 0.4083				
11.0	33.78 0.2549	v ·	36.01 0.331 $36.01 0.2788$	37.29 0.2922	38.83 0.3108				
$\frac{11.0}{12.0}$	32.6 0.2162	33.49 0.2234	34.46 0.2314	37.29 0.2922 $35.52 0.2403$	36.76 0.2526				
13.0	31.6 0.1874	32.39 0.193	33.25 0.1991	34.18 0.2057	35.18 0.213				
14.0	30.7 0.1645	31.42 0.1689	32.19 0.1735	33.05 0.1797	33.94 0.1854				
15.0	29.92 0.1472	30.59 0.1508	31.29 0.1546	32.04 0.1587	32.85 0.163				
16.0	29.21 0.133	29.82 0.136	30.48 0.1392	31.17 0.1426	31.91 0.1463				
17.0	28.54 0.1212	29.12 0.1238	29.73 0.1265	$30.38 \mid 0.1295$	31.06				
18.0	27.89 0.1108	28.44 0.113	29.03 0.1159	$29.63 \mid 0.1184$	30.28 0.1211				
19.0	27.29 0.1024	27.81 0.1043	28.35 0.1064	28.92 0.1085	29.54 0.1113				
			$d_1 = 0.6 \text{ M}$						
$\alpha_{19\Phi}$	0.00	0.04	$\frac{\rho}{0.05}$	0.00	0.05				
	0.03	0.04		0.06	0.07				
9.0	21.7 0.1736	22.18 0.1777		23.22 0.1868	23.79 0.1918				
10.0	21.1 0.1483	The state of the s		22.46 0.1584	22.97 0.1621				
$11.0 \\ 12.0$	$\begin{array}{c c} 20.57 0.1289 \\ 20.11 0.1143 \end{array}$	20.96 0.1314 $20.48 0.1164$		$ \begin{array}{c} 21.83 0.1373 \\ 21.27 0.1208 \end{array} $	$\begin{array}{c} 22.29 0.1403 \\ 21.7 0.1232 \end{array}$				
13.0	19.7 0.1026	20.45 0.1104 $20.05 0.104$	· ·	20.79 0.1208	21.7 0.1232 $21.19 0.1101$				
14.0	19.31 0.093	19.64 0.0945		20.79 0.1031 $20.34 0.0978$	20.72 0.0995				
15.0	18.95 0.085	19.26 0.0863		19.93 0.0892	20.29 0.0907				
16.0	18.6 0.0782	18.9 0.0794		19.54 0.0819	19.88 0.0832				
17.0	18.27 0.0723	18.55 0.0734		19.16 0.0757	19.49 0.0769				
18.0	17.93 0.0671	18.21 0.0681	· ·	18.8 0.0703	19.11 0.0714				
19.0	17.61 0.0627	The state of the s	*.	18.44 0.0654	18.74 0.0664				
			$d_1 = 0.7 \text{ M}$						
$\alpha_{19\Phi}$	റ റൗ	0.04	$\frac{ ho}{0.05}$	0.06	0.07				
9.0	$\frac{0.03}{14.72 0.1092}$	$\frac{0.04}{14.97 0.111}$	$\frac{0.05}{15.24 0.1128}$	$\frac{0.06}{15.51 0.1147}$	$\frac{0.07}{15.79 0.1167}$				
10.0	14.42 0.0955	14.65 0.097	14.9 0.0985	15.16 0.1001	15.42 0.1017				
11.0	14.15 0.0846	14.37 0.0861	14.6 0.0874	14.84 0.0887	15.09 0.0901				
12.0	13.9 0.0762	14.11 0.0772	14.33 0.0783	14.56 0.0794	14.79 0.0806				
13.0	13.67 0.0692	13.87 0.0701	$\boldsymbol{14.08} \boldsymbol{0.071}$	14.3 0.072	14.53 0.0731				
14.0	13.45 0.0633	13.64 0.0641	13.84 0.065	14.06 0.0659	14.27 0.0668				
15.0	13.24 0.0583	13.42 0.0591	13.62 0.0598	$13.82 \mid 0.0606$	14.03 0.0615				
16.0	13.03 0.0541	13.21 0.0547	13.4 0.0554	13.59 0.0562	13.79 0.0569				
17.0	12.82 0.0503	13.0 0.0509	13.18 0.0516	13.37 0.0522	13.56 0.0529				
18.0	$12.62 \mid 0.0471$	12.79 0.0476	12.97 0.0482	13.15 0.0488	13.34 0.0494				
19.0	12.42 0.0442	12.58 0.0447	12.75 0.0452	$12.93 \mid 0.0458$	13.12 0.0464				

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$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$d_1 = 0.8 \text{ M}$									
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	α_{1ad}		0.00	0.04		ρ		0.00	0	0=
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$\begin{array}{c c c c c c c c c c c c c c c c c c c $,				
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	18.0	9.4	0.0356	9.52 0.	036	9.64 0.036	64	9.77 0.0368	9.9 0	0.0372
$\begin{array}{ c c c c c c c c c }\hline \alpha_{13} & 0.03 & 0.04 & 0.05 & 0.06 & 0.07 \\ \hline 9.0 & 8.23 0.0608 & 8.34 0.0615 & 8.45 0.0622 & 8.57 0.0629 & 8.69 0.0637 \\ \hline 10.0 & 8.11 0.0539 & 8.22 0.0545 & 8.33 0.0552 & 8.44 0.0559 & 8.56 0.0566 \\ \hline 11.0 & 7.99 0.0486 & 8.11 0.0491 & 8.21 0.0497 & 8.32 0.0502 & 8.43 0.0508 \\ \hline 12.0 & 7.89 0.0442 & 7.99 0.0447 & 8.1 0.0451 & 8.21 0.0456 & 8.32 0.0461 \\ \hline 13.0 & 7.79 0.0405 & 7.89 0.0409 & 7.99 0.0413 & 8.1 0.0418 & 8.21 0.0422 \\ \hline 14.0 & 7.69 0.0373 & 7.79 0.0377 & 7.89 0.0381 & 7.99 0.0385 & 8.1 0.0389 \\ \hline 15.0 & 7.59 0.0346 & 7.69 0.0349 & 7.78 0.0353 & 7.88 0.0357 & 7.98 0.0361 \\ \hline 16.0 & 7.50 0.0322 & 7.59 0.0325 & 7.68 0.0329 & 7.78 0.0332 & 7.87 0.0336 \\ \hline 17.0 & 7.4 0.0301 & 7.48 0.0305 & 7.58 0.0308 & 7.67 0.0311 & 7.77 0.0314 \\ \hline 18.0 & 7.30 0.0283 & 7.38 0.0286 & 7.47 0.0289 & 7.56 0.0292 & 7.66 0.0295 \\ \hline 19.0 & 7.19 0.0267 & 7.28 0.027 & 7.37 0.0272 & 7.46 0.0275 & 7.55 0.0278 \\ \hline \hline 20.0 & 6.52 0.0493 & 6.6 0.0498 & 6.68 0.0503 & 6.77 0.0508 & 6.86 0.0514 \\ \hline 10.0 & 6.43 0.0397 & 6.44 0.0401 & 6.52 0.0449 & 6.68 0.0453 & 6.77 0.0458 \\ \hline 11.0 & 6.28 0.0361 & 6.36 0.0364 & 6.44 0.0368 & 6.52 0.0372 & 6.6 0.0376 \\ \hline 13.0 & 6.21 0.0331 & 6.28 0.0334 & 6.36 0.0338 & 6.44 0.0314 & 6.52 0.0345 \\ \hline 14.0 & 6.06 0.0284 & 6.14 0.0287 & 6.2 0.029 & 6.28 0.0293 & 6.36 0.0296 \\ \hline 16.0 & 5.98 0.0265 & 6.06 0.0268 & 6.13 0.027 & 6.2 0.0273 & 6.28 0.0296 \\ \hline 16.0 & 5.98 0.0265 & 6.06 0.0268 & 6.13 0.027 & 6.2 0.0273 & 6.28 0.0256 \\ \hline 17.0 & 5.9 0.0248 & 5.97 0.0251 & 6.05 0.0238 & 6.04 0.024 & 6.12 0.0243 \\ \hline 19.0 & 5.75 0.0221 & 5.81 0.0223 & 5.88 0.0225 & 5.95 0.0227 & 6.03 0.0229 \\ \hline 20.0 & 5.3 0.0413 & 5.36 0.0417 & 5.43 0.0421 & 5.5 0.0425 & 5.57 0.0249 \\ \hline 10.0 & 5.24 0.0369 & 5.3 0.0372 & 5.37 0.0376 & 5.43 0.0343 & 5.44 0.0366 \\ \hline 12.0 & 5.13 0.0343 & 5.24 0$	19.0	9.26	6 0.0335	9.38 0.0	339	9.5 0.034	3	9.62 0.0346	9.74	0.035
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$\begin{array}{ c c c c c c c c c c c c c c c c c c c$		10.0	11.10 0.02						1.00 0.021	
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$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	α_1	эф 📙	0.03	0	.04			0.06	0.07	7
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9.	.0	6.52 0.0493	6.6	0.0498	6.68 0.0	503	6.77 0.0508	6.86 0.0	0514
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10	0.0	6.43 0.0439			6.6 0.04	149		6.77 0.0	0458
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	11	.0	6.36 0.0397	6.44	0.0401	6.52 0.0	405	6.6 0.0409	6.68 0.0)413
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			6.28 0.0361	6.36	0.0364	6.44 0.0	368	$6.52 \mid 0.0372$		
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$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		0 4.96 0.024								
$18.0 4.78 0.0198 \qquad 4.83 0.02 \qquad 4.89 0.0202 \qquad 4.94 0.0204 \qquad \textbf{5.0} \textbf{0.0206}$										
$19.0 4.72 0.0187 \qquad 4.77 0.0189 \qquad 4.82 0.0191 \qquad 4.88 0.0192 \qquad 4.94 0.0194$,	
	19.	$\cup \mid 4$.72 0.0187	4.77 0	J.U189	4.82 0.01	191	4.88 0.0192	4.94 0.	0194

$d_1=1.2~{ m M}$							
$\alpha_{19\Phi}$	ρ						
атэф	0.03	0.04	0.05	0.06	0.07		
9.0	4.41 0.0355	4.46 0.0358	4.51 0.0361	4.57 0.0365	4.62 0.0368		
10.0	4.36 0.0318	4.41 0.0321	4.46 0.0324	4.52 0.0327	4.57 0.033		
11.0	4.32 0.0288	4.37 0.029	4.42 0.0293	4.47 0.0296	4.52 0.0298		
12.0	4.27 0.0263	4.32 0.0265	4.37 0.0267	4.42 0.027	4.48 0.0272		
13.0	4.23 0.0242	4.28 0.0244	4.33 0.0246	4.38 0.0248	4.43 0.025		
14.0	4.19 0.0224	4.23 0.0226	4.28 0.0228	4.33 0.023	4.38 0.0232		
15.0	4.14 0.0208	4.19 0.021	4.23 0.0212	4.28 0.0214	4.33 0.0216		
16.0	$4.09 \mid 0.0195$	4.14 0.0197	4.18 0.0198	4.23 0.02	4.28 0.0202		
17.0	$4.04 \mid 0.0183$	$4.09 \mid 0.0185$	4.14 0.0186	4.18 0.0188	4.23 0.0189		
18.0	3.96 0.0172	$4.04 \mid 0.0174$	$4.08 \mid 0.0175$	4.13 0.0177	4.18 0.0178		
19.0	$3.91 \mid 0.0163$	3.96 0.0164	$\boldsymbol{4.03 0.0166}$	$4.08 \mid 0.0167$	4.12 0.0169		