## Chapter 13

13.1 — 13.4 
$$K_o = (1 - \sin \phi')(OCR)^{\sin \phi'}$$

Problem	φ' (deg)	$K_o$	$P_o = \frac{1}{2} K_o \gamma H^2$	$\bar{z} = \frac{H}{3}$
13.1	38	0.676	281.55 kN/m	2.33 m
13.2	32	0.679	8,402.6 lb/ft	5 ft
13.3	35	0.635	205.7 kN/m	2 m
13.4	30	0.5	10,500.0 lb/ft	6.67 ft

13.5 — 13.8 
$$K_a = \tan^2(45 - \phi'/2)$$

Prob.	φ' (deg)	$K_a$	$\sigma'_{a(z=H)} = K_a \gamma H$	$P_a = \frac{1}{2} K_a \gamma H^2$	$\overline{z} = \frac{H}{3}$
13.5	30	0.333	(0.333)(105)(15) = <b>524.5</b> lb/ft <sup>2</sup>	$\frac{1}{2}(0.333)(105)(15)^2$ = <b>3933.6 lb/ft</b>	5 ft
13.6	32	0.307	(0.307)(100)(18) = <b>552.6 lb/ft</b> <sup>2</sup>	$\frac{1}{2}(0.307)(100)(18)^2$ = <b>4973.4 lb/ft</b>	6 ft
13.7	36	0.26	$(0.26)(18)(4) = 18.72 \text{ kN/m}^2$	$\frac{1}{2}(0.26)(18)(4)^2$ = <b>37.44 kN/m</b>	1.33 m
13.8	40	0.217	(0.217)(17)(5) = <b>18.45</b> kN/m <sup>2</sup>	$\frac{1}{2}(0.217)(17)(5)^2$ = <b>46.11 kN/m</b>	1.67 m

Note: 1. Pressure distribution is similar to that shown in Figure 13.13a., i.e.,  $\sigma'_a = 0$  at z = 0 and  $\sigma'_a = K_a \gamma H$  at z = H.

2.  $\overline{z}$  = distance measured from the bottom of the wall.

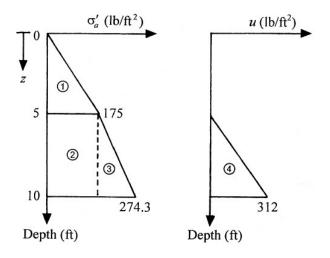
13.9 — 13.12 
$$K_p = \tan^2(45 + \phi'/2)$$

Prob.	φ' (deg)	K <sub>a</sub>	$\sigma'_{a(z=H)} = K_a \gamma H$	$P_a = \frac{1}{2} K_a \gamma H^2$	$\bar{z} = \frac{H}{3}$
13.9	34	3.537	(3.537)(110)(8) = <b>3112.6 lb/ft</b> <sup>2</sup>	$\begin{array}{c} \frac{1}{2}(3.537)(\ 110)(8)^2 \\ = 12,450 \ \mathbf{lb/ft} \end{array}$	2.67 ft
13.10	36	3.852	(3.852)(105)(10) = <b>4044.6</b> lb/ft <sup>2</sup>	$\frac{1}{2}(3.852)(105)(10)^2$ = <b>20,223 lb/ft</b>	3.33 ft
13.11	35	3.69	(3.69)(14)(5) = 258.3 kN/m <sup>2</sup>	$\frac{1}{2}(3.69)(14)(5)^2$ = <b>645.8 kN/m</b>	1.67 m
13.12	30	3	$(3)(15)(4) = 1890 \text{kN/m}^2$	$\frac{1}{2}(3)(15)(4)^2$ = <b>360 kN/m</b>	1.33 m

*Note*: 1.  $\sigma'_{p(z=0)} = 0$ ; triangular pressure distribution.

2.  $\overline{z}$  = distance measured from the bottom of the wall.

13.13 
$$K_a = \tan^2\left(45 - \frac{\phi'}{2}\right) = \tan^2\left(45 - \frac{30}{2}\right) = \frac{1}{3}$$
. Refer to the figure.



$$z = 0$$
 ft:  $\sigma'_a = \sigma'_a K_a = 0$ ;  $u = 0$   
 $z = 5$  ft:  $\sigma'_a = (105)(5)(\frac{1}{3}) = 175 \text{ lb/ft}^2$ ;  $u = 0$   
 $z = 10$  ft:  $\sigma'_a = [(105)(5) + (122 - 62.4)(5)](\frac{1}{3}) = 274.3 \text{ lb/ft}^2$   
 $u = (62.4)(5) = 312 \text{ lb/ft}^2$ 

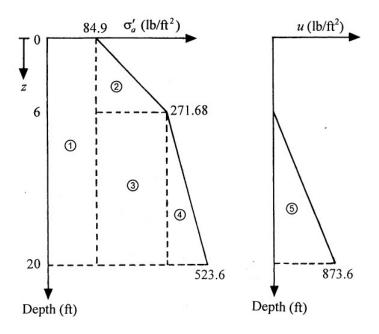
Area No.	Area
1	$(\frac{1}{2})(5)(175) = 437.5$
2	(175)(5) = 875.0
3	$(\frac{1}{2})(5)(274.3 - 175) = 248.3$
4	$(\frac{1}{2})(5)(312) = 780.0$
	D - 52 240 8 lb/ft

 $P_a = \Sigma 2,340.8$  lb/ft

Resultant: Taking the moment about the bottom of the wall,

$$\overline{z} = \frac{\left[ (437.5)\left(5 + \frac{5}{3}\right) + (875)\left(\frac{5}{2}\right) + (248.3)\left(\frac{5}{3}\right) + (780)\left(\frac{5}{3}\right) \right]}{2340.8}$$
$$= \frac{2916.7 + 2187.5 + 413.8 + 1300}{2340.8} = 2.91 ft$$

13.14  $K_a = \tan^2\left(45 - \frac{34}{2}\right) = 0.283$ . Refer to the figure.



$$z = 0$$
 ft:  $\sigma'_a = \sigma'_a K_a = (300)(0.283) = 84.9 \text{ lb/ft}^2$ ;  $u = 0$   
 $z = 6$  ft:  $\sigma'_a = [300 + (6)(110)](0.283) = 271.68 \text{ lb/ft}^2$ ;  $u = 0$   
 $z = 20$  ft:  $\sigma'_a = [300 + (6)(110) + (126 - 62.4)(14)](0.283) = 523.66 \text{ lb/ft}^2$   
 $u = (62.4)(14) = 873.6 \text{ lb/ft}^2$ 

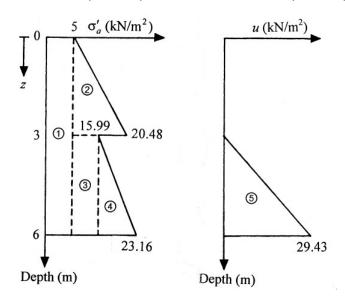
Area No.	Area
1	(84.9)(20) = 1,698.00
2	$(\frac{1}{2})(6)(271.68 - 84.9) = 560.34$
3	(14)(271.68 - 84.9) = 2,614.92
4	$(\frac{1}{2})(14)(523.6 - 271.68) = 1,763.44$
5	$(\frac{1}{2})(14)(873.6) = 6,115.20$
	$P_a = \Sigma 12,751.90 \text{ lb/ft}$

Location of resultant: Taking the moment about the bottom of the wall,

$$\bar{z} = \frac{\left[ (1,698) \left( \frac{20}{2} \right) + (560.34) \left( 14 + \frac{6}{3} \right) + (2,614.92) \left( \frac{14}{2} \right) \right] + (1,763.44) \left( \frac{14}{3} \right) + (6,115.2) \left( \frac{14}{3} \right)}{12,751.9}$$

$$= \frac{16,980 + 8,965.44 + 18,304.44 + 8,229.4 + 28,573.6}{12,751.9} = 6.35$$

13.15 
$$K_{a(1)} = \tan^2\left(45 - \frac{30}{2}\right) = 0.333$$
;  $K_{a(2)} = \tan^2\left(45 - \frac{36}{2}\right) = 0.26$ . Refer to the figure.



$$z = 0 \text{ m}$$
:  $\sigma'_a = \sigma'_a K_{a(1)} = (15)(0.333) = 5 \text{ kN/m}^2; \ u = 0$   
 $z = 3 \text{ m}$ :  $\sigma'_a = \sigma'_a K_{a(1)} = [(15.5)(3) + 15](0.333) = 20.48 \text{ kN/m}^2$   
 $\sigma'_a = \sigma'_a K_{a(2)} = [(15.5)(3) + 15](0.26) = 15.99 \text{ kN/m}^2$   
 $u = 0$   
 $z = 6 \text{ m}$ :  $\sigma'_a = \sigma'_a K_{a(2)} = [(15.5)(3) + (19 - 9.81)(3)](0.26) = 23.16 \text{ kN/m}^2$   
 $u = (9.81)(3) = 29.43 \text{ kN/m}^2$ 

Area No.	Area
1	(6)(5) = 30.00
2	$(\frac{1}{2})(3)(20.48 - 5) = 23.22$
3	(3)(15.99 - 5) = 32.97
4	$(\frac{1}{2})(3)(23.16 - 15.99) = 10.76$
5	$(\frac{1}{2})(3)(29.43) = 44.15$
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 $P_a = \Sigma 141.10 \text{ kN/m}$ 

**Location of resultant:** Taking the moment about the bottom of the wall,

$$\overline{z} = \frac{\left[ (30) \left( \frac{6}{2} \right) + (23.22) \left( 3 + \frac{3}{3} \right) + (32.97) \left( \frac{3}{2} \right) + (10.76) \left( \frac{3}{3} \right) + (44.15) \left( \frac{3}{3} \right) \right]}{141.1}$$

$$= \frac{90 + 92.88 + 49.46 + 10.76 + 44.15}{141.1} = \frac{287.25}{141.1} = 2.04 m$$

13.16 a. Eq. (13.23): 
$$\sigma_a' = \frac{\gamma z \cos \alpha \sqrt{1 + \sin^2 \phi' - 2 \sin \phi' \cos \psi_a}}{\cos \alpha + \sqrt{\sin^2 \phi' - \sin^2 \alpha}}$$

$$\psi_a = \sin^{-1} \left( \frac{\sin \alpha}{\sin \phi'} \right) - \alpha + 2\theta = \sin^{-1} \left( \frac{\sin 15}{\sin 35} \right) - 15 + (2)(10) = 31.82^{\circ}$$

$$\sigma_a' = \frac{(15)(5)(\cos 15)\sqrt{1 + \sin^2(35) - (2)(\sin 35)(\cos 31.82)}}{\cos 15 + \sqrt{\sin^2 35 - \sin^2 15}} = 29.18 \text{ kN/m}^2$$

Eq. (13.25):

$$\beta = \tan^{-1} \left( \frac{\sin \phi' \sin \psi_a}{1 - \sin \phi' \cos \psi_a} \right) = \tan^{-1} \left[ \frac{(\sin 35)(\sin 31.28)}{1 - (\sin 35)(\cos 31.28)} \right] = 30.54^{\circ}$$

b. Eq. (13.27):

$$K_{a(R)} = \frac{\cos(\alpha - \theta)\sqrt{1 + \sin^2 \phi' - 2\sin \phi' \cos \psi_a}}{\cos^2 \theta \left(\cos \alpha + \sqrt{\sin^2 \phi' - \sin^2 \alpha}\right)}$$

$$= \frac{\cos(15 - 10)\sqrt{1 + \sin^2 35 - (2)(\sin 35)(\cos 31.82)}}{\cos^2 10 \left(\cos 15 + \sqrt{\sin^2 35 - \sin^2 10}\right)} = 0.4137$$

$$P_a = \frac{1}{2}\gamma H^2 K_{a(R)} = \frac{1}{2}(15)(5)^2(0.4137) = 77.57 \text{ kN/m}$$

Location and Direction of Resultant: At a distance of H/3 = 5/3 = 1.67 m above the bottom of the wall inclined at an angle  $\beta = 30.54^{\circ}$  to the normal drawn to the back face of the wall

13.17 This is a Rankine case, since  $\delta' = 0$ .  $P_p = \frac{1}{2} \gamma H^2 K_{p(R)}$ .

Eq. (13.33): 
$$K_{p(R)} = \frac{\cos(\alpha - \theta)\sqrt{1 + \sin^2 \phi' + 2\sin \phi' \cos \psi_p}}{\cos^2 \theta \left(\cos \alpha - \sqrt{\sin^2 \phi' - \sin^2 \alpha}\right)}$$

$$\alpha=0;\,\theta=10^{\rm o};\ \phi'=30^{\rm o}$$

$$\psi_p = \sin^{-1} \left( \frac{\sin \alpha}{\sin \phi'} \right) + \alpha - 2\theta = \sin^{-1} \left( \frac{\sin 0}{\sin 30} \right) + 0 - (2)(10) = -20^{\circ}$$

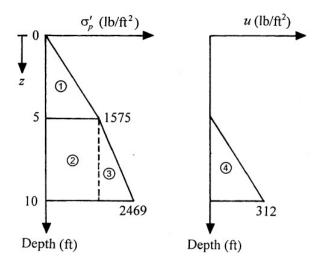
$$P_p = \frac{1}{2}(16.5)(4)^2(3.05) = 402.6 \text{ kN/m}$$

Eq. (13.32):

$$\beta = \tan^{-1} \left( \frac{\sin \phi' \sin \psi_p}{1 + \sin \phi' \cos \psi_p} \right) = \tan^{-1} \left\{ \frac{(\sin 30)[\sin(-20)]}{1 + (\sin 30)[\cos(-20)]} \right\} = -6.64^{\circ}$$

 $P_p$  acts at a distance of H/3 = 4/3 = 1.33 m from the bottom of the wall inclined at an angle  $\beta = -6.64^{\circ}$  to the normal drawn to the back face of the wall.

13.18 
$$K_p = \tan^2\left(45 + \frac{30}{2}\right) = 3$$
. Refer to the figure.



$$z = 0$$
 ft:  $\sigma'_{p} = 0$ ;  $u = 0$   
 $z = 5$  ft:  $\sigma'_{p} = \gamma_{1} z K_{p} = (105)(5)(3) = 1575 \text{ lb/ft}^{2}$ ;  $u = 0$   
 $z = 10$  ft:  $\sigma'_{p} = [(105)(5) + (122 - 62.4)(5)](3) = 2469 \text{ lb/ft}^{2}$   
 $u = (62.4)(5) = 312 \text{ lb/ft}^{2}$ 

Area No.	Area	
1	$(\frac{1}{2})(5)(1575) = 3,937.5$	
2	(5)(1575) = 7,875.0	
3	$(\frac{1}{2})(5)(2469 - 1575) = 2,235.0$	
4	$(\frac{1}{2})(5)(312) = 780.0$	
	D 714 010 A	h/ft

 $P_a = \Sigma 14,828.0$  lb/ft

Location of the resultant: Taking the moment about the bottom of the wall,

$$\overline{z} = \frac{\left[ (3937.5) \left( 5 + \frac{5}{3} \right) + (7875) \left( \frac{5}{2} \right) + (2235) \left( \frac{5}{3} \right) + (780) \left( \frac{5}{3} \right) \right]}{14,828} = \mathbf{3.44 ft}$$

13.19 a. 
$$H = 15$$
 ft;  $c_u = 350$  lb/ft<sup>2</sup>;  $\gamma = 122$  lb/ft<sup>2</sup>;  $\phi = 0$ 

$$K_a = \tan^2\left(45 - \frac{\phi}{2}\right) = 1; \sigma'_a = \gamma z - 2c_u$$

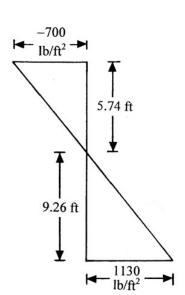
At the top (z = 0 ft):

$$\sigma_a' = -2c_u = (-2)(350)$$
$$= -700 \,\text{lb/ft}^2$$

At the bottom (z = 15 ft):

$$\sigma'_a = (122)(15) - (2)(350)$$
  
= 1830 - 700 = 1130 lb/ft<sup>2</sup>

The pressure diagram is shown.



b. Eq. (13.49): 
$$z_o = \frac{2c_u}{\gamma} = \frac{(2)(350)}{122} =$$
**5.74 ft**

c. Eq. (13.51): 
$$P_a = \frac{1}{2}\gamma H^2 - 2c_u H = \frac{1}{2}(122)(15)^2 - (2)(350)(15) = 3225 \text{ lb/ft}$$

d. Eq. (13.53):

$$P_a = \frac{1}{2}\gamma H^2 - 2c_u H + \frac{2c_u^2}{\gamma}$$
$$= \frac{1}{2}(122)(15)^2 - (2)(350)(15) + \frac{(2)(350)^2}{122} = 5233 \text{ lb/ft}$$

Resultant measured from the bottom:  $\bar{z} = \frac{H - z_o}{3} = \frac{15 - 5.74}{3} = 3.09 \text{ ft}$ 

13.20 a. 
$$\sigma_a = \sigma_o K_a - 2c\sqrt{K_a}$$

$$\sigma_o = \gamma z + q$$
;  $K_a = 1$ .

At 
$$z = 0$$
 ft:

$$\sigma_o = 200 \text{ lb/ft}^2$$

$$\sigma_a = 200 - (2)(350)$$

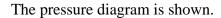
$$= -500 \, lb/ft^2$$

At 
$$z = 15$$
 ft:

$$\sigma_o = (122)(15) + 200$$

$$= 2030 \text{ lb/ft}^2$$

$$\sigma_a = 2030 - (2)(350) = 1330 \,\text{lb/ft}^2$$



b. 
$$\sigma_a = 0$$
;  $(\gamma z_o + q) - 2c = 0$ 

$$z_o = \frac{2c_u - q}{\gamma} = \frac{700 - 200}{122} = 4.1 \, \text{ft}$$

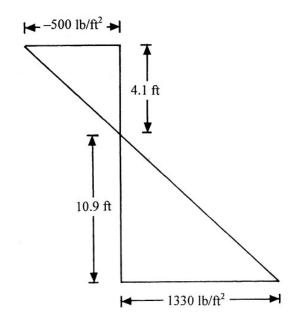
c. Referring to the diagram in Part a,

$$P_a = \frac{1}{2}(10.9)(1330) - \frac{1}{2}(500)(4.1) = 6223.5 \text{ lb/ft}$$

d. 
$$P_a = \frac{1}{2}(10.9)(1330) = 7248.5 \text{ lb/ft}$$

Location of the resultant from the bottom of the wall:  $\frac{10.9}{3} = 3.63 \,\text{ft}$ 

13.21 
$$K_a = \tan^2\left(45 - \frac{\phi'}{2}\right) = \tan^2\left(45 - \frac{16}{2}\right) = 0.568; \sqrt{K_a} = 0.754.$$
 Eq. (13.52):



$$P_a = \frac{1}{2} K_a \gamma H^2 - 2\sqrt{K_a} c' H + \frac{2c'^2}{\gamma}$$

$$= \frac{1}{2} (0.568)(19)(5)^2 - (2)(0.754)(26)(5) + \frac{(2)(26)^2}{19} = \mathbf{10.02 \, kN/m}$$

13.22 Eq. (13.63): 
$$z_o = \frac{2c'}{\gamma} \sqrt{\frac{1+\sin\phi'}{1-\sin\phi'}} = \frac{(2)(5)}{18} \sqrt{\frac{1+\sin25}{1-\sin25}} = 0.872 \text{ m}$$

At 
$$z = 0$$
 m:  $\sigma'_{a} = 0$ 

At 
$$z = 5$$
 m:  $\sigma'_a = \gamma z K'_{a(R)} \cos \alpha$ 

$$\frac{c'}{\gamma z} = \frac{5}{(18)(5)} = 0.055$$

For 
$$\alpha=10^{\circ}$$
,  $\phi'=25^{\circ}$  and  $\frac{c'}{\gamma z}=0.055$ , the value of  $K'_{a(R)}\approx 0.366$ 

$$\sigma_a' = (18)(5)(0.366)(\cos 10) = 32.44 \text{ kN/m}^2$$

$$P_a = \frac{1}{2}(5 - 0.872)(32.44) = 66.96 \text{ kN/m}$$

13.23 Use Eqs. (13.68) and (13.69). 
$$\alpha = 0$$
;  $\theta = 10^{\circ}$ ;  $\phi' = 30^{\circ}$ ;  $\gamma = 18 \text{ kN/m}^3$ ;  $H = 5 \text{ m}$ 

Part	δ΄	$K_a$	$P_a = \frac{1}{2} K_a \gamma H^2$
	(deg)	[Eq. (13.69)]	[Eq. (13.68)]
1	15	0.3784	85.14 kN/m
2	20	0.3769	84.80 kN/m

 $P_a$  is located at a vertical distance of 5/3 = 1.67 m above the bottom of the wall and is inclined at an angle  $\delta'$  to the normal drawn to the back face of the wall.

13.24 a. 
$$\phi' = 38^{\circ}$$
;  $\psi = 90 - \theta - \delta' = 90 - 5 - 20 = 65^{\circ}$ 

Weight of wedge 
$$ABC = \frac{1}{2}(11.6)(7.1)\underbrace{(128)}_{y} = 5271 \text{ lb/ft} = 5.271 \text{ kip/ft}$$

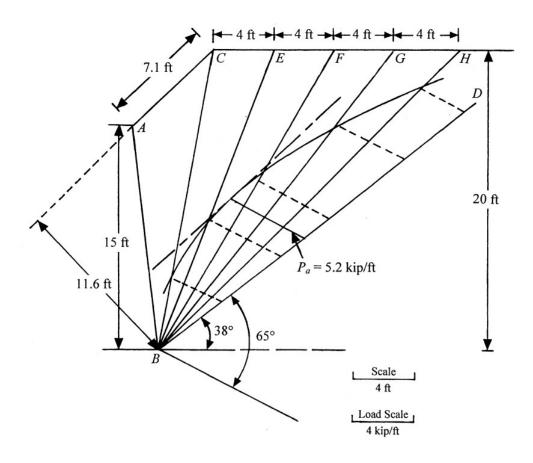
The weight of each of the wedges

$$CBE, EBF, FBG, GBH = \frac{1}{2}(20)(4)(128) = 5120 \text{ lb/ft} = 5.12 \text{ kip/ft}$$

Wedge	Weight (kip/ft)
ABC	5.271
ABE	5.271 + 5.12 = 10.391
ABF	10.391 + 5.12 = 15.511
ABG	15.511 + 5.12 = 20.631
ABH	20.631 + 5.12 = 25.751

The graphical construction is shown.

$$P_a = 5.2 \text{ kip/ft}$$



b. 
$$\gamma = \frac{(1680)(9.81)}{1000} = 16.48 \text{ kN/m}^3; \phi' = 30^\circ; \ \psi = 90 - 10 - 30 = 50^\circ$$

Weight of wedge 
$$ABC = \frac{1}{2}(5.25)(2.5)(16.48) = 108.15 \text{ kN/m}$$

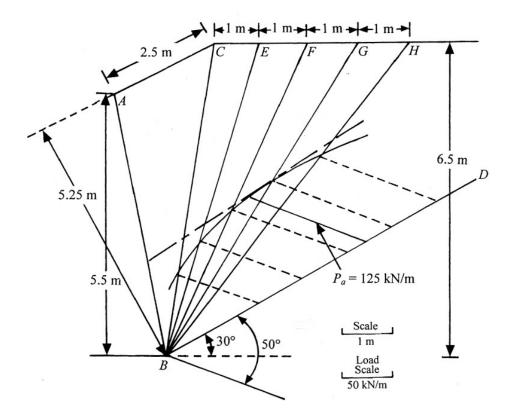
The weight of each of the wedges

CBE, EBF, FBG, GBH = 
$$\frac{1}{2}$$
(1)(6.5)(16.48) = 53.56 kN/m

Wedge	Weight (kip/ft)
ABC	108.15
ABE	108.15 + 53.56 = 161.71
ABF	161.71 + 53.56 = 215.27
ABG	215.27 + 53.56 = 268.83
ABH	268.83 + 53.56 = 322.39

The graphical construction is shown.

$$P_a = 125 \text{ kN/m}$$



13.25 From Eqs. (13.81) and (13.82),  $\theta^* = \theta + \overline{\beta}$  and  $\alpha^* = \alpha + \overline{\beta}$ .

$$\overline{\beta} = \tan^{-1} \left( \frac{k_h}{1 - k_v} \right) = \tan^{-1} \left( \frac{0.15}{1 - 0} \right) = 8.53^{\circ}$$

$$\theta^* = 10^{\circ} + 8.53^{\circ} = 18.53^{\circ}$$

$$\alpha^* = 10^{\circ} + 8.53^{\circ} = 18.53^{\circ}$$

$$P_a(\theta^*, \alpha^*) = \frac{1}{2} \gamma H^2 K_a$$

$$\frac{\delta'}{\phi'} = \frac{2}{3}$$

From Table 13.7, for  $\theta^* = 18.53^{\circ}$  and  $\alpha^* = 18.53^{\circ}$ , the value of  $K_a \approx 0.61$ .

From Eq. (13.85):

$$P_{ae} = P_a(\theta^*, \alpha^*)(1 - k_v) \left[ \frac{\cos^2(\theta + \overline{\beta})}{\cos \theta \cos^2 \overline{\beta}} \right]$$
$$= \left[ \left( \frac{1}{2} \right) (0.61)(15)(4)^2 \right] (1 - 0) \left[ \frac{\cos^2(10 + 8.53)}{\cos(10)\cos^2(8.53)} \right] = 68.3 \text{ kN/m}$$

13.26 Eq. (13.93): 
$$P_{ae} = \gamma (H - z_o)^2 N'_{a\gamma} - c' (H - z_o)^2 N'_{ac}$$

Given 
$$z_0 = 0$$
;  $\theta = 10^{\circ}$ ;  $\phi' = 15^{\circ}$ ;  $k_h = 0.15$ 

$$N'_{ac} = N_{ac} = 1.75$$
 (Figure 13.31);  $N_{a\gamma} = 0.3$  (Figure 13.33);  $\lambda = 1.3$  (Figure 13.34);

$$N'_{a\gamma} = \lambda N_{a\gamma}$$
. So,

$$P_{ae} = (19)(6-0)^2(1.3 \times 0.3) - (20)(6-0)(1.75) =$$
**56.76 kN/m**