

Definitions

Nonlinear differential eqns

$$\frac{d}{dt}x = f(x, u) \quad \begin{array}{l} \text{vector of control inputs} \\ \text{vector of state} \end{array}$$

For mechanical systems ($F=ma$)

q — position variables (joint angles, etc)

\dot{q} — velocities

$$\ddot{q} = f(q, \dot{q}, u) \quad \text{second-order diff eqn}$$

$$\ddot{q} = f_1(q, \dot{q}) + f_2(q, \dot{q}) u \quad \text{"control affine"}$$

\mathbb{R}^n \mathbb{R}^m $\mathbb{R}^{n \times m}$

Def

A system

is

fully-actuated in state (q, \dot{q}) if $f_2(q, \dot{q})$ is full row rank

Def

underactuated in (q, \dot{q}) if $\text{rank}[f_2(q, \dot{q})] < n$
may be state dependent,

Feed back Cancellation

Given $\ddot{q} = f_1(q, \dot{q}) + f_2(q, \dot{q}) u$ f_1, f_2 are known

~~Consider the~~ ~~Consider the~~

Consider the control law

$$u = f_2^{-1}(q, \dot{q}) (\ddot{q}^d - f_1(q, \dot{q}))$$

2

$$\Rightarrow \ddot{q} = \ddot{q}^d$$

"feedback equivalent" to $\ddot{q} = u$

$f_2^{-1}(q, \dot{q})$ exists

| vs Feedback linearization

not the same

Defn

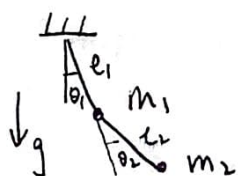
$$\ddot{q} = f(q, \dot{q}, u)$$

Input limits

State constraints

Model uncertainty / state estimation

Eqs of motion



Kinematics

$$\begin{matrix} \nearrow P_1 = \begin{bmatrix} l_1 \sin \theta_1 \\ -l_1 \cos \theta_1 \end{bmatrix} = \begin{bmatrix} l_1 s_1 \\ -l_1 c_1 \end{bmatrix} \\ \text{x1 of } m_1 \end{matrix}$$

$$P_2 = P_1 + \begin{bmatrix} l_2 \sin(\theta_1 + \theta_2) \\ -l_2 \cos(\theta_1 + \theta_2) \end{bmatrix}$$

$$\text{Kinematic energy } T = \frac{1}{2} \dot{P}_1^T m_1 \dot{P}_1 + \frac{1}{2} \dot{P}_2^T m_2 \dot{P}_2$$

$$\text{Potential energy } U = m_1 g y_1 + m_2 g y_2$$

\Rightarrow Lagrangian

$$\begin{aligned} & (m_1 + m_2) l_1^2 \ddot{q}_1 + m_2 l_1^2 (\ddot{q}_1 + \ddot{q}_2) + m_2 l_1 l_2 (2\ddot{q}_1 + \ddot{q}_2) c_2 \\ & - m_2 l_1 l_2 (2\dot{q}_1 + \dot{q}_2) \dot{q}_2 s_2 + (m_1 + m_2) l_1 g s_1 \\ & + m_2 g l_2 s_{1+2} = T_1 \end{aligned}$$

$$m_2 l_1^2 (\ddot{q}_1 + \ddot{q}_2) + m_2 l_1 l_2 \ddot{q}_1 c_2 + m_2 l_1 l_2 \dot{q}_1^2 s_2 + m_2 g l_2 s_{1+2} = T_2$$

The manipulator eqs

$$m_a = \sum_i F_i$$

$$\underbrace{M(q)}_{\substack{\uparrow \\ \text{mass/inertia} \\ \text{matrix}}} \ddot{q} + C(q, \dot{q}) \dot{q} = \tau_g(q) + B(q) u$$

\uparrow map from control to inputs to q

$$T = \frac{1}{2} \dot{q}^T M(q) \dot{q}$$

\uparrow
positive definite
invertible

$$\ddot{q} = M^{-1}(q) [\tau_g(q) + B(q) u - C(q, \dot{q}) \dot{q}]$$

$$f_2(q, \dot{q}) = M^{-1}(q) B(q) \quad B(q) \text{ full-row rank}$$

underactuated iff $\text{rank}[B] < \text{dim}(q)$
dimension $B(q)$ $\text{dim}(q) \times \text{dim}(u)$

\uparrow degree of freedom \uparrow control inputs

\Rightarrow fully-actuated

if $\text{dim}(u) < \text{dim}(q)$, ~~under articulated~~
under actuated

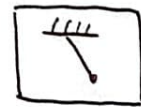
Feedback Cancellation of Double Pendulum

target single pendulum $\ddot{\theta}_1 = -\frac{g}{l} \sin \theta_1 - b \dot{\theta}_1$

dynamics $\ddot{\theta}_2 = 0$

$$\bar{u} = B^{-1} \left[C \dot{q} - \tau_g + M \begin{bmatrix} -\frac{g}{l} s_1 - b \dot{\theta}_1 \\ 0 \end{bmatrix} \right]$$

4 Course schedule



nonlinear dynamics
dynamic programming

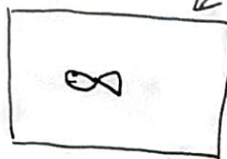


model
underactuated
systems

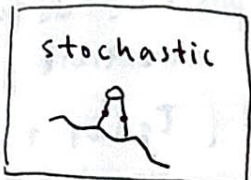
vehicles



manipulation
humanoids



Fluid dynamics



stochastic