# SCANNING ELECTRON MICROSCOPY

Copies of transparencies

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### **OUTLINE**

## Introduction to scanning probe imaging

- Electron gun and electromagnetic lenses
- Principles of backscattered and secondary electron emission and their dependence on sample composition, topography, voltage, detector position, sample tilt, etc.,
- Resolution and the constraints imposed by aberrations, beam spreading, signal to noise ratio and type of signal
- Other types of signals, including absorbed current, cathodoloumninescence
- Examples of SEM investigations in materials science
- Principles of x-ray emission and detection
- Qualitative and quantitative x-ray analysis for elemental identification and composition
- X-ray mapping, resolution of energy dispersive x-ray spectroscopy (EDAX)
- Electron backscattering patterns: principle, applications for texture and orientation measurements, crystallography in the SEM
- Environmental microscopy, insulating samples
- Modern high resolution capabilities, field emission SEMs, low voltage operation

## **BOOKS**

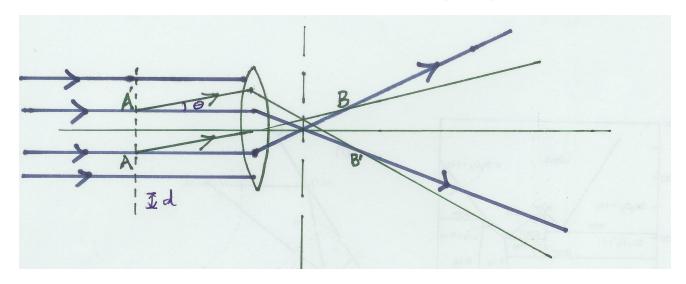
Scanning electron microscopy and x-ray microanalysis Goldstein et al., (8 authors)

Scanning electron microscopy
O.C. Wells

Micro structural Characterization of Materials
D. Brandon and W.D. Kaplan

Also look under scanning electron microscopy in the library. The metals Handbook and a book on Fractrography by Hull are additional sources of information on metallurgical aspects.

## Conventional Imaging



AA' is imaged at BB'. Sin  $\theta \sim \lambda/d$  Optically,  $\lambda_{min} \sim 0.5 \,\mu m$ ,  $d_{min} \sim 0.3 \,\mu m$ 

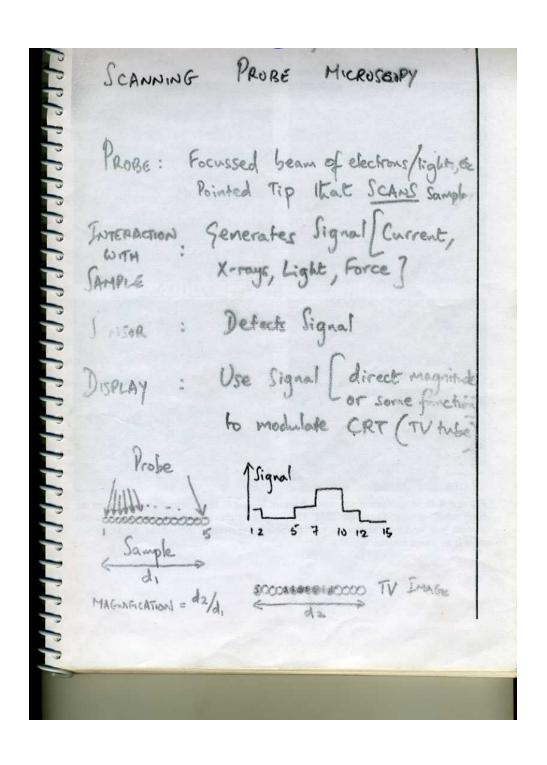
CONTRAST: Amplitude, Frequency, Phase

DEPTH OF FIELD ~  $\lambda$ / Sin  $\theta$  ~  $\lambda$  at high magnification, i.e., 0.5  $\mu$ m

STEREO: Eyes see slightly different images

### **LIMITATIONS**

Poor resolution for many fine scale materials, Poor depth of field, Need to polish / etch sample, No compositional information



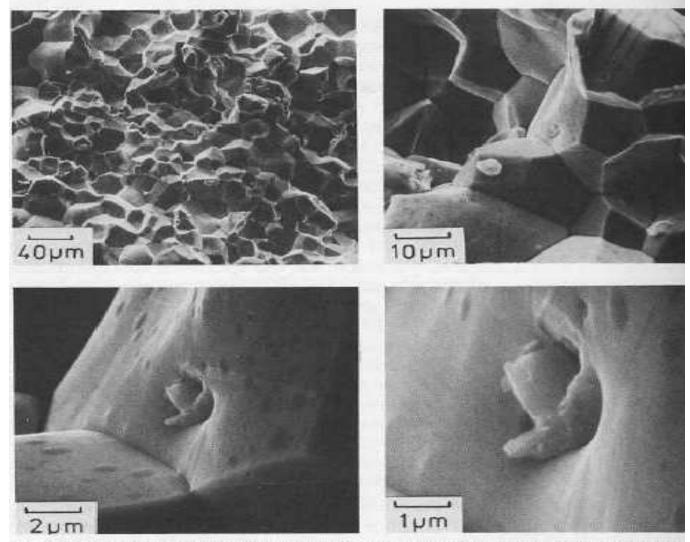


Figure 4.6. Magnification series of a fracture surface of high-purity iron, illustratin rapid surveying capability of the SEM. The images are recorded at constant objective strength and working distance. Note that focus is maintained throughout the series there is no image rotation.

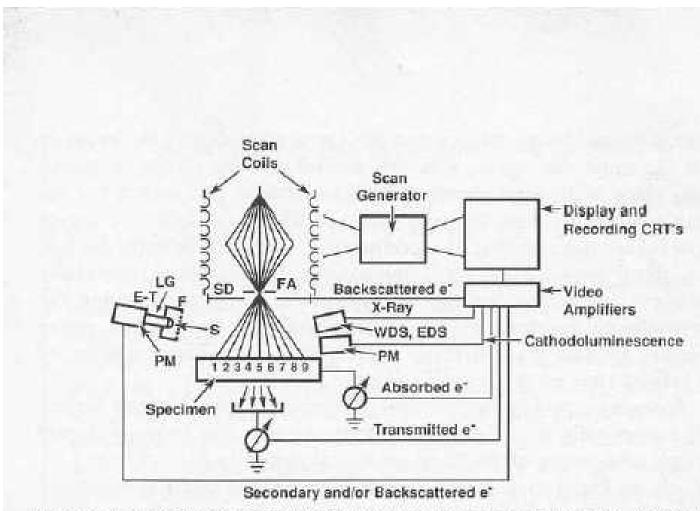


Figure 4.1. Schematic illustration of the scanning system of the SEM. Abbreviations: FA, final aperture; SD, solid-state backscattered-electron detector; EDS, energy-dispersive x-ray spectrometer; WDS, wavelength-dispersive x-ray spectrometer; CRTs, cathode ray tubes, and E-T, Everhart-Thornley secondary/backscattered-electron detector, consisting of F, Faraday cage; S, scintillator; LG, light guide; and PM, photomultiplier. Successive beam positions are indicated by the numbered rays of a scanning sequence.

## Table 4.1 Area Sampled as a Function of Magnification<sup>a</sup>

Magnification	Area on
	sample
10X	$(1 \text{ cm})^2$
100X	$(1 \text{ mm})^2$
1,000X	$(100  \mu m)^2$
10,000X	$(10  \mu m)^2$
100,000X	$(1  \mu m)^2$
1,000,000X	$(100 \text{ nm})^2$

<sup>&</sup>lt;sup>a</sup> Assumes CRT screen measures 10 cm x 10 cm.

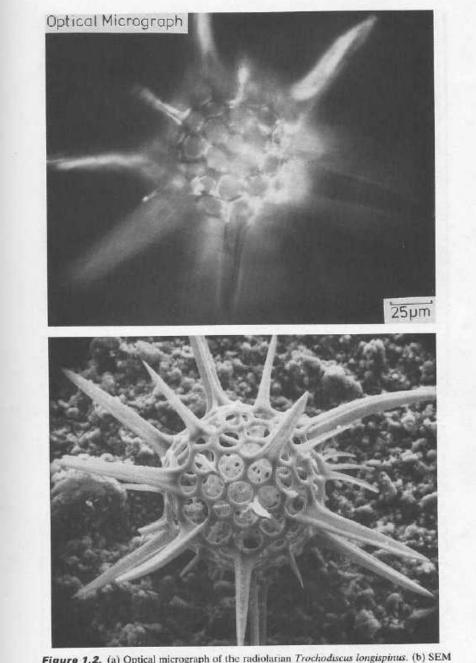


Figure 1.2. (a) Optical micrograph of the radiolarian *Trochodiscus longispinus*. (b) SEM micrograph of same radiolarian. The greater depth of focus and superior resolving capability are apparent.

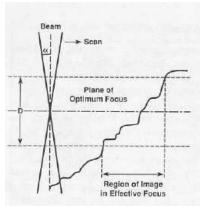


Figure 4.9. Schematic illustration of the depth of focus (field) in a SEM image.

optimum focus. For a sufficiently rough specimen, it is clear from Fig. 4.9 that the beam intersecting some features will become so large that some portion of the specimen will not appear in focus.

To calculate the depth of focus, we must know at what distance above and below the plane of optimum focus the beam has broadened to a noticeable size. The depth-of-focus criterion then depends on where the beam reaches a condition of overlapping adjacent pixels. The geometrical argument in Fig. 4.9 indicates that, to a first approximation, the vertical distance D/2 required to broaden the beam of minimum size  $r_0$  to a radius r is given by

$$\tan \alpha = \frac{r}{D/2}. (4.4a)$$

For small angles,  $\tan \alpha \approx \alpha$ ,

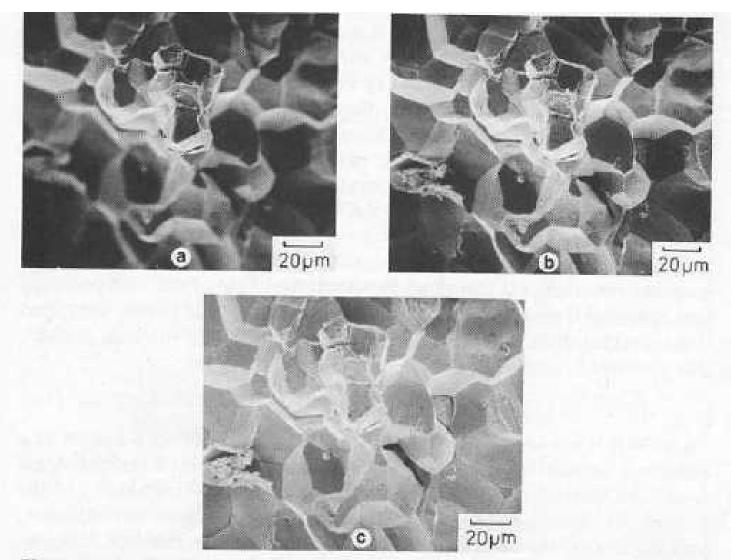
$$D/2 \approx r/\alpha$$
 (4.4b)

$$D \approx 2r/\alpha$$
, (4.4c)

where  $\alpha$  is the beam divergence, as defined by the semicone angle. Consider that r equals the pixel size of the image. On a high-resolution CRT (spot size = 0.1 mm =  $100 \, \mu \text{m}$ ), most observers will find that defocusing becomes objectionable when two pixels are fully overlapped. The pixel size on the specimen is then given by  $0.1/M \, \text{mm}$ , where M is the magnification. Substituting this expression into Eq. (4.4b) gives a practical expression for the depth of focus:

$$D = \frac{0.2}{\alpha M} \text{ mm.} \tag{4.4d}$$

Equation (4.4) indicates that to increase the depth of focus D, the operator can choose to reduce either the magnification M or the divergence  $\alpha$ . Changing the magnification is not generally an option, since the magnification is chosen to fill the image with the details of interest. This leaves the divergence as the adjustable parameter. The divergence is adjusted by the selection of the final aperture radius,  $R_{\rm Ap}$ 



**Figure 4.10.** Appearance of a fracture surface with different depths of focus obtained by varying the aperture size and the working distance. (a) Small depth of focus, most of the field of view is out of focus (15-mm working distance, 600- $\mu$ m aperture), (b) Intermediate depth of focus; more of the surface appears in focus (15-mm working distance, 100- $\mu$ m aperture), (c) maximum depth of focus, entire field in focus (45-mm working distance, 100- $\mu$ m aperture). Beam energy 20 keV.

Table 4.3. Depth of Focus (Field) in µm

Magnification	$\alpha$ (rad)		
	$5 \times 10^{-3}$	$1 \times 10^{-2}$	$3 \times 10^{-2}$
10X	4,000	2,000	670
50X	800	400	133
100X	400	200	67
500X	80	40	13
1,000X	40	20	6.7
10,000X	4	2	0.67
100,000X	0.4	0.2	0.067

Table 4.2. Size of Picture Element as a Function of Magnification"

Magnification	Edge of picture element	
10X	10 μm	
100X	1 µm	
1,000X	0.1 µm (100 nm)	
10,000X	0.01 µm (10 nm)	
100,000X	1 nm	

<sup>&</sup>quot;  $1000 \times 1000$  scan matrix;  $10 \, \mathrm{cm} \times 10 \, \mathrm{cm}$  display on CRT.

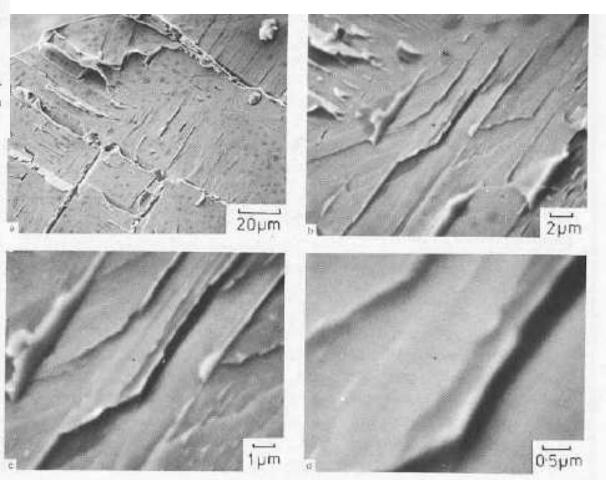
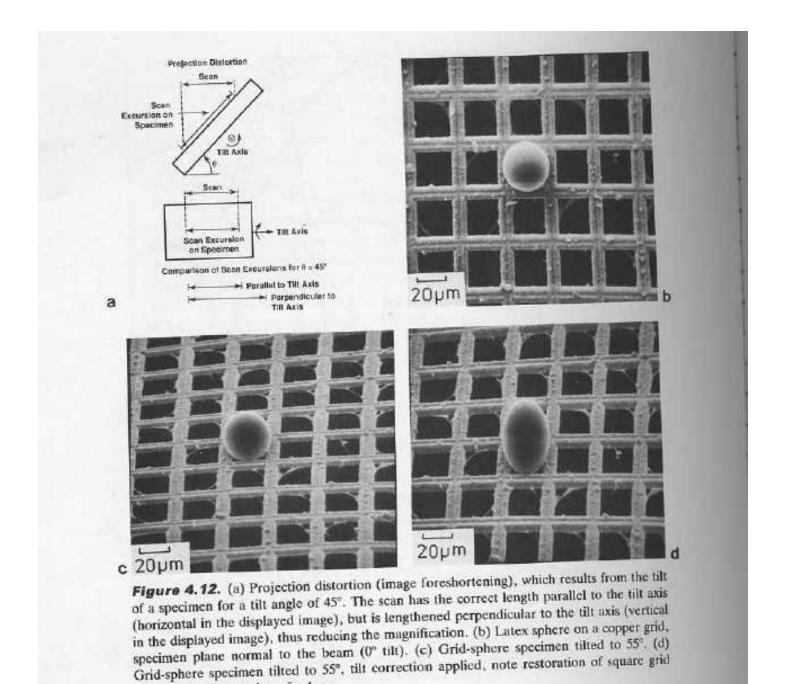


Figure 4.8. Images of a fracture surface illustrating the effects of pixel overlap (hollow magnification). The finest details in the image at low magnification appear sharp, while at the highest magnification, blurring can be observed.



openings, but distortion of sphere.

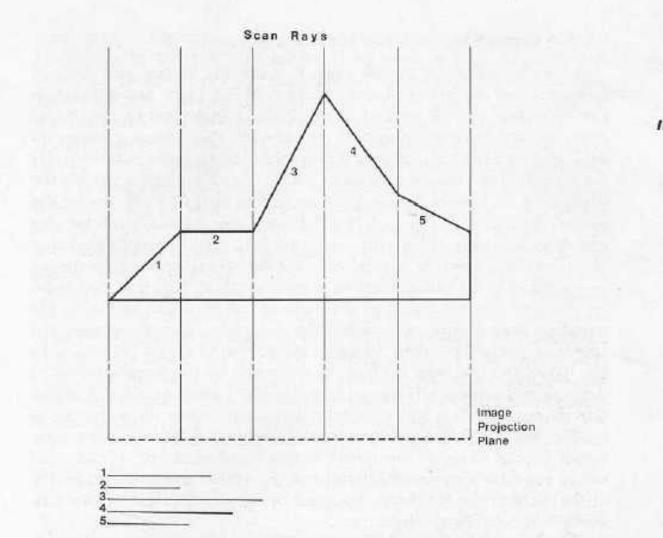
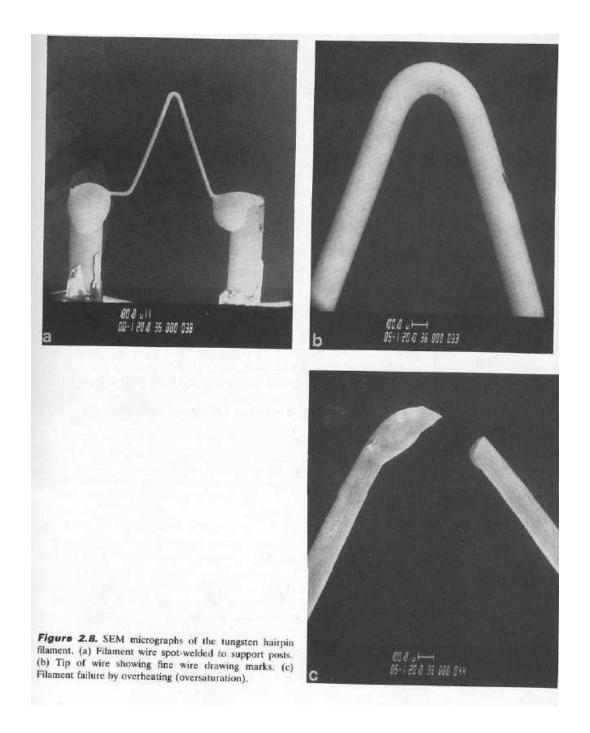


Figure 4.13. Projection distortion of facets with different inclinations to the beam. The magnification is sufficiently high that the scan angle is negligible and the scan rays are nearly parallel to the optic axis. Although the numbered facets have different lengths, their images in projection all have the same apparent length. Below the image projection plane are shown the relative true lengths of the numbered facets.



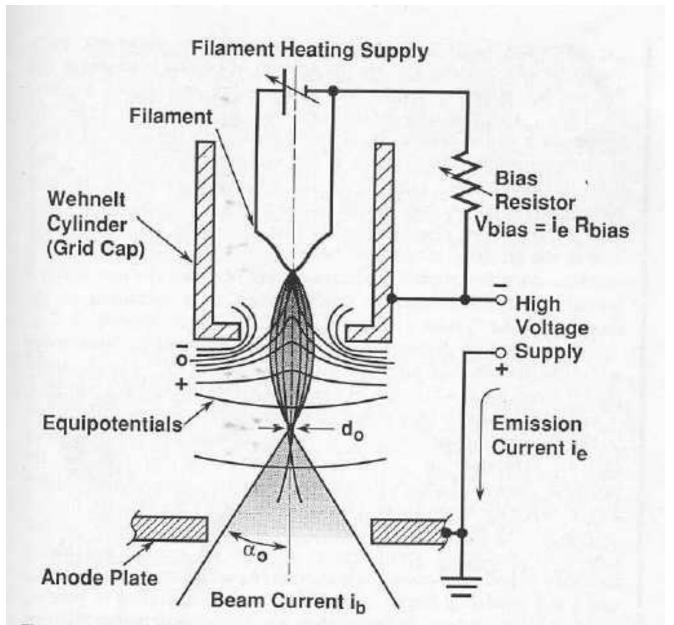


Figure 2.4. Schematic diagram of the conventional self-biased thermionic (triode) electron gun (adapted from Hall, 1966).

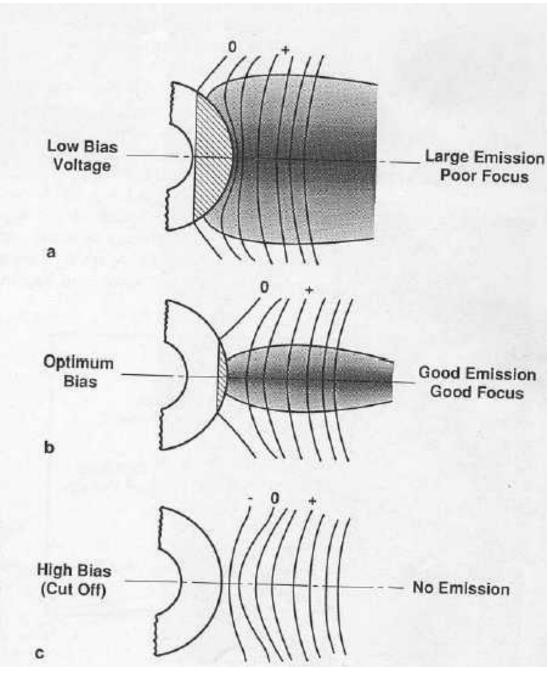


Figure 2.6. Typical emission distributions from the tip of a tungsten hairpin filament for (a) low bias voltage producing high emission but poor focusing, (b) optimum bias voltage producing good focus and good emission, and (c) high bias voltage (cut off) emitting no current (adapted from Haine and Cosslett, 1961).

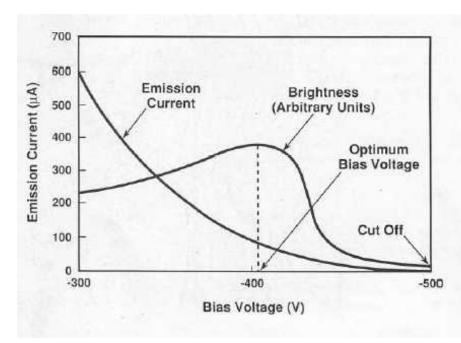


Figure 2.7. Relationship of emission current and brightness to bias voltage. While a brightness maximum should be obtainable in any gun, this schematic diagram shows values and curves for a hypothetical system.

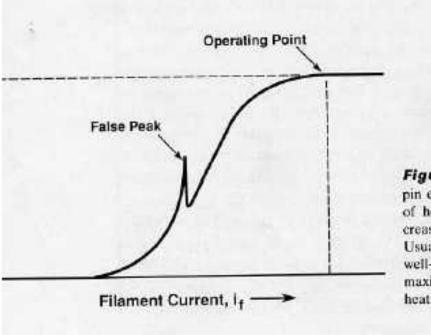


Figure 2.5. Saturation of a tungs pin electron gun. Operating point is of heating current for which no fu crease in beam current can be a Usually a false peak is observed ever well-aligned gun. A misaligned gun maximum emission with increased heating current.

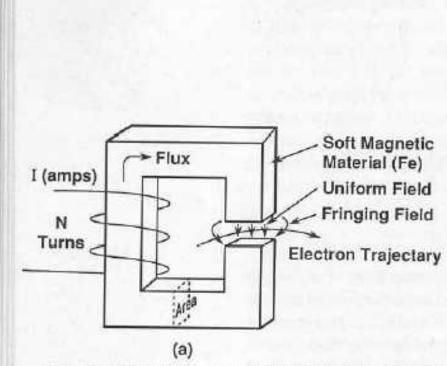
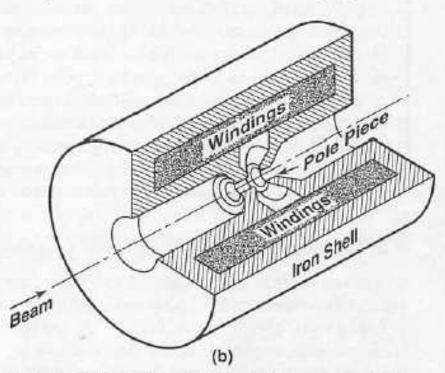
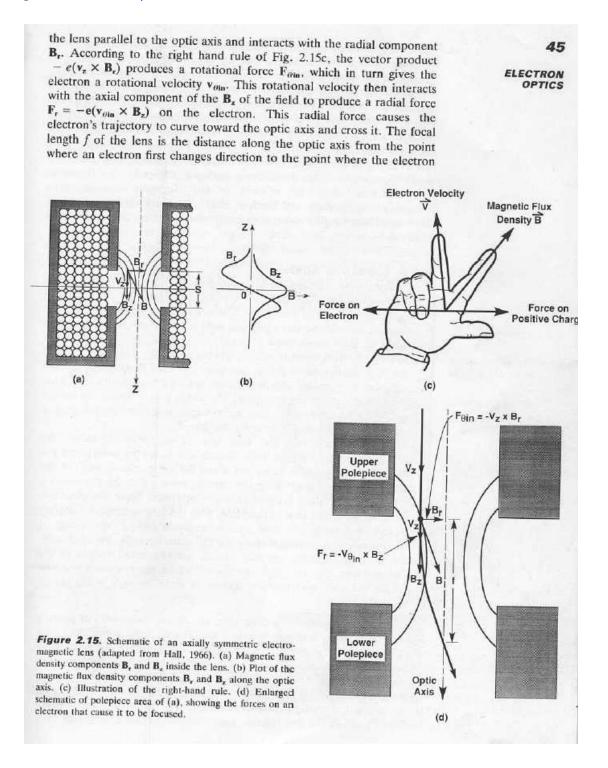


Figure 2.14. Production of a magnetic field inside an electromagnetic lens. (a) A coil of wire energizing a simple magnetic circuit to produce a magnetic field across a gap in the iron circuit. (b) A rotationally symmetric electron lens



where the coil windings are inside the iron shroud and the field is produced across the lens gap between polepieces (adapted from Hall, 1966).



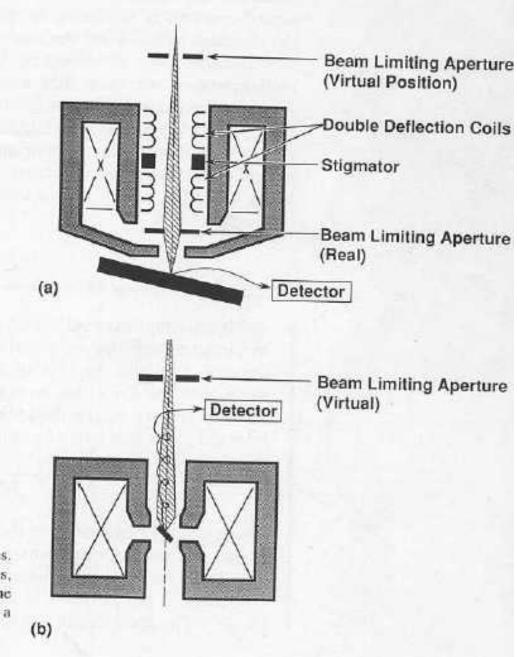


Figure 2.16. Two objective lens configurations.

(a) Asymmetrical pinhole lens or conical lens, allowing a large specimen to be placed outside the lens. (b) Symmetrical immersion lens, where a small specimen is placed inside the lens.

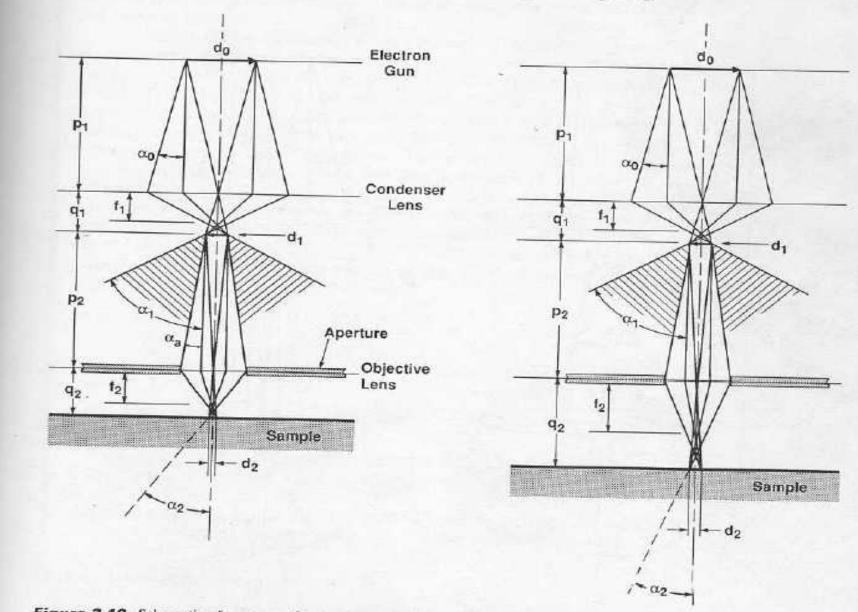


Figure 2.19. Schematic of ray traces for two-lens probe forming system. (a) Small working distance. (b) Large working distance.

#### 52

#### CHAPTER 2

decreases, giving rise to an improved depth of field. To obtain this focusing condition at large W, the objective lens current must be decreased, which in turn increases the focal length  $f_2$  of the lens. This increased working distance also increases the scan length that the beam traverses on the specimen. Thus, long working distances can be used to obtain very low magnifications. Finally, by considering Fig. 2.19, one can understand the alternate method of focusing whereby the working distance is selected by setting the current in the objective lens and the operator physically moves the specimen vertically along the z-axis until it comes into focus on the screen.

Effect of Condenser Lens Strength. Increasing the strength of the condenser lens decreases both the final probe size  $d_p = d_2$  and the amount of current  $i_p$  in the final probe, as shown in Fig. 2.20. With a constant working distance and objective lens aperture size, an increase

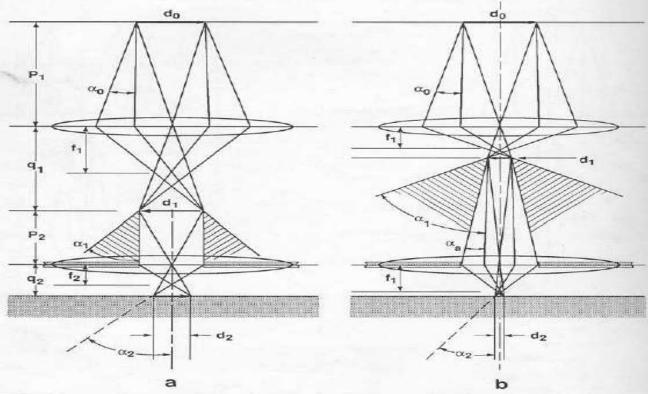


Figure 2.20. Schematic of ray traces for two-lens probe forming system: (a) weak condenser lens, (b) strong condenser lens.

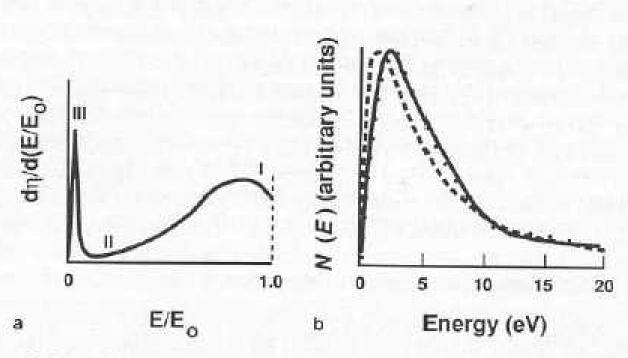
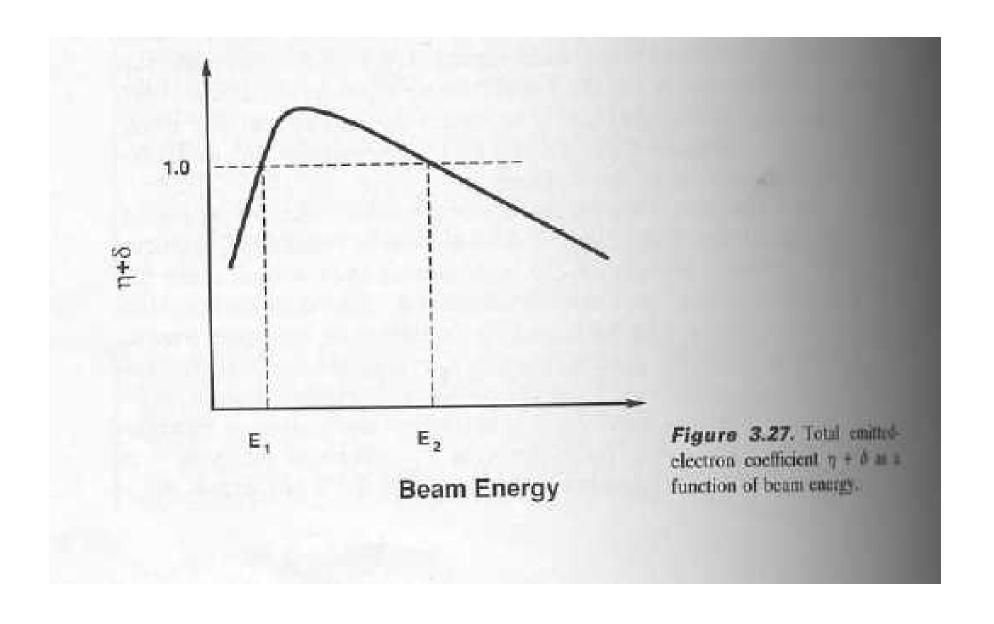


Figure 3.25. (a) Complete energy distribution of electrons emitted from a target, including backscattered electrons (regions I and II) and secondary electrons (region III). Note that the width of region III is exaggerated. (b) Secondary-electron energy distribution as measured (points) and as calculated (lines) with different assumptions on secondary propagation (Koshikawa and Shimizu, 1974).



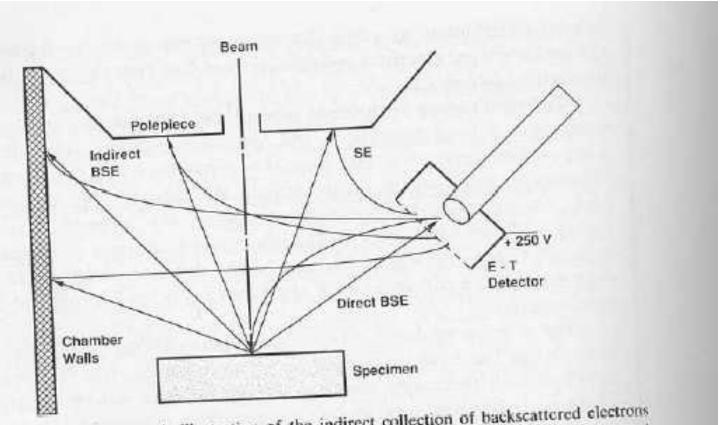
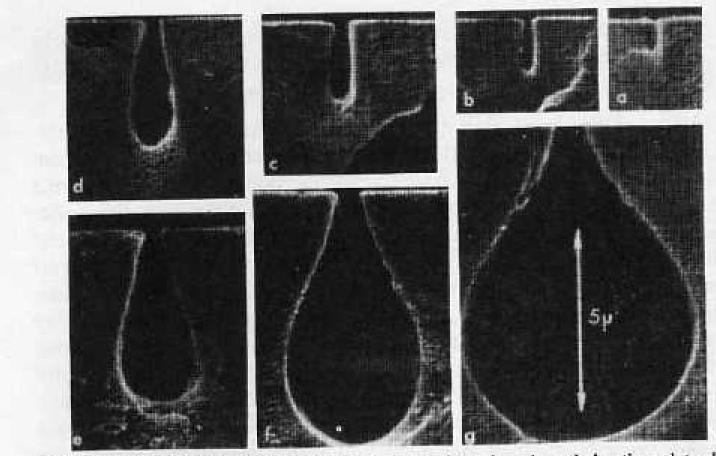
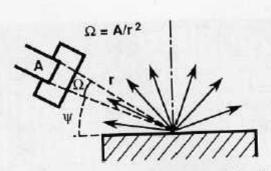


Figure 4.21. Schematic illustration of the indirect collection of backscattered electrons by a positively biased E-T detector. The backscattered electrons strike the polepiece and chamber walls, where they create secondary electrons. These secondaries are collected by the E-T detector with high efficiency. Although nominally a contribution to the secondary electron signal they really represent the backscattered-electron signal component.



**Figure 3.5.** Direct visualization of the electron volume in polymethylmethacrylate. In (a) through (g), the electron dose is the same, but the etching time is increased progressively to reveal successively lower energy deposition (radiation damage) levels (from Everhart et al., 1972).



**Figure 4.17.** General characteristics of detectors. The position of the detector relative to the beam and the specimen is described by the take-off angle,  $\psi$ . The size of the detector is given by the solid angle  $\Omega$ , which is equal to the area of the detector divided by the square of the radial distance to the beam impact point,  $\Omega = A/r^2$ .

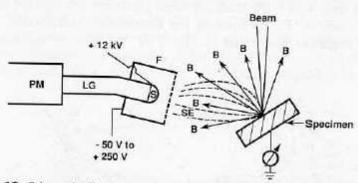


Figure 4.18. Schematic diagram of the Everhart-Thornley detector; B, backscattered-electron trajectories; SE, secondary-electron trajectories; F, Faraday cage (bias range -50 V to +250 V); S, scintillator, with thin metallic coating; high bias (+12 kV) supply to the scintillator coating; LG, light guide; PM, photomultiplier.

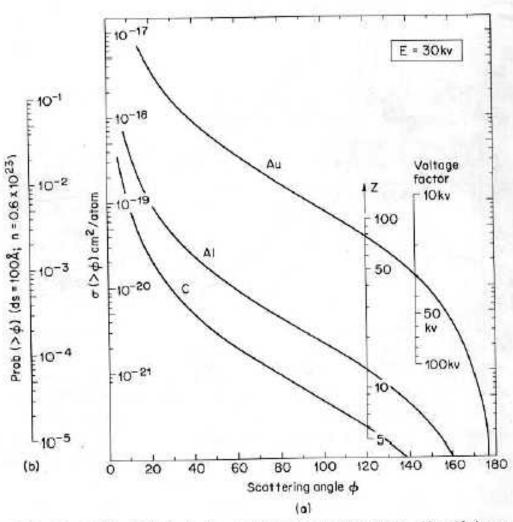


FIG. 3.1 (a) Total Rutherford scattering cross section for C, Al, and Au at 30 kv; (b) probability of a Rutherford scattering event through an angle  $> \phi$  for a path element of length 100 Å.

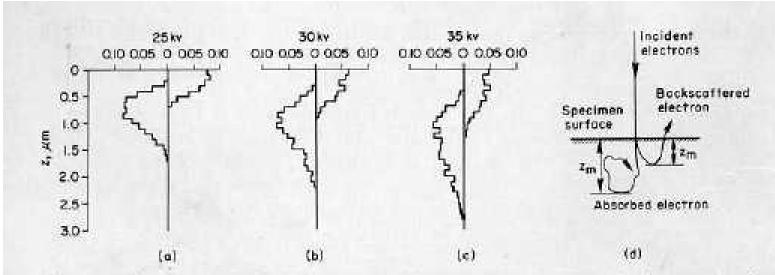
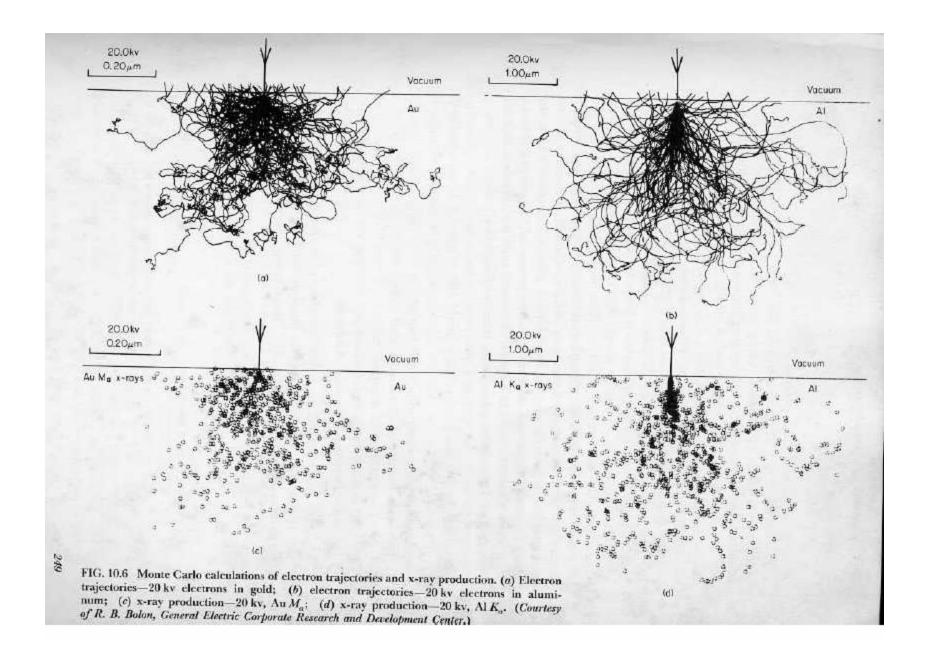


FIG. 3.4 (a), (b), and (c) Distribution of maximum penetration depth for backscattered (right-hand side) and absorbed (left-hand side) electrons in copper specimen as calculated by the Monte Carlo method; (d) definitions of depth. (Shinoda, Kawabe, Murata, and Shirai 1966. Courtesy of Tech. Rep. Osaka Univ.)



MAXIMUM BRIGHTNESS : Jc e Vo [ current density / solid angle ] TRT where Jc = 120 Te = EW/kT Amp cm=2 W- typical: 2700 K, 20 kV -> 105 A/cm ster KANAYA - OKAYAMA RANGE (MM) 20.89 0 Z0.89 0 P= density g cm 3, Z = Aformic No. Tilled Sample: R (0) = Reo Cos 0 (03) Rko at 5 kV = 0.5 0.4 0.14 0.065 20 kV = 5.3 4.2 1.5 0.86

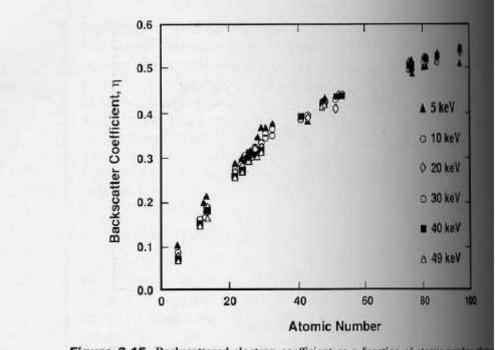
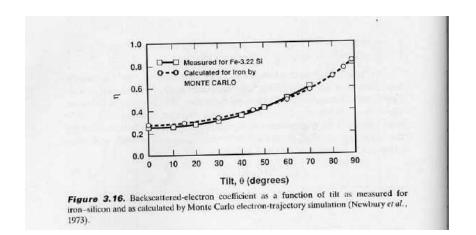
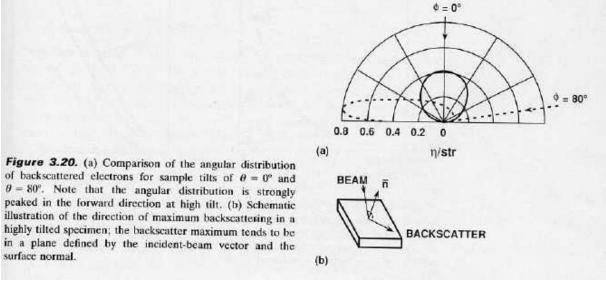
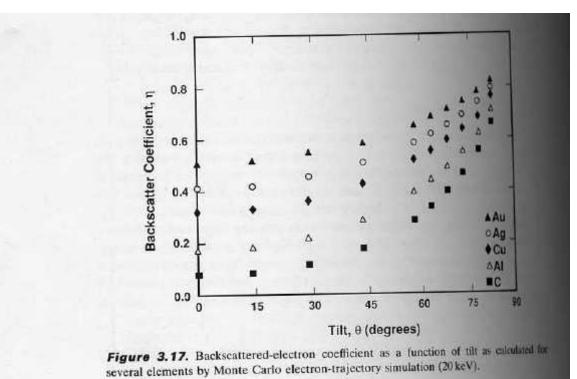
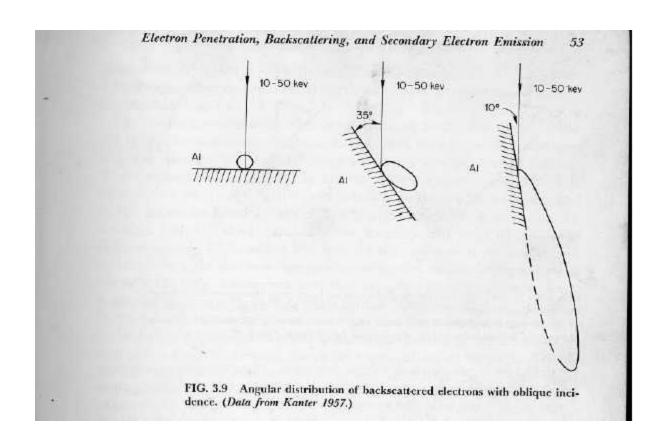


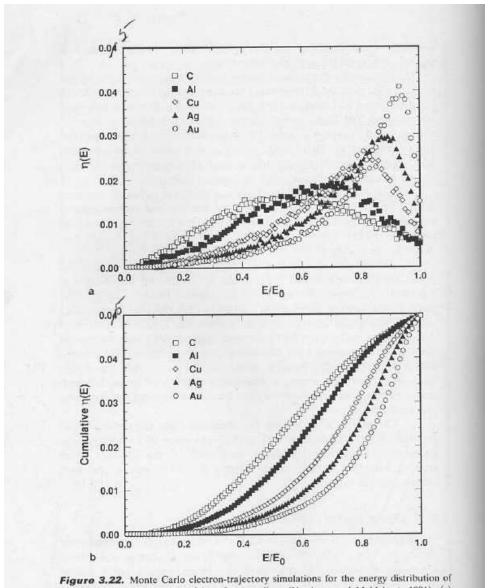
Figure 3.15. Backscattered-electron coefficient as a function of atomic number plan for a range of beam energies from 5 keV to 49 keV [data of Bishop (1966) and Heard (1966a)].











**Figure 3.22.** Monte Carlo electron-trajectory simulations for the energy distribution of backscattered electrons emitted into  $2\pi$  steradians (Newbury and Myklebust, 1991): (a)  $\eta(E)$  vs  $E/E_0$ ; (b) cumulative  $\eta(E)$  distribution.

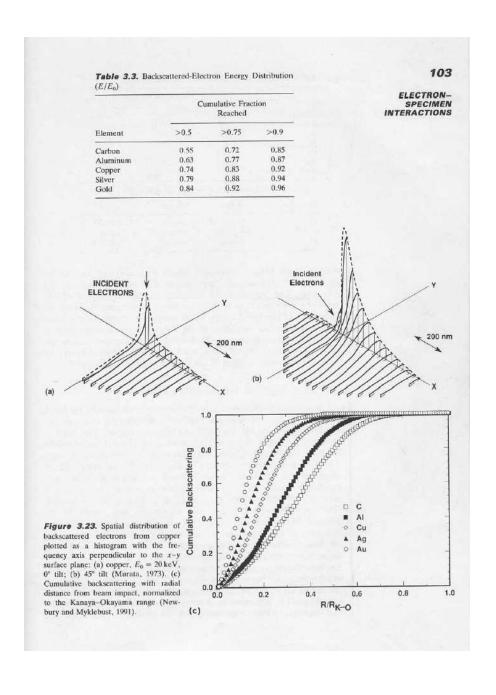
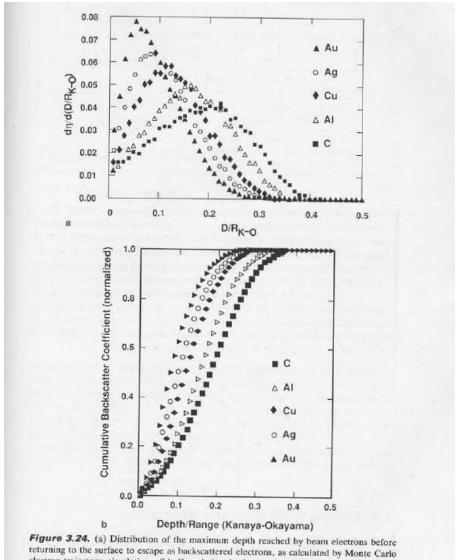
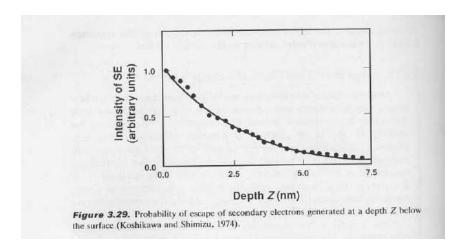


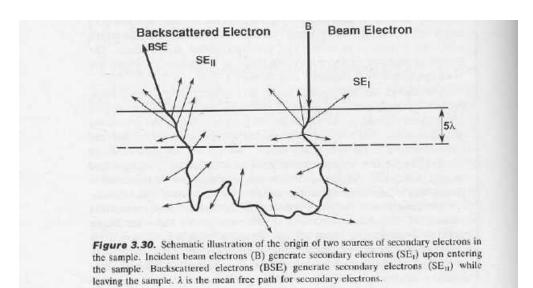
Table 3.4. Cumulative Radial Backscattering (20 keV)

	a. Distribution Fraction				
Element	80%	90%	95%		
С	0.502	0.575	0.63		
Al	0.419	0.490	0.545		
Cu	0.318	0.382	0.439		
Ag	0.250	0.310	0.365		
Au	0.195	0.248	0.295		
	b. Quadratic fit (y	$= M_0 + M_1 Z + M$	$A_2Z^2$ )		
Coefficient	80%	90%	95%		
$M_0$	0.5453	0.6210	0.6745		
$M_2$	-9.535E-3	-9.964E-3	-9.754E-3		
$M_2$	6.494E-5	6.675E-5	6.304E-5		



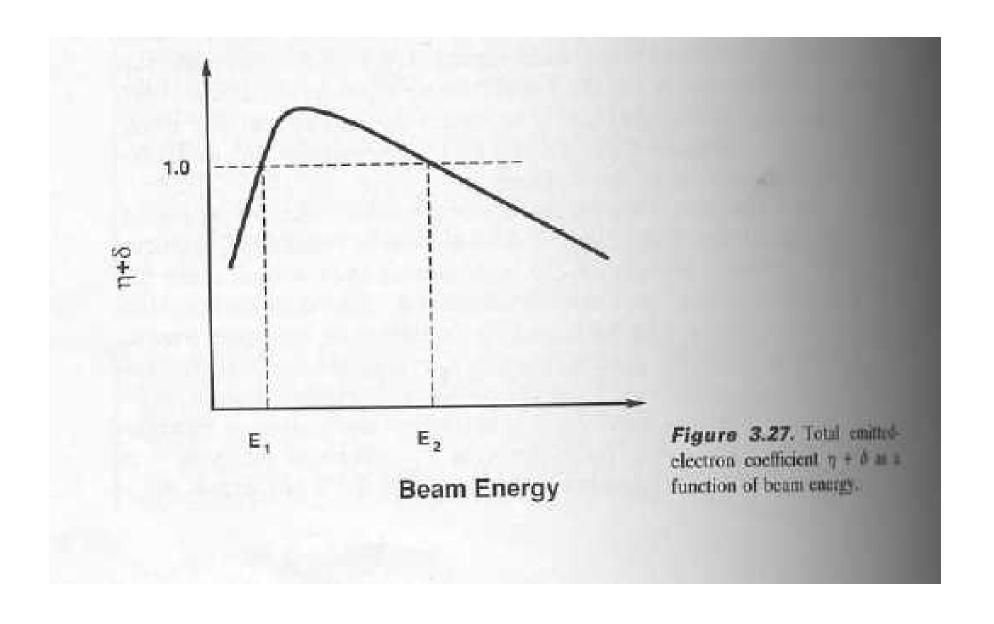
electron-trajectory simulation. (b) Cumulative backscattering as a function of depth, derived from (a) (Newbury and Myklebust, 1991)  $E_0=20\,\mathrm{keV}$ .

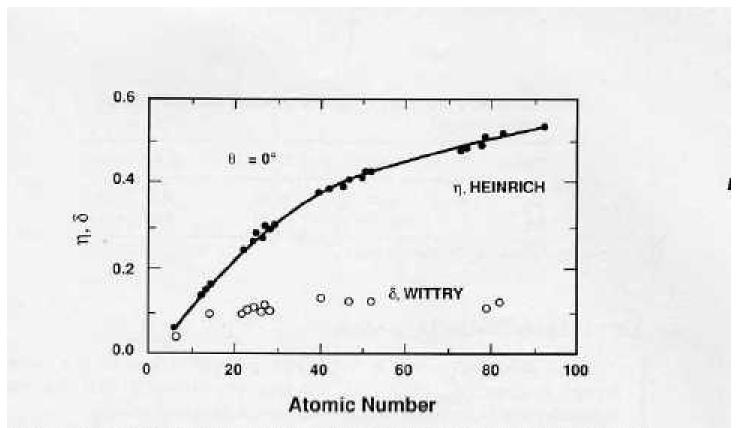




**TABLE 3.8** SE, BSE yields and ratio of SE produced by primary beam to those generated by BSE.

	δ	η	SEII / SEI		
Carbon	0.05	0.06	0.18		
Aluminium	0.1	0.16	0.48		
Copper	0.1	0.30	0.9		
Gold	0.2	0.50	1.5		





**Figure 3.26.** Comparison of backscattered-electron and secondary-electron coefficients as a function of atomic number,  $E_0 = 30 \, \text{keV}$  [data of Wittry (1966) and Heinrich (1966a)].

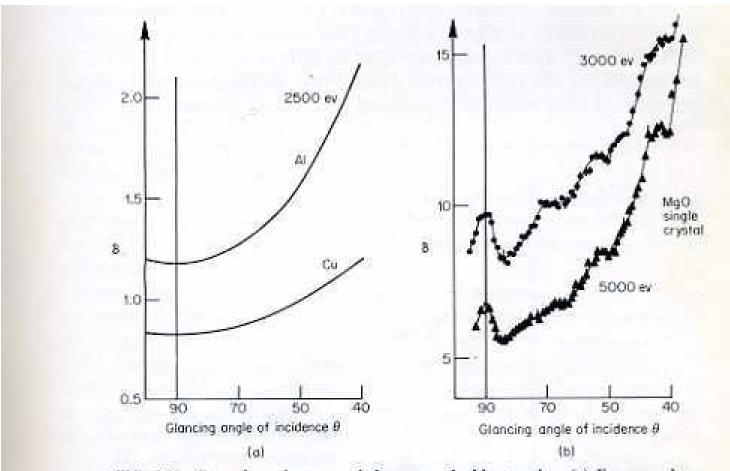


FIG. 3.20 Secondary electron emission versus incident angle. (a) For amorphous metals (Müller 1937. Courtesy of Z. Phys.); (b) for single-crystal MgO. (Laponsky and Whetten 1960. Courtesy of Phys. Rev. Lett.)

## BACKSCATTERED ELECTRON YIELD

 $(\eta)$ 

A SERVICE STATE	
Atomic Number	More or less smooth increase, but $\partial I/\partial z \downarrow$ as $Z \uparrow$
Voltage	Not very sensitive! Range $\uparrow$ as $E_0^{1.7}$ , but stopping power $\downarrow$ as $E_0$ $\uparrow$ , i.e., electrons get in deeper (and therefore have a harder time getting out), but having gone in deeper they can undergo more high angle scattering events and get out. These 2 partly cancel one another. (But remember, that beam intensity as $\uparrow$ voltage $\uparrow$ .
Specimen Tilt	$\eta(\theta)\sim(1+\cos\theta)^{-p}$ , where $P\sim9/Z^{1/2}$ Small $\theta$ (near normal incidence), beam penetrates deep into the sample and path length out of sample is large.
Angular Variation	Path length out of sample, $P=P_0/\cos\phi$ . Probability of not being scattered in $P \sim 1/P$ $\eta_{\phi} = \eta_0 \cos \phi$ If surface is tilted: Scattered electrons are strongly peaked along direction close to incident direction (influence of forward scattering in Rutherford collisions).

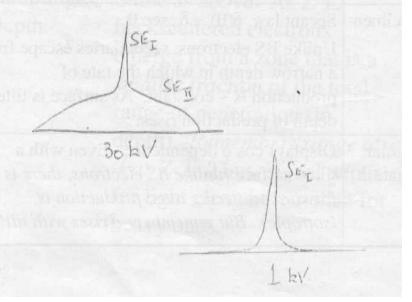
As  $Z^{\uparrow}$ , the fraction of Energy Distrib" backscattered electrons which have lost only a small amount of energy also increases As Z1, backscattered electrons Radial Distance emerge laterally from a zone that is a smaller fraction of the total range of penetration (in depth). Remember: range also ↓ as Z ↑ Same as above. As  $Z \uparrow$ , Sampling Depth backscattered electrons emerge from a zone that is a smaller fraction of the total range of penetration (in depth). Remember: range also  $\sqrt{as} Z \uparrow$ . Thus, signal depth for light elements >> than for heavy ones.

## SECONDARY ELECTRON YIELD (δ)

Atomic Number	Insensitive to Z! (Possibly due to the high surface sensitivity and contamination in an SEM vacuum)							
Voltage	$\delta \uparrow$ as $E_0 \downarrow$							
		Element   ↓	kV →	5	20	50		
		Aluminium		0.4	0.1	0.05		
		Gold		0.7	0.2	0.1		
Specimen Tilt	Secant law, $\delta(\theta) \sim \delta_0$ sec $\theta$ Unlike BS electrons, secondaries escape from a narrow depth in which the rate of production is $\sim$ constant. As surface is tilted, depth of production rises.							
Angular Variation	Displays cos φ dependence. Even with a tilted surface (unlike BS electrons, there is no forward scattering bias; production is isotropic). But remember: δ rises with tilt!							

## LOW VOLTAGE MICROSCOPY

- Backscatter yield can increase for low Z at < 5 kV</li>
- Secondary yield can go beyond unity for insulators and bad conductors. Charging eliminated
- Lateral resolution improves due to reduced backscattering-induced secondaries
- Depth resolution improves substantially due to reduced range. Backscatter and secondary ranges become comparable
- Sensitivity to topography increases substantially
- Beam current drops!! Poor signal! Cannot use W-sources below ~ 5 kV. Need field emission cathodes



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FIG. 6.16 Increase in image contrasts obtained by reducing the accelerating potential. Hydrogen embrittlement crack surface, 18% Ni (250 grade) maraging steel, examined at (a) 5 kv; (b) 20 kv. (Pickwick and Smith 1972. Courtesy of Micron.)

127

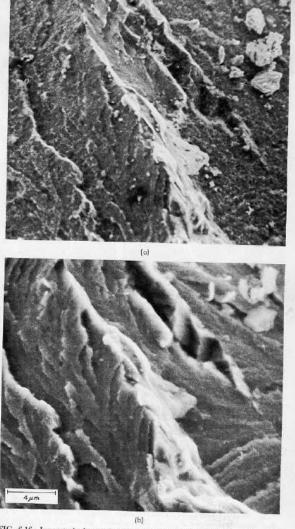
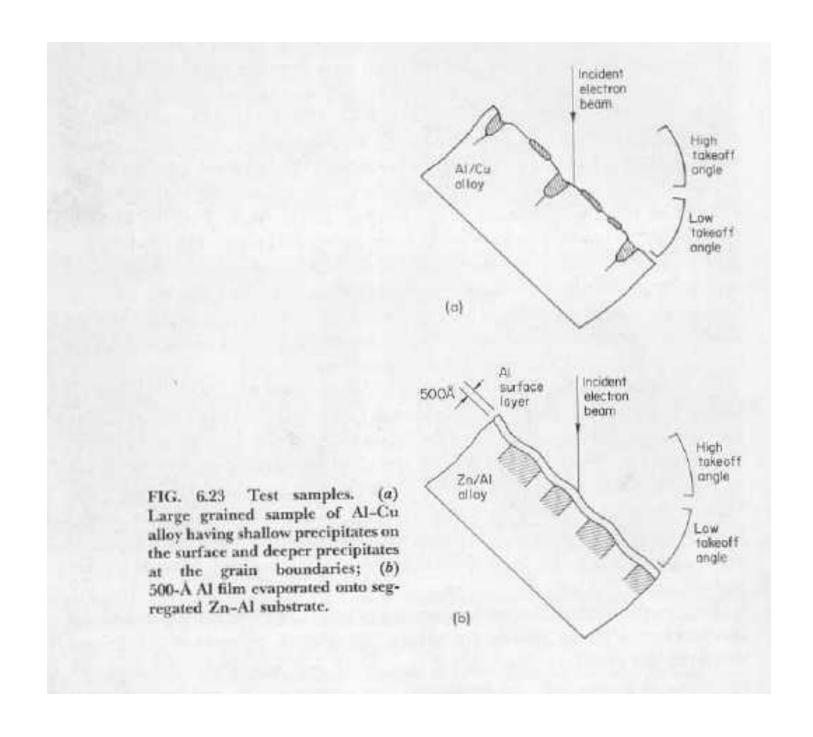
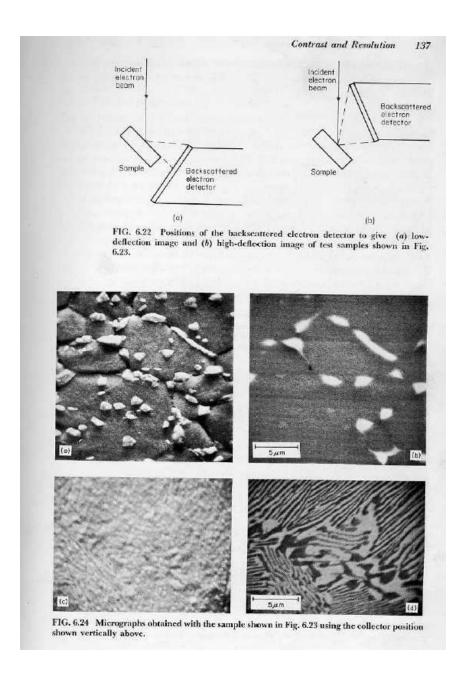


FIG. 6.16 Increase in image contrasts obtained by reducing the accelerating potential. Hydrogen embrittlement crack surface, 18% Ni (250 grade) maraging steel, examined at (a) 5 kv; (b) 20 kv. (Pickwick and Smith 1972. Courtey of Micron.)

127





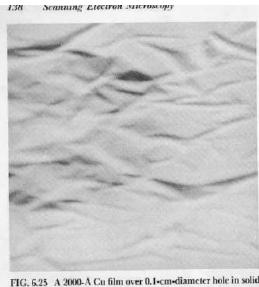


FIG. 5.25 A 2000-A Cu film over 0.1-cm-diameter hole in solid substrate imaged using solid-state backscattered electron detector with low takeoff angle  $(\theta=45^\circ;\theta'=25^\circ)$ . (R. Shimizu and T. Matsukawa unpublished, Dept. of Physics, Osaka Univ.)

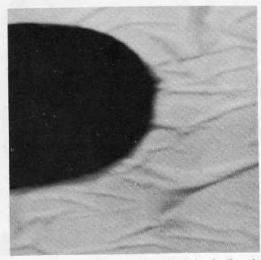


FIG. 6.26 Same as Fig. 6.25 but with high takeoff angle ( $\theta=45^\circ;\,\theta'=90^\circ$ ).

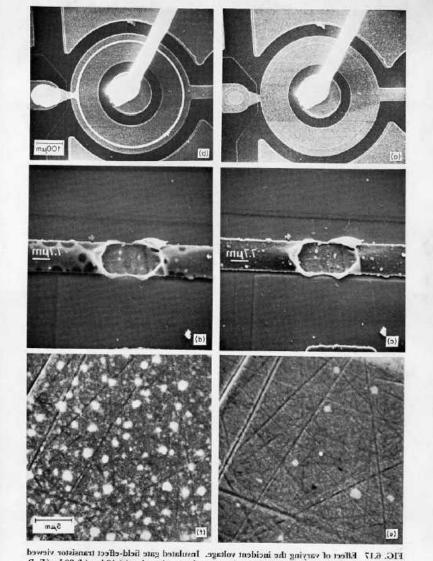


FIG. 6.17 Effect of varying the incident voltage. Insulated gate field-effect transistor viewed at (a) 10 kv; (b) 20 kv. Also, failed aluminum conductor viewed at (c) 10 kv; (d) 20 kv (E. D. Wolf, unpublished, Hughes Res. Lab, Malibu, Calif.), (e) and (f) Al-Cu alloy with precipitates examined at 5 kv and 25 kv (secondary electron image with normal incidence). (P. Beaufrer et al. unpublished, IBM Essonnes Plant, France.)

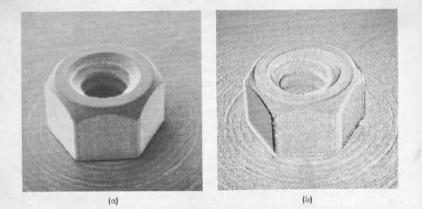
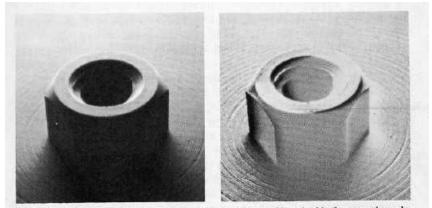
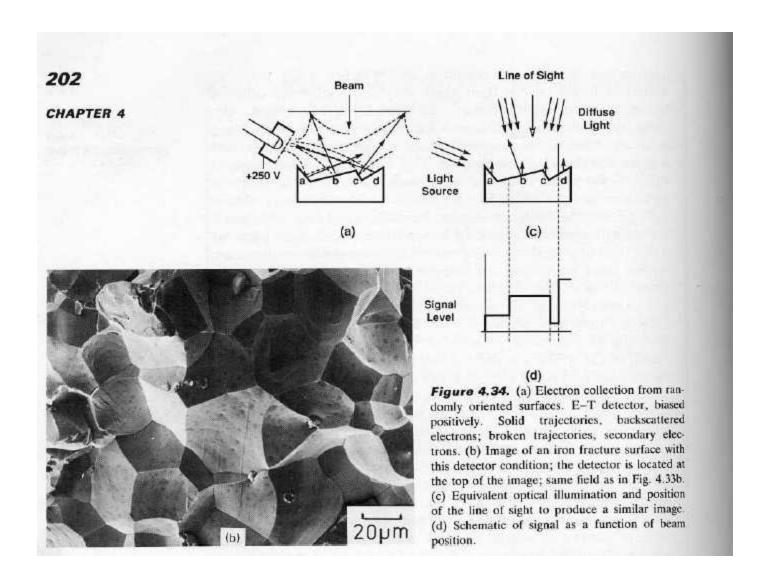
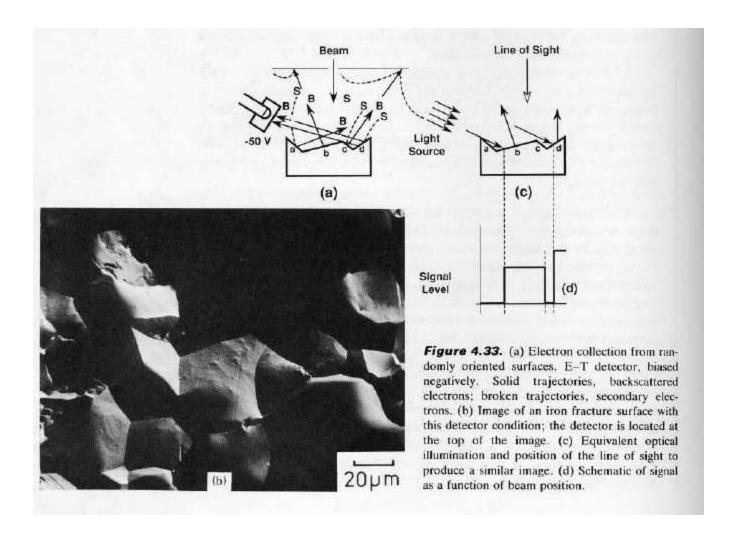


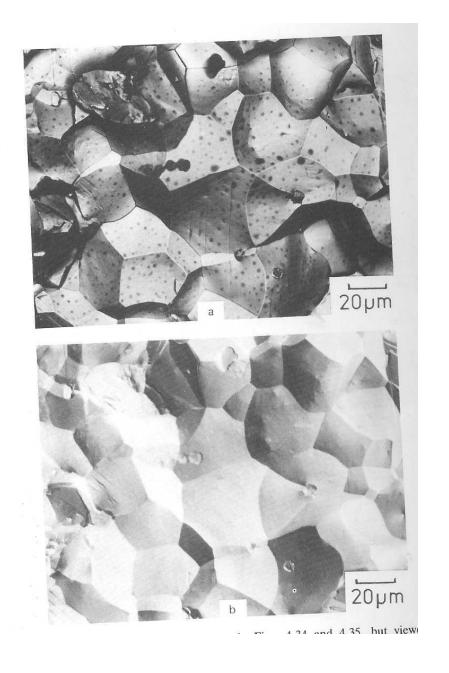
FIG. 6.1 Secondary electron images of 00-90 brass nut. (a) Usual display method; (b) with the video waveform differentiated (horizontal scan). Distances between flats = 1.95 mm. All the images in this chapter were obtained by collecting the secondary electrons unless stated otherwise.

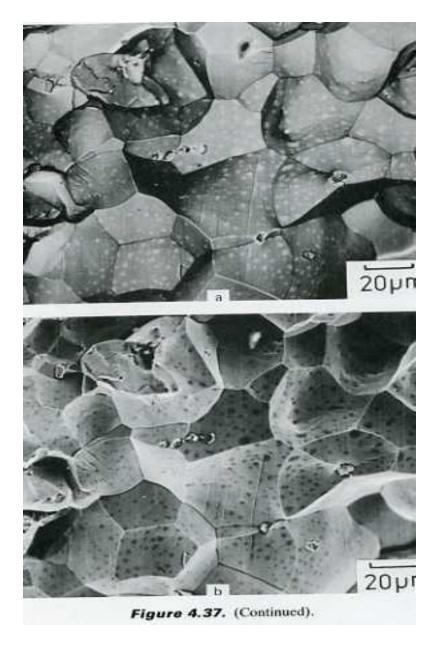


 $FIG.\ 6.2$  As Fig. 6.1 but the backscattered electron image. Note the blank areas where the surface is shielded from the collector.









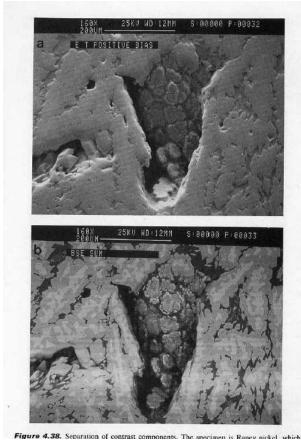


Figure 4.38. Separation of contrast components. The specimen is Raney nickel, which contains multiple phases that produce atomic number contrast and surface defects that produce topographic contrast. (a) The specimen is viewed with a positively biased E-T detector, showing predominantly topographic contrast. (b) Four-quadrant solid-state BSE detector, sum mode: atomic number contrast dominates the image. (c) Difference mode, TOP - BOTTOM: topographic contrast dominates, with apparent top illumination. (d) Difference mode, BOTTOM - TOP: topographic contrast dominates, with apparent bottom illumination. (c) Difference mode, RIGHT - LEFT: topographic contrast dominates, with apparent illumination from the right. (f) Difference mode, LEFT - RIGHT: topographic contrast dominates, with apparent illumination from the left.

