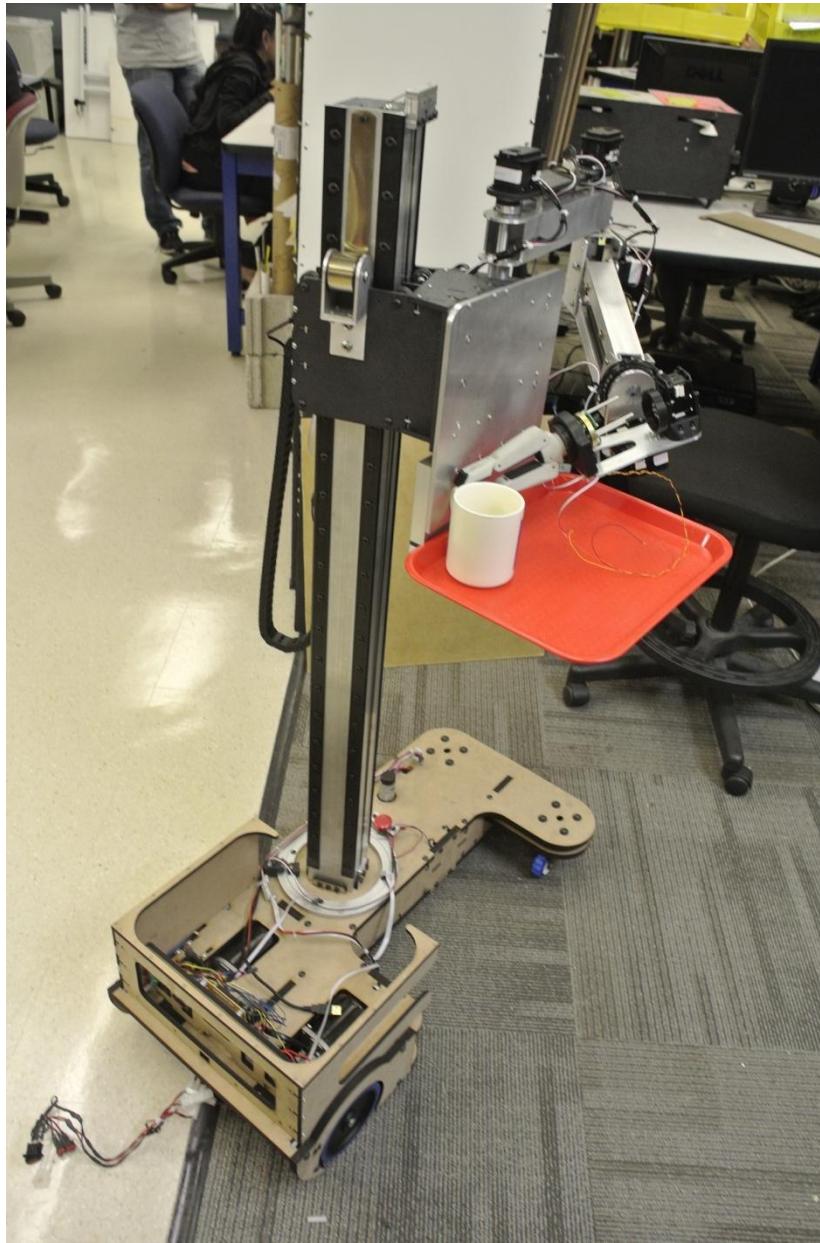


Robotics: Fundamentals

Prof. Mark Yim
University of Pennsylvania

Week 6: Inverse Kinematics

Inverse Kinematics



Inverse Kinematics Definition

$$H = \begin{bmatrix} R & P \\ 0 & 1 \end{bmatrix}$$

$$T_{0n}(q_1 \cdots q_n) = H$$

$$T_{0n}(q_1 \cdots q_n) = A_1 \cdots A_n$$

$$T_{ij}(q_1 \cdots q_n) = H_{ij}$$

Where, T_{ij}, H_{ij} refer to the 12 nontrivial entries of T_{0n} , and H

Stanford Arm Transform

$$H = \begin{bmatrix} r_{11} & r_{12} & r_{13} & P_x \\ r_{21} & r_{22} & r_{23} & P_y \\ r_{31} & r_{32} & r_{33} & P_z \\ 0 & 0 & 0 & 1 \end{bmatrix},$$

$$\begin{aligned} r_{11} &= c_1[c_2(c_4c_5c_6 - s_4s_6) - s_2s_5c_6] - s_1(s_4c_5c_6 + c_4s_6) \\ r_{21} &= s_1[c_2(c_4c_5c_6 - s_4s_6) - s_2s_5c_6] + c_1(s_4c_5c_6 + c_4s_6) \\ r_{31} &= -s_2(c_4c_5c_6 - s_4s_6) - c_2s_5c_6 \\ r_{12} &= c_1[-c_2(c_4c_5s_6 + s_4s_6) + s_2s_5s_6] - s_1(-s_4c_5c_6 + c_4s_6) \\ r_{22} &= s_1[-c_2(c_4c_5s_6 + s_4s_6) + s_2s_5s_6] + c_1(-s_4c_5c_6 + c_4s_6) \\ r_{32} &= s_2(c_4c_5c_6 + s_4s_6) + c_2s_5c_6 \\ r_{13} &= c_1(c_2c_4s_5 + s_2c_5) - s_1s_4s_5 \\ r_{23} &= s_1(c_2c_4s_5 + s_2c_5) + c_1s_4s_5 \\ r_{33} &= -s_2c_4s_5 + c_2c_5 \\ P_x &= c_1s_2d_3 - s_1d_2 + d_6(c_1c_2c_4s_5 + c_1s_2c_5 - s_1s_4s_5) \\ P_y &= s_1s_2d_3 + c_1d_2 + d_6(s_1c_2c_4s_5 + s_1s_2c_5 + c_1s_4s_5) \\ P_z &= c_2d_3 + d_6(c_2c_5 - s_2c_4s_5) \end{aligned}$$

Approaches

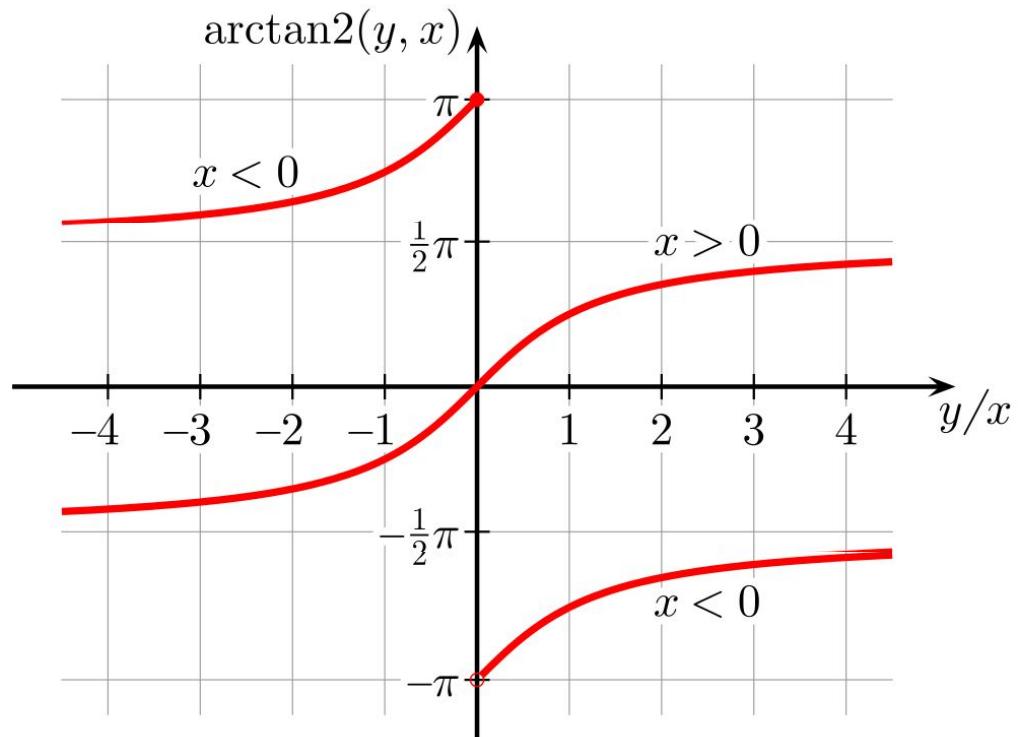
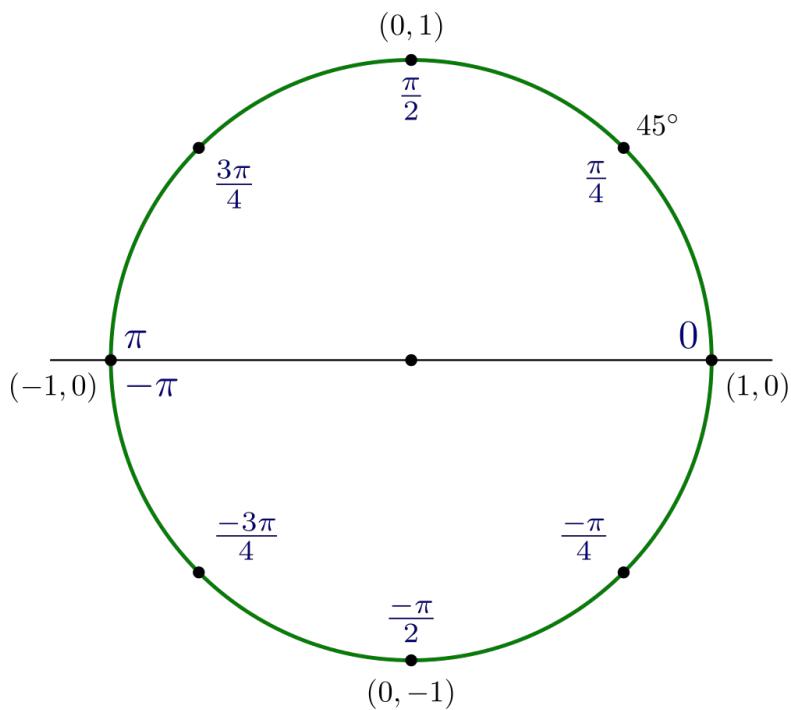
Closed form

- $q_k = f_k(h_{11}, \dots, h_{34}), k = 1, \dots, n$
- Geometric approach
- *IKFast* (open source C++ code)

Approximate Solutions

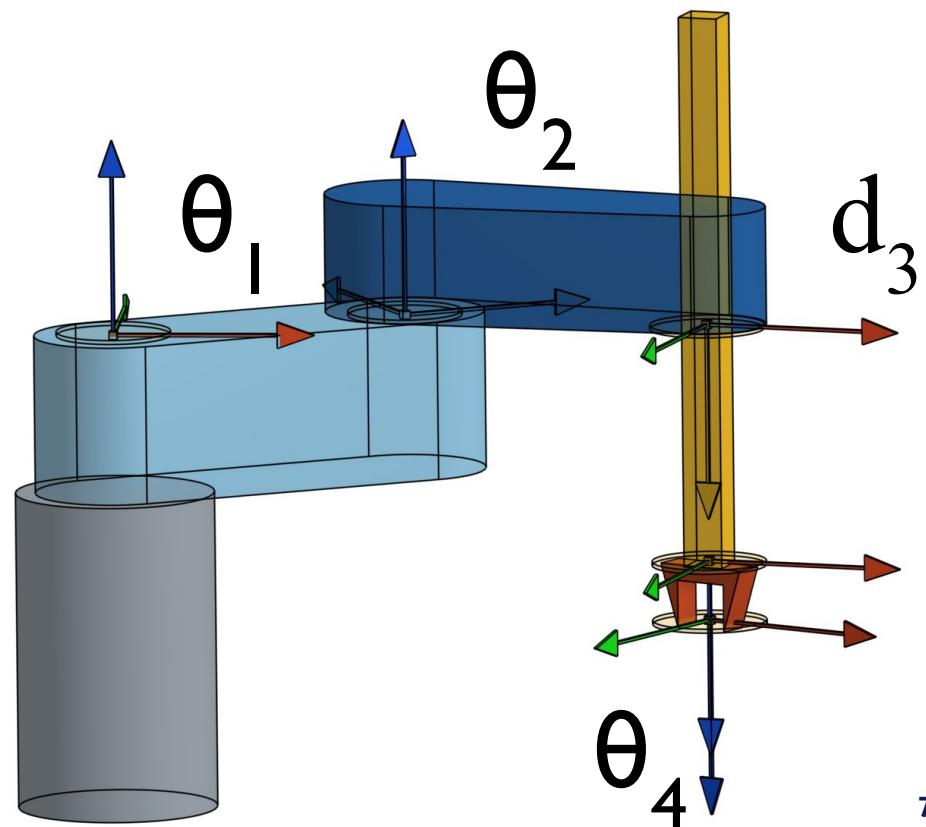
- Iterative optimization
- Jacobian Inverse

$\text{atan}(y/x)$ vs $\text{atan2}(y, x)$



SCARA IK

$$\begin{bmatrix}
 c_{12}c_4 + s_{12}s_4 & -c_{12}s_4 + s_{12}c_4 & 0 & a_1c_1 + a_2c_{12} \\
 s_{12}c_4 - c_{12}s_4 & -s_{12}s_4 - c_{12}c_4 & 0 & a_1s_1 + a_2s_{12} \\
 0 & 0 & -1 & -d_3 - d_4 \\
 0 & 0 & 0 & 1
 \end{bmatrix} \\
 = \begin{bmatrix}
 r_{11} & r_{12} & r_{13} & P_x \\
 r_{21} & r_{22} & r_{23} & P_y \\
 r_{31} & r_{32} & r_{33} & P_z \\
 0 & 0 & 0 & 1
 \end{bmatrix}$$



SCARA IK

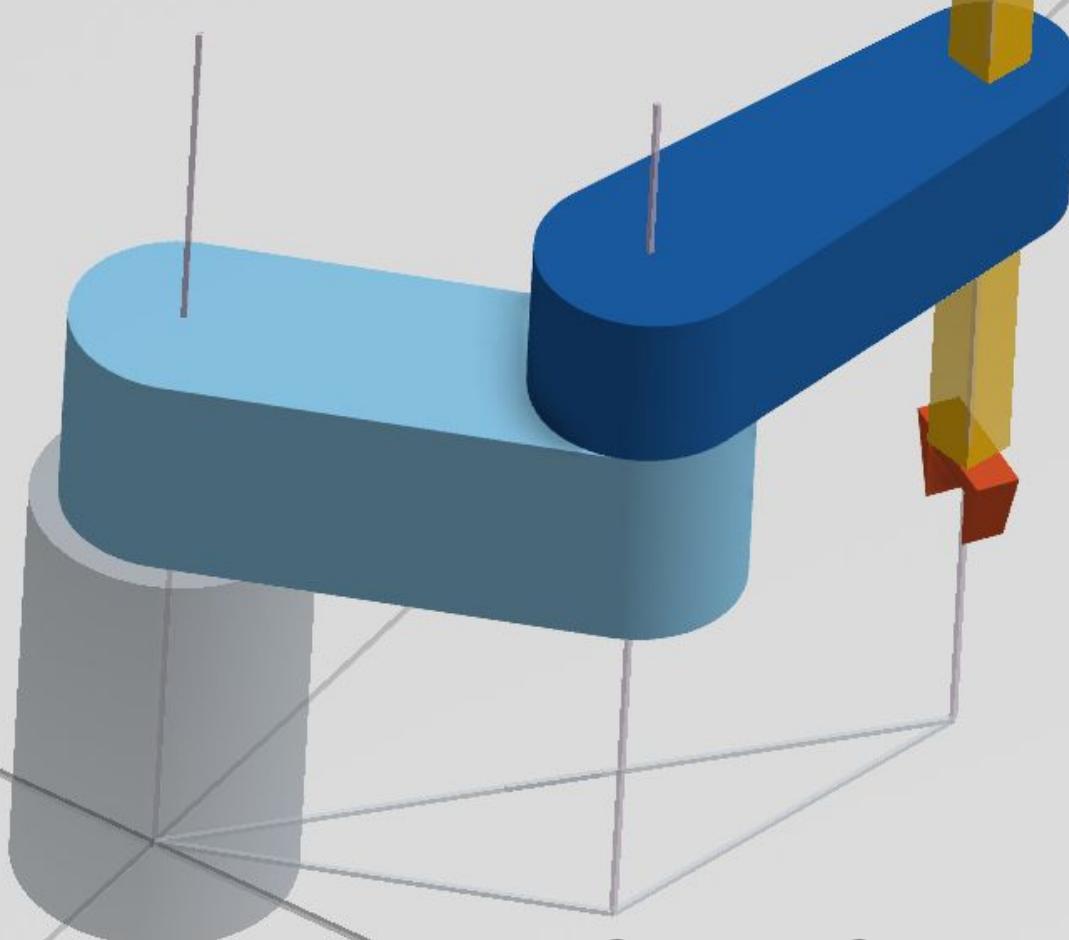
$$\begin{bmatrix} c_{12}c_4 + s_{12}s_4 & -c_{12}s_4 + s_{12}c_4 & 0 \\ s_{12}c_4 - c_{12}s_4 & -s_{12}s_4 - c_{12}c_4 & 0 \\ 0 & 0 & -1 \end{bmatrix}$$

$$\begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix} = \begin{bmatrix} c_\psi & s_\psi & 0 \\ s_\psi & -c_\psi & 0 \\ 0 & 0 & -1 \end{bmatrix}$$

$$angle = \text{atan2}(y, x)$$

$$\psi = \text{atan2}(r_{12}, r_{11})$$

SCARA IK



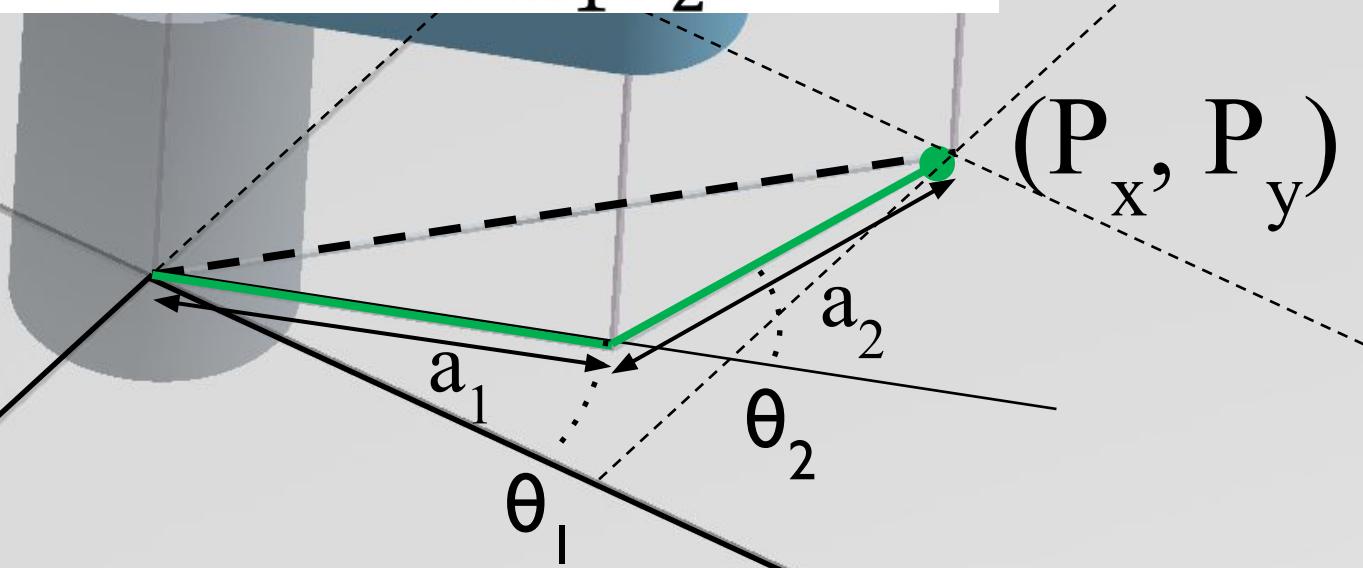
$$\theta_1 + \theta_2 - \theta_4 = \psi$$

SCARA IK

$$r^2 = a_1^2 + a_2^2 - 2a_1a_2 \cos(\theta)$$

$$P_x^2 + P_y^2 = a_1^2 + a_2^2 + 2a_1a_2 c_2$$

$$c_2 = \frac{P_x^2 + P_y^2 - a_1^2 - a_2^2}{2a_1a_2}$$

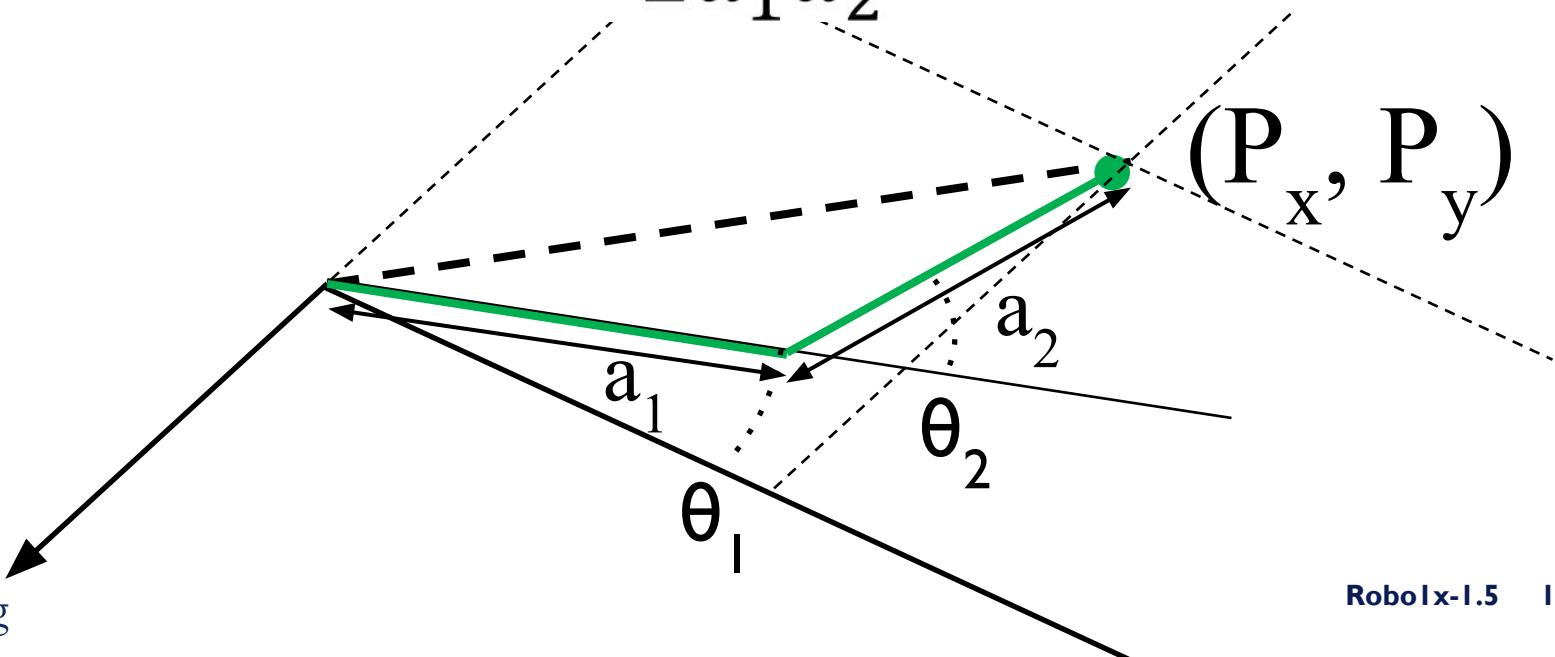


SCARA IK θ_2

$$r^2 = a_1^2 + a_2^2 - 2a_1a_2 \cos(\theta_2)$$

$$P_x^2 + P_y^2 = a_1^2 + a_2^2 - 2a_1a_2 c_2$$

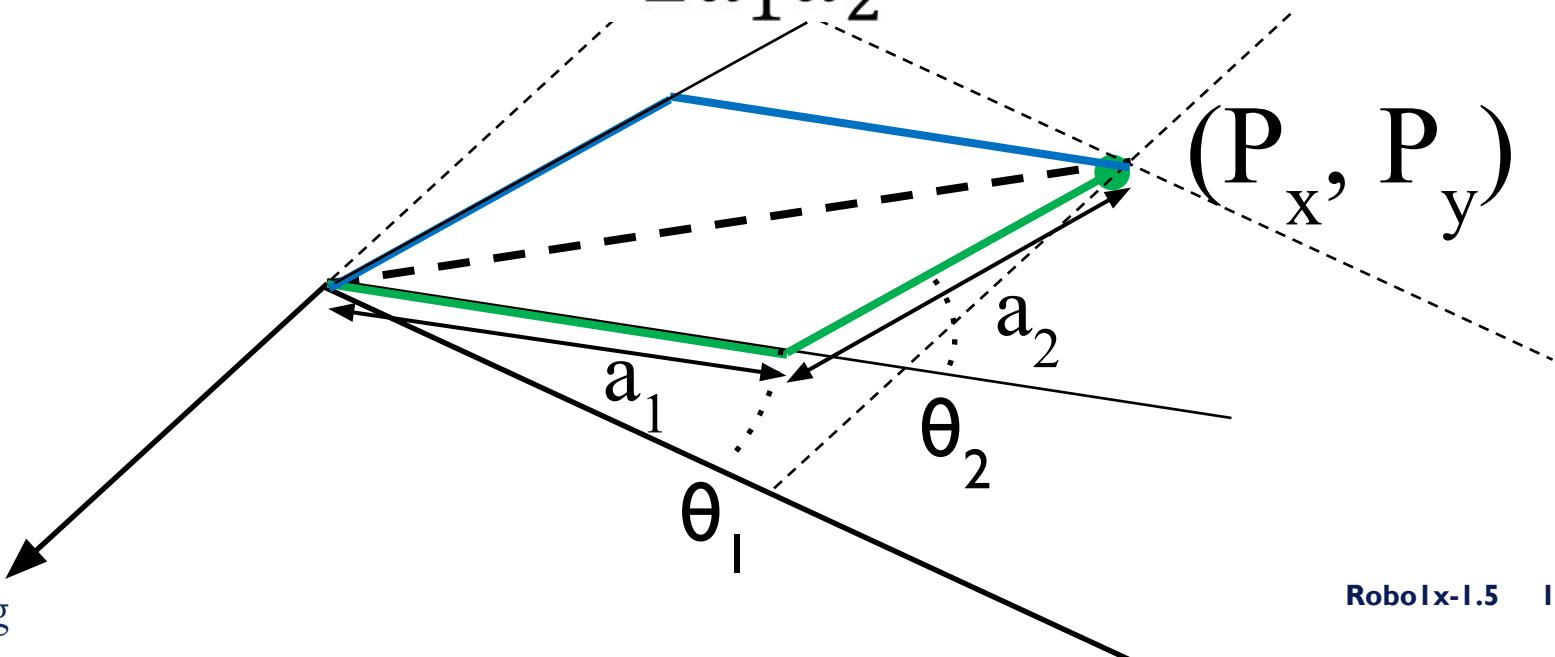
$$c_2 = \frac{P_x^2 + P_y^2 - (a_1^2 + a_2^2)}{2a_1a_2}$$



SCARA IK θ_2

$$\theta_2 = \pm \cos^{-1} \left(\frac{P_x^2 + P_y^2 - (a_1^2 + a_2^2)}{2a_1a_2} \right)$$

$$c_2 = \frac{P_x^2 + P_y^2 - a_1^2 - a_2^2}{2a_1a_2}$$



SCARA IK θ_1

$$\theta_1 = \alpha - \beta$$

A 3D diagram of a SCARA robot arm. The arm consists of three cylindrical segments: a grey base, a blue middle segment, and a blue top segment. A yellow rectangular end effector is attached to the top segment. The diagram illustrates the geometric parameters for inverse kinematics:

- The total horizontal reach is labeled a .
- The length of the first segment is labeled a_1 .
- The length of the second segment is labeled a_2 .
- The angle between the horizontal and the second segment is labeled θ_2 .
- The angle between the vertical axis of the first segment and the second segment is labeled β .
- The angle between the vertical axis of the first segment and the horizontal is labeled α .
- The coordinates of the end effector are given as (P_x, P_y) .
- Red labels indicate components of the second segment's length: $a_2 c_2$ and $a_2 s_2$.

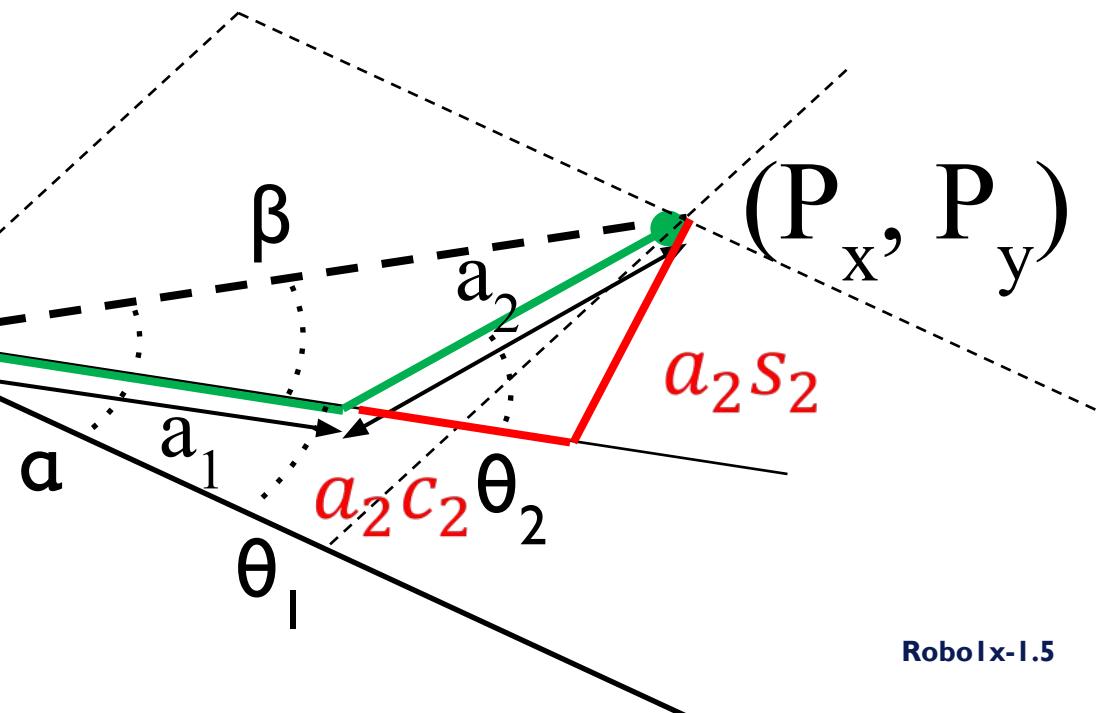
Below the diagram, two equations are shown:

$$\alpha = \text{atan2}(P_y, P_x)$$
$$\theta_1 = \alpha - \beta$$

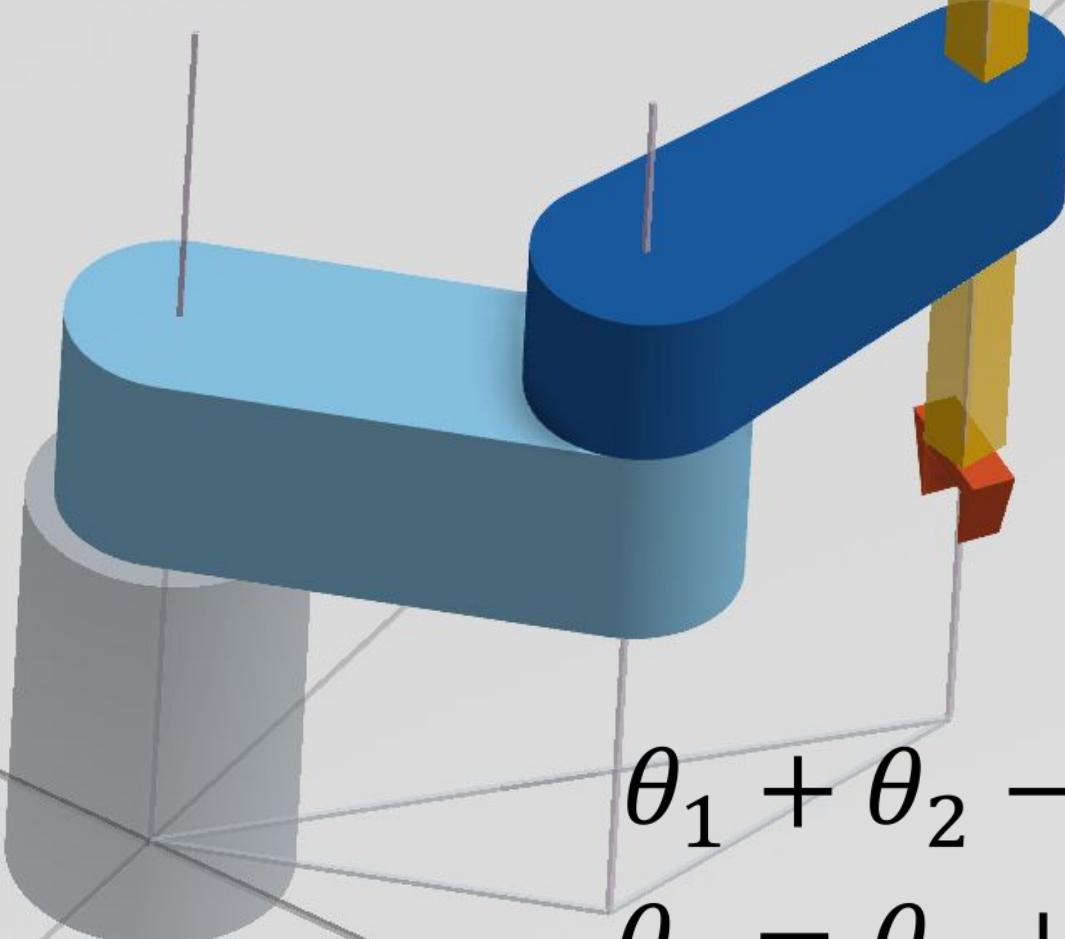
SCARA IK θ_1

$$\theta_1 = \alpha - \beta$$

$$\theta_1 = \text{atan2}(P_y, P_x) - \text{atan2}(a_2 s_2, a_1 + a_2 c_2)$$



SCARA IK

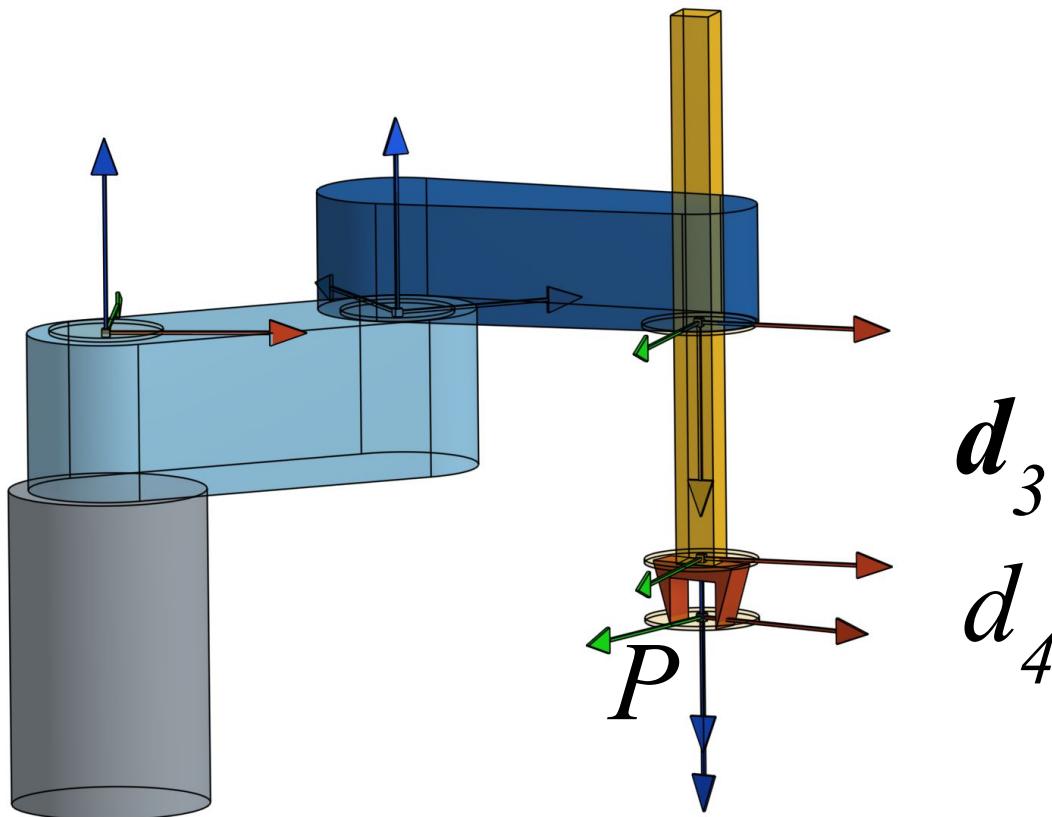


$$\theta_1 + \theta_2 - \theta_4 = \psi$$

$$\theta_4 = \theta_1 + \theta_2 - \psi$$

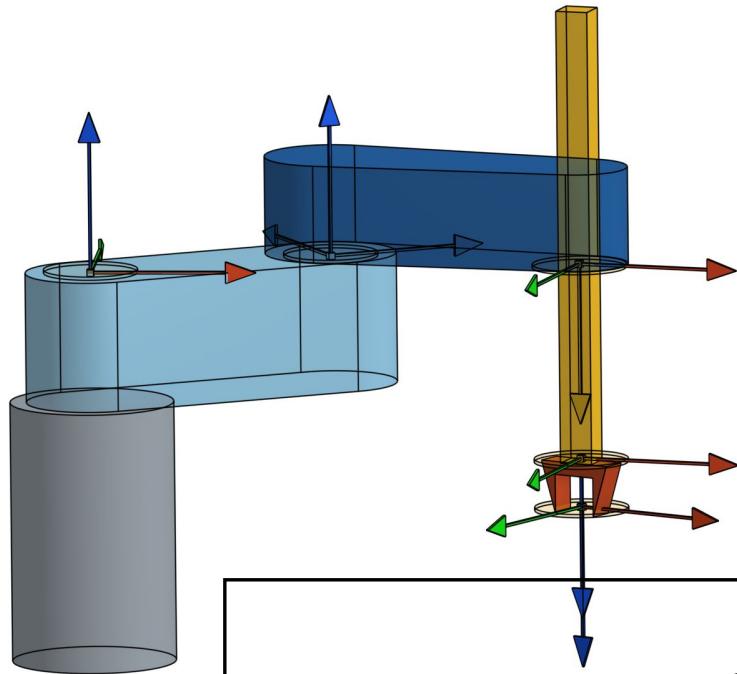
$$\boxed{\theta_4 = \theta_1 + \theta_2 - \text{atan}(r_{12}, r_{11})}$$

SCARA IK d_3



$$d_3 = P_z + d_4$$

SCARA IK



$$\theta_2 = \pm \cos^{-1} \left(\frac{P_x^2 + P_y^2 - (a_1^2 + a_2^2)}{2a_1a_2} \right)$$

$$\theta_1 = \text{atan2}(P_y, P_x) - \text{atan2}(a_2 s_2, a_1 + a_2 c_2)$$

$$\theta_4 = \theta_1 + \theta_2 - \text{atan}(r_{12}, r_{11})$$

$$d_3 = P_z + d_4$$

SCARA IK

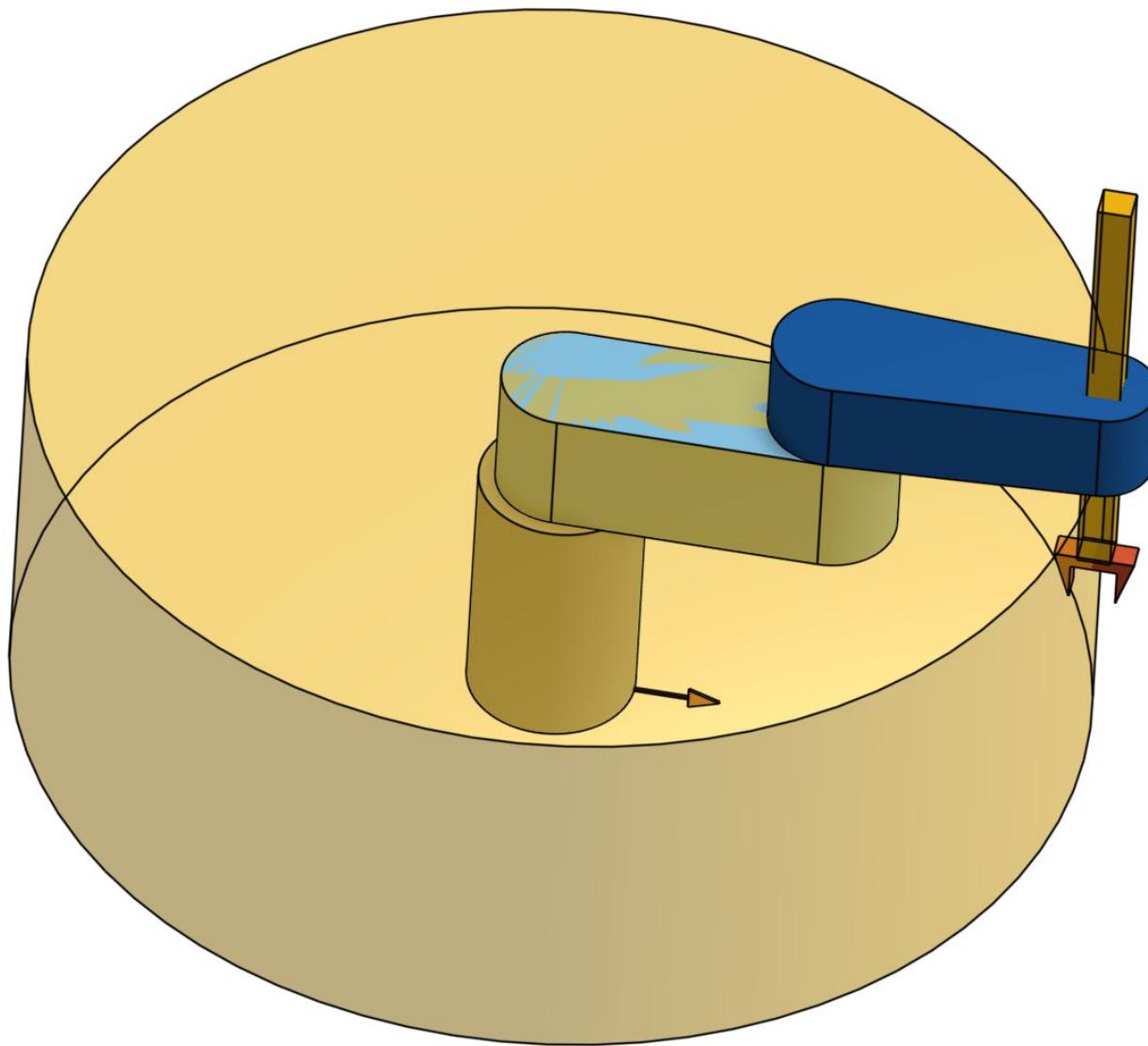
$$\begin{bmatrix} c_{12}c_4 + s_{12}s_4 & -c_{12}s_4 + s_{12}c_4 & 0 \\ s_{12}c_4 - c_{12}s_4 & -s_{12}s_4 - c_{12}c_4 & 0 \\ 0 & 0 & -1 \end{bmatrix}$$

$$\theta_2 = \pm \cos^{-1} \left(\frac{P_x^2 + P_y^2 - (a_1^2 + a_2^2)}{2a_1a_2} \right)$$

$$\sqrt{P_x^2 + P_y^2} = \sqrt{(a_1 + a_2)^2}$$

$$P_x^2 + P_y^2 = a_1^2 + 2a_1a_2 + a_2^2$$

Workspace

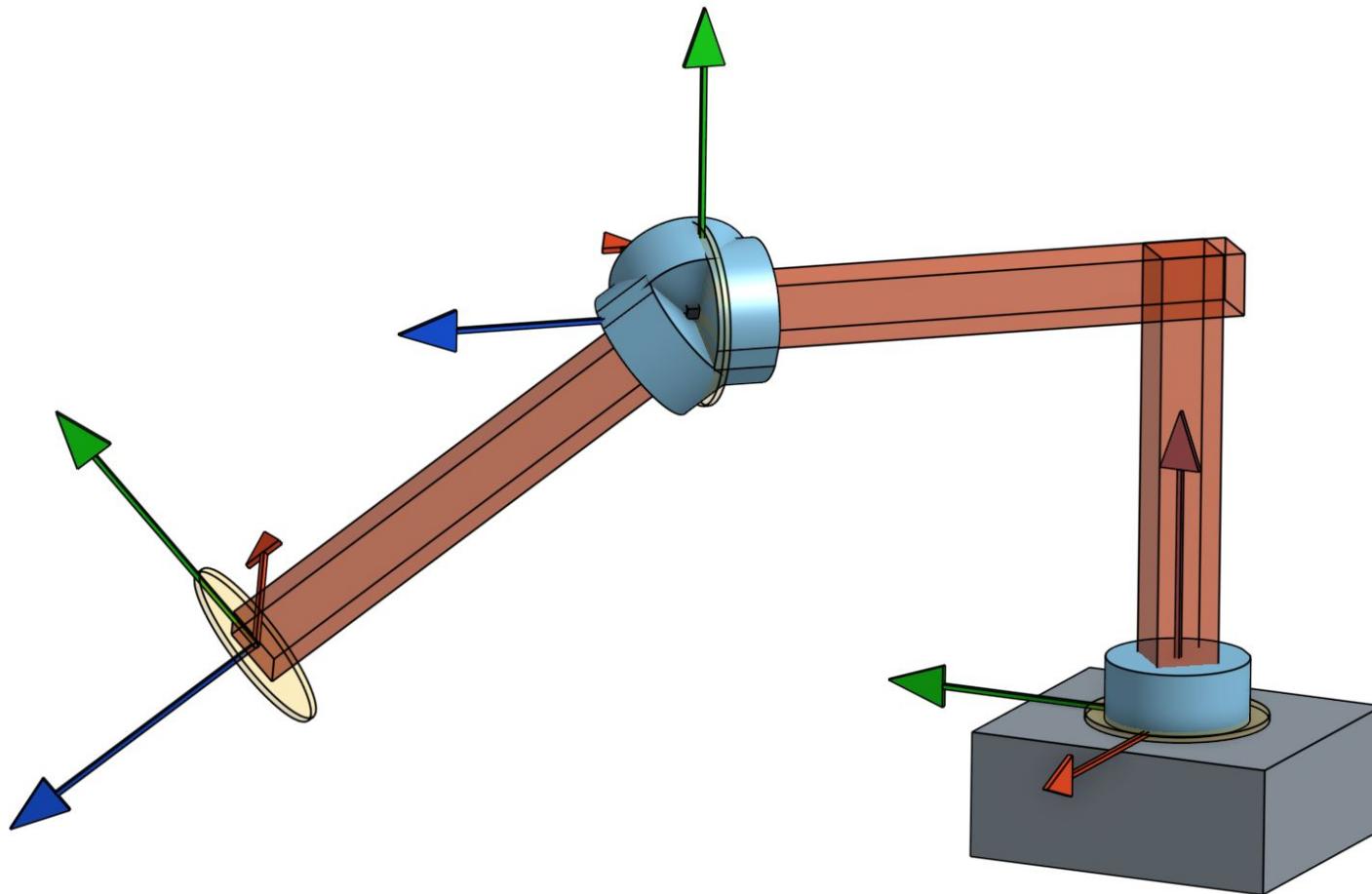


Robotics: Fundamentals

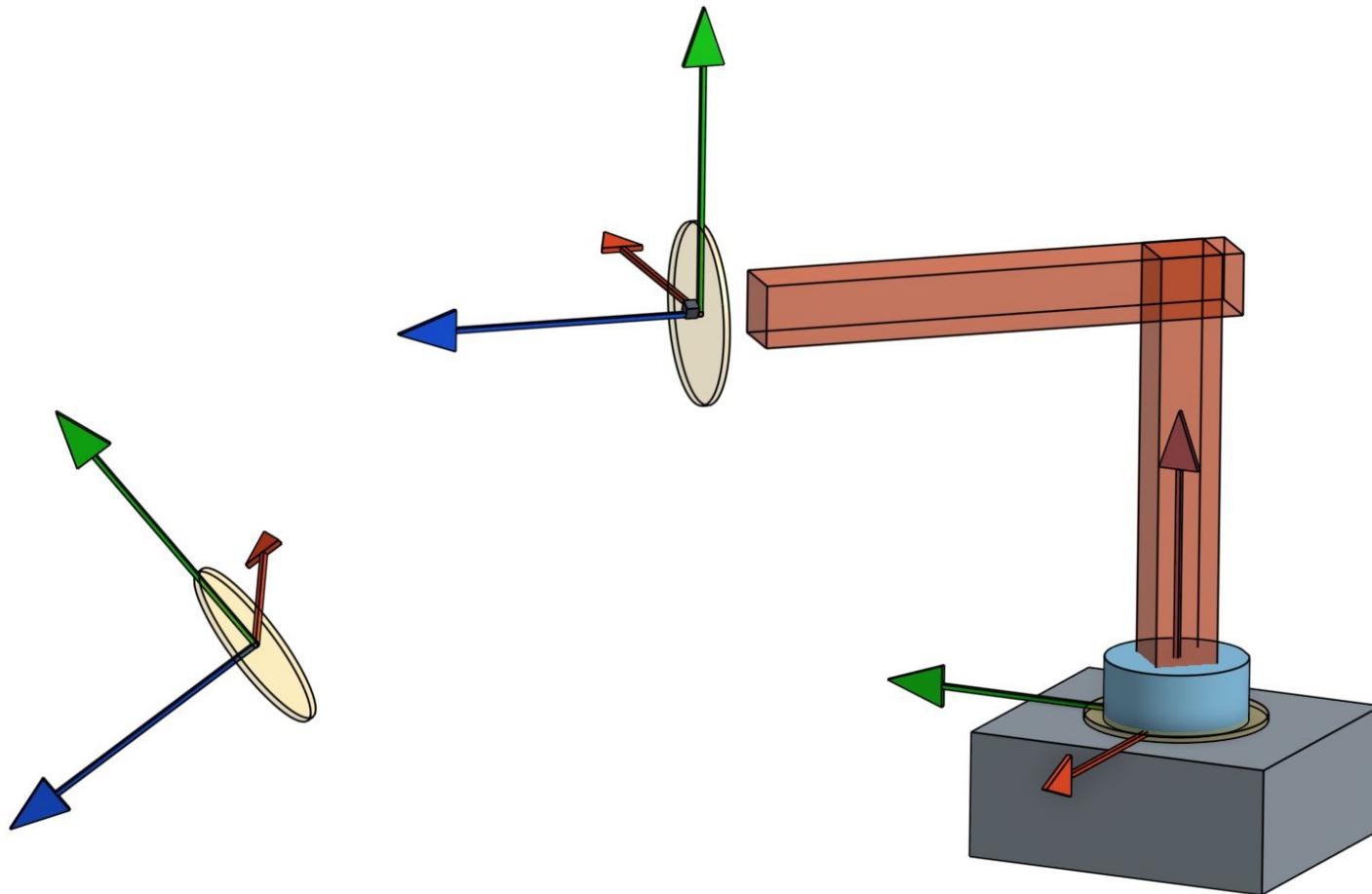
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Week 6: Kinematic Decoupling and Inverse Position

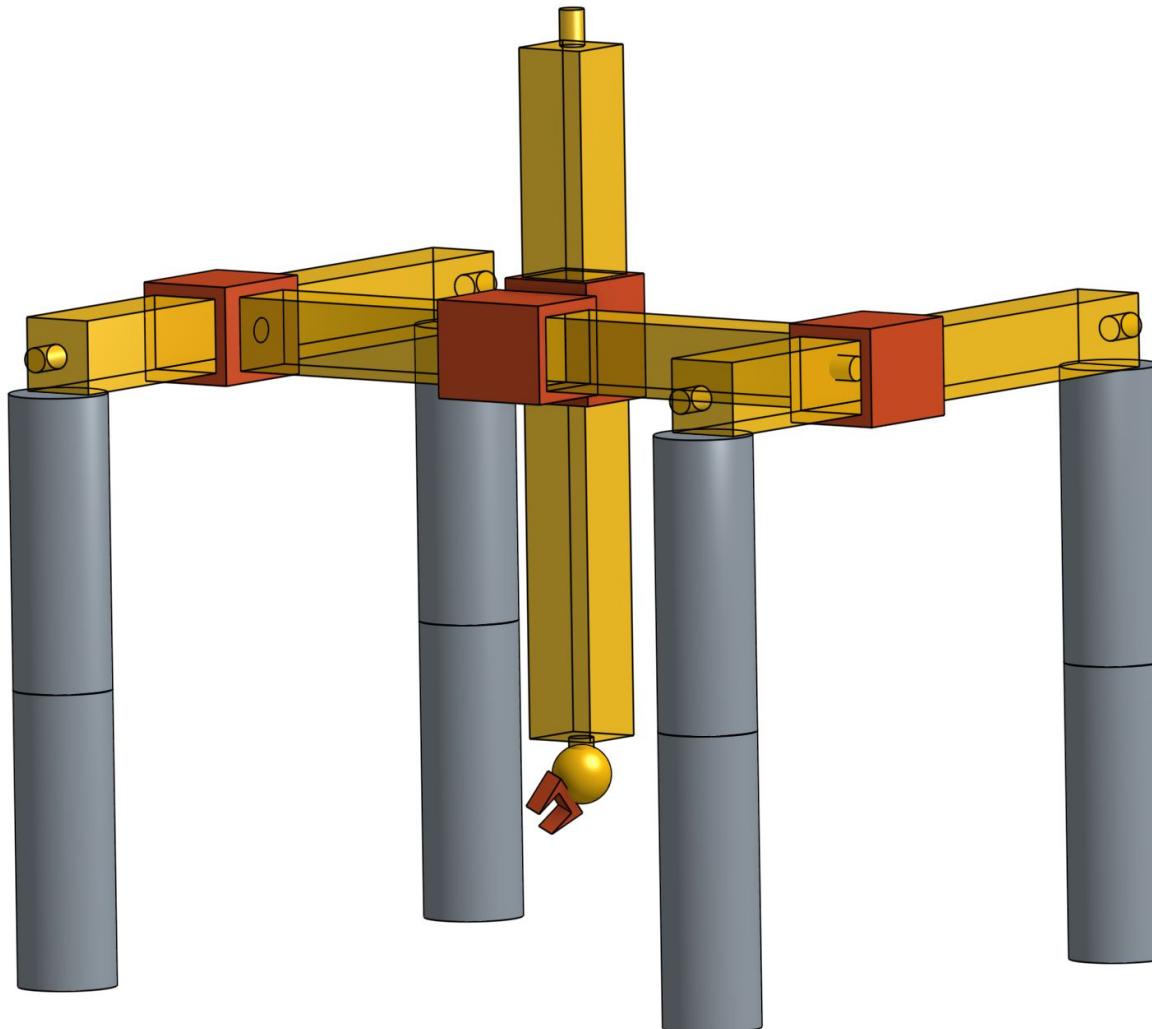
Kinematic Decoupling



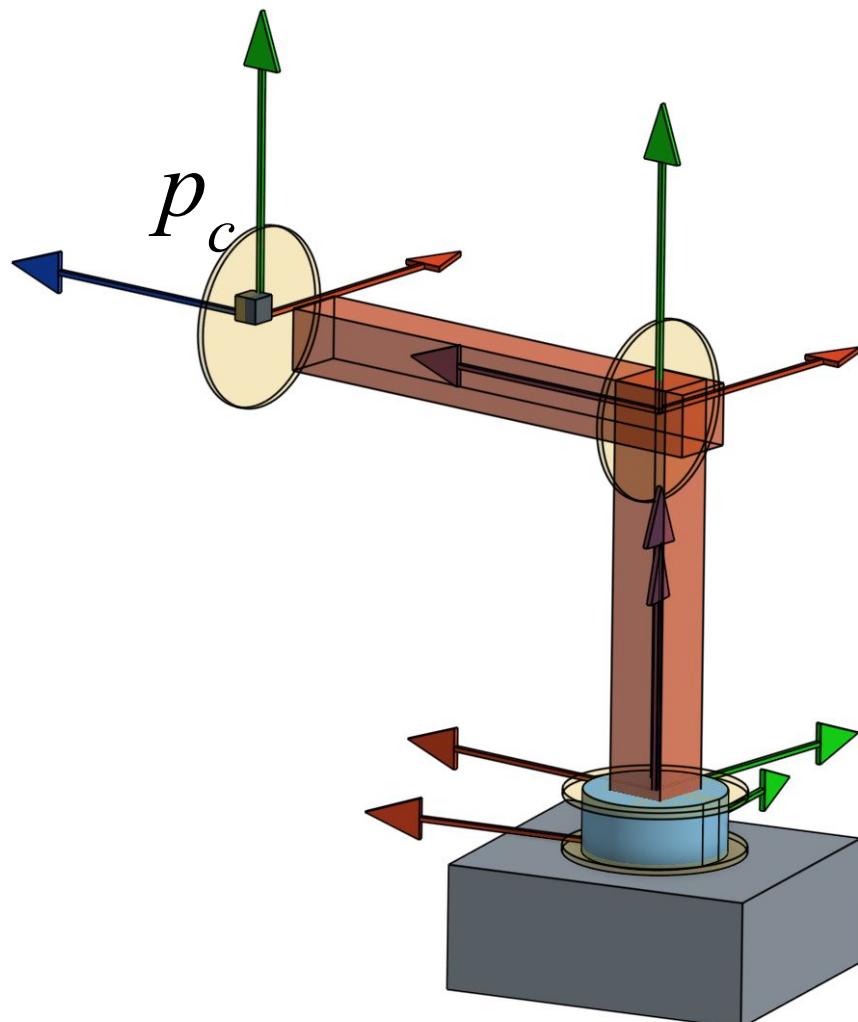
Kinematic Decoupling



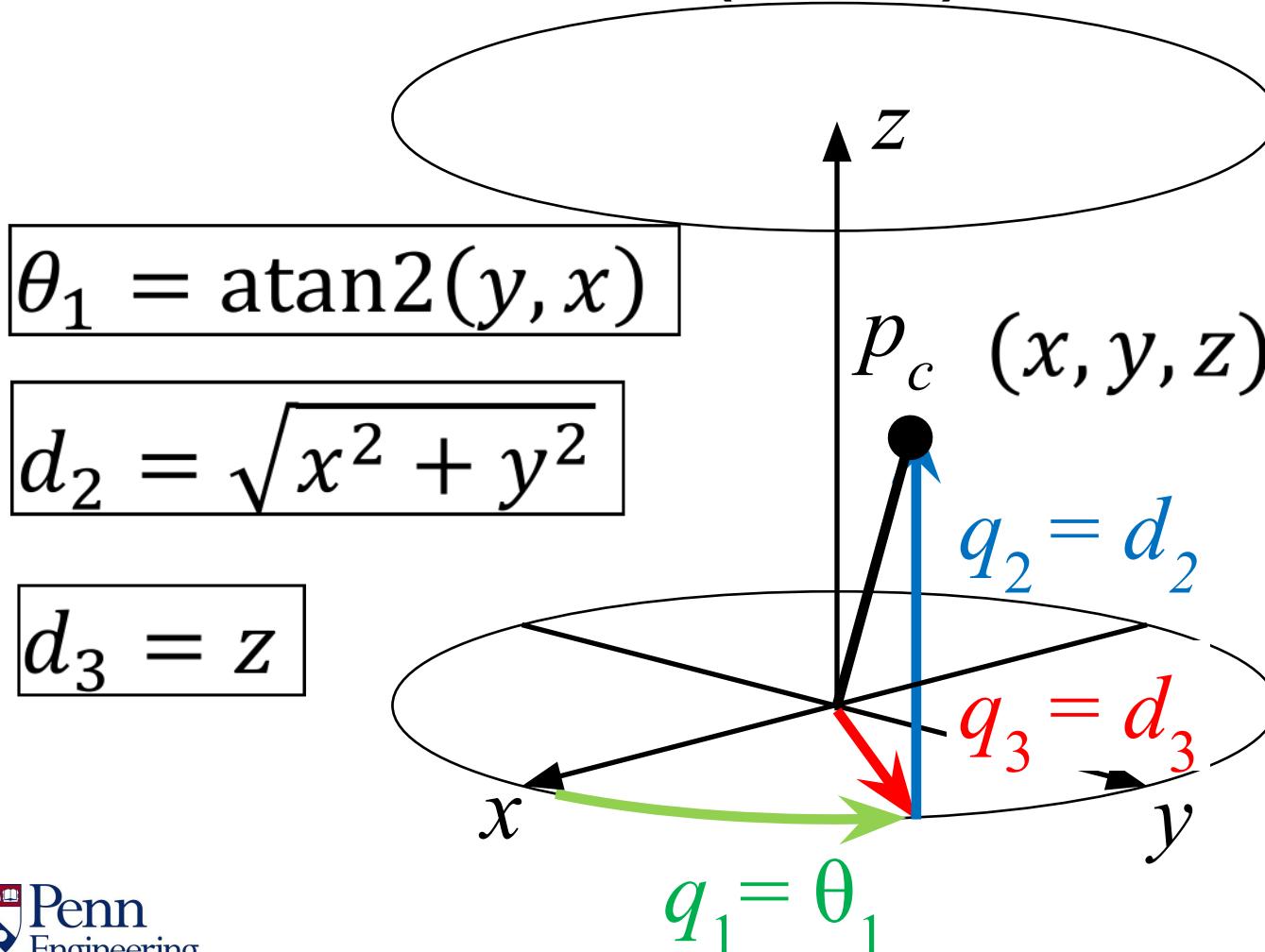
Kinematic Decoupling



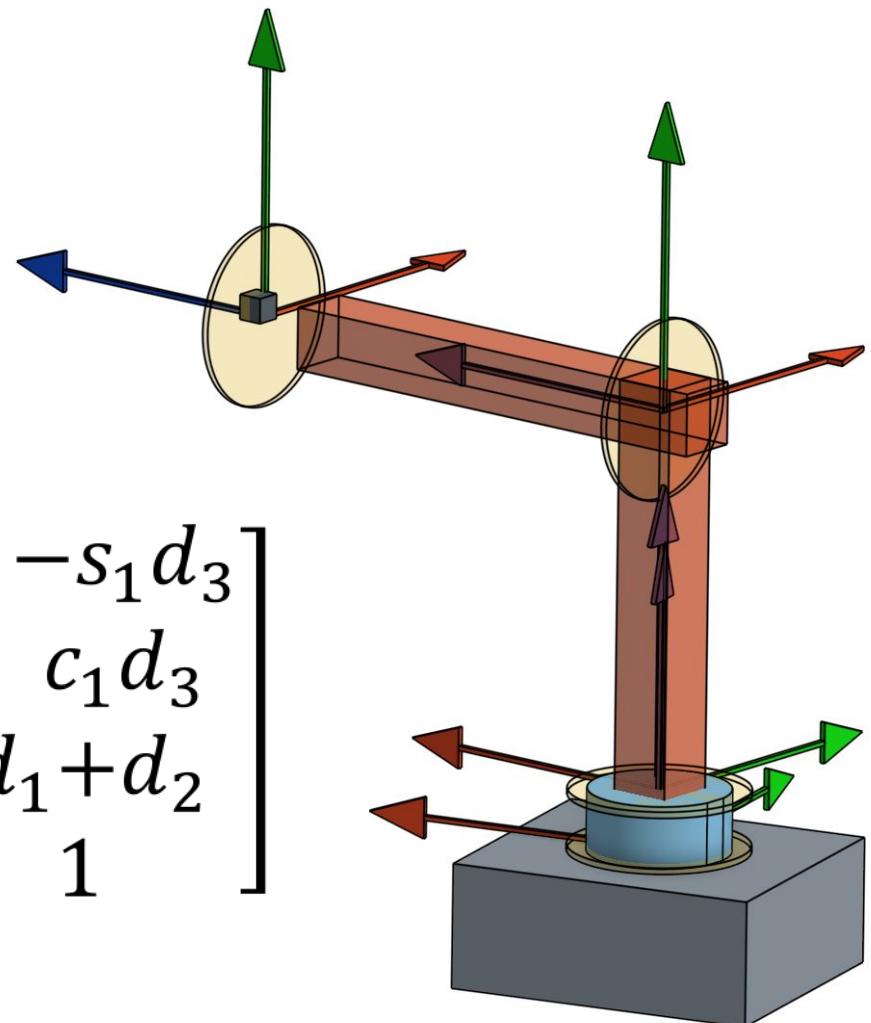
Inverse Position: Cylindrical robot case



Cylindrical coordinates (RPP)

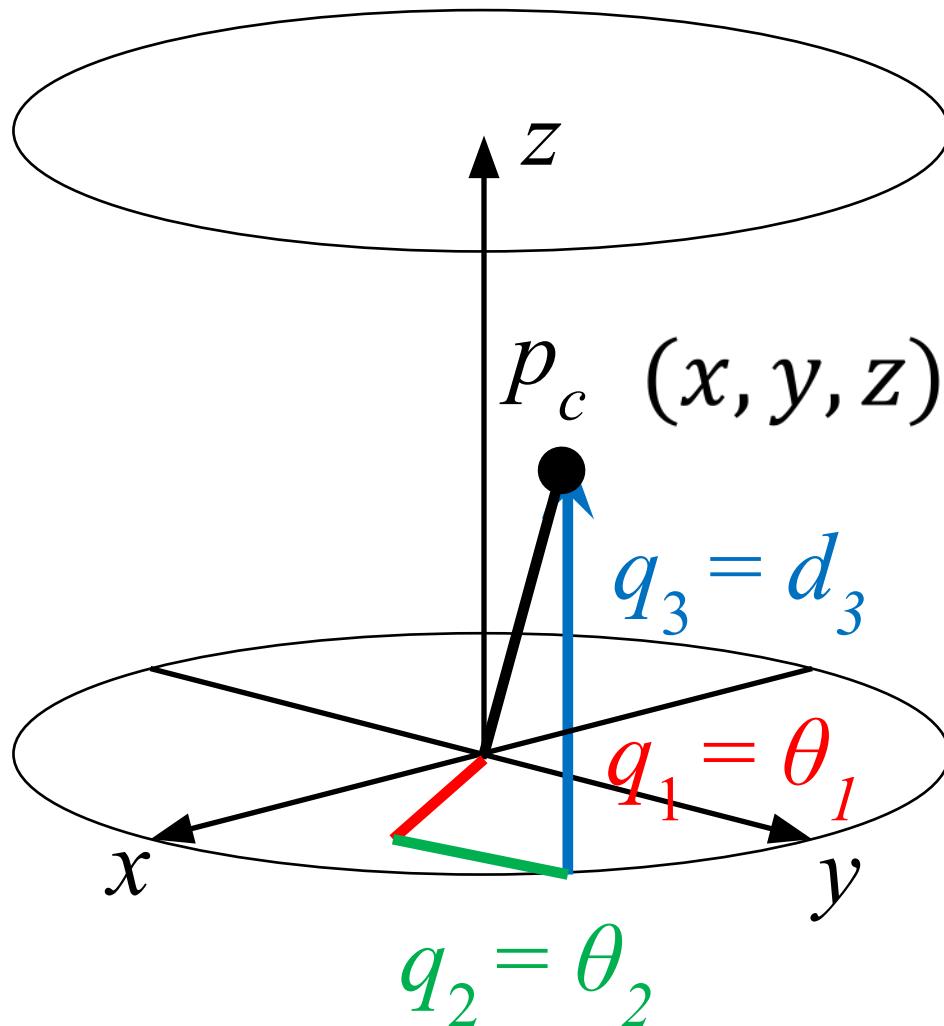


Wrist Center Rotation

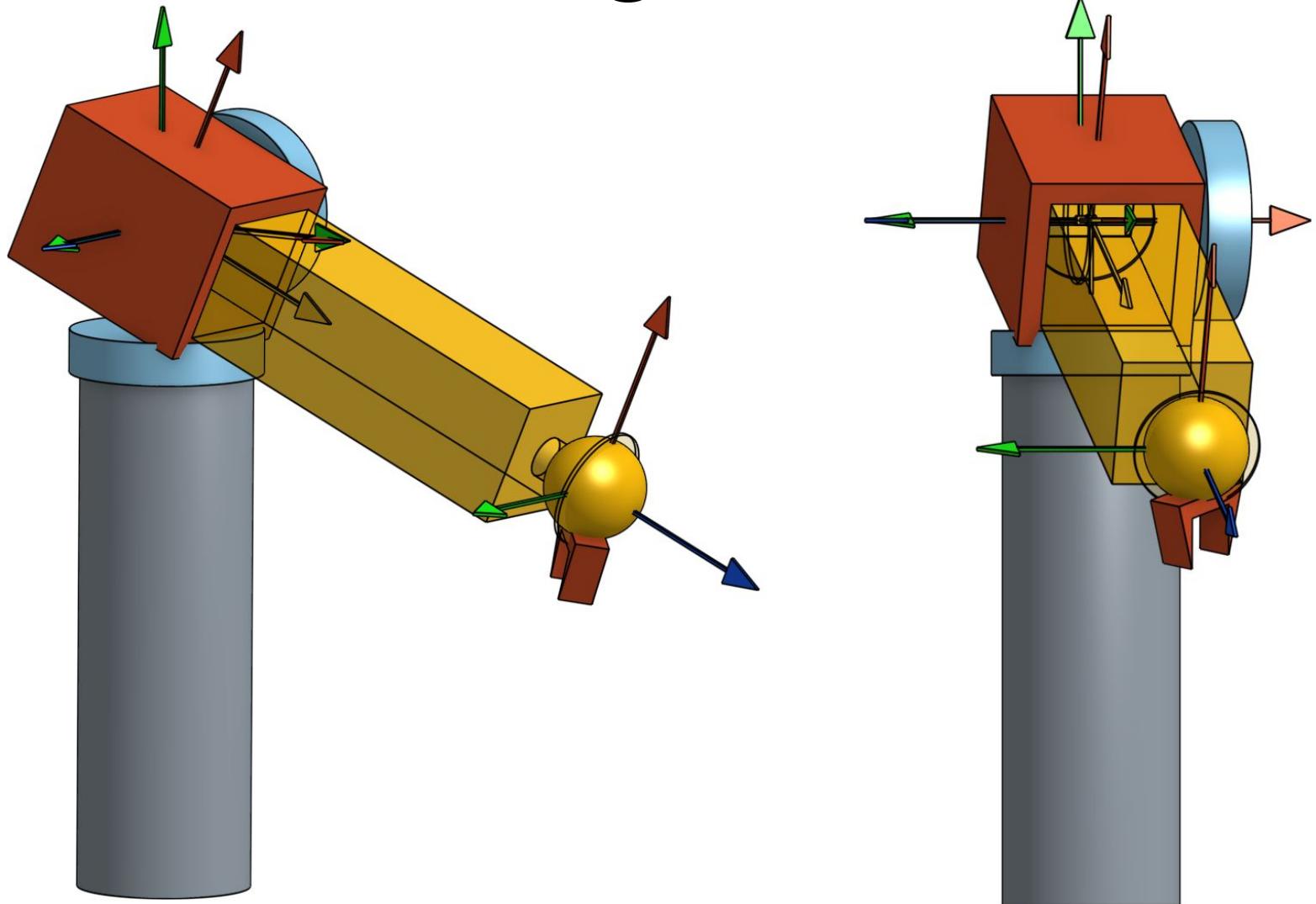


$$T_{03} = \begin{bmatrix} c_1 & 0 & -s_1 & -s_1 d_3 \\ s_1 & 0 & c_1 & c_1 d_3 \\ 0 & -1 & 0 & d_1 + d_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

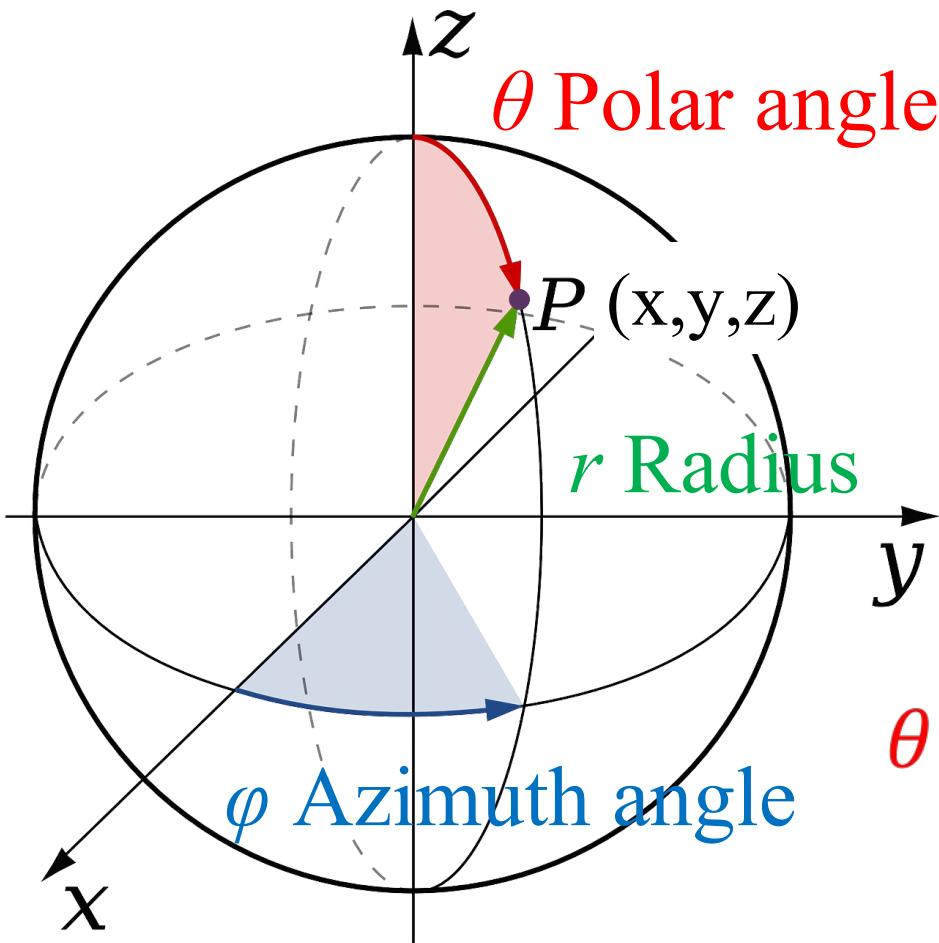
Ist part of SCARA (RRP)



Inverse Position Spherical Configuration (RRP)



Spherical Coordinates

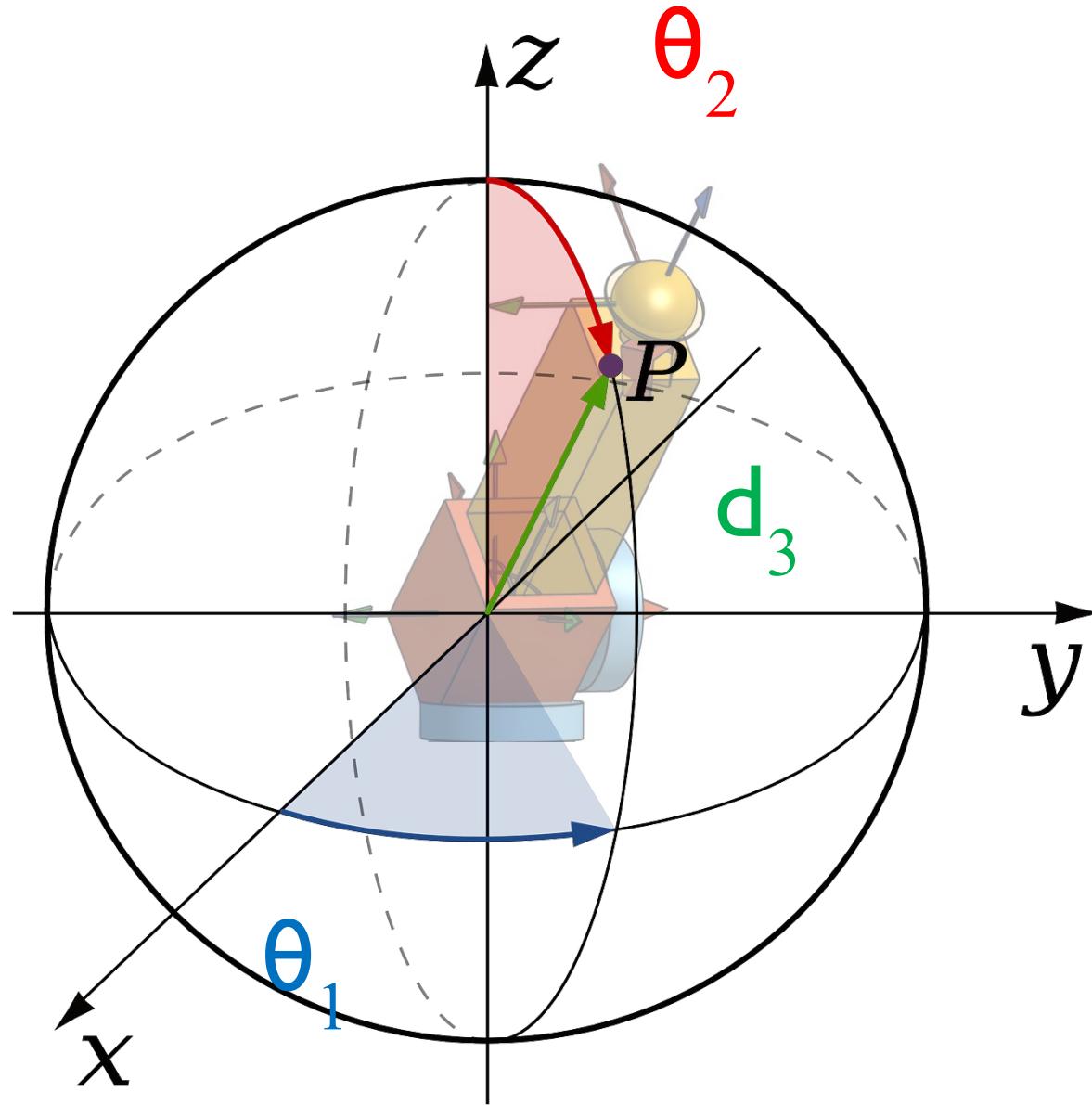


$$r = \sqrt{x^2 + y^2 + z^2}$$

$$\phi = \text{atan2}(y, x)$$

$$\theta = \text{atan2}(\sqrt{x^2 + y^2}, z)$$

Inv. Pos. Spherical (RRP)

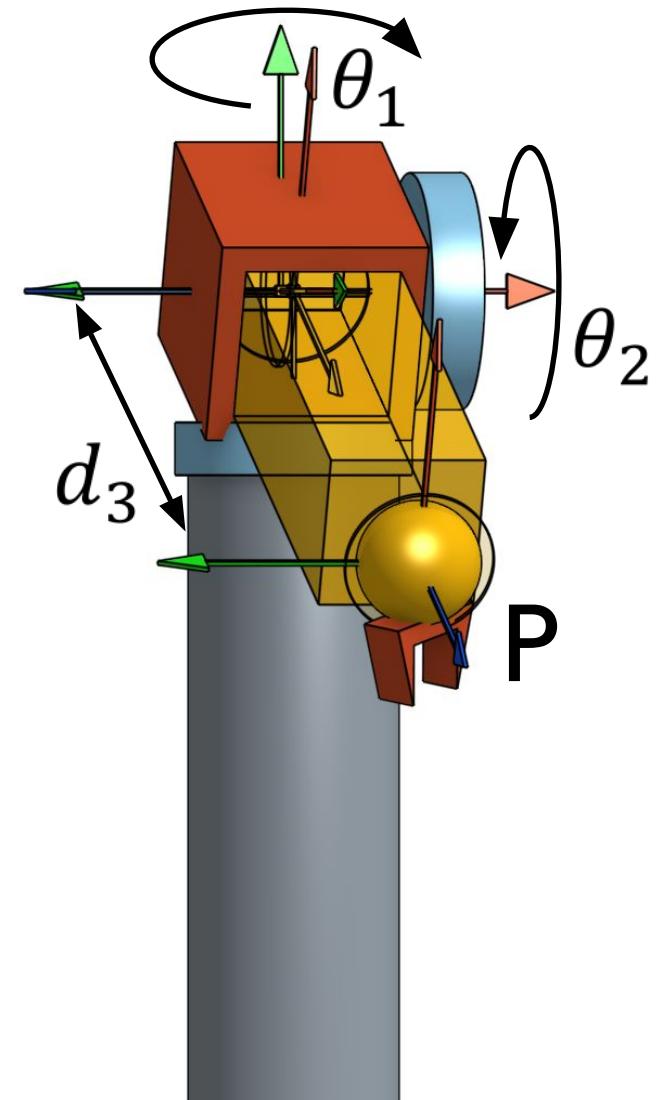


Inv. Pos. Spherical (RRP)

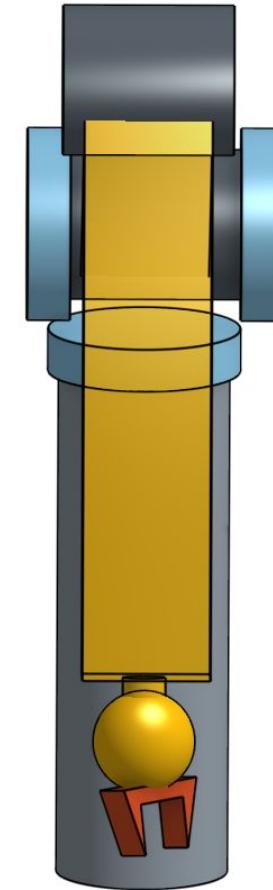
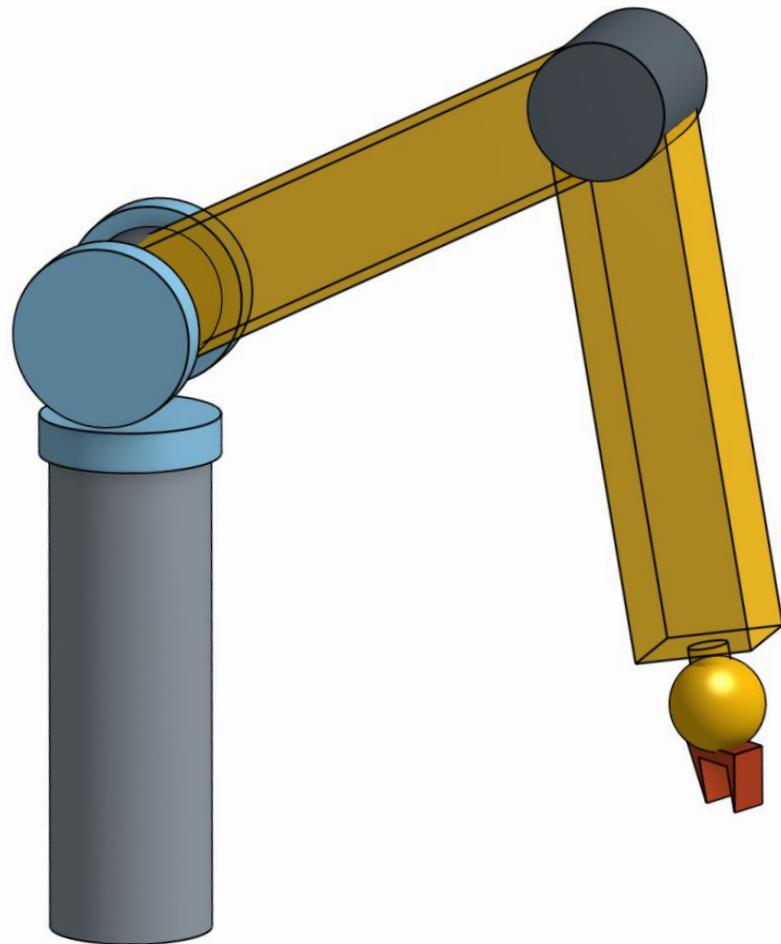
$$\theta_1 = \text{atan}2(P_y, P_x)$$

$$\theta_2 = \text{atan}2\left(\sqrt{P_x^2 + P_y^2}, P_z\right)$$

$$d_3 = \sqrt{P_x^2 + P_y^2 + P_z^2}$$

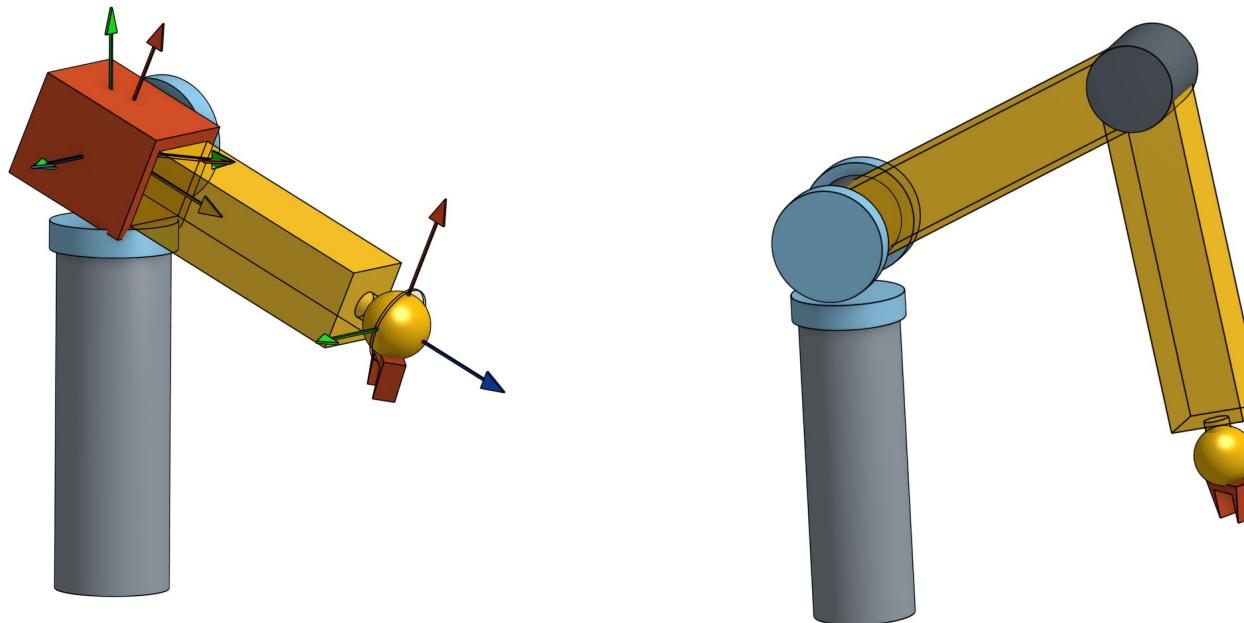


Inv. Pos. Articulated (RRR)

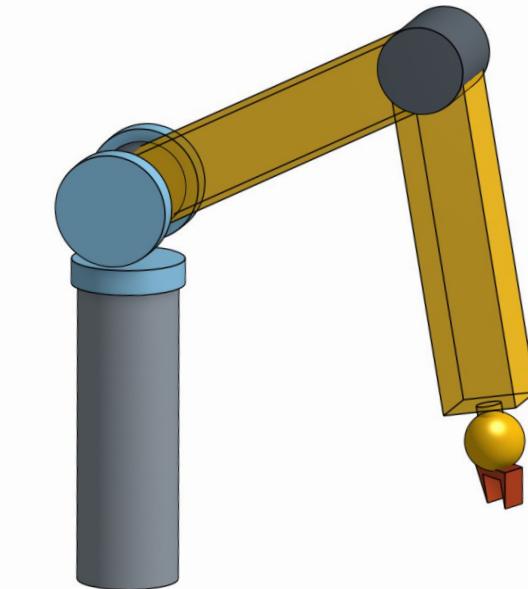
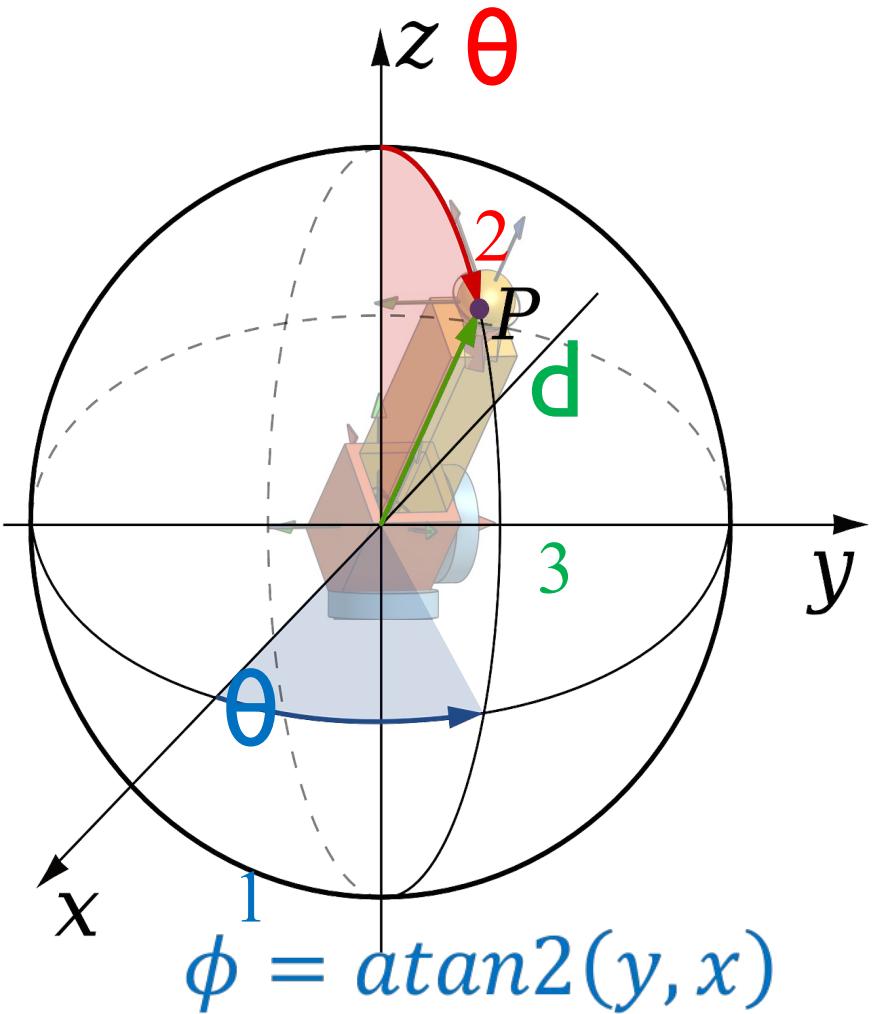


Inv. Pos. Articulated (RRR)

[insert videos here running next
To each other simultaneously]

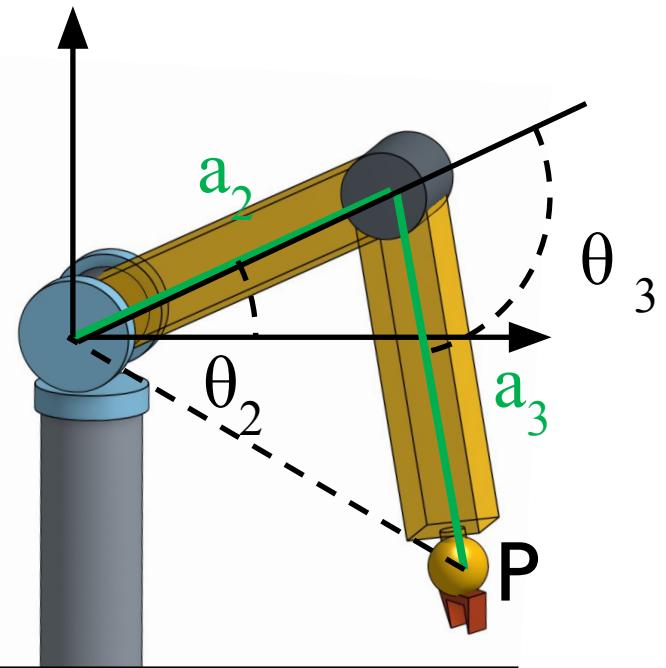


Inv. Pos. Articulated (RRR)



$$\theta_1 = \text{atan}2(y, x)$$

Inv. Pos. Articulated (RRR)



$$\theta_1 = \text{atan2}(P_y, P_x)$$

$$\theta_2 = \text{atan2}(P_y, P_x) - \text{atan2}(a_3 s_3, a_2 + a_3 c_3)$$

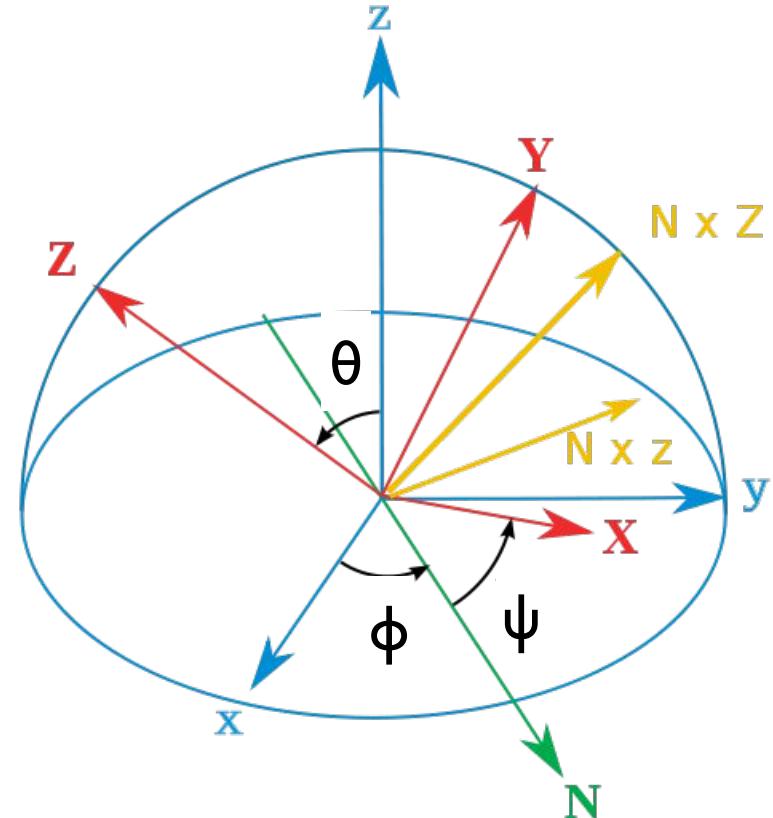
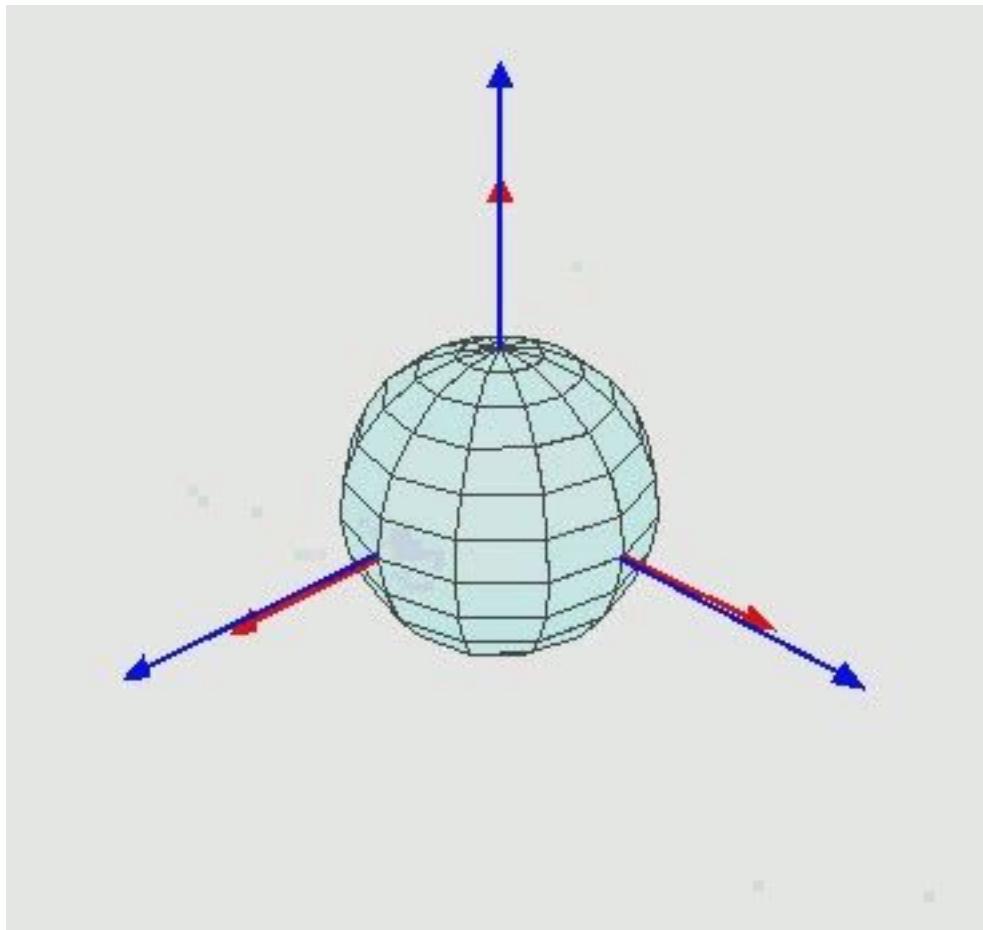
$$\theta_3 = \pm \cos^{-1} \left(\frac{P_x^2 + P_y^2 - (a_2^2 + a_3^2)}{2a_2 a_3} \right)$$

Robotics: Fundamentals

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Week 6: Spherical Wrist and Inverse Orientation

Sequential Rotations



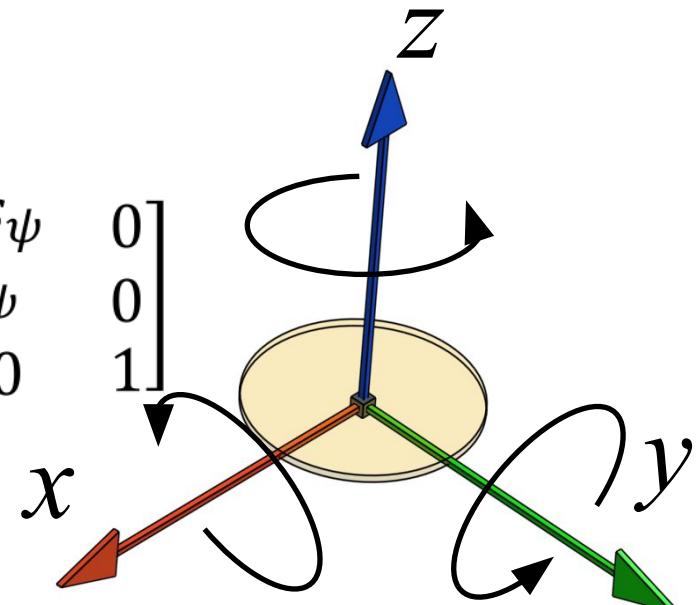
By Euler2.gif: Juansemperederivative work: Xavax -
This file was derived from Euler2.gif;, CC BY-SA 3.0,

By Juansemper - Own work, GFDL,

Euler Angle Rotation

$$R_{01} = R_{Z,\phi} R_{Y,\theta} R_{Z,\psi}$$

$$= \begin{bmatrix} c_\phi & -s_\phi & 0 \\ s_\phi & c_\phi & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} c_\theta & 0 & s_\theta \\ 0 & 1 & 0 \\ -s_\theta & 0 & c_\theta \end{bmatrix} \begin{bmatrix} c_\psi & -s_\psi & 0 \\ s_\psi & c_\psi & 0 \\ 0 & 0 & 1 \end{bmatrix}$$



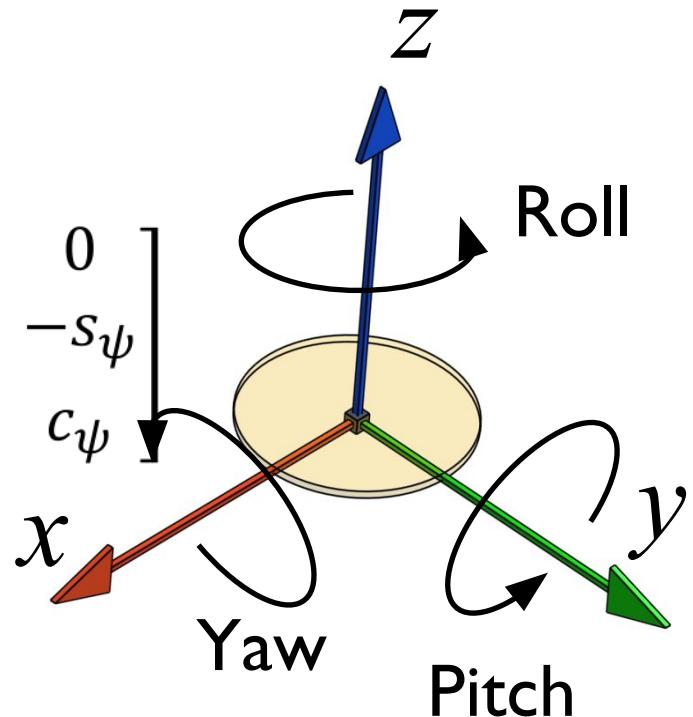
$$= \begin{bmatrix} c_\phi c_\theta c_\psi - s_\phi s_\psi & -c_\phi c_\theta s_\psi - s_\theta c_\psi & c_\phi s_\theta \\ s_\phi c_\theta c_\psi + c_\phi s_\psi & -s_\phi c_\theta s_\psi + c_\phi c_\psi & s_\phi s_\theta \\ -s_\theta c_\psi & s_\theta s_\psi & c_\theta \end{bmatrix}$$

Roll Pitch Yaw Rotation

$$R_{01} = R_{Z,\phi} R_{Y,\theta} R_{X,\psi}$$

$$= \begin{bmatrix} c_\phi & -s_\phi & 0 \\ s_\phi & c_\phi & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} c_\theta & 0 & s_\theta \\ 0 & 1 & 0 \\ -s_\theta & 0 & c_\theta \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 \\ 0 & c_\psi & s_\psi \\ 0 & s_\psi & c_\psi \end{bmatrix}$$

$$= \begin{bmatrix} c_\phi c_\theta & -s_\phi c_\psi + c_\phi s_\theta s_\psi & s_\phi s_\psi + c_\phi s_\theta c_\psi \\ s_\phi c_\theta & c_\phi c_\psi + s_\phi s_\psi s_\theta & -c_\phi s_\psi + s_\phi s_\theta c_\psi \\ -s_\theta & c_\theta s_\psi & c_\theta c_\psi \end{bmatrix}$$



12 possible orderings

Proper Euler angles

$$X_1 Z_2 X_3 = \begin{bmatrix} c_2 & -c_3 s_2 & s_2 s_3 \\ c_1 s_2 & c_1 c_2 c_3 - s_1 s_3 & -c_3 s_1 - c_1 c_2 s_3 \\ s_1 s_2 & c_1 s_3 + c_2 c_3 s_1 & c_1 c_3 - c_2 s_1 s_3 \end{bmatrix}$$

$$X_1 Y_2 X_3 = \begin{bmatrix} c_2 & s_2 s_3 & c_3 s_2 \\ s_1 s_2 & c_1 c_3 - c_2 s_1 s_3 & -c_1 s_3 - c_2 c_3 s_1 \\ -c_1 s_2 & c_3 s_1 + c_1 c_2 s_3 & c_1 c_2 c_3 - s_1 s_3 \end{bmatrix}$$

$$Y_1 X_2 Y_3 = \begin{bmatrix} c_1 c_3 - c_2 s_1 s_3 & s_1 s_2 & c_1 s_3 + c_2 c_3 s_1 \\ s_2 s_3 & c_2 & -c_3 s_2 \\ -c_3 s_1 - c_1 c_2 s_3 & c_1 s_2 & c_1 c_2 c_3 - s_1 s_3 \end{bmatrix}$$

$$Y_1 Z_2 Y_3 = \begin{bmatrix} c_1 c_2 c_3 - s_1 s_3 & -c_1 s_2 & c_3 s_1 + c_1 c_2 s_3 \\ c_3 s_2 & c_2 & s_2 s_3 \\ -c_1 s_3 - c_2 c_3 s_1 & s_1 s_2 & c_1 c_3 - c_2 s_1 s_3 \end{bmatrix}$$

$$Z_1 Y_2 Z_3 = \begin{bmatrix} c_1 c_2 c_3 - s_1 s_3 & -c_3 s_1 - c_1 c_2 s_3 & c_1 s_2 \\ c_1 s_3 + c_2 c_3 s_1 & c_1 c_3 - c_2 s_1 s_3 & s_1 s_2 \\ -c_3 s_2 & s_2 s_3 & c_2 \end{bmatrix}$$

$$Z_1 X_2 Z_3 = \begin{bmatrix} c_1 c_3 - c_2 s_1 s_3 & -c_1 s_3 - c_2 c_3 s_1 & s_1 s_2 \\ c_3 s_1 + c_1 c_2 s_3 & c_1 c_2 c_3 - s_1 s_3 & -c_1 s_2 \\ s_2 s_3 & c_3 s_2 & c_2 \end{bmatrix}$$

Tait-Bryan angles

$$X_1 Z_2 Y_3 = \begin{bmatrix} c_2 c_3 & -s_2 & c_2 s_3 \\ s_1 s_3 + c_1 c_3 s_2 & c_1 c_2 & c_1 s_2 s_3 - c_3 s_1 \\ c_3 s_1 s_2 - c_1 s_3 & c_2 s_1 & c_1 c_3 + s_1 s_2 s_3 \end{bmatrix}$$

$$X_1 Y_2 Z_3 = \begin{bmatrix} c_2 c_3 & -c_2 s_3 & s_2 \\ c_1 s_3 + c_3 s_1 s_2 & c_1 c_3 - s_1 s_2 s_3 & -c_2 s_1 \\ s_1 s_3 - c_1 c_3 s_2 & c_3 s_1 + c_1 s_2 s_3 & c_1 c_2 \end{bmatrix}$$

$$Y_1 X_2 Z_3 = \begin{bmatrix} c_1 c_3 + s_1 s_2 s_3 & c_3 s_1 s_2 - c_1 s_3 & c_2 s_1 \\ c_2 s_3 & c_2 c_3 & -s_2 \\ c_1 s_2 s_3 - c_3 s_1 & c_1 c_3 s_2 + s_1 s_3 & c_1 c_2 \end{bmatrix}$$

$$Y_1 Z_2 X_3 = \begin{bmatrix} c_1 c_2 & s_1 s_3 - c_1 c_3 s_2 & c_3 s_1 + c_1 s_2 s_3 \\ s_2 & c_2 c_3 & -c_2 s_3 \\ -c_2 s_1 & c_1 s_3 + c_3 s_1 s_2 & c_1 c_3 - s_1 s_2 s_3 \end{bmatrix}$$

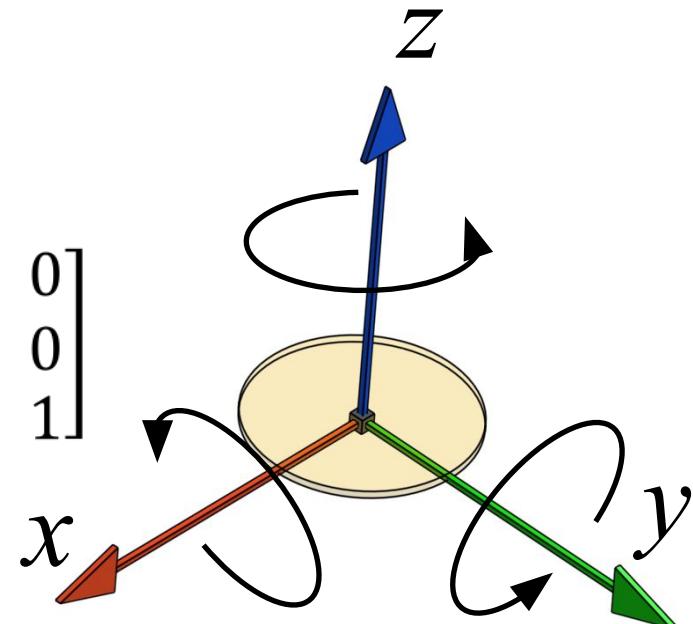
$$Z_1 Y_2 X_3 = \begin{bmatrix} c_1 c_2 & c_1 s_2 s_3 - c_3 s_1 & s_1 s_3 + c_1 c_3 s_2 \\ c_2 s_1 & c_1 c_3 + s_1 s_2 s_3 & c_3 s_1 s_2 - c_1 s_3 \\ -s_2 & c_2 s_3 & c_2 c_3 \end{bmatrix}$$

$$Z_1 X_2 Y_3 = \begin{bmatrix} c_1 c_3 - s_1 s_2 s_3 & -c_2 s_1 & c_1 s_3 + c_3 s_1 s_2 \\ c_3 s_1 + c_1 s_2 s_3 & c_1 c_2 & s_1 s_3 - c_1 c_3 s_2 \\ -c_2 s_3 & s_2 & c_2 c_3 \end{bmatrix}$$

Euler Angle Rotation

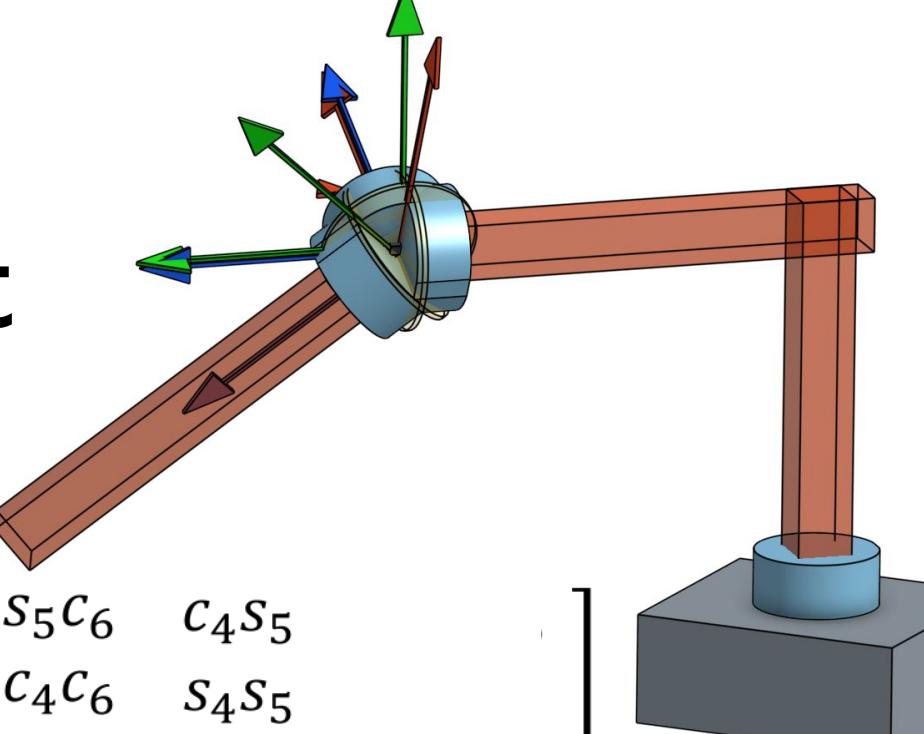
$$R_{01} = R_{Z,\phi} R_{Y,\theta} R_{Z,\psi}$$

$$= \begin{bmatrix} c_\phi & -s_\phi & 0 \\ s_\phi & c_\phi & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} c_\theta & 0 & s_\theta \\ 0 & 1 & 0 \\ -s_\theta & 0 & c_\theta \end{bmatrix} \begin{bmatrix} c_\psi & -s_\psi & 0 \\ s_\psi & c_\psi & 0 \\ 0 & 0 & 1 \end{bmatrix}$$



$$= \begin{bmatrix} c_\phi c_\theta c_\psi - s_\phi s_\psi & -c_\phi c_\theta s_\psi - s_\theta c_\psi & c_\phi s_\theta \\ s_\phi c_\theta c_\psi + c_\phi s_\psi & -s_\phi c_\theta s_\psi + c_\phi c_\psi & s_\phi s_\theta \\ -s_\theta c_\psi & s_\theta s_\psi & c_\theta \end{bmatrix}$$

Euler Angle vs Spherical Wrist



$$T_{36} = \begin{bmatrix} c_4c_5c_6 - s_4s_6 & -c_4c_5s_6 - s_5c_6 & c_4s_5 \\ s_4c_5c_6 + c_4s_6 & -s_4c_5s_6 + c_4c_6 & s_4s_5 \\ -s_5c_6 & s_5s_6 & c_5 \end{bmatrix}$$

$$= \begin{bmatrix} c_\phi c_\theta c_\psi - s_\phi s_\psi & -c_\phi c_\theta s_\psi - s_\theta c_\psi & c_\phi s_\theta \\ s_\phi c_\theta c_\psi + c_\phi s_\psi & -s_\phi c_\theta s_\psi + c_\phi c_\psi & s_\phi s_\theta \\ -s_\theta c_\psi & s_\theta s_\psi & c_\theta \end{bmatrix}$$

$$\theta_4 = \phi, \quad \theta_5 = \theta, \quad \theta_6 = \psi$$

Inverse Orientation (ZYX)

$$T_{36} = \begin{bmatrix} c_4c_5c_6 - s_4s_6 & -c_4c_5s_6 - s_5c_6 & c_4s_5 & c_4s_5d_6 \\ s_4c_5c_6 + c_4s_6 & -s_4c_5s_6 + c_4c_6 & s_4s_5 & s_4s_5d_6 \\ -s_5c_6 & s_5s_6 & c_5 & c_5d_6 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} r_{11} & r_{12} & r_{13} & P_x \\ r_{21} & r_{22} & r_{23} & P_y \\ r_{31} & r_{32} & r_{33} & P_z \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad \begin{aligned} \theta_4 &= ? \\ \theta_5 &= ? \\ \theta_6 &= ? \end{aligned}$$

$$c_5 = r_{33}$$

$$\theta_5 = \pm \cos^{-1}(r_{33})$$

Euler Angle Rotation

$$T_{36} = \begin{bmatrix} c_4 c_5 c_6 - s_4 s_6 & -c_4 c_5 s_6 - s_5 c_6 & c_4 s_5 & c_4 s_5 d_6 \\ s_4 c_5 c_6 + c_4 s_6 & -s_4 c_5 s_6 + c_4 c_6 & s_4 s_5 & s_4 s_5 d_6 \\ -s_5 c_6 & s_5 s_6 & c_5 & c_5 d_6 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} r_{11} & r_{12} & r_{13} & P_x \\ r_{21} & r_{22} & r_{23} & P_y \\ r_{31} & r_{32} & r_{33} & P_z \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad \theta_4 = ?$$

$\theta_5 = \pm \cos^{-1}(r_{33})$

$$\theta_6 = ?$$

$$\text{atan2}(y, x) = \text{atan2}(Cy, Cx), C > 0$$

$$\theta_4 = \text{atan2}(r_{23}, r_{13}), \quad s_5 > 0$$

$$\theta_4 = \text{atan2}(-r_{23}, -r_{13}), \quad s_5 < 0$$

Euler Angle Rotation

$$T_{36} = \begin{bmatrix} c_4c_5c_6 - s_4s_6 & -c_4c_5s_6 - s_5c_6 & c_4s_5 & c_4s_5d_6 \\ s_4c_5c_6 + c_4s_6 & -s_4c_5s_6 + c_4c_6 & s_4s_5 & s_4s_5d_6 \\ -s_5c_6 & s_5s_6 & c_5 & c_5d_6 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} r_{11} & r_{12} & r_{13} & P_x \\ r_{21} & r_{22} & r_{23} & P_y \\ r_{31} & r_{32} & r_{33} & P_z \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$\theta_4 = \text{atan2}(\pm r_{23}, \pm r_{13})$

$\theta_5 = \pm \cos^{-1}(r_{33})$

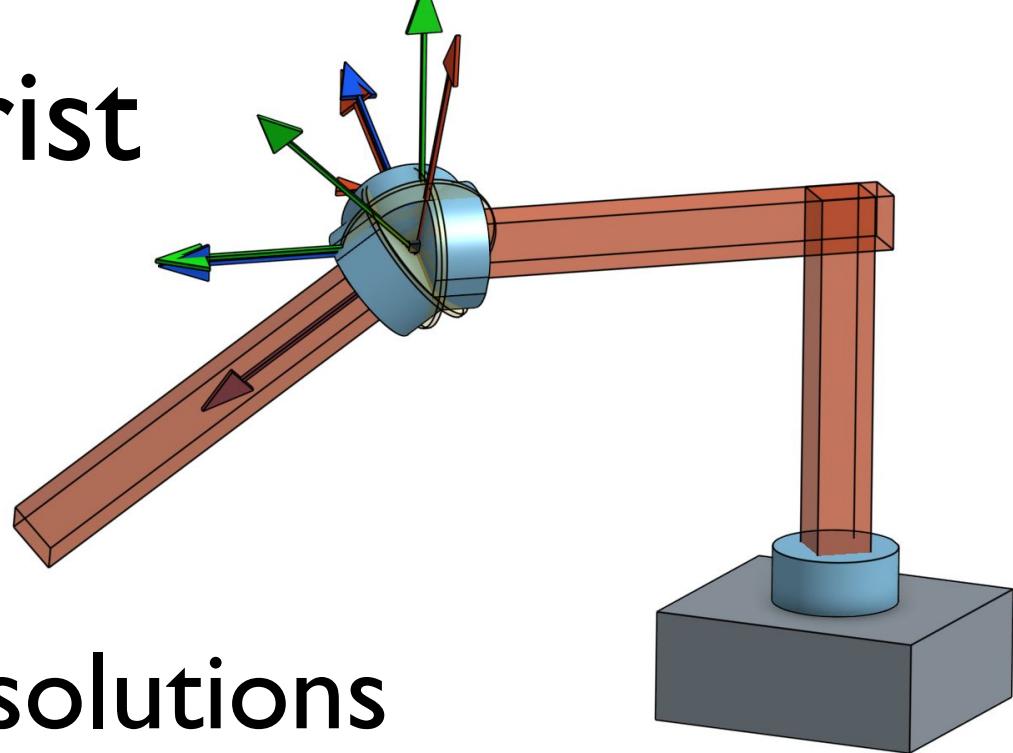
$\theta_6 = ?$

$$\text{atan2}(y, x) = \text{atan2}(Cy, Cx), C > 0$$

$$\theta_6 = \text{atan2}(-r_{31}, r_{32}), \quad s_5 > 0$$

$$\theta_6 = \text{atan2}(r_{31}, -r_{32}), \quad s_5 < 0$$

Spherical Wrist (ZYX)



Two solutions

$$\theta_4 = \text{atan}2(r_{23}, r_{13})$$

$$\theta_5 = \cos^{-1}(r_{33})$$

$$\theta_6 = \text{atan}2(r_{32}, -r_{31})$$

$$\theta_4 = \text{atan}2(-r_{23}, -r_{13})$$

$$\theta_5 = -\cos^{-1}(r_{33})$$

$$\theta_6 = \text{atan}2(-r_{32}, r_{31})$$

Inverse Pos. + Ori. For P_c

- From Inverse Position we have the joint variables $q_{1\dots 3}$ for $T_{03} = \begin{bmatrix} R_{03} & P_c \\ 0 & 1 \end{bmatrix}$
- From Inverse Orientation we have the joint variables $q_{4\dots 6}$ for a given arbitrary R
- Can we put the two together to solve our initial problem for 6DOF?

$$T_{06}(q_1 \dots q_6) = H$$

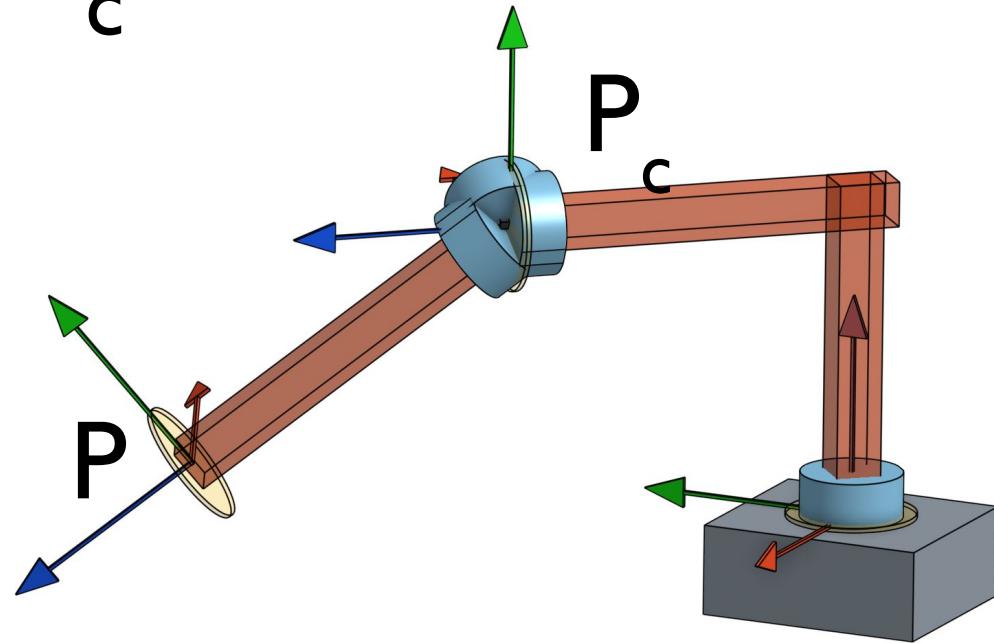
Offset from P_c wrist center

$$H = \begin{bmatrix} R & P \\ 0 & 1 \end{bmatrix}$$

$$P_c = P - d_6 \hat{k}$$

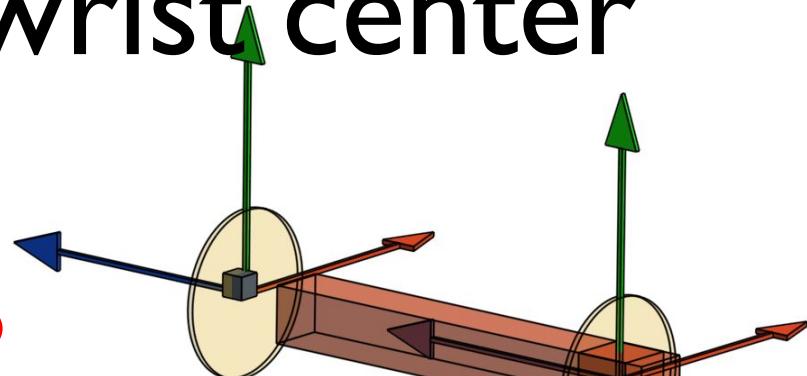
$$\begin{bmatrix} P_{cx} \\ P_{cy} \\ P_{cz} \end{bmatrix} = \begin{bmatrix} P_x - d_6 r_{13} \\ P_y - d_6 r_{23} \\ P_z - d_6 r_{33} \end{bmatrix}$$

$$H_c = \begin{bmatrix} R & P - d_6 \hat{k} \\ 0 & 1 \end{bmatrix} = \begin{bmatrix} [R] & P_x - d_6 r_{13} \\ [0 & 0 & 0] & P_y - d_6 r_{23} \\ & P_z - d_6 r_{33} \\ & 1 \end{bmatrix}$$

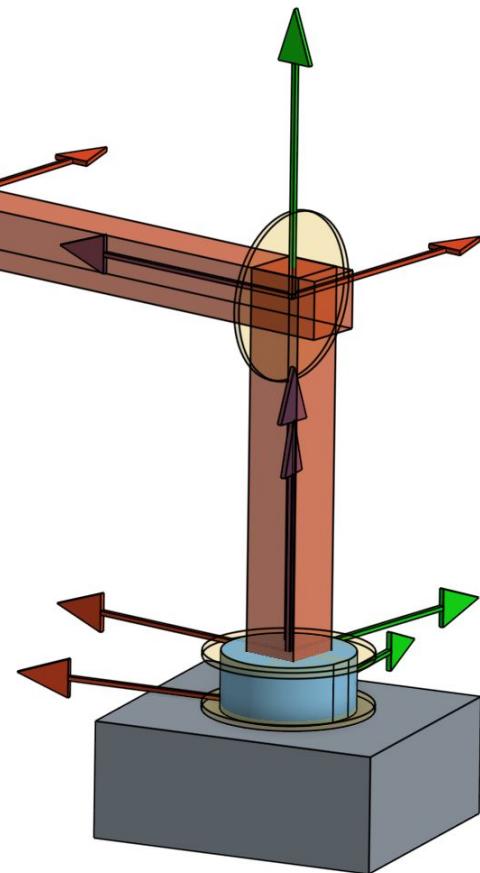


Offset from P wrist center

$$H_c = \begin{bmatrix} [R] & P_x - d_6 r_{13} \\ [0 \ 0 \ 0] & P_y - d_6 r_{23} \\ & P_z - d_6 r_{33} \end{bmatrix}$$



$$T_{03} = \begin{bmatrix} c_1 & 0 & -s_1 & -s_1 d_3 \\ s_1 & 0 & c_1 & c_1 d_3 \\ 0 & -1 & 0 & d_1 + d_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



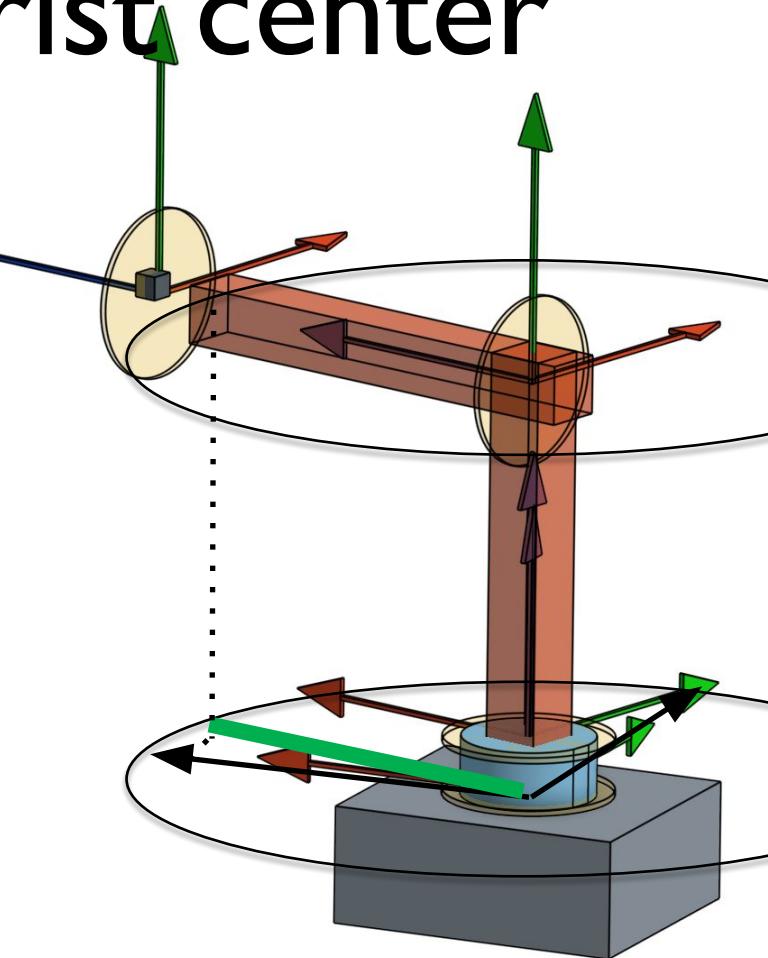
$$d_2 = P_z - d_6 r_{33} - d_1$$

Offset from P wrist center

$$H_c = \begin{bmatrix} [R] \\ [0 \quad 0 \quad 0] & 1 \\ P_x - d_6 r_{13} \\ P_y - d_6 r_{23} \\ P_z - d_6 r_{33} \end{bmatrix}$$

$$T_{03} = \begin{bmatrix} c_1 & 0 & -s_1 & -s_1 d_3 \\ s_1 & 0 & c_1 & c_1 d_3 \\ 0 & -1 & 0 & d_1 + d_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$d_3 = \sqrt{x^2 + y^2}$$



$$d_3 = \sqrt{(P_y - d_6 r_{23})^2 + (P_x - d_6 r_{13})^2}$$

Offset from P wrist center

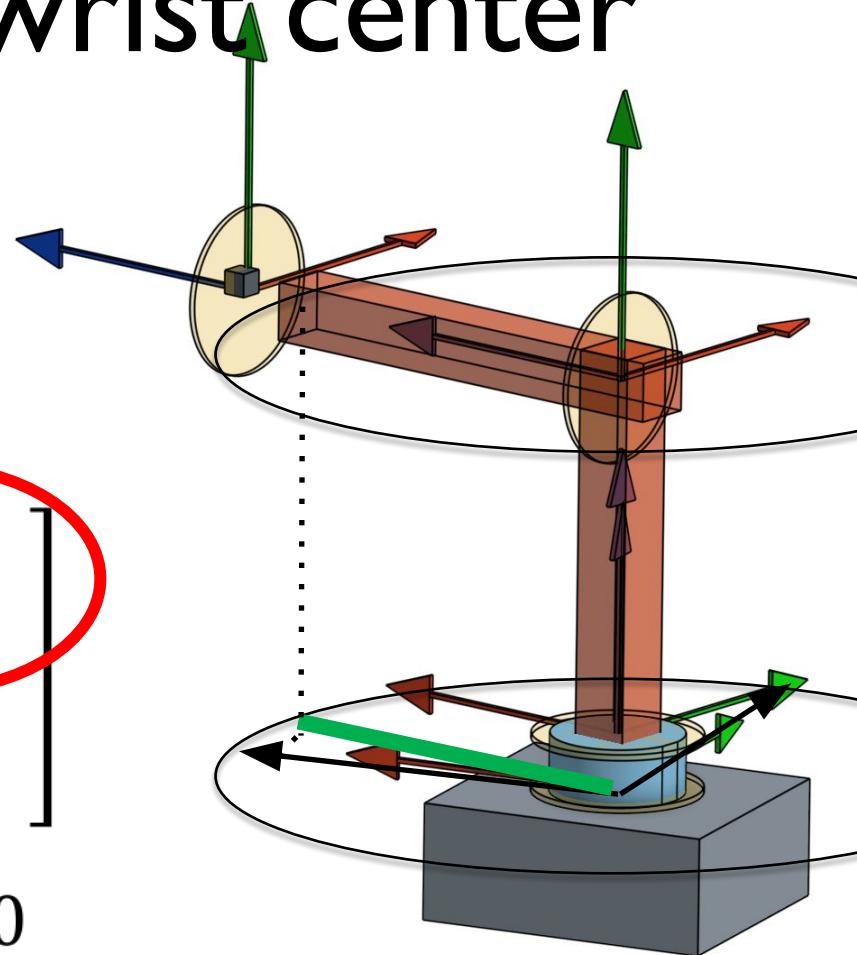
$$H_c = \begin{bmatrix} [R] \\ [0 \quad 0 \quad 0] & 1 \\ P_x - d_6 r_{13} \\ P_y - d_6 r_{23} \\ P_z - d_6 r_{33} \end{bmatrix}$$

$$T_{03} = \begin{bmatrix} c_1 & 0 & -s_1 & -s_1 d_3 \\ s_1 & 0 & c_1 & c_1 d_3 \\ 0 & -1 & 0 & d_1 + d_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\theta_1 = \text{atan2}(C \sin, C \cos), C > 0$$

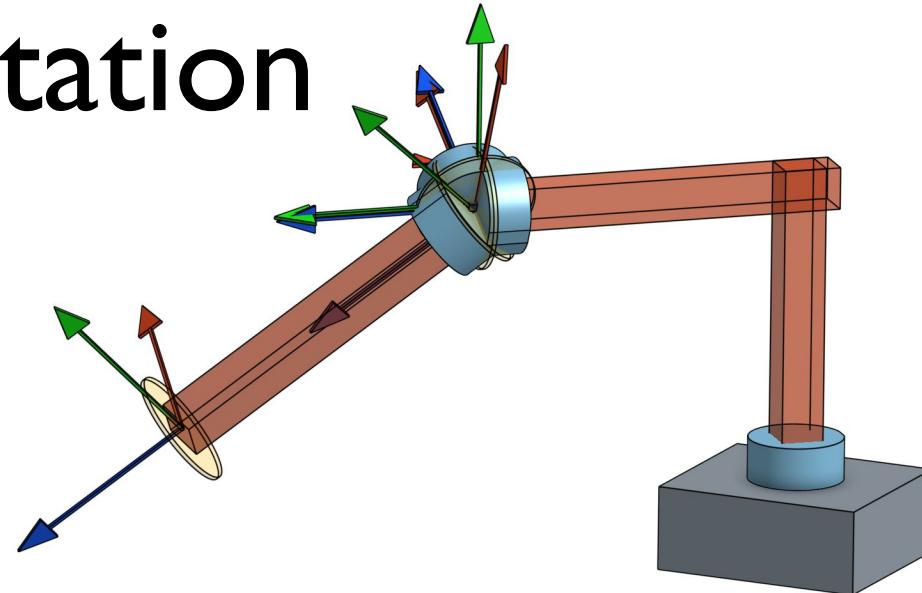
$$\boxed{\theta_1 = \text{atan2}(-(P_x - d_6 r_{13}), P_y - d_6 r_{23}), d_3 > 0}$$

$$\boxed{\theta_1 = \text{atan2}(P_x - d_6 r_{13}, -P_y + d_6 r_{23}), d_3 < 0}$$



Inverse Orientation

$$H_c = \begin{bmatrix} [R] & [P - d_6 \hat{k}] \\ [0] & 1 \end{bmatrix}$$



Spherical Wrist solution for R ?

$$\theta_4 = \text{atan2}(\pm r_{23}, \pm r_{13})$$

$$\theta_5 = \pm \cos^{-1} (r_{33})$$

$$\theta_6 = \text{atan2}(\mp r_{31}, \pm r_{32})$$

Inverse Orientation

$$H_c = \begin{bmatrix} [R] & [P - d_6 \hat{k}] \\ [0] & 1 \end{bmatrix}$$

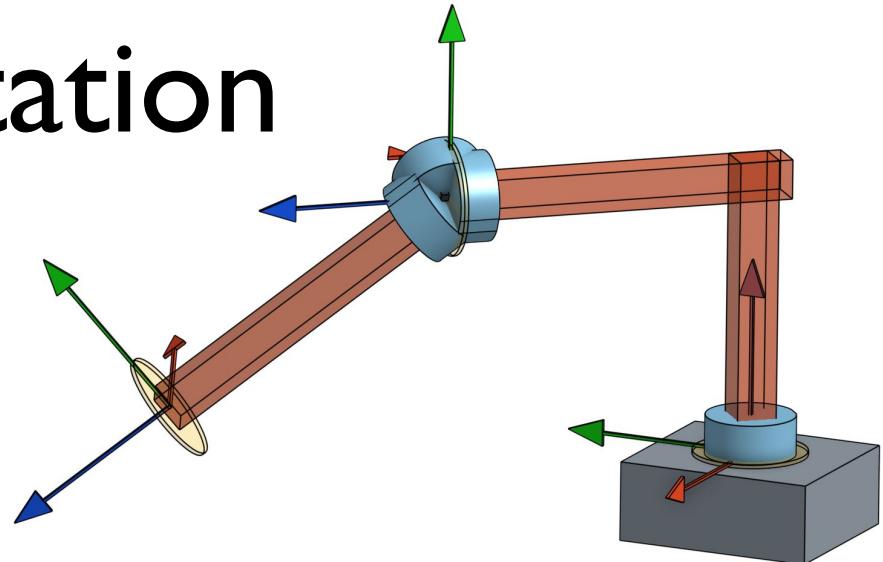
$$T_{06} = \begin{bmatrix} [R_{03}][R_{36}] & P_c \\ [0] & 1 \end{bmatrix}$$

$$R_{06} = R_{03}R_{36} = R$$

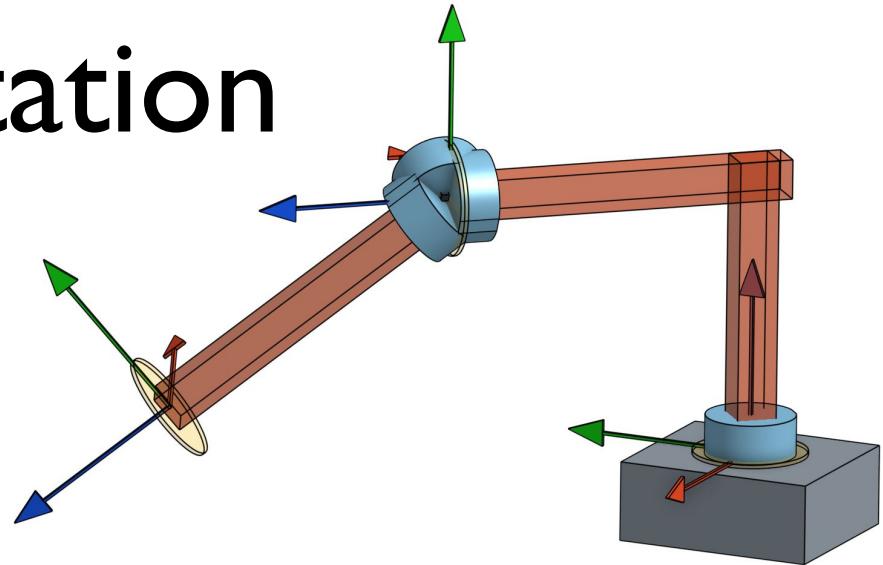
$$R_{36} = (R_{03})^{-1}R$$

$$R_{36} = (R_{03})^T R$$

$$T_{03} = \begin{bmatrix} c_1 & 0 & -s_1 & -s_1 d_3 \\ s_1 & 0 & c_1 & c_1 d_3 \\ 0 & -1 & 0 & d_1 + d_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



Inverse Orientation



$$R_{36} = \begin{bmatrix} c_1 r_{11} + s_1 r_{21} & c_1 r_{12} + s_1 r_{22} & c_1 r_{13} + s_1 r_{23} \\ -r_{31} & -r_{32} & -r_{33} \\ c_1 r_{21} - s_1 r_{11} & c_1 r_{22} - s_1 r_{12} & c_1 r_{23} - s_1 r_{13} \end{bmatrix}$$

$$R_{36} = (R_{03})^T R$$

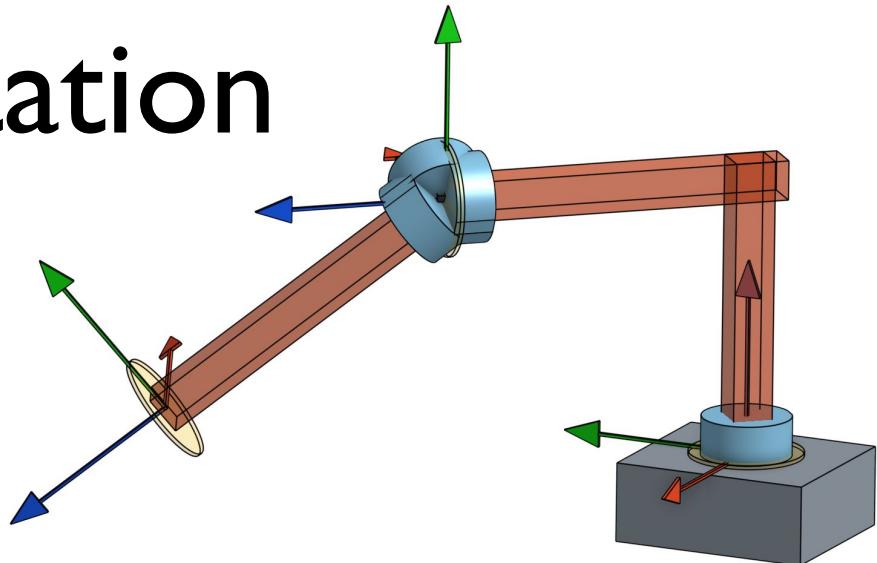
$$T_{03} = \begin{bmatrix} c_1 & 0 & -s_1 & -s_1 d_3 \\ s_1 & 0 & c_1 & c_1 d_3 \\ 0 & -1 & 0 & d_1 + d_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Inverse Orientation

$$\theta_4 = \text{atan2}(r_{23}, r_{13})$$

$$\theta_5 = \pm \cos^{-1}(r_{33})$$

$$\theta_6 = \text{atan2}(-r_{31}, r_{32})$$



$$R_{36} = \begin{bmatrix} c_1 r_{11} + s_1 r_{21} & c_1 r_{12} + s_1 r_{22} & c_1 r_{13} + s_1 r_{23} \\ -r_{31} & -r_{32} & -r_{33} \\ c_1 r_{21} - s_1 r_{11} & c_1 r_{22} - s_1 r_{12} & c_1 r_{23} - s_1 r_{13} \end{bmatrix}$$

$$\boxed{\theta_4 = \text{atan2}(-r_{33}, c_1 r_{13} + s_1 r_{23})}$$

$$\boxed{\theta_5 = \pm \cos^{-1}(c_1 r_{23} - s_1 r_{13})}$$

$$\boxed{\theta_6 = \text{atan2}(\pm(s_1 r_{11} - c_1 r_{21}), \pm(c_1 r_{22} - s_1 r_{12}))}$$

IK for Cylindrical RPP

2 soln {

$$\theta_1 = \text{atan2}(\mp(P_x - d_6 r_{13}), \pm(P_y - d_6 r_{13}))$$
$$d_2 = P_z - d_6 r_{33}$$
$$d_3 = \sqrt{(P_y - d_6 r_{23})^2 + (P_x - d_6 r_{13})^2}$$

2 soln {

$$\theta_4 = \text{atan2}(\mp r_{33}, \pm c_1 r_{13} \pm s_1 r_{23})$$
$$\theta_5 = \pm \cos^{-1}(c_1 r_{23} - s_1 r_{13})$$
$$\theta_6 = \text{atan2}(\pm(s_1 r_{11} - c_1 r_{21}), \pm(c_1 r_{22} - s_1 r_{12}))$$

Robotics: Fundamentals

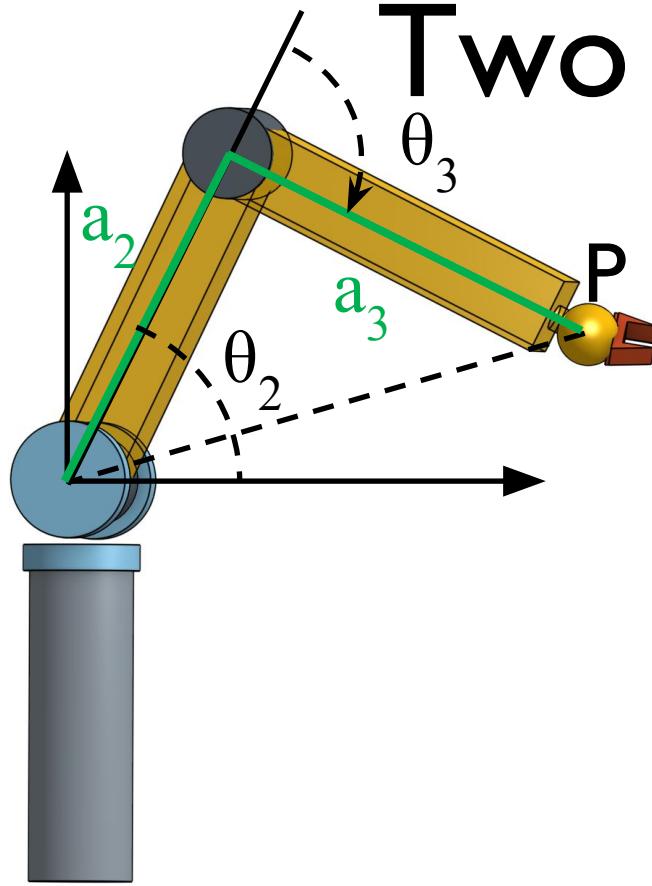
Prof. Mark Yim
University of Pennsylvania

Week 6: Multiple Inverse Kinematic Solutions

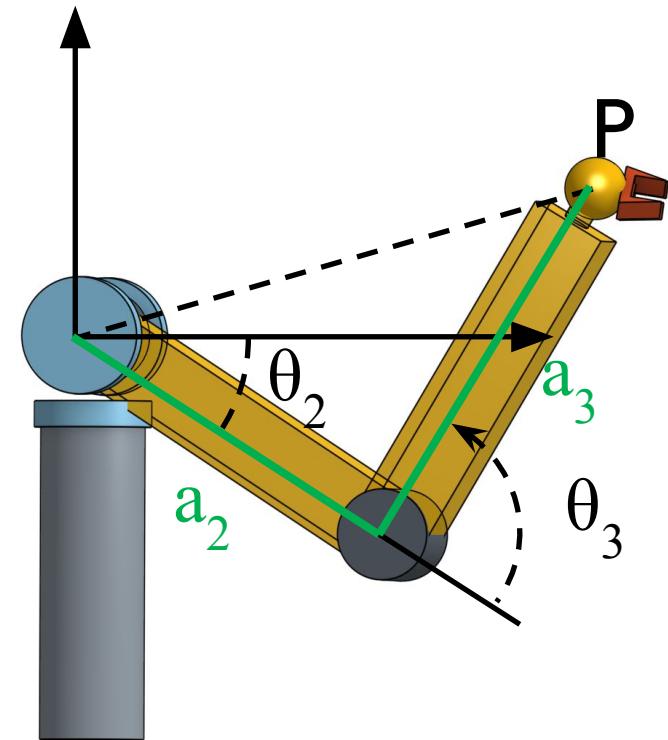
Special cases

- Multiple solutions
- Gimbal lock
- Representation singularity
- Joint singularity
- Dextrous workspace

Two solutions

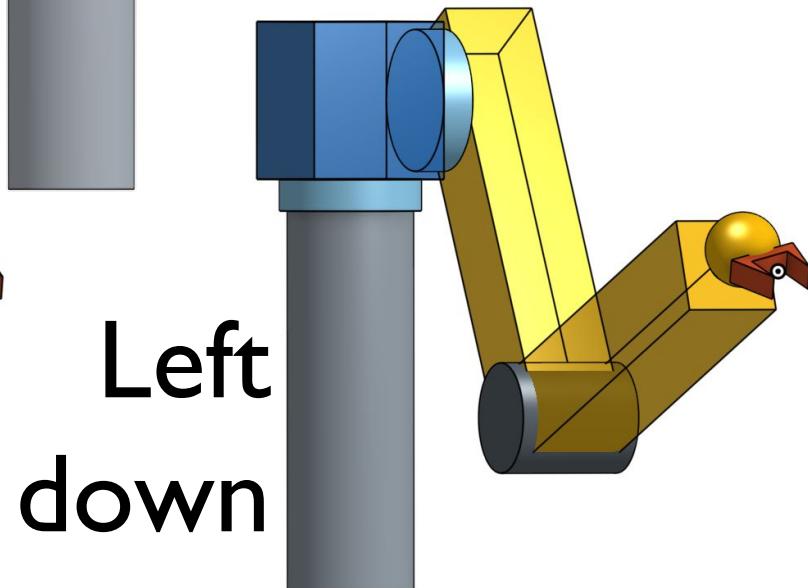
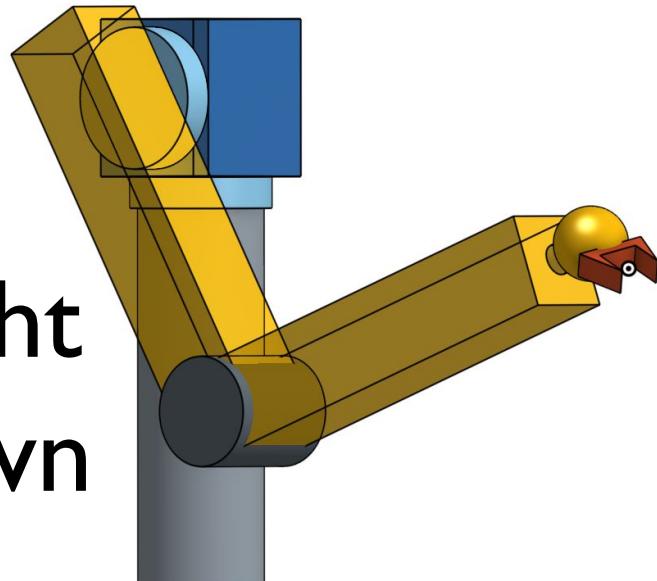
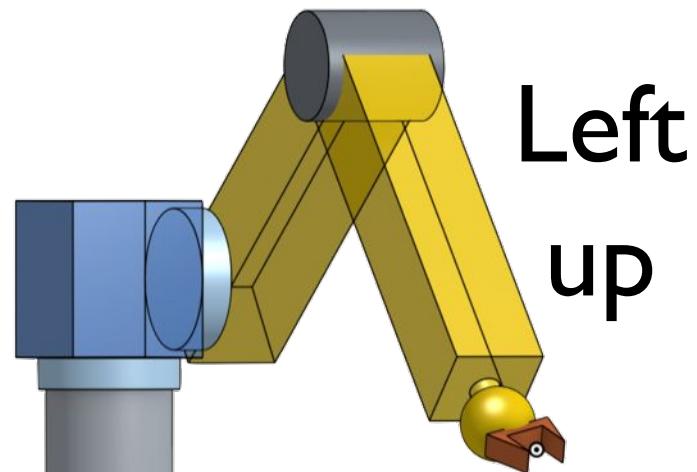
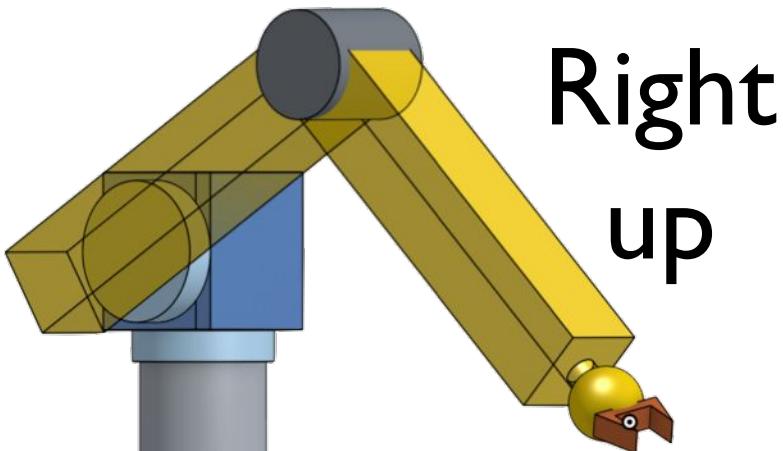


Positive θ_3



Negative θ_3

Four Solutions to 6R robot



Wrist multiple solution

$$\theta_4 = \text{atan2}(\mp r_{33}, \pm c_1 r_{13} \pm s_1 r_{23})$$

$$\theta_5 = \pm \cos^{-1}(c_1 r_{23} - s_1 r_{13})$$

$$\theta_6 = \text{atan2}(\pm(s_1 r_{11} - c_1 r_{21}), \pm(c_1 r_{22} - s_1 r_{12}))$$

$$\theta_4 = \text{atan2}(-r_{33}, c_1 r_{13} + s_1 r_{23}) - \pi$$

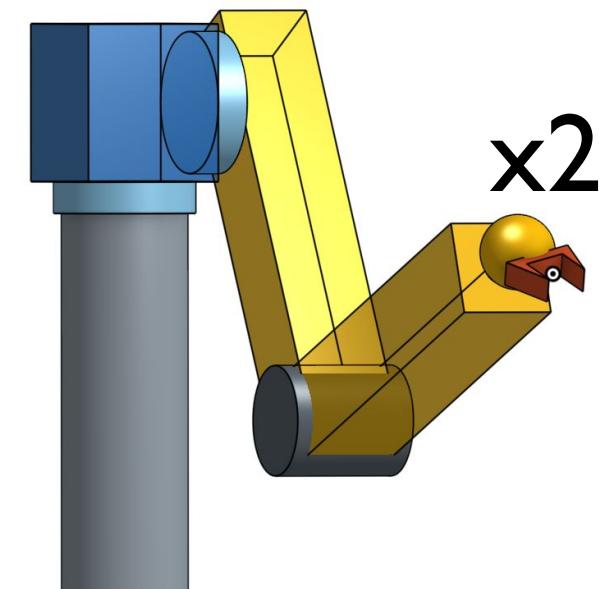
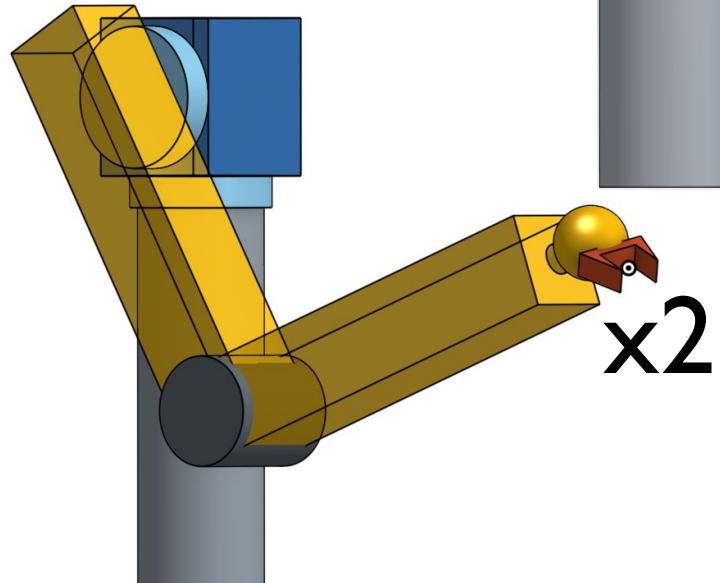
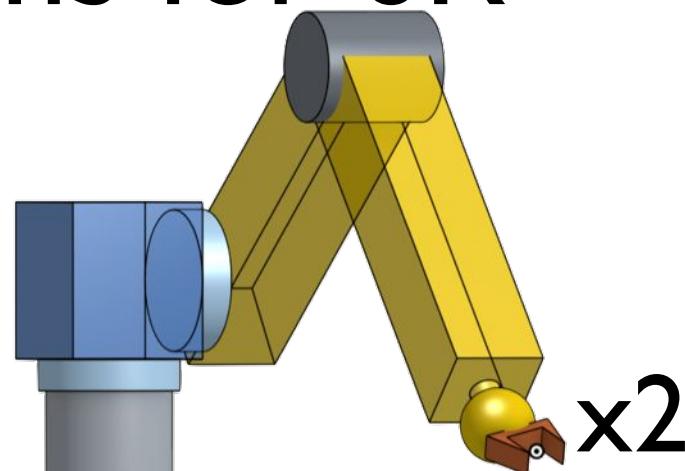
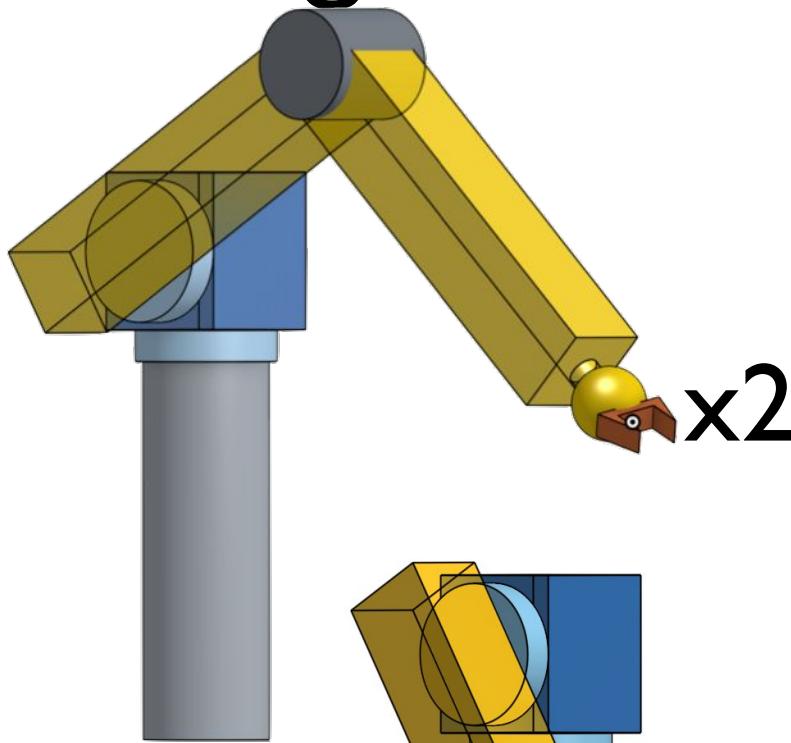
$$\theta_5 = \cos^{-1}(c_1 r_{23} - s_1 r_{13}) * (-1)$$

$$\theta_6 = \text{atan2}(s_1 r_{11} - c_1 r_{21}, c_1 r_{22} - s_1 r_{12}) - \pi$$

1st solution

2nd solution

Eight Solutions for 6R



Infinite solutions

$$\theta_5 = 0,$$
$$\psi = \theta_4 + \theta_6$$

Two Solutions

$$\theta_4 = \text{atan}2(r_{23}, r_{13})$$

$$\theta_5 = \cos^{-1}(r_{33})$$

$$\theta_6 = \text{atan}2(-r_{31}, r_{32})$$

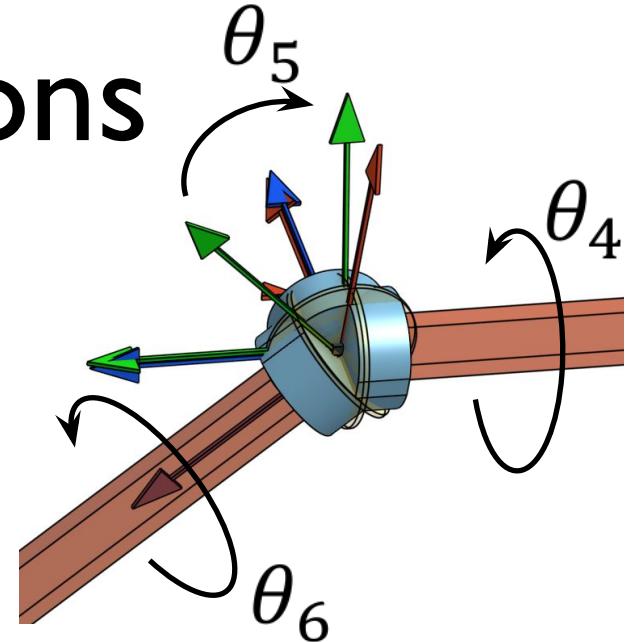
$$s_5 > 0$$

$$\theta_4 = \text{atan}2(-r_{23}, -r_{13})$$

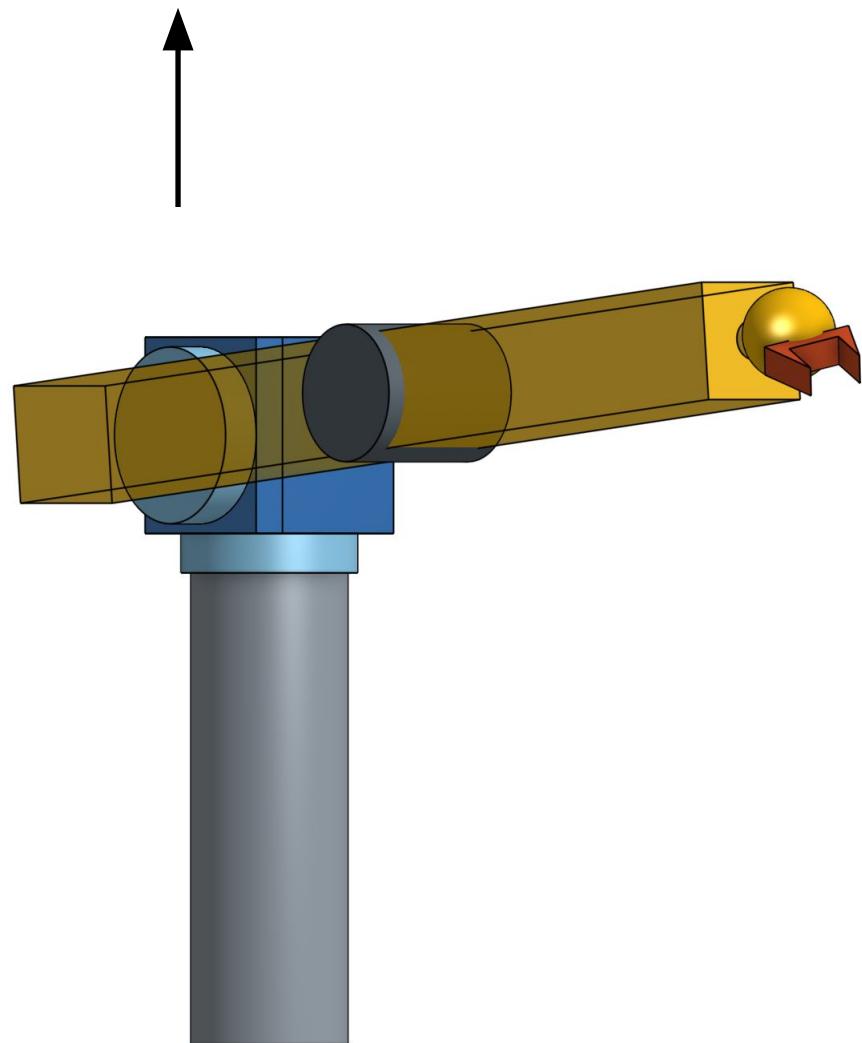
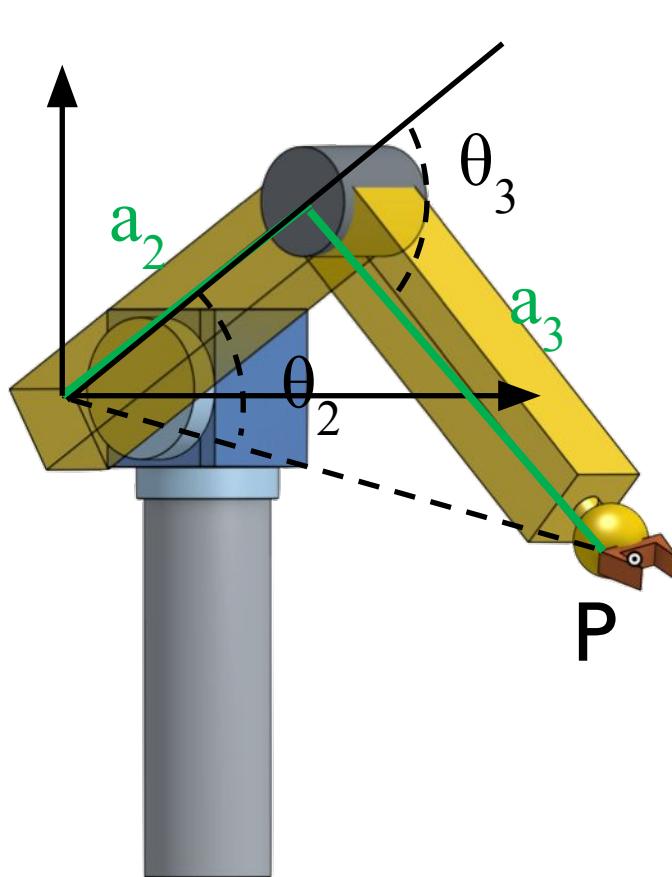
$$\theta_5 = -\cos^{-1}(r_{33})$$

$$\theta_6 = \text{atan}2(r_{31}, -r_{32})$$

$$s_5 < 0$$



Elbow Solutions



Positive θ_3