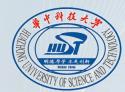


Huazhong University of Science & Technology

Electronic Circuit of Communications

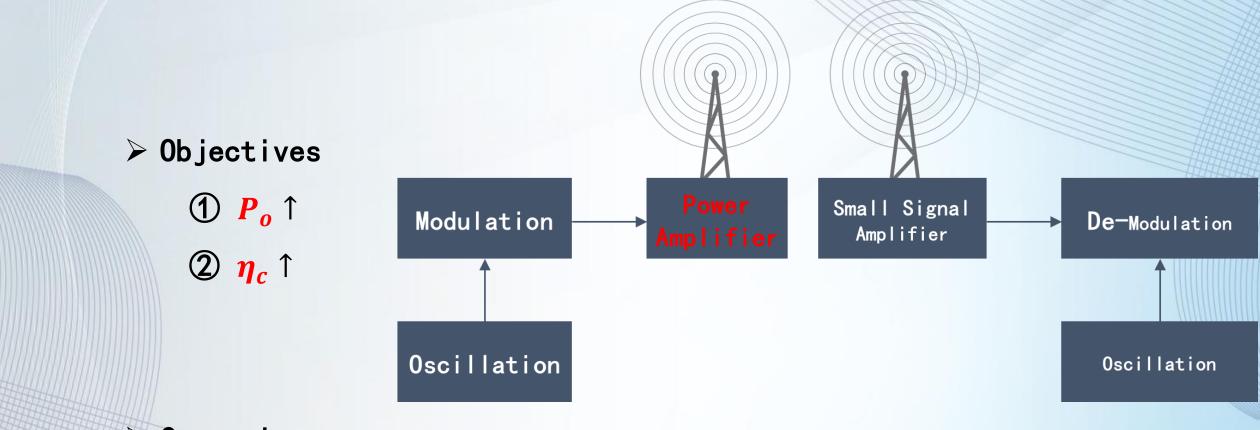
School of Electronic Information and Commnications

Jiaqing Huang



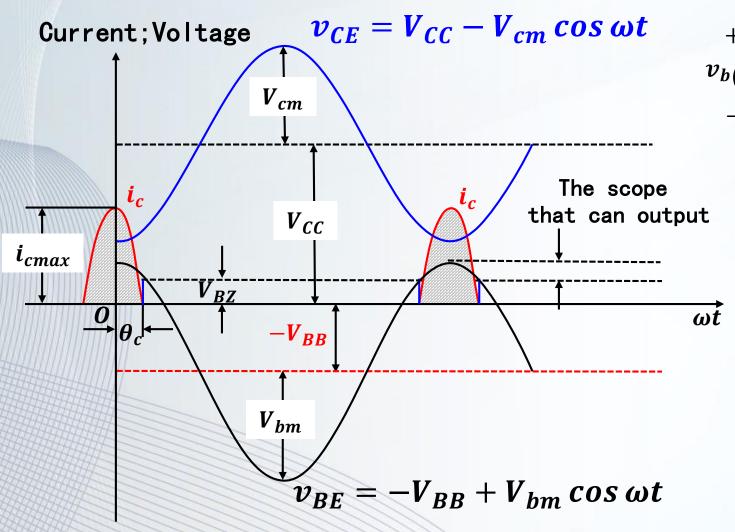
RF Power Amplifier

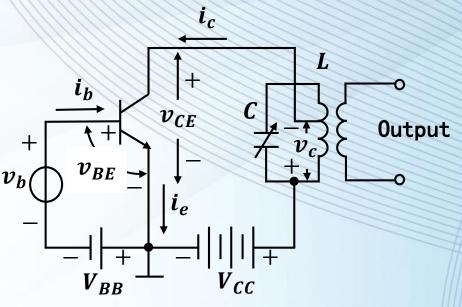
Radio Frequency Power Amplifier



- > Comparison
 - lacktriangle RF Power Amplifier vs. RF Small Signal Amplifier?
 - RF Power Amplifier vs. Audio Power Amplifier?

RF Power Amplifier — Principle

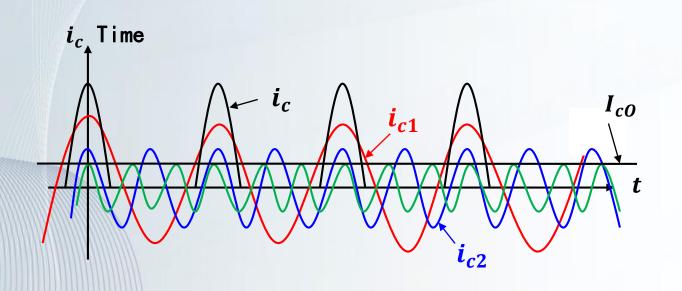


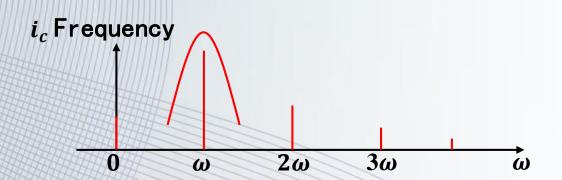


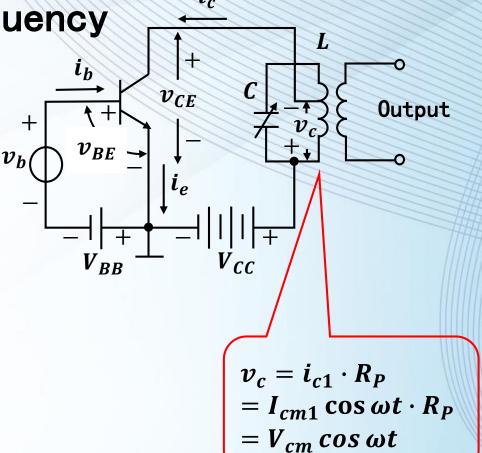
Key Concepts

- > Reversely Biased
- $> \theta_c < 90^\circ$ (Class C)
- \succ Cosine Pulses i_c
- ➤ Nonlinear+Linear

RF Power Amplifier — Time & Frequency



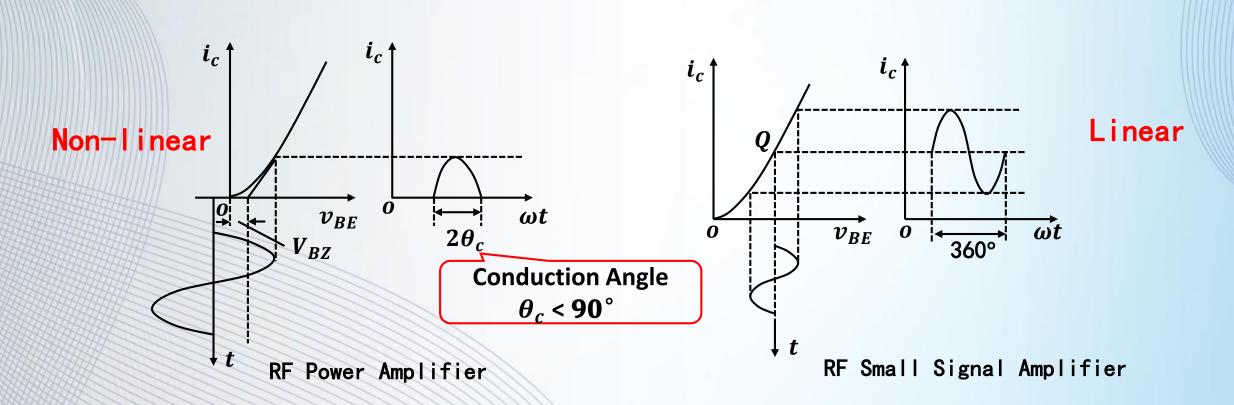




RF Power Amplifier vs. RF Small Signal Amplifier

- > Samilarity
 - **♦** Radio frequency
 - **♦** Load is resonance

- Difference
 - **◆** Amplitude of input
 - ◆ Quiescent point of Transistor
 - **♦** Dynamic range

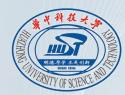


RF Power Amplifier vs. Audio Power Amplifier

- > Similarity
 - ♦ High Power
 - ♦ High Efficiency

Difference

	RF Power Amplifier	Audio Power Amplifier
Load	Parallel Resonance	Resistance
Status	Class C	Class A / B
Relative Bandwidth	Radio Narrowband	Audio Wideband



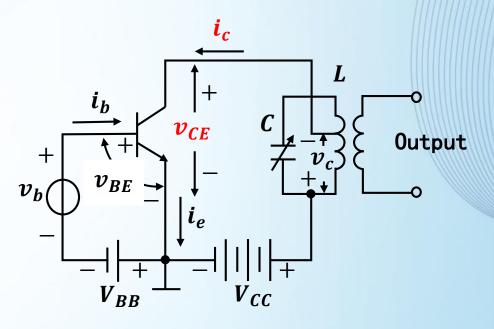
Output Power and Efficiency

RF Power Amplifier — Power & Efficiency

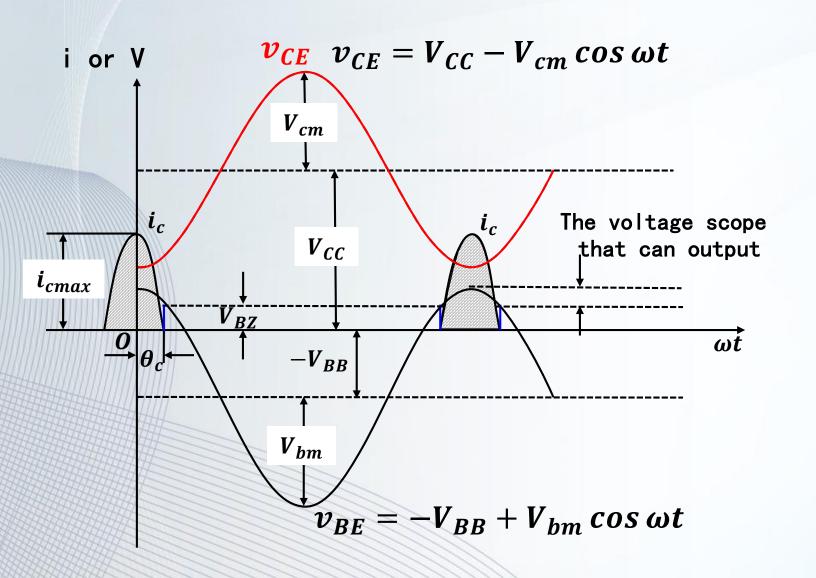
Power: Output Power
$$P_o$$
 = DC Power P_c = Efficiency: Collector η_c = $\frac{P_o}{P_c}$ = $\frac{P_o}{P_o + P_c}$

 $ightharpoonup P_c
ightharpoonup P_o
ightharpoonup \eta_c
ightharpoonup P_o
ightharpoonup \eta_c
ightharpoonup P_c
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Collector
Dissipation Power P_c $P_c = \frac{1}{T} \int_0^T i_C \cdot v_{CE} dt$



RF Power Amplifier — Decrease P_c

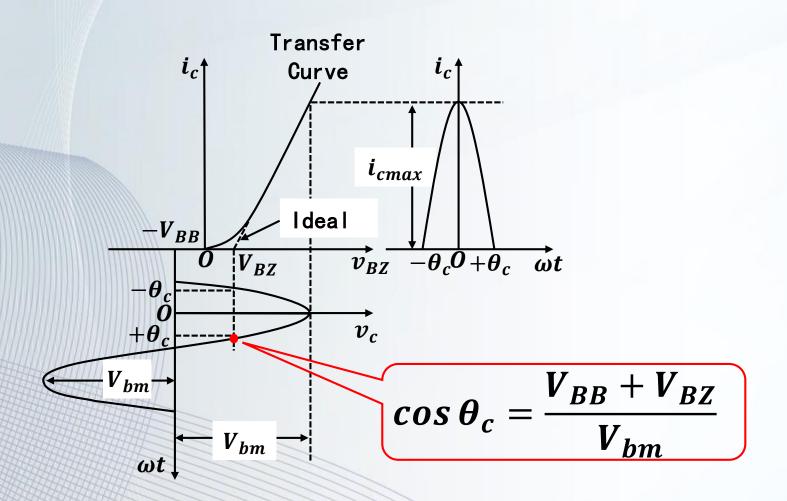


$$P_c = \frac{1}{T} \int_0^T i_C \cdot v_{CE} \, dt$$

How to decrease P_c :

- \succ LC Resonant on ω $i_{cmax} \Leftrightarrow v_{CEmin}$
- \triangleright Decrease θ_c

RF Power Amplifier — Decrease P_c



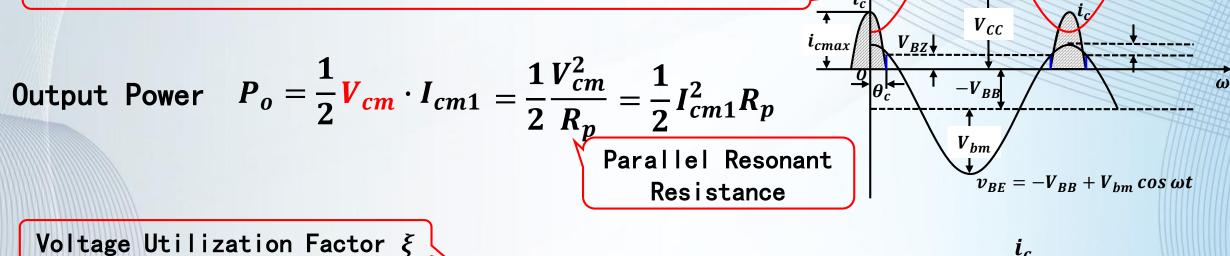
$$P_c = \frac{1}{T} \int_0^T i_C \cdot v_{CE} \, dt$$

How to decrease P_c :

- $\succ LC$ Resonant on ω
 - $i_{cmax} \Leftrightarrow v_{CEmin}$
- \triangleright Decrease θ_c

RF Power Amplifier—Detailed Definition in v

$$i_c = I_{c0} + I_{cm1} \cos \omega t + I_{cm2} \cos 2 \omega t + \cdots + I_{cmn} \cos n\omega t + \cdots$$



Collector Efficiency

for
$$\eta_c = \frac{P_o}{P_=} = \frac{\frac{1}{2} V_{cm} \cdot I_{cm1}}{V_{cc} \cdot I_{c0}} = \frac{1}{2} \xi g_1(\theta_c)$$

DC Power $P_= = V_{cc} \cdot I_{c0}$

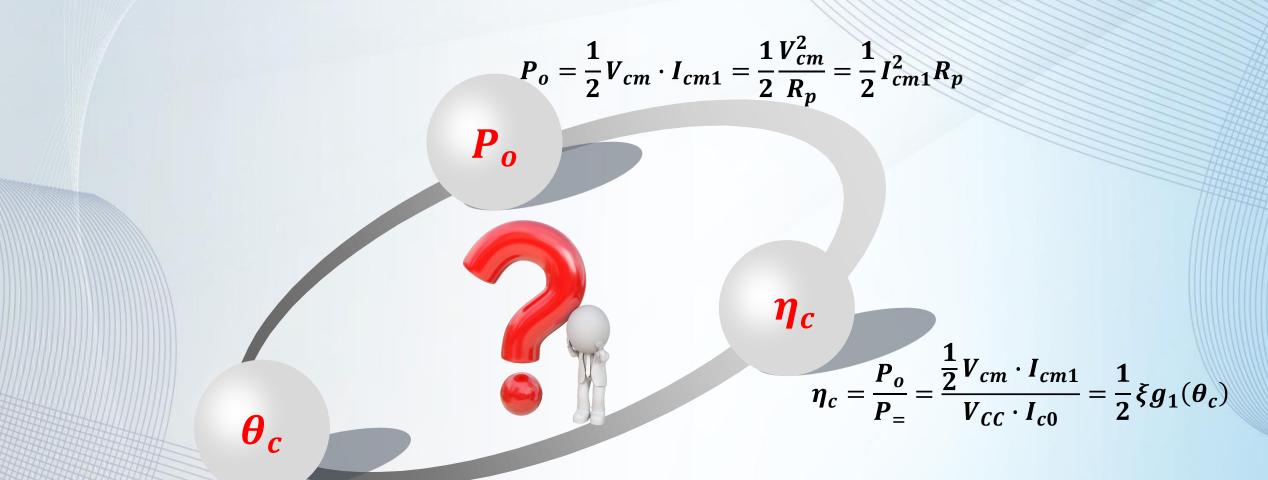
Utilization Factor $g_1(\theta_c)$

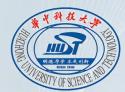
 $\begin{array}{c|c} & & & & & \\ & & & & \\$

 $v_{CE} = V_{CC} - V_{cm} \cos \omega t$

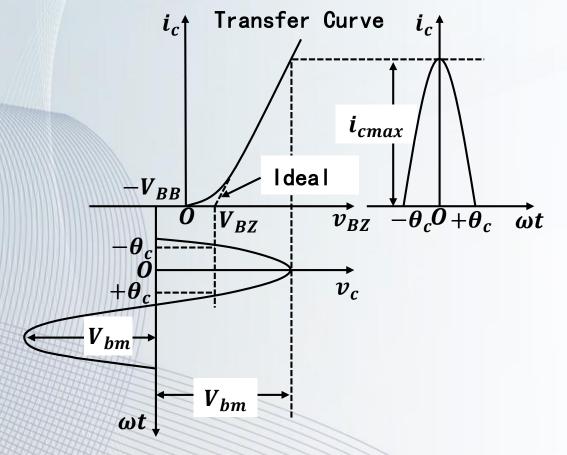
 \Leftrightarrow Compute I_{cm1} & $I_{c0} \Leftarrow$ Analyze i_c by Fourier Series

Summary—Output Power & Efficiency





RF Power Amplifier Computation



RF Power Amplifier — Clue
$$\begin{cases} P_o = \frac{1}{2}V_{cm} \cdot I_{cm1} = \frac{V_{cm}^2}{2R_p} = \frac{1}{2}I_{cm1}^2R_p \\ \eta_c = \frac{P_o}{P_=} = \frac{\frac{1}{2}V_{cm} \cdot I_{cm1}}{V_{cc} \cdot I_{c0}} = \frac{1}{2}\xi g_1(\theta_c) \end{cases}$$

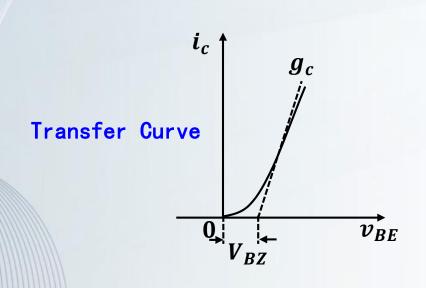
- \triangleright Key: compute I_{c0} & I_{cm1}
- \Leftarrow Analyze Cosine Pulse i_c

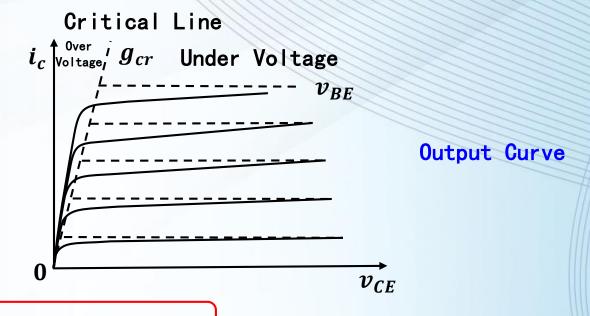
$$\rightarrow i_c =? (\theta_c =? i_{cmax} =?)$$

- > By Fourier Series
- ← Piecewise Linear Approximation

(Transfer Curve, Output Curve)

RF Power Amplifier — Piecewise Linear Approximation





Transfer Equation:

$$i_c = g_c(v_{BE} - V_{BZ}) \quad (v_{BE} > V_{BZ})$$
 (1)

Critical Line Equation: $i_c = g_{cr}v_{CE}$

$$i_c = g_{cr} v_{CE} \tag{2}$$

Critical Line Gradient

Trans-conductance

Periodic Cosine Pulses

Transfer Equation:
$$i_c = g_c(v_{BE} - V_{BZ})$$
 (1)

Base Equation :
$$v_{BE} = -V_{BB} + V_{bm} \cos \omega t$$
 (3)

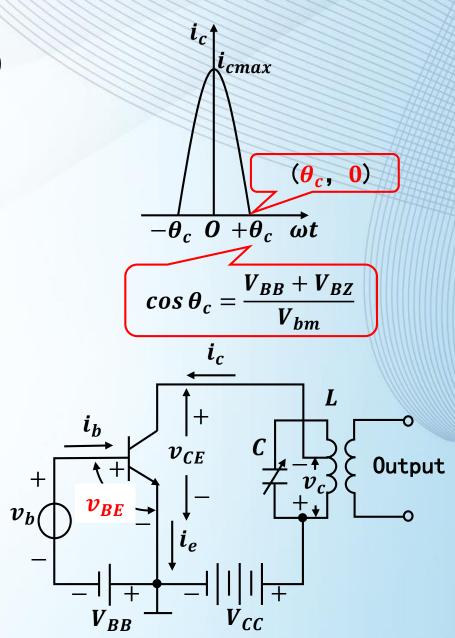
Substitute (3) into (1),

$$i_c = g_c(-V_{BB} + V_{bm}\cos\omega t - V_{BZ}) \quad (4)$$

If $\omega t = \theta_c$, $i_c = 0$, Substitute into (4),

$$\mathbf{0} = g_c(-V_{BB} + V_{bm}\cos\theta_c - V_{BZ}) \tag{5}$$

Obtain
$$\cos \theta_c = \frac{V_{BB} + V_{BZ}}{V_{bm}}$$



Periodic Cosine Pulses

$$\begin{cases} i_c = g_c(-V_{BB} + V_{bm}\cos\omega t - V_{BZ}) & (4) \\ 0 = g_c(-V_{BB} + V_{bm}\cos\theta_c - V_{BZ}) & (5) \end{cases}$$

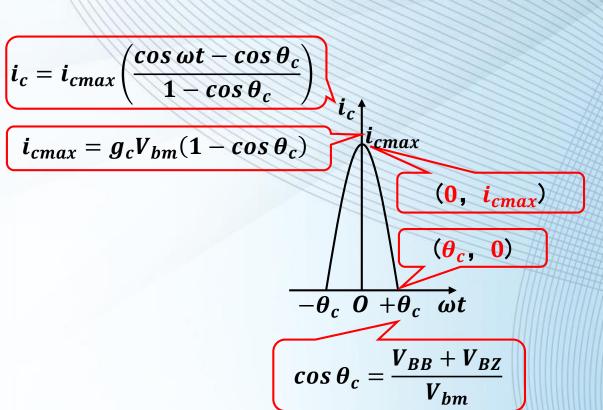
$$(4)-(5)$$
, 得

$$i_c = g_c V_{bm}(\cos \omega t - \cos \theta_c) \quad (6)$$

If $\omega t = 0$, $i_c = i_{cmax}$, Substitute into (6)

$$i_{cmax} = g_c V_{bm} (1 - \cos \theta_c) \tag{7}$$

(6) ÷ (7),
$$i_c = i_{cmax} \left(\frac{\cos \omega t - \cos \theta_c}{1 - \cos \theta_c} \right)$$
 Cosine Pulse Formula



Periodic Cosine Pulses-Decompose $i_c = i_{cmax} \left(\frac{\cos \omega t - \cos \theta_c}{1 - \cos \theta_c} \right)$

$$i_c = i_{cmax} \left(\frac{\cos \omega t - \cos \theta_c}{1 - \cos \theta_c} \right)$$

 $i_{cmax} = g_c V_{bm} (1 - \cos \theta_c)$

> By Fourier Series

$$i_c = I_{c0} + I_{cm1} \cos \omega t + I_{cm2} \cos 2 \omega t + \cdots + I_{cmn} \cos n\omega t + \cdots$$

Compute Coefficents
$$I_{c0} = \frac{1}{2\pi} \int_{-\theta_c}^{+\theta_c} i_c \, d\omega t = i_{cmax} \cdot \alpha_0(\theta_c)$$

$$\alpha_0(\theta_c) = \frac{\sin \theta_c - \theta_c \cos \theta_c}{\pi(1 - \cos \theta_c)}$$
Output Power
$$\alpha_n = \frac{1}{2\pi} \int_{-\theta_c}^{+\theta_c} i_c \cos \omega t \, d\omega t = i_{cmax} \cdot \alpha_1(\theta_c)$$

$$\alpha_1(\theta_c) = \frac{\theta_c - \cos \theta_c \sin \theta_c}{\pi(1 - \cos \theta_c)}$$
0.5
0.4
0.3
1.0

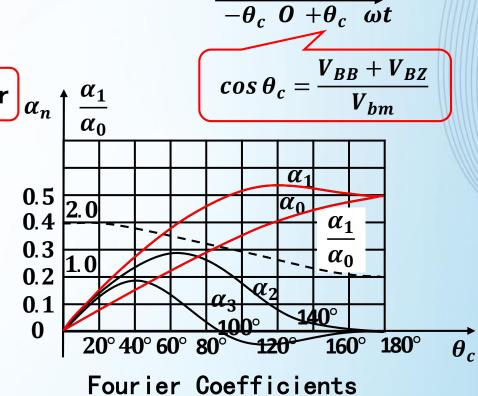
$$\alpha_0(\theta_c) = \frac{1}{\pi(1-\cos\theta_c)}$$

$$I_{cm1} = \frac{1}{2\pi} \int_{0}^{+\theta_{c}} i_{c} \cos \omega t \, d\omega t = i_{cmax} \cdot \alpha_{1}(\theta_{c})$$

$$\alpha_1(\theta_c) = \frac{\theta_c - \cos\theta_c \sin\theta_c}{\pi(1 - \cos\theta_c)}$$

$$I_{cmn} = \frac{1}{2\pi} \int_{-\theta_c}^{+\theta_c} i_c \cos n\omega t \, d\omega t = i_{cmax} \cdot \alpha_n(\theta_c)$$

$$\alpha_n(\theta_c) = \frac{2}{\pi} \cdot \frac{\sin n\theta_c \cos \theta_c - n \cos n\theta_c \sin \theta_c}{n(n^2 - 1)(1 - \cos \theta_c)}$$



lcmax

Periodic Cosine Pulses-Decompose $i_c = i_{cmax} \left(\frac{\cos \omega t - \cos \theta_c}{1 - \cos \theta_c} \right)$

$$e\left[i_{c}=i_{cmax}\left(\frac{\cos\omega t-\cos\theta_{c}}{1-\cos\theta_{c}}\right)\right]$$

> By Fourier Series

$$i_c = I_{c0} + I_{cm1} \cos \omega t + I_{cm2} \cos 2 \omega t + \cdots + I_{cmn} \cos n\omega t + \cdots$$

> Compute Coefficents

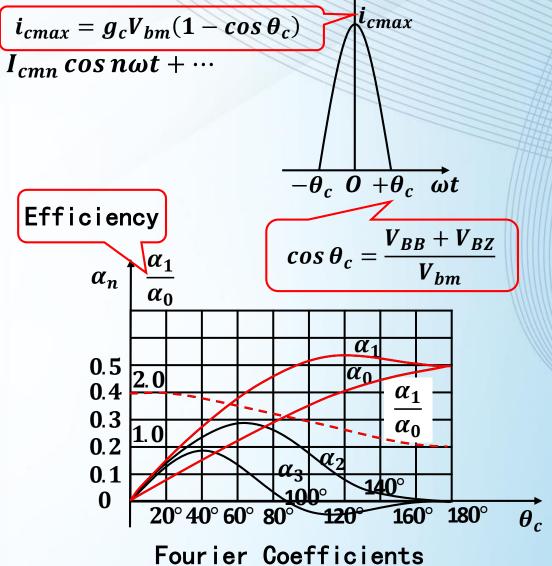
$$I_{c0} = \frac{1}{2\pi} \int_{-\theta_c}^{+\theta_c} i_c \, d\omega t = i_{cmax} \cdot \alpha_0(\theta_c)$$

$$I_{cm1} = \frac{1}{2\pi} \int_{-\theta_c}^{+\theta_c} i_c \cos \omega t \, d\omega t = i_{cmax} \cdot \alpha_1(\theta_c)$$

$$\eta_c = \frac{P_o}{P_e} = \frac{\frac{1}{2} V_{cm} \cdot I_{cm1}}{V_{cc} \cdot I_{c0}} = \frac{1}{2} \xi \cdot g_1(\theta_c)$$

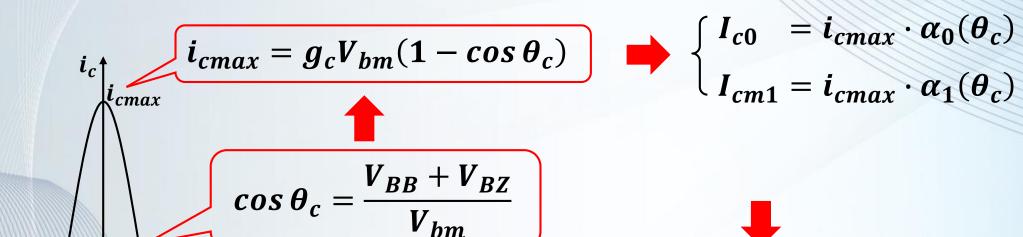
$$g_1(\theta_c) = \frac{I_{cm1}}{I_{c0}} = \frac{\alpha_1(\theta_c)}{\alpha_0(\theta_c)}$$

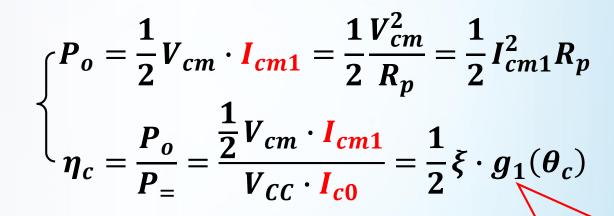
> Tradeoff between Power & Efficiency, Optimal θ_c around 70



Summary—Computation of RF Power Amplifier

 $-\theta_c \ 0 + \theta_c \ \omega t$





$$g_1(\theta_c) = \frac{\alpha_1(\theta_c)}{\alpha_0(\theta_c)}$$

Exp 4-1 The transfer characteristic of a RF power amplifier is as figure. The parameters of transistor are : $f_T \ge 150 MHz$, $A_p \ge 13 dB$, $I_{cmax} = 3A$, $P_{cmax} = 5W$. $V_{BZ} = 0.6V$, $V_{BB} = 1.4V$, $\theta_c = 70^{\circ}$, $V_{CC} = 24V$, $\xi = 0.9$. Compute all metrics.

Figure
$$\Rightarrow g_c = \frac{1A}{(2.6-0.6)V} = 0.5A/V$$
 $\cos \theta_c = \frac{V_{BB} + V_{BZ}}{V_{bm}}, \Rightarrow V_{bm} = \frac{1.4 + 0.6}{\cos 70^{\circ}} = 5.8 V$

Solution:
$$i_{cmax} = g_c V_{bm} (1 - \cos \theta_c)$$
, Compute I_{cm1} , I_{c0}

$$i_{cmax} = \frac{1}{2} \times 5.8 \times (1 - \cos 70^{\circ}) = 2A < I_{cmax}$$
 (Safe)

$$\Rightarrow \begin{cases}
I_{cm1} = i_{cmax} \cdot \alpha_1(70^\circ) = 2 \times 0.436 = 0.872A \\
I_{c0} = i_{cmax} \cdot \alpha_0(70^\circ) = 2 \times 0.253 = 0.506A
\end{cases}$$

$$P_{o} = \frac{1}{2}I_{cm1} \cdot V_{cm} = \frac{1}{2}I_{cm1} \cdot (\xi V_{cc}) = \frac{1}{2} \times 0.872 \times 0.9 \times 24 = 9.4W$$

$$P_{=} = V_{cc} \cdot I_{c0} = 24 \times 0.506 = 12W \quad \Rightarrow P_{c} = P_{=} - P_{o} = 2.6W < P_{cmax} \text{ (Safe)}$$

$$\eta_c = \frac{P_o}{P_-} = \frac{9.4}{12} = 78\%$$