

fluid

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Citing

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1 Flow past a cylinder

Let ρ_0 be the radius of the cylinder, ρ, ξ the polar coordinate system in use. One possible solution of this problem have these potential and streamline functions:

$$\phi(\rho, \xi) = \left(\rho + \frac{\rho_0^2}{\rho} \right) \cos \xi \quad (1)$$

$$\psi(\rho, \xi) = \left(\rho - \frac{\rho_0^2}{\rho} \right) \sin \xi \quad (2)$$

Although these equations are deeply coupled, the radius ρ and the phase ξ can be obtained as a function of the other quantities. For our purposes, we use ψ .

$$\rho(\psi, \xi) = \frac{\psi + \sqrt{\psi^2 + 4\rho_0^2 \sin^2 \xi}}{2 \sin \xi} \quad (3)$$

$$\xi(\psi, \rho) = \arcsin \left(\frac{\rho \psi}{\rho^2 - \rho_0^2} \right) \quad (4)$$

The velocity field can also be derived through

$$\begin{aligned} v_\rho(\rho, \xi) &= \frac{\partial \phi}{\partial \rho} = \left(1 - \frac{\rho_0^2}{\rho^2}\right) \cos \xi \\ v_\xi(\rho, \xi) &= \frac{1}{\rho} \frac{\partial \phi}{\partial \xi} = -\left(1 + \frac{\rho_0^2}{\rho^2}\right) \sin \xi \end{aligned} \quad (5)$$

2 Conformal mapping

From the reference plane, which is equivalent to a two-pole machine, we use a complex map to obtain the quantities in the actual plane. Let p be the number of pole pairs. Then:

$$\begin{aligned} \zeta &\xrightarrow{\mathcal{M}} z = \sqrt[p]{\zeta} \\ \rho e^{j\xi} &\xrightarrow{\mathcal{M}} r e^{j\vartheta} = \sqrt[p]{\rho} e^{j\xi/p} \\ \chi + j\eta &\xrightarrow{\mathcal{M}} x + jy \end{aligned} \quad (6)$$

It is easy to find the inverse map:

$$\mathcal{M}: \sqrt[p]{\cdot} \quad \mathcal{M}^{-1}: (\cdot)^p \quad (7)$$

In the transformed plane, the velocities have a different expression:

$$\begin{aligned} v_r(r, \vartheta) &= p \left(r^{p-1} - \frac{R_0^{2p}}{r^{p+1}} \right) \cos p\vartheta \\ v_\vartheta(r, \vartheta) &= -p \left(r^{p-1} + \frac{R_0^{2p}}{r^{p+1}} \right) \sin p\vartheta \end{aligned} \quad (8)$$

This vector field is tangent to the streamlines in every point in the transformed plane. In order to work with this field in x, y coordinates, we need a rotational map:

$$\begin{aligned} v_x(r, \vartheta) &= v_r \cos \vartheta - v_\vartheta \sin \vartheta \\ v_y(r, \vartheta) &= v_r \sin \vartheta + v_\vartheta \cos \vartheta \end{aligned} \quad (9)$$

3 Computation of flux-barrier base points

Let the flux-barrier and flux-carrier thicknesses be given. Then the base points for the flux-barriers can be computed easily. Let D_r be the rotor outer diameter, $w_{\text{rib},t}$ the tangential iron rib width, $w_{c,k}$ the k -th flux-carrier width, and $t_{c,k}$ the k -th flux-barrier thickness.¹ Then

$$\begin{aligned} R_r &= \frac{D_r}{2} - w_{\text{rib},t} \\ R_{A_1} &= R_r - w_{c,1} \\ R_{B_1} &= R_{A_1} - t_{c,1} \\ &\vdots \end{aligned} \tag{10}$$

So, in general:

$$\begin{aligned} R_{A_k} &= R_{B_{k-1}} - w_{c,k} \\ R_{B_k} &= R_{A_{k-1}} - t_{c,k} \end{aligned} \tag{11}$$

with the exception $R_{B_0} = R_r$.

Now we know both the radii and the angle – always $\pi/(2p)$ – of the flux-barrier internal points. So we can compute their respective streamline value.

3.1 Magnet insertion

$$w_{\text{rib},k} = w_{\text{rib},k} + w_{m,k}$$

where $w_{m,k}$ is the k -th magnet width.

3.2 Central base points

We refer to points A and B.

¹You may wonder why the main dimensions of the flux-carrier and flux-barrier differ in the name (width versus thickness). This is due to a choice of mine, because I prefer to refer to width when the flux flows perpendicularly to the dimension, and to thickness when it flows in parallel.

The line describing the q -axis is

$$\begin{aligned} y &= mx + q \\ m &= \tan \frac{\pi}{2p} \\ q &= \frac{w_{\text{rib}}}{\cos \frac{\pi}{2p}} \end{aligned} \tag{12}$$

$$\begin{cases} y_{A'} - mx_{A'} - q = 0 \\ x_{A'} - r_{A'}(\psi_A, \vartheta_{A'}) \cos \vartheta_{A'} = 0 \\ y_{A'} - r_{A'}(\psi_A, \vartheta_{A'}) \sin \vartheta_{A'} = 0 \end{cases} \tag{13}$$

where ϑ_A is used as the third degree of freedom and r_A is then a function of it. The solution of such system can be determined solving the single equation

$$r_{A'}(\psi_A, \vartheta_{A'}) (\sin \vartheta_{A'} - m \cos \vartheta_{A'}) - q = 0 \tag{14}$$

in the unknown $\vartheta_{A'}$. The function $r(\psi, \vartheta)$ is simply

$$r(\psi, \vartheta) = \sqrt[p]{\rho(\psi, \vartheta/p)}$$

The same equation can be written for point B with the proper substitution and repeated for all the flux-barriers.

4 Outer base points

We refer to points C, D, and E. If the flux-barrier angle, α_b , is given, then

$$\begin{aligned} x_E &= R_r \cos\left(\frac{\pi}{2p} - \alpha_b\right) \\ y_E &= R_r \sin\left(\frac{\pi}{2p} - \alpha_b\right) \end{aligned} \tag{15}$$

Points C and D results from the connection of the flux-barrier sidelines and point E. This connection should be as smooth as possible in order to avoid dangerous mechanical stress concentrations. We are going to

use circular arcs to make this connection. So we impose the tangency between the flux-barrier sideline and the arc, between the arc and the radius through point E. The tangent to the sideline can be obtained through the velocity field described above.

Then we want point C to lay on the flux-barrier sideline. These conditions represent a nonlinear system of 4 equations, in 6 unknowns. So we need two more equations, which are that points C and E belong to the fillet circle with radius R .

$$\begin{cases} x_C - r_C(\psi_C, \vartheta_C) \cos \vartheta_C = 0 \\ y_C - r_C(\psi_C, \vartheta_C) \sin \vartheta_C = 0 \\ (x_C - x_{O_C})^2 + (y_C - y_{O_C})^2 - R_{EC}^2 = 0 \\ (x_E - x_{O_C})^2 + (y_E - y_{O_C})^2 - R_{EC}^2 = 0 \\ (x_{O_C} - x_E)y_E - (y_{O_C} - y_E)x_E = 0 \\ (x_O - x_C)v_x(r_C, \vartheta_C) + (y_O - y_C)v_y(r_C, \vartheta_C) \end{cases} \quad (16)$$

The very same system can be written and solved for point D.

5 Flux-barrier sideline points