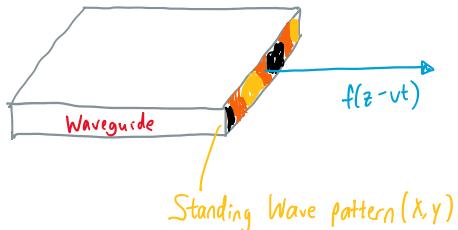


3.2-3.4 Waveguides

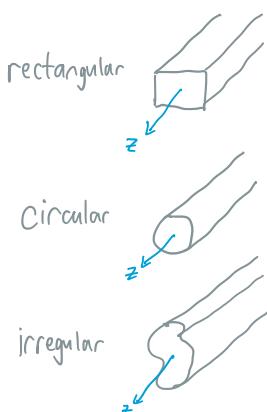
Monday, November 20, 2023 10:04 PM

Fields Formulation

- Waves in a waveguide: cross-section components & travelling component
- Cross-section components are standing waves, denoted as **Standing wave pattern (x, y)**
- Travelling component travelling down \hat{z} , denoted as $f(z-vt)$



Building a Waveguide



$$\vec{E} = \vec{E}_\perp + \hat{z} E_z, \quad \vec{H} = \vec{H}_\perp + \hat{z} H_z$$

$$\vec{\nabla} = \vec{\nabla}_\perp + \hat{z} \frac{\partial}{\partial z}$$

$$\vec{\nabla} \times \vec{E} = (\vec{\nabla}_\perp + \hat{z} \frac{\partial}{\partial z}) \times (\vec{E}_\perp + \hat{z} E_z) = -j\omega\mu (\vec{H}_\perp + \hat{z} H_z) \quad \textcircled{A}$$

$$\vec{\nabla} \times \vec{H} = (\vec{\nabla}_\perp + \hat{z} \frac{\partial}{\partial z}) \times (\vec{H}_\perp + \hat{z} H_z) = j\omega\epsilon (\vec{E}_\perp + \hat{z} E_z) \quad \textcircled{B}$$

$$(\vec{\nabla}_\perp \times \hat{z} E_z) + (\hat{z} \frac{\partial}{\partial z} \times \vec{E}_\perp) = -j\omega\mu H_\perp \quad \textcircled{C}$$

$$(\vec{\nabla}_\perp \times \hat{z} H_z) + (\hat{z} \frac{\partial}{\partial z} \times \vec{H}_\perp) = j\omega\epsilon \vec{E}_\perp \quad \textcircled{D}$$

Sub \textcircled{D} to \textcircled{C} looking at transverse — no z direction

$$(\vec{\nabla}_\perp \times \hat{z} E_z) + \left(\hat{z} \frac{\partial}{\partial z} \times \frac{(\vec{\nabla}_\perp \times \hat{z} H_z) + (\hat{z} \frac{\partial}{\partial z} \times \vec{H}_\perp)}{j\omega\epsilon} \right) = -j\omega\mu \vec{H}_\perp$$

$$j\omega\epsilon (\vec{\nabla}_\perp \times \hat{z} E_z) + \frac{\partial}{\partial z} \hat{z} \times \left(\vec{\nabla}_\perp \times \hat{z} H_z + \frac{\partial}{\partial z} \hat{z} \times \vec{H}_\perp \right) = \omega^2 \mu \epsilon \vec{H}_\perp$$

$\hat{z} \times \vec{H}_\perp$ replace with jk_2

BAC-CAB

$$\hat{z} \times (\vec{\nabla}_\perp \times \hat{z}) = \vec{\nabla}_\perp \left(\hat{z} \cdot \hat{z} \right) - \hat{z} \left(\vec{\nabla}_\perp \cdot \hat{z} \right) = \vec{\nabla}_\perp$$

$$\hat{z} \times (\hat{z} \times \vec{H}_\perp) = \hat{z} \left(\hat{z} \cdot \vec{H}_\perp \right) - \vec{H}_\perp \left(\hat{z} \cdot \hat{z} \right) = -\vec{H}_\perp$$

Equating z components from \textcircled{A} and \textcircled{B}

Equating z components from \textcircled{A} and \textcircled{B}

$$\vec{\nabla}_\perp \times \vec{E}_\perp = -j\omega\mu H_z \hat{z} \quad \textcircled{E}$$

$$\vec{\nabla}_\perp \times \vec{H}_\perp = j\omega\epsilon E_z \hat{z} \quad \textcircled{F}$$

Sub $\vec{E}_\perp + \vec{H}_\perp$ into \textcircled{E} and \textcircled{F} to get: (Helmholtz Equation)

$$[\nabla_\perp^2 + (k^2 - k_z^2)] H_z = 0 \quad \text{TE Waves}$$

$$[\nabla_\perp^2 + (k^2 - k_z^2)] E_z = 0 \quad \text{TM Waves}$$

$\text{TE: } H_z = e^{-jk_z z} f(x, y)$

$$f(x, y) = (A \cos k_x x + \beta \sin k_x x) \cdot (C \cos k_y y + D \sin k_y y)$$

(see in-class 11-29-2023 \textcircled{S})

$\text{@ } x=0, x=a, E_y = 0 \rightarrow E_y \propto \frac{\partial H_z}{\partial x} = 0$

along (tangential to) the side wall
See in-class 11-29-2023 \textcircled{S}

$\text{@ } x=0 \quad B \text{ must be } 0$

$\text{@ } x=a \quad -A \sin k_x a = 0$

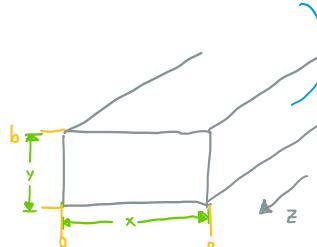
sides are perfect conductors by Coulomb's Law

$$E_x = \frac{\partial H_z}{\partial y} = 0$$

$$\text{@ } y=0, D=0$$

$$\text{@ } y=b, k_y = \frac{n\pi}{b}, n \in \mathbb{Z}$$

(see in-class 12-06-2023 \textcircled{S})



> If A is 0, everything becomes 0. So

$$A \neq 0, k_x = \frac{m\pi}{a}, k_y = \frac{n\pi}{b}, m, n \in \mathbb{Z}$$

$$\text{TE: } H_z = G \cos k_x x \cos k_y y e^{-jk_z z}$$

$$k_x = \frac{m\pi}{a} \quad k_y = \frac{n\pi}{b}$$

$$k_x^2 + k_y^2 + k_z^2 = ? = k^2 = \omega^2 \mu \epsilon \rightarrow \text{a sphere}$$

k_z depends on geometry. But there is a square root, so k_z can be imaginary. So we won't have energy going down the waveguide. Cutoff

Q1 BAC-CAB Rule is a way of decoupling rotations. True

Q2 Components of \vec{E} tangential to the surface of the waveguide must vanish. True

Cutoff

Cutoff

$$k_x^2 + k_y^2 + k_z^2 = k^2 = \omega^2 \mu \epsilon = \frac{\omega^2}{v^2} , v = \frac{c}{n}$$

$$k_z = \sqrt{\frac{\omega^2 n^2}{c^2} - \left(\frac{m\pi}{a}\right)^2 - \left(\frac{n\pi}{b}\right)^2}$$

At $k_z = 0$
no propagation

CUT-OFF

$$\omega_{c,mn} = \frac{c}{n} \sqrt{\left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2}$$

$$\lambda_{c,mn} = \frac{v}{f_{c,mn}} = \frac{c}{n} \frac{2\pi}{\omega_{c,mn}}$$

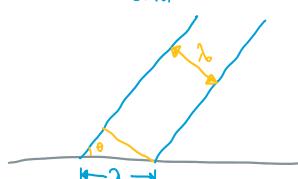
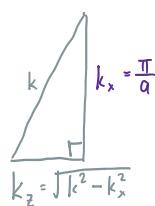
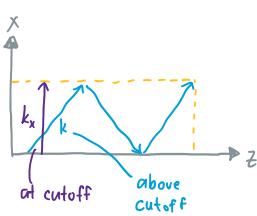
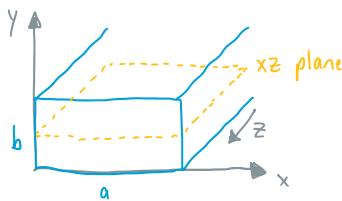
[comes from the source]

Interpretation of Cutoff

Example: $TE_{10} [m=1, n=0]$ dominant mode ($k_z = \sqrt{\omega^2 \mu \epsilon - k_x^2}$ where $k_x = \frac{m\pi}{a}$)

$$\begin{aligned} \text{Along guide, } \lambda_g &= \frac{2\pi}{k_z} = \frac{2\pi}{\sqrt{\left(\frac{2\pi f}{c}\right)^2 - \left(\frac{m\pi}{a}\right)^2}} \rightarrow m=1, v=c, \frac{v}{f} = \lambda_0 \\ &= \frac{2\pi}{2\pi \sqrt{\frac{1}{\lambda_0^2} - \left(\frac{1}{2a}\right)^2}} \\ &= \frac{\lambda_0}{\sqrt{1 - \left(\frac{\lambda_0}{2a}\right)^2}} \end{aligned}$$

Recall - Counting wave crests at the beach (2.6)



$$k_z = \sqrt{\omega^2 \mu \epsilon - \left(\frac{m\pi}{a}\right)^2 - \left(\frac{n\pi}{b}\right)^2}$$

$$\lambda_g = \frac{2\pi}{k_z}$$

Apps 1 - TE

$$\text{Phase Velocity: } V_p = \frac{\omega}{k_z} = \frac{\omega}{\sqrt{\omega^2 \mu \epsilon - k_x^2}} \cdot \frac{\frac{1}{\omega \sqrt{\mu \epsilon}}}{\frac{1}{\omega \sqrt{\mu \epsilon}}} \Rightarrow k_x^2 + k_y^2 = \left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2$$

$$V_p = \frac{1}{\sqrt{\mu\epsilon}} \cdot \frac{1}{\sqrt{1 - \frac{k_z^2}{w^2 \mu \epsilon}}} > \frac{1}{\sqrt{\mu\epsilon}} \quad \text{in air: } \frac{1}{\sqrt{\mu_0 \epsilon_0}} = c \quad \text{phase velocity} > c? \text{ Math is correct,}$$

less than 1!

$$\text{Group velocity: } V_g = \frac{dw}{dk_z} = \left(\frac{dk_z}{dw} \right)^{-1} \rightarrow V_p \cdot V_g = \frac{1}{\mu\epsilon} = c^2$$

and not violating Einstein's relation
since a point has no energy

$$\text{Transverse Impedance: } Z^{TE} = \frac{w\mu}{k_z} = \frac{E_x}{H_y} = \frac{-E_y}{H_x}$$

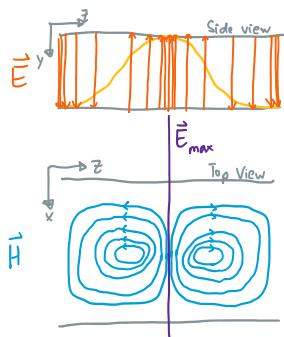
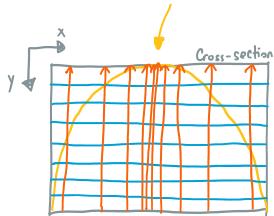
In a vacuum, c^2 .

For waves, it will be the group speed
 $\rightarrow V_g \neq c$

Apps 2 - TE10 Shape

$$E_{ys} = E_0 \sin\left(\frac{m\pi x}{a}\right) e^{-jk_z z}$$

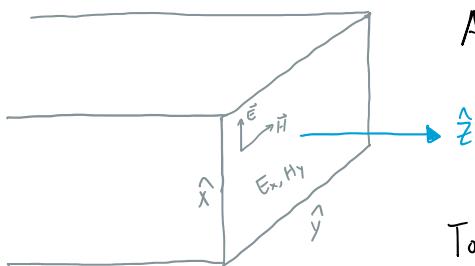
$$k_z = \sqrt{w^2 \mu \epsilon - \left(\frac{m\pi}{a}\right)^2}$$



TE20:

TE30:

In-class 11-22-2023



$E_z = 0$
by definition
of transverse
in TEM

$$\text{Ampère: } \vec{\nabla} \times \vec{H} = \cancel{\sigma E} + \epsilon \frac{\partial \vec{E}}{\partial t}$$

conductivity in middle of waveguide
= conductivity of air
= 0

To generate \vec{H} , we need a current. (By RHR (curling hand))

If \vec{H} is an \vec{H} into plane, there should be a current, in \vec{z} direction.

But there's no E_z , so there's no current. $\epsilon \frac{\partial \vec{E}}{\partial t} = 0 = \vec{\nabla} \times \vec{H}$

We assumed $\nabla \times \vec{H} \neq 0$ because there's a current, but there's no current. So we can't have TEM (plane) waves down the guide.

How do we get energy down the guide?

> Plane waves bounce off sides of waveguide (ping pong), so we get transverse standing waves.

From TE part above:

$$\vec{k} \cdot \vec{k} = \omega^2 \mu \epsilon$$

$$k_x^2 + k_y^2 + k_z^2 = \omega^2 \mu \epsilon$$

$$k_z = \pm \sqrt{\omega^2 \mu \epsilon - k_x^2 - k_y^2}$$

 depends on boundary conditions of the side of the waveguide

When frequency is low enough, k_z will be imaginary \rightarrow Cut off

In-class 11-29-2023

$$H_z = A(x, y) e^{j\omega t - jk_z z}$$

⑥

$$k_x^2 + k_y^2 + k_z^2 = k^2 = \omega^2 \mu \epsilon$$

$$k_z^2 = k^2 - k_x^2 - k_y^2$$

 > 0

We don't want this to be imaginary or we get exponential decay

$$k_z^2 = \omega^2 \mu \epsilon - k_x^2 - k_y^2$$

fixed by geometry

$$\omega^2 \mu \epsilon = -k_x^2 - k_y^2$$

$\omega \rightarrow$ Cut off frequency



$$\frac{\partial^2}{\partial x^2} H_z + \frac{\partial^2}{\partial y^2} H_z + (k_x^2 + k_y^2) H_z = 0$$

⑦

Assume no y dependence

$$\frac{\partial^2}{\partial x^2} H_z + \frac{\partial^2}{\partial y^2} H_z + (k_x^2 + k_y^2) H_z = 0$$

assume no y dependence

$$\frac{\partial^2 H_z}{\partial x^2} + k_x^2 H_z = 0$$

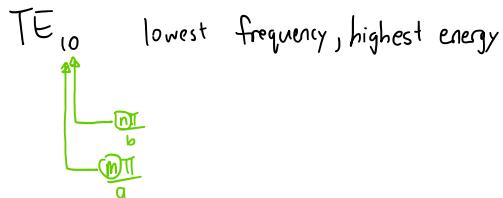
$$\frac{\partial^2 H_z}{\partial x^2} = -k_x^2 H_z$$

$$H_z = C \sin k_x x + D \cos k_x x$$

$$\vec{\nabla} \times \vec{H} = j \omega \epsilon \vec{E} ; \quad H_x, H_y = 0$$

$$\begin{bmatrix} \hat{x} & \hat{y} & \hat{z} \\ \partial_x & \partial_y & \partial_z \\ 0 & 0 & H_z \end{bmatrix} \rightarrow E_y \propto \frac{\partial H_z}{\partial x}$$

In-class 12-01-2023



How does a wave get transmitted down the waveguide?

> It bounces off the walls

For TEM waves, none gets transmitted. No energy goes to the end of the waveguide. $k_z = 0$

$$V_p V_g = \frac{w}{k_z} \frac{dw}{dk_z} = \sqrt{\frac{w^2}{w^2 \mu \epsilon - k_z}}$$

$$V_g = \frac{1}{\sqrt{\mu \epsilon}} \sqrt{1 - \frac{k_z^2}{w^2 \mu \epsilon}}$$

$$\begin{aligned} V_g &= \frac{dw}{dk_z} = \left(\frac{dk_z}{dw} \right)^{-1} \\ &= \left(\frac{d}{dw} \left(w \sqrt{\frac{1}{w^2 \mu \epsilon - k_z}} \right) \right)^{-1} \\ &= \left(w \left(-\left(\frac{1}{w^2 \mu \epsilon - k_z} \right) \left(2w \mu \epsilon - k_z dk_z \right) \right) - \sqrt{\frac{1}{w^2 \mu \epsilon - k_z}} \right) \end{aligned}$$

$$(w(-\omega_{pe-k_z})e^{i\omega_{pe}k_z}ak_z) / \sqrt{\omega_{pe-k_z}}$$

In-class 12-06-23 LAST LECTURE

$$f(x,y) = (A \cos(k_x x) + B \sin(k_x x)) \cdot (C \cos(k_y y) + D \sin(k_y y))$$

$$\frac{\partial f}{\partial y} = -k_y C \sin k_y y + k_y D \cos k_y y$$

↳ If $k_y = 0$, get a wave with infinite wavelength
 → DC, will not propagate

② $y = 0$

$$\frac{\partial f}{\partial y} = -k_y(0) + k_y D(1)$$

D should be 0

③ $y = b$

C cannot be 0 (see why A can't be 0)

$$\sin k_y b \rightarrow k_y b = n\pi$$

