

# A Comparative Study of Low-Dissipation Numerical Schemes for Hyperbolic Conservation Laws

Shaoshuai Chu\* and Michael Herty†

## Abstract

This work provides a comparative assessment of several low-dissipation numerical schemes for hyperbolic conservation laws, highlighting their performance relative to the classical Harten–Lax–van Leer (HLL) schemes. The schemes under consideration include the classical Harten–Lax–van Leer–Contact (HLLC), the recently proposed TV flux splitting, the low-dissipation Central-Upwind (LDCU), and the local characteristic decomposition-based Central-Upwind (LCDCU) schemes. These methods are extended to higher orders of accuracy, up to the fifth order, within both finite-volume and finite-difference frameworks. A series of numerical experiments for the one- and two-dimensional Euler equations of gas dynamics are performed to evaluate the accuracy, robustness, and computational efficiency of the studied schemes. The comparison highlights the trade-offs between resolution of contact and shear waves, robustness in the presence of shocks, and computational cost. The investigated low-dissipation schemes show comparable levels of numerical dissipation, with only subtle differences appearing in selected benchmark problems. The results provide practical guidance for selecting efficient low-dissipation solvers for the simulation of complex compressible flows.

**Keywords:** Hyperbolic conservation laws, HLL and HLLC solvers, TV flux splitting scheme, Low-dissipation Central-Upwind scheme, Local characteristic decomposition-based Central-Upwind scheme

**AMS subject classification:** 35L65, 65M06, 65M08, 76M12, 76M20, 76L05, 76N15

## 1 Introduction

This paper focuses on the numerical solution of hyperbolic conservation laws, which in one and two spatial dimensions take the form

$$\mathbf{U}_t + \mathbf{F}(\mathbf{U})_x = \mathbf{0}, \quad (1.1)$$

and

$$\mathbf{U}_t + \mathbf{F}(\mathbf{U})_x + \mathbf{G}(\mathbf{U})_y = \mathbf{0}, \quad (1.2)$$

where  $t$  denotes time,  $x$  and  $y$  are spatial coordinates,  $\mathbf{U} \in \mathbb{R}^d$  is the vector of conserved variables, and  $\mathbf{F}, \mathbf{G} : \mathbb{R}^d \rightarrow \mathbb{R}^d$  are the flux functions in the  $x$ - and  $y$ -directions, respectively.

It is well-known that the systems (1.1) and (1.2) may involve complex wave patterns, including shocks, rarefactions, and contact discontinuities, even when the initial data are very smooth, which presents significant challenges for numerical methods. Traditional approaches, particularly first-order methods, often fail to capture these discontinuities accurately and require extremely fine meshes to produce reliable results.

Since the pioneering works [20, 24, 44], numerous methods have been developed to solve hyperbolic systems (1.1) and (1.2); for a detailed overview, see, e.g., the monographs and review papers [5, 29, 34, 45, 63, 70] and the references therein. The Harten–Lax–van Leer (HLL) solver from [28] is one of

\*Department of Mathematics, RWTH Aachen University, 52056, Aachen, Germany; chu@igpm.rwth-aachen.de

†Department of Mathematics, RWTH Aachen University, 52056, Aachen, Germany; Department of Mathematics and Applied Mathematics, University of Pretoria, Private Bag X20, Hatfield 0028, South Africa; herty@igpm.rwth-aachen.de

the most widely used approximate Riemann solvers for hyperbolic conservation laws. It replaces the exact Riemann solution, which may involve multiple nonlinear waves, by a simple two-wave model. Specifically, the solution is approximated by a single intermediate state separated from the left and right data by two waves propagating with estimated minimum and maximum signal velocities. The HLL flux is robust and positivity preserving, but the main drawback is that intermediate waves such as contact and shear discontinuities are excessively smeared, since they are not explicitly represented in the two-wave model. To overcome this limitation, the Harten–Lax–van Leer–Contact (HLLC) solver was introduced in [73], which extends the HLL framework by restoring the missing contact wave. The HLLC scheme thus consists of three waves, separating the solution into two intermediate states. The presence of the contact wave allows the solver to resolve contact discontinuities and shear layers more sharply, while maintaining the robustness and efficiency of the HLL scheme. Owing to this balance between accuracy and robustness, the HLLC flux has become one of the most popular approximate Riemann solvers for the compressible Euler equations and related hyperbolic systems.

Another important class of schemes is based on flux vector splitting. In the flux splitting methods, one can decompose fluxes into components corresponding to different wave families, such as shock, contact, and expansion waves, which makes them fundamental in computational fluid dynamics. This decomposition enhances the resolution of shock waves and discontinuities, which is crucial for accurate simulations of compressible flows; see, e.g., [1, 2, 17, 27, 50–53, 66, 75, 76, 79]. However, the classical flux splitting schemes (e.g., [1, 2, 66, 75, 76]) often struggle to resolve intermediate characteristic fields, leading to excessive dissipation or numerical artifacts, even though they are effective. To overcome these limitations, more advanced methods, such as the advection upstream splitting method (AUSM), have been developed (see, e.g., [50]), offering better handling of contact waves and improved resolution of wave patterns. AUSM has since garnered considerable attention and undergone refinement, with further developments [51–53]. Additionally, a flux splitting approach similar to AUSM was proposed in [79], and subsequent advancements have been recorded in works such as [17, 27, 35, 57], further enriching the field of computational fluid dynamics. Recently, a new flux splitting method, known as the TV splitting scheme for the one-dimensional (1-D) Euler equations of gas dynamics, was introduced in [74] and later extended to higher dimensions and orders in [10, 71]. The proposed schemes are characterized by their simplicity, robustness, and accuracy, offering significant improvements over existing flux splitting methods. In particular, they effectively capture contact and shear waves while precisely preserving isolated stationary contacts. Beyond their applications to high-dimensional Euler equations, it has also been extended to other systems, including magnetohydrodynamics and shallow water equations; see, e.g., [4, 16, 69, 72].

While flux splitting methods such as TV splitting focus on decomposing fluxes along characteristic fields, an alternative direction is offered by central schemes. These methods avoid explicit Riemann solvers altogether and instead compute fluxes through staggered or modified control volumes [3, 32, 46, 48, 56, 58]. Central schemes are easy to implement and broadly applicable, but they tend to suffer from relatively large numerical dissipation. To overcome this drawback, central-upwind (CU) schemes were developed in [39, 41], in which control volumes are adapted to local wave speeds. CU schemes retain the simplicity of central methods while achieving significantly improved accuracy. Further refinements include anti-diffusion corrections [36], dissipation switches [37], and more accurate wave-speed estimates [23]. Recently, two refinements of CU schemes have been proposed to further reduce dissipation. Low-dissipation CU (LDCU) schemes [14, 43] introduce a novel projection step based on subcell resolution, which sharply approximates contact waves while ensuring non-oscillatory behavior of the projected solution; see also, e.g., [12, 13, 38]. This significantly decreases dissipation in contact- and shear-dominated regions. In parallel, LCD-based CU (LCDCU) schemes [6] apply local characteristic decomposition to the diffusion term, which also leads to substantially improved resolution by further suppressing excessive numerical dissipation; see also, e.g., [9, 11].

As mentioned above, the HLLC, TV splitting, LDCU, and LCDCU schemes are low-dissipation numerical schemes for solving the hyperbolic conservation laws (1.1) and (1.2), and it is instructive to check the dissipations contained in these schemes by comparing the resolution of the computed numerical results in a series of benchmarks. To this end, we carry out a systematic comparative

study of the first-, second-, third-, and fifth-order HLL, HLLC, TV splitting, LCDCU, and LDCU schemes, focusing on their robustness, accuracy, and efficiency in resolving complex wave interactions in hyperbolic conservation laws. The second-order extension employs a piecewise linear interpolant for reconstructing one-sided point values, while the third- and fifth-order schemes are formulated within the finite-difference (FD) A-WENO framework. This framework effectively generalizes low-order finite-volume (FV) schemes to higher-order FD ones, especially in multidimensional settings, through its simple dimension-by-dimension reconstruction; see, e.g., [31, 33, 55].

The rest of this paper is organized as follows. In §2, we begin with a brief overview of the first-order HLL scheme for the 1-D Euler equations of gas dynamics and then extend it to second-, third-, and fifth-order accuracy. The corresponding HLLC, TV, LDCU, and LCDCU schemes are subsequently reviewed. In §3, we describe the two-dimensional (2-D) extensions of these schemes in a dimension-by-dimension manner. Finally, in §4, we present a number of 1-D and 2-D numerical results to compare their performance.

## 2 One-Dimensional Schemes

In this section, we consider the 1-D Euler equations of gas dynamics and briefly review the first-, second-, third-, and fifth-order 1-D HLL, HLLC, TV, LDCU, and LCDCU schemes, respectively. The 1-D Euler equations of gas dynamics read as (1.1) with

$$\mathbf{U} := (\rho, \rho u, E)^\top, \quad \text{and} \quad \mathbf{F}(\mathbf{U}) = (\rho u, \rho u^2 + p, u(E + p))^\top, \quad (2.1)$$

where  $\rho$ ,  $u$ ,  $p$ , and  $E$  are the density, velocity, pressure, and total energy, respectively. The system is completed through the following equations of state (EOS):

$$p = (\gamma - 1) \left[ E - \frac{1}{2} \rho u^2 \right], \quad (2.2)$$

where the parameter  $\gamma$  represents the specific heat ratio.

### 2.1 One-Dimensional HLL Schemes

We first briefly review the 1-D HLL scheme from [28] and show its high-order extensions.

#### 2.1.1 One-Dimensional First-Order HLL Scheme

Assume the computational domain is covered with uniform cells  $C_j := [x_{j-\frac{1}{2}}, x_{j+\frac{1}{2}}]$  with  $x_{j+\frac{1}{2}} - x_{j-\frac{1}{2}} \equiv \Delta x$  centered at  $x_j = (x_{j-\frac{1}{2}} + x_{j+\frac{1}{2}})/2$ ,  $j = 1, \dots, N$ , and the cell average values

$$\bar{\mathbf{U}}_j(t) := \frac{1}{\Delta x} \int_{C_j} \mathbf{U}(x, t) dx$$

are available at a certain time level  $t$ . The computed cell averages  $\bar{\mathbf{U}}_j$  of the 1-D system (1.1) are evolved in time by solving the following semi-discrete system of ordinary differential equations (ODEs):

$$\frac{d\bar{\mathbf{U}}_j}{dt} = -\frac{\mathcal{F}_{j+\frac{1}{2}}^{\text{FV}} - \mathcal{F}_{j-\frac{1}{2}}^{\text{FV}}}{\Delta x}, \quad (2.3)$$

where  $\mathcal{F}_{j+\frac{1}{2}}^{\text{FV}} = \mathcal{F}_{j+\frac{1}{2}}^{\text{FV}}(\mathbf{U}_{j+\frac{1}{2}}^-, \mathbf{U}_{j+\frac{1}{2}}^+)$  is the numerical flux, defined by

$$\mathcal{F}^{\text{FV}}(\mathbf{U}_{j+\frac{1}{2}}^-, \mathbf{U}_{j+\frac{1}{2}}^+) = \begin{cases} \mathbf{F}(\mathbf{U}_{j+\frac{1}{2}}^-), & a_{j+\frac{1}{2}}^- \geq 0, \\ \frac{a_{j+\frac{1}{2}}^+ \mathbf{F}(\mathbf{U}_{j+\frac{1}{2}}^-) - a_{j+\frac{1}{2}}^- \mathbf{F}(\mathbf{U}_{j+\frac{1}{2}}^+) + a_{j+\frac{1}{2}}^+ a_{j+\frac{1}{2}}^- (\mathbf{U}_{j+\frac{1}{2}}^+ - \mathbf{U}_{j+\frac{1}{2}}^-)}{a_{j+\frac{1}{2}}^+ - a_{j+\frac{1}{2}}^-}, & a_{j+\frac{1}{2}}^- \leq 0 \leq a_{j+\frac{1}{2}}^+, \\ \mathbf{F}(\mathbf{U}_{j+\frac{1}{2}}^+), & a_{j+\frac{1}{2}}^+ \leq 0, \end{cases} \quad (2.4)$$

where  $\mathbf{U}_{j+\frac{1}{2}}^\pm$  are the left/right-sided point values of  $\mathbf{U}$  at the cell interfaces  $x_{j+\frac{1}{2}}$ . For the first order scheme, we take  $\mathbf{U}_{j+\frac{1}{2}}^+ = \mathbf{U}_{j+1}$  and  $\mathbf{U}_{j+\frac{1}{2}}^- = \mathbf{U}_j$ . The one-sided local speeds of propagation  $a_{j+\frac{1}{2}}^\pm$  can be estimated by

$$a_{j+\frac{1}{2}}^+ = \max \left\{ u_{j+\frac{1}{2}}^+ + c_{j+\frac{1}{2}}^+, u_{j+\frac{1}{2}}^- + c_{j+\frac{1}{2}}^- \right\}, \quad a_{j+\frac{1}{2}}^- = \min \left\{ u_{j+\frac{1}{2}}^+ - c_{j+\frac{1}{2}}^+, u_{j+\frac{1}{2}}^- - c_{j+\frac{1}{2}}^- \right\}, \quad (2.5)$$

where

$$u_{j+\frac{1}{2}}^\pm = \frac{(\rho u)_{j+\frac{1}{2}}^\pm}{\rho_{j+\frac{1}{2}}^\pm}, \quad p_{j+\frac{1}{2}}^\pm = (\gamma - 1) \left[ E_{j+\frac{1}{2}}^\pm - \frac{1}{2} \rho_{j+\frac{1}{2}}^\pm (u_{j+\frac{1}{2}}^\pm)^2 \right], \quad c_{j+\frac{1}{2}}^\pm = \sqrt{\frac{\gamma p_{j+\frac{1}{2}}^\pm}{\rho_{j+\frac{1}{2}}^\pm}}.$$

### 2.1.2 One-Dimensional Second-Order HLL Scheme

We now extend the first-order HLL scheme introduced in §2.1 to the second order of accuracy. The resulting scheme (2.3)–(2.5) achieves second-order accuracy provided that the one-sided point values  $\mathbf{U}_{j+\frac{1}{2}}^\pm$ , used to compute the numerical flux  $\mathcal{F}_{j+\frac{1}{2}}^{\text{FV}}$ , are second-order accurate. To this end, we approximate  $\mathbf{U}_{j+\frac{1}{2}}^\pm$  using a piecewise linear interpolant

$$\tilde{\mathbf{U}}(x) = \bar{\mathbf{U}}_j + (\mathbf{U}_x)_j(x - x_j), \quad x \in C_j, \quad (2.6)$$

which leads to

$$\mathbf{U}_{j+\frac{1}{2}}^- = \bar{\mathbf{U}}_j + \frac{\Delta x}{2} (\mathbf{U}_x)_j, \quad \mathbf{U}_{j+\frac{1}{2}}^+ = \bar{\mathbf{U}}_{j+1} - \frac{\Delta x}{2} (\mathbf{U}_x)_{j+1}. \quad (2.7)$$

In order to ensure the reconstruction (2.6)–(2.7) is non-oscillatory, one needs to compute the slopes  $(\mathbf{U}_x)_j$  in (2.6) with the help of a nonlinear limiter. In all of the numerical experiments reported in §4, we have used a generalized minmod limiter [49, 58, 67]:

$$(\mathbf{U}_x)_j = \text{minmod} \left( \theta \frac{\bar{\mathbf{U}}_j - \bar{\mathbf{U}}_{j-1}}{\Delta x}, \frac{\bar{\mathbf{U}}_{j+1} - \bar{\mathbf{U}}_{j-1}}{2\Delta x}, \theta \frac{\bar{\mathbf{U}}_{j+1} - \bar{\mathbf{U}}_j}{\Delta x} \right), \quad \theta \in [1, 2], \quad (2.8)$$

applied in a component-wise manner. Here, the minmod function is defined as

$$\text{minmod}(z_1, z_2, \dots) := \begin{cases} \min_j \{z_j\} & \text{if } z_j > 0 \quad \forall j, \\ \max_j \{z_j\} & \text{if } z_j < 0 \quad \forall j, \\ 0 & \text{otherwise.} \end{cases} \quad (2.9)$$

The parameter  $\theta$  in (2.8) is used to control the amount of numerical viscosity present in the resulting scheme, and larger values of  $\theta$  correspond to sharper but, in general, more oscillatory reconstructions. In this paper, we use  $\theta = 1.3$ .

### 2.1.3 One-Dimensional Third-Order HLL Scheme

In this section, we extend the HLL scheme to the third-order accuracy in the framework of the FD A-WENO scheme introduced in [33] (see also [55]), which has been proven to be a powerful tool for generalizing low-order FV schemes to higher-order FD ones.

Following [33], the point values  $\mathbf{U}_j$  are evolved in time by solving the following system of ODEs:

$$\frac{d\mathbf{U}_j}{dt} = -\frac{\mathbf{H}_{j+\frac{1}{2}} - \mathbf{H}_{j-\frac{1}{2}}}{\Delta x}, \quad (2.10)$$

where  $\mathbf{H}_{j+\frac{1}{2}}$  is the (third-order accurate) numerical flux defined by

$$\mathbf{H}_{j+\frac{1}{2}} = \mathcal{F}_{j+\frac{1}{2}}^{\text{FV}} - \frac{1}{24} (\Delta x)^2 (\mathbf{F}_{xx})_{j+\frac{1}{2}}.$$

Here,  $\mathcal{F}_{j+\frac{1}{2}}^{\text{FV}}$  is the FV numerical flux as in (2.4) and  $(\mathbf{F}_{xx})_{j+\frac{1}{2}}$  is the higher-order correction term used to increase the order of the numerical flux. The correction term  $(\mathbf{F}_{xx})_{j+\frac{1}{2}}$  can be approximated with the help of the FV numerical fluxes  $\mathcal{F}_{j+\frac{1}{2}}^{\text{FV}}$ :

$$(\mathbf{F}_{xx})_{j+\frac{1}{2}} = \frac{1}{(\Delta x)^2} [\mathcal{F}_{j-\frac{1}{2}}^{\text{FV}} - 2\mathcal{F}_{j+\frac{1}{2}}^{\text{FV}} + \mathcal{F}_{j+\frac{3}{2}}^{\text{FV}}],$$

which has been proved to be more efficient than the old version

$$(\mathbf{F}_{xx})_{j+\frac{1}{2}} = \frac{1}{2(\Delta x)^2} [\mathbf{F}_{j-1} - \mathbf{F}_j - \mathbf{F}_{j+1} + \mathbf{F}_{j+2}],$$

where  $\mathbf{F}_j = \mathbf{F}(\mathbf{U}_j)$ , while affecting neither the accuracy nor the quality of resolution. The resulting scheme is third-order once the one-sided point values  $\mathbf{U}_{j+\frac{1}{2}}^\pm$  employed to compute the numerical flux  $\mathcal{F}_{j+\frac{1}{2}}^{\text{FV}}$  are third-order accurate. This can be done by implementing a certain nonlinear limiting procedure like the third-order WENO-type interpolation (see, e.g., [8, 21, 22, 47]) applied to the local characteristic variables; see [10, Appendix A] for a detailed explanation.

#### 2.1.4 One-Dimensional Fifth-Order HLL Scheme

According to [33], to achieve fifth-order accuracy, the point values  $\mathbf{U}_j$  are evolved in time by solving the system (2.10) with the (fifth-order accurate) numerical flux

$$\mathbf{H}_{j+\frac{1}{2}} = \mathcal{F}_{j+\frac{1}{2}}^{\text{FV}} - \frac{1}{24}(\Delta x)^2 (\mathbf{F}_{xx})_{j+\frac{1}{2}} + \frac{7}{5760}(\Delta x)^4 (\mathbf{F}_{xxxx})_{j+\frac{1}{2}},$$

where  $\mathcal{F}_{j+\frac{1}{2}}^{\text{FV}}$  is the FV numerical flux as in (2.4),  $(\mathbf{F}_{xx})_{j+\frac{1}{2}}$  and  $(\mathbf{F}_{xxxx})_{j+\frac{1}{2}}$  are the higher-order correction terms computed by the fourth- and second-order accurate FDs, respectively; see, e.g., [7, 15]. Here, we have used the following higher-order correction terms from [15]:

$$\begin{aligned} (\mathbf{F}_{xx})_{j+\frac{1}{2}} &= \frac{1}{12(\Delta x)^2} \left[ -\mathcal{F}_{j-\frac{3}{2}}^{\text{FV}} + 16\mathcal{F}_{j-\frac{1}{2}}^{\text{FV}} - 30\mathcal{F}_{j+\frac{1}{2}}^{\text{FV}} + 16\mathcal{F}_{j+\frac{3}{2}}^{\text{FV}} - \mathcal{F}_{j+\frac{5}{2}}^{\text{FV}} \right], \\ (\mathbf{F}_{xxxx})_{j+\frac{1}{2}} &= \frac{1}{(\Delta x)^4} \left[ \mathcal{F}_{j-\frac{3}{2}}^{\text{FV}} - 4\mathcal{F}_{j-\frac{1}{2}}^{\text{FV}} + 6\mathcal{F}_{j+\frac{1}{2}}^{\text{FV}} - 4\mathcal{F}_{j+\frac{3}{2}}^{\text{FV}} + \mathcal{F}_{j+\frac{5}{2}}^{\text{FV}} \right], \end{aligned}$$

which is more efficient than the old version:

$$\begin{aligned} (\mathbf{F}_{xx})_{j+\frac{1}{2}} &= \frac{1}{48(\Delta x)^2} \left[ -5\mathbf{F}_{j-2} + 39\mathbf{F}_{j-1} - 34\mathbf{F}_j - 34\mathbf{F}_{j+1} + 39\mathbf{F}_{j+2} - 5\mathbf{F}_{j+3} \right], \\ (\mathbf{F}_{xxxx})_{j+\frac{1}{2}} &= \frac{1}{2(\Delta x)^4} \left[ \mathbf{F}_{j-2} - 3\mathbf{F}_{j-1} + 2\mathbf{F}_j + 2\mathbf{F}_{j+1} - 3\mathbf{F}_{j+2} + \mathbf{F}_{j+3} \right]. \end{aligned}$$

In order to ensure the resulting scheme is fifth order, the one-sided point values  $\mathbf{U}_{j+\frac{1}{2}}^\pm$  employed to compute the numerical flux  $\mathcal{F}_{j+\frac{1}{2}}^{\text{FV}}$  need to be at least fifth-order accurate. This can be done by using a certain nonlinear limiting procedure like the fifth-order WENO-Z interpolation from [33, 55, 77] applied to the local characteristic variables; see [10, Appendix B] for details.

## 2.2 One-Dimensional HLLC Schemes

According to [73], the 1-D first-, second-, third-, and fifth-order HLLC schemes can be obtained similar to the corresponding HLL schemes by replacing the numerical fluxes  $\mathcal{F}_{j+\frac{1}{2}}^{\text{FV}}$  in (2.4) by

$$\mathcal{F}_{j+\frac{1}{2}}^{\text{FV}}(\mathbf{U}_{j+\frac{1}{2}}^-, \mathbf{U}_{j+\frac{1}{2}}^+) = \begin{cases} \mathbf{F}(\mathbf{U}_{j+\frac{1}{2}}^-), & a_{j+\frac{1}{2}}^- \geq 0, \\ \mathbf{F}(\mathbf{U}_{j+\frac{1}{2}}^-) + a_{j+\frac{1}{2}}^- (\mathbf{U}_{j+\frac{1}{2}}^{*, -} - \mathbf{U}_{j+\frac{1}{2}}^-), & a_{j+\frac{1}{2}}^- \leq 0 \leq a_{j+\frac{1}{2}}^*, \\ \mathbf{F}(\mathbf{U}_{j+\frac{1}{2}}^+) + a_{j+\frac{1}{2}}^+ (\mathbf{U}_{j+\frac{1}{2}}^{*, +} - \mathbf{U}_{j+\frac{1}{2}}^+), & a_{j+\frac{1}{2}}^* \leq 0 \leq a_{j+\frac{1}{2}}^+, \\ \mathbf{F}(\mathbf{U}_{j+\frac{1}{2}}^+), & a_{j+\frac{1}{2}}^+ \leq 0, \end{cases}$$

where

$$\mathbf{U}_{j+\frac{1}{2}}^{*,\pm} = \mathbf{U}_{j+\frac{1}{2}}^{\pm} \frac{a_{j+\frac{1}{2}}^{\pm} - u_{j+\frac{1}{2}}^{\pm}}{a_{j+\frac{1}{2}}^{\pm} - a_{j+\frac{1}{2}}^*},$$

and

$$a_{j+\frac{1}{2}}^* = \frac{p_{j+\frac{1}{2}}^+ - p_{j+\frac{1}{2}}^- + \rho_{j+\frac{1}{2}}^- u_{j+\frac{1}{2}}^- (a_{j+\frac{1}{2}}^- - u_{j+\frac{1}{2}}^-) - \rho_{j+\frac{1}{2}}^+ u_{j+\frac{1}{2}}^+ (a_{j+\frac{1}{2}}^+ - u_{j+\frac{1}{2}}^+)}{\rho_{j+\frac{1}{2}}^- (a_{j+\frac{1}{2}}^- - u_{j+\frac{1}{2}}^-) - \rho_{j+\frac{1}{2}}^+ (a_{j+\frac{1}{2}}^+ - u_{j+\frac{1}{2}}^+)}.$$

### 2.3 One-Dimensional TV Splitting Schemes

According to [10, 74], the 1-D first-, second-, third-, and fifth-order TV schemes can be obtained by replacing the numerical fluxes  $\mathcal{F}_{j+\frac{1}{2}}^{\text{FV}}$  in (2.4) by

$$\mathcal{F}_{j+\frac{1}{2}}^{\text{FV}}(\mathbf{U}_{j+\frac{1}{2}}^-, \mathbf{U}_{j+\frac{1}{2}}^+) = \mathcal{F}_{j+\frac{1}{2}}^A(\mathbf{U}_{j+\frac{1}{2}}^-, \mathbf{U}_{j+\frac{1}{2}}^+) + \mathcal{F}_{j+\frac{1}{2}}^P(\mathbf{U}_{j+\frac{1}{2}}^-, \mathbf{U}_{j+\frac{1}{2}}^+).$$

Here,  $\mathcal{F}_{j+\frac{1}{2}}^A(\mathbf{U}_{j+\frac{1}{2}}^-, \mathbf{U}_{j+\frac{1}{2}}^+)$  is the advection flux given by

$$\mathcal{F}_{j+\frac{1}{2}}^A(\mathbf{U}_{j+\frac{1}{2}}^-, \mathbf{U}_{j+\frac{1}{2}}^+) = \begin{cases} u_{j+\frac{1}{2}}^* \begin{pmatrix} \rho_{j+\frac{1}{2}}^- \\ (\rho u)_{j+\frac{1}{2}}^- \\ \frac{1}{2} \rho_{j+\frac{1}{2}}^- (u_{j+\frac{1}{2}}^-)^2 \end{pmatrix}, & \text{if } u_{j+\frac{1}{2}}^* \geq 0, \\ u_{j+\frac{1}{2}}^* \begin{pmatrix} \rho_{j+\frac{1}{2}}^+ \\ (\rho u)_{j+\frac{1}{2}}^+ \\ \frac{1}{2} \rho_{j+\frac{1}{2}}^+ (u_{j+\frac{1}{2}}^+)^2 \end{pmatrix}, & \text{otherwise,} \end{cases}$$

and  $\mathcal{F}_{j+\frac{1}{2}}^P(\mathbf{U}_{j+\frac{1}{2}}^-, \mathbf{U}_{j+\frac{1}{2}}^+)$  is the pressure flux given by

$$\mathcal{F}_{j+\frac{1}{2}}^P(\mathbf{U}_{j+\frac{1}{2}}^-, \mathbf{U}_{j+\frac{1}{2}}^+) = \begin{pmatrix} 0 \\ p_{j+\frac{1}{2}}^* \\ \frac{\gamma u_{j+\frac{1}{2}}^* p_{j+\frac{1}{2}}^*}{\gamma - 1} \end{pmatrix},$$

where

$$\begin{aligned} u_{j+\frac{1}{2}}^* &= \frac{C_{j+\frac{1}{2}}^+ u_{j+\frac{1}{2}}^+ - C_{j+\frac{1}{2}}^- u_{j+\frac{1}{2}}^-}{C_{j+\frac{1}{2}}^+ - C_{j+\frac{1}{2}}^-} - \frac{2}{C_{j+\frac{1}{2}}^+ - C_{j+\frac{1}{2}}^-} (p_{j+\frac{1}{2}}^+ - p_{j+\frac{1}{2}}^-), \\ p_{j+\frac{1}{2}}^* &= \frac{C_{j+\frac{1}{2}}^+ p_{j+\frac{1}{2}}^- - C_{j+\frac{1}{2}}^- p_{j+\frac{1}{2}}^+}{C_{j+\frac{1}{2}}^+ - C_{j+\frac{1}{2}}^-} + \frac{C_{j+\frac{1}{2}}^+ C_{j+\frac{1}{2}}^-}{2(C_{j+\frac{1}{2}}^+ - C_{j+\frac{1}{2}}^-)} (u_{j+\frac{1}{2}}^+ - u_{j+\frac{1}{2}}^-), \\ C_{j+\frac{1}{2}}^{\pm} &= \rho_{j+\frac{1}{2}}^{\pm} \left( u_{j+\frac{1}{2}}^{\pm} \pm \sqrt{(u_{j+\frac{1}{2}}^{\pm})^2 + 4(c_{j+\frac{1}{2}}^{\pm})^2} \right). \end{aligned}$$

### 2.4 One-Dimensional LDCU Schemes

According to [12, 14, 43], the 1-D first-, second-, third-, and fifth-order LDCU schemes can be obtained by replacing the numerical fluxes  $\mathcal{F}_{j+\frac{1}{2}}^{\text{FV}}$  in (2.4) by

$$\mathcal{F}_{j+\frac{1}{2}}^{\text{FV}}(\mathbf{U}_{j+\frac{1}{2}}^-, \mathbf{U}_{j+\frac{1}{2}}^+) = \frac{a_{j+\frac{1}{2}}^+ \mathbf{F}(\mathbf{U}_{j+\frac{1}{2}}^-) - a_{j+\frac{1}{2}}^- \mathbf{F}(\mathbf{U}_{j+\frac{1}{2}}^+)}{a_{j+\frac{1}{2}}^+ - a_{j+\frac{1}{2}}^-} + \frac{a_{j+\frac{1}{2}}^+ a_{j+\frac{1}{2}}^-}{a_{j+\frac{1}{2}}^+ - a_{j+\frac{1}{2}}^-} (\mathbf{U}_{j+\frac{1}{2}}^+ - \mathbf{U}_{j+\frac{1}{2}}^-) + \mathbf{q}_{j+\frac{1}{2}},$$

and the anti-diffusion term  $\mathbf{q}_{j+\frac{1}{2}}$  is given by (see, e.g., [14])

$$\mathbf{q}_{j+\frac{1}{2}} = \alpha_{j+\frac{1}{2}}^* q_{j+\frac{1}{2}}^\rho \left( 1, u_{j+\frac{1}{2}}^*, \frac{1}{2} (u_{j+\frac{1}{2}}^*)^2 \right)^\top.$$

Here,

$$q_{j+\frac{1}{2}}^\rho = \text{minmod}\left( (u_{j+\frac{1}{2}}^* - a_{j+\frac{1}{2}}^-)(\rho_{j+\frac{1}{2}}^* - \rho_{j+\frac{1}{2}}^-), (a_{j+\frac{1}{2}}^+ - u_{j+\frac{1}{2}}^*)(\rho_{j+\frac{1}{2}}^+ - \rho_{j+\frac{1}{2}}^+) \right),$$

$u_{j+\frac{1}{2}}^* = (\rho u)_{j+\frac{1}{2}}^*/\rho_{j+\frac{1}{2}}^*$  with  $\rho_{j+\frac{1}{2}}^*$  and  $(\rho u)_{j+\frac{1}{2}}^*$  being the first and second components of

$$\mathbf{U}_{j+\frac{1}{2}}^* = \frac{a_{j+\frac{1}{2}}^+ \mathbf{U}_{j+\frac{1}{2}}^+ - a_{j+\frac{1}{2}}^- \mathbf{U}_{j+\frac{1}{2}}^- - [\mathbf{F}(\mathbf{U}_{j+\frac{1}{2}}^+) - \mathbf{F}(\mathbf{U}_{j+\frac{1}{2}}^-)]}{a_{j+\frac{1}{2}}^+ - a_{j+\frac{1}{2}}^-},$$

$$\alpha_{j+\frac{1}{2}}^* = \begin{cases} \frac{a_{j+\frac{1}{2}}^+}{a_{j+\frac{1}{2}}^+ - u_{j+\frac{1}{2}}^*} & \text{if } u_{j+\frac{1}{2}}^* < 0, \\ \frac{a_{j+\frac{1}{2}}^-}{a_{j+\frac{1}{2}}^- - u_{j+\frac{1}{2}}^*} & \text{otherwise,} \end{cases}$$

and the minmod function is defined by  $\text{minmod}(a, b) := \frac{\text{sgn}(a) + \text{sgn}(b)}{2} \min(|a|, |b|)$ .

Finally, the one-sided local speeds of propagation  $a_{j+\frac{1}{2}}^\pm$  are slightly different from (2.5), and are defined by

$$a_{j+\frac{1}{2}}^+ = \max \left\{ u_{j+\frac{1}{2}}^+ + c_{j+\frac{1}{2}}^+, u_{j+\frac{1}{2}}^- + c_{j+\frac{1}{2}}^-, 0 \right\}, \quad a_{j+\frac{1}{2}}^- = \min \left\{ u_{j+\frac{1}{2}}^+ - c_{j+\frac{1}{2}}^+, u_{j+\frac{1}{2}}^- - c_{j+\frac{1}{2}}^-, 0 \right\}. \quad (2.11)$$

## 2.5 One-Dimensional LCDCU Schemes

According to [6, 7], the 1-D first-, second-, third-, and fifth-order LCDCU schemes can be obtained by replacing the numerical fluxes  $\mathcal{F}_{j+\frac{1}{2}}^{\text{FV}}$  in (2.4) by

$$\mathcal{F}_{j+\frac{1}{2}}^{\text{FV}}(\mathbf{U}_{j+\frac{1}{2}}^-, \mathbf{U}_{j+\frac{1}{2}}^+) = R_{j+\frac{1}{2}} P_{j+\frac{1}{2}}^{\text{LCD}} R_{j+\frac{1}{2}}^{-1} \mathbf{F}_{j+\frac{1}{2}}^- + R_{j+\frac{1}{2}} M_{j+\frac{1}{2}}^{\text{LCD}} R_{j+\frac{1}{2}}^{-1} \mathbf{F}_{j+\frac{1}{2}}^+ + R_{j+\frac{1}{2}} Q_{j+\frac{1}{2}}^{\text{LCD}} R_{j+\frac{1}{2}}^{-1} (\mathbf{U}_{j+\frac{1}{2}}^+ - \mathbf{U}_{j+\frac{1}{2}}^-).$$

The diagonal matrices  $P_{j+\frac{1}{2}}^{\text{LCD}}$ ,  $M_{j+\frac{1}{2}}^{\text{LCD}}$ , and  $Q_{j+\frac{1}{2}}^{\text{LCD}}$  are given by

$$P_{j+\frac{1}{2}}^{\text{LCD}} = \text{diag}((P_1^{\text{LCD}})_{j+\frac{1}{2}}, \dots, (P_d^{\text{LCD}})_{j+\frac{1}{2}}), \quad M_{j+\frac{1}{2}}^{\text{LCD}} = \text{diag}((M_1^{\text{LCD}})_{j+\frac{1}{2}}, \dots, (M_d^{\text{LCD}})_{j+\frac{1}{2}}),$$

$$Q_{j+\frac{1}{2}}^{\text{LCD}} = \text{diag}((Q_1^{\text{LCD}})_{j+\frac{1}{2}}, \dots, (Q_d^{\text{LCD}})_{j+\frac{1}{2}})$$

with

$$((P_i^{\text{LCD}})_{j+\frac{1}{2}}, (M_i^{\text{LCD}})_{j+\frac{1}{2}}, (Q_i^{\text{LCD}})_{j+\frac{1}{2}}) = \begin{cases} \frac{1}{(\lambda_i^+)_j - (\lambda_i^-)_j} ((\lambda_i^+)_j, -(\lambda_i^-)_j, (\lambda_i^+)_j (\lambda_i^-)_j) & \text{if } (\lambda_i^+)_j - (\lambda_i^-)_j > \varepsilon_0, \\ \left( \frac{1}{2}, \frac{1}{2}, 0 \right) & \text{otherwise,} \end{cases}$$

where

$$(\lambda_i^+)_j = \max \left\{ \lambda_i(A(\mathbf{U}_{j+\frac{1}{2}}^-)), \lambda_i(A(\mathbf{U}_{j+\frac{1}{2}}^+)), 0 \right\}, \quad i = 1, \dots, d.$$

$$(\lambda_i^-)_j = \min \left\{ \lambda_i(A(\mathbf{U}_{j+\frac{1}{2}}^-)), \lambda_i(A(\mathbf{U}_{j+\frac{1}{2}}^+)), 0 \right\},$$

Here,  $A(\mathbf{U}) = \frac{\partial \mathbf{F}}{\partial \mathbf{U}}(\mathbf{U})$  is the Jacobian,  $\lambda_1(A(\mathbf{U})) \leq \dots \lambda_d(A(\mathbf{U}))$  are its eigenvalues, and the matrices  $R_{j+\frac{1}{2}}$  and  $R_{j+\frac{1}{2}}^{-1}$  are such that  $R_{j+\frac{1}{2}}^{-1} \hat{A}_{j+\frac{1}{2}} R_{j+\frac{1}{2}}$  is diagonal, where  $\hat{A}_{j+\frac{1}{2}} = A(\hat{\mathbf{U}}_{j+\frac{1}{2}})$  and  $\hat{\mathbf{U}}_{j+\frac{1}{2}}$  is either a simple average  $(\bar{\mathbf{U}}_j + \bar{\mathbf{U}}_{j+1})/2$  or another type of average of the  $\bar{\mathbf{U}}_j$  and  $\bar{\mathbf{U}}_{j+1}$  states. Finally,  $\varepsilon_0$  is a very small desingularization constant, which is taken  $\varepsilon_0 = 10^{-12}$  in all of the numerical examples reported in §4.

### 3 Two-Dimensional Schemes

We now present a 2-D overview of the HLL, HLLC, TV, LDCU, and LCDCU schemes for the 2-D Euler equations of gas dynamics, which read as

$$\mathbf{U}_t + \mathbf{F}(\mathbf{U})_x + \mathbf{G}(\mathbf{U})_y = \mathbf{0}, \quad (3.1)$$

with  $\mathbf{U} := (\rho, \rho u, \rho v, E)^\top$ ,  $\mathbf{F}(\mathbf{U}) = (\rho u, \rho u^2 + p, \rho uv, u(E+p))^\top$ , and  $\mathbf{G}(\mathbf{U}) = (\rho v, \rho uv, \rho v^2 + p, v(E+p))^\top$ . Here,  $v$  is the  $y$ -velocity and the rest of the notation is the same as in the 1-D case (2.1)–(2.2). The system is completed through the following EOS:

$$p = (\gamma - 1) \left[ E - \frac{\rho}{2}(u^2 + v^2) \right]. \quad (3.2)$$

#### 3.1 Two-Dimensional HLL Schemes

As in the 1-D case, we first briefly review the first-order 2-D HLL scheme from [28] and show its high-order extensions.

##### 3.1.1 Two-Dimensional First-Order HLL Scheme

Supposing that the computational domain is covered with uniform cells  $C_{j,k} := [x_{j-\frac{1}{2}}, x_{j+\frac{1}{2}}] \times [y_{k-\frac{1}{2}}, y_{k+\frac{1}{2}}]$  centered at  $(x_j, y_k) = ((x_{j-\frac{1}{2}} + x_{j+\frac{1}{2}})/2, (y_{k+\frac{1}{2}} + y_{k-\frac{1}{2}})/2)$  with  $x_{j+\frac{1}{2}} - x_{j-\frac{1}{2}} \equiv \Delta x$  and  $y_{k+\frac{1}{2}} - y_{k-\frac{1}{2}} \equiv \Delta y$  for all  $j, k$ , we assume that the cell averages

$$\bar{\mathbf{U}}_{j,k}(t) := \frac{1}{\Delta x \Delta y} \int_{C_{j,k}} \mathbf{U}(x, y, t) dx dy$$

are available at a certain time level  $t$ . The cell averages  $\bar{\mathbf{U}}_{j,k}$  are then evolved in time by numerically solving the following system of ODEs:

$$\frac{d\bar{\mathbf{U}}_{j,k}}{dt} = -\frac{\mathcal{F}_{j+\frac{1}{2},k}^{\text{FV}} - \mathcal{F}_{j-\frac{1}{2},k}^{\text{FV}}}{\Delta x} - \frac{\mathcal{G}_{j,k+\frac{1}{2}}^{\text{FV}} - \mathcal{G}_{j,k-\frac{1}{2}}^{\text{FV}}}{\Delta y}. \quad (3.3)$$

Here,  $\mathcal{F}_{j+\frac{1}{2},k}^{\text{FV}}(\mathbf{U}_{j+\frac{1}{2},k}^-, \mathbf{U}_{j+\frac{1}{2},k}^+)$  and  $\mathcal{G}_{j,k+\frac{1}{2}}^{\text{FV}}(\mathbf{U}_{j,k+\frac{1}{2}}^-, \mathbf{U}_{j,k+\frac{1}{2}}^+)$  are the numerical fluxes, defined by

$$\mathcal{F}^{\text{FV}}(\mathbf{U}_{j+\frac{1}{2},k}^-, \mathbf{U}_{j+\frac{1}{2},k}^+) = \begin{cases} \mathbf{F}(\mathbf{U}_{j+\frac{1}{2},k}^-), & a_{j+\frac{1}{2},k}^- \geq 0, \\ \frac{a_{j+\frac{1}{2},k}^+ \mathbf{F}(\mathbf{U}_{j+\frac{1}{2},k}^-) - a_{j+\frac{1}{2},k}^- \mathbf{F}(\mathbf{U}_{j+\frac{1}{2},k}^+) + a_{j+\frac{1}{2},k}^+ a_{j+\frac{1}{2},k}^- (\mathbf{U}_{j+\frac{1}{2},k}^+ - \mathbf{U}_{j+\frac{1}{2},k}^-)}{a_{j+\frac{1}{2},k}^+ - a_{j+\frac{1}{2},k}^-}, & a_{j+\frac{1}{2},k}^- \leq 0 \leq a_{j+\frac{1}{2},k}^+, \\ \mathbf{F}(\mathbf{U}_{j+\frac{1}{2},k}^+), & a_{j+\frac{1}{2},k}^+ \leq 0, \end{cases} \quad (3.4)$$

$$\mathcal{G}^{\text{FV}}(\mathbf{U}_{j,k+\frac{1}{2}}^-, \mathbf{U}_{j,k+\frac{1}{2}}^+) = \begin{cases} \mathbf{G}(\mathbf{U}_{j,k+\frac{1}{2}}^-), & b_{j,k+\frac{1}{2}}^- \geq 0, \\ \frac{b_{j,k+\frac{1}{2}}^+ \mathbf{G}(\mathbf{U}_{j,k+\frac{1}{2}}^-) - b_{j,k+\frac{1}{2}}^- \mathbf{G}(\mathbf{U}_{j,k+\frac{1}{2}}^+) + b_{j,k+\frac{1}{2}}^+ b_{j,k+\frac{1}{2}}^- (\mathbf{U}_{j,k+\frac{1}{2}}^+ - \mathbf{U}_{j,k+\frac{1}{2}}^-)}{b_{j,k+\frac{1}{2}}^+ - b_{j,k+\frac{1}{2}}^-}, & b_{j,k+\frac{1}{2}}^- \leq 0 \leq b_{j,k+\frac{1}{2}}^+, \\ \mathbf{G}(\mathbf{U}_{j,k+\frac{1}{2}}^+), & b_{j,k+\frac{1}{2}}^+ \leq 0, \end{cases} \quad (3.5)$$

where  $\mathbf{U}_{j+\frac{1}{2},k}^\pm$  and  $\mathbf{U}_{j,k+\frac{1}{2}}^\pm$  are the left/right-sided point values of  $\mathbf{U}$  at the cell interfaces  $(x_{j+\frac{1}{2}}, y_k)$  and  $(x_j, y_{k+\frac{1}{2}})$ , respectively. In the first-order scheme, we take  $\mathbf{U}_{j+\frac{1}{2},k}^+ = \mathbf{U}_{j+1,k}$ ,  $\mathbf{U}_{j,k+\frac{1}{2}}^+ = \mathbf{U}_{j,k+1}$ , and  $\mathbf{U}_{j+\frac{1}{2},k}^- = \mathbf{U}_{j,k+\frac{1}{2}}^- = \mathbf{U}_{j,k}$ .

Here, the one-sided local speeds of propagation  $a_{j+\frac{1}{2},k}^\pm$  and  $a_{j,k+\frac{1}{2}}^\pm$  can be estimated by

$$\begin{aligned} a_{j+\frac{1}{2},k}^+ &= \max \left\{ u_{j+\frac{1}{2},k}^+ + c_{j+\frac{1}{2},k}^+, u_{j+\frac{1}{2},k}^- + c_{j+\frac{1}{2},k}^- \right\}, \quad a_{j+\frac{1}{2},k}^- = \min \left\{ u_{j+\frac{1}{2},k}^+ - c_{j+\frac{1}{2},k}^+, u_{j+\frac{1}{2},k}^- - c_{j+\frac{1}{2},k}^- \right\}, \\ b_{j,k+\frac{1}{2}}^+ &= \max \left\{ v_{j,k+\frac{1}{2}}^+ + c_{j,k+\frac{1}{2}}^+, v_{j,k+\frac{1}{2}}^- + c_{j,k+\frac{1}{2}}^- \right\}, \quad b_{j,k+\frac{1}{2}}^- = \min \left\{ v_{j,k+\frac{1}{2}}^+ - c_{j,k+\frac{1}{2}}^+, v_{j,k+\frac{1}{2}}^- - c_{j,k+\frac{1}{2}}^- \right\}, \end{aligned} \quad (3.6)$$

where

$$\begin{aligned} u_{j+\frac{1}{2},k}^\pm &= \frac{(\rho u)_{j+\frac{1}{2},k}^\pm}{\rho_{j+\frac{1}{2},k}^\pm}, \quad u_{j,k+\frac{1}{2}}^\pm = \frac{(\rho u)_{j,k+\frac{1}{2}}^\pm}{\rho_{j,k+\frac{1}{2}}^\pm}, \quad v_{j+\frac{1}{2},k}^\pm = \frac{(\rho v)_{j+\frac{1}{2},k}^\pm}{\rho_{j+\frac{1}{2},k}^\pm}, \quad v_{j,k+\frac{1}{2}}^\pm = \frac{(\rho v)_{j,k+\frac{1}{2}}^\pm}{\rho_{j,k+\frac{1}{2}}^\pm}, \\ p_{j+\frac{1}{2},k}^\pm &= (\gamma - 1) \left[ E_{j+\frac{1}{2},k}^\pm - \frac{1}{2} \rho_{j+\frac{1}{2},k}^\pm \left( (u_{j+\frac{1}{2},k}^\pm)^2 + (v_{j+\frac{1}{2},k}^\pm)^2 \right) \right], \quad c_{j+\frac{1}{2},k}^\pm = \sqrt{\frac{\gamma p_{j+\frac{1}{2},k}^\pm}{\rho_{j+\frac{1}{2},k}^\pm}}, \\ p_{j,k+\frac{1}{2}}^\pm &= (\gamma - 1) \left[ E_{j,k+\frac{1}{2}}^\pm - \frac{1}{2} \rho_{j,k+\frac{1}{2}}^\pm \left( (u_{j,k+\frac{1}{2}}^\pm)^2 + (v_{j,k+\frac{1}{2}}^\pm)^2 \right) \right], \quad c_{j,k+\frac{1}{2}}^\pm = \sqrt{\frac{\gamma p_{j,k+\frac{1}{2}}^\pm}{\rho_{j,k+\frac{1}{2}}^\pm}}. \end{aligned}$$

### 3.1.2 Two-Dimensional Second-Order HLL Scheme

As in the 1-D case, the resulting scheme (3.3)–(3.6) is second-order accurate once the one-sided point values  $\mathbf{U}_{j+\frac{1}{2},k}^\pm$  and  $\mathbf{U}_{j,k+\frac{1}{2}}^\pm$  employed to compute the numerical fluxes (3.4)–(3.5) are second order. To this end, we approximate  $\mathbf{U}_{j+\frac{1}{2},k}^\pm$  and  $\mathbf{U}_{j,k+\frac{1}{2}}^\pm$  by

$$\tilde{\mathbf{U}}(x, y) = \bar{\mathbf{U}}_{j,k} + (\mathbf{U}_x)_{j,k}(x - x_j) + (\mathbf{U}_y)_{j,k}(y - y_k), \quad x \in C_{j,k},$$

which leads to

$$\begin{aligned} \mathbf{U}_{j+\frac{1}{2},k}^- &= \bar{\mathbf{U}}_{j,k} + \frac{\Delta x}{2} (\mathbf{U}_x)_{j,k}, \quad \mathbf{U}_{j+\frac{1}{2},k}^+ = \bar{\mathbf{U}}_{j+1,k} - \frac{\Delta x}{2} (\mathbf{U}_x)_{j+1,k}, \\ \mathbf{U}_{j,k+\frac{1}{2}}^- &= \bar{\mathbf{U}}_{j,k} + \frac{\Delta y}{2} (\mathbf{U}_y)_{j,k}, \quad \mathbf{U}_{j,k+\frac{1}{2}}^+ = \bar{\mathbf{U}}_{j,k+1} - \frac{\Delta y}{2} (\mathbf{U}_y)_{j,k+1}, \end{aligned}$$

where

$$\begin{aligned} (\mathbf{U}_x)_{j,k} &= \text{minmod} \left( \theta \frac{\bar{\mathbf{U}}_{j,k} - \bar{\mathbf{U}}_{j-1,k}}{\Delta x}, \frac{\bar{\mathbf{U}}_{j+1,k} - \bar{\mathbf{U}}_{j-1,k}}{2\Delta x}, \theta \frac{\bar{\mathbf{U}}_{j+1,k} - \bar{\mathbf{U}}_{j,k}}{\Delta x} \right), \\ (\mathbf{U}_y)_{j,k} &= \text{minmod} \left( \theta \frac{\bar{\mathbf{U}}_{j,k} - \bar{\mathbf{U}}_{j,k-1}}{\Delta y}, \frac{\bar{\mathbf{U}}_{j,k+1} - \bar{\mathbf{U}}_{j,k-1}}{2\Delta y}, \theta \frac{\bar{\mathbf{U}}_{j,k+1} - \bar{\mathbf{U}}_{j,k}}{\Delta y} \right). \end{aligned}$$

Here, the minmod function is defined by (2.9).

### 3.1.3 Two-Dimensional Third-Order HLL Scheme

Following [33], the point values  $\mathbf{U}_{j,k}$  are evolved in time by solving the following system of ODEs:

$$\frac{d\mathbf{U}_{j,k}}{dt} = -\frac{\mathbf{H}_{j+\frac{1}{2},k} - \mathbf{H}_{j-\frac{1}{2},k}}{\Delta x} - \frac{\mathbf{H}_{j,k+\frac{1}{2}} - \mathbf{H}_{j,k-\frac{1}{2}}}{\Delta y}, \quad (3.7)$$

where the numerical fluxes  $\mathbf{H}_{j+\frac{1}{2},k}$  and  $\mathbf{H}_{j,k+\frac{1}{2}}$  are defined by

$$\mathbf{H}_{j+\frac{1}{2},k} = \mathcal{F}_{j+\frac{1}{2},k}^{\text{FV}} - \frac{1}{24}(\Delta x)^2(\mathbf{F}_{xx})_{j+\frac{1}{2},k}, \quad \mathbf{H}_{j,k+\frac{1}{2}} = \mathcal{G}_{j,k+\frac{1}{2}}^{\text{FV}} - \frac{1}{24}(\Delta y)^2(\mathbf{G}_{yy})_{j,k+\frac{1}{2}}.$$

Here,  $\mathcal{F}_{j+\frac{1}{2},k}^{\text{FV}}$  and  $\mathcal{G}_{j,k+\frac{1}{2}}^{\text{FV}}$  are the FV numerical fluxes as in (3.4)–(3.5),  $(\mathbf{F}_{xx})_{j+\frac{1}{2},k}$  and  $(\mathbf{G}_{yy})_{j,k+\frac{1}{2}}$  are the higher-order correction terms computed by the numerical fluxes

$$\begin{aligned} (\mathbf{F}_{xx})_{j+\frac{1}{2},k} &= \frac{1}{(\Delta x)^2} [\mathcal{F}_{j-\frac{1}{2},k}^{\text{FV}} - 2\mathcal{F}_{j+\frac{1}{2},k}^{\text{FV}} + \mathcal{F}_{j+\frac{3}{2},k}^{\text{FV}}], \\ (\mathbf{G}_{yy})_{j,k+\frac{1}{2}} &= \frac{1}{(\Delta y)^2} [\mathcal{G}_{j,k-\frac{1}{2}}^{\text{FV}} - 2\mathcal{G}_{j,k+\frac{1}{2}}^{\text{FV}} + \mathcal{G}_{j,k+\frac{3}{2}}^{\text{FV}}], \end{aligned} \quad (3.8)$$

or the standard central FDs:

$$\begin{aligned} (\mathbf{F}_{xx})_{j+\frac{1}{2},k} &= \frac{1}{2(\Delta x)^2} [\mathbf{F}_{j-1,k} - \mathbf{F}_{j,k} - \mathbf{F}_{j+1,k} + \mathbf{F}_{j+2,k}], \\ (\mathbf{G}_{yy})_{j,k+\frac{1}{2}} &= \frac{1}{2(\Delta y)^2} [\mathbf{G}_{j,k-1} - \mathbf{G}_{j,k} - \mathbf{G}_{j,k+1} + \mathbf{G}_{j,k+2}]. \end{aligned} \quad (3.9)$$

As in the 1-D case, using (3.8) is more efficient than (3.9), without affecting the accuracy or the quality of resolution. To ensure the resulting scheme is third-order accurate, the one-sided point values  $\mathbf{U}_{j+\frac{1}{2},k}^\pm$  and  $\mathbf{U}_{j,k+\frac{1}{2}}^\pm$  are also computed using third-order WENO-type interpolation applied to the local characteristic variables. Note that this can be done in a “dimension-by-dimension” manner as in the 1-D case; we therefore omit the details for the sake of brevity.

### 3.1.4 Two-Dimensional Fifth-Order HLL Scheme

According to [33], the point values  $\mathbf{U}_{j,k}$  are evolved in time by solving the system of ODEs (3.7) with the following numerical fluxes  $\mathbf{H}_{j+\frac{1}{2},k}$  and  $\mathbf{H}_{j,k+\frac{1}{2}}$ :

$$\begin{aligned} \mathbf{H}_{j+\frac{1}{2},k} &= \mathcal{F}_{j+\frac{1}{2},k}^{\text{FV}} - \frac{1}{24}(\Delta x)^2(\mathbf{F}_{xx})_{j+\frac{1}{2},k} + \frac{7}{5760}(\Delta x)^4(\mathbf{F}_{xxxx})_{j+\frac{1}{2},k}, \\ \mathbf{H}_{j,k+\frac{1}{2}} &= \mathcal{G}_{j,k+\frac{1}{2}}^{\text{FV}} - \frac{1}{24}(\Delta y)^2(\mathbf{G}_{yy})_{j,k+\frac{1}{2}} + \frac{7}{5760}(\Delta y)^4(\mathbf{G}_{yyyy})_{j,k+\frac{1}{2}}. \end{aligned}$$

Here,  $\mathcal{F}_{j+\frac{1}{2},k}^{\text{FV}}$  and  $\mathcal{G}_{j,k+\frac{1}{2}}^{\text{FV}}$  are the FV numerical fluxes as in (3.4)–(3.5),  $(\mathbf{F}_{xx})_{j+\frac{1}{2},k}$ ,  $(\mathbf{F}_{xxxx})_{j+\frac{1}{2},k}$ ,  $(\mathbf{G}_{yy})_{j,k+\frac{1}{2}}$ ,  $(\mathbf{G}_{yyyy})_{j,k+\frac{1}{2}}$  are approximations of the second- and fourth-order spatial derivatives of  $\mathbf{F}$  at  $(x, y) = (x_{j+\frac{1}{2}}, y_k)$  and  $\mathbf{G}$  at  $(x, y) = (x_j, y_{k+\frac{1}{2}})$ , respectively. In this paper, we have used the following higher-order correction terms:

$$\begin{aligned} (\mathbf{F}_{xx})_{j+\frac{1}{2},k} &= \frac{1}{12(\Delta x)^2} \left[ -\mathcal{F}_{j-\frac{3}{2},k}^{\text{FV}} + 16\mathcal{F}_{j-\frac{1}{2},k}^{\text{FV}} - 30\mathcal{F}_{j+\frac{1}{2},k}^{\text{FV}} + 16\mathcal{F}_{j+\frac{3}{2},k}^{\text{FV}} - \mathcal{F}_{j+\frac{5}{2},k}^{\text{FV}} \right], \\ (\mathbf{F}_{xxxx})_{j+\frac{1}{2},k} &= \frac{1}{(\Delta x)^4} \left[ \mathcal{F}_{j-\frac{3}{2},k}^{\text{FV}} - 4\mathcal{F}_{j-\frac{1}{2},k}^{\text{FV}} + 6\mathcal{F}_{j+\frac{1}{2},k}^{\text{FV}} - 4\mathcal{F}_{j+\frac{3}{2},k}^{\text{FV}} + \mathcal{F}_{j+\frac{5}{2},k}^{\text{FV}} \right], \\ (\mathbf{G}_{yy})_{j,k+\frac{1}{2}} &= \frac{1}{12(\Delta y)^2} \left[ -\mathcal{G}_{j,k-\frac{3}{2}}^{\text{FV}} + 16\mathcal{G}_{j,k-\frac{1}{2}}^{\text{FV}} - 30\mathcal{G}_{j,k+\frac{1}{2}}^{\text{FV}} + 16\mathcal{G}_{j,k+\frac{3}{2}}^{\text{FV}} - \mathcal{G}_{j,k+\frac{5}{2}}^{\text{FV}} \right], \\ (\mathbf{G}_{yyyy})_{j,k+\frac{1}{2}} &= \frac{1}{(\Delta y)^4} \left[ \mathcal{G}_{j,k-\frac{3}{2}}^{\text{FV}} - 4\mathcal{G}_{j,k-\frac{1}{2}}^{\text{FV}} + 6\mathcal{G}_{j,k+\frac{1}{2}}^{\text{FV}} - 4\mathcal{G}_{j,k+\frac{3}{2}}^{\text{FV}} + \mathcal{G}_{j,k+\frac{5}{2}}^{\text{FV}} \right]. \end{aligned} \quad (3.10)$$

One can also compute the high-order correction terms using the standard FDs:

$$\begin{aligned} (\mathbf{F}_{xx})_{j+\frac{1}{2},k} &= \frac{1}{48(\Delta x)^2} (-5\mathbf{F}_{j-2,k} + 39\mathbf{F}_{j-1,k} - 34\mathbf{F}_{j,k} - 34\mathbf{F}_{j+1,k} + 39\mathbf{F}_{j+2,k} - 5\mathbf{F}_{j+3,k}), \\ (\mathbf{F}_{xxxx})_{j+\frac{1}{2},k} &= \frac{1}{2(\Delta x)^4} (\mathbf{F}_{j-2,k} - 3\mathbf{F}_{j-1,k} + 2\mathbf{F}_{j,k} + 2\mathbf{F}_{j+1,k} - 3\mathbf{F}_{j+2,k} + \mathbf{F}_{j+3,k}), \\ (\mathbf{G}_{yy})_{j,k+\frac{1}{2}} &= \frac{1}{48(\Delta y)^2} (-5\mathbf{G}_{j,k-2} + 39\mathbf{G}_{j,k-1} - 34\mathbf{G}_{j,k} - 34\mathbf{G}_{j,k+1} + 39\mathbf{G}_{j,k+2} - 5\mathbf{G}_{j,k+3}), \\ (\mathbf{G}_{yyyy})_{j,k+\frac{1}{2}} &= \frac{1}{2(\Delta y)^4} (\mathbf{G}_{j,k-2} - 3\mathbf{G}_{j,k-1} + 2\mathbf{G}_{j,k} + 2\mathbf{G}_{j,k+1} - 3\mathbf{G}_{j,k+2} + \mathbf{G}_{j,k+3}), \end{aligned} \quad (3.11)$$

where  $\mathbf{F}_{j,k} := \mathbf{F}(\mathbf{U}_{j,k})$  and  $\mathbf{G}_{j,k} := \mathbf{G}(\mathbf{U}_{j,k})$ . As in the 1-D case, using (3.10) is more efficient than (3.11); see, e.g., [15]. To achieve fifth-order accuracy, the one-sided point values  $\mathbf{U}_{j+\frac{1}{2},k}^\pm$  and  $\mathbf{U}_{j,k+\frac{1}{2}}^\pm$  employed to compute the numerical flux  $\mathcal{F}_{j+\frac{1}{2},k}^{\text{FV}}$  and  $\mathcal{G}_{j,k+\frac{1}{2}}^{\text{FV}}$  need to be at least fifth-order accurate. This can also be done in a “dimension-by-dimension” manner as in the 1-D case, we therefore omit the details for the sake of brevity.

### 3.2 Two-Dimensional HLLC Schemes

According to [73], the 2-D first-, second-, third-, and fifth-order HLLC schemes can be obtained by replacing the numerical fluxes  $\mathcal{F}_{j+\frac{1}{2},k}^{\text{FV}}$  and  $\mathcal{G}_{j,k+\frac{1}{2}}^{\text{FV}}$  in (3.4)–(3.5) by

$$\begin{aligned} \mathcal{F}_{j+\frac{1}{2},k}^{\text{FV}}(\mathbf{U}_{j+\frac{1}{2},k}^-, \mathbf{U}_{j+\frac{1}{2},k}^+) &= \begin{cases} \mathbf{F}(\mathbf{U}_{j+\frac{1}{2},k}^-), & a_{j+\frac{1}{2},k}^- \geq 0, \\ \mathbf{F}(\mathbf{U}_{j+\frac{1}{2},k}^-) + a_{j+\frac{1}{2},k}^-(\mathbf{U}_{j+\frac{1}{2},k}^{*,-} - \mathbf{U}_{j+\frac{1}{2},k}^-), & a_{j+\frac{1}{2},k}^- \leq 0 \leq a_{j+\frac{1}{2},k}^*, \\ \mathbf{F}(\mathbf{U}_{j+\frac{1}{2},k}^+) + a_{j+\frac{1}{2},k}^+(\mathbf{U}_{j+\frac{1}{2},k}^{*,+} - \mathbf{U}_{j+\frac{1}{2},k}^+), & a_{j+\frac{1}{2},k}^* \leq 0 \leq a_{j+\frac{1}{2},k}^+, \\ \mathbf{F}(\mathbf{U}_{j+\frac{1}{2},k}^+), & a_{j+\frac{1}{2},k}^+ \leq 0, \end{cases} \\ \mathcal{G}_{j,k+\frac{1}{2}}^{\text{FV}}(\mathbf{U}_{j,k+\frac{1}{2}}^-, \mathbf{U}_{j,k+\frac{1}{2}}^+) &= \begin{cases} \mathbf{G}(\mathbf{U}_{j,k+\frac{1}{2}}^-), & b_{j,k+\frac{1}{2}}^- \geq 0, \\ \mathbf{G}(\mathbf{U}_{j,k+\frac{1}{2}}^-) + b_{j,k+\frac{1}{2}}^-(\mathbf{U}_{j,k+\frac{1}{2}}^{*-} - \mathbf{U}_{j,k+\frac{1}{2}}^-), & b_{j,k+\frac{1}{2}}^- \leq 0 \leq b_{j,k+\frac{1}{2}}^*, \\ \mathbf{G}(\mathbf{U}_{j,k+\frac{1}{2}}^+) + b_{j,k+\frac{1}{2}}^+(\mathbf{U}_{j,k+\frac{1}{2}}^{*+} - \mathbf{U}_{j,k+\frac{1}{2}}^+), & b_{j,k+\frac{1}{2}}^* \leq 0 \leq b_{j,k+\frac{1}{2}}^+, \\ \mathbf{G}(\mathbf{U}_{j,k+\frac{1}{2}}^+), & b_{j,k+\frac{1}{2}}^+ \leq 0, \end{cases} \end{aligned}$$

where

$$\mathbf{U}_{j+\frac{1}{2},k}^{*,\pm} = \mathbf{U}_{j+\frac{1}{2},k}^\pm \frac{a_{j+\frac{1}{2},k}^\pm - u_{j+\frac{1}{2},k}^\pm}{a_{j+\frac{1}{2},k}^\pm - a_{j+\frac{1}{2},k}^*}, \quad \mathbf{U}_{j,k+\frac{1}{2}}^{*,\pm} = \mathbf{U}_{j,k+\frac{1}{2}}^\pm \frac{b_{j,k+\frac{1}{2}}^\pm - v_{j,k+\frac{1}{2}}^\pm}{b_{j,k+\frac{1}{2}}^\pm - b_{j,k+\frac{1}{2}}^*},$$

and

$$\begin{aligned} a_{j+\frac{1}{2},k}^* &= \frac{p_{j+\frac{1}{2},k}^+ - p_{j+\frac{1}{2},k}^- + \rho_{j+\frac{1}{2},k}^- u_{j+\frac{1}{2},k}^-(a_{j+\frac{1}{2},k}^- - u_{j+\frac{1}{2},k}^-) - \rho_{j+\frac{1}{2},k}^+ u_{j+\frac{1}{2},k}^+(a_{j+\frac{1}{2},k}^+ - u_{j+\frac{1}{2},k}^+)}{\rho_{j+\frac{1}{2},k}^-(a_{j+\frac{1}{2},k}^- - u_{j+\frac{1}{2},k}^-) - \rho_{j+\frac{1}{2},k}^+(a_{j+\frac{1}{2},k}^+ - u_{j+\frac{1}{2},k}^+)}, \\ b_{j,k+\frac{1}{2}}^* &= \frac{p_{j,k+\frac{1}{2}}^+ - p_{j,k+\frac{1}{2}}^- + \rho_{j,k+\frac{1}{2}}^- v_{j,k+\frac{1}{2}}^-(b_{j,k+\frac{1}{2}}^- - v_{j,k+\frac{1}{2}}^-) - \rho_{j,k+\frac{1}{2}}^+ v_{j,k+\frac{1}{2}}^+(b_{j,k+\frac{1}{2}}^+ - v_{j,k+\frac{1}{2}}^+)}{\rho_{j,k+\frac{1}{2}}^-(b_{j,k+\frac{1}{2}}^- - v_{j,k+\frac{1}{2}}^-) - \rho_{j,k+\frac{1}{2}}^+(b_{j,k+\frac{1}{2}}^+ - v_{j,k+\frac{1}{2}}^+)}. \end{aligned}$$

### 3.3 Two-Dimensional TV Splitting Schemes

According to [10, 71], the 2-D first-, second-, third-, and fifth-order TV schemes can be obtained by replacing the numerical fluxes  $\mathcal{F}_{j+\frac{1}{2},k}^{\text{FV}}$  and  $\mathcal{G}_{j,k+\frac{1}{2}}^{\text{FV}}$  in (3.4)–(3.5) by

$$\begin{aligned}\mathcal{F}_{j+\frac{1}{2},k}^{\text{FV}}(\mathbf{U}_{j+\frac{1}{2},k}^-, \mathbf{U}_{j+\frac{1}{2},k}^+) &= \mathcal{F}_{j+\frac{1}{2},k}^A(\mathbf{U}_{j+\frac{1}{2},k}^-, \mathbf{U}_{j+\frac{1}{2},k}^+) + \mathcal{F}_{j+\frac{1}{2},k}^P(\mathbf{U}_{j+\frac{1}{2},k}^-, \mathbf{U}_{j+\frac{1}{2},k}^+), \\ \mathcal{G}_{j,k+\frac{1}{2}}^{\text{FV}}(\mathbf{U}_{j,k+\frac{1}{2}}^-, \mathbf{U}_{j,k+\frac{1}{2}}^+) &= \mathcal{G}_{j,k+\frac{1}{2}}^A(\mathbf{U}_{j,k+\frac{1}{2}}^-, \mathbf{U}_{j,k+\frac{1}{2}}^+) + \mathcal{G}_{j,k+\frac{1}{2}}^P(\mathbf{U}_{j,k+\frac{1}{2}}^-, \mathbf{U}_{j,k+\frac{1}{2}}^+).\end{aligned}$$

Here,  $\mathcal{F}_{j+\frac{1}{2},k}^A(\mathbf{U}_{j+\frac{1}{2},k}^-, \mathbf{U}_{j+\frac{1}{2},k}^+)$  is the  $x$ -direction advection flux given by

$$\mathcal{F}_{j+\frac{1}{2},k}^A(\mathbf{U}_{j+\frac{1}{2},k}^-, \mathbf{U}_{j+\frac{1}{2},k}^+) = \begin{cases} u_{j+\frac{1}{2},k}^* \begin{pmatrix} \rho_{j+\frac{1}{2},k}^- \\ (\rho u)_{j+\frac{1}{2},k}^- \\ (\rho v)_{j+\frac{1}{2},k}^- \\ \frac{1}{2} \rho_{j+\frac{1}{2}}^- [(u_{j+\frac{1}{2},k}^-)^2 + (v_{j+\frac{1}{2},k}^-)^2] \end{pmatrix}, & \text{if } u_{j+\frac{1}{2},k}^* \geq 0, \\ u_{j+\frac{1}{2},k}^* \begin{pmatrix} \rho_{j+\frac{1}{2},k}^+ \\ (\rho u)_{j+\frac{1}{2},k}^+ \\ (\rho v)_{j+\frac{1}{2},k}^+ \\ \frac{1}{2} \rho_{j+\frac{1}{2}}^+ [(u_{j+\frac{1}{2},k}^+)^2 + (v_{j+\frac{1}{2},k}^+)^2] \end{pmatrix}, & \text{otherwise,} \end{cases}$$

and  $\mathcal{F}_{j+\frac{1}{2},k}^P(\mathbf{U}_{j+\frac{1}{2},k}^-, \mathbf{U}_{j+\frac{1}{2},k}^+)$  is the  $x$ -direction pressure flux given by

$$\mathcal{F}_{j+\frac{1}{2},k}^P(\mathbf{U}_{j+\frac{1}{2},k}^-, \mathbf{U}_{j+\frac{1}{2},k}^+) = \begin{pmatrix} 0 \\ p_{j+\frac{1}{2},k}^* \\ 0 \\ \frac{\gamma u_{j+\frac{1}{2},k}^* p_{j+\frac{1}{2},k}^*}{\gamma - 1} \end{pmatrix},$$

where

$$\begin{aligned}u_{j+\frac{1}{2},k}^* &= \frac{C_{j+\frac{1}{2},k}^+ u_{j+\frac{1}{2},k}^+ - C_{j+\frac{1}{2},k}^- u_{j+\frac{1}{2},k}^-}{C_{j+\frac{1}{2},k}^+ - C_{j+\frac{1}{2},k}^-} - \frac{2}{C_{j+\frac{1}{2},k}^+ - C_{j+\frac{1}{2},k}^-} (p_{j+\frac{1}{2},k}^+ - p_{j+\frac{1}{2},k}^-), \\ p_{j+\frac{1}{2},k}^* &= \frac{C_{j+\frac{1}{2},k}^+ p_{j+\frac{1}{2},k}^- - C_{j+\frac{1}{2},k}^- p_{j+\frac{1}{2},k}^+}{C_{j+\frac{1}{2},k}^+ - C_{j+\frac{1}{2},k}^-} + \frac{C_{j+\frac{1}{2},k}^+ C_{j+\frac{1}{2},k}^-}{2(C_{j+\frac{1}{2},k}^+ - C_{j+\frac{1}{2},k}^-)} (u_{j+\frac{1}{2},k}^+ - u_{j+\frac{1}{2},k}^-), \\ C_{j+\frac{1}{2},k}^\pm &= \rho_{j+\frac{1}{2},k}^\pm \left( u_{j+\frac{1}{2},k}^\pm \pm \sqrt{(u_{j+\frac{1}{2},k}^\pm)^2 + 4(c_{j+\frac{1}{2},k}^\pm)^2} \right).\end{aligned}$$

Similarly,  $\mathcal{G}_{j,k+\frac{1}{2}}^A(\mathbf{U}_{j,k+\frac{1}{2}}^-, \mathbf{U}_{j,k+\frac{1}{2}}^+)$  is the  $y$ -direction advection flux given by

$$\mathcal{G}_{j,k+\frac{1}{2}}^A(\mathbf{U}_{j,k+\frac{1}{2}}^-, \mathbf{U}_{j,k+\frac{1}{2}}^+) = \begin{cases} v_{j,k+\frac{1}{2}}^* \begin{pmatrix} \rho_{j,k+\frac{1}{2}}^- \\ (\rho u)_{j,k+\frac{1}{2}}^- \\ (\rho v)_{j,k+\frac{1}{2}}^- \\ \frac{1}{2}\rho_{j,k+\frac{1}{2}}^- [(u_{j,k+\frac{1}{2}}^-)^2 + (v_{j,k+\frac{1}{2}}^-)^2] \end{pmatrix}, & \text{if } v_{j,k+\frac{1}{2}}^* \geq 0, \\ v_{j,k+\frac{1}{2}}^* \begin{pmatrix} \rho_{j,k+\frac{1}{2}}^+ \\ (\rho u)_{j,k+\frac{1}{2}}^+ \\ (\rho v)_{j,k+\frac{1}{2}}^+ \\ \frac{1}{2}\rho_{j,k+\frac{1}{2}}^+ [(u_{j,k+\frac{1}{2}}^+)^2 + (v_{j,k+\frac{1}{2}}^+)^2] \end{pmatrix}, & \text{otherwise,} \end{cases}$$

and  $\mathcal{G}_{j,k+\frac{1}{2}}^P(\mathbf{U}_{j,k+\frac{1}{2}}^-, \mathbf{U}_{j,k+\frac{1}{2}}^+)$  is the  $y$ -direction pressure flux given by

$$\mathcal{G}_{j,k+\frac{1}{2}}^P(\mathbf{U}_{j,k+\frac{1}{2}}^-, \mathbf{U}_{j,k+\frac{1}{2}}^+) = \begin{pmatrix} 0 \\ 0 \\ p_{j,k+\frac{1}{2}}^* \\ \frac{\gamma v_{j,k+\frac{1}{2}}^* p_{j,k+\frac{1}{2}}^*}{\gamma - 1} \end{pmatrix},$$

where

$$\begin{aligned} v_{j,k+\frac{1}{2}}^* &= \frac{C_{j,k+\frac{1}{2}}^+ v_{j,k+\frac{1}{2}}^+ - C_{j,k+\frac{1}{2}}^- v_{j,k+\frac{1}{2}}^-}{C_{j,k+\frac{1}{2}}^+ - C_{j,k+\frac{1}{2}}^-} - \frac{2}{C_{j,k+\frac{1}{2}}^+ - C_{j,k+\frac{1}{2}}^-} (p_{j,k+\frac{1}{2}}^+ - p_{j,k+\frac{1}{2}}^-), \\ p_{j,k+\frac{1}{2}}^* &= \frac{C_{j,k+\frac{1}{2}}^+ p_{j,k+\frac{1}{2}}^- - C_{j,k+\frac{1}{2}}^- p_{j,k+\frac{1}{2}}^+}{C_{j,k+\frac{1}{2}}^+ - C_{j,k+\frac{1}{2}}^-} + \frac{C_{j,k+\frac{1}{2}}^+ C_{j,k+\frac{1}{2}}^-}{2(C_{j,k+\frac{1}{2}}^+ - C_{j,k+\frac{1}{2}}^-)} (v_{j,k+\frac{1}{2}}^+ - v_{j,k+\frac{1}{2}}^-), \\ C_{j,k+\frac{1}{2}}^\pm &= \rho_{j,k+\frac{1}{2}}^\pm \left( v_{j,k+\frac{1}{2}}^\pm \pm \sqrt{(v_{j,k+\frac{1}{2}}^\pm)^2 + 4(c_{j,k+\frac{1}{2}}^\pm)^2} \right). \end{aligned}$$

### 3.4 Two-Dimensional LDCU Schemes

According to [12, 14, 43], the 2-D first-, second-, third-, and fifth-order LDCU schemes can be obtained by replacing the numerical fluxes  $\mathcal{F}_{j+\frac{1}{2},k}^{\text{FV}}$  and  $\mathcal{G}_{j,k+\frac{1}{2}}^{\text{FV}}$  in (3.4)–(3.5) by

$$\begin{aligned} \mathcal{F}_{j+\frac{1}{2},k}^{\text{FV}}(\mathbf{U}_{j+\frac{1}{2},k}^-, \mathbf{U}_{j+\frac{1}{2},k}^+) &= \frac{a_{j+\frac{1}{2},k}^+ \mathbf{F}(\mathbf{U}_{j+\frac{1}{2},k}^-) - a_{j+\frac{1}{2},k}^- \mathbf{F}(\mathbf{U}_{j+\frac{1}{2},k}^+)}{a_{j+\frac{1}{2},k}^+ - a_{j+\frac{1}{2},k}^-} \\ &\quad + \frac{a_{j+\frac{1}{2},k}^+ a_{j+\frac{1}{2},k}^-}{a_{j+\frac{1}{2},k}^+ - a_{j+\frac{1}{2},k}^-} (\mathbf{U}_{j+\frac{1}{2},k}^+ - \mathbf{U}_{j+\frac{1}{2},k}^-) + \mathbf{q}_{j+\frac{1}{2},k}^x, \\ \mathcal{G}_{j,k+\frac{1}{2}}^{\text{FV}}(\mathbf{U}_{j,k+\frac{1}{2}}^-, \mathbf{U}_{j,k+\frac{1}{2}}^+) &= \frac{b_{j,k+\frac{1}{2}}^+ \mathbf{G}(\mathbf{U}_{j,k+\frac{1}{2}}^-) - b_{j,k+\frac{1}{2}}^- \mathbf{G}(\mathbf{U}_{j,k+\frac{1}{2}}^+)}{b_{j,k+\frac{1}{2}}^+ - b_{j,k+\frac{1}{2}}^-} \\ &\quad + \frac{b_{j,k+\frac{1}{2}}^+ b_{j,k+\frac{1}{2}}^-}{b_{j,k+\frac{1}{2}}^+ - b_{j,k+\frac{1}{2}}^-} (\mathbf{U}_{j,k+\frac{1}{2}}^+ - \mathbf{U}_{j,k+\frac{1}{2}}^-) + \mathbf{q}_{j,k+\frac{1}{2}}^y, \end{aligned}$$

where

$$\mathbf{q}_{j+\frac{1}{2},k}^x = \alpha_{j+\frac{1}{2},k}^* (q_{j+\frac{1}{2},k}^\rho, u_{j+\frac{1}{2},k}^*, q_{j+\frac{1}{2},k}^\rho, q_{j+\frac{1}{2},k}^{\rho v}, q_{j+\frac{1}{2},k}^E)^\top,$$

$$\mathbf{q}_{j,k+\frac{1}{2}}^y = \alpha_{j,k+\frac{1}{2}}^* (q_{j,k+\frac{1}{2}}^\rho, q_{j,k+\frac{1}{2}}^{\rho u}, v_{j,k+\frac{1}{2}}^*, q_{j,k+\frac{1}{2}}^\rho, q_{j,k+\frac{1}{2}}^E)^\top.$$

Here,

$$\begin{aligned} \mathbf{U}_{j+\frac{1}{2},k}^* &= \frac{a_{j+\frac{1}{2},k}^+ \mathbf{U}_{j+\frac{1}{2},k}^+ - a_{j+\frac{1}{2},k}^- \mathbf{U}_{j+\frac{1}{2},k}^- - [\mathbf{F}(\mathbf{U}_{j+\frac{1}{2},k}^+) - \mathbf{F}(\mathbf{U}_{j+\frac{1}{2},k}^-)]}{a_{j+\frac{1}{2},k}^+ - a_{j+\frac{1}{2},k}^-}, \quad u_{j+\frac{1}{2},k}^* = \frac{(\rho u)_{j+\frac{1}{2},k}^*}{\rho_{j+\frac{1}{2},k}^*}, \\ q_{j+\frac{1}{2},k}^\rho &= \text{minmod} \left( -a_{j+\frac{1}{2},k}^{*,-} (\rho_{j+\frac{1}{2},k}^* - \rho_{j+\frac{1}{2},k}^-), a_{j+\frac{1}{2},k}^{*,+} (\rho_{j+\frac{1}{2},k}^+ - \rho_{j+\frac{1}{2},k}^*) \right), \\ q_{j+\frac{1}{2},k}^{\rho v} &= \text{minmod} \left( -a_{j+\frac{1}{2},k}^{*,-} ((\rho v)_{j+\frac{1}{2},k}^* - (\rho v)_{j+\frac{1}{2},k}^-), a_{j+\frac{1}{2},k}^{*,+} ((\rho v)_{j+\frac{1}{2},k}^+ - (\rho v)_{j+\frac{1}{2},k}^*) \right), \\ q_{j+\frac{1}{2},k}^E &= \frac{a_{j+\frac{1}{2},k}^{*,+} a_{j+\frac{1}{2},k}^{*-}}{a_{j+\frac{1}{2},k}^+ - a_{j+\frac{1}{2},k}^-} \left\{ \frac{\left( (\rho v)_{j+\frac{1}{2},k}^* + \frac{q_{j+\frac{1}{2},k}^{\rho v}}{a_{j+\frac{1}{2},k}^{*,+}} \right)^2}{2 \left( \rho_{j+\frac{1}{2},k}^* + \frac{q_{j+\frac{1}{2},k}^{\rho v}}{a_{j+\frac{1}{2},k}^{*,+}} \right)} - \frac{\left( (\rho v)_{j+\frac{1}{2},k}^* + \frac{q_{j+\frac{1}{2},k}^{\rho v}}{a_{j+\frac{1}{2},k}^{*-}} \right)^2}{2 \left( \rho_{j+\frac{1}{2},k}^* + \frac{q_{j+\frac{1}{2},k}^{\rho v}}{a_{j+\frac{1}{2},k}^{*-}} \right)} \right\} + \frac{(u_{j+\frac{1}{2},k}^*)^2}{2} q_{j+\frac{1}{2},k}^\rho, \end{aligned}$$

and

$$\alpha_{j+\frac{1}{2},k}^* = \begin{cases} \frac{a_{j+\frac{1}{2},k}^+}{a_{j+\frac{1}{2},k}^{*,+}} & \text{if } u_{j+\frac{1}{2},k}^* < 0, \\ \frac{a_{j+\frac{1}{2},k}^-}{a_{j+\frac{1}{2},k}^{*,+}} & a_{j+\frac{1}{2},k}^{*,\pm} = a_{j+\frac{1}{2},k}^\pm - u_{j+\frac{1}{2},k}^*. \\ \frac{a_{j+\frac{1}{2},k}^-}{a_{j+\frac{1}{2},k}^{*-}} & \text{otherwise,} \\ \frac{a_{j+\frac{1}{2},k}^{*-}}{a_{j+\frac{1}{2},k}^+} \end{cases}$$

Similarly,

$$\begin{aligned} \mathbf{U}_{j,k+\frac{1}{2}}^* &= \frac{b_{j,k+\frac{1}{2}}^+ \mathbf{U}_{j,k+\frac{1}{2}}^+ - b_{j,k+\frac{1}{2}}^- \mathbf{U}_{j,k+\frac{1}{2}}^- - [\mathbf{G}(\mathbf{U}_{j,k+\frac{1}{2}}^+) - \mathbf{G}(\mathbf{U}_{j,k+\frac{1}{2}}^-)]}{b_{j,k+\frac{1}{2}}^+ - b_{j,k+\frac{1}{2}}^-}, \quad v_{j,k+\frac{1}{2}}^* = \frac{(\rho v)_{j,k+\frac{1}{2}}^*}{\rho_{j,k+\frac{1}{2}}^*}, \\ q_{j,k+\frac{1}{2}}^\rho &= \text{minmod} \left( -b_{j,k+\frac{1}{2}}^{*,-} (\rho_{j,k+\frac{1}{2}}^* - \rho_{j,k+\frac{1}{2}}^-), b_{j,k+\frac{1}{2}}^{*,+} (\rho_{j,k+\frac{1}{2}}^+ - \rho_{j,k+\frac{1}{2}}^*) \right), \\ q_{j,k+\frac{1}{2}}^{\rho u} &= \text{minmod} \left( -b_{j,k+\frac{1}{2}}^{*,-} ((\rho u)_{j,k+\frac{1}{2}}^* - (\rho u)_{j,k+\frac{1}{2}}^-), b_{j,k+\frac{1}{2}}^{*,+} ((\rho u)_{j,k+\frac{1}{2}}^+ - (\rho u)_{j,k+\frac{1}{2}}^*) \right), \\ q_{j,k+\frac{1}{2}}^E &= \frac{b_{j,k+\frac{1}{2}}^{*,+} b_{j,k+\frac{1}{2}}^{*-}}{b_{j,k+\frac{1}{2}}^+ - b_{j,k+\frac{1}{2}}^-} \left\{ \frac{\left( (\rho u)_{j,k+\frac{1}{2}}^* + \frac{q_{j,k+\frac{1}{2}}^{\rho u}}{b_{j,k+\frac{1}{2}}^{*,+}} \right)^2}{2 \left( \rho_{j,k+\frac{1}{2}}^* + \frac{q_{j,k+\frac{1}{2}}^{\rho u}}{b_{j,k+\frac{1}{2}}^{*,+}} \right)} - \frac{\left( (\rho u)_{j,k+\frac{1}{2}}^* + \frac{q_{j,k+\frac{1}{2}}^{\rho u}}{b_{j,k+\frac{1}{2}}^{*-}} \right)^2}{2 \left( \rho_{j,k+\frac{1}{2}}^* + \frac{q_{j,k+\frac{1}{2}}^{\rho u}}{b_{j,k+\frac{1}{2}}^{*-}} \right)} \right\} + \frac{(v_{j,k+\frac{1}{2}}^*)^2}{2} q_{j,k+\frac{1}{2}}^\rho, \end{aligned}$$

and

$$\alpha_{j,k+\frac{1}{2}}^* = \begin{cases} \frac{b_{j,k+\frac{1}{2}}^+}{b_{j,k+\frac{1}{2}}^{*,+}} & \text{if } v_{j,k+\frac{1}{2}}^* < 0, \\ \frac{b_{j,k+\frac{1}{2}}^-}{b_{j,k+\frac{1}{2}}^{*,+}} & b_{j,k+\frac{1}{2}}^{*,\pm} = b_{j,k+\frac{1}{2}}^\pm - v_{j,k+\frac{1}{2}}^*. \\ \frac{b_{j,k+\frac{1}{2}}^-}{b_{j,k+\frac{1}{2}}^{*-}} & \text{otherwise,} \\ \frac{b_{j,k+\frac{1}{2}}^{*-}}{b_{j,k+\frac{1}{2}}^+} \end{cases}$$

Finally, the one-sided local speeds of propagation  $a_{j+\frac{1}{2},k}^\pm$  and  $b_{j,k+\frac{1}{2}}^\pm$  are slightly different from (3.6), and defined by

$$\begin{aligned} a_{j+\frac{1}{2},k}^+ &= \max \left\{ u_{j+\frac{1}{2},k}^+ + c_{j+\frac{1}{2},k}^+, u_{j+\frac{1}{2},k}^- + c_{j+\frac{1}{2},k}^-, 0 \right\}, \quad a_{j+\frac{1}{2},k}^- = \min \left\{ u_{j+\frac{1}{2},k}^+ - c_{j+\frac{1}{2},k}^+, u_{j+\frac{1}{2},k}^- - c_{j+\frac{1}{2},k}^-, 0 \right\}, \\ b_{j,k+\frac{1}{2}}^+ &= \max \left\{ v_{j,k+\frac{1}{2}}^+ + c_{j,k+\frac{1}{2}}^+, v_{j,k+\frac{1}{2}}^- + c_{j,k+\frac{1}{2}}^-, 0 \right\}, \quad b_{j,k+\frac{1}{2}}^- = \min \left\{ v_{j,k+\frac{1}{2}}^+ - c_{j,k+\frac{1}{2}}^+, v_{j,k+\frac{1}{2}}^- - c_{j,k+\frac{1}{2}}^-, 0 \right\}. \end{aligned} \quad (3.12)$$

### 3.5 Two-Dimensional LCDCU Schemes

According to [6, 7], the 2-D first-, second-, third-, and fifth-order LCDCU schemes can be obtained by replacing the numerical fluxes  $\mathcal{F}_{j+\frac{1}{2},k}^{\text{FV}}$  and  $\mathcal{G}_{j,k+\frac{1}{2}}^{\text{FV}}$  in (3.4)–(3.5) by

$$\begin{aligned} \mathcal{F}_{j+\frac{1}{2},k}^{\text{FV}}(\mathbf{U}_{j+\frac{1}{2},k}^-, \mathbf{U}_{j+\frac{1}{2},k}^+) &= R_{j+\frac{1}{2}} P_{j+\frac{1}{2},k}^{\text{LCD}} R_{j+\frac{1}{2},k}^{-1} \mathbf{F}_{j+\frac{1}{2},k}^- + R_{j+\frac{1}{2}} M_{j+\frac{1}{2},k}^{\text{LCD}} R_{j+\frac{1}{2},k}^{-1} \mathbf{F}_{j+\frac{1}{2},k}^+ + R_{j+\frac{1}{2}} Q_{j+\frac{1}{2},k}^{\text{LCD}} R_{j+\frac{1}{2},k}^{-1} (\mathbf{U}_{j+\frac{1}{2},k}^+ - \mathbf{U}_{j+\frac{1}{2},k}^-), \\ \mathcal{G}_{j,k+\frac{1}{2}}^{\text{FV}}(\mathbf{U}_{j,k+\frac{1}{2}}^-, \mathbf{U}_{j,k+\frac{1}{2}}^+) &= R_{j,k+\frac{1}{2}} P_{j,k+\frac{1}{2}}^{\text{LCD}} R_{j,k+\frac{1}{2}}^{-1} \mathbf{G}_{j,k+\frac{1}{2}}^- + R_{j,k+\frac{1}{2}} M_{j,k+\frac{1}{2}}^{\text{LCD}} R_{j,k+\frac{1}{2}}^{-1} \mathbf{G}_{j,k+\frac{1}{2}}^+ + R_{j,k+\frac{1}{2}} Q_{j,k+\frac{1}{2}}^{\text{LCD}} R_{j,k+\frac{1}{2}}^{-1} (\mathbf{U}_{j,k+\frac{1}{2}}^+ - \mathbf{U}_{j,k+\frac{1}{2}}^-). \end{aligned}$$

The matrices  $R_{j+\frac{1}{2},k}$ ,  $R_{j+\frac{1}{2},k}^{-1}$  and  $R_{j,k+\frac{1}{2}}$ ,  $R_{j,k+\frac{1}{2}}^{-1}$  are the matrices such that  $R_{j+\frac{1}{2},k}^{-1} \hat{A}_{j+\frac{1}{2},k} R_{j+\frac{1}{2},k}$  and  $R_{j,k+\frac{1}{2}}^{-1} \hat{B}_{j,k+\frac{1}{2}} R_{j,k+\frac{1}{2}}$  are diagonal. Here,  $\hat{A}_{j+\frac{1}{2},k} = A(\hat{\mathbf{U}}_{j+\frac{1}{2},k})$ ,  $\hat{B}_{j,k+\frac{1}{2}} = B(\hat{\mathbf{U}}_{j,k+\frac{1}{2}})$  with  $A(\mathbf{U}) = \frac{\partial \mathbf{F}(\mathbf{U})}{\partial \mathbf{U}}$ ,  $B(\mathbf{U}) = \frac{\partial \mathbf{G}(\mathbf{U})}{\partial \mathbf{U}}$ , and  $\hat{\mathbf{U}}_{j+\frac{1}{2},k}$ ,  $\hat{\mathbf{U}}_{j,k+\frac{1}{2}}$  are either simple averages  $(\bar{\mathbf{U}}_{j,k} + \bar{\mathbf{U}}_{j+1,k})/2$ ,  $(\bar{\mathbf{U}}_{j,k} + \bar{\mathbf{U}}_{j,k+1})/2$  or another type of averages of  $\bar{\mathbf{U}}_{j,k}$ ,  $\bar{\mathbf{U}}_{j+1,k}$  and  $\bar{\mathbf{U}}_{j,k}$ ,  $\bar{\mathbf{U}}_{j,k+1}$  states, respectively. The diagonal matrices  $P_{j+\frac{1}{2},k}^{\text{LCD}}$ ,  $M_{j+\frac{1}{2},k}^{\text{LCD}}$ ,  $Q_{j+\frac{1}{2},k}^{\text{LCD}}$ ,  $P_{j,k+\frac{1}{2}}^{\text{LCD}}$ ,  $M_{j,k+\frac{1}{2}}^{\text{LCD}}$ , and  $Q_{j,k+\frac{1}{2}}^{\text{LCD}}$  are defined by

$$\begin{aligned} P_{j+\frac{1}{2},k}^{\text{LCD}} &= \text{diag} \left( (P_1^{\text{LCD}})_{j+\frac{1}{2},k}, \dots, (P_d^{\text{LCD}})_{j+\frac{1}{2},k} \right), & P_{j,k+\frac{1}{2}}^{\text{LCD}} &= \text{diag} \left( (P_1^{\text{LCD}})_{j,k+\frac{1}{2}}, \dots, (P_d^{\text{LCD}})_{j,k+\frac{1}{2}} \right), \\ M_{j+\frac{1}{2},k}^{\text{LCD}} &= \text{diag} \left( (M_1^{\text{LCD}})_{j+\frac{1}{2},k}, \dots, (M_d^{\text{LCD}})_{j+\frac{1}{2},k} \right), & M_{j,k+\frac{1}{2}}^{\text{LCD}} &= \text{diag} \left( (M_1^{\text{LCD}})_{j,k+\frac{1}{2}}, \dots, (M_d^{\text{LCD}})_{j,k+\frac{1}{2}} \right), \\ Q_{j+\frac{1}{2},k}^{\text{LCD}} &= \text{diag} \left( (Q_1^{\text{LCD}})_{j+\frac{1}{2},k}, \dots, (Q_d^{\text{LCD}})_{j+\frac{1}{2},k} \right), & Q_{j,k+\frac{1}{2}}^{\text{LCD}} &= \text{diag} \left( (Q_1^{\text{LCD}})_{j,k+\frac{1}{2}}, \dots, (Q_d^{\text{LCD}})_{j,k+\frac{1}{2}} \right), \end{aligned}$$

where

$$\begin{aligned} &\left( (P_i^{\text{LCD}})_{j+\frac{1}{2},k}, (M_i^{\text{LCD}})_{j+\frac{1}{2},k}, (Q_i^{\text{LCD}})_{j+\frac{1}{2},k} \right) \\ &= \begin{cases} \frac{1}{\Delta(\lambda_i)_{j+\frac{1}{2},k}} \left( (\lambda_i^+)_{j+\frac{1}{2},k}, -(\lambda_i^-)_{j+\frac{1}{2},k}, (\lambda_i^+)_{j+\frac{1}{2},k} (\lambda_i^-)_{j+\frac{1}{2},k} \right) & \text{if } \Delta(\lambda_i)_{j+\frac{1}{2},k} > \varepsilon_0, \\ \left( \frac{1}{2}, \frac{1}{2}, 0 \right) & \text{otherwise,} \end{cases} \\ &\left( (P_i^{\text{LCD}})_{j,k+\frac{1}{2}}, (M_i^{\text{LCD}})_{j,k+\frac{1}{2}}, (Q_i^{\text{LCD}})_{j,k+\frac{1}{2}} \right) \\ &= \begin{cases} \frac{1}{\Delta(\mu_i)_{j,k+\frac{1}{2}}} \left( (\mu_i^+)_{j,k+\frac{1}{2}}, -(\mu_i^-)_{j,k+\frac{1}{2}}, (\mu_i^+)_{j,k+\frac{1}{2}} (\mu_i^-)_{j,k+\frac{1}{2}} \right) & \text{if } \Delta(\mu_i)_{j,k+\frac{1}{2}} > \varepsilon_0, \\ \left( \frac{1}{2}, \frac{1}{2}, 0 \right) & \text{otherwise.} \end{cases} \end{aligned}$$

Here,  $\Delta(\lambda_i)_{j+\frac{1}{2},k} := (\lambda_i^+)_{j+\frac{1}{2},k} - (\lambda_i^-)_{j+\frac{1}{2},k}$ ,  $\Delta(\mu_i)_{j,k+\frac{1}{2}} := (\mu_i^+)_{j,k+\frac{1}{2}} - (\mu_i^-)_{j,k+\frac{1}{2}}$ , and

$$\begin{aligned} (\lambda_i^+)_{j+\frac{1}{2},k} &= \max \left\{ \lambda_i(A(\mathbf{U}_{j+\frac{1}{2},k}^-)), \lambda_i(A(\mathbf{U}_{j+\frac{1}{2},k}^+)), 0 \right\}, \\ (\lambda_i^-)_{j+\frac{1}{2},k} &= \min \left\{ \lambda_i(A(\mathbf{U}_{j+\frac{1}{2},k}^-)), \lambda_i(A(\mathbf{U}_{j+\frac{1}{2},k}^+)), 0 \right\}, \\ (\mu_i^+)_{j,k+\frac{1}{2}} &= \max \left\{ \lambda_i(A(\mathbf{U}_{j,k+\frac{1}{2}}^-)), \lambda_i(A(\mathbf{U}_{j,k+\frac{1}{2}}^+)), 0 \right\}, \\ (\mu_i^-)_{j,k+\frac{1}{2}} &= \min \left\{ \lambda_i(A(\mathbf{U}_{j,k+\frac{1}{2}}^-)), \lambda_i(A(\mathbf{U}_{j,k+\frac{1}{2}}^+)), 0 \right\}, \end{aligned}$$

where  $\lambda_i$  and  $\mu_i$  are the eigenvalues of the Jacobians  $A(\mathbf{U})$  and  $B(\mathbf{U})$ :  $\lambda_1(A) \leq \dots \leq \lambda_d(A)$  and  $\mu_1(B) \leq \dots \leq \mu_d(B)$ , respectively.

## 4 Numerical Examples

In this section, we test the studied first-, second-, third-, and fifth-order schemes on several numerical examples and compare their performances. For the sake of brevity, these schemes will be referred to as the 1-Order, 2-Order, 3-Order, and 5-Order schemes, respectively.

We numerically integrate the ODE systems (2.3), (2.10), (3.3), and (3.7) by the three-stage third-order strong stability preserving Runge-Kutta (SSP RK3) method (see, e.g., [25, 26]) and use the CFL number 0.45.

### 4.1 One-Dimensional Examples

We begin with the 1-D Euler equations of gas dynamics (1.1), (2.1)–(2.2). In all of the Examples 1–6, we take the specific heat ratio  $\gamma = 1.4$ .

#### Example 1—1-D Accuracy Test

In the first example taken from [10], we consider the system (1.1), (2.1)–(2.2) subject to the following periodic initial conditions,

$$\rho(x, 0) = 1 + \frac{1}{5} \sin(2\pi x), \quad u(x, 0) \equiv 1, \quad p(x, 0) \equiv 1.$$

The exact solution of this initial value problem is given by

$$\rho(x, t) = 1 + \frac{1}{5} \sin[2\pi(x - t)], \quad u(x, t) \equiv 1, \quad p(x, t) \equiv 1.$$

We first compute the numerical solution on the computational domain  $[-1, 1]$  until the final time  $t = 0.1$  by the 1-Order, 2-Order, 3-Order, and 5-Order schemes on a sequence of uniform meshes: 100, 200, and 400, measure the  $L^1$ -errors, and then compute the corresponding experimental convergence rates for the density. The obtained results are presented in Table 4.1, where one can clearly see that the expected order of accuracy is achieved for the studied schemes. At the same time, one can see that the four low-dissipation schemes are more accurate than the HLL counterparts.

**Remark 4.1** We stress that in order to achieve the fifth order of accuracy for the 5-Order scheme, we use smaller time steps with  $\Delta t \sim (\Delta x)^{\frac{5}{3}}$  to balance the spatial and temporal errors.

#### Example 2—Moving Contact Wave

In the second example, we consider the moving contact discontinuity problem from [36] with the following initial conditions:

$$(\rho, u, p)(x, 0) = \begin{cases} (1.4, 0.1, 1), & x < 0.5, \\ (1, 0.1, 1), & x > 0.5, \end{cases}$$

which is considered on the interval  $[0, 1]$  with the free boundary conditions at both ends.

We compute the numerical solutions until the final time  $t = 0.2$  by the 1-Order, 2-Order, 3-Order, and 5-Order schemes on a uniform mesh with  $\Delta x = 1/200$  and then plot them in Figure 4.1 together with the exact solution. As one can see, the numerical results computed by four low-dissipation schemes coincide and are better than those computed by the corresponding HLL schemes, even when they are extended to high orders.

Mesh	HLL, 1-Order		HLL, 2-Order		HLL, 3-Order		HLL, 5-Order	
	Error	Rate	Error	Rate	Error	Rate	Error	Rate
100	9.91e-03	—	1.01e-03	—	2.37e-05	—	7.01e-08	—
200	4.98e-03	0.992	2.46e-04	2.04	2.96e-06	3.00	2.20e-09	5.00
400	2.50e-03	0.996	5.98e-05	2.04	3.70e-07	3.00	6.86e-11	5.00
Mesh	HLLC, 1-Order		HLLC, 2-Order		HLLC, 3-Order		HLLC, 5-Order	
	Error	Rate	Error	Rate	Error	Rate	Error	Rate
100	7.99e-03	—	9.40e-04	—	1.99e-05	—	5.90e-08	—
200	4.03e-03	0.990	2.24e-04	2.07	2.49e-06	3.00	1.85e-09	5.00
400	2.02e-03	0.995	5.51e-05	2.03	3.12e-07	3.00	5.78e-11	5.00
Mesh	TV, 1-Order		TV, 2-Order		TV, 3-Order		TV, 5-Order	
	Error	Rate	Error	Rate	Error	Rate	Error	Rate
100	7.99e-03	—	9.40e-04	—	1.99e-05	—	5.90e-08	—
200	4.03e-03	0.990	2.24e-04	2.07	2.49e-06	3.00	1.85e-09	5.00
400	2.02e-03	0.995	5.51e-05	2.03	3.12e-07	3.00	5.78e-11	5.00
Mesh	LDCU, 1-Order		LDCU, 2-Order		LDCU, 3-Order		LDCU, 5-Order	
	Error	Rate	Error	Rate	Error	Rate	Error	Rate
100	7.99e-03	—	9.40e-04	—	1.99e-05	—	5.90e-08	—
200	4.03e-03	0.990	2.24e-04	2.07	2.49e-06	3.00	1.85e-09	5.00
400	2.02e-03	0.995	5.51e-05	2.03	3.12e-07	3.00	5.78e-11	5.00
Mesh	LCD CU, 1-Order		LCD CU, 2-Order		LCD CU, 3-Order		LCD CU, 5-Order	
	Error	Rate	Error	Rate	Error	Rate	Error	Rate
100	7.99e-03	—	9.40e-04	—	1.99e-05	—	5.90e-08	—
200	4.03e-03	0.990	2.24e-04	2.07	2.49e-06	3.00	1.85e-09	5.00
400	2.02e-03	0.995	5.51e-05	2.03	3.12e-07	3.00	5.78e-11	5.00

Table 4.1: Example 1: The  $L^1$ -errors and experimental convergence rates for the density  $\rho$  computed by the 1-Order, 2-Order, 3-Order, and 5-Order schemes.

### Example 3—Stationary Contact Wave, Traveling Shock and Rarefaction Wave

In the third example, we consider the strong shocks interaction problem proposed in [78]. The initial conditions,

$$(\rho, u, p)(x, 0) = \begin{cases} (1, -19.59745, 1000) & \text{if } x < 0.8, \\ (1, -19.59745, 0.01) & \text{otherwise,} \end{cases}$$

are prescribed in the computational domain  $[-1, 1]$ , in which free boundary conditions are implemented.

We compute the numerical solutions until the final time  $t = 0.03$  using the studied 1-Order, 2-Order, 3-Order, and 5-Order schemes on a uniform mesh with  $\Delta x = 1/20$ . The obtained numerical results are plotted in Figure 4.2, as well as the reference solution, which is obtained by the HLL scheme on a much finer mesh with  $\Delta x = 1/400$ , showing that the numerical results obtained with the four low-dissipation schemes are consistent with each other and outperform those produced by the corresponding HLL schemes, especially near the contact wave; see Figures 4.2 (bottom right), where we zoom at the neighborhood of the contact wave. When the studied schemes are extended to higher

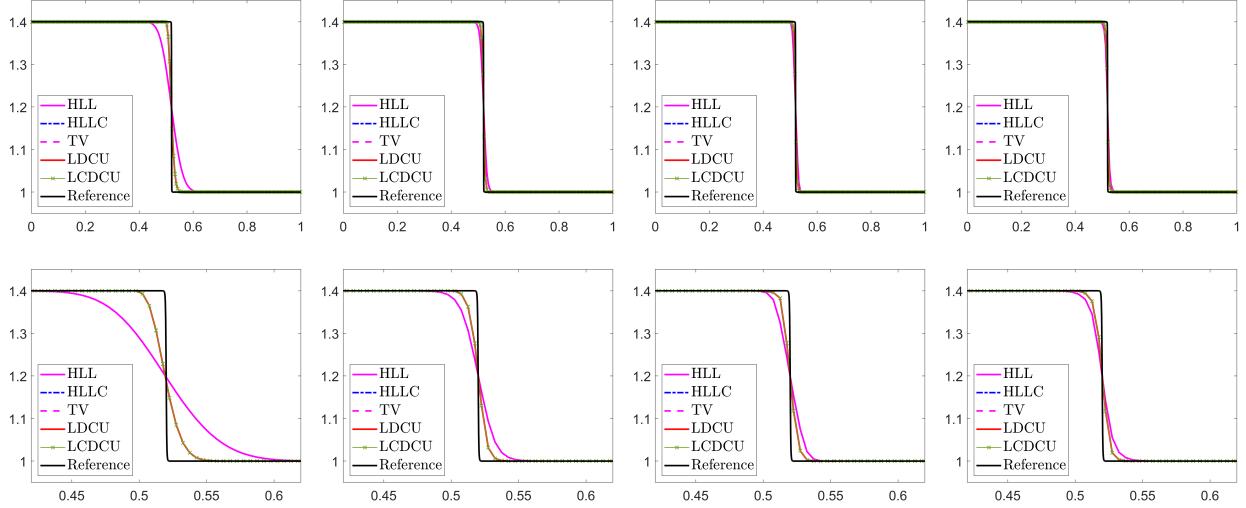


Figure 4.1: Example 2: Density  $\rho$  computed by the 1-Order, 2-Order, 3-Order and 5-Order schemes (top row) and zoom at  $[0.42, 0.62]$  (bottom row).

orders, there differences are very limited.

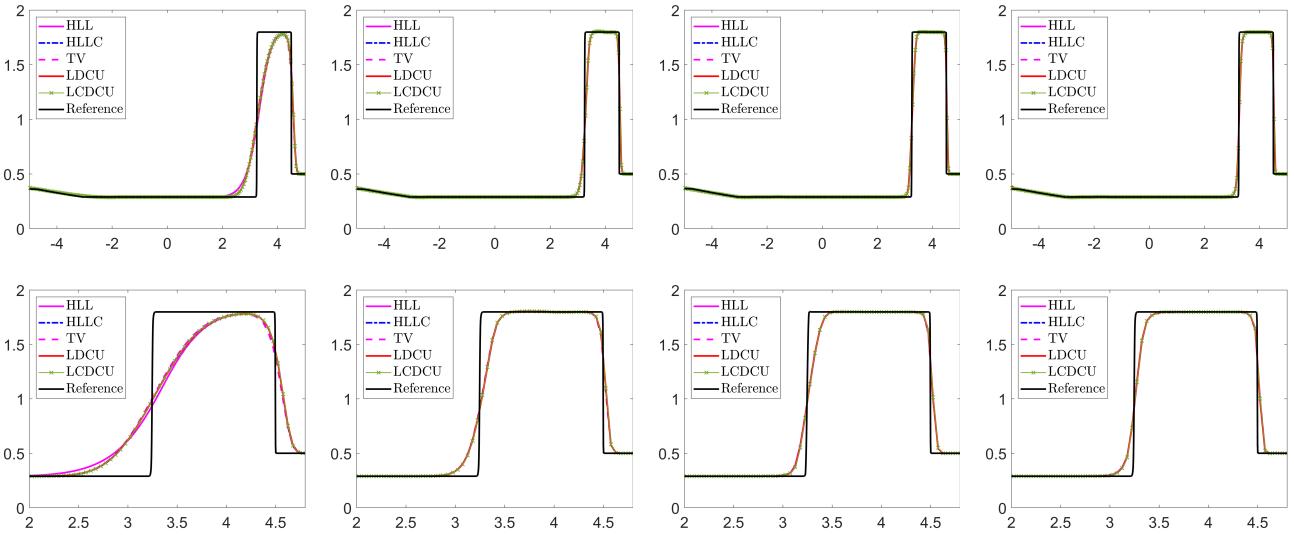


Figure 4.2: Example 3: Density  $\rho$  computed by the 1-Order, 2-Order, 3-Order, and 5-Order schemes (top row) and zoom at  $[2, 4.8]$  (bottom row).

#### Example 4—Shock Bubble Wave

In the fourth example, we consider the “shock-bubble” interaction problem taken from [43]. The initial data, given by

$$(\rho, u, p)(x, 0) = \begin{cases} (13.1538, 0, 1) & \text{if } |x| < 0.25, \\ (1.3333, -0.3535, 1.5) & \text{if } x > 0.75, \\ (1, 0, 1) & \text{otherwise,} \end{cases}$$

correspond to a left-moving shock, initially located at  $x = 0.75$ , and a bubble of radius 0.25, initially located at the origin. We implement solid wall boundary conditions on the left and free boundary conditions on the right of the computational domain  $[-1, 1]$ .

We compute the numerical solution until the final time  $t = 3$  using the studied 1-Order, 2-Order, 3-Order, and 5-Order schemes on the uniform mesh with  $\Delta x = 1/100$ . The obtained numerical results

are presented in Figure 4.3 along with the reference solution computed by the HLL schemes on a much finer mesh with  $\Delta x = 1/2000$ . One can notice that there are no clear differences in the numerical results computed by the four low-dissipation schemes, but the results computed by the low-dissipation schemes are better than the HLL scheme, especially in the 1-Order and 2-Order results.

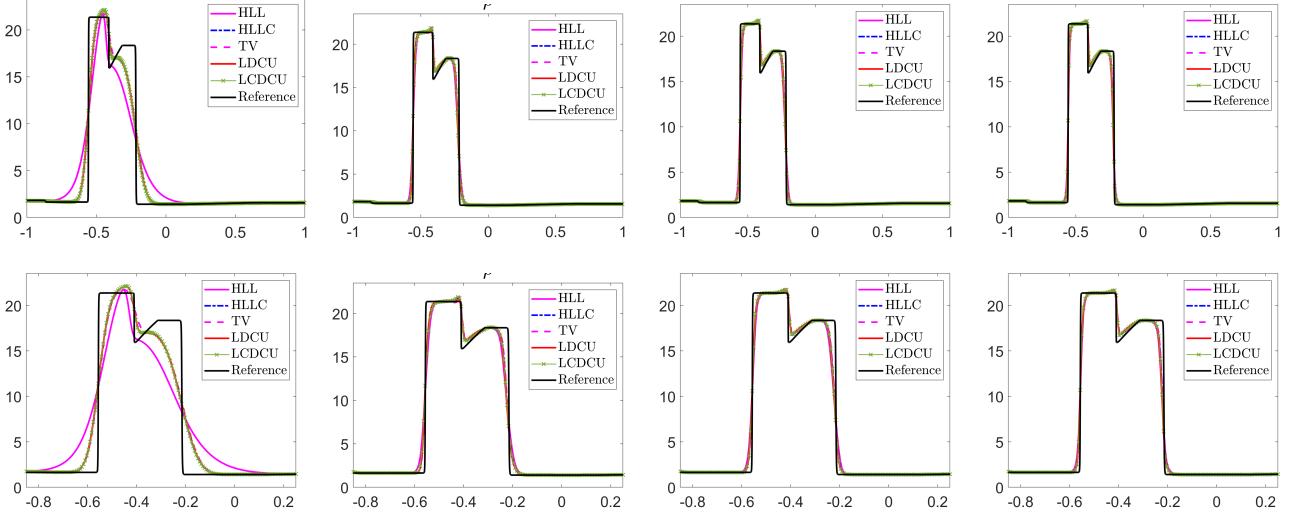


Figure 4.3: Example 4: Density  $\rho$  computed by the 1-Order, 2-Order, 3-Order, and 5-Order schemes (top row) and zoom at  $[-0.85, 0.25]$  (bottom row).

### Example 5—Shock-Density Wave Interaction Problem

In this example taken from [65], we consider the shock-density wave interaction problem with the following initial data,

$$(\rho, u, p)\Big|_{(x,0)} = \begin{cases} \left(\frac{27}{7}, \frac{4\sqrt{35}}{9}, \frac{31}{3}\right), & x < -4, \\ (1 + 0.2 \sin(5x), 0, 1), & x > -4, \end{cases}$$

prescribed in the computational domain  $[-5, 5]$  subject to the free boundary conditions.

We compute the numerical solutions until the final time  $t = 5$  by the 1-Order, 2-Order, 3-Order, and 5-Order schemes on a uniform mesh of 400 cells, and present the obtained numerical results in Figures 4.4–4.5 together with the reference solution computed by the HLL scheme on a much finer mesh of 8000 cells. It can be seen from this example that the TV schemes exhibit higher dissipation than the other schemes, including the HLL scheme, near the shock waves even for the high-order schemes. However, the TV schemes achieve better resolution than HLL schemes in the smooth parts of the results.

### Example 6—Shock-Entropy Wave Interaction Problem

In the last 1-D example, we consider the shock-entropy problem taken from [64]. The initial conditions,

$$(\rho, u, p)(x, 0) = \begin{cases} (1.51695, 0.523346, 1.805), & x < -4.5, \\ (1 + 0.1 \sin(20x), 0, 1), & x > -4.5, \end{cases}$$

correspond to a forward-facing shock wave of Mach 1.1 interacting with high-frequency density perturbations, that is, as the shock wave moves, the perturbations spread ahead. In this example, the free boundary conditions are imposed at both ends of the computational domain  $[-10, 5]$ .

We compute the solutions until the final time  $t = 5$  by the 1-Order, 2-Order, 3-Order, and 5-Order schemes on a uniform mesh of 1200 cells. The numerical results are shown in Figures 4.6–4.7 along with the reference solution computed by the HLL scheme on a much finer mesh of 12000 cells. The

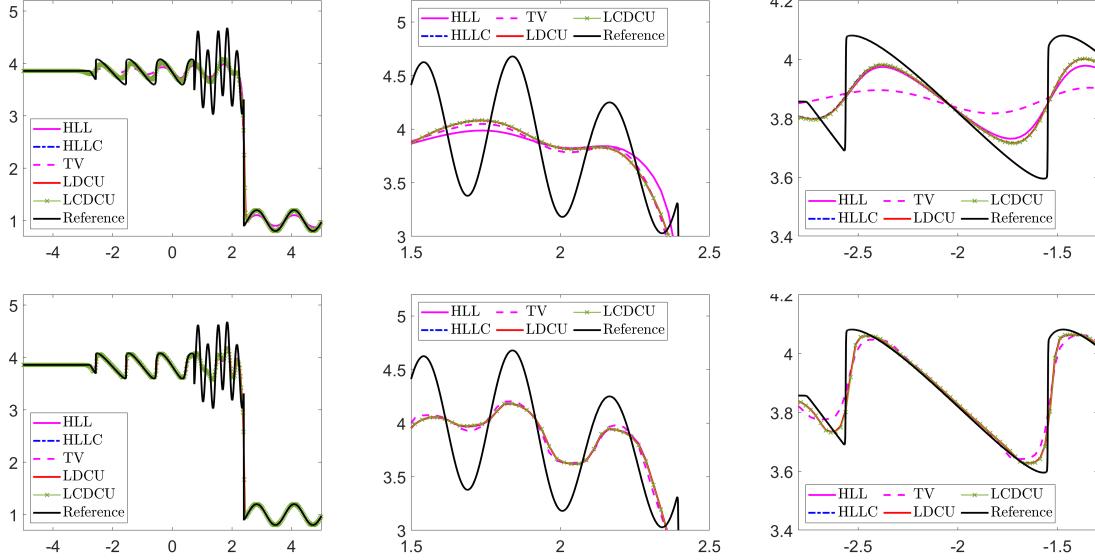


Figure 4.4: Example 5: Density  $\rho$  computed by the 1-Order and 2-Order schemes (left column) and zoom at  $[1.5, 2.5]$  (middle column), and  $[-2.8, -1.3]$  (right column).

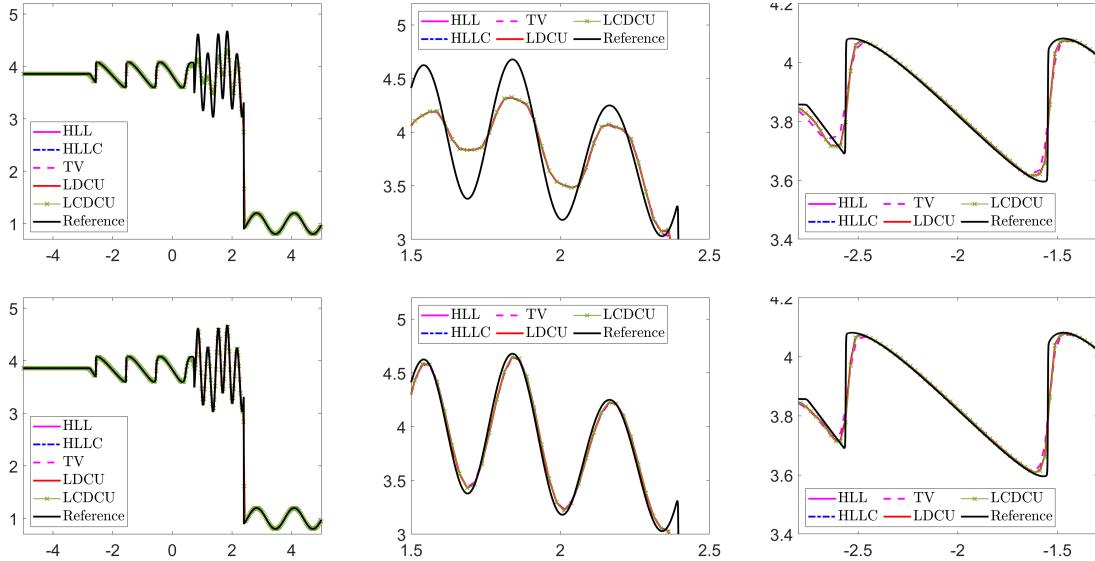


Figure 4.5: Example 5: Density  $\rho$  computed by the 3- and 5-Order schemes (left column) and zoom at  $[1.5, 2.5]$  (middle column), and  $[-2.8, -1.3]$  (right column).

obtained results clearly demonstrate a substantial difference in the resolution computed by HLL and the four low-dissipation schemes. One can also see that in the 1-Order results, the LDCU scheme has slightly more dissipation than the TV, HLLC, and LCDCU schemes, but still significantly better than the HLL scheme. At the same time, the four low-dissipation schemes coincide when extended to higher orders; see Figures 4.6 (bottom) and 4.7.

## 4.2 Two-Dimensional Examples

In this section, we consider the 2-D Euler equations of gas dynamics (1.2), (3.1)–(3.2). In Examples 7–14, we take the specific heat ratio  $\gamma = 1.4$ , while in Example 15, we take  $\gamma = 5/3$ .

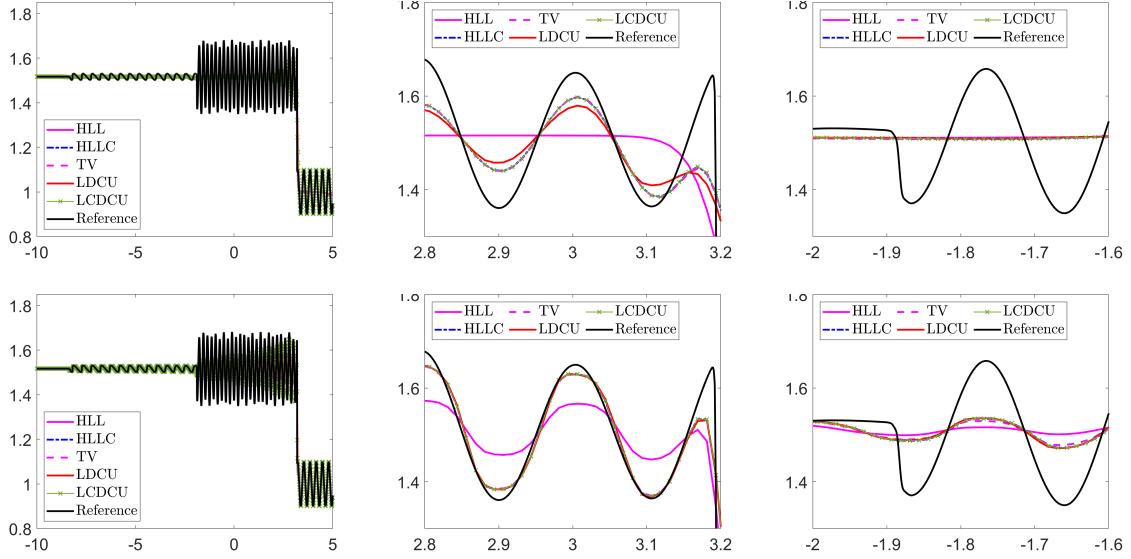


Figure 4.6: Example 6: Density  $\rho$  computed by the 1-Order and 2-Order schemes (left) and zoom at  $[2.8, 3.2]$  (middle) and  $[-2, -1.6]$  (right).

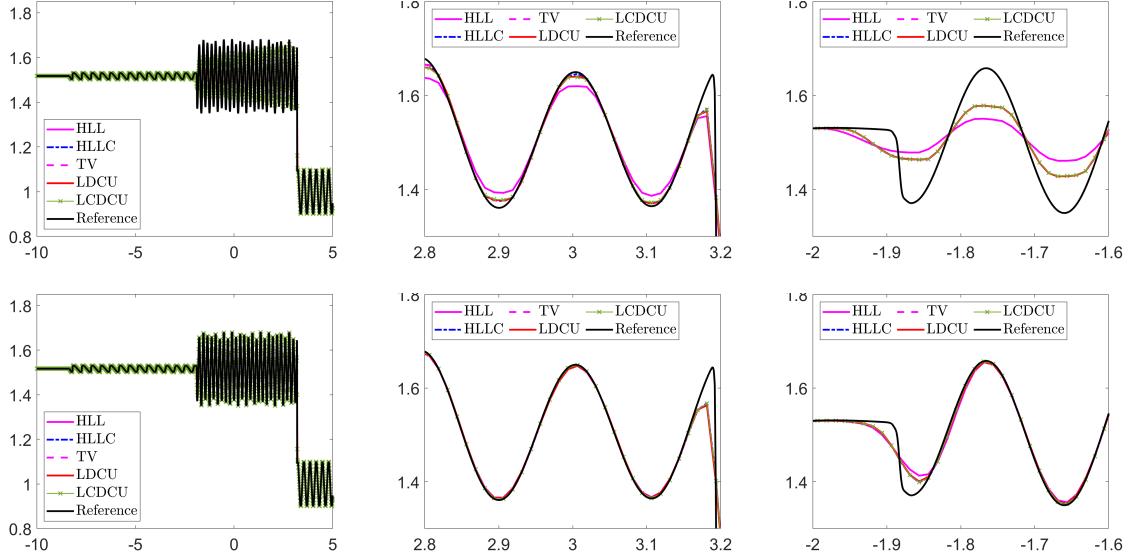


Figure 4.7: Example 6: Density  $\rho$  computed by the 3-Order and 5-Order schemes (left) and zoom at  $[2.8, 3.2]$  (middle) and  $[-2, -1.6]$  (right).

### Example 7—2-D Accuracy Test

In the first 2-D example taken from [6, 40], we consider the 2-D Euler equations of gas dynamics subject to the periodic initial conditions,

$$\rho(x, y, 0) = 1 + \frac{1}{5} \sin(\pi(x + y)), \quad u(x, y, 0) \equiv 1, \quad v(x, y, 0) \equiv -0.7, \quad p(x, y, 0) \equiv 1,$$

prescribed on  $[-1, 1] \times [-1, 1]$ . The exact solution of this initial value problem can be easily obtained and is given by

$$\rho(x, y, t) = 1 + \frac{1}{5} \sin [\pi(x + y - 0.3t)], \quad u(x, y, t) \equiv 1, \quad v(x, y, t) \equiv -0.7, \quad p(x, y, t) \equiv 1.$$

We first compute the numerical solution until the final time  $t = 0.1$  using the 1-Order, 2-Order, 3-Order, and 5-Order schemes on a sequence of uniform meshes:  $100 \times 100$ ,  $200 \times 200$ , and  $400 \times 400$ ,

and then measure the  $L^1$ -errors and the corresponding experimental convergence rates for the density. The obtained results are presented in Table 4.2, where one can see that the studied 1-Order, 2-Order, 3-Order, and 5-Order schemes achieve the expected order of accuracy. At the same time, the four low-dissipation schemes are slightly more accurate than the HLL schemes, while the four low-dissipation schemes achieve exactly the same numerical results. As in Example 1, we had to use smaller time steps with  $\Delta t \sim \min\{(\Delta x)^{\frac{5}{3}}, (\Delta y)^{\frac{5}{3}}\}$  to achieve the fifth order of accuracy.

Method	Mesh	1-Order		2-Order		3-Order		5-Order	
		Error	Rate	Error	Rate	Error	Rate	Error	Rate
HLL	$100 \times 100$	1.18e-02	—	3.59e-04	—	6.02e-06	—	4.36e-09	—
	$200 \times 200$	5.91e-03	0.994	8.38e-05	2.10	7.37e-07	3.03	1.36e-10	5.00
	$400 \times 400$	2.96e-03	0.997	1.91e-05	2.13	9.22e-08	3.00	4.42e-12	4.95
HLLC	$100 \times 100$	8.39e-03	—	2.64e-04	—	4.32e-06	—	3.12e-09	—
	$200 \times 200$	4.21e-03	0.994	6.16e-05	2.10	5.27e-07	3.03	9.76e-11	5.00
	$400 \times 400$	2.11e-03	0.997	1.47e-05	2.06	6.59e-08	3.00	3.19e-12	4.93
TV	$100 \times 100$	8.39e-03	—	2.64e-04	—	4.32e-06	—	3.12e-09	—
	$200 \times 200$	4.21e-03	0.994	6.16e-05	2.10	5.27e-07	3.03	9.76e-11	5.00
	$400 \times 400$	2.11e-03	0.997	1.47e-05	2.06	6.59e-08	3.00	3.19e-12	4.93
LDCU	$100 \times 100$	8.39e-03	—	2.64e-04	—	4.32e-06	—	3.12e-09	—
	$200 \times 200$	4.21e-03	0.994	6.16e-05	2.10	5.27e-07	3.03	9.76e-11	5.00
	$400 \times 400$	2.11e-03	0.997	1.47e-05	2.06	6.59e-08	3.00	3.19e-12	4.93
LCDCU	$100 \times 100$	8.39e-03	—	2.64e-04	—	4.32e-06	—	3.12e-09	—
	$200 \times 200$	4.21e-03	0.994	6.16e-05	2.10	5.27e-07	3.03	9.76e-11	5.00
	$400 \times 400$	2.11e-03	0.997	1.47e-05	2.06	6.59e-08	3.00	3.19e-12	4.93

Table 4.2: Example 7: The  $L^1$ -errors and experimental convergence rates for the density  $\rho$  computed by the 1-Order, 2-Order, 3-Order, and 5-Order schemes.

### Example 8—2-D Vortex Evolution Problem

In this example taken from [68]; see also [10, 30], we consider the 2-D vortex evolution problem with the following initial conditions

$$(\rho(x, y, 0), u(x, y, 0), v(x, y, 0), p(x, y, 0)) = \left( T^{\frac{1}{\gamma-1}}, 1 - \frac{\varepsilon}{2\pi} e^{\frac{1}{2}(1-r^2)} y, 1 + \frac{\varepsilon}{2\pi} e^{\frac{1}{2}(1-r^2)} x, \rho^\gamma \right),$$

where  $T = 1 - \frac{(\gamma-1)\varepsilon^2}{8\gamma\pi^2} e^{(1-r^2)}$ ,  $r^2 = x^2 + y^2$ , and  $\varepsilon = 5$  is the vortex strength. The initial data, prescribed in the computational domain  $[-5, 5] \times [-5, 5]$  subject to the periodic boundary conditions, corresponds to a smooth vortex placed at the origin and is defined as the isentropic perturbation to the uniform flow of unit values of primitive variables and the exact solution is a vortex moving with a constant velocity at  $45^\circ$  to the Cartesian mesh lines.

We compute the numerical solution until the final time  $t = 10$  using the 1-Order, 2-Order, 3-Order, and 5-Order schemes on a sequence of uniform meshes:  $100 \times 100$ ,  $200 \times 200$ , and  $400 \times 400$ , and then measure the  $L^1$ -errors between the computed solutions and the exact solutions and the corresponding experimental convergence rates for the density. The obtained results are presented in Table 4.3, where one can see that both 1-Order and 2-Order convergence rates are observed only after significant mesh refinement, while the 3-Order and 5-Order schemes achieve the expected order of accuracy. In order to have a better view, we also show the  $L^1$ -errors in Figure 4.8, where we also show the results computed

by the 1-Order and 2-Order schemes on finer meshes  $800 \times 800$  and  $1600 \times 1600$  to show that the 1-Order and 2-Order schemes achieve expected convergence rates after mesh refinement. It is noticed that, in this example, the TV schemes are slightly more dissipative than the HLL schemes, but HLLC, LDCU, and LCDCU schemes are slightly more accurate than the HLL schemes.

Method	Mesh	1-Order		2-Order		3-Order		5-Order	
		Error	Rate	Error	Rate	Error	Rate	Error	Rate
HLL	$100 \times 100$	1.86	—	1.48e-01	—	2.45e-02	—	7.88e-04	—
	$200 \times 200$	1.33	4.84e-01	4.54e-02	1.71	2.94e-03	3.06	2.42e-05	5.02
	$400 \times 400$	0.84	6.71e-01	1.00e-02	2.18	3.08e-04	3.25	6.16e-07	5.30
HLLC	$100 \times 100$	1.74	—	1.44e-01	—	2.26e-02	—	7.03e-04	—
	$200 \times 200$	1.21	5.26e-01	4.67e-02	1.62	2.68e-03	3.08	2.27e-05	4.95
	$400 \times 400$	0.74	7.04e-01	9.88e-03	2.24	2.70e-04	3.31	5.60e-07	5.34
LDCU	$100 \times 100$	1.76	—	1.54e-01	—	2.23e-02	—	7.07e-04	—
	$200 \times 200$	1.23	5.21e-01	5.07e-02	1.60	2.71e-03	3.04	2.32e-05	4.93
	$400 \times 400$	0.76	6.97e-01	1.05e-02	2.28	2.85e-04	3.25	5.94e-07	5.29
LCDCU	$100 \times 100$	1.74	—	1.44e-01	—	2.28e-02	—	7.03e-04	—
	$200 \times 200$	1.21	5.26e-01	4.69e-02	1.62	2.70e-03	3.07	2.27e-05	4.95
	$400 \times 400$	0.74	7.04e-01	9.88e-03	2.25	2.70e-04	3.32	5.60e-07	5.34
TV	$100 \times 100$	2.49	—	1.24e-01	—	2.98e-02	—	9.23e-04	—
	$200 \times 200$	1.91	3.84e-01	3.00e-02	2.05	3.58e-03	3.06	2.49e-05	5.21
	$400 \times 400$	1.26	5.97e-01	6.75e-03	2.15	3.99e-04	3.16	6.62e-07	5.23

Table 4.3: Example 8:  $L^1$ -errors and experimental convergence rates for the density  $\rho$  computed by the 1-Order, 2-Order, 3-Order, and 5-Order HLL, HLLC, TV, LDCU, and LCDCU schemes.

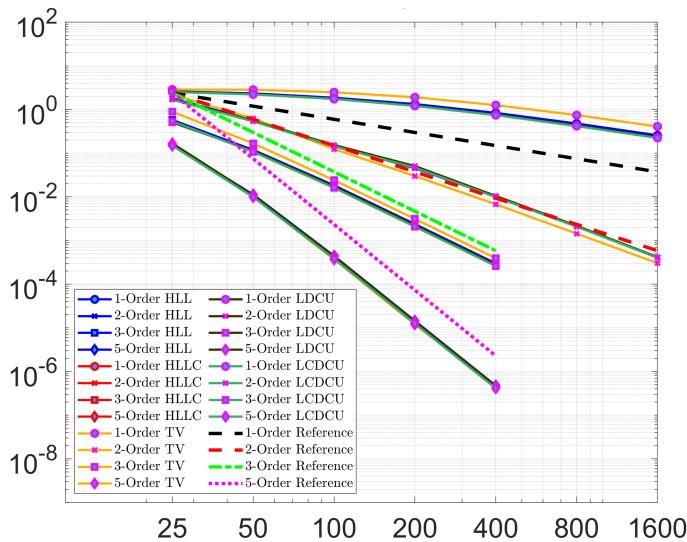


Figure 4.8: Example 8:  $L^1$ -errors for the density  $\rho$  computed by the 1-Order, 2-Order, 3-Order, and 5-Orders HLL, HLLC, TV, LDCU, and LCDCU schemes.

### Example 9—2-D Moving Contact Waves

In this example taken from [37] (see also [12, 43]), we consider an isolated moving contact wave with the following initial data:

$$(\rho, u, v, p)(x, y, 0) = \begin{cases} (1.4, 0, 0.2, 1), & (x, y) \in D \\ (1, 0, 0.2, 1), & \text{otherwise,} \end{cases}$$

where the domain  $D$  consists of the points  $(x, y)$  satisfying the following conditions:

$$\begin{aligned} & \{-0.1 < x < 0.1, 0 < y < 0.02\} \cup \{-0.02 < x < 0.02, 0.02 < y < 0.1\} \cup \\ & \{(x + 0.02)^2 + (y - 0.02)^2 < 0.08^2\} \cup \{(x - 0.02)^2 + (y - 0.02)^2 < 0.08^2\}. \end{aligned}$$

The initial data are prescribed in the computational domain  $[-0.2, 0.2] \times [0, 0.8]$  subject to the free boundary conditions.

We compute the numerical solutions until the final time  $t = 2$  by the studied 1-Order, 2-Order, 3-Order, and 5-Order schemes on a uniform mesh with  $\Delta x = \Delta y = 1/400$  and plot the obtained results in Figure 4.9. As one can see, the four low-dissipation schemes produce nearly identical numerical results, which are significantly sharper than those computed by the HLL schemes, especially for the non-moving jumps across the lines  $x = \pm 0.1$ .

### Example 10—Explosion Problem

In this example, we consider the explosion problem studied in [54, 70] (see also [7, 43]). We take the following initial conditions,

$$(\rho(x, y, 0), u(x, y, 0), v(x, y, 0), p(x, y, 0)) = \begin{cases} (1, 0, 0, 1), & x^2 + y^2 < 0.16, \\ (0.125, 0, 0, 0.1), & \text{otherwise,} \end{cases}$$

which are prescribed in the computational domain  $[-1, 1] \times [-1, 1]$ , subject to free boundary conditions at all the four sides. The solution of this initial-boundary value problem develops circular shock and contact waves. While the shock wave is stable and requires sufficient dissipation for stable capturing, the contact wave is unstable and can only be stabilized by numerical diffusion. This makes the problem a useful benchmark for evaluating the dissipation of numerical schemes, where the goal is to minimize dissipation while retaining shock stability.

We apply the studied 1-Order, 2-Order, 3-Order, and 5-Order schemes and compute the numerical solutions until the final time  $t = 3.2$  on a uniform mesh with  $\Delta x = \Delta y = 3/800$ . The obtained results are presented in Figure 4.10, where one can see that the differences between the numerical results computed by the four low-dissipation schemes are limited, but much more substantially “curlier” and the mixing layer is slightly wider (indicating a more severe instability) than those computed by the HLL schemes, while the shock is still stable.

### Example 11—Implosion Problem

In this example, we consider the implosion problem taken from [54] (see also [6, 36]). The initial conditions,

$$(\rho(x, y, 0), u(x, y, 0), v(x, y, 0), p(x, y, 0)) = \begin{cases} (0.125, 0, 0, 0.14), & |x| + |y| < 0.15, \\ (1, 0, 0, 1), & \text{otherwise,} \end{cases}$$

are prescribed in the computational domain  $[0, 0.3] \times [0, 0.3]$  with solid boundary conditions imposed at all four sides. This example is designed to assess the numerical diffusion of different schemes: a jet forms near the origin and propagates along the diagonal  $y = x$ , and excessive diffusion may either smear the jet entirely or alter its propagation velocity.

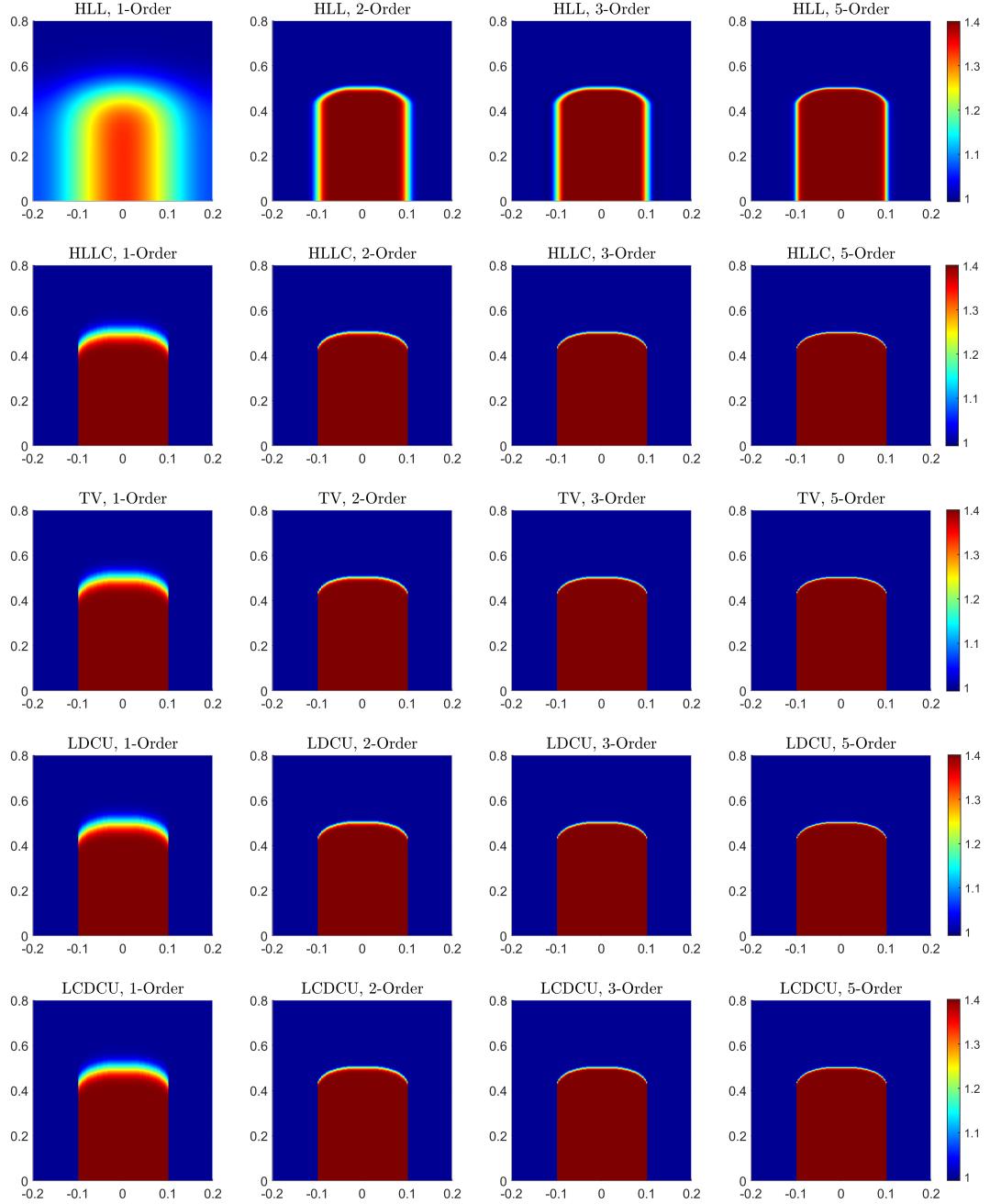


Figure 4.9: Example 9: Density  $\rho$  computed by the 1-Order, 2-Order, 3-Order, and 5-Order HLL (top row), HLLC (second row), TV (third row), LDCU (fourth row), and LCDCU (bottom row) schemes.

We compute the numerical solutions until the final time  $t = 2.5$  by the 1-Order, 2-Order, 3-Order, and 5-Order schemes on a uniform mesh with  $\Delta x = \Delta y = 3/4000$  and plot the obtained results in Figure 4.11, where one can clearly observe that the jet propagates much further in the diagonal direction when using the four low-dissipation schemes. At the same time, the LDCU scheme is slightly less dissipative than the other three low-dissipation counterparts.

It is instructive to check the efficiency of the studied schemes. To this end, we measure the CPU time consumed by the 1-Order, 2-Order, 3-Order and 5-Order LCDCU schemes and refine the mesh used by the other four schemes to the level that exactly the same CPU time is consumed to compute all three numerical solutions. The corresponding meshes are  $400 \times 400$  for the 1-Order, 2-Order, 3-Order, and 5-Order LCDCU schemes,  $570 \times 570$ ,  $568 \times 568$ ,  $482 \times 482$ , and  $462 \times 462$  for the HLL schemes,  $568 \times 568$ ,  $565 \times 565$ ,  $479 \times 479$ , and  $458 \times 458$  for the HLLC schemes,  $591 \times 591$ ,  $590 \times 590$ ,  $487 \times 487$ , and  $466 \times 466$  for the TV schemes, and  $565 \times 565$ ,  $563 \times 563$ ,  $475 \times 475$ , and  $455 \times 455$

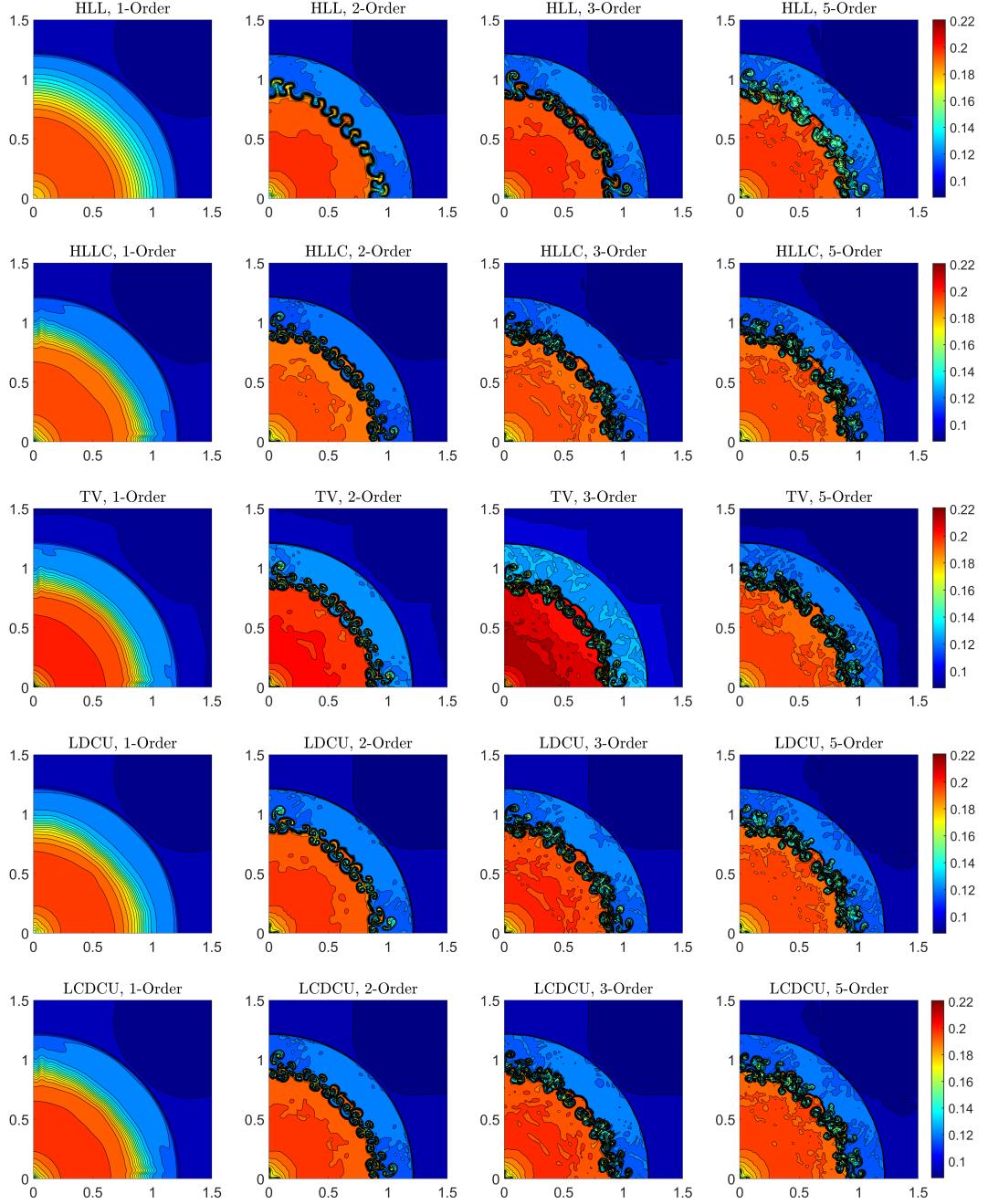


Figure 4.10: Example 10: Density  $\rho$  computed by the 1-Order, 2-Order, 3-Order, and 5-Order HLL (top row), HLLC (second row), TV (third row), LDCU (fourth row), and LCDCU (bottom row) schemes.

for the LDCU schemes. The obtained numerical results, presented in Figure 4.12, indicate that the four low-dissipation schemes are more efficient than the HLL counterparts. At the same time, it is noticed that the positions of the jets produced by the HLLC and TV schemes are consistent, which are slightly further than the ones produced by the LDCU schemes. While the LCDCU schemes are more computationally expensive than the other three low-dissipation schemes, and the reason is that the LCDCU fluxes defined in §3.5 are more complicated than the others.

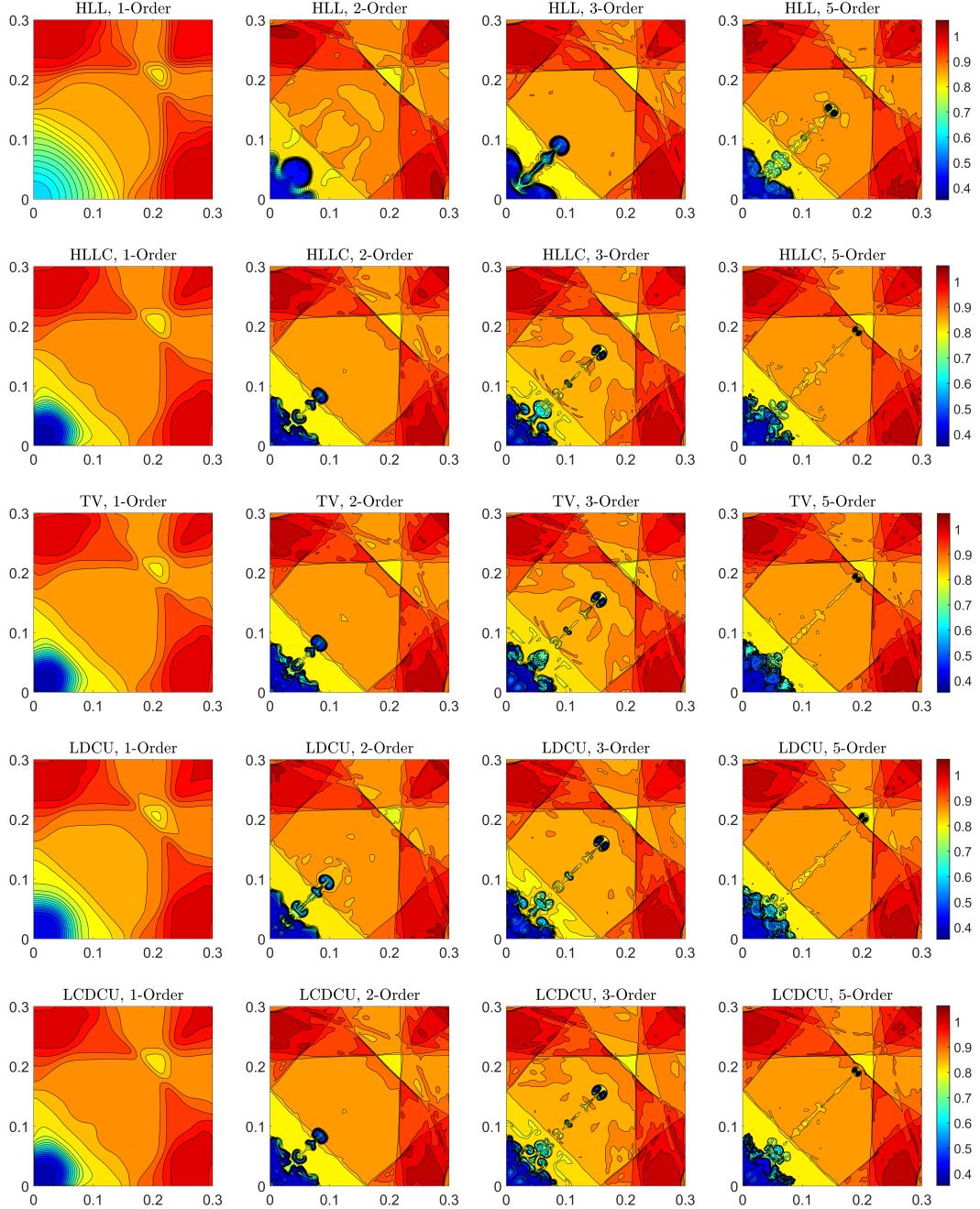


Figure 4.11: Example 11: Density  $\rho$  computed by the 1-Order, 2-Order, 3-Order, and 5-Order HLL (top row), HLLC (second row), TV (third row), LDCU (fourth row), and LCDCU (bottom row) schemes.

### Example 12—2-D Riemann Problem (Configuration 3)

In this example, we consider Configuration 3 of the 2-D Riemann problems from [42] (see also [60, 61, 80]) with the following initial conditions:

$$(\rho, u, v, p)(x, y, 0) = \begin{cases} (1.5, 0, 0, 1.5), & x > 1, y > 1, \\ (0.5323, 1.206, 0, 0.3), & x < 1, y > 1, \\ (0.138, 1.206, 1.206, 0.029), & x < 1, y < 1, \\ (0.5323, 0, 1.206, 0.3), & x > 1, y < 1. \end{cases}$$

which are prescribed in the computational domain  $[0, 1.2] \times [0, 1.2]$  subject to the free boundary conditions.

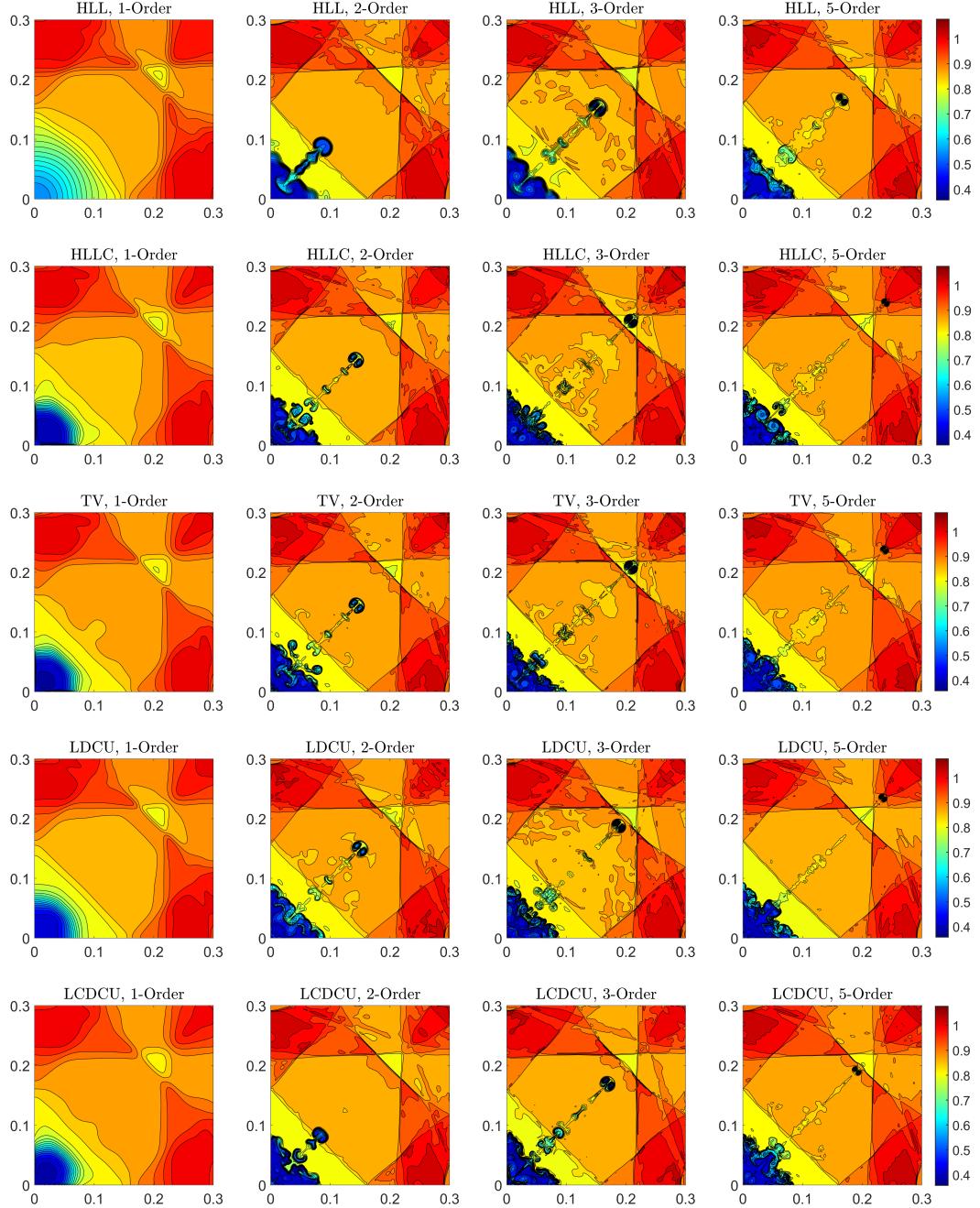


Figure 4.12: Example 11: Density  $\rho$  computed by the 1-Order, 2-Order, 3-Order, and 5-Order HLL (top row), HLLC (second row), TV (third row), LDCU (fourth row), and LCDCU (bottom row) schemes.

We compute the numerical solution until the final time  $t = 1$  by the 1-Order, 2-Order, 3-Order, and 5-Order schemes on a uniform mesh with  $\Delta x = \Delta y = 6/5000$  and plot the obtained results in Figure 4.13, where one can see that the HLLC, LDCU, and LCDCU schemes outperform the HLL scheme in capturing a sideband instability of the jet in the zones of strong along-jet velocity shear and the instability along the jet's neck. However, one can see that the TV schemes can capture more details of the instability along the jet's neck, but there are some oscillations in the numerical results. At the same time, the higher-order (3- and 5-Order) schemes fail in the simulation because of the oscillation, which leads to negative pressure in the computed numerical results.

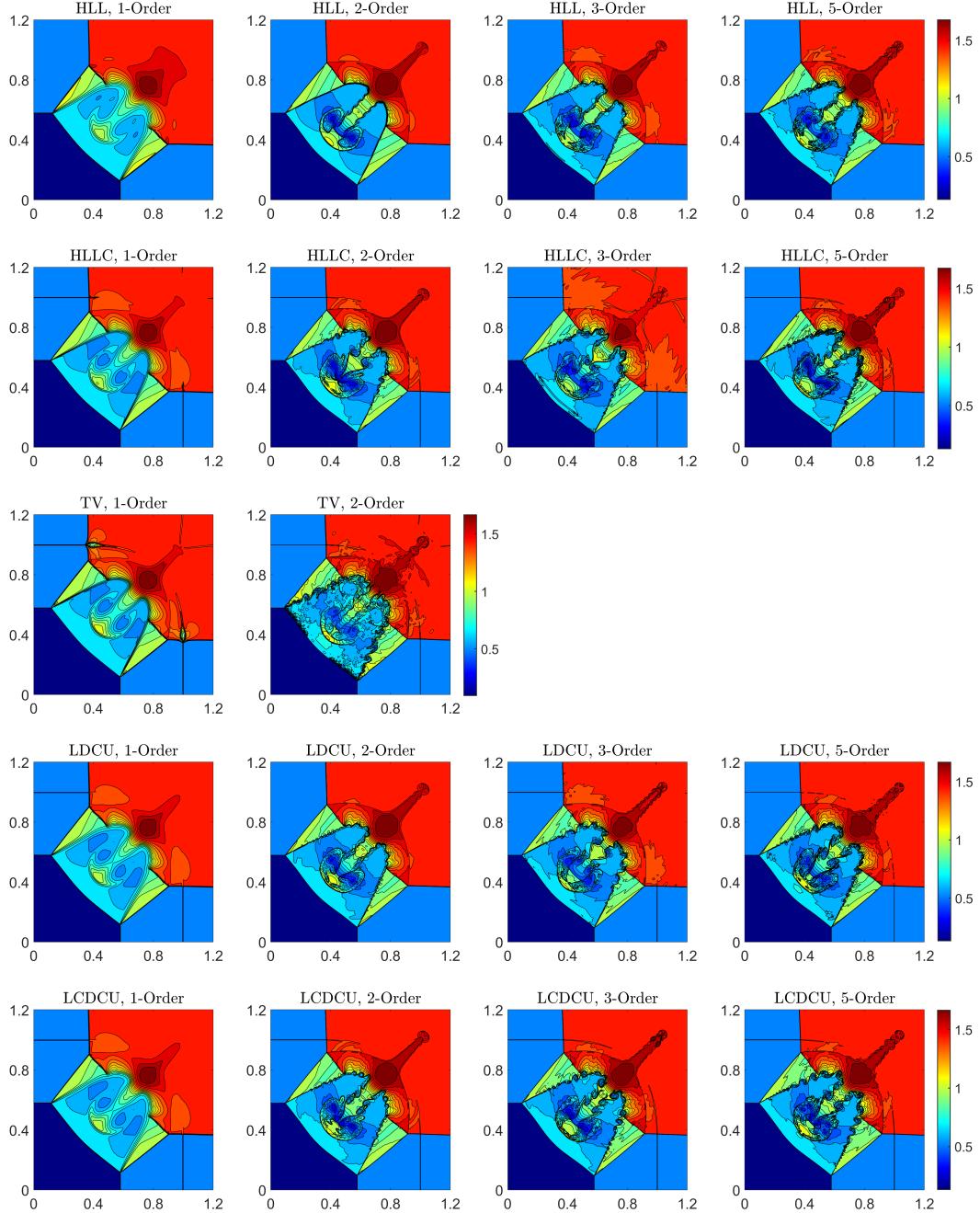


Figure 4.13: Example 12: Density  $\rho$  computed by the 1-Order, 2-Order, 3-Order, and 5-Order HLL (top row), HLLC (second row), TV (third row), LDCU (fourth row), and LCDCU (bottom row) schemes.

### Example 13—2-D Riemann Problem (Configuration 6)

In this example, we consider Configuration 6 of the 2-D Riemann problems from [42] (see also [60, 61, 80]) with the following initial conditions:

$$(\rho, u, v, p)|_{(x,y,0)} = \begin{cases} (1, 0.75, -0.5, 1), & x > 0.5, y > 0.5, \\ (2, 0.75, 0.5, 1), & x < 0.5, y > 0.5, \\ (1, -0.75, 0.5, 1), & x < 0.5, y < 0.5, \\ (3, -0.75, -0.5, 1), & x > 0.5, y < 0.5, \end{cases}$$

which are prescribed in the computational domain  $[0, 1] \times [0, 1]$  subject to the free boundary conditions.

We compute the numerical solution until the final time  $t = 1$  by the 1-Order, 2-Order, 3-Order,

and 5-Order schemes on a uniform mesh with  $\Delta x = \Delta y = 1/600$  and plot the obtained results in Figure 4.14, where one can see that the four low-dissipation schemes clearly outperform the HLL ones. At the same time, the low-dissipation schemes are capable of capturing more complicated vortex structures compared with the HLL scheme, which demonstrates higher resolution and lower numerical dissipation of the low-dissipation schemes.

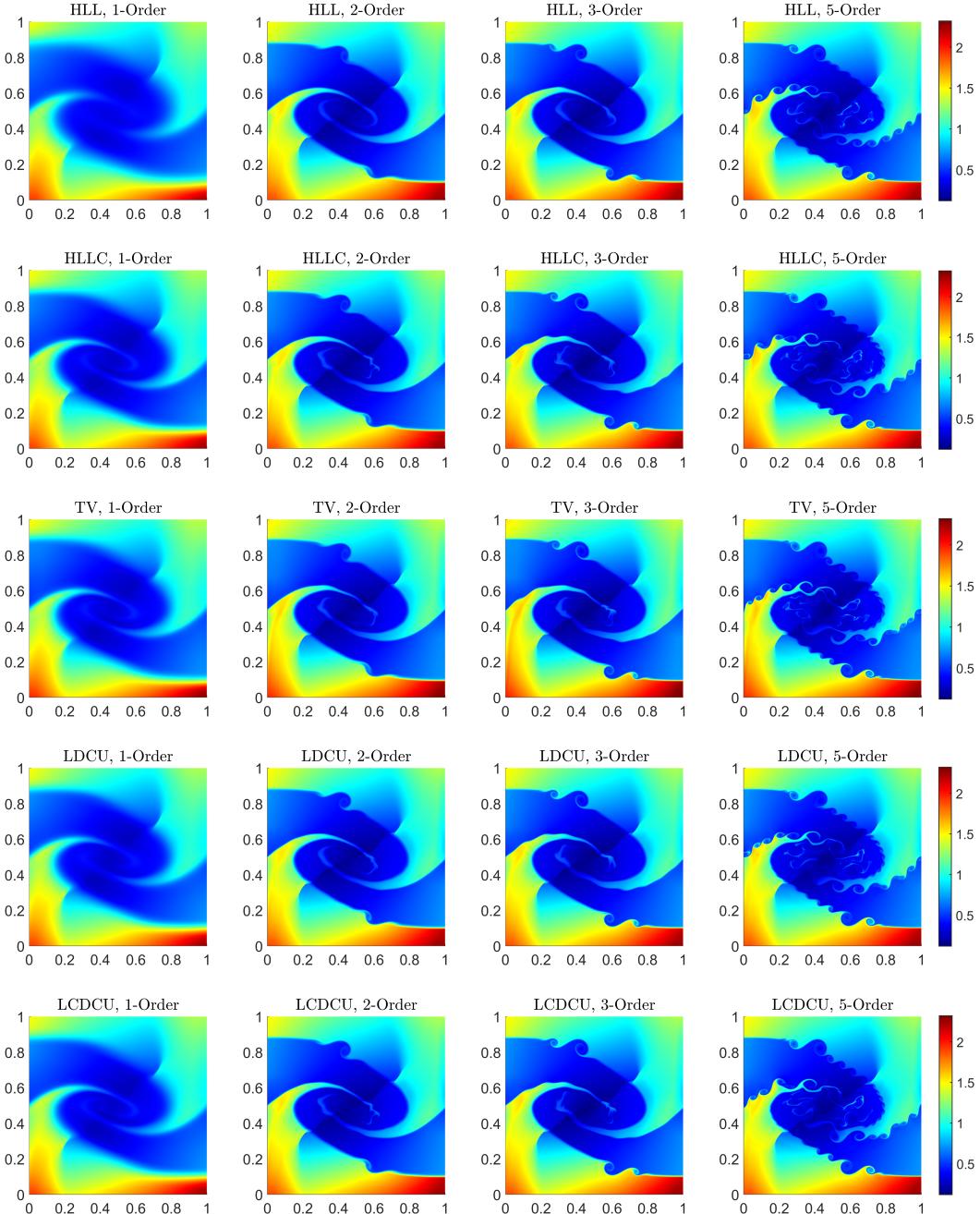


Figure 4.14: Example 13: Density  $\rho$  computed by the 1-Order, 2-Order, 3-Order, and 5-Order HLL (top row), HLLC (second row), TV (third row), LDCDU (fourth row), and LCDCU (bottom row) schemes.

### Example 14—Kelvin-Helmholtz (KH) Instability

In this example, we study the KH instability taken from [19, 59] (see also [6, 18]). We take the following initial data:

$$(\rho(x, y, 0), u(x, y, 0)) = \begin{cases} (1, -0.5 + 0.5e^{(y+0.25)/L}), & y < -0.25, \\ (2, 0.5 - 0.5e^{(-y-0.25)/L}), & -0.25 < y < 0, \\ (2, 0.5 - 0.5e^{(y-0.25)/L}), & 0 < y < 0.25, \\ (1, -0.5 + 0.5e^{(0.25-y)/L}), & y > 0.25, \end{cases}$$

$$v(x, y, 0) = 0.01 \sin(4\pi x), \quad p(x, y, 0) \equiv 1.5,$$

where  $L$  is a smoothing parameter (we take  $L = 0.00625$ ), which corresponds to a thin shear interface with a perturbed vertical velocity field  $v$  in the conducted simulations. The periodic boundary conditions are imposed on all four sides of the computational domain  $[-0.5, 0.5] \times [-0.5, 0.5]$ .

We compute the numerical solutions until the final time  $t = 4$  by the 1-Order, 2-Order, 3-Order, and 5-Order schemes on a uniform mesh of  $1024 \times 1024$  cells, and plot the numerical results at times  $t = 1, 2.5$ , and  $4$  in Figures 4.15–4.17. One can observe that at the early time  $t = 1$ , the vortex streets generated by the high-order schemes are more pronounced; see Figure 4.15. These structures grow exponentially over time, leading to increasingly complex turbulent mixing, particularly evident at later times  $t = 2.5$  and  $4$ ; see Figures 4.16–4.17. At the same time, it is clear that the four low-dissipation schemes outperform the HLL schemes in achieving more complex structures of the KH instabilities.

### Example 15—Rayleigh-Taylor (RT) Instability

In the last example taken from [62], we investigate the RT instability, which is a physical phenomenon occurring when a layer of heavier fluid is placed on top of a layer of lighter fluid. The model is governed by the 2-D Euler equations (3.1)–(3.2) with added gravitational source terms and the modified system reads as

$$\begin{aligned} \rho_t + (\rho u)_x + (\rho v)_y &= 0, \\ (\rho u)_t + (\rho u^2 + p)_x + (\rho u v)_y &= 0, \\ (\rho v)_t + (\rho u v)_x + (\rho v^2 + p)_y &= \rho, \\ E_t + [u(E + p)]_x + [v(E + p)]_y &= \rho v. \end{aligned}$$

We consider the following initial conditions:

$$(\rho(x, y, 0), u(x, y, 0), v(x, y, 0), p(x, y, 0)) = \begin{cases} (2, 0, -0.025 c \cos(8\pi x), 2y + 1), & y < 0.5, \\ (1, 0, -0.025 c \cos(8\pi x), y + 1.5), & \text{otherwise}, \end{cases}$$

where  $c := \sqrt{\gamma p / \rho}$  is the speed of sound, prescribed in the computational domain  $[0, 0.25] \times [0, 1]$  with the solid wall boundary conditions imposed at  $x = 0$  and  $x = 0.25$ , and the following Dirichlet boundary conditions imposed at the top and bottom boundaries:

$$(\rho, u, v, p)|_{y=1} = (1, 0, 0, 2.5), \quad (\rho, u, v, p)|_{y=0} = (2, 0, 0, 1).$$

We compute the numerical solutions until the final time  $t = 2.95$  by 1-Order, 2-Order, 3-Order, and 5-Order schemes on the uniform mesh of  $256 \times 1024$  cells and present the numerical results at times  $t = 1.95$  and  $2.95$  in Figures 4.18–4.21. One can see that there are pronounced differences between the solutions computed by the HLL and four low-dissipation schemes since the structures captured by the low-dissipation schemes are much more complicated, which again demonstrates that the four schemes contain less dissipation than the corresponding HLL counterparts. At the same time, the differences between the studied four low-dissipation schemes are limited, especially in a shorter time; see Figures 4.18–4.19. In the later times, they produce different complex structures because of the unstable nature of the Rayleigh-Taylor instability problem.

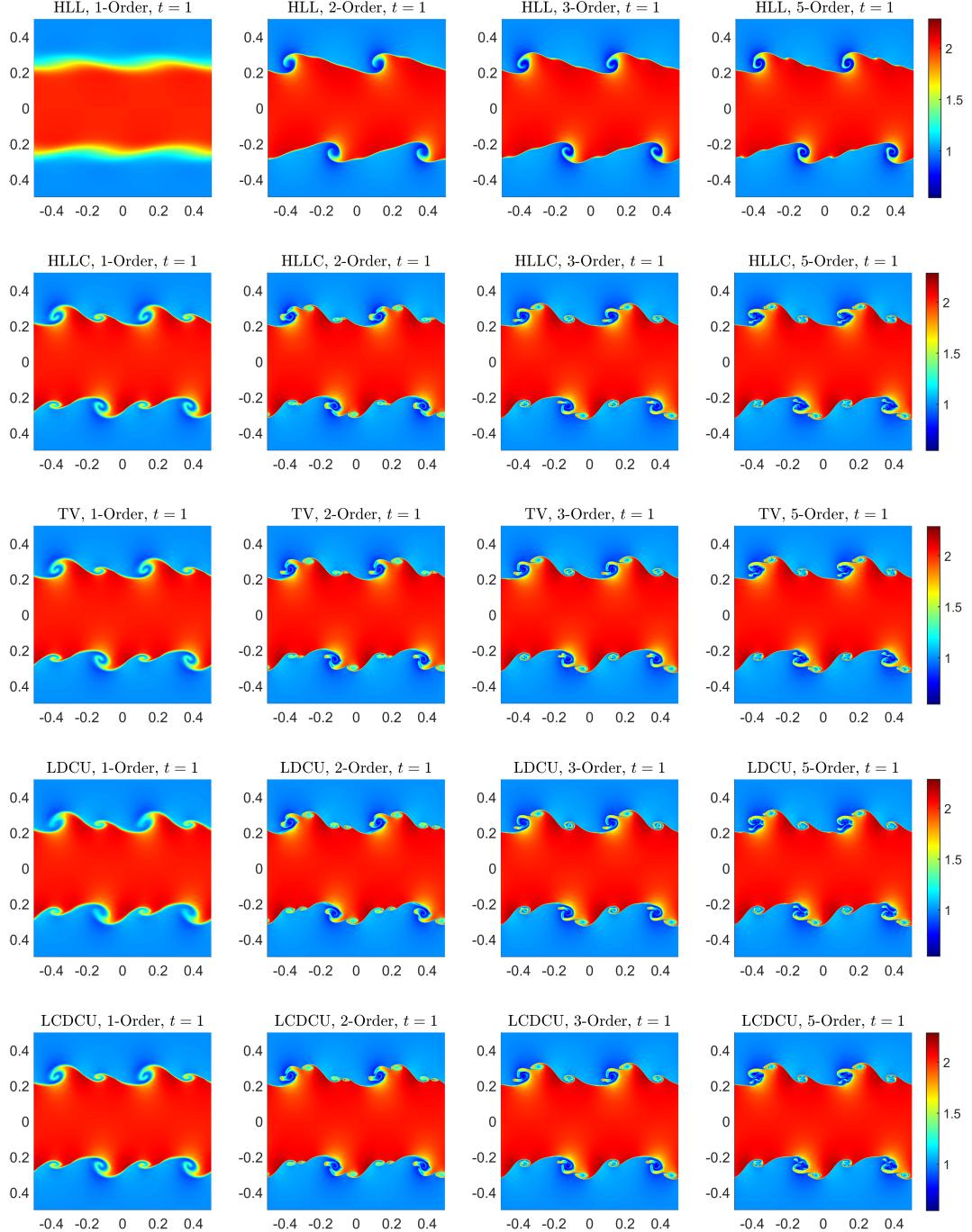


Figure 4.15: Example 14: Time snapshots of density  $\rho$  computed by the 1-Order, 2-Order, 3-Order, and 5-Order HLL (top row), HLLC (second row), TV (third row), LDCU (fourth row), and LCDCU (bottom row) schemes at  $t = 1$ .

## 5 Conclusions

In this paper, we have carried out a systematic comparative study of several low-dissipation numerical schemes for hyperbolic conservation laws, including the HLLC and three recently proposed low-dissipation schemes — TV flux splitting, LDCU, and LCDCU schemes. All of these schemes were extended to higher orders of accuracy, up to the fifth order, within both finite-volume and finite-difference frameworks. Through a series of one- and two-dimensional numerical experiments for the Euler equations of gas dynamics, we have examined their accuracy, robustness, and computational efficiency. Our results indicate that all of the studied low-dissipation schemes exhibit a comparable level

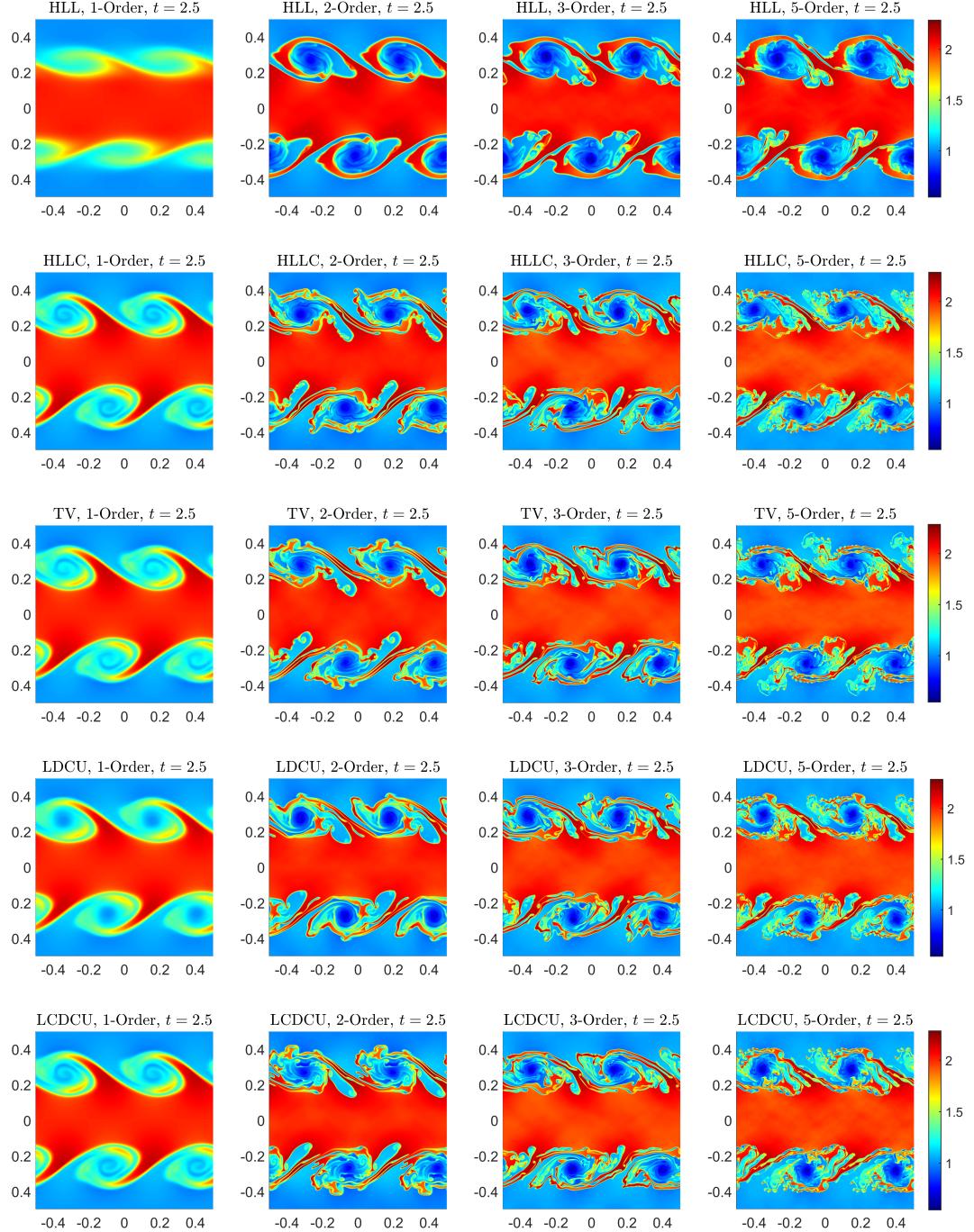


Figure 4.16: Example 14: Time snapshots of density  $\rho$  computed by the 1-Order, 2-Order, 3-Order, and 5-Order HLL (top row), HLLC (second row), TV (third row), LDCU (fourth row), and LCDCU (bottom row) schemes at  $t = 2.5$ .

of numerical dissipation, with only minor differences observed in specific test cases. The transition from first- to second-order accuracy yields the most significant improvement in resolution, whereas higher-order versions (third- and fifth-order) further enhance accuracy and efficiency for complex multidimensional flows. One can see that these low-dissipation schemes achieve better resolution than HLL counterparts near the contact waves, and among the four low-dissipation schemes, TV splitting schemes exhibit slightly higher dissipation in several examples, and fail in the Riemann problem — Configuration 3. While the LCDCU schemes are slightly more computationally expensive than the other three low-dissipation schemes, compared with the HLLC, TV, and LDCU schemes, they can be directly applied to other systems since they only need to compute the corresponding eigenvectors

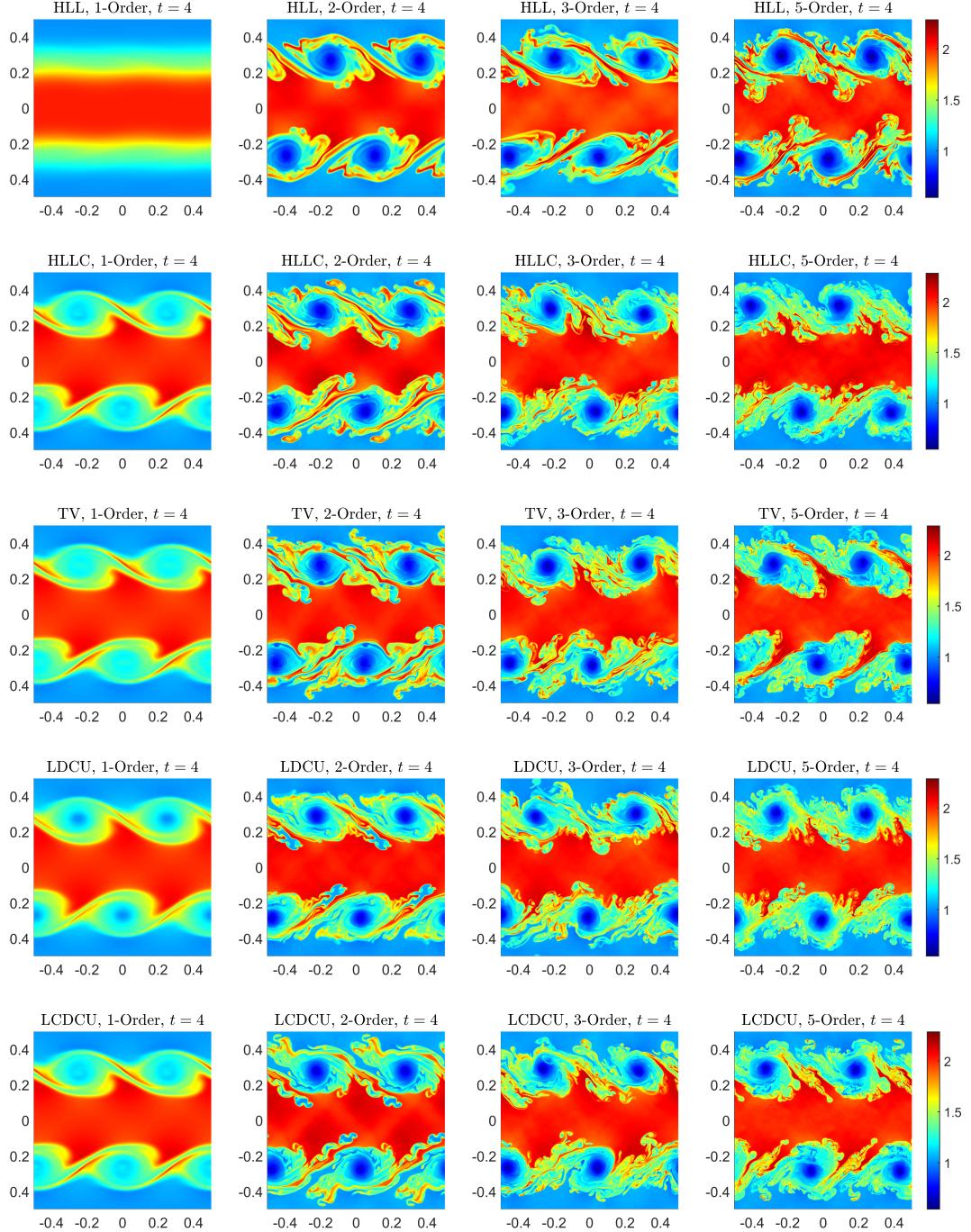


Figure 4.17: Example 14: Time snapshots of density  $\rho$  computed by the 1-Order, 2-Order, 3-Order, and 5-Order HLL (top row), HLLC (second row), TV (third row), LDCU (fourth row), and LCDCU (bottom row) schemes at  $t = 4$ .

based on the systems on hand. Overall, this study confirms that each of the considered solvers represents a viable and efficient option for the simulation of compressible flows. The comparative findings provide practical guidance for the choice of low-dissipation schemes in applications requiring both accuracy and robustness.

#### Declarations:

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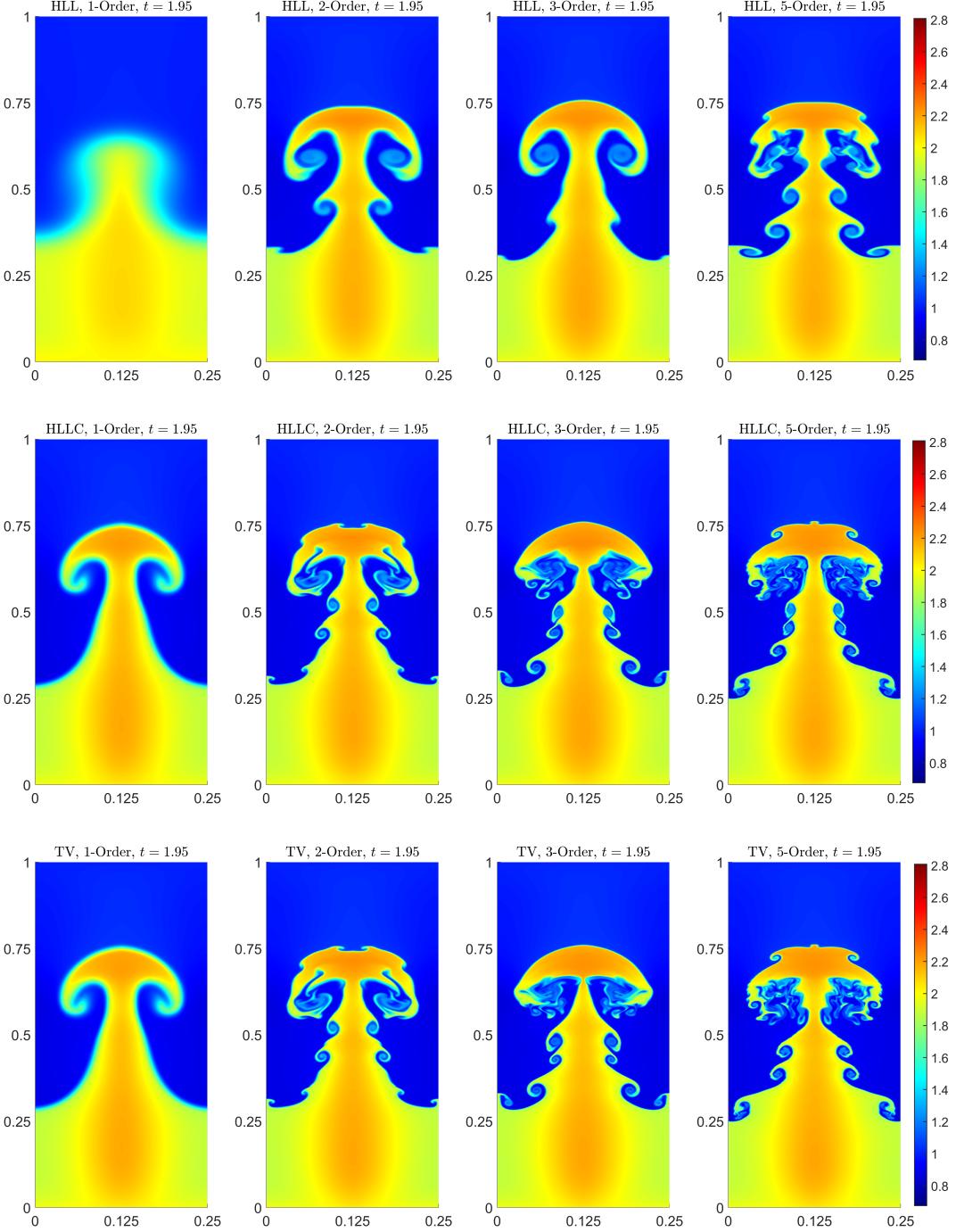


Figure 4.18: Example 15: Density  $\rho$  computed by the 1-Order (first column), 2-Order (second column), 3-Order (third column), and 5-Order (fourth column) HLL (top row), HLLC (second row), and TV (bottom row) schemes at  $t = 1.95$ .

für gekoppelte Mehrskalenprobleme, 5255842915) und (Zufällige kompressible Euler Gleichungen: Numerik und ihre Analysis, 5255853336) HE5386/27-1, and the Deutsche Forschungsgemeinschaft (DFG, German Research Foundation) - SPP 2183: Eigenschaftsgeregelte Umformprozesse with the Project(s) HE5386/19-2,19-3 Entwicklung eines flexiblen isothermen Reckschmiedeprozesses für die eigenschaftsgeregelte Herstellung von Turbinenschaufeln aus Hochtemperaturwerkstoffen (424334423).

**Conflicts of interest.** On behalf of all authors, the corresponding author states that there is no conflict of interest.

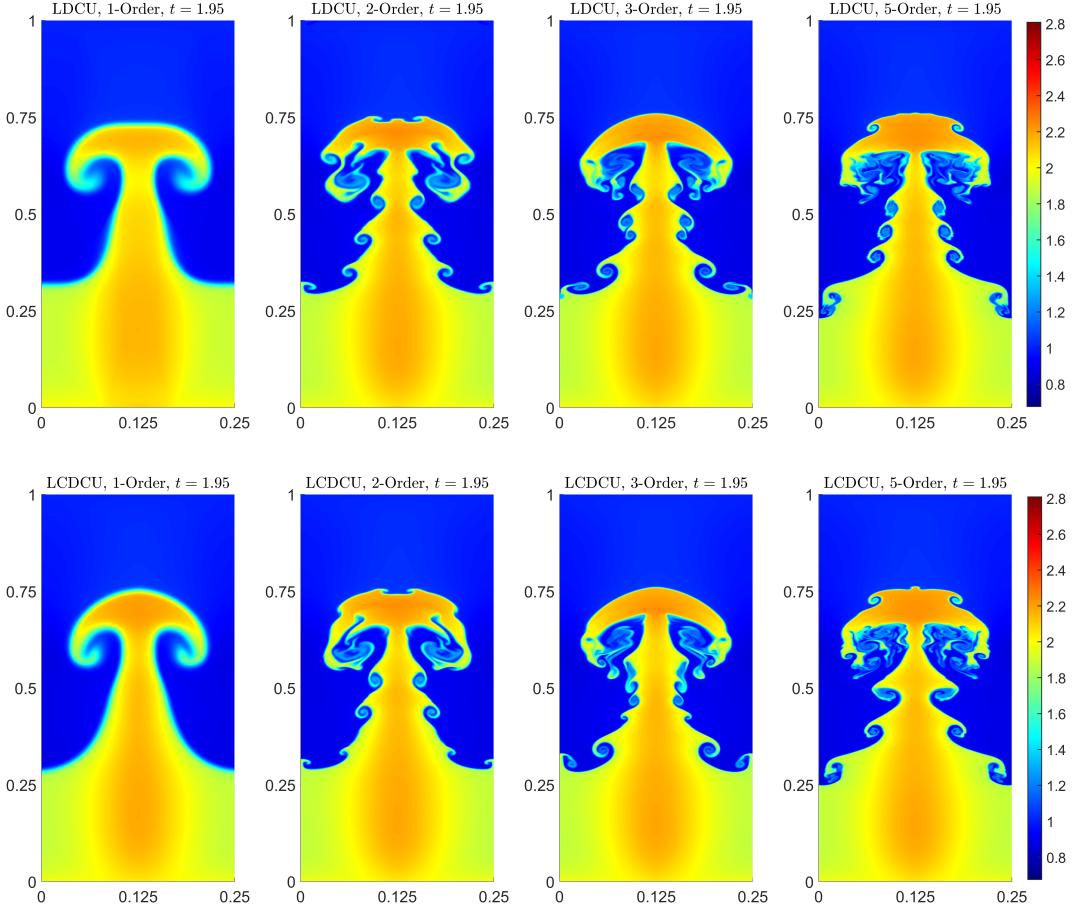


Figure 4.19: Example 15: Density  $\rho$  computed by the 1-Order (first column), 2-Order (second column), 3-Order (third column), and 5-Order (fourth column) LDCU (top row) and LCDCU (bottom row) schemes at  $t = 1.95$ .

**Data and software availability.** The data that support the findings of this study and FORTRAN codes developed by the authors and used to obtain all of the presented numerical results are available from the corresponding author upon reasonable request.

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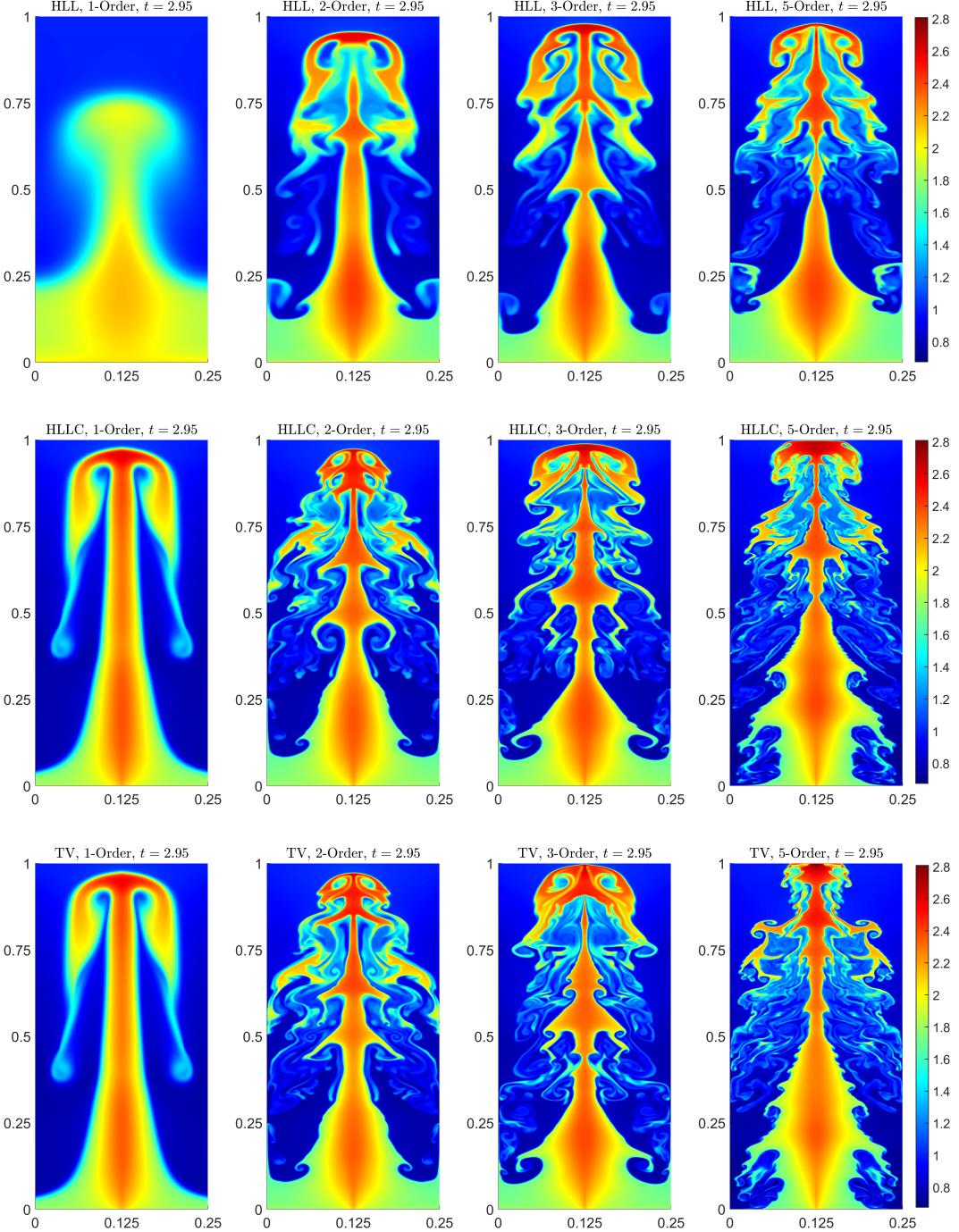


Figure 4.20: Example 15: Density  $\rho$  computed by the 1-Order (first column), 2-Order (second column), 3-Order (third column), and 5-Order (fourth column) HLL (top row), HLLC (second row), and TV (bottom row) schemes at  $t = 2.95$ .

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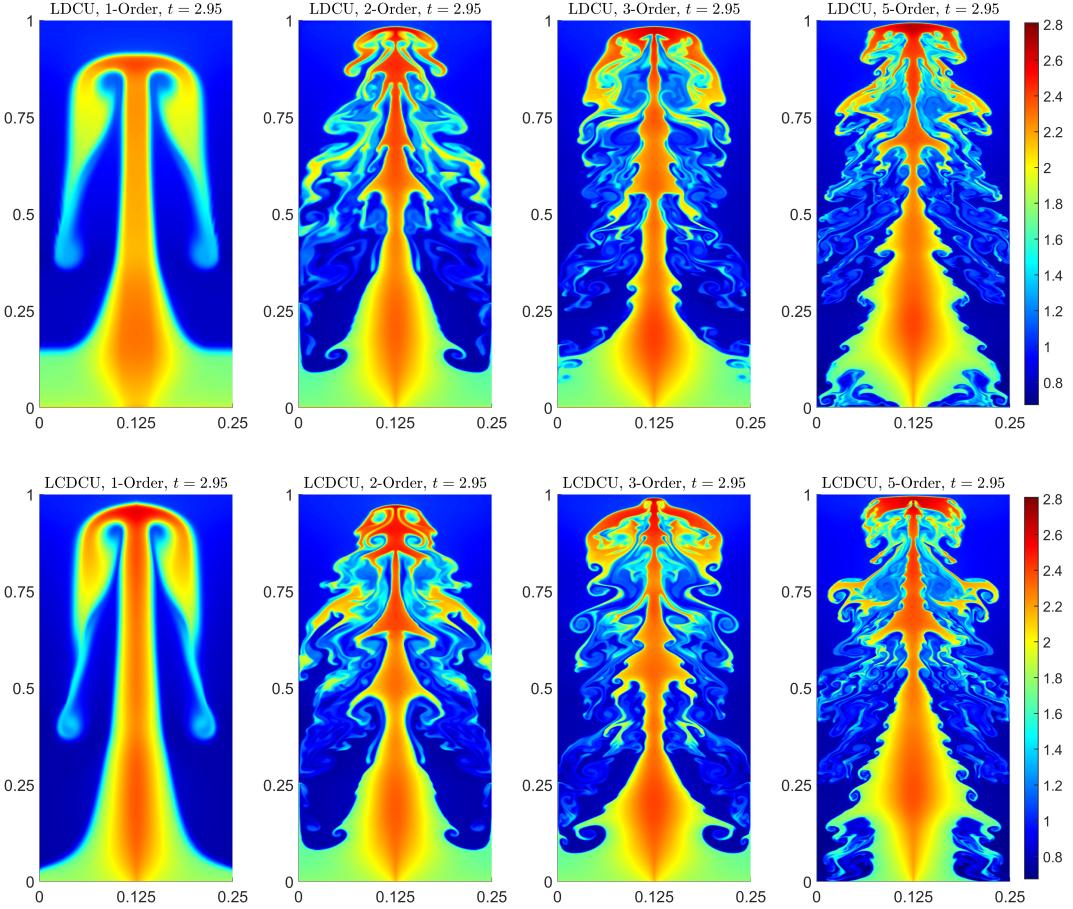


Figure 4.21: Example 15: Density  $\rho$  computed by the 1-Order (first column), 2-Order (second column), 3-Order (third column), and 5-Order (fourth column) LDCU (top row) and LCDCU (bottom row) schemes at  $t = 2.95$ .

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