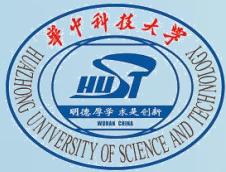


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and Communications

Jiaqing Huang

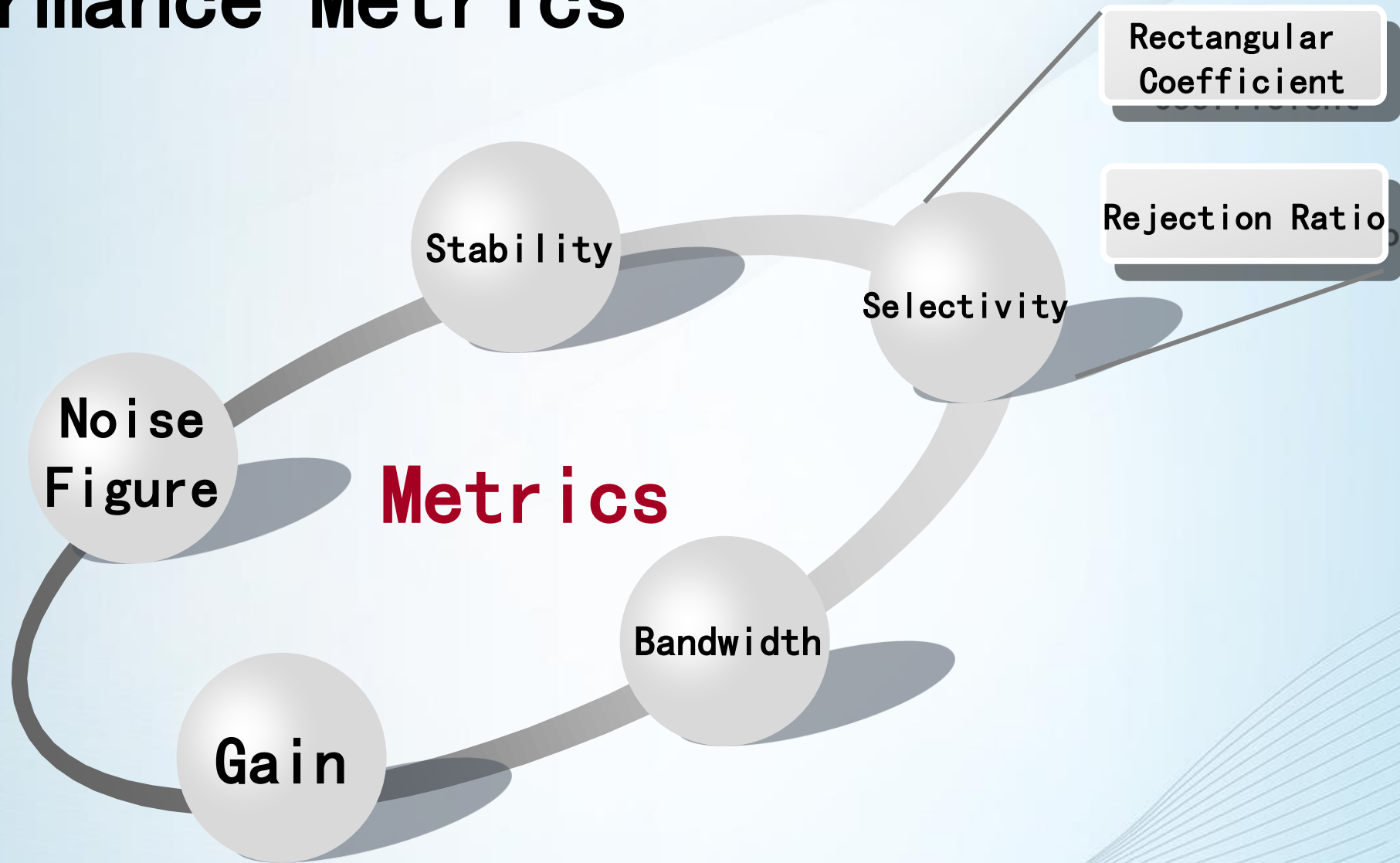


Small Signal Tuned Amplifier

Classification of Tuned Amplifier

- Devices: **Transistor**、FET、IC
- Stages: **Single Stage**, Multiple Stage
- Bandwidth: **NarrowBand**, WideBand
- Load: **Resonant**, Non-Resonant

Performance Metrics



Performance Metrics

➤ Gain

➤ Voltage Gain: $\dot{A}_V = \frac{\dot{V}_o}{\dot{V}_i}$

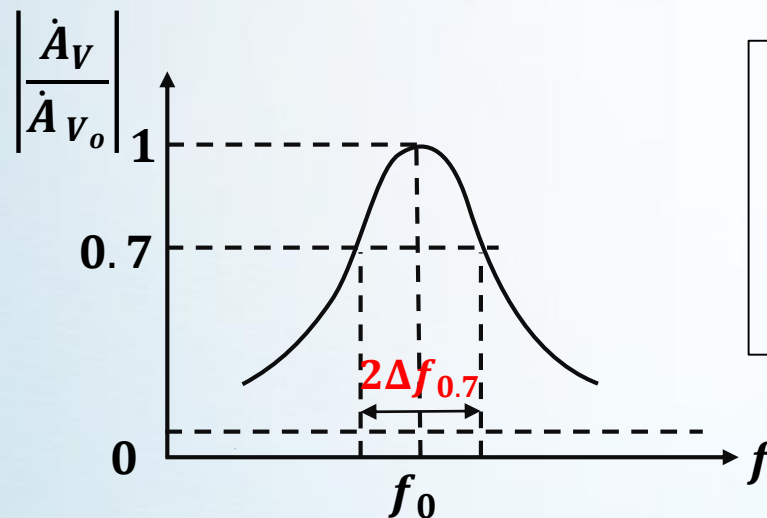
➤ Power Gain: $A_P = \frac{P_o}{P_i}$

Performance Metrics

➤ Bandwidth (3dB Bandwidth)

➤ \dot{A}_V down to its 0.707

$$\left| \frac{\dot{A}_V}{\dot{A}_{V_o}} \right| = \frac{1}{\sqrt{2}} \sim 2\Delta f_{0.7} \text{ (Bandwidth)}$$

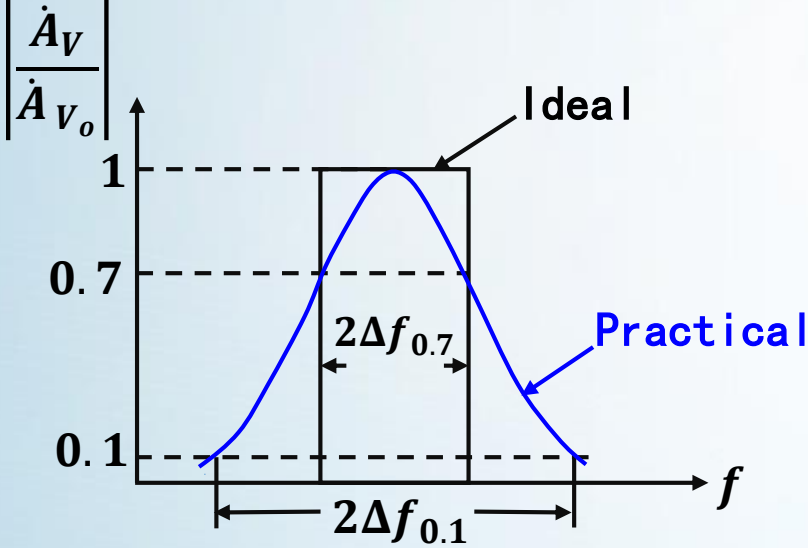
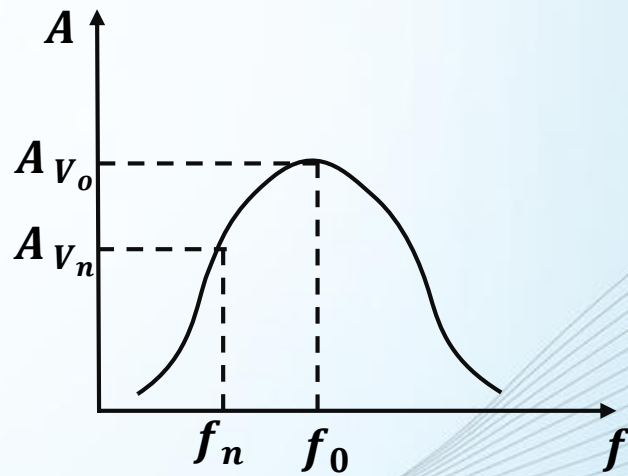


Review

- $|N(f)| = \left| \frac{i}{I_0} \right| = \frac{1}{\sqrt{2}} \sim 2\Delta f_{0.7}$ (Series Curve)
- $|N(f)| = \left| \frac{\dot{V}}{\dot{V}_0} \right| = \frac{1}{\sqrt{2}} \sim 2\Delta f_{0.7}$ (Parallel Curve)

Performance Metrics

➤ Selectivity:

<p>Rectangular Coefficient $K_{r0.1} = \frac{2\Delta f_{0.1}}{2\Delta f_{0.7}}$</p>	<p>Rejection Ratio $d_n = \frac{A_{V_o}}{A_{V_n}}$</p>
<p>How close to ideal</p>	<p>Rejection to f_n</p>
 <p>The graph plots the normalized voltage gain $\left \frac{\dot{A}_V}{\dot{A}_{V_o}} \right$ on the y-axis against frequency f on the x-axis. It compares two responses: an 'Ideal' response, represented by a rectangular pulse with a height of 1 and a width of $2\Delta f_{0.1}$, and a 'Practical' response, represented by a bell-shaped curve. The practical curve passes through the points (0.1, 0.1) and (0.7, 0.7) on the normalized gain scale. The width of the practical curve at the 0.7 level is marked as $2\Delta f_{0.7}$.</p>	 <p>The graph plots the voltage gain A on the y-axis against frequency f on the x-axis. It shows a bell-shaped curve centered at the passband frequency f_0. At a noise frequency f_n, the gain is A_{V_n}. The peak gain at f_0 is A_{V_o}. The rejection ratio d_n is the ratio of these two gains.</p>

Performance Metrics

➤ Stability

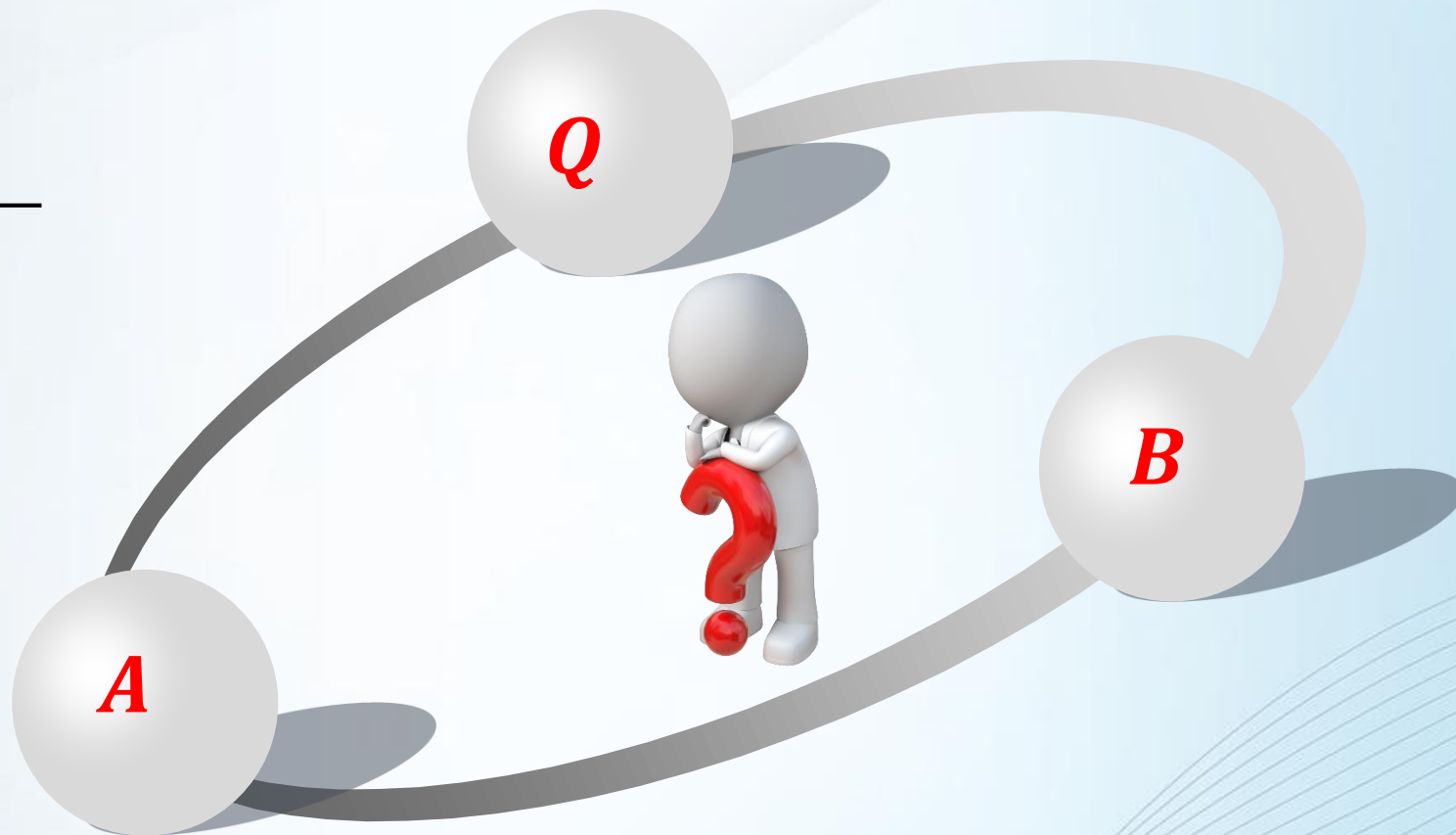
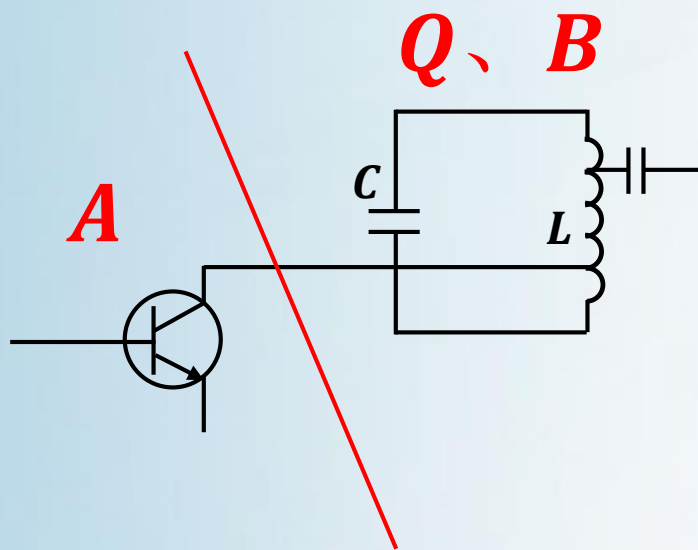
➤ Stability Coefficient

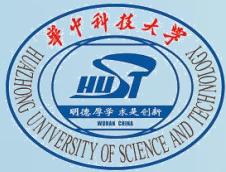
➤ Noise Figure N_F

➤ N_F the closer to 1, the better

$$N_F = \frac{S_i/N_i}{S_o/N_o}$$

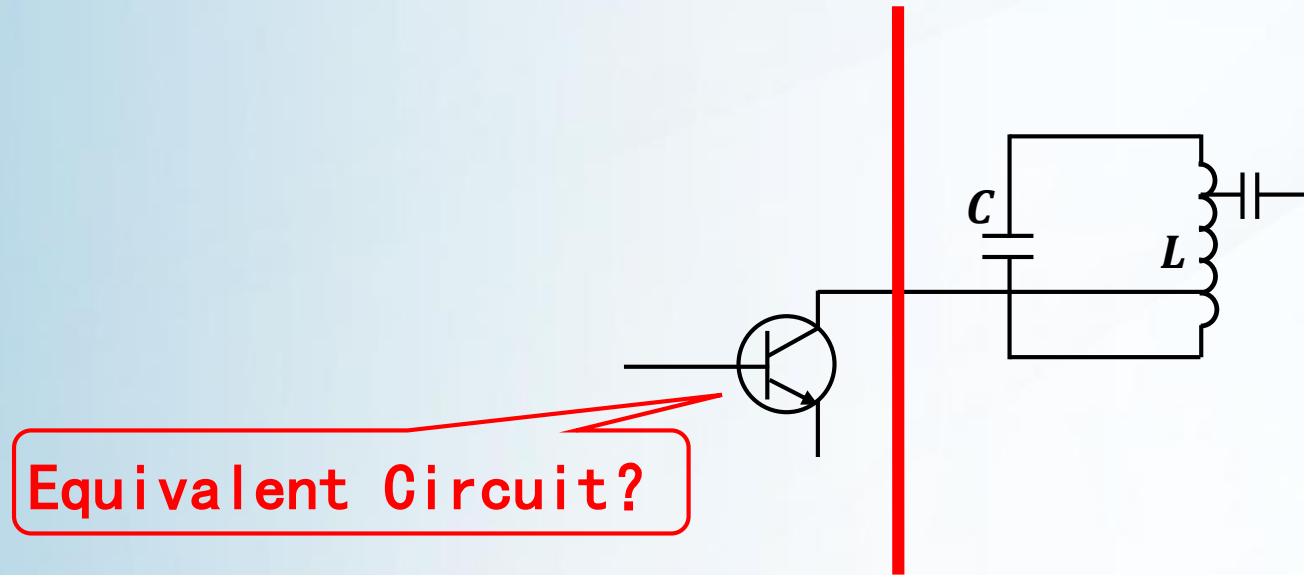
Key Relationship



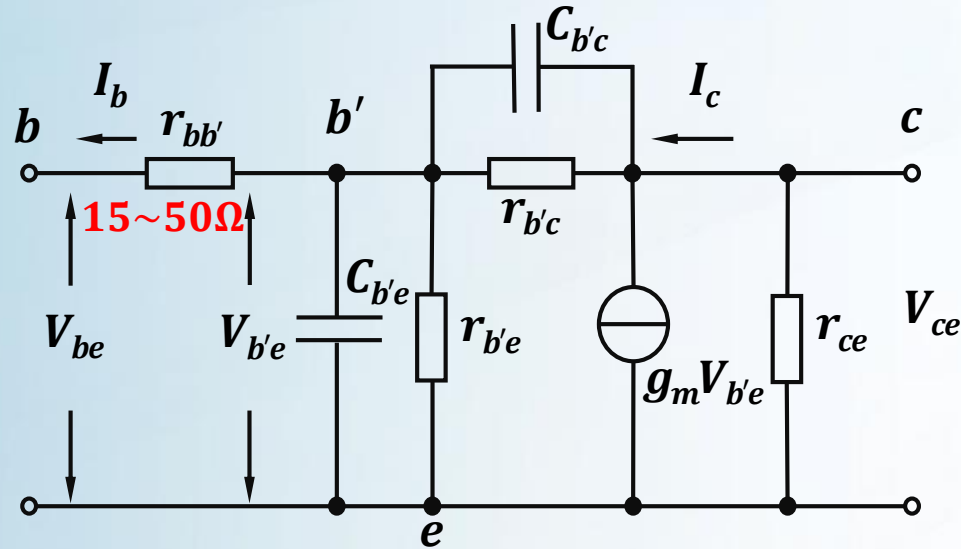


Equivalent Circuit

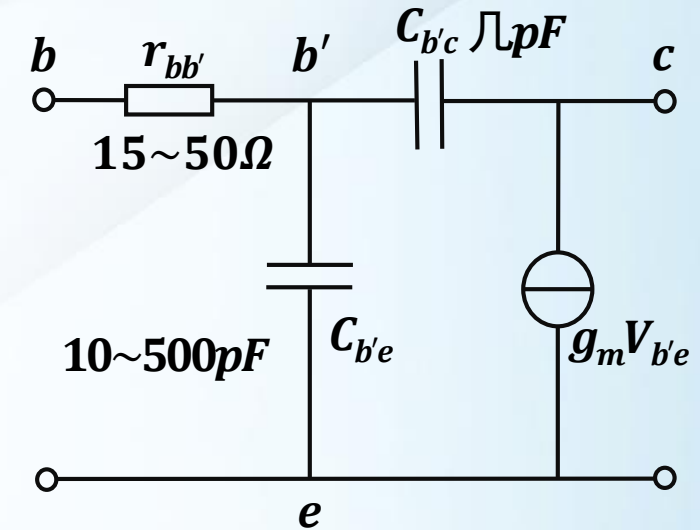
Small Signal Tuned Amplifier



Hybrid π Equivalent Circuit



simplify



$r_{bb'}$ Base Resistance

$C_{b'e}$ PN Capacitance

$C_{b'c}$ PN Capacitance

$r_{b'e} \Rightarrow r_{b'e} > C_{b'e}$, Open

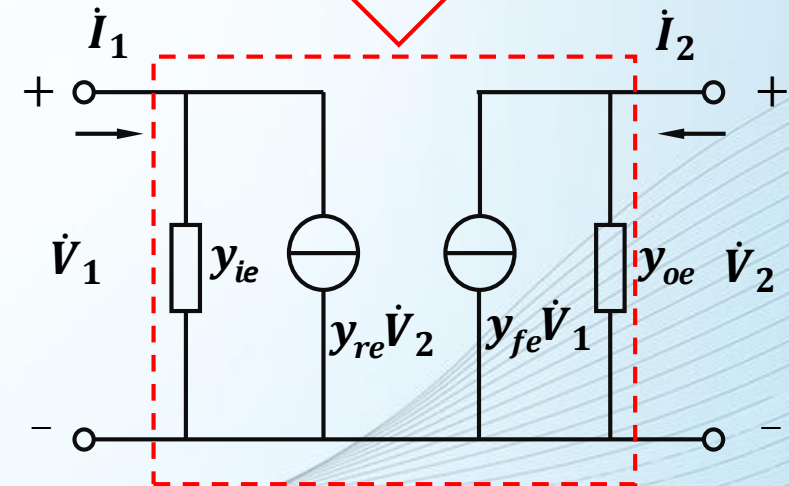
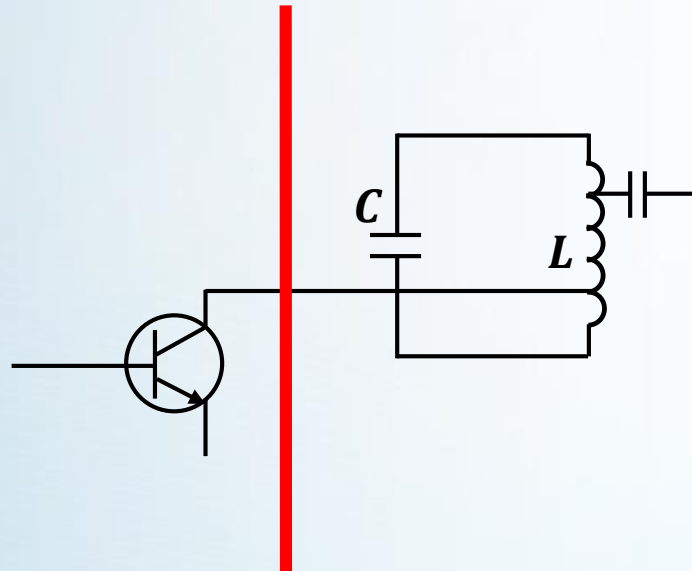
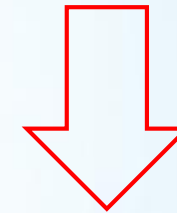
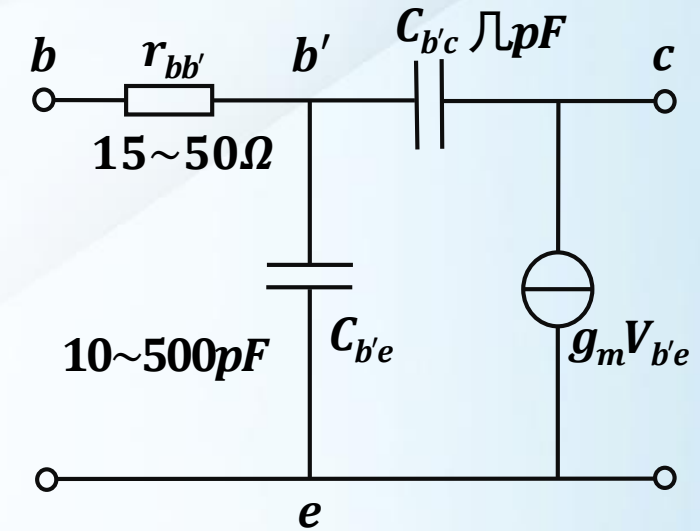
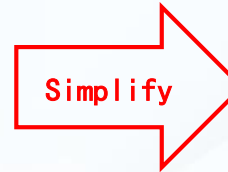
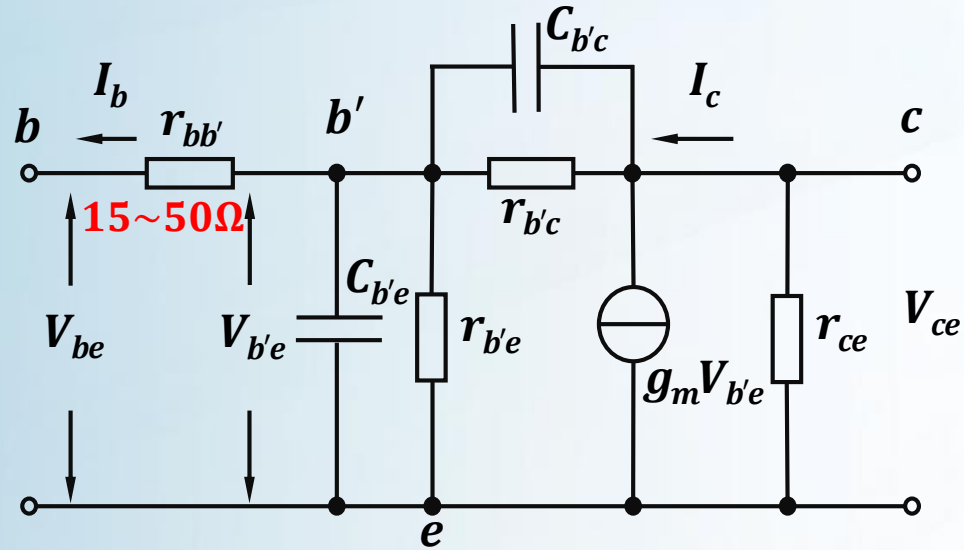
$r_{b'c} \Rightarrow r_{b'c} > C_{b'c}$, Open

$r_{ce} \Rightarrow r_{ce} > \text{Load}$, Open

Stability

$g_m V_{b'e}$ current source, amplify ability (g_m transconductance)

Hybrid π Equivalent Circuit



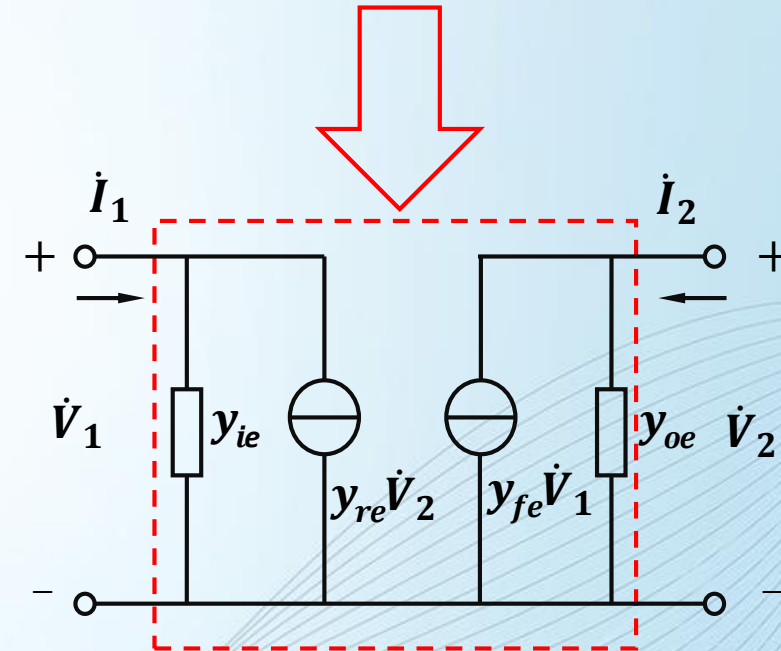
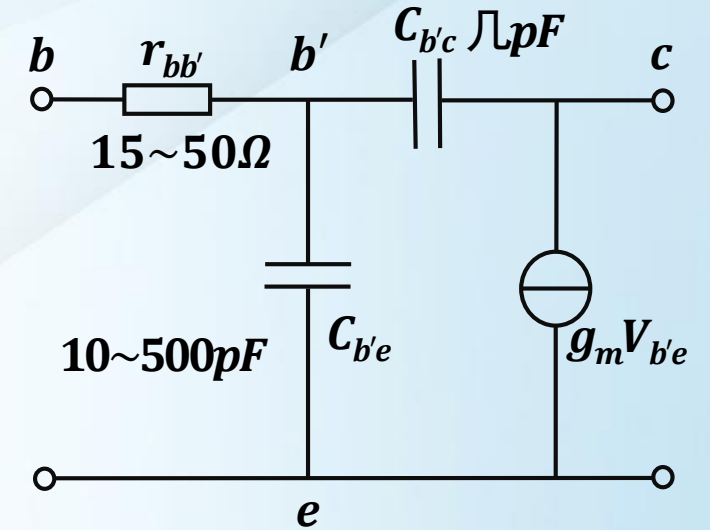
Y Parameter Equivalent Circuit

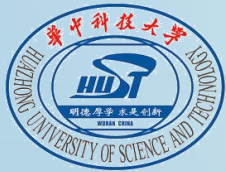
Input Admittance: $y_{ie} = \frac{i_1}{\dot{V}_1} \Big|_{\dot{V}_2=0} = \frac{Y_{b'e}}{1+r_{bb'}Y_{b'e}}$

Forward Transfer Admittance: $y_{fe} = \frac{i_2}{\dot{V}_1} \Big|_{\dot{V}_2=0} = \frac{g_m}{1+r_{bb'}Y_{b'e}}$

Reverse Transfer Admittance : $y_{re} = \frac{i_1}{\dot{V}_2} \Big|_{\dot{V}_1=0} = -\frac{j\omega C_{b'c}}{1+r_{bb'}Y'_{b'e}}$

Output Admittance: $y_{oe} = \frac{i_2}{\dot{V}_2} \Big|_{\dot{V}_1=0} = j\omega C_{b'c} \left(1 + \frac{g_m r_{bb'}}{1+r_{bb'}Y'_{b'e}} \right)$

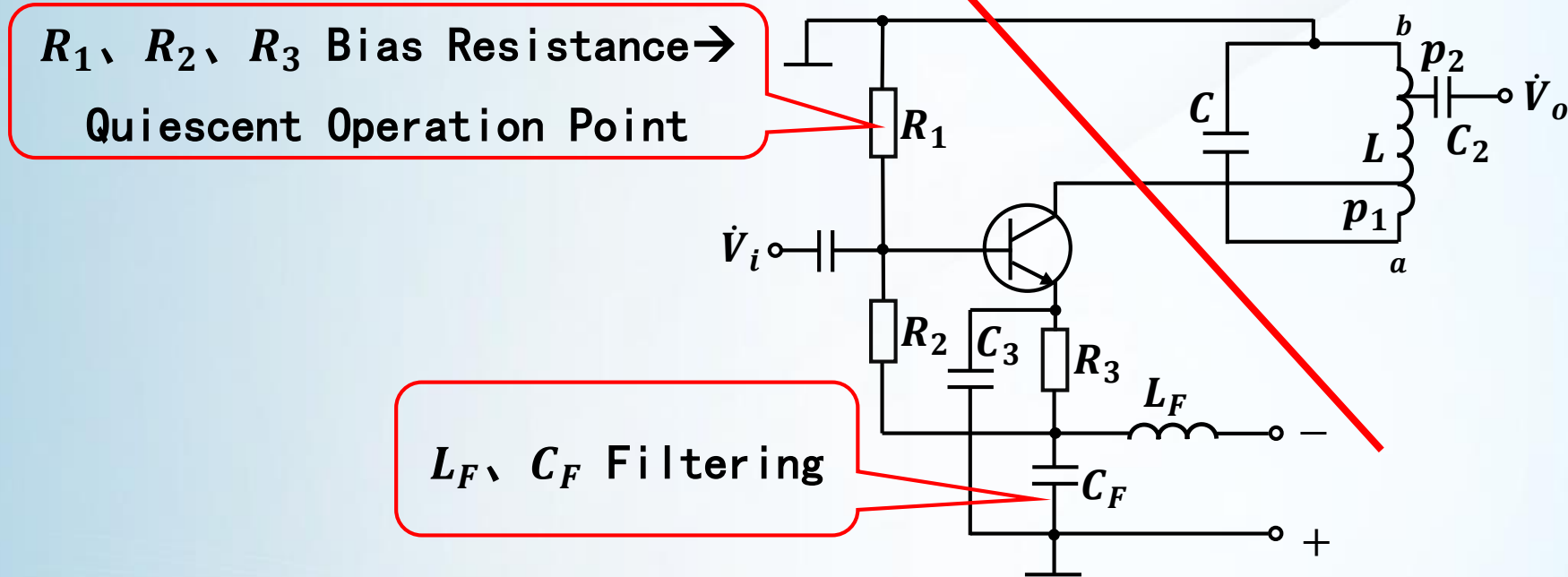




Gain

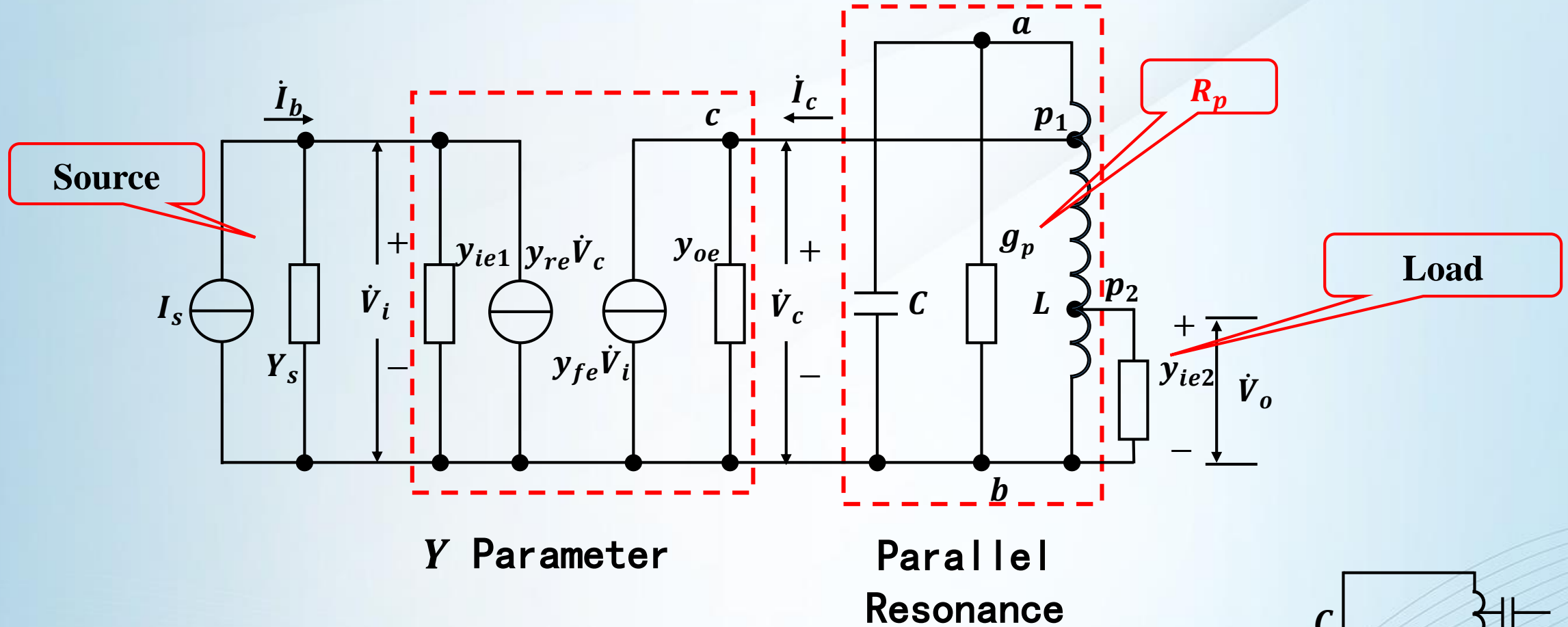
Small Signal Tuned Amplifier

➤ Clue: \Rightarrow Gain, B, Selectivity

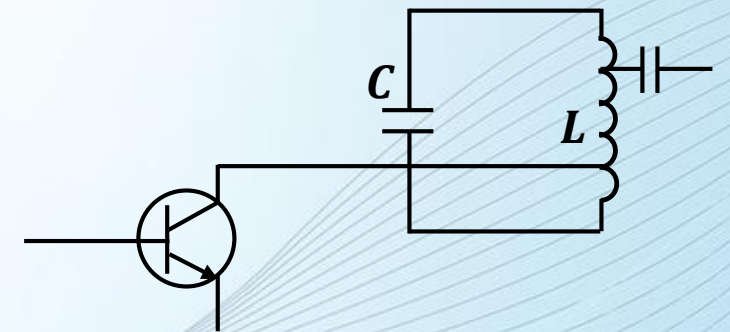


Y Parameter + Parallel Resonance (With Tap)

Equivalent Circuit



★Do not miss R_p



Gain

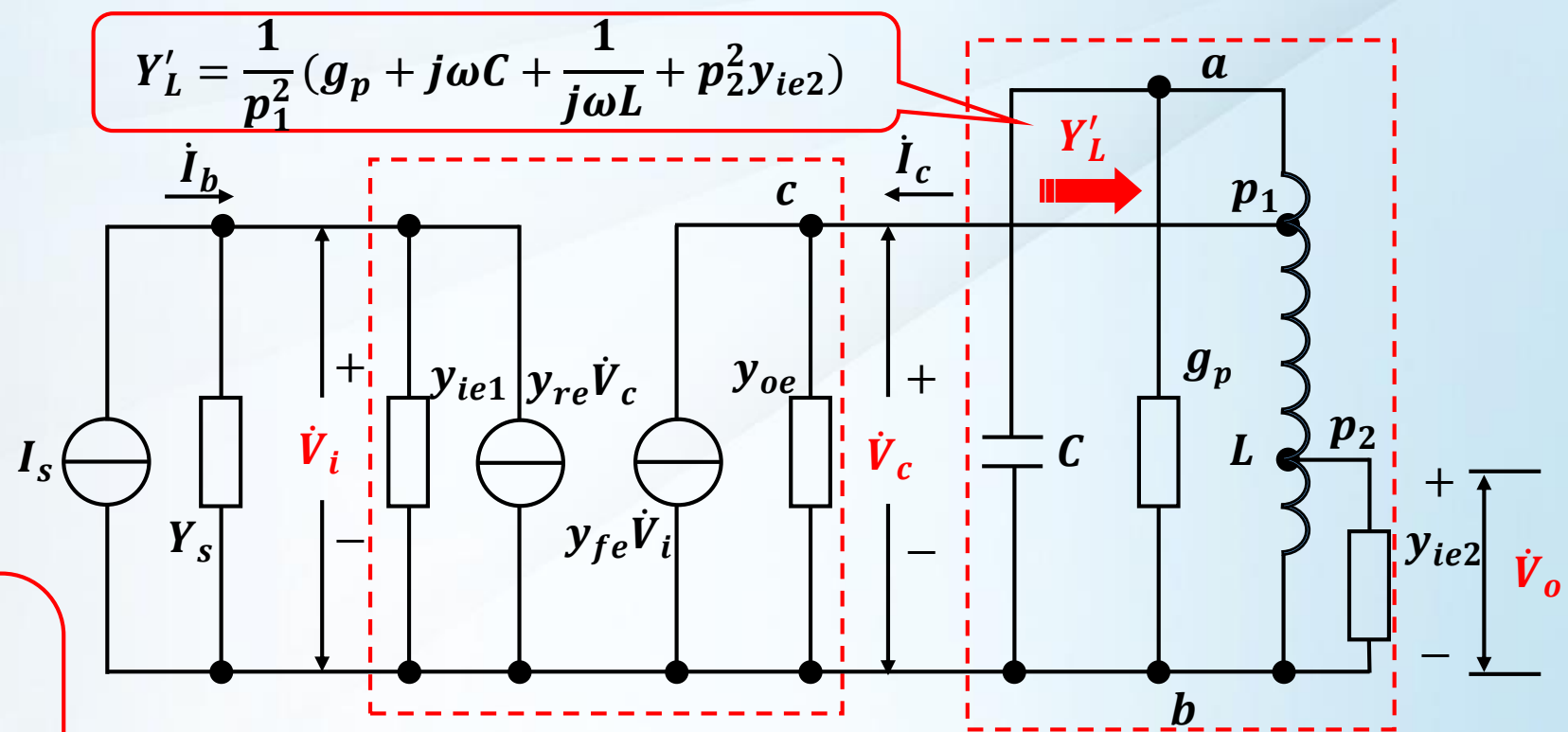
$$\begin{cases} \dot{I}_b = y_{ie}\dot{V}_i + y_{re}\dot{V}_c & (1) \\ \dot{I}_c = y_{fe}\dot{V}_i + y_{oe}\dot{V}_c & (2) \\ \dot{I}_c = -\dot{V}_c Y'_L & (3) \end{cases}$$

Y'_L From right of collector c

$$Y'_L = \frac{1}{p_1^2} (g_p + j\omega C + \frac{1}{j\omega L} + p_2^2 y_{ie2})$$

$$\because (3) = (2)$$

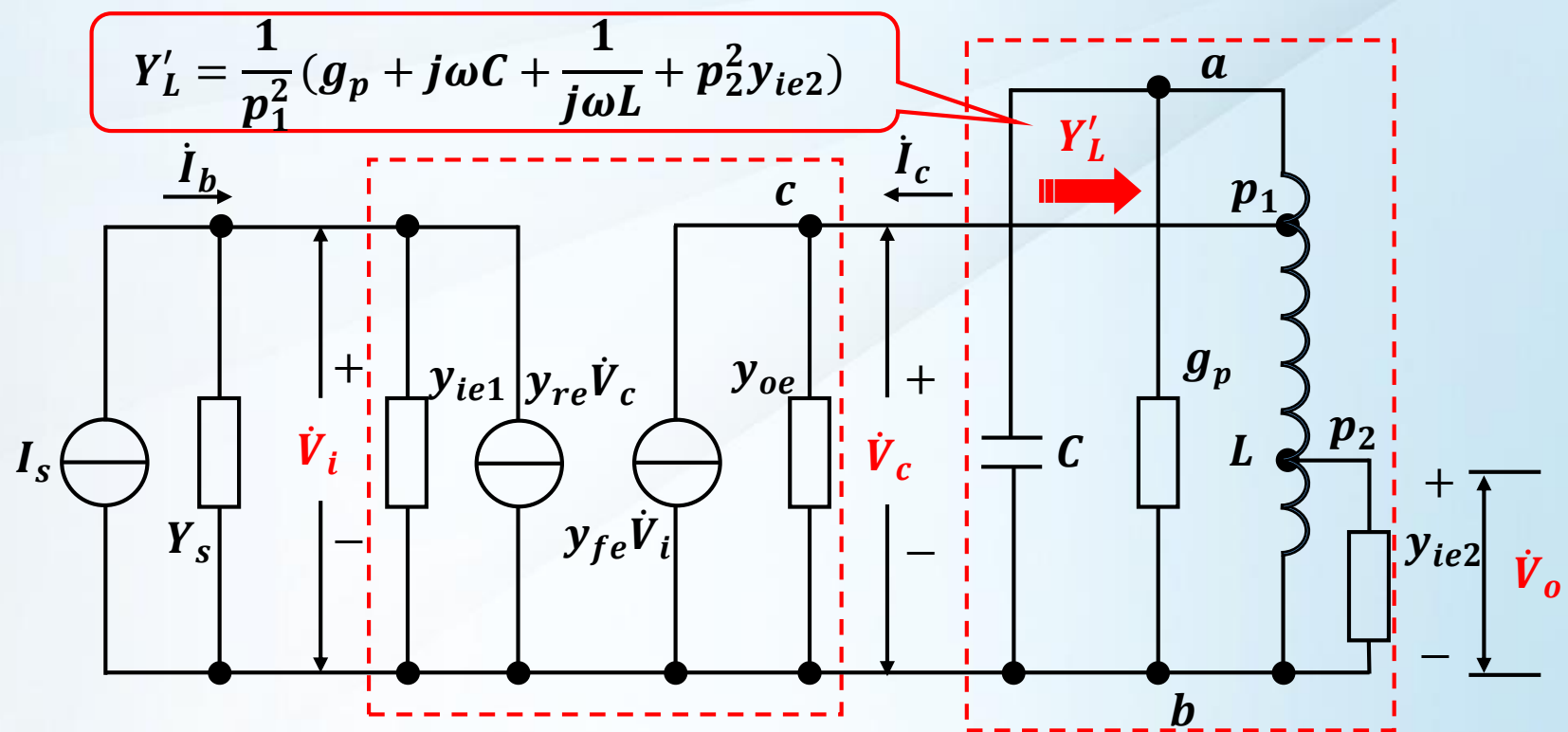
$$\Rightarrow \dot{V}_c = -\frac{y_{fe}}{y_{oe} + Y'_L} \dot{V}_i \quad (4)$$



$$\dot{V}_c = -\frac{y_{fe}}{y_{oe} + Y'_L} \dot{V}_i$$

$$\dot{A}_V = \frac{\dot{V}_o}{\dot{V}_i}$$

Gain



Tap p_1 p_2 :

$$\left. \begin{aligned} \dot{V}_o &= p_2 \dot{V}_{ab} \\ \dot{V}_c &= p_1 \dot{V}_{ab} \end{aligned} \right\} \Rightarrow \dot{V}_o = \frac{p_2}{p_1} \dot{V}_c$$

$$\dot{V}_c = -\frac{y_{fe}}{y_{oe} + Y'_L} \dot{V}_i \quad \dot{V}_o = \frac{p_2}{p_1} \dot{V}_c$$

$$\dot{A}_V = \frac{\dot{V}_o}{\dot{V}_i}$$

Gain

$$\dot{A}_V = \frac{\dot{V}_o}{\dot{V}_i}$$

$$= \frac{p_2 \dot{V}_c}{p_1 \dot{V}_i} = - \frac{p_2 y_{fe}}{p_1 (y_{oe} + Y'_L)}$$

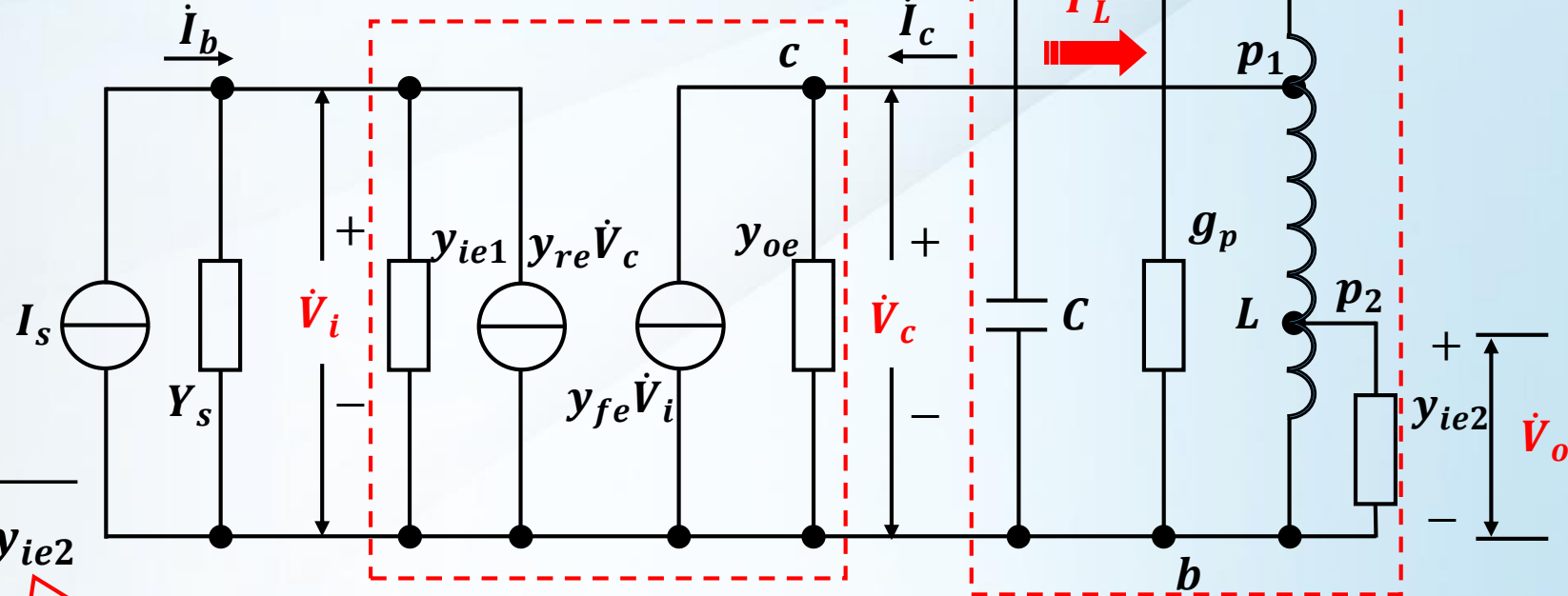
$$= - \frac{p_1 p_2 y_{fe}}{p_1^2 y_{oe} + \boxed{g_p + j\omega C + \frac{1}{j\omega L}} + p_2^2 y_{ie2}}$$

$$y_{oe} = g_{oe} + j\omega C_{oe}$$

$$y_{ie2} = g_{ie2} + j\omega C_{ie2}$$

$$= \frac{-p_1 p_2 y_{fe}}{\underbrace{(p_1^2 g_{oe} + g_p + p_2^2 g_{ie2})}_{g_\Sigma} + j\omega \underbrace{(p_1^2 C_{oe} + C + p_2^2 C_{ie2})}_{C_\Sigma} + \frac{1}{j\omega L}}$$

$$Y'_L = \frac{1}{p_1^2} (g_p + j\omega C + \frac{1}{j\omega L} + p_2^2 y_{ie2})$$



$$\begin{aligned} \dot{V}_c &= - \frac{y_{fe}}{y_{oe} + Y'_L} \dot{V}_i \\ \dot{V}_o &= \frac{p_2}{p_1} \dot{V}_c \\ \Rightarrow \dot{A}_V &= \frac{-p_1 p_2 y_{fe}}{g_\Sigma + j\omega C_\Sigma + \frac{1}{j\omega L}} \end{aligned}$$

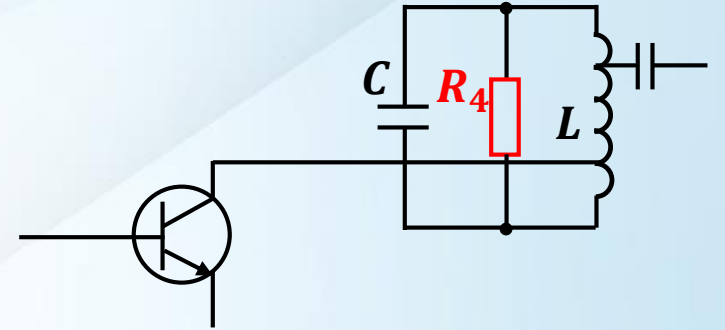
Gain

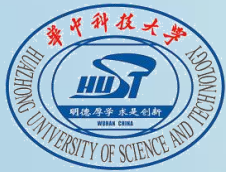
$$\dot{A}_V = \frac{\dot{V}_o}{\dot{V}_i} \left\{ \begin{aligned} \dot{A}_V &= \frac{-p_1 p_2 y_{fe}}{g_\Sigma + \boxed{j\omega C_\Sigma + \frac{1}{j\omega L}}} \end{aligned} \right.$$

$$(p_1^2 g_{oe} + g_p + p_2^2 g_{ie2})$$

$$\dot{A}_{V0} = \frac{-p_1 p_2 y_{fe}}{g_\Sigma}$$

$$\text{Resonant, } j\omega C_\Sigma + \frac{1}{j\omega L} = 0$$



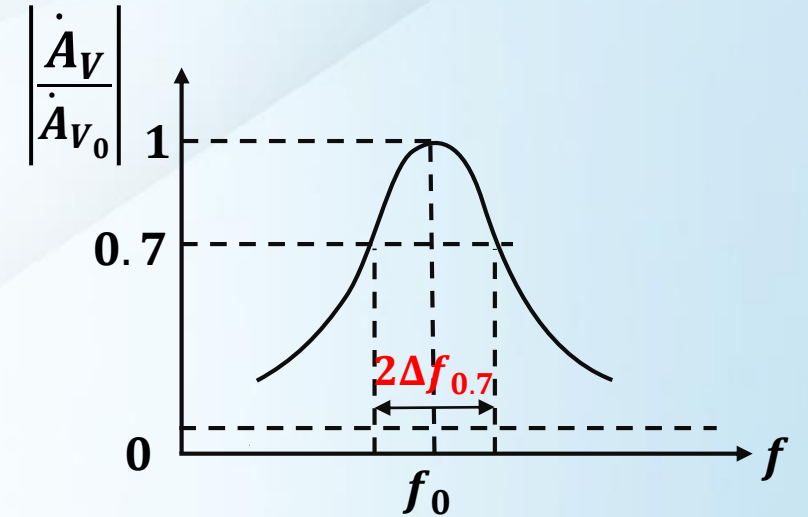


Bandwidth & Selectivity

Bandwidth

➤ Bandwidth: $2\Delta f_{0.7}$

$$\left| \frac{\dot{A}_V}{\dot{A}_{V_0}} \right| = \frac{1}{\sqrt{2}} \sim 2\Delta f_{0.7}$$



$$\left. \begin{aligned} \dot{A}_V &= \frac{-p_1 p_2 y_{fe}}{g_\Sigma + j\omega C_\Sigma + \frac{1}{j\omega L}} = \frac{-p_1 p_2 y_{fe}}{g_\Sigma + j\left(\omega C_\Sigma - \frac{1}{\omega L}\right)} = \frac{-p_1 p_2 y_{fe}}{g_\Sigma (1 + j\xi)} \\ \dot{A}_{V_0} &= \frac{-p_1 p_2 y_{fe}}{g_\Sigma} \end{aligned} \right\} \Rightarrow \frac{\dot{A}_V}{\dot{A}_{V_0}} = \frac{1}{1 + j\xi}$$

$$\xi = \frac{\omega C - \frac{1}{\omega L}}{G} \approx Q \cdot \frac{2\Delta f}{f_p}$$

Bandwidth *vs.* Quality Factor

$$\left. \begin{aligned} \frac{\dot{A}_V}{\dot{A}_{V_0}} &= \frac{1}{1 + j\xi} \\ \left| \frac{\dot{A}_V}{\dot{A}_{V_0}} \right| &= \frac{1}{\sqrt{1 + \xi^2}} = \frac{1}{\sqrt{2}} \end{aligned} \right\} \Rightarrow \left. \begin{aligned} &\text{当 } 2\Delta f = 2\Delta f_{0.7} \\ &\xi = 1 \\ &\xi = Q_L \cdot \frac{2\Delta f}{f_p} \end{aligned} \right\} \Rightarrow 1 = Q_L \cdot \frac{2\Delta f_{0.7}}{f_p}$$

$2\Delta f = 2\Delta f_{0.7}$

Note: $Q_L \cdot B = f_p$

Bandwidth *vs.* Gain

$$Q_L = \frac{1}{\frac{\omega_0 L}{g_\Sigma}} = \frac{\omega_0 C_\Sigma}{g_\Sigma} \Rightarrow g_\Sigma = \frac{\omega_0 C_\Sigma}{Q_L} = \frac{2\pi f_0 C_\Sigma}{\frac{f_0}{2\Delta f_{0.7}}} = 2\pi C_\Sigma \cdot 2\Delta f_{0.7}$$

$$Q_L \cdot 2\Delta f_{0.7} = f_0$$

$$\dot{A}_{V_0} = \frac{-p_1 p_2 y_{fe}}{g_\Sigma} = -\frac{p_1 p_2 y_{fe}}{2\pi C_\Sigma \cdot 2\Delta f_{0.7}}$$

$$\Rightarrow |A_{V_0} \cdot 2\Delta f_{0.7}| = \frac{|p_1 p_2 y_{fe}|}{2\pi C_\Sigma}$$

Note: Constant

Selectivity (Rectangle Coefficient)

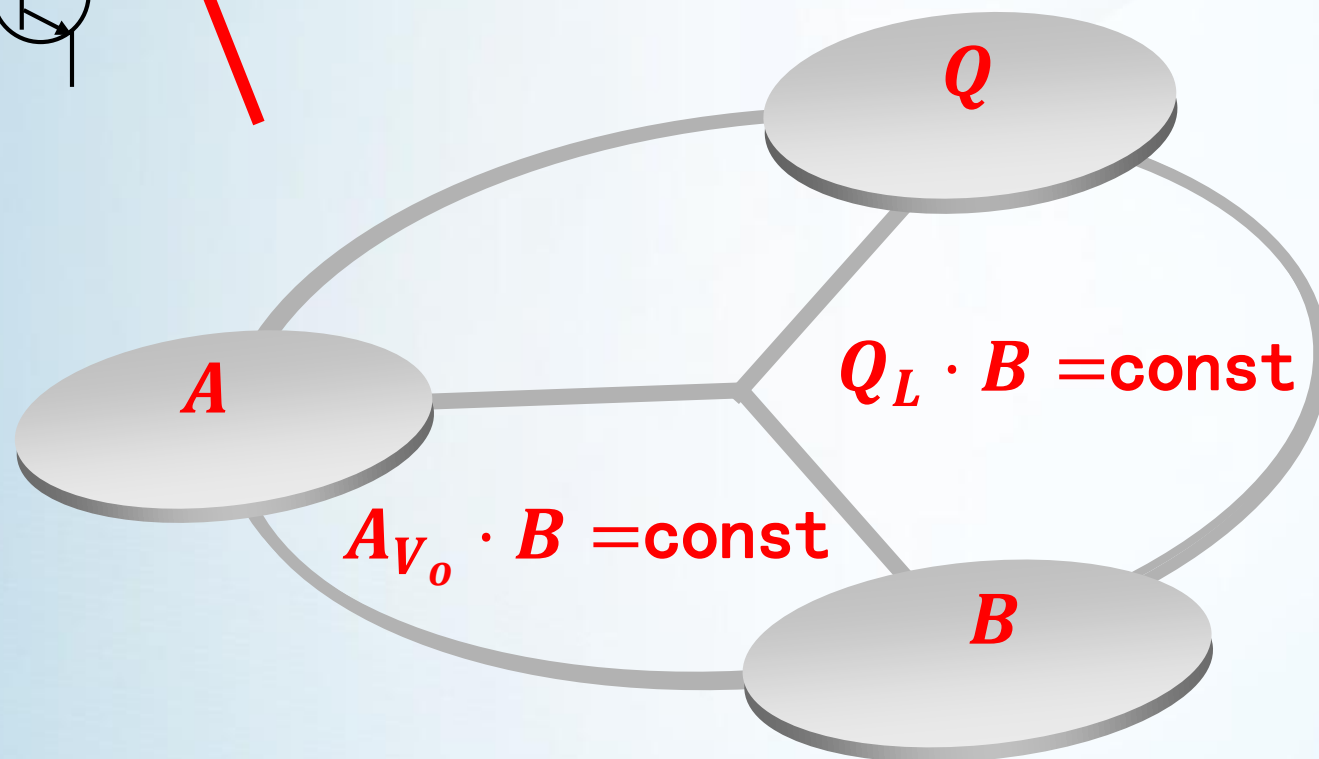
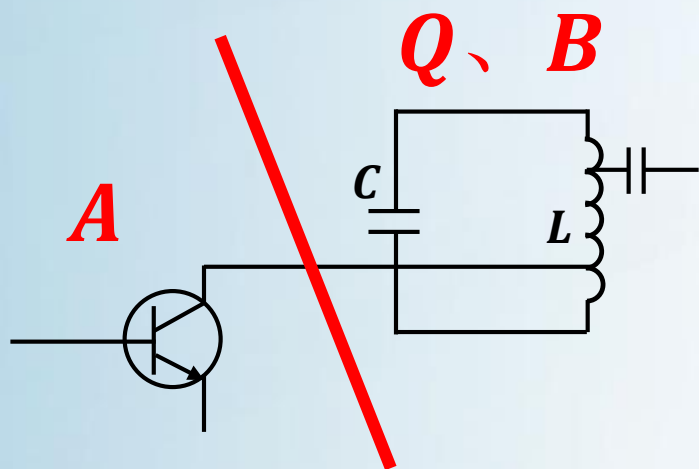
$$\left| \frac{\dot{A}_V}{\dot{A}_{V_0}} \right| = \frac{1}{\sqrt{1 + \left(Q_L \frac{2\Delta f_{0.1}}{f_p} \right)^2}} = 0.1$$

$$\Rightarrow 2\Delta f_{0.1} = \sqrt{10^2 - 1} \cdot \frac{f_p}{Q_L} = \sqrt{10^2 - 1} \cdot 2\Delta f_{0.7}$$

$$K_{r0.1} = \frac{2\Delta f_{0.1}}{2\Delta f_{0.7}} = \sqrt{10^2 - 1} = 9.9499$$

Note: Far away from ideal 1

Summary



Selectivity