

# Today: Acrobat, Cart-Poles, Quadrotors II

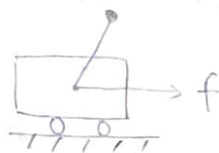
- Partial Feedback Linearization
  - Strong inertial coupling
- Energy-shaping w/ Lyapunov
- Differential Flatness

Last time: PFL of Cart-Pole

collocated PFL

$$\ddot{x} = \ddot{x}^d$$

$$\ddot{\theta} = \underline{\text{nonlinear}}$$



Non-collocated PFL

$$\ddot{\theta} = \ddot{\theta}^d$$

almost always

$$\ddot{x} = \text{nonlinear}$$



$$M(q) \ddot{q} + C(q, \dot{q}) \dot{q} = \tau_g(q) + Bu$$

$$q = \begin{bmatrix} q_1 \\ q_2 \end{bmatrix} \begin{matrix} \leftarrow \text{passive} \\ \leftarrow \text{actuated} \end{matrix}$$

$$B \in \mathbb{R}^{n \times m} \begin{matrix} \swarrow \text{num dof} \\ \uparrow \text{num actuators} \end{matrix}$$

$$M(q) = \begin{bmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{bmatrix}$$

$$\begin{aligned} M_{11}(q) \ddot{q}_1 + M_{12}(q) \ddot{q}_2 \\ = \tau_1(q, \dot{q}) \end{aligned}$$

$$\begin{aligned} M_{21}(q) \ddot{q}_1 + M_{22}(q) \ddot{q}_2 \\ = \tau_2(q, \dot{q}) + u \end{aligned}$$

$$T = \frac{1}{2} \dot{q}^T M(q) \dot{q} \quad M(q) > 0$$

$$\Rightarrow M_{11} > 0, M_{22} > 0$$

$$\ddot{q}_1 = M_{11}^{-1} [\tau_1 - M_{12} \ddot{q}_2]$$

$$M_{21} (M_{11}^{-1} [\tau_1 - M_{12} \ddot{q}_2]) + M_{22} \ddot{q}_2 = \tau_2 + u$$

$$(M_{22} - M_{21} M_{11}^{-1} M_{12}) \ddot{q}_2 + M_{21} M_{11}^{-1} \tau_1 - \tau_2 = u$$

$$\ddot{q}_2 = \ddot{q}_2^d$$

Schur Complement

$$> 0$$

$$\ddot{q}_2 = M_{12}^{\oplus} (\tau_1 - M_{11} \ddot{q}_1)$$

Pseudo-inverse

$\mathbb{R}^{(n-m) \times m}$   
soln

has a unique solution when  $\text{rank}(M_{12}) = n-m$

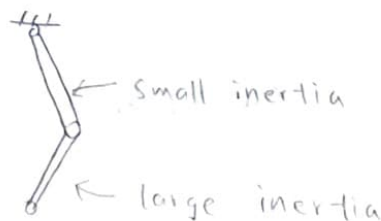


Can be state dependent

"inertial coupling"

Example:

Acrobat, small inertia on up part, larger inertia on lower part



Task-space "output"

$$z = h(q) \quad \text{e.g. example} \quad = -l \cos \theta$$

$$H = \frac{\partial h}{\partial q} \quad H_1 = \frac{\partial h}{\partial q_1} \quad H_2 = \frac{\partial h}{\partial q_2}$$

$$H = [H_1, H_2]$$

Theorem 3.1 - Task Space PFL

If the actuated joints are commanded so that

$$\ddot{q}_2 = \bar{H}^+ [\ddot{y}^d - \dot{H} \dot{q} - H_1 M_{11}^{-1} \tau_1],$$

where  $\bar{H} = H_2 - H_1 M_{11}^{-1} M_{12}$  and  $\bar{H}^+$  is the right Moore-Penrose pseudo-inverse,

$$\bar{H}^+ = \bar{H}^T (\bar{H} \bar{H}^T)^{-1}$$

then we have

$$\ddot{y} = \ddot{y}^d$$

subject to

$$\text{rank}(\bar{H}) = p,$$

proof sketch.

Differentiating the output function we have

$$\dot{y} = H \dot{q}$$

$$\ddot{y} = \dot{H} \dot{q} + H_1 \ddot{q}_1 + H_2 \ddot{q}_2$$

Solving 32 for the dynamics of the unactuated joints we have:

$$\ddot{q}_1 = M_{11}^{-1} (\tau_1 - M_{12} \ddot{q}_2)$$

Substituting, we have

$$\ddot{Y} = \dot{H} \dot{q} + H_1 M_{11}^{-1} \tau_1 + \underbrace{(H_2 - H_1 M_{11}^{-1} M_{12})}_{\bar{H}} \ddot{q}_2$$

$$\text{take } \ddot{q}_2 = \bar{H}^+ [\ddot{Y}^d - \dot{H} \dot{q} - H_1 M_{11}^{-1} \tau_1]$$

$$\begin{aligned} \ddot{Y} &= \dot{H} \dot{q} + H_1 M_{11}^{-1} \tau_1 + \bar{H} \bar{H}^+ [\ddot{Y}^d - \dot{H} \dot{q} - H_1 M_{11}^{-1} \tau_1] \\ &= \dot{H} \dot{q} + H_1 M_{11}^{-1} \tau_1 + \ddot{Y}^d - \dot{H} \dot{q} - H_1 M_{11}^{-1} \tau_1 \\ &= \ddot{Y}^d \end{aligned}$$

Note that the last line required the rank condition that  $\text{rank}(\bar{H}) = p$  be full <sup>row</sup> ~~row~~ column rank, the rows of  $\bar{H}$  are linearly independent, allowing  $\bar{H} \bar{H}^+ = I$

$$\text{null}(\bar{H} \bar{H}^T) = \text{null}(\bar{H}^T)$$

$$\text{if } \bar{H}^T x = 0, \text{ then } \bar{H} \bar{H}^T x = 0$$

$$\text{if } \bar{H} \bar{H}^T x = 0, \text{ then } \bar{H}^T x \in \text{null}(\bar{H})$$

$$\text{ran}(\bar{H}^T) \perp \text{null}(\bar{H})$$

$$\bar{H} y = 0, \quad y \perp \text{row vectors of } \bar{H}$$

$$y \perp \text{column vectors of } \bar{H}^T$$

if  $y = \bar{H}^T x$

$$y^T y = y^T \bar{H}^T x = x^T \bar{H} y = 0$$

then  $y = 0$

if  $\text{ran } A \perp \text{ran } B$ ,  $x \in \text{ran } A \cap \text{ran } B$

$$x^T x = 0, \quad x = 0$$

right pseudo inverse, full row rank, each rows are linearly independent

$$\ddot{q}_2 = \ddot{q}_2^d + K_p (q_2 - q_2^d) + K_d (\dot{q}_2 - \dot{q}_2^d)$$

Energy shaping for the Cart - Pole

Idea: Regulate pole to its homoclinic orbit using collocated PFL

$$\ddot{x} = u$$

$$\ddot{\theta} = -u \underset{\substack{\uparrow \\ \cos \theta}}{c} - \underset{\substack{\uparrow \\ \sin \theta}}{s}$$

$$E = \frac{1}{2} \dot{\theta}^2 - \cos \theta$$

$$E^d = 1 \leftarrow \text{homoclinic orbit of pendulum}$$

$$V(\cdot) = \frac{1}{2} \underbrace{(E - E^d)^2}_{\tilde{E}}$$

$$\tilde{E} = E - E^d$$

$$\dot{\tilde{E}} = \dot{E} - \dot{E}^d = \ddot{\theta} \ddot{s} + \sin \theta \cdot \dot{\theta}$$

$$= \ddot{\theta} (-u \cos \theta) + \dot{\theta} \sin \theta$$

$$= -u \ddot{\theta} \cos \theta$$

$$\dot{V}(x) = \tilde{E} \dot{\tilde{E}}$$

$$= (E - E^d) (-u \ddot{\theta} \cos \theta)$$

$$= -u \ddot{\theta} \cos \theta (E - E^d)$$

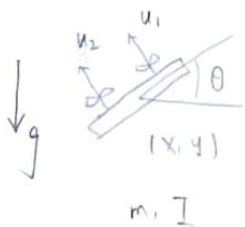
Choose  $u = k(\cos \theta) \dot{\tilde{E}}$

$$\Rightarrow \dot{V} = -k \dot{\tilde{E}}^2 \cos^2 \theta$$

Regulation on cart, cart at the center middle, and zero velocity

$$V(x) = \frac{1}{2} (E - E^d)^2 + \frac{1}{2} \dot{x}^2 + \frac{1}{2} \dot{\tilde{x}}^2$$

Quadrotor has larger range where LQR can be used



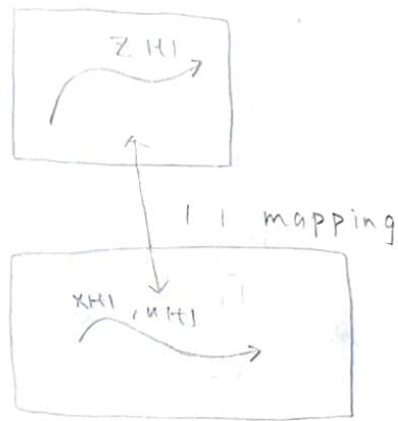
$$m\ddot{x} = -(u_1 + u_2) \sin \theta$$

$$m\ddot{y} = (u_1 + u_2) \cos \theta - mg$$

$$I\ddot{\theta} = r(u_1 - u_2)$$

Differential flatness

$$Z = h(q)$$

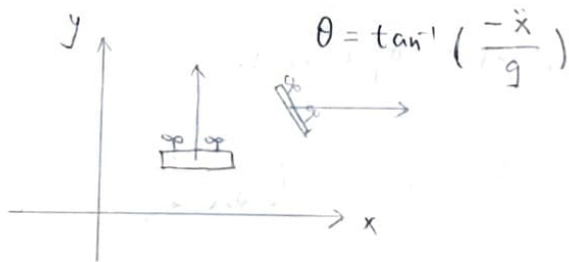


$$Z = \begin{bmatrix} x \\ y \end{bmatrix}$$

Claim: If you give me  $\forall t \in [t_0, t_f]$

$Z(t) \Rightarrow x(t), u(t)$   
 $\uparrow$  four times  
 must be differentiable

$$\frac{-m\ddot{x}}{m\ddot{y} + mg} = \frac{(u_1 + u_2) \sin \theta}{(u_1 + u_2) \cos \theta} = \tan \theta$$



$$\ddot{\theta} = f\left(\frac{d^2 \ddot{x}}{dt^2}, \frac{d^2 \ddot{y}}{dt^2}\right) = f\left(\frac{d^4 x}{dt^4}, \frac{d^4 y}{dt^4}\right)$$

given a dynamic system

$$\dot{x} = f(x, u)$$

$$Z = h(x, u, \dot{x}, \ddot{x})$$



Differential flatness in  $z$

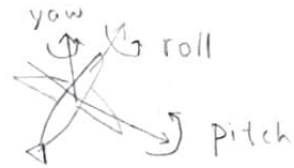
$$z = h(x, u, \dot{u}, \dots, \frac{d^k u}{dt^k})$$

$$x = x(z, \dot{z}, \dots, \frac{d^k z}{dt^k})$$

$$u = u(z, \dot{z}, \dots, \frac{d^k z}{dt^k})$$

3D Version

$$z = [x, y, z, \theta_{yaw}]$$



motors are not pure force, has torque or inertia coupling, ~~other~~ otherwise cannot stabilize at some state

moment produced by the rotating props

Note:

Linearizing the manipulator equations

$$\dot{x} = f(x, u) \approx f(x^*, u^*) + \left[ \frac{\partial f}{\partial x} \right]_{x=x^*, u=u^*} (x - x^*) + \left[ \frac{\partial f}{\partial u} \right]_{x=x^*, u=u^*} (u - u^*)$$

$$f(x, u) = \left[ M^{-1}(q) \left[ -C(q, \dot{q}) \dot{q} + \tau_g(q) + B u \right] \right]$$

$$\approx A_{lin} (x - x^*) + B_{lin} (u - u^*)$$



we define  $\bar{x} = x - x^*$ ,  $\bar{u} = u - u^*$ , and write

$$\dot{\bar{x}} = A_{lin} \bar{x} + B_{lin} \bar{u}$$

$$A_{lin} = \begin{bmatrix} 0 & I \\ M^{-1} \frac{\partial \tau_g}{\partial q} + \sum_j M^{-1} \frac{\partial B_j}{\partial q} u_j & 0 \end{bmatrix}_{x=x^*, u=u^*}$$

note

$$\begin{aligned} & \frac{\partial}{\partial q} \left\{ M^{-1}(q) [\tau_g(q) + B(q)u - C(q, \dot{q})\dot{q}] \right\} \\ &= \frac{\partial}{\partial q} M^{-1}(q) \cdot [\tau_g(q) + B(q)u - C(q, \dot{q})\dot{q}] \\ & \quad + M^{-1}(q) \left[ \frac{\partial \tau_g(q)}{\partial q} + \frac{\partial B(q)}{\partial q} u \right. \\ & \quad \left. - \frac{\partial C(q, \dot{q})}{\partial q} \cdot \dot{q} \right] \end{aligned}$$

at equilibrium point, we have  $\dot{q} = 0$  and

$$\tau_g(q) + B(q)u - C(q, \dot{q})\dot{q} = 0.$$

$$\begin{aligned} & \frac{\partial}{\partial q} \left\{ M^{-1}(q) [\tau_g(q) + B(q)u - C(q, \dot{q})\dot{q}] \right\} \\ &= M^{-1}(q) \left( \frac{\partial \tau_g(q)}{\partial q} + \frac{\partial B(q)}{\partial q} u \right) \end{aligned}$$

$$\frac{d}{d\dot{q}} \left\{ M^{-1}(q) [T_g(q) + B(q)u - C(q, \dot{q})\dot{q}] \right\}$$

$$= -M^{-1}(q) \left[ \frac{\partial C(q, \dot{q})}{\partial \dot{q}} \dot{q} + C(q, \dot{q}) \right]$$

when  $\dot{q} = 0$ ,  $C(q, \dot{q}) = 0$  ~~or~~

$$\frac{d}{d\dot{q}} \left\{ M^{-1}(q) [T_g(q) + B(q)u - C(q, \dot{q})\dot{q}] \right\} = 0$$

take derivative with respect to  $u$

$$\frac{\partial}{\partial u} \left\{ M^{-1}(q) [T_g(q) + B(q)u - C(q, \dot{q})\dot{q}] \right\}$$

$$= M^{-1}(q) B(q)$$

Manipulator equation of cart-pole system



$$T = \frac{1}{2} m_1 \dot{x}^2 + \frac{1}{2} m_2 [(\dot{x} + \dot{\theta} l \cos \theta)^2 + (\dot{\theta} l \sin \theta)^2]$$

$$V = m_2 g l \cos \theta$$

$$L = T - V$$

$$\frac{\partial L}{\partial \dot{x}} = m_1 \dot{x} + m_2 (\dot{x} + \dot{\theta} l \cos \theta)$$

$$\frac{\partial L}{\partial \dot{\theta}} = m_2 (\dot{x} + \dot{\theta} l \cos \theta) l \sin \theta + m_2 \dot{\theta} l \sin \theta \cdot l \sin \theta$$

ft

$$\frac{\partial L}{\partial x} = 0$$

$$\begin{aligned}\frac{\partial L}{\partial \theta} &= m_2 (\dot{x} + \dot{\theta} l \cos \theta) (-\dot{\theta} l \sin \theta) + m_2 \dot{\theta} l \sin \theta \dot{\theta} l \cos \theta \\ &\quad - m_2 g l \sin \theta \\ &= -m_2 \dot{x} \dot{\theta} l \sin \theta - m_2 \dot{\theta}^2 l^2 \sin \theta \cos \theta + m_2 \dot{\theta}^2 l^2 \sin \theta \cos \theta \\ &\quad - m_2 g l \sin \theta \\ &= -m_2 (\dot{x} \dot{\theta} + g l) \sin \theta\end{aligned}$$

Lagrangian equation

$$(m_1 + m_2) \ddot{x} + m_2 \ddot{\theta} l \cos \theta - m_2 l \dot{\theta}^2 \sin \theta = f$$

$$m_2 \ddot{x} l \cos \theta + m_2 l^2 \ddot{\theta} + m_2 g l \sin \theta = 0$$

$$M(q) = \begin{bmatrix} m_1 + m_2 & m_2 l \cos \theta \\ m_2 l \cos \theta & m_2 l^2 \end{bmatrix} \quad C(q, \dot{q}) = \begin{bmatrix} 0 & -m_2 l \dot{\theta} \sin \theta \\ 0 & 0 \end{bmatrix}$$

$$T_g(q) = \begin{bmatrix} 0 \\ -m_2 g l \sin \theta \end{bmatrix} \quad B = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$$

$$\ddot{x} = \frac{1}{m_c + m_p \sin^2 \theta} \left[ f + m_p \sin \theta (l \dot{\theta}^2 + g \cos \theta) \right]$$

$$\ddot{\theta} = \frac{1}{l (m_c + m_p \sin^2 \theta)} \left[ -f \cos \theta - m_p l \dot{\theta}^2 \cos \theta \sin \theta - (m_c + m_p) g \sin \theta \right]$$

$$A_{lin} = \begin{bmatrix} 0 & I \\ M^{-1} \frac{\partial T_g}{\partial \dot{q}} + \sum_j \bar{M}_j^{-1} \frac{\partial B_j}{\partial \dot{q}} u_j & 0 \end{bmatrix}$$

$$M^{-1} = \frac{1}{(m_1 + m_2)m_2 l^2 - m_2^2 l^2 \cos^2 \theta} \begin{bmatrix} m_2 l^2 & -m_2 l \cos \theta \\ -m_2 l \cos \theta & m_1 + m_2 \end{bmatrix}$$

$$= \frac{1}{(m_1 + m_2 \sin^2 \theta) m_2 l^2} \begin{bmatrix} m_2 l^2 & -m_2 l \cos \theta \\ -m_2 l \cos \theta & m_1 + m_2 \end{bmatrix}$$

$$\frac{\partial T_g}{\partial \dot{q}} = \begin{bmatrix} 0 & 0 \\ 0 & -m_2 g l \cos \theta \end{bmatrix}$$

$$\frac{\partial B}{\partial \dot{q}} = \begin{bmatrix} 0 \\ 0 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

$$A_{lin} = \begin{bmatrix} 0 & I \\ M^{-1} \frac{\partial T_g}{\partial \dot{q}} & 0 \end{bmatrix}$$

$$M^{-1} \frac{\partial T_g}{\partial \dot{q}} = \frac{1}{(m_1 + m_2 \sin^2 \theta) m_2 l^2} \begin{bmatrix} m_2 l^2 & -m_2 l \cos \theta \\ -m_2 l \cos \theta & m_1 + m_2 \end{bmatrix} \begin{bmatrix} 0 & 0 \\ 0 & -m_2 g l \cos \theta \end{bmatrix}$$

$$= \begin{bmatrix} 0 & \frac{m_2^2 g l^2 \cos^2 \theta}{\cancel{m_2 l^2}} \\ 0 & -(m_1 + m_2) m_2 g l \cos \theta \end{bmatrix} \frac{1}{(m_1 + m_2 \sin^2 \theta) m_2 l^2}$$

$$= \begin{bmatrix} 0 & \frac{m_2 g \cos^2 \theta}{m_1 + m_2 \sin^2 \theta} \\ 0 & -\frac{(m_1 + m_2) g \cos \theta}{(m_1 + m_2 \sin^2 \theta) l} \end{bmatrix}$$

$$B_{lin} = \begin{bmatrix} 0 \\ M^{-1} B \end{bmatrix} \quad x = x^*, \quad u = u^*$$

$$M^{-1} B = \frac{1}{(m_1 + m_2 \sin^2 \theta) m_2 l^2} \begin{bmatrix} m_2 l^2 & -m_2 l \cos \theta \\ -m_2 l \cos \theta & m_1 + m_2 \end{bmatrix} \begin{bmatrix} 1 \\ 0 \end{bmatrix}$$

$$= \frac{1}{m_1 + m_2 \sin^2 \theta} \begin{bmatrix} 1 \\ -\frac{\cos \theta}{l} \end{bmatrix}$$

Note we linearize near  $x=0, \theta=\pi$

$$M^{-1} \frac{\partial \mathcal{L}_j}{\partial \dot{q}} = \begin{bmatrix} 0 & \frac{m_2}{m_1} q \\ 0 & \frac{m_1 + m_2}{m_1} \frac{q}{l} \end{bmatrix}$$

$$M^{-1} B = \begin{bmatrix} \frac{1}{m_1} \\ -\frac{\cos \theta}{m_1 l} \end{bmatrix}$$