

Chapter-2 Electric Fields

Coulomb's Law and field Intensity

Coulomb's Law is an experimental law formulated in 1785 by the French Colonel, Charles Augustin de Coulomb. It deals with the force a point charge exerts on another point charge. Charges are measured in coulombs (C). One coulomb is approximately equivalent to 6×10^{18} electrons; it is a very large unit of charge because one electron charge

$$e = -1.6019 \times 10^{-19} \text{ C.}$$

Coulomb's Law - statement

Coulomb's law states that the force F bet. two point charges q_1 and q_2 is:

- ① along the line joining them
- ② Directly proportional to the product $q_1 \cdot q_2$ of the charges
- ③ Inversely proportional to the square of the distance R bet. them.

or

The force bet. two charges separated in a vacuum or free space by a distance which is large compared to their size is proportional to the charge on each and inversely proportional to the square of the distance bet. them.

That is;

$$F \propto q_1 \cdot q_2 \quad \dots \quad \text{(a)}$$

$$F \propto \frac{1}{R^2} \quad \dots \quad \text{(b)}$$

Combining ① & ②

$$F \propto \frac{Q_1 Q_2}{R^2}$$

$$\therefore F = \frac{k Q_1 Q_2}{R^2} \quad \textcircled{③}$$

where k is the proportionality constant. In SI units, charges Q_1 and Q_2 are in coulombs (C), the distance R is in meters (m), and the force F is in newtons (N) so that $k = \frac{4}{4\pi\epsilon_0}$. The constant ϵ_0 is known as the permittivity of free space (in farads per meter) and has the value

$$\epsilon_0 = 8.854 \times 10^{-12} \approx \frac{10^{-9}}{36\pi} \text{ F/m}$$

$$\text{or } k = \frac{1}{4\pi\epsilon_0} \approx 9 \times 10^9 \text{ N/F}$$

Now, the expression ③ becomes

$$F = \boxed{\frac{Q_1 Q_2}{4\pi\epsilon_0 R^2}}$$

If point charges Q_1 & Q_2 are located at points having position vectors \vec{r}_1 & \vec{r}_2 , then the force \vec{F}_{12} on Q_2 due to Q_1 is given by

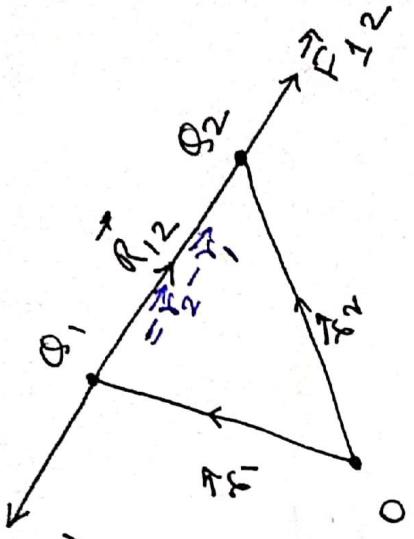
$$\vec{F}_{12} = \frac{Q_1 Q_2}{4\pi\epsilon_0 R^2} \hat{r}_{12} \quad \text{where, } \vec{R}_{12} = \vec{r}_2 - \vec{r}_1 \\ R = |\vec{R}_{12}|$$

$$\text{and } \hat{q}_{R_{12}} = \frac{\vec{R}_{12}}{|\vec{R}_{12}|} = \frac{\vec{R}_{12}}{R}$$

Substituting in above expression; $\hat{q}_{R_{12}} = \frac{\vec{R}_{12}}{R}$
we get.

$$\vec{F}_{12} = \frac{q_1 q_2}{4\pi\epsilon_0 R^2} \cdot \frac{\vec{R}_{12}}{R}$$

$$\therefore \vec{F}_{12} = \boxed{\frac{q_1 q_2}{4\pi\epsilon_0 R^3} \cdot \vec{R}_{12}}$$



or,

$$\vec{F}_{12} = \frac{q_1 q_2}{4\pi\epsilon_0 |\vec{r}_2 - \vec{r}_1|^3} \cdot (\vec{r}_2 - \vec{r}_1)$$

Again, for the force on charge q_1 due to charge q_2 we can write as:

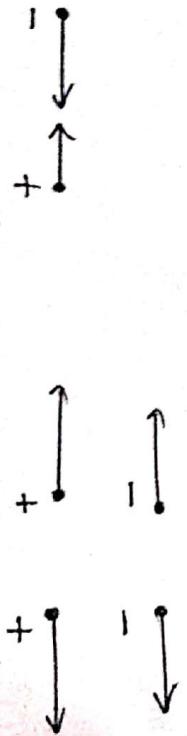
$$\vec{F}_{21} = \frac{q_1 q_2}{4\pi\epsilon_0 R^2} \cdot \hat{q}_{R_{21}}$$

$$\therefore \vec{F}_{21} = - \frac{q_1 q_2}{4\pi\epsilon_0 R^3} \cdot \hat{q}_{R_{21}} = - \frac{q_{R_{21}}}{R} \quad \boxed{\hat{q}_{R_{21}} = - \hat{q}_{R_{12}}}$$

$$\therefore \vec{F}_{21} = - \frac{q_1 q_2}{4\pi\epsilon_0 |\vec{r}_1 - \vec{r}_2|^3} \cdot \vec{r}_{12} \quad \boxed{\vec{r}_{12} = - \vec{r}_{21}}$$

$$\text{or } \vec{F}_{21} = - \frac{q_1 q_2}{4\pi\epsilon_0 |\vec{r}_1 - \vec{r}_2|^3} \cdot (\vec{r}_2 - \vec{r}_1)$$

Notes:



- ① Like charges (charges of same sign) repel each other while unlike charges attract.
- ② The distance bet. the charged bodies q_1 & q_2 must be large compared with the linear dimensions of the bodies i.e. q_1 & q_2 must be point charges.
- ③ q_1 & q_2 must be static (at rest).
- ④ The signs of q_1 & q_2 must be taken into account.

If we have more than two point charges, we can use the principle of superposition to determine the force on a particular charge. The principle states that if there are N charges q_1, q_2, \dots, q_N located respectively, at points with position vectors $\vec{r}_1, \vec{r}_2, \dots, \vec{r}_N$, the resultant force \vec{F} on a charge q located at point \vec{r} is the vector sum of the forces exerted on q by each of the charges q_1, q_2, \dots, q_N .

Hence,

$$\vec{F} = \frac{q q_1 (\vec{r} - \vec{r}_1)}{4\pi\epsilon_0 |\vec{r} - \vec{r}_1|^3} + \frac{q q_2 (\vec{r} - \vec{r}_2)}{4\pi\epsilon_0 |\vec{r} - \vec{r}_2|^3} + \dots + \frac{q q_N (\vec{r} - \vec{r}_N)}{4\pi\epsilon_0 |\vec{r} - \vec{r}_N|^3}$$

or,

$$\vec{F} = \frac{q}{4\pi\epsilon_0} \sum_{k=1}^N \frac{q_k (\vec{r} - \vec{r}_k)}{|\vec{r} - \vec{r}_k|^3}$$

The electric field intensity \vec{E} (or electric field strength) is the force per unit charge when placed in the electric field.

$$\text{Thus, } \vec{E} = \lim_{Q \rightarrow 0} \frac{\vec{F}}{Q}$$

or simply

$$\boxed{\vec{E} = \frac{\vec{F}}{Q}}$$

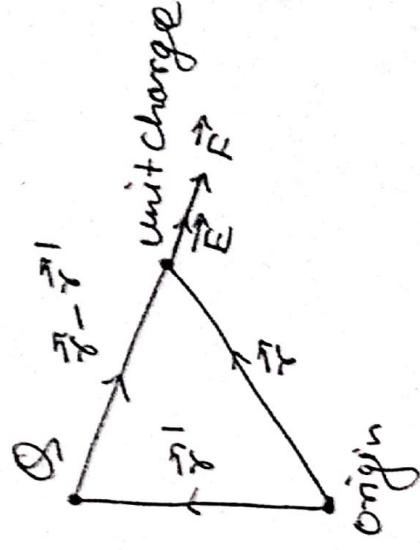
The electric field intensity \vec{E} is in the direction of the force \vec{F} and is measured in newtons/coulomb or volts/meter. The electric field intensity at point \vec{r} due to a point charge located at \vec{r}' is readily obtained as:

$$\boxed{\vec{E} = \frac{Q}{4\pi\epsilon_0 R^2} \hat{a}_r = \frac{Q(\vec{r} - \vec{r}')}{4\pi\epsilon_0 |\vec{r} - \vec{r}'|^3}}$$

Now, For N point charges Q_1, Q_2, \dots, Q_N located at $\vec{r}_1, \vec{r}_2, \vec{r}_3, \dots, \vec{r}_N$, the electric field intensity at point \vec{r} is obtained as:

$$\vec{E} = \frac{Q_1(\vec{r} - \vec{r}_1)}{4\pi\epsilon_0 |\vec{r} - \vec{r}_1|^3} + \frac{Q_2(\vec{r} - \vec{r}_2)}{4\pi\epsilon_0 |\vec{r} - \vec{r}_2|^3} + \dots + \frac{Q_N(\vec{r} - \vec{r}_N)}{4\pi\epsilon_0 |\vec{r} - \vec{r}_N|^3}$$

$$\text{or, } \boxed{\vec{E} = \frac{1}{4\pi\epsilon_0} \sum_{k=1}^N \frac{Q_k(\vec{r} - \vec{r}_k)}{|\vec{r} - \vec{r}_k|^3}}$$



Ques: If the point charge Q is located at origin then find
 2 Force and electric field intensity at point $P(x, y, z)$
 where; a unit charge is located.

Soln:

Given,

Point charge is at origin $O(0, 0, 0)$
 and a unit charge is at located at point $P(x, y, z)$
 i.e. $\vec{r} = x\hat{a}_x + y\hat{a}_y + z\hat{a}_z$
 then

$$r = |\vec{r}| = \sqrt{x^2 + y^2 + z^2} \quad \text{&} \quad \hat{a}_r = \frac{\vec{r}}{|\vec{r}|} = \frac{x\hat{a}_x + y\hat{a}_y + z\hat{a}_z}{\sqrt{x^2 + y^2 + z^2}}$$

Now, we have, the force due to point charge Q on
 the unit charge at point $P(x, y, z)$ is:

$$\begin{aligned} \vec{F} &= \frac{Q \cdot 1}{4\pi\epsilon_0 r^2} \cdot \hat{a}_r = \frac{Q}{4\pi\epsilon_0 r^2} \cdot \frac{\vec{r}}{r} = \frac{Q}{4\pi\epsilon_0 r^3} \cdot \vec{r} \\ &= \frac{Q}{4\pi\epsilon_0} \cdot \frac{(x\hat{a}_x + y\hat{a}_y + z\hat{a}_z)}{(x^2 + y^2 + z^2)^{3/2}} \end{aligned}$$

Since, the charge at point $P(x, y, z)$ is unit charge the
 above calculated force is the electric field intensity.

$$\therefore \vec{E} = \vec{F} = \frac{Q}{4\pi\epsilon_0} \cdot \frac{(x\hat{a}_x + y\hat{a}_y + z\hat{a}_z)}{(x^2 + y^2 + z^2)^{3/2}}$$

If the point charge Q is not at origin but at any point $P(x_1, y_1, z_1)$ and the unit charge is at point $P'(x_2, y_2, z_2)$ then calculate the electric field intensity at P' .

Given: The charge Q is located at $P(x_1, y_1, z_1)$ & unit charge is located at $P'(x_2, y_2, z_2)$ then the position vectors will be

$$\vec{r}_1 = x_1 \hat{a}_x + y_1 \hat{a}_y + z_1 \hat{a}_z$$

$$\vec{r}_2 = x_2 \hat{a}_x + y_2 \hat{a}_y + z_2 \hat{a}_z$$

$$\therefore \vec{r} = \vec{r}_2 - \vec{r}_1 = (x_2 - x_1) \hat{a}_x + (y_2 - y_1) \hat{a}_y + (z_2 - z_1) \hat{a}_z$$

Now, the electric field intensity at $P'(x_2, y_2, z_2)$ is

$$\vec{E} = \frac{Q}{4\pi\epsilon_0} \cdot \frac{\hat{a}_r}{r^2} = \frac{Q}{4\pi\epsilon_0} \cdot \frac{\hat{a}_r}{(x_2 - x_1)^2 + (y_2 - y_1)^2 + (z_2 - z_1)^2}$$

$$\therefore \vec{E} = \frac{Q}{4\pi\epsilon_0} \cdot \frac{[(x_2 - x_1) \hat{a}_x + (y_2 - y_1) \hat{a}_y + (z_2 - z_1) \hat{a}_z]}{\left[(x_2 - x_1)^2 + (y_2 - y_1)^2 + (z_2 - z_1)^2\right]^{3/2}}$$

where, $r = |\vec{r}| = \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2 + (z_2 - z_1)^2}$

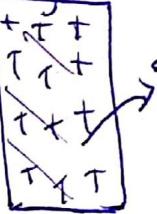
Charge Densities

④ Line charge Density - It is the charge per unit length of the straight line charge. Its unit is Coulomb/meter (C/m) and represented by ρ_L .

$$\text{i.e. } \rho_L = \frac{Q}{l}$$


where, Q = total charge on the straight line
 l = length of straight line charge.

⑤ Surface charge density - It is the charge per unit area of the sheet containing charge. Its unit is Coulomb/m² (C/m²) and represented by ρ_S .

$$\text{i.e. } \rho_S = \frac{Q}{A}$$


where, Q = total charge on the sheet

$$Q = \int_S \rho_S dS$$

A = Area of the sheet

⑥ Volume charge density - It is the charge per unit volume of the space containing charge inside it. Its unit is Coulomb / meter³ (C/m³) and represented by ρ_V .

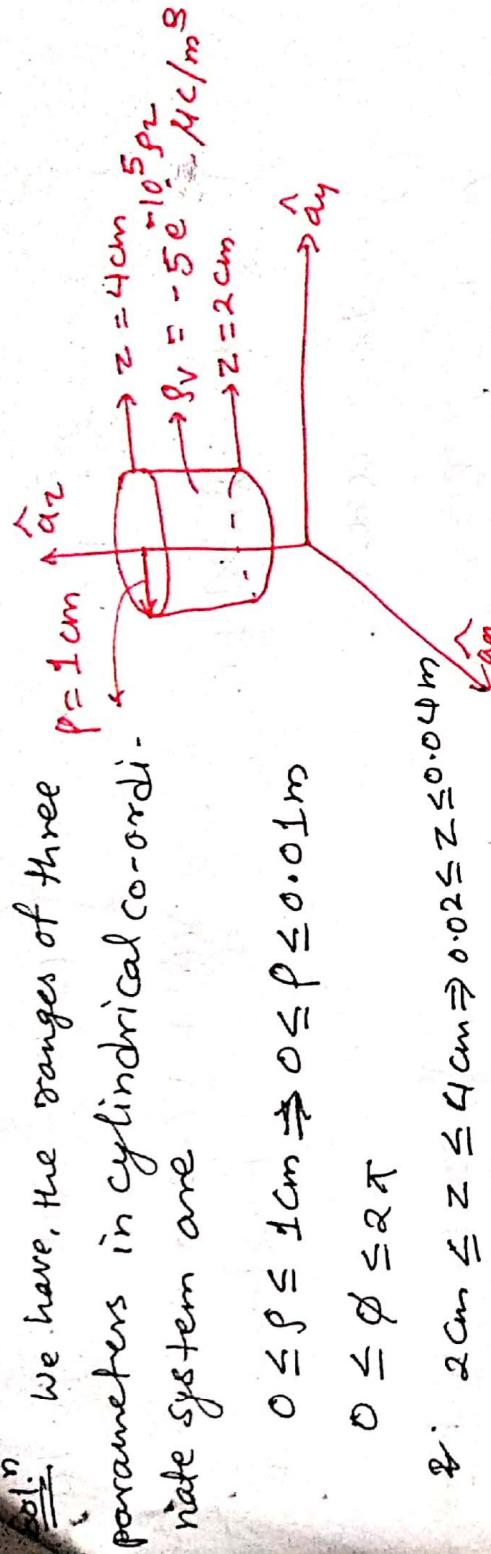
$$\text{i.e. } \rho_V = \lim_{\Delta V \rightarrow 0} \frac{\Delta Q}{\Delta V}$$

$$\text{or, } \Delta Q = \rho_V \Delta V$$

$$\therefore \text{Total charge, } Q = \int_V \rho_V dV = \frac{Q}{\text{vol.}}$$



Q1. Find the total charge within the volume shown below.



Now, we can evaluate the total charge within the volume as:

$$Q = \int_{\text{vol.}} \rho_v \, dv$$

$$\begin{aligned}
 &= \int_{-5e^{-10.5\rho z}}^{5e^{-10.5\rho z}} \int_{0.01}^{0.04} \int_{0}^{2\pi} -5e^{-10.5\rho z} \times 10^{-6} \, dr \, d\phi \, dz \quad [1 \mu C = 10^{-6} C] \\
 &= \int_{\rho=0}^{\rho=0.01} \int_{\phi=0}^{\phi=0.04} \int_{z=0}^{z=0.02} -5e^{-10.5\rho z} \times 10^{-6} \, d\phi \, d\rho \, dz \\
 &= \int_{\rho=0}^{\rho=0.01} \int_{z=0}^{z=0.02} -5e^{-10.5\rho z} \times 10^{-6} (2\pi) \rho \, d\rho \, dz \\
 &= -10\pi \times 10^{-6} \int_{\rho=0}^{\rho=0.01} \int_{z=0}^{z=0.02} e^{-10.5\rho z} \rho \, d\rho \, dz \\
 &= -\pi \times 10^{-5} \int_{\rho=0}^{0.01} \left(\frac{e^{-10.5\rho z}}{-10.5\rho} \right)^{0.04} \rho \, d\rho
 \end{aligned}$$

$$= 10^{-10} \pi \int_{\rho=0}^{\rho=0.01} \left(e^{-10^5 \rho \cdot 0.04} - e^{-10^5 \rho \cdot 0.02} \right) d\rho$$

$$= 10^{-10} \pi \int_{\rho=0}^{\rho=0.01} \left(e^{-4000\rho} - e^{-2000\rho} \right) d\rho$$

$$= 10^{-10} \pi \left\{ \frac{e^{-4000\rho}}{(-4000)} \Big|_0^{0.01} - \frac{e^{-2000\rho}}{(-2000)} \Big|_0^{0.01} \right\}$$

$$= 10^{-10} \pi \left\{ \frac{e^{-40}-e^0}{(-4000)} - \frac{e^{-20}-e^0}{(-2000)} \right\}$$

$$= -\frac{10^{-13}}{4} \pi \cdot (e^{-40}-1) + \frac{10^{-13}}{2} \pi (e^{-20}-1)$$

$$\approx -\frac{10^{-13}}{4} \pi (-1) + \frac{10^{-13}}{2} \pi (-1)$$

$$= 10^{-13} \pi \left[\frac{1}{4} - \frac{1}{2} \right]$$

$$= -\frac{10^{-13}}{4} \pi$$

$$= -\frac{\pi}{40} \rho C$$

$$= -0.0785 \rho C$$

i. Total charge enclosed in a given volume is

$$\Phi = -0.0785 \rho C.$$

Integration

$$\int x \, dx = \frac{x^2}{2} + C$$

$$\int u \, dv = uv - \int v \, du$$

$u(x)$ & $v(x)$ are different functions.

$$\int a \, dx = ax + C$$

Differentiation

$$\int \frac{1}{ax+b} \, dx = \frac{1}{a} \ln |ax+b| + C$$

$$\int \frac{dx}{a^2+x^2} = \frac{1}{a} \tan^{-1} \frac{x}{a} + C$$

$$\int \frac{dx}{x^2-a^2} = \frac{1}{2a} \ln \left| \frac{x-a}{x+a} \right| + C$$

$$\int \frac{dx}{a^2-x^2} = \frac{1}{2a} \ln \left| \frac{a+x}{a-x} \right| + C$$

$$\int \frac{x \, dx}{a^2+x^2} = \frac{1}{2} \ln (x^2+a^2) + C$$

$$\int \frac{x \, dx}{a^2-x^2} = \frac{1}{2} \ln (a^2-x^2) + C$$

$$\begin{aligned} \int \sin x \, dx &= -\cos x + C \\ \int \cos x \, dx &= \sin x + C \end{aligned}$$

$$\begin{aligned} \int e^x \, dx &= e^x + C \\ \int a^x \, dx &= \frac{a^x}{\ln a} + C \end{aligned}$$

$$\begin{aligned} \int x^n \, dx &= \frac{x^{n+1}}{n+1} + C \\ \int x^m a^n \, dx &= \frac{a^m x^{m+n+1}}{m+n+1} + C \end{aligned}$$

Electric field intensity due to a line charge

Let us assume a straight-line charge extending along the z-axis in a cylindrical co-ordinate system from $-\infty$ to ∞ , as shown in figure. We need to evaluate the electric field intensity \vec{E} at any point resulting from a uniform line charge density ρ_L .

If we vary ϕ keeping ρ & z constant

the field does not change that means azimuthal symmetry is present.

Again, if we keep ϕ & P constant and vary z , the field at arbitrary point P will not be changed. This means it has

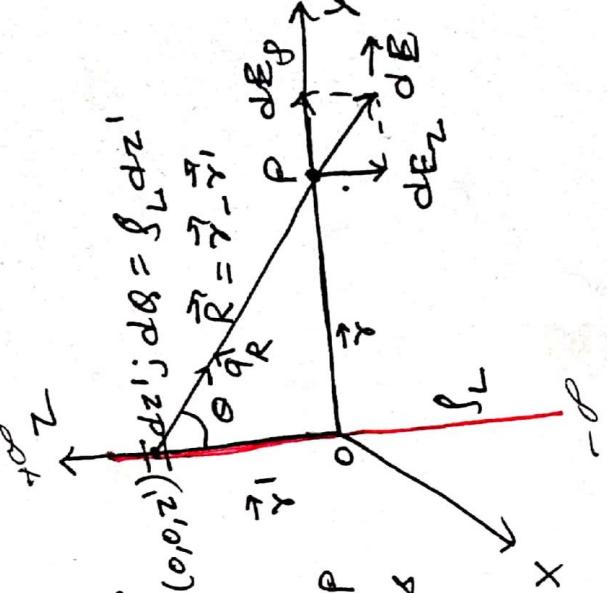
axial symmetry it present.

But if we change P keeping z & ϕ constant the field value changes accordingly. so, it says that the field changes only with the variation of P .

Now, from the figure we can see that the field has two components \vec{E}_z & \vec{E}_ϕ . Since, the line charge is symmetric about origin; the field due to +ve z-direction cancels the field due to -ve z-direction. So, we will have only \vec{E}_ϕ component. Now, let us choose a point $P(0, y, 0)$ on the y-axis at which the field is to be determined.

i. The incremental field due to the incremental charge $d\rho = \rho_L dz'$ at point P is given as:

$$d\vec{E} = \frac{\rho_L dz' (\hat{z} - \hat{z}')}{4\pi\epsilon_0 1^2 + (z - z')^2}$$



$$\begin{aligned} \hat{z}' &= y\hat{j} \\ \hat{z} &= z'\hat{i} \end{aligned}$$

$$d\vec{E} = \frac{\rho_L dz' (\hat{z} - \hat{z}')}{4\pi\epsilon_0 1^2 + (z - z')^2}$$

$$\text{and } \vec{r} - \vec{r}' = \rho \hat{a}_\rho - z' \hat{a}_z$$

$$\text{Therefore, } d\vec{E} = \frac{\rho_L dz' (\rho \hat{a}_\rho + z' \hat{a}_z)}{4\pi\epsilon_0 (\rho^2 + z'^2)^{3/2}}$$

since, only E_ρ component is present we may simplify;

$$dE_\rho = \frac{\rho \rho_L dz'}{4\pi\epsilon_0 (\rho^2 + z'^2)^{3/2}}$$

$$\text{and } E_\rho = \int_{-\infty}^{\infty} \frac{\rho \rho_L dz'}{4\pi\epsilon_0 (\rho^2 + z'^2)^{3/2}}$$

Now, let us assume $z' = \rho \cot\theta$, we have

$$E_\rho = \frac{\rho_L}{4\pi\epsilon_0 \rho} \rho \left(\frac{1}{\rho^2} \cdot \frac{z'}{\sqrt{\rho^2 + z'^2}} \right)_{\rho=0}^\infty$$

$$= -\frac{\rho_L}{4\pi\epsilon_0 \rho^2} \int_0^\pi \frac{\sin\theta d\theta}{\sqrt{1 + (\cot\theta)^2}}$$

$$= -\frac{\rho_L}{4\pi\epsilon_0 \rho^2} \int_0^\pi \frac{\cos\theta d\theta}{\csc^3\theta}$$

$$= -\frac{\rho_L}{4\pi\epsilon_0 \rho^2} \int_0^\pi \frac{\cos\theta d\theta}{\sin^2\theta}$$

$$= -\frac{\rho_L}{4\pi\epsilon_0 \rho^2} \left[-\cos\theta \right]_0^\pi$$

$$= \frac{\rho_L}{4\pi\epsilon_0 \rho^2} [\cos 0 - \cos \pi]$$

$$= \frac{\rho_L}{4\pi\epsilon_0 \rho^2}$$

$$\boxed{E_\rho = \frac{\rho_L}{2\pi\epsilon_0 \rho}}$$

Here, we see that the field falls off

inversely with the distance to the charged line, as compared to point charge, where the field decreased with the square of the distance.

Electric field intensity due to sheet charge

Let us consider a sheet of charge, having uniform charge density $\rho_s \text{ C/m}^2$ is placed in the yz -plane as shown in figure. As from the symmetry, the field due to the sheet charge at any arbitrary point P does not vary with the variation of $z \& y$.

The $y \& z$ components of the field

at point $P(x, 0, 0)$ arising from differential elements of charge symmetrically located with respect to $R = \sqrt{x^2 + y^2}$ to the point P will cancel.

Hence, only \vec{E}_x component is present.

Let us divide the sheet into differential-width strips, so that we can use the infinite line charge field expression. Here,

the line charge density $\rho_L = \rho_s dy'$, and the distance from this line charge to the general point P on the x axis is $R = \sqrt{x^2 + y'^2}$.

Then, the field E_x due to differential width strip is

$$dE_x = \frac{\rho_s dy'}{2\pi\epsilon_0 \sqrt{x^2 + y'^2}} \cdot \cos\theta = \frac{\rho_s}{2\pi\epsilon_0} \cdot \frac{x}{(x^2 + y'^2)} \cdot dy' \\ [dE_x = dE \cos\theta]$$

Now, integrating effects of all the strips,

$$E_x = \frac{\rho_s}{2\pi\epsilon_0} \cdot \int_{-\infty}^{\infty} \frac{x dy'}{x^2 + y'^2} = \frac{\rho_s}{2\pi\epsilon_0} \cdot \tan^{-1} \frac{y'}{x} \Big|_{-\infty}^{\infty} = \frac{\rho_s}{2\epsilon_0}$$

If the point P were chosen at -ve x-axis the field will be $E_x = -\frac{\rho_s}{2\epsilon_0}$

For the direction we use the normal vector perpendicular to the sheet containing the charge and is directed outward or away from the sheet.

$$\therefore \vec{E} = \frac{\rho_s \hat{a}_n}{2\epsilon_0}$$

If a second infinite sheet of charge, having a negative charge density $-\rho_s$, is located in the plane $x=a$, we may find the total field by adding the contribution of each sheet.

In the region, $x > a$

$$\vec{E}_+ = \frac{\rho_s \hat{a}_n}{2\epsilon_0}$$

$$\vec{E}_- = -\frac{\rho_s \hat{a}_n}{2\epsilon_0}$$

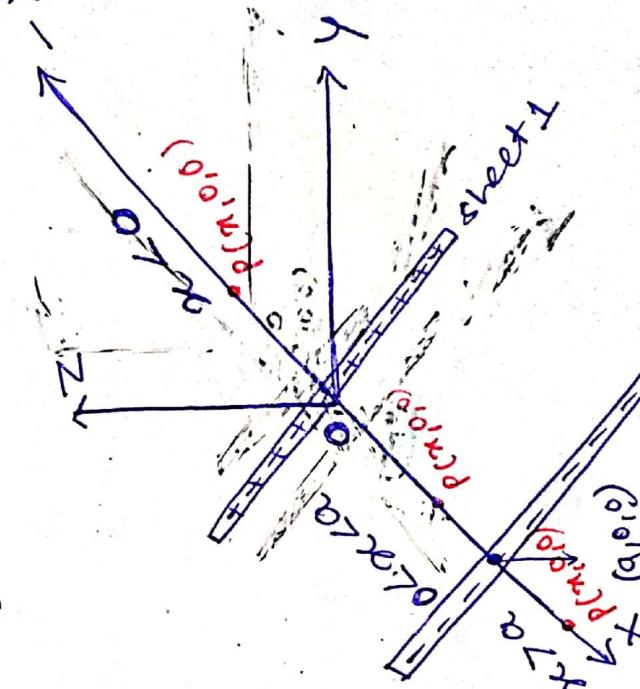
$$\therefore \vec{E} = \vec{E}_+ + \vec{E}_- = 0$$

and for $x < 0$,

$$\vec{E}_+ = -\frac{\rho_s}{2\epsilon_0} \hat{a}_n$$

$$\vec{E}_- = \frac{(-\rho_s)}{2\epsilon_0} \hat{a}_n = \frac{\rho_s}{2\epsilon_0} \hat{a}_n$$

$$\therefore \vec{E} = \vec{E}_+ + \vec{E}_- = 0$$



and when $0 < x < a$,

$$\vec{E}_+ = \frac{\rho_s}{2\epsilon_0} \hat{a}_x$$

$$\vec{E}_- = -\frac{(-\rho_s)}{2\epsilon_0} \hat{a}_x = \frac{\rho_s}{2\epsilon_0} \hat{a}_x$$

$$\therefore \vec{E} = \vec{E}_+ + \vec{E}_- = \left[\frac{\rho_s}{2\epsilon_0} + \frac{\rho_s}{2\epsilon_0} \right] \hat{a}_x$$

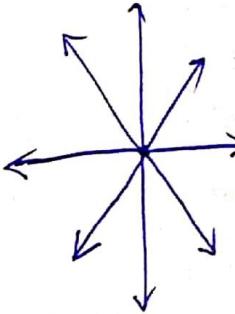
$$\text{or, } \vec{E} = \frac{\rho_s}{\epsilon_0} \hat{a}_x$$

It is the field bet' the parallel plates of an air capacitor, provided the linear dimensions of the plates are very much greater than their separation.

Equations of Streamlines (Flux Lines/Direction Lines)

Streamlines are those lines which are everywhere tangent to \vec{E} around the charge. Streamlines are also called flux lines or direction lines.

A small positive test charge placed at any point in this field and free to move would accelerate in the dir' of the streamline passing through that point.



streamlines

The equation of streamlines is obtained by solving the differential equation $\frac{E_y}{E_x} = \frac{dy}{dx} = \lim_{\Delta x \rightarrow 0} \frac{\Delta y}{\Delta x}$ obtained from the geom.

try.

Let us consider the field of the uniform line charge with line charge density $\rho_L = 2\pi\epsilon_0$

$$\text{then, } \vec{E} = \frac{1}{\rho} \hat{a}_\rho \left[\vec{E} = \frac{\rho_L}{2\pi\epsilon_0\rho} \hat{a}_\rho = \frac{2\pi\epsilon_0}{2\pi\epsilon_0\rho} \hat{a}_\rho = \frac{1}{\rho} \hat{a}_\rho \right]$$

In rectangular Co-ordinates; [set $E_x = 0$]

$$\vec{E} = \frac{x}{x^2+y^2} \hat{a}_x + \frac{y}{x^2+y^2} \hat{a}_y$$

Thus, from differential equations

$$\boxed{\frac{dy}{dx} = \frac{E_y}{E_x} = \frac{y}{x}}$$

$$\text{or, } \frac{dy}{dx} = \frac{y}{x}$$

$$\text{or, } \frac{dy}{y} = -\frac{dx}{x}$$

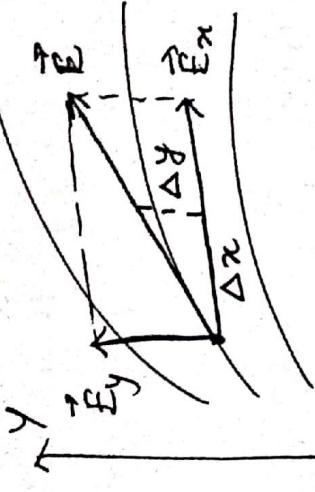
$$\text{or, } \ln y = \ln x + C, \text{ or } \ln x + \ln C$$

from which the equations of streamlines are obtained as:

$$y = Cx$$

If we want to find the eqn of one particular streamline, say one passing through $P(-2, 7, 10)$, we substitute the co-ordinates of that point into the streamline eqn and evaluate C. i.e. $7 = C(-2)$

$$\therefore C = -3.5$$



$$\vec{E} = \frac{1}{\rho} \hat{a}_\rho \left[\vec{E} = \frac{\rho_L}{2\pi\epsilon_0\rho} \hat{a}_\rho = \frac{2\pi\epsilon_0}{2\pi\epsilon_0\rho} \hat{a}_\rho = \frac{1}{\rho} \hat{a}_\rho \right]$$

$$\begin{aligned} E_x &= \vec{E} \cdot \hat{a}_x = \frac{1}{\rho} \hat{a}_\rho \cdot \hat{a}_x \\ &= \frac{1}{\rho} \cos \theta = \frac{x}{\rho^2} \\ \therefore E_x &= \frac{x}{x^2+y^2} \\ &\text{& } E_y = \vec{E} \cdot \hat{a}_y = \frac{y}{\rho^2} = \frac{y}{x^2+y^2} \end{aligned}$$

so, $y = -3.5x$ is the required streamline passing through $P(-2, 7, 10)$.

Q1. Find the equation of that streamline that passes through the point $P(1, 4, -2)$ in the field $\vec{E} = -\frac{8x}{y^2} \hat{i}_x + \frac{4x^2}{y^2} \hat{j}_y$

Soln.

$$\text{Given, } \vec{E} = -\frac{8x}{y^2} \hat{i}_x + \frac{4x^2}{y^2} \hat{j}_y$$

$$\text{where, } E_x = -\frac{8x}{y^2} \quad \& \quad E_y = \frac{4x^2}{y^2}$$

Now, we have from differential equation

$$\frac{dy}{dx} = \frac{E_y}{E_x} = \frac{\frac{4x^2}{y^2}}{-\frac{8x}{y^2}} = -\frac{x}{2y}$$

$$\text{or, } 2y dy = -x dx$$

Integrating both sides

$$\frac{2y^2}{2} = -\frac{x^2}{2} + C_1$$

$$\text{or, } y^2 = -\frac{x^2}{2} + C_1$$

Since, this streamline passes through $P(1, 4, -2)$

$$16 = -\frac{1}{2} + C_1$$

$$\text{or, } C_1 = 33$$

The Eqn. of streamline is

$$y^2 = -\frac{x^2}{2} + \frac{33}{2}$$

$$\text{or, } x^2 + 2y^2 = 33 \quad /$$

Qn: A Uniform line charge having charge density ρ_L is placed at $x=6$ and $y=8$. Find the electric field intensity due to this line charge at point (x, y, z) .

Sol: Here, we have ρ_L = line charge density of a line charge at $x=6$ & $y=8$.

So, the point in XY-plane is $(6, 8, 0)$ where the line charge is passed.

Also, the point $(x, y, 0)$ is the projected point of $P(x, y, z)$ in XY-plane.

Now, the distance between the line charge and the point $P(x, y, z)$ can be calculated by calculating the distance bet. $(6, 8, 0)$ & $(x, y, 0)$ as:

$$|\vec{R}| = R = \sqrt{(x-6)^2 + (y-8)^2}$$

$$\text{or } \vec{R} = (x-6)\hat{a}_x + (y-8)\hat{a}_y$$

Again, the electric field intensity at point P is

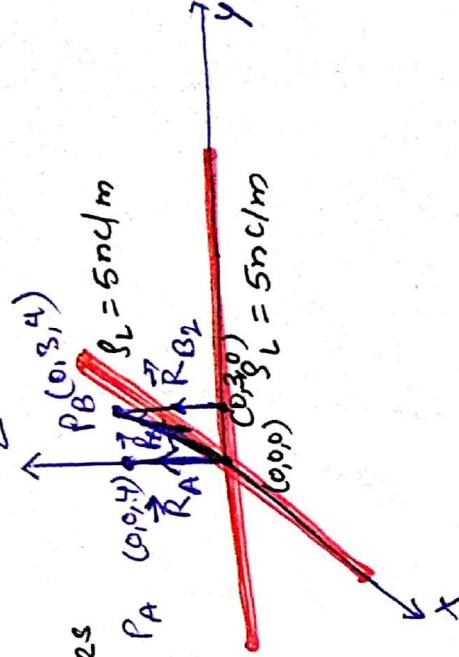
$$\vec{E}_P = \frac{\rho_L}{2\pi\epsilon_0 R} \cdot \hat{a}_R = \frac{\rho_L}{2\pi\epsilon_0} \cdot \frac{1}{\sqrt{(x-6)^2 + (y-8)^2}} \cdot \hat{a}_R$$

$$\text{where, } \hat{a}_R = \frac{(x-6)\hat{a}_x + (y-8)\hat{a}_y}{\sqrt{(x-6)^2 + (y-8)^2}}$$

$$\therefore \vec{E}_P = \frac{\rho_L [(x-6)\hat{a}_x + (y-8)\hat{a}_y]}{2\pi\epsilon_0 [(x-6)^2 + (y-8)^2]} \text{ where, } \epsilon_0 = 8.854 \times 10^{-12} \text{ F/m}$$

Qn: Infinite uniform line charges of 5 nC/m lie along the +ve and -ve X and Y axes in free space. Find \vec{E} at @ $P_A(0,0,4)$ and @ $P_B(0,3,4)$

Sol:



Here, the infinite uniform line charges of charge density $\rho_L = 5 \text{ nC/m}$ lie along the +ve and -ve X & Y axes as shown in figure.

Now, @ for the \vec{E} at $P_A(0,0,4)$

we need to calculate the distance

vector \vec{R}_A as:

$$\begin{aligned}\vec{R}_A &= (0-0)\hat{a}_x + (0-0)\hat{a}_y + (4-0)\hat{a}_z \\ &= 4\hat{a}_z\end{aligned}$$

$$R_A = |\vec{R}_A| = \sqrt{4^2} = 4 \quad \text{also, } \hat{a}_{RA} = \hat{a}_z$$

so, \vec{E}_A at $P_A(0,0,4)$ due to line charge at X -axis is

$$\vec{E}_{Ax} = \frac{\rho_L}{2\pi\epsilon_0 R_A} \cdot \hat{a}_{RA} = \frac{5 \times 10^{-9}}{2\pi \times 8.854 \times 10^{-12} \times 4} \cdot \hat{a}_{RA} = \frac{5 \times 10^{-9}}{2\pi \times 8.854 \times 10^{-12} \times 4} \cdot \hat{a}_z$$

$$= \frac{5 \times 10^{-9+12}}{8\pi \times 8.854} \cdot \hat{a}_z$$

$$\therefore \vec{E}_{Ax} = \frac{5000}{70.832\pi} \hat{a}_z \text{ V/m.}$$

Again, the \vec{E} at $P_A(0,0,4)$ due to line charge at Y -axis is same as due to line charge at X -axis.

$$\therefore \vec{E}_{Ay} = \vec{E}_{Ax} = \frac{5000}{70.832\pi} \hat{a}_z \text{ V/m.}$$

Hence, the total field intensity at $P_A(0,0,4)$ due to line charges at x & y axes is

$$\vec{E} = \vec{E}_{A_x} + \vec{E}_{A_y} = 2 \times \frac{5000}{70.83\pi} \cdot \hat{q}_2 \text{ V/m.}$$

$$\therefore \vec{E} = 45 \hat{q}_2 \text{ V/m.}$$

Again, (b) For the \vec{E} at $P_B(0,3,4)$ due to the line charge at x -axis

$$\text{if } \vec{E}_{Bx} = \frac{f_L}{2\pi\epsilon_0 R_{Bx}} \cdot \hat{q}_{R_{Bx}}$$

$$\text{where, } R_{Bx} = (0-0)\hat{a}_m + (3-0)\hat{a}_y + (4-0)\hat{a}_z \\ = 3\hat{a}_y + 4\hat{a}_z$$

$$R_{Bx} = |\vec{R}_{Bx}| = \sqrt{3^2 + 4^2} = 5 \\ \text{or } \hat{q}_{R_{Bx}} = \frac{\vec{R}_{Bx}}{|R_{Bx}|} = \frac{3\hat{a}_y + 4\hat{a}_z}{5} = \frac{3}{5}\hat{a}_y + \frac{4}{5}\hat{a}_z$$

$$\therefore \vec{E}_{Bx} = \frac{5 \times 10^{-9}}{2\pi \times 8.854 \times 10^{-12}} \cdot \frac{(3\hat{a}_y + 4\hat{a}_z)}{25} \\ = (10.78 \hat{a}_y + 14.38 \hat{a}_z) \text{ V/m}$$

Again, For the \vec{E} at $P_B(0,3,4)$ due to the line charge at y -axis is

$$\vec{E}_{By} = \frac{f_L}{2\pi\epsilon_0 R_{By}} \cdot \hat{q}_{R_{By}}$$

$$\text{where, } R_{By} = (0-0)\hat{a}_m + (3-3)\hat{a}_y + (4-0)\hat{a}_z = 4\hat{a}_z \\ \text{or } \hat{q}_{R_{By}} = \frac{\vec{R}_{By}}{|R_{By}|} = \frac{4\hat{a}_z}{|R_{By}|} = \frac{\hat{a}_z}{4}$$

$$R_{By} = |\vec{R}_{By}| = 4 \\ \text{or } \hat{q}_{R_{By}} = \frac{\vec{R}_{By}}{|R_{By}|} = \frac{\hat{a}_z}{4}$$

$$\vec{E}_{B1} = \frac{5 \times 10^{-9}}{2\pi \times 8.85 \times 10^{-12}} \cdot \frac{\hat{a}_z}{4}$$

$$= 22.47 \hat{a}_z \text{ V/m}$$

Total \vec{E} at $P_3(0, 3, 4)$ due to line charges at X & Y axes

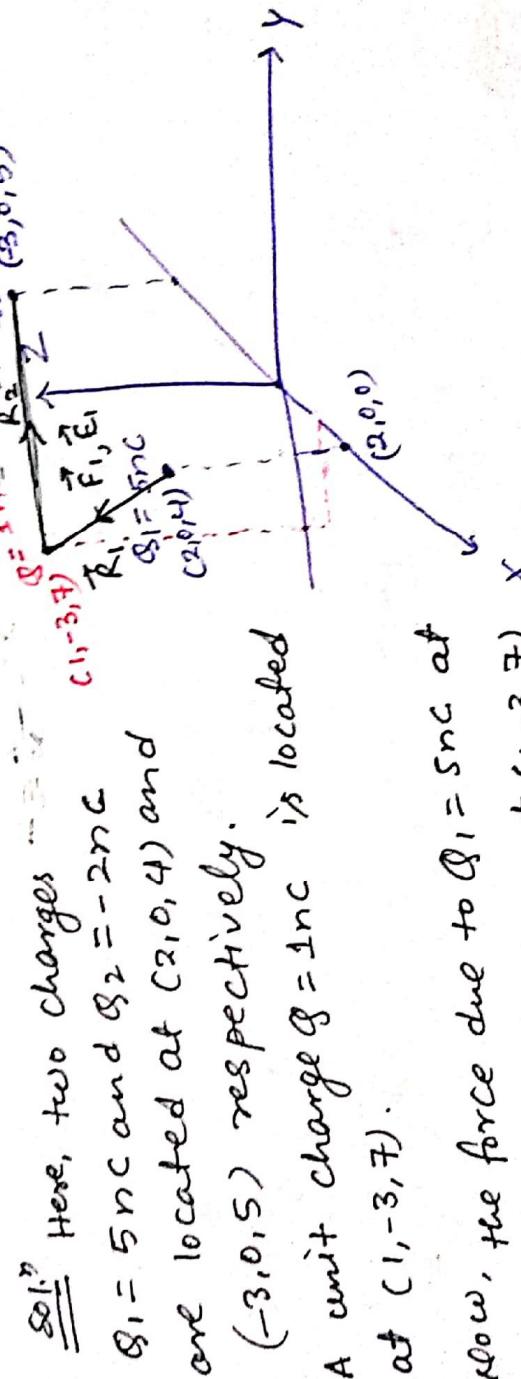
$$\text{if } \vec{E} = \vec{E}_{Bx} + \vec{E}_{By} = (10.78 \hat{a}_y + 14.38 \hat{a}_z) + 22.47 \hat{a}_z$$

$$= 10.78 \hat{a}_y + 36.9 \hat{a}_z \text{ V/m.}$$

Sri: Point charges 5nC and -2nC are located at $(2, 0, 4)$

and $(-3, 0, 5)$ respectively.

- ② Determine the force on a 1nC point charge located at $(1, -3, 7)$ $-1.004 \hat{a}_y - 1.384 \hat{a}_z + 1.04 \hat{a}_x$ N/C
 ③ Find the electric field \vec{E} at $(1, -3, 7)$ $-1.004 \hat{a}_y - 1.384 \hat{a}_z$ N/C



Now, the force due to $Q_1 = 5\text{nC}$ at $(2, 0, 4)$

$$\text{if } \vec{F}_1 = \frac{Q_1 \cdot \vec{q}}{4\pi \epsilon_0 R_1^2} \cdot \hat{a}_{R_1}$$

$$\text{where, } \vec{R}_1 = (1-2) \hat{a}_x + (-3-0) \hat{a}_y + (7-4) \hat{a}_z$$

$$= -1 \hat{a}_x - 3 \hat{a}_y + 3 \hat{a}_z$$

$$R_1 = |\vec{R}_1| = \sqrt{(-1)^2 + (-3)^2 + 3^2} = \sqrt{19} = 4.36$$

$$\text{if } \vec{q}_{R_1} = \frac{\vec{R}_1}{|\vec{R}_1|} = \frac{-1}{4.36} \hat{a}_x - \frac{3}{4.36} \hat{a}_y + \frac{3}{4.36} \hat{a}_z$$

$$\therefore \vec{F}_1 = \frac{5 \times 1 \times 10^{-9} \times 10^{-9}}{4\pi \times \left(\frac{10^{-9}}{36\pi}\right)} \cdot \frac{(-\hat{a}_x - 3\hat{a}_y + 3\hat{a}_z)}{(4.36)^3}$$

$$= \frac{45 \times 10^{-9}}{82.88} \cdot (-\hat{a}_x - 3\hat{a}_y + 3\hat{a}_z)$$

$$= (-0.543\hat{a}_x - 1.63\hat{a}_y + 1.63\hat{a}_z) \text{ N}$$

Also, the force due to $\varphi_2 = -2 \text{ nc}$ at $(-3, 0, 5)$ to $\varphi = 1 \text{ nc}$ at $(1, -3, 7)$ is

$$\vec{F}_2 = \frac{\varphi_2 \cdot \varphi}{4\pi\epsilon_0 R^2} \cdot \hat{a}_{R_2}$$

$$\begin{aligned} \text{where, } \vec{R}_2 &= (1+3)\hat{a}_x + (-3-0)\hat{a}_y + (7-5)\hat{a}_z \\ &= 4\hat{a}_x - 3\hat{a}_y + 2\hat{a}_z \end{aligned}$$

$$R_2 = |\vec{R}_2| = \sqrt{4^2 + (-3)^2 + 2^2} = \sqrt{29} = 5.385$$

$$\text{& } \hat{a}_{R_2} = \frac{\vec{R}_2}{|\vec{R}_2|} = \frac{4}{5.385} \hat{a}_x$$

$$\therefore \vec{F}_2 = \frac{-2 \times 1 \times 10^{-9} \times 10^{-9}}{4\pi \times \left(\frac{10^{-9}}{36\pi}\right)} \cdot \frac{(4\hat{a}_x - 3\hat{a}_y + 2\hat{a}_z)}{5.385^3}$$

$$= -\frac{18}{5.385^3} \cdot (4\hat{a}_x - 3\hat{a}_y + 2\hat{a}_z)$$

$$\begin{aligned} &= -0.115 (4\hat{a}_x - 3\hat{a}_y + 2\hat{a}_z) \text{ N} \\ &= (-0.461\hat{a}_x + 0.346\hat{a}_y - 0.2305\hat{a}_z) \text{ N} \end{aligned}$$

Total force at $(1, -3, 7)$ is

$$\begin{aligned}\vec{F} = \vec{F}_1 + \vec{F}_2 &= -0.543\hat{a}_x - 1.63\hat{a}_y + 1.63\hat{a}_z - 0.461\hat{a}_x \\ &\quad + 0.346\hat{a}_y - 0.2305\hat{a}_z \\ &= (-1.004\hat{a}_x - 1.284\hat{a}_y + 1.4\hat{a}_z) \text{ N}\end{aligned}$$

Now, (b) \vec{E} at $(1, -3, 7)$ is

$$\vec{E} = \frac{\vec{F}}{q} = \frac{(-1.004\hat{a}_x - 1.284\hat{a}_y + 1.4\hat{a}_z) \times 10^{-9}}{1 \times 10^{-9}}$$

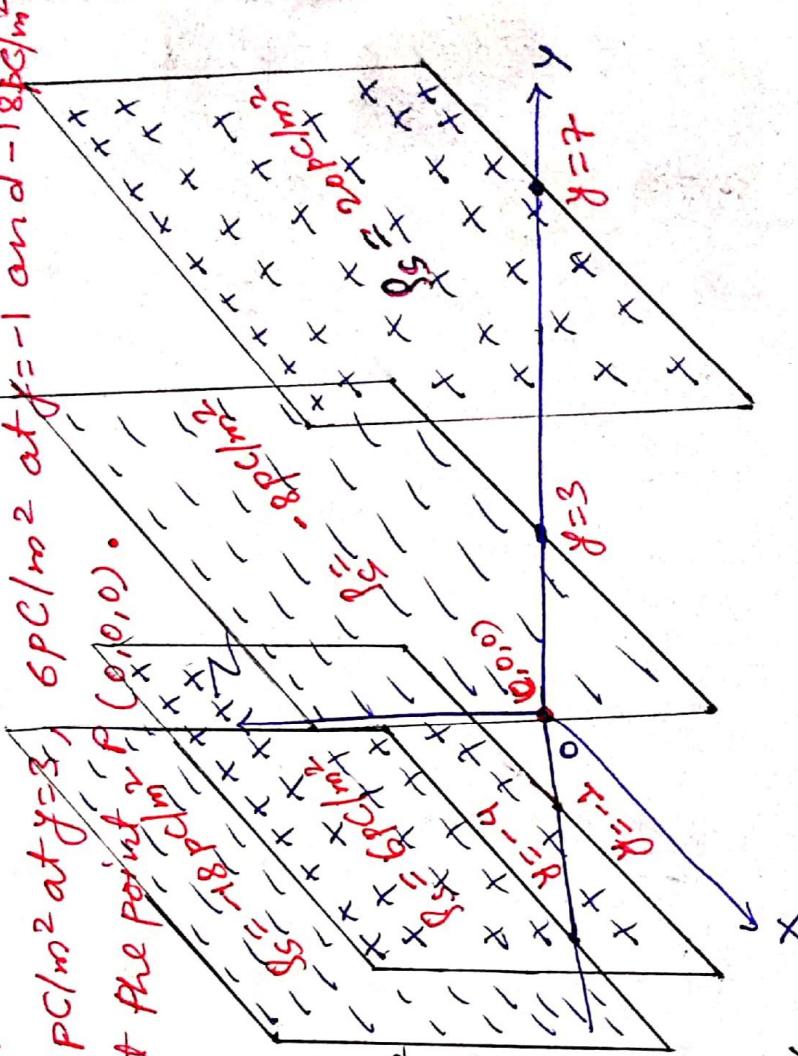
$$\therefore \vec{E} = (-1.004\hat{a}_x - 1.284\hat{a}_y + 1.4\hat{a}_z) \text{ V/m}.$$

Qn: Four infinite uniform sheets of charge are located as follows:

On $y=3$ at $x=7, -8 \text{ PC/m}^2$, 6 PC/m^2 at $x=1$ and -18 PC/m^2 at $x=-1$, -8 PC/m^2 at $y=7$, 20 PC/m^2 at $y=-1$. Find \vec{E} at the point $P(0, 0, 0)$.

Sol.?

Here, the sheet charges of charge densities $20 \text{ PC/m}^2, -8 \text{ PC/m}^2, 6 \text{ PC/m}^2$ and -18 PC/m^2 are located at $y=3, x=3, y=-1$ & $x=-4$ respectively.



then, the electric field intensity due to $\rho_s = 20 \text{ PC/m}^2$ (at $y=7$) to the test charge at $P(0,0,0)$ is

$$\vec{E}_{20} = \frac{\rho_s}{2\epsilon_0} \hat{a}_x = \frac{10 \times 10^{-12}}{2 \times \left(\frac{10^{-9}}{36\pi}\right)} \cdot (-\hat{a}_x)$$

$$\therefore \vec{E}_{20} = -360\pi \times 10^{-3} \hat{a}_y \text{ V/m.}$$

Again,

Electric field intensity due to $p_s = -8 \text{ PC/m}^2$ (at $y=3$) to the test charge at $P(0,0,0)$ is

$$\vec{E}_{-8} = \frac{p_s}{2\epsilon_0} \hat{a}_y = -\frac{-8 \times 10^{-12}}{2 \times 10^{-9}} \cdot (-\hat{a}_y)$$

$$\therefore \vec{E}_{-8} = 144\pi \times 10^{-3} \hat{a}_y \text{ V/m}$$

Also, Electric field intensity due to $p_s = 8 \text{ PC/m}^2$ (at $y=-1$) to the test charge at $P(0,0,0)$ is

$$\vec{E}_6 = \frac{p_s}{2\epsilon_0} \hat{a}_y = \frac{\frac{2}{6} \times 10^{-12}}{2 \times 10^{-9}} \hat{a}_y$$

$$\therefore \vec{E}_6 = 108\pi \times 10^{-3} \hat{a}_y \text{ V/m}$$

Similarly, Electric field intensity due to $p_s = -18 \text{ PC/m}^2$ (at $y=-4$) to the test charge at $P(0,0,0)$ is

$$\vec{E}_{-18} = \frac{p_s}{2\epsilon_0} \hat{a}_y = -\frac{-18 \times 10^{-12}}{2 \times 10^{-9}} \cdot \hat{a}_y$$

$$\therefore \vec{E}_{-18} = -324\pi \times 10^{-3} \hat{a}_y \text{ V/m}$$

Finally,

Total electric field intensity at $P(0,0,0)$ is

$$\vec{E} = \vec{E}_{20} + \vec{E}_{-8} + \vec{E}_6 + \vec{E}_{-18}$$

$$= (-360\pi \times 10^{-3} + 144\pi \times 10^{-3} + 108\pi \times 10^{-3} - 324\pi \times 10^{-3}) \hat{a}_y \text{ V/m}$$

Qn A line charge of 8 nC/m is located at $x = -1, y = -1$, a point charge of $6 \mu\text{C}$ at $y = -4$ and a surface charge of 30 pC/m^2 at $z = 0$. Find \vec{E} at $P(4, 1, 3)$.

Sol: Here, a line charge density $\rho_L = 8 \text{ nC/m}$ is located at $x = -1, y = -1$, a point charge of $Q = 6 \mu\text{C}$ at $y = -4$ and a surface charge density $\rho_s = 30 \text{ pC/m}^2$ at $z = 0$ (i -exy-plane).

then, The electric field

intensity at point $P(4, 1, 3)$ due to a line charge is

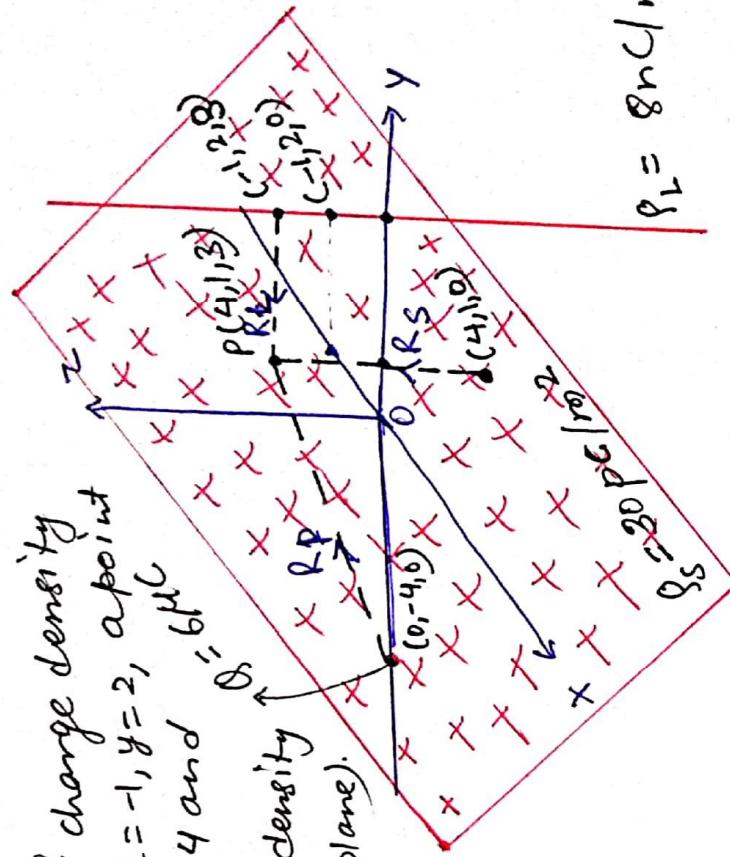
$$\vec{E}_L = \frac{\rho_L}{2\pi\epsilon_0 R_L} \cdot \hat{a}_{R_L}$$

$$\begin{aligned} \text{where, } \vec{R}_L &= [4 - (-1)]\hat{a}_x + (1 - 2)\hat{a}_y + (3 - 3)\hat{a}_z \\ &= 5\hat{a}_x - \hat{a}_y \\ \Rightarrow R_L &= |\vec{R}_L| = \sqrt{5^2 + 1^2} = \sqrt{26}, \quad \hat{a}_{R_L} = \frac{5\hat{a}_x - \hat{a}_y}{\sqrt{26}} \\ \therefore \vec{E}_L &= \frac{8 \times 10^{-9} [5\hat{a}_x - \hat{a}_y]}{2 \cdot \pi \cdot 10^{-9} \cdot \sqrt{26} \cdot \sqrt{26}} \\ &= \frac{8 \times 18}{26} [5\hat{a}_x - \hat{a}_y] \\ &= 27.69 \hat{a}_x - 5.54 \hat{a}_y \text{ V/m} \end{aligned}$$

Again, the electric field intensity due to point charge is

$$\vec{E}_P = \frac{Q}{4\pi\epsilon_0 R_P^2} \hat{a}_{RP}$$

$$\begin{aligned} \text{where, } \vec{R}_P &= (4 - 0)\hat{a}_x + (1 + 4)\hat{a}_y + (3 - 0)\hat{a}_z \\ &= 4\hat{a}_x + 5\hat{a}_y + 3\hat{a}_z \end{aligned}$$



$$R_P = |\vec{R}_P| = \sqrt{16 + 25 + 9} = \sqrt{50} = 5\sqrt{2}$$

$$\& \hat{E}_P = \frac{4\hat{a}_x + 5\hat{a}_y + 3\hat{a}_z}{5\sqrt{2}}$$

$$\therefore \vec{E}_P = \frac{6 \times 10^{-6} (4\hat{a}_x + 5\hat{a}_y + 3\hat{a}_z)}{4\pi \times 10^{-9} \times (5\sqrt{2})^3}$$

$$\begin{aligned}
 &= \frac{9 \times 6 \times 10^{-3}}{353.55} (4\hat{a}_x + 5\hat{a}_y + 3\hat{a}_z) \\
 &= 152.074 (4\hat{a}_x + 5\hat{a}_y + 3\hat{a}_z) \\
 &= 610.95 \hat{a}_x + 763.68 \hat{a}_y + 458.24 \hat{a}_z \text{ V/m}.
 \end{aligned}$$

And, the electric field intensity due to sheet charge is

$$\vec{E}_S = \frac{\rho_S}{2\epsilon_0} \hat{a}_{R_S}$$

$$\text{where, } \vec{R}_S = (4-4)\hat{a}_x + (1-1)\hat{a}_y + (3-0)\hat{a}_z$$

$$R_S = |\vec{R}_S| = 3$$

$$\& \hat{a}_{R_S} = \frac{3\hat{a}_x}{3} - \hat{a}_z \quad [\text{or directly } \hat{a}_{R_S} = \hat{a}_z]$$

$$\begin{aligned}
 \therefore \vec{E}_S &= \frac{30 \times 10^{-12}}{2 \times 10^{-9}} (\hat{a}_z) \\
 &= 30 \times 10^{-12} \times 10^{-3} \hat{a}_z \\
 &= 1.696 \hat{a}_z \text{ V/m}.
 \end{aligned}$$

i. Total electric field intensity of P(4, 1, 3) is

$$\vec{E} = \vec{E}_L + \vec{E}_P + \vec{E}_S = 638.64 \hat{a}_x + 758.14 \hat{a}_y + 459.91 \hat{a}_z \text{ V/m}$$

Electric Flux Density

रवित काशल
इन्जिनियर

Faraday's Law

In 1837 Faraday performed an experiment about the static charge. He made the concentric metallic spheres one with small diameter and put the dielectric material in between them. He charged the inner sphere with a known positive charge & the outer sphere was discharged by connecting it to ground. He then separated the outer sphere to measure the induced -ve charge on it. He found that the total charge on the outer sphere was equal in magnitude to the original charge placed on the inner sphere and that was true regardless of the dielectric material in bet." the two spheres. He concluded that there was some sort of "displacement" from inner sphere to the outer which was independent of the medium; which is referred to as displacement flux or simply electric flux.

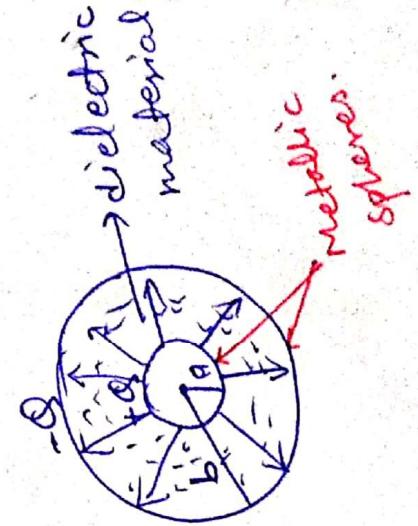
Faraday's experiments also showed that larger the charge in inner sphere; larger will be the induced charge in outer sphere; leading to direct proportionality bet. the electric flux and the charge on the inner sphere. The constant of proportionality is different for different system of units involved. In SI unit the constant is equal to unity. i.e. ψ (flux) $\propto Q$

$$\text{or, } \psi = kQ$$

where, $k=1$ for SI unit

$$\boxed{\psi = Q}$$

The electric flux is measured in Coulombs.



Consider an inner sphere of radius a and an outer sphere of radius b , with charges of $+q$ and $-q$ respectively. The paths of electric flux ψ extending from the inner sphere to the outer sphere are indicated by symmetrically distributed streamlines drawn radially from one sphere to the other.

At the surface of inner sphere, ψ coulombs of electric flux are produced by the charge $Q = (4\pi) \text{ coulombs}$ distributed uniformly over the surface of area $4\pi a^2 \text{ m}^2$. The density of flux at this surface is $\psi / 4\pi a^2$ or $Q / 4\pi a^2 \text{ C/m}^2$ and this quantity is called electric flux density; measured in coulombs per square meter (or lines per square meter for each line due to one coulomb). It is represented by \vec{D} .

The direction of \vec{D} at a point is the direction of the flux lines at that point, and the magnitude is given by the number of flux lines crossing a surface normal to the lines divided by the surface area.

i. Electric flux density of inner and outer spheres are

$$\vec{D}_{\text{inner}} = \frac{Q}{4\pi a^2} \hat{A}_r \quad \& \quad \vec{D}_{\text{outer}} = \frac{Q}{4\pi b^2} \hat{A}_r$$

and in bet' the two spheres with radius & the electric flux density will be

$$\vec{D}_{\text{bet'}} = \frac{Q}{4\pi r^2} \hat{A}_r$$

If we assume inner sphere (as very small) as point charge then the electric flux density at "inbet" spheres with charge Q at inner sphere will be same as:

$$\vec{D}_{\text{bet'}} = \frac{Q}{4\pi r^2} \hat{A}_r$$

so, we have from electric field intensity of point charge

$$\vec{E} = \frac{Q}{4\pi \epsilon_0 r^2} \hat{A}_r = \frac{\vec{D}}{\epsilon_0} \Rightarrow \boxed{\vec{D} = \epsilon_0 \vec{E}}$$

Now, for a volume charge with density ρ_v the intensity is

$$\vec{E} = \int_{\text{Vol.}} \frac{\rho_v dr}{4\pi\epsilon_0 r^2} \hat{ar}$$
 Also, $\Psi (\text{flux}) = \int \vec{D} \cdot d\vec{s}$

$$\therefore \vec{D} = \int_{\text{Vol.}} \frac{\rho_v dr}{4\pi\epsilon_0 r^2} \hat{ar}$$

Gauss's Law

It states that the total electric flux Ψ passing through any closed surface is equal to the total charge enclosed by that surface.

Thus, $\Psi = \Phi_{\text{enclosed}}$

$$\text{i.e. } \Psi = \oint d\Psi = \oint_S \vec{D} \cdot d\vec{s} = \text{Total charge enclosed}$$

Also, for volume charge

$$\Psi = \oint_S \vec{D} \cdot d\vec{s} = \int_{\text{Vol.}} \rho_v dv$$

We can assume the small incremental area of the surface enclosing the small charge ΔQ . If P be any point where \vec{D} makes an angle θ with $d\vec{s}$ (incremental surface). Then, the electric flux passing through the incremental surface $d\vec{s}$ is given by

$$\Delta \Psi = D_{\text{norm}} \cdot \Delta \vec{s} = |\vec{D}| \cos\theta \cdot \Delta s$$

$$\text{or, } \Delta \Psi = \Delta Q = \vec{D} \cdot \vec{ds}$$

Total flux passing through closed surface is $\Psi = \Phi_{\text{enclosed}} = \oint_S \vec{D} \cdot d\vec{s}$

For point charge, total charge = $\sum_{i=1}^n Q_i$ (n-charges)

For line charge, total charge = $\int_L \rho_s ds$ (length-L)

For surface charge, total charge = $\int_S \rho_s ds$.

For volume charge, total charge = $\int_{\text{Vol.}} \rho_v dv$

Gauss's Law Proof:

To prove Gauss's Law, let us consider the point charge, Q is placed at origin of the spherical co-ordinate system with sphere of radius a . Here, the enclosed surface will be the sphere of radius a .

From the derivation of electric field intensity of point charge at distance r we can write.

$$\vec{E} = \frac{Q}{4\pi\epsilon_0 r^2} \hat{r}$$

$$\text{and } \vec{D} = \epsilon_0 \vec{E}$$

$$\text{we have, } \vec{D} = \frac{Q}{4\pi r^2} \hat{r}$$

$$\text{At the Surface of the Sphere, } \vec{D} = \frac{Q}{4\pi a^2} \hat{r}$$

Also, The differential element of area on a spherical surface is

$$dS = a^2 \sin\theta d\phi d\theta \quad \text{or} \quad d\vec{S} = a^2 \sin\theta d\phi d\theta \hat{r}$$

At the Surface, $d\vec{S} = a^2 \sin\theta d\phi d\theta \hat{r}$

$$\text{Now, } \int_S \vec{D} \cdot d\vec{S} = \int_S \frac{Q}{4\pi a^2} \hat{r} \cdot a^2 \sin\theta d\phi d\theta$$

$$\psi = \int_S \frac{Q}{4\pi} \sin\theta \cdot d\phi$$

$$= \frac{Q}{4\pi} \int_{\phi=0}^{\phi=2\pi} \int_{\theta=0}^{\theta=\pi} \sin\theta \cdot d\theta \cdot d\phi$$

$$= \frac{Q}{4\pi} \int_{\phi=0}^{\phi=2\pi} (-\cos\theta) \Big|_{\theta=0}^{\theta=\pi} d\phi$$

$$= \frac{Q}{4\pi} \int_{\phi=0}^{2\pi} 2 \Big|_{\theta=0}^{\theta=\pi} d\phi$$

$$= \frac{Q}{4\pi} \cdot 2 \cdot 2\pi$$

$\therefore \psi = Q = \text{enclosed charge}$

i.e. ψ coulombs of electric flux are crossing the surface which is equal to the enclosed charge.

Application of Gauss's law

Gauss law is applicable only for symmetrical cases and symmetrical charge distributions. Here, Gauss's law can only be applied if we consider the closed surface called Gaussian surface. The surface must satisfy the following conditions:

- ① \vec{D} is everywhere either normal or tangential to the closed surface, so that $\vec{D} \cdot d\vec{s}$ becomes either $D ds$ or zero, respectively.
- ② If $\vec{D} \cdot d\vec{s}$ is not zero then \vec{D} must be constant over the surface.

Application of Gauss's law to find the Electric field intensity due to point charge

Let us consider a point charge q located at origin. To determine \vec{B} at a point P ; it is easy to see that choosing a spherical surface containing P will satisfy symmetry conditions. Thus, a spherical surface centered at origin is a Gaussian Surface.

Since, \vec{B} is everywhere normal to the Gaussian surface,

$$\text{i.e. } \vec{B} = D\hat{r} dr$$

applying Gauss's law

$$\psi = \oint_{\text{closed}} \vec{B} \cdot d\vec{s} = q = \int_0^{2\pi} \int_0^{\pi} \vec{B} \cdot d\vec{s} = D r \int_0^{2\pi} \int_0^{\pi} \sin\theta \cdot d\theta \cdot d\phi = D r 4\pi r^2$$

where $d\vec{s} = \int_0^{2\pi} \int_0^{\pi} r^2 \sin\theta \cdot d\theta \cdot d\phi = 4\pi r^2$ is the surface area of the Gaussian surface.

$$\therefore \vec{B} = \frac{q}{4\pi r^2} \hat{r}$$

Since, $\vec{B} = \epsilon_0 \vec{E}$

we can evaluate \vec{E} as:

$$\boxed{\vec{E} = \frac{\vec{B}}{\epsilon_0} = \frac{q}{4\pi \epsilon_0 r^2} \hat{r}}$$

Field Due to Line Charge

Let us consider the infinite line of unit linear charge density $\rho_L \text{ C/m}$ lies along z -axis. To determine \vec{D} at point P , we choose a cylindrical surface containing P to satisfy symmetry condition. \vec{D} is constant on and normal to the cylindrical Gaussian surface. i.e. $\vec{D} = D\hat{\vec{a}}_p$.

Applying Gauss's Law to an arbitrary length l of the line charge.

$$\rho_L l = Q = \oint \vec{D} \cdot d\vec{s}$$

$$= Dg \oint ds$$

$$= Dg 2\pi pl$$

$$\text{where, } \oint ds = \int_{0=0}^{l=0} \int_{\phi=0}^{2\pi} p d\phi d\theta = \int_{0=0}^{l=0} \int_{\phi=0}^{2\pi} p dl d\phi$$

$$\text{or, } \oint ds = p \int_{l=0}^{l=0} 2\pi dl$$

or, $\oint ds = p 2\pi l$ is a Gaussian surface

Since, z -component of \vec{D} is zero the $\oint \vec{D} \cdot d\vec{s}$ at top and bottom surface will be zero. i.e. tangential to those surfaces.

$$\therefore \vec{D} = \frac{Q}{2\pi\rho_L} \hat{a}_p = \frac{\rho_L l}{2\pi\rho_L} \hat{a}_p = \frac{\rho_L}{2\pi\rho_L} \hat{a}_p$$

$$\vec{B} = \vec{E}$$

Again, we have

$$\vec{E} = \frac{\rho_L \hat{a}_p}{2\pi\rho_L} \hat{a}_p$$

Field due to infinite sheet of charge

Let us consider the infinite sheet of uniform charge $\sigma_s \text{ C/m}^2$ lying on the $z=0$ plane. To determine \vec{D} at point P, we choose a rectangular box that is cut symmetrically by the sheet of charge and has two of its faces parallel to the sheet. As \vec{D} is normal to the sheet, $\vec{D} = D_z \hat{q}_z$.

Applying Gauss's law

$$\oint_S \int dS = Q = \int \vec{D} \cdot d\vec{s}$$

$$= D_z \left[\int_{\text{top}} dS + \int_{\text{bottom}} dS \right]$$

Here, $\vec{D} \cdot d\vec{s}$ evaluated on the sides of box is zero because \vec{D} has no components along \hat{a}_x & \hat{a}_y . If the top and bottom area of the box each has area A.

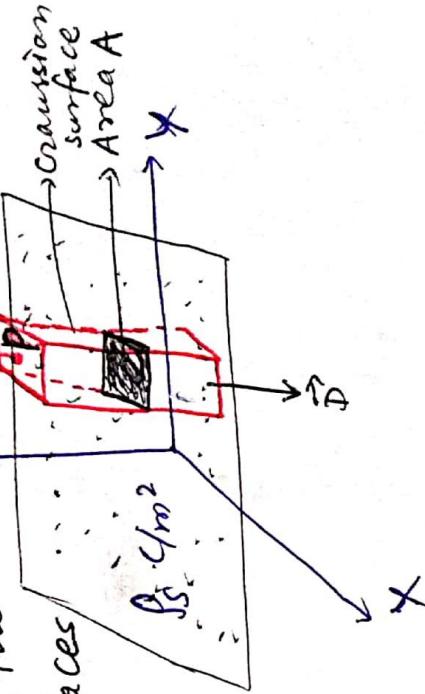
$$\oint_S dS = D_z [A + A]$$

$$\text{or, } D_z = \frac{\rho_s}{2}$$

$$\therefore \vec{D} = \frac{\rho_s}{2} \hat{q}_z = \frac{\rho_s}{2} \hat{a}_z$$

Again, $\vec{D} = \epsilon_0 \vec{E}$

$$\text{So, } \vec{E} = \frac{\rho_s}{2 \epsilon_0} \hat{a}_z$$



Field in a Co-axial cable

Let us consider a Co-axial cable of infinite length having inner conductor of radius a and outer conductor of radius b .

A uniformly distributed surface charge density ρ_s is placed on the outer surface of inner conductor.

To determine \vec{D} at point P in

$\rho < a$, $\rho > b$ and $a < \rho < b$, we choose a cylindrical surfaces as shown in figure for symmetry conditions to satisfy. Since, the circular surface of the cylinder has \vec{D} tangential to surface if $\vec{D} \cdot \vec{ds} = 0$; so only \vec{D} along radius will be present; i.e. $\vec{D} = D\hat{r}$.

Now, for $\rho < a$

Applying Gauss's law : $\oint \vec{D} \cdot d\vec{s} = \text{charge enclosed} = 0$ [no charge enclosed]

$$\oint \vec{D} \cdot d\vec{s} = \text{charge enclosed} = 0$$

$$\text{Hence, } \vec{D} = 0 \Rightarrow \vec{E} = 0.$$

for $a < \rho < b$

Gauss's law

Applying Gauss's law $\oint \vec{D} \cdot d\vec{s} = D_s \oint ds_0 = D_s 2\pi r L$

$$\rho_s \int ds_0 = Q = D_s \oint ds_0 = D_s 2\pi r L$$

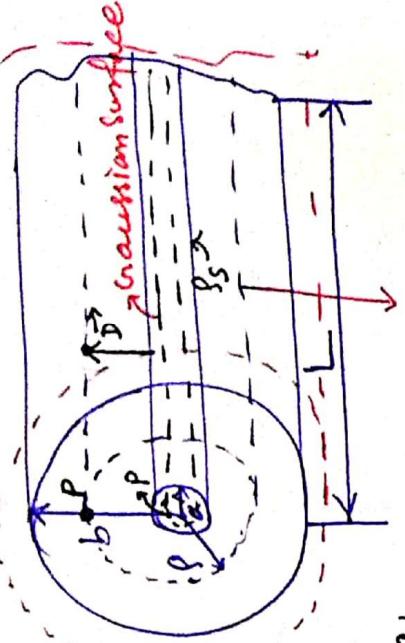
where, $\int ds_0 = \text{surface area of Gaussian surface} = 2\pi r L$

$\int ds_0 = \text{surface area of inner conductor} = 2\pi a L$

$L = \text{arbitrary length of the Co-axial cable.}$

$$\therefore \rho_s \cdot 2\pi a L = D_s 2\pi a L$$

$$\text{or, } D_s = \frac{\rho_s a}{L} \quad \text{or, } \vec{D} = \frac{\rho_s a}{L} \hat{r}$$



(6) Since, $\vec{B} = \epsilon_0 \vec{E}$
we have,

$$\vec{E} = \frac{\rho_s a}{\epsilon_0 p} \hat{a}_p$$

for $p > b$

Since, due to induction the equal but opposite charge will be seen in outer conductor.

Applying Gauss's Law.

$$\text{Enclosed} = \rho_{sI} \int ds_I + \rho_{sO} \int ds_O = 0 = \oint \vec{B} \cdot d\vec{s}$$

Thus, the field outside the coaxial cable is zero.

$$\text{but } \rho_{sI} \cdot (2\pi bl) = -\rho_{sO} (2\pi bl)$$

$$\text{or, } \rho_{sO} = -\frac{q}{b} \rho_{sI}$$

And, since total charge enclosed = 0, $\vec{B} = 0 \Rightarrow \vec{E} = 0$.

Ques: A uniform line charge of 15nC/m lies along the z -axis and a uniform sheet of charge ρ_s of 4nC/m^2 is located at the plane $z=1$. Find the electric flux density \vec{D} in spherical co-ordinate system at point $(2, 0, 0)$.

Sol.:

Here, line charge of $\rho_L = 15 \text{nC/m}$ lies along the z -axis.

Sheet charge of $\rho_s = 4 \text{nC/m}^2$ is located at $z = 1$ plane.

Now, we have to find the electric

flux density at point $P(2, 0, 0)$:

Firstly, we calculate the electric field intensity due to both charges at:

\vec{E} due to line charge $\rho_L = 15 \text{nC/m}$ is

$$\vec{E}_L = \frac{\rho_L}{2\pi\epsilon_0 r} \cdot \hat{a}_r$$

where, $\hat{r} = (2-0) \hat{a}_x + (0-0) \hat{a}_y + (0-0) \hat{a}_z = \hat{a}_x$
 $\rho = (\rho_L / 2) = 2$ & $\hat{a}_r = \hat{a}_x$

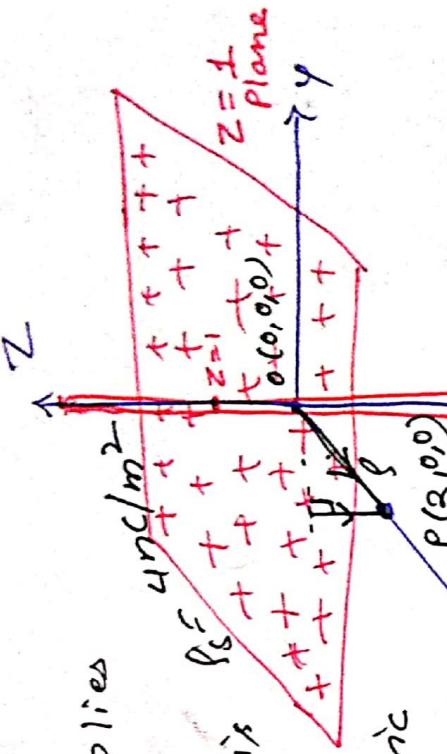
$$\therefore \vec{E}_L = \frac{15 \times 10^{-9}}{2\pi \times 10^{-9} \times 2} \hat{a}_x = 15 \times 10^9 \hat{a}_x \text{ N/C}$$

Again, \vec{E} due to sheet charge $\rho_s = 4 \text{nC/m}^2$ is

$$\vec{E}_s = \frac{\rho_s}{2\epsilon_0} \hat{a}_z$$

where, $\hat{a}_z = -\hat{a}_z$

$$\therefore \vec{E}_s = -\frac{4 \times 10^{-9}}{2 \times 10^{-9}} = -226.19 \hat{a}_z \text{ V/m}$$



$$\vec{E}_{\text{total at point } P(2,0,0)} = \vec{E}_x + \vec{E}_z = 135 \hat{a}_x - 226 \cdot 19 \hat{a}_z \text{ V/m}$$

Now, we have, electric flux density is

$$\vec{D} = \epsilon_0 \vec{E} = \frac{10^{-9}}{36\pi} \times (135 \hat{a}_x - 226 \cdot 19 \hat{a}_z)$$

$$= (1195 \cdot 29 \hat{a}_x - 2000 \hat{a}_z) \times 10^{-12} \text{ C/m}^2$$

$$= (1195 \cdot 29 \hat{a}_x - 2000 \hat{a}_z) \text{ PC/m}^2$$

since, this value is in Cartesian Co-ordinate system
we need to change it to spherical co-ordinate
System at point $P(2,0,0)$,
so, we need to have values of $r, \phi, \theta, D_r, D_\theta, D_\phi$

$$\text{as: } r = \sqrt{x^2 + y^2 + z^2} = \sqrt{2^2 + 0^2 + 0^2} = 2$$

$$\phi = \tan^{-1} \left(\frac{y}{x} \right) = \tan^{-1}(0) = 0^\circ$$

$$\theta = \tan^{-1} \left(\frac{\sqrt{x^2 + y^2}}{z} \right) = \tan^{-1} \left(\frac{2}{0} \right) = \tan^{-1}(\infty) = \frac{\pi}{2}.$$

$$\begin{aligned} D_r &= \vec{D} \cdot \hat{a}_r = 1195 \cdot 29 (\hat{a}_x \cdot \hat{a}_r) - 2000 (\hat{a}_z \cdot \hat{a}_r) \\ &= 1195 \cdot 29 \sin\theta \cos\phi - 2000 \cos\theta \\ &= 1195 \cdot 29 \cdot \sin\left(\frac{\pi}{2}\right) \cdot \cos 0 - 2000 \cos\frac{\pi}{2} \\ &= 1195 \cdot 29 \text{ PC/m}^2 \\ D_\theta &= \vec{D} \cdot \hat{a}_\theta = 1195 \cdot 29 (\hat{a}_x \cdot \hat{a}_\theta) - 2000 (\hat{a}_z \cdot \hat{a}_\theta) \\ &= 1195 \cdot 29 \cdot \cos\theta \cdot \cos\phi - 2000 (-\sin\theta) \\ &= 1195 \cdot 29 \cdot \frac{\sqrt{3}}{2} \cdot \cos 0 + 2000 \cdot \sin\frac{\pi}{2} \\ &= 2080 \text{ PC/m}^2 \\ D_\phi &= \vec{D} \cdot \hat{a}_\phi = 1195 \cdot 29 (\hat{a}_x \cdot \hat{a}_\phi) - 2000 (\hat{a}_z \cdot \hat{a}_\phi) \\ &= 1195 \cdot 29 \cdot \frac{1}{2} \cdot \sin\theta \cdot \sin\phi - 2000 \times 0 \\ &= 1195 \cdot 29 \times 0 \\ &= 0 \text{ PC/m}^2 \end{aligned}$$

$$\vec{B}_{\text{spherical}} = D_r \hat{a}_r + D_\theta \hat{a}_\theta + D_\phi \hat{a}_\phi$$

$$= 1195.29 \hat{a}_r + 2000 \hat{a}_\theta + 0 \cdot 48 \hat{a}_\phi$$

$$= 1195.29 \hat{a}_r + 2000 \hat{a}_\theta \text{ pC/m}^2$$

- Given, $\vec{D} = \frac{Q}{3} r \hat{a}_r \text{ nC/m}^2$ in free space \textcircled{a} Find $E = |\vec{E}|$ at $r = 0.2 \text{ m}$.
- \textcircled{b} Find the total charge within the sphere $r = 0.2 \text{ m}$.
- \textcircled{c} Find the total electric flux leaving the sphere $r = 0.3 \text{ m}$.

So, Here,

$$\vec{D} = \frac{Q}{3} r \hat{a}_r \text{ in spherical co-ordinate system.}$$

- \textcircled{a} To evaluate $E = |\vec{E}|$ we have

$$\vec{D} = \epsilon_0 \vec{E}$$

$$\text{or, } \vec{E} = \frac{\vec{D}}{\epsilon_0} = \frac{Q}{3\epsilon_0} r \hat{a}_r \text{ V/m}$$

Putting $r = 0.2 \text{ m}$

$$\vec{E} = \frac{0.2}{3\epsilon_0} Q \hat{a}_r \text{ V/m.}$$

$$\therefore E = |\vec{E}| = \frac{0.2}{3\epsilon_0} = \frac{0.2 \times 10^{-9}}{36\pi} = 7.053 \cdot 10^{-9} \text{ V/m}$$

Again, \textcircled{b} Let Q be the total charge within the sphere, and assuming Gaussian surface at the surface of the sphere $r = 0.2 \text{ m}$ then \vec{D} will be perpendicular to the surface of the sphere. So, the differential area of the sphere, $d\vec{A} = r^2 \sin\theta d\phi \hat{a}_\phi$

Now, from Gauss's law

$$Q = \oint_S \vec{D} \cdot d\vec{A} = \int_S \frac{2}{3} Q \hat{a}_r \cdot r^2 \sin\theta d\phi \hat{a}_\phi$$

$$= \int_S \frac{2}{3} r^3 \sin\theta d\phi \cdot d\theta$$

since, $r = 0.2 \text{ m}$.

$$Q = \int_S \frac{(0.2)^3}{3} \sin\theta d\phi \cdot d\theta$$

$$\Phi = \int_0^{\pi} \int_0^{2\pi} \frac{(0.2)^3}{3} \cdot \sin\theta \cdot [2\pi - 0] d\theta$$

$$= \frac{(0.2)^3}{3} \times 2\pi \times [-\cos\theta]_0^{\pi}$$

$$= 33.51 \text{ pC}$$

Q Again, since from Gauss's law, total electric flux leaving the surface is equal to the charge enclosed by the surface. So, At $r = 0.8 \text{ m}$:

$$\begin{aligned}\Psi = \Phi &= \oint_S \vec{D} \cdot d\vec{S} = \oint_S \frac{(0.3)^3}{3} \sin\theta \cdot d\theta \cdot d\phi \\ &= \frac{(0.3)^3}{3} \times 2\pi \times [-\cos\theta]_0^{\pi} \\ &= 113.097 \text{ pC} / \text{l}\end{aligned}$$

Qn: A point charge of $6 \mu\text{C}$ is located at the origin, a uniform line charge density of 180nC/m lies along the x -axis and a uniform sheet of charge equal to 25nC/m^2 lies in the $z=0$ plane. Find \vec{D} at $B(1, 2, 4)$. [20170 Ashad]

Sol: Here, a point charge of $6 \mu\text{C}$ is located at origin, a uniform line charge of $\rho_L = 180 \text{nC/m}$ lies along the x -axis and a uniform sheet of charge density, $\sigma_S = 25 \text{nC/m}^2$ lies in the $z=0$ plane as shown in figure.

Now, the electric flux density due to a point charge at origin, $q(0,0,0)$ is

$$\vec{D}_P = \frac{\rho}{4\pi R^2} \hat{a}_R$$

$$\text{where, } \vec{R} = (1-0) \hat{a}_x + (2-0) \hat{a}_y + (4-0) \hat{a}_z \\ = \hat{a}_x + 2\hat{a}_y + 4\hat{a}_z$$

$$R = |\vec{R}| = \sqrt{1^2 + 2^2 + 4^2} = \sqrt{21}$$

$$\& \hat{a}_R = \hat{a}_x + 2\hat{a}_y + 4\hat{a}_z$$

$$\therefore \vec{D}_P = \frac{6 \times 10^{-6}}{4\pi \times 21} \cdot \left(\frac{\hat{a}_x + 2\hat{a}_y + 4\hat{a}_z}{\sqrt{21}} \right)$$

$$= 4.96 \times 10^{-9} (\hat{a}_x + 2\hat{a}_y + 4\hat{a}_z) \\ = (4.96 \hat{a}_x + 9.92 \hat{a}_y + 19.84 \hat{a}_z) \text{ nC/m}^2$$

Again, Electric flux density due to line charge is

$$\vec{D}_L = \frac{\rho_L}{2\pi s} \hat{a}_g$$

$$\text{where, } \vec{g} = (1-1) \hat{a}_x + (2-0) \hat{a}_y + (4-0) \hat{a}_z \\ = 2\hat{a}_y + 4\hat{a}_z$$

$$\rho = |\vec{g}| = \sqrt{2^2 + 4^2} = \sqrt{20}$$

$$\& \hat{g} = \frac{2\hat{a}_y + 4\hat{a}_z}{\sqrt{20}}$$

$$\therefore \vec{D}_L = \frac{180 \times 10^{-9}}{2\pi \times \sqrt{20}} \cdot \frac{(2\hat{a}_y + 4\hat{a}_z)}{\sqrt{20}} \\ = 1.432 \times 10^{-9} (2\hat{a}_y + 4\hat{a}_z) \\ = (2.86 \hat{a}_y + 5.73 \hat{a}_z) \text{ nC/m}^2$$

Again, Electric flux density due to sheet charge is

$$\vec{D}_S = \frac{\rho_s}{2} \hat{a}_N \text{ where, } \hat{a}_N = \hat{a}_z$$

$$\therefore \vec{D}_S = \frac{2.5 \times 10^{-9}}{2} \cdot \hat{q}_2$$

$$= 12.5 \hat{q}_2 \text{ nC/m}^2$$

Total flux density at B(1, 2, 4); $\vec{D} = \vec{D}_P + \vec{D}_L + \vec{B}_S$

$$= 4.96 \hat{a}_x + 9.92 \hat{a}_y + 19.84 \hat{a}_z + 2.86 \hat{a}_y + 5.73 \hat{a}_z + 12.5 \hat{a}_z$$

$$= (4.96 \hat{a}_x + 12.78 \hat{a}_y + 18.23 \hat{a}_z) \text{ nC/m}^2$$

Qn: Along z-axis there is a uniform line charge of density $\rho_L = 4\pi \text{ C/m}$ and in the x=1 plane there is a surface charge with $\rho_S = 20 \text{ C/m}^2$. Find the electric flux density at (0, 5, 0, 0). [2010 Chaitra]

Sol:

$$\vec{D}_L = \frac{\rho_L}{2\pi\rho} \hat{a}_P \Rightarrow \vec{D}_S = \frac{\rho_S}{2} \hat{a}_N$$

$$\therefore \vec{D} = \frac{4\pi}{2\pi \times 0.5} \hat{a}_x + \frac{10}{2} (\hat{a}_N)$$

$$= 4 \hat{a}_x - 10 \hat{a}_N$$

$$= -6 \hat{a}_x \text{ C/m}^2$$

$$\therefore \rho_L = 4\pi \text{ C/m}$$

Qn: Find \vec{D} at the point (-3, 4, 2) if the following charge distributions are present in free space: point charge, 12 nC at P(2, 0, 6); uniform line charge density, 3 nC/m at x = -3; y = 3; uniform surface charge density, 0.2 nC/m² at x = -3, y = 3.

Sol:

$$\vec{D} = \vec{D}_P + \vec{D}_L + \vec{B}_S$$

$$= \frac{Q}{4\pi R^2} \hat{a}_R + \frac{\rho_L}{2\pi\rho} \hat{a}_P + \frac{\rho_S}{2} \hat{a}_N$$

Qn: Let a uniform line charge density, 3nC/m at $y=3$; uniform surface charge density, 0.2nC/m^2 at $x=2$.

Find \vec{E} at origin. [2017-18 Ashwin]

Qn: A uniform line charge density of 2nC/m is located at $y=3$ and $z=5$. Find \vec{E} at $P(5, 6, 1)$. [2017-18 Chaitra]

Qn: Find Electric flux density at point $P(5, 4, 3)$ due to a uniform line charge of 2nC/m at $x=5$, $y=3$, point charge 12nC at $Q(2, 0, 6)$ and uniform surface charge density of 0.2nC/m^2 at $x=2$. [2017-18 Chaitra]

Qn: Along the z -axis there is a uniform line of charge with $g_L = 4\pi \text{ cm}^{-1}$ and in the $x=1$ plane there is a surface charge with $g_S = 20 \text{ cm}^{-2}$. Find the Electric flux Density at $(0.5, 0, 0)$. [2020 Chaitra]

Qn: Find \vec{B} at the point $(-3, 4, 2)$ if the following charge distributions are present in free space : point charge, 12nC at $P(2, 0, 6)$; uniform line charge density, 8nC/m at $x=-2$, $y=3$; uniform surface charge density, 0.2nC/m^2 at $x=2$.

[2021 Shrawan]

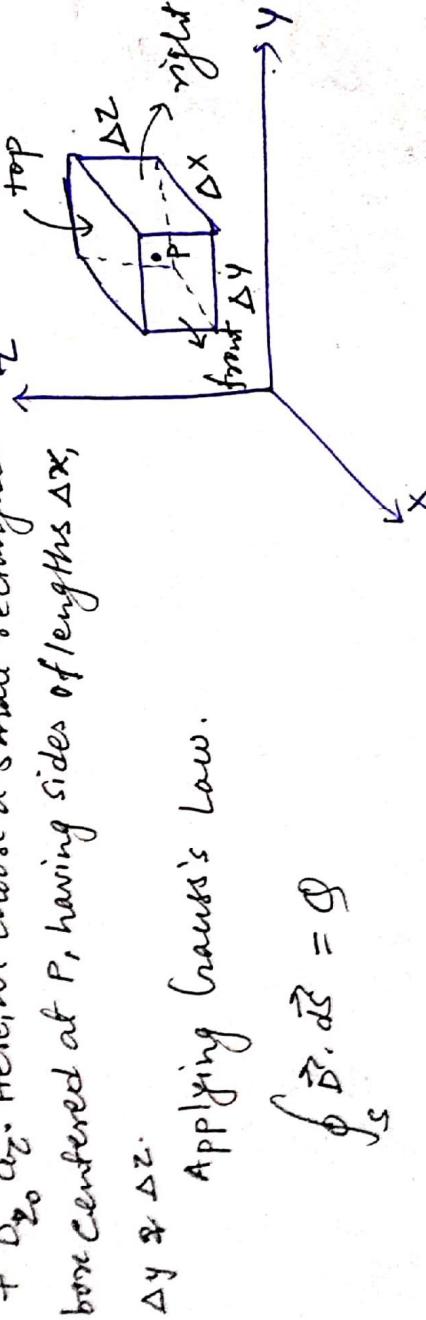
Application of Gauss's Law : Differential Volume Element

Gauss's Law is only applicable for the symmetrical charge distributions and the Gaussian surface must be simple where the flux density has normal component either constant or zero everywhere on the surface. Without such surface, the integral cannot be evaluated. So, for unsymmetrical cases; there is only way to apply Gauss's law by considering or choosing a very small closed surface that \vec{B} is almost constant over the surface. The result will become more nearly correct as the volume enclosed by the Gaussian surface decreases.

Let us consider any point P in a rectangular co-ordinate system with co-ordinate $P(x_0, y_0, z_0)$. The value of \vec{B} at the point P may be expressed in rectangular components, $D_x = D_{x0} \hat{x} + D_{y0} \hat{y} + D_{z0} \hat{z}$. Here, we choose a small rectangular box centered at P, having sides of lengths Δx , Δy & Δz .

Applying Gauss's Law.

$$\oint_S \vec{B} \cdot d\vec{s} = 0$$



In order to evaluate the integral over the closed surface, the integral must be broken into six for each face.

$$\oint_S \vec{B} \cdot d\vec{s} = \int_{\text{front}} + \int_{\text{back}} + \int_{\text{left}} + \int_{\text{right}} + \int_{\text{bottom}} + \int_{\text{top}}$$

Now,

$$\begin{aligned} \int_{\text{front}} &= \vec{B}_{\text{front}} \cdot \vec{\Delta s}_{\text{front}} \\ &= \vec{B}_{\text{front}} \cdot \hat{y} \Delta z \hat{x} \end{aligned}$$

Since, the front face is at a distance of $\frac{\Delta x}{2}$ from P, and approximating Δx value at the front face. hence

$$D_{x, \text{front}} = D_{x0} + \frac{\Delta x}{2} \times \text{rate of change of } D_x \text{ with } x$$

(74)

$$\text{or, } D_{x, \text{front}} = D_{x_0} + \frac{\Delta x}{2} \frac{\partial D_x}{\partial x}$$

where D_{x_0} is the value of D_x at P and where a partial derivative must be used to express the rate of change of D_x with x , as D_x in general vary with y & z also. This expression could have been obtained more formally by using the constant term and the terms involving the first derivative in the Taylor's series expansion for D_x in the neighborhood of P.

$$\therefore f_{\text{front}} = \left(D_{x_0} + \frac{\Delta x}{2} \frac{\partial D_x}{\partial x} \right) \Delta y \cdot \Delta z$$

Similarly for back surface,

$$\begin{aligned} f_{\text{back}} &= \vec{D}_{\text{back}} \cdot \vec{\Delta r}_{\text{back}} \\ &= \vec{D}_{\text{back}} \cdot (-\Delta y \cdot \Delta z \hat{x}) \\ &= D_{x, \text{back}} \Delta y \cdot \Delta z \end{aligned}$$

$$\text{and } D_{x, \text{back}} = D_{x_0} - \frac{\Delta x}{2} \frac{\partial D_x}{\partial x}$$

$$f_{\text{back}} = \left(-D_{x_0} + \frac{\Delta x}{2} \frac{\partial D_x}{\partial x} \right) \Delta y \Delta z$$

Combining we get

$$f_{\text{front}} + f_{\text{back}} = \frac{\partial D_x}{\partial x} \Delta x \Delta y \Delta z$$

Doing same for other surfaces, we get

$$f_{\text{right}} + f_{\text{left}} = \frac{\partial D_y}{\partial y} \Delta x \Delta y \Delta z$$

$$2 \left(f_{\text{top}} + f_{\text{bottom}} \right) = \frac{\partial D_z}{\partial z} \Delta x \Delta y \Delta z$$

Taylor's Series expansion.

$$f(x, y, z) = f(x_0, y_0, z_0) + \frac{\partial f}{\partial x}(x-x_0) + \frac{\partial f}{\partial y}(y-y_0) + \frac{\partial f}{\partial z}(z-z_0) + \frac{1}{2!} \left[\frac{\partial^2 f}{\partial x^2}(x-x_0)^2 + \frac{\partial^2 f}{\partial y^2}(y-y_0)^2 + \frac{\partial^2 f}{\partial z^2}(z-z_0)^2 \right] + \frac{1}{3!} \left[\frac{\partial^3 f}{\partial x^3}(x-x_0)^3 + \frac{\partial^3 f}{\partial y^3}(y-y_0)^3 + \frac{\partial^3 f}{\partial z^3}(z-z_0)^3 \right] + \dots$$

$$\textcircled{*} f(x) = f(a) + \frac{f'(a)}{1!}(x-a) + \frac{f''(a)}{2!}(x-a)^2 + \frac{f'''(a)}{3!}(x-a)^3 + \dots$$
$$= \sum_{n=0}^{\infty} \frac{f^{(n)}(a)}{n!} (x-a)^n$$

(35). Therefore, we have

$$\oint_S \vec{B} \cdot d\vec{s} = \int_{\text{c}} \frac{\partial B_z}{\partial x} dx + \frac{\partial B_x}{\partial z} dz + \frac{\partial B_y}{\partial z} dz - \frac{\partial B_z}{\partial x} dx - \frac{\partial B_x}{\partial z} dz + \frac{\partial B_y}{\partial x} dx$$

$$\text{or, } \oint_S \vec{B} \cdot d\vec{s} = \int_{\text{c}} \left(\frac{\partial B_x}{\partial z} + \frac{\partial B_y}{\partial x} + \frac{\partial B_z}{\partial x} \right) dV$$

Hence, charge enclosed in volume $\Delta V = \left(\frac{\partial B_x}{\partial z} + \frac{\partial B_y}{\partial x} + \frac{\partial B_z}{\partial x} \right) \Delta V$

Divergence and Maxwell's first Equation.

The divergence of \vec{B} at a given point P is the outward flux per unit volume as the volume shrinks about P.

$$\text{i.e. divergence of } \vec{B} = \nabla \cdot \vec{B} = \lim_{\Delta V \rightarrow 0} \frac{\oint_S \vec{B} \cdot d\vec{s}}{\Delta V}$$

From above expression, if we allow the ΔV to shrink to zero, then

$$\left(\frac{\partial B_x}{\partial z} + \frac{\partial B_y}{\partial x} + \frac{\partial B_z}{\partial x} \right) = \lim_{\Delta V \rightarrow 0} \frac{\oint_S \vec{B} \cdot d\vec{s}}{\Delta V} = \lim_{\Delta V \rightarrow 0} \frac{\vec{P} \cdot d\vec{S}}{\Delta V} = \vec{P} \cdot \vec{dS}$$

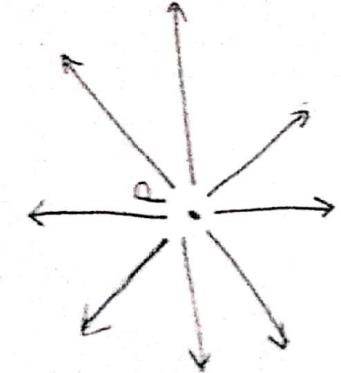
Also, if we assume any general vector, \vec{A} then

$$\frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z} = \lim_{\Delta V \rightarrow 0} \frac{\vec{A} \cdot d\vec{S}}{\Delta V}$$

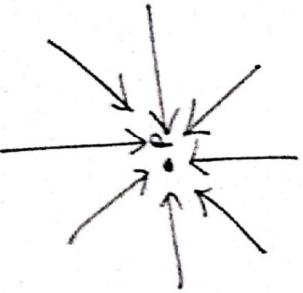
$$\therefore \text{divergence of } \vec{A} = \nabla \cdot \vec{A} = \lim_{\Delta V \rightarrow 0} \frac{\vec{A} \cdot d\vec{S}}{\Delta V}$$

where, $\nabla \cdot \vec{A} = \frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z}$

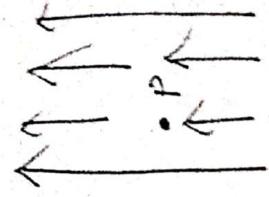
The divergence of the vector flux density \vec{A} is the outflow of flux from a small closed surface per unit volume as the volume shrinks to zero.



positive divergence
at Point P



negative divergence
at point P



zero divergence

Physically, we may regard the divergence of the vector field \vec{A} at a given point as a measure of how much the field diverges or ~~converges~~ emanates from that point. In above figures, the ~~vector diverges (or spreads out)~~ in first figure, so it's +ve. The vector converges at P in second figure so it's -ve. But in 3rd figure, the vector neither diverges nor converges, so it has zero divergence.

Divergence Theorem

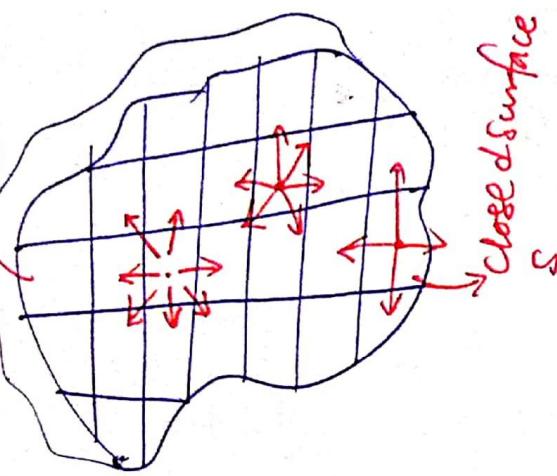
It states that the total outward flux of a vector field \vec{A} through the closed surface S is the same as the volume integral of the divergence of \vec{A} .

$$\text{i.e. } \int_S \vec{A} \cdot d\vec{S} = \int_{\text{vol.}} \nabla \cdot \vec{A} dV$$

The integral of the normal component of any vector field over a closed surface is equal to the integral of the divergence of this vector field through the volume enclosed by the closed surface. To prove the divergence theorem, let us subdivide volume V into a large number of small cells. If the km cell has volume ΔV_k and is bounded by surface S_k

$$\int_S \vec{A} \cdot d\vec{S} = \sum_k \int_{S_k} \vec{A} \cdot d\vec{S} = \sum_k \frac{\int_{S_k} \vec{A} \cdot d\vec{S}}{\Delta V_k} \cdot \Delta V_k$$

(3) since the outward flux to one cell is inward to some neighbouring cells, there is cancellation on every interior surface, so the sum of the surface integrals over S_k 's the same as the surface integral over the surface S . Taking limit of right side and incorporating volume, V



$$\text{div. } \vec{A} = \nabla \cdot \vec{A} = \lim_{\Delta V \rightarrow 0} \frac{\oint_S \vec{A} \cdot d\vec{s}}{\Delta V}$$

$$\text{and } \oint_S \vec{A} \cdot d\vec{s} = \sum_k \frac{\oint_S \vec{A} \cdot d\vec{s}}{\Delta V_k} \cdot \Delta V_k$$

gives,

$$\boxed{\oint_S \vec{A} \cdot d\vec{s} = \int_V \nabla \cdot \vec{A} dV}$$

which is a divergence theorem. The theorem applies to any volume V bounded by the closed surface S .

Maxwell's first Equation

From divergence theorem.

$$\text{div. } \vec{A} = \nabla \cdot \vec{A} = \lim_{\Delta V \rightarrow 0} \frac{\oint_S \vec{A} \cdot d\vec{s}}{\Delta V}$$

$$\text{or, } \boxed{\nabla \cdot \vec{A} = \rho_V}$$

where, $\rho_V = \lim_{\Delta V \rightarrow 0} \frac{\oint_S \vec{A} \cdot d\vec{s}}{\Delta V}$, volume charge density.

This is the Maxwell's first equation or point form of Gauss's Law.

(78) Qn: Evaluate both sides of the divergence theorem for the field $\vec{B} = xy\hat{a}_x + x^2y\hat{a}_y \text{ C/m}^2$ and the rectangular parallel piped formed by the planes $x=0 \text{ & } 1$, $y=0 \text{ & } 2$ and $z=0 \text{ & } 3$.

Soln:

Given,

$\vec{B} = 2xy\hat{a}_x + x^2y\hat{a}_y \text{ C/m}^2$ and a rectangular parallelopiped formed by the planes $x=0 \text{ & } 1$, $y=0 \text{ & } 2$ and $z=0 \text{ & } 3$.

Now, from divergence theorem.

$$\oint_S \vec{B} \cdot d\vec{s} = \int_{\text{vol.}} \nabla \cdot \vec{B} \, dv$$

For left part

$$\begin{aligned} \oint_S \vec{B} \cdot d\vec{s} &= \int_0^2 \int_0^2 (\vec{B})_{x=0} \cdot (-dy \, dz \hat{a}_x) + \int_0^3 \int_0^2 (\vec{B})_{x=1} \cdot (dy \, dz \hat{a}_x) \\ &\quad + \int_0^3 \int_0^1 (\vec{B})_{y=0} \cdot (-dx \, dz \hat{a}_y) + \int_0^3 \int_0^1 (\vec{B})_{y=2} \cdot (dx \, dz \hat{a}_y) \\ &\quad + \int_0^2 \int_0^1 (\vec{B})_{z=0} \cdot (-dx \, dy \hat{a}_z) + \int_0^2 \int_0^1 (\vec{B})_{z=3} \cdot (dx \, dy \hat{a}_z) \end{aligned}$$

since, the z -component of \vec{B} is zero; the \vec{B} seems to be parallel to $z=0 \text{ & } z=3$ planes.

$$\begin{aligned} \therefore \oint_S \vec{B} \cdot d\vec{s} &= - \int_0^3 \int_0^2 (\nabla_x)_{x=0} dy \, dz + \int_0^3 \int_0^2 (\nabla_x)_{x=1} dy \, dz \\ &\quad - \int_0^3 \int_0^1 (\nabla_y)_{y=0} dx \, dz + \int_0^3 \int_0^1 (\nabla_y)_{y=2} dx \, dz \end{aligned}$$

For, $x=0$

$$\vec{B} = 0 \text{ so, } \oint_S \vec{B} \cdot d\vec{s} = \int_0^3 \int_0^2 (\nabla_x)_{x=1} dy \, dz + \int_0^3 \int_0^1 (\nabla_y)_{y=2} dx \, dz$$

$$(7) = 0 + 0 + \int_{y=0}^2 \int_{z=0}^3 2xy \, dy \, dz + 0 + 0 - \int_{z=0}^3 \int_{x=0}^1 x^2 \, dx \, dz$$

at $y=0$

$$+ \int_{z=0}^3 \int_{x=0}^1 x^2 \, dx \, dz$$

at $y=2$

$$= \int_{y=0}^2 \int_{z=0}^3 2xy \, dy \, dz$$

at $x=1$

$$= \int_{y=0}^2 \int_{z=0}^3 2y \, dy \, dz$$

at $x=1$

$$= \int_{y=0}^2 6y \, dy$$

$$= \frac{6y^2}{2} \Big|_0^2$$

$$= 3 [2^2 - 0^2]$$

$$= 12 \, C$$

Again taking right part only.

$$\int_{\text{vol.}} (\nabla \cdot \vec{B}) \, dv = \int_{\text{vol.}} \left(\frac{\partial D_x}{\partial x} + \frac{\partial D_y}{\partial y} + \frac{\partial D_z}{\partial z} \right) \, dv$$

$$\text{Here, } D_x = 2xy, \quad D_y = x^2 \quad \& \quad D_z = 0$$

$$\text{So, } \int_{\text{vol.}} (\nabla \cdot \vec{B}) \, dv = \int_{\text{vol.}} \left[\frac{\partial (2xy)}{\partial x} + \frac{\partial (x^2)}{\partial y} \right] \, dv$$

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$$\int_{\text{vol.}} (\nabla \cdot \vec{B}) \, dv = \int_{\text{vol.}} [2y + 0 + 0] \, dy \, dz$$

$$\begin{aligned}
 &= \int_0^1 \int_0^2 \int_0^3 2y \, dy \, dz \\
 &\quad y=0 \quad z=0 \\
 &= \int_0^1 \int_0^2 2yx_3 \, dy \, dz \\
 &\quad x=0 \quad y=0 \\
 &= \int_0^1 \left[-6 \frac{y^2}{2} \right]_0^2 \, dz \\
 &\quad \text{or } x=0 \\
 &= 12 \left[1 - 0 \right] \\
 &= 12 \, c
 \end{aligned}$$

$$\therefore \int_S (\vec{D} \cdot d\vec{s}) = \int_{\text{vol.}} (\nabla \cdot \vec{D}) \cdot dv = 12c / 1$$

Qn: Verify the divergence theorem [Calculate both sides of the divergence theorem] for the function $\vec{A}^2 = x^2 \hat{i} + \sin\theta \cos\phi \hat{j} + \sin\theta \cos\phi \hat{k}$, over the surface of quarter of a hemisphere defined by: $0 < r < 3$, $0 < \theta < \frac{\pi}{2}$, $0 < \phi < \frac{\pi}{2}$. [2009 chart 9]

Soln. Here, $\vec{A}^2 = r^2 \hat{i} + \sin\theta \cos\phi \hat{j} + \sin\theta \cos\phi \hat{k}$

& $0 < r < 3$, $0 < \theta < \frac{\pi}{2}$, $0 < \phi < \frac{\pi}{2}$

from divergence theorem

$$\int_S (\vec{A} \cdot d\vec{s}) = \int_{\text{vol.}} (\nabla \cdot \vec{A}) \, dv$$

Taking only left part

$$\int_S (\vec{A} \cdot d\vec{s}) = - \oint_{\text{top}} \vec{A} \cdot d\vec{s} + \oint_{\text{bottom}} \vec{A} \cdot d\vec{s}$$

$$\begin{aligned}
 &= - \oint_{\text{top}} \vec{A} \cdot d\vec{s} + \oint_S \vec{A} \cdot d\vec{s} + \oint_{\text{bottom}} \vec{A} \cdot d\vec{s} \\
 &\quad \text{top } (\theta = 0) \quad \text{side } (\theta = \frac{\pi}{2}) \quad \text{bottom } (\theta = \pi/2)
 \end{aligned}$$

$$\begin{aligned}
 & = -\int_S r^2 \sin^2 \theta (r^2 \cos \phi) \cdot (\sin \theta \hat{a}_\theta) + \int_S (A_\theta \hat{a}_\theta) \cdot (\sin \theta \hat{a}_\theta) + f(A_\theta \hat{a}_\theta) \\
 & \quad \theta = \frac{\pi}{2} \quad r = 3 \quad (\text{since } d\theta \text{ dr}) \\
 & = -\int_S r^2 \sin^2 \theta (r^2 \cos^2 \phi) dr + \int_S r^2 \sin^2(\frac{\pi}{2}) \cos^2 \phi dr + \int_S (3)^4 \sin^2 \theta \cdot dr \\
 & \quad \theta = \frac{\pi}{2} \quad r = 3 \\
 & = \int_0^3 \int_0^{\frac{\pi}{2}} r^2 \cos^2 \phi dr d\phi + 81 \int_0^{\frac{\pi}{2}} \int_0^{\frac{\pi}{2}} \sin^2 \theta d\theta d\phi \\
 & \quad \theta = 0 \quad \phi = 0 \\
 & = \int_{r=0}^3 r^2 [\sin \phi]_0^{\frac{\pi}{2}} dr + 81 \int_{\theta=0}^{\frac{\pi}{2}} \sin \theta \left[\frac{\pi}{2} - 0 \right] d\theta \\
 & = \frac{(3)^3}{3} \cdot 1 + 81 \times \frac{\pi}{2} \times [-\cos \theta]_0^{\frac{\pi}{2}} \\
 & = 9 + \frac{81\pi}{2}
 \end{aligned}$$

Again, Taking only right part

$$\begin{aligned}
 \int_{\text{vol.}} (\nabla \cdot \vec{A}) dV & = \int_{\text{vol.}} \left[\frac{1}{r^2} \frac{\partial (r^2 A_r)}{\partial r} + \frac{1}{r \sin \theta} \frac{\partial (r \sin \theta A_\theta)}{\partial \theta} + \frac{1}{r \sin \theta} \frac{\partial A_\phi}{\partial \phi} \right] \\
 & \quad [r^2 \sin \theta \cdot dr \cdot d\theta \cdot d\phi] \\
 & = \int_{\text{vol.}} \left[\frac{1}{r^2} \times 4r^3 + \frac{1}{r \sin \theta} \times (r \sin^2 \theta \cdot \cos \theta) + 0 \right] [r^2 \sin \theta \cdot dr \cdot d\theta \cdot d\phi] \\
 & = \int_{\text{vol.}} [4r + \frac{r \cos \theta}{\sin \theta} \cdot 2 \sin \theta \cdot \cos \theta] [r^2 \sin \theta \cdot dr \cdot d\theta \cdot d\phi] \\
 & = 4 \int_{r=0}^3 \int_{\theta=0}^{\frac{\pi}{2}} \int_{\phi=0}^{\frac{\pi}{2}} \sin \theta \left(\frac{\pi}{2} - 0 \right) dr d\theta d\phi + \int_{r=0}^3 \int_{\theta=0}^{\frac{\pi}{2}} \int_{\phi=0}^{\frac{\pi}{2}} \sin^2 \theta \sin \theta \cos 2\theta d\phi d\theta dr \\
 & = 2\pi \int_{r=0}^3 r^3 (r^4) dr + \frac{1}{2} \int_{r=0}^3 r^2 (-\cos 2\theta) \int_{\phi=0}^{\frac{\pi}{2}} d\phi dr
 \end{aligned}$$

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$$\begin{aligned}
 &= \frac{2\pi}{4} [x^4]_0^3 + \frac{1}{2} \cdot 2 \left[\frac{x^3}{3} \right]_0^3 \\
 &= \frac{81\pi}{2} + 9 \\
 &= 9 + \frac{81\pi}{2}
 \end{aligned}$$

इन्हानीय

$$= -9 + \frac{81\pi}{2}$$

$$\therefore \int_S \vec{A} \cdot d\vec{s} = \int_{vol.} (\nabla \cdot \vec{A}) \cdot dr = 9 + \frac{81\pi}{2} //$$

Qn: Given the flux density $\vec{D} = (2\cos\theta / r^3) \hat{a}_r + (\sin\theta / r^3) \hat{a}_\theta$ c/m²; evaluate both sides of the divergence theorem for the region defined by $1 < r < 2$, $0 < \theta < \frac{\pi}{2}$, $0 < \phi < \frac{\pi}{2}$.

Sol: Given,

$$\vec{D} = \frac{2\cos\theta}{r^3} \hat{a}_r + \frac{\sin\theta}{r^3} \hat{a}_\theta$$

$$\nabla \cdot \vec{D} = 0 < \theta < \frac{\pi}{2}, 0 < \phi < \frac{\pi}{2}.$$

From divergence theorem.

$$\int_S \vec{D} \cdot d\vec{s} = \int_{vol.} (\nabla \cdot \vec{D}) dr$$

Taking only left part

$$\begin{aligned}
 \int_S \vec{D} \cdot d\vec{s} &= \int_S \vec{D} \cdot \hat{a}_r \hat{s} + \int_S \vec{D} \cdot \hat{a}_\theta \hat{s} - \int_S \vec{D} \cdot \hat{a}_\phi \hat{s} \\
 &\text{front} \quad \text{back} \quad \text{top} \quad \text{bottom} \\
 &(r=2) \quad (r=1) \quad (\theta=\pi/2) \quad (\theta=0)
 \end{aligned}$$

* Taking only right part

$$\begin{aligned}
 \int_{vol.} (\nabla \cdot \vec{D}) dr &= \int_{vol.} \left[\frac{1}{r^2} \cdot \frac{\partial (r^2 D_r)}{\partial r} + \frac{1}{r^2} \cdot \frac{\partial D_\theta}{\partial \theta} + \frac{1}{r^2} \cdot \frac{\partial D_\phi}{\partial \phi} \right] dr
 \end{aligned}$$

$$\nabla \cdot \vec{B} = \frac{1}{r^2} \frac{\partial (r^2 \frac{\cos\theta}{r^3})}{\partial r} + \frac{1}{r \sin\theta} \cdot \frac{\partial (\sin\theta \cdot \frac{\sin\phi}{r^3})}{\partial \theta} + 0$$

$$= -\frac{2 \cos\theta}{r^2} \cdot \frac{1}{r^2} + \frac{1}{r \sin\theta} \cdot \frac{1}{r^3} \cdot 2 \sin\theta \cdot \cos\theta$$

$$= -\frac{2 \cos\theta}{r^4} + \frac{2 \cos\theta}{r^4}$$

$= 0$

$$\int_{\text{rel.}} (\nabla \cdot \vec{B}) dr = 0.$$

$$\begin{aligned}
 \oint \vec{B} \cdot d\vec{s} &= - \iint_{\theta=0}^{\pi/2} \frac{2 \cos\theta}{r^3} \cdot r^2 \sin\theta d\theta + \int_{\theta=0}^{\pi/2} \int_{r=2}^{\pi/2} \frac{2 \cos\theta}{r^3} \cdot r^2 \sin\theta d\theta dr \\
 &\quad (\theta=0) \quad (\theta=\pi/2) \\
 &+ \int_{r=1}^2 \int_{\theta=0}^{\pi/2} \frac{\sin\theta}{r^3} \cdot r \sin\theta d\theta dr - \int_{r=1}^2 \int_{\theta=0}^{\pi/2} \frac{\sin\theta}{r^3} \cdot r \sin\theta d\theta dr \\
 &\quad (\theta=0) \quad (\theta=\pi/2) \\
 &\quad |(\theta=\frac{\pi}{2}) \\
 &= - \iint_{\theta=0}^{\pi/2} \frac{\sin 2\theta}{4} d\theta + \int_{\theta=0}^{\pi/2} \int_{r=2}^{\pi/2} \frac{\sin 2\theta}{2r} d\theta dr \\
 &+ \int_{r=1}^2 \int_{\theta=0}^{\pi/2} \frac{1}{r^2} d\theta dr - 0 \\
 &= + \frac{1}{2} \left[\frac{\cos 2\theta}{2} \right]_0^{\pi/2} \cdot \left[\frac{\pi}{2} - 0 \right] + \left(-\frac{1}{2} \right) \left[\frac{1}{r} \right]^2_1 \cdot \left[\frac{\pi}{2} - 0 \right]
 \end{aligned}$$

Qn: Given $\vec{D} = 8xy \hat{i} + 4x^2z^4 \hat{i} + 16x^2y^2z^2 \hat{k}$ A/m^2
 verify both sides of divergence theorem for the rectangular parallelopiped $0 < x < 2, 0 < y < 3, 0 < z < 2.$

$$\boxed{\text{Ans: } [8.17] 4.9 \text{ pC}}$$

Qn: Given the field $\vec{D} = 6s \sin \frac{\theta}{2} \hat{i} + 4s \cos \frac{\theta}{2} \hat{j} \text{ A/m}^2$
 evaluate both sides of the divergence theorem for the region bounded by $\rho = 2, \theta = 0, \theta = \pi, z = 0 \text{ to } z = 5.$

$$\text{Ans: } -225 \epsilon_0 225 \text{ C}$$

Qn: Evaluate both

Qn: Let $\vec{D} = 8s \sin \frac{\theta}{2} \hat{i} + 4s \cos \frac{\theta}{2} \hat{j} \text{ A/m}^2,$
 sides of divergence theorem for the region $0 < s < 1.8,$
 $\theta < \phi < \pi/2$ [8.13c]

$$20^\circ < \phi < 70^\circ, 2.4 < z < 3.1.$$

$$\begin{aligned}
 \text{Sol: } \nabla \cdot \vec{D} &= \frac{1}{s} \frac{\partial (s D_p)}{\partial s} + \frac{1}{p} \frac{\partial D_\theta}{\partial \theta} + \frac{\partial D_z}{\partial z} \\
 &= \frac{6}{p} \frac{\partial (p^2 \sin \frac{\theta}{2})}{\partial p} + \frac{1}{p} \frac{\partial (1.8 \rho \cos \frac{\theta}{2})}{\partial \theta} + 0 \\
 &= \frac{6 \times 2 \rho \sin \frac{\theta}{2}}{p} + \frac{1 \times 1.8 \rho (-\sin \frac{\theta}{2})}{p} \\
 &= 12 \sin \frac{\theta}{2} + 0.75 \sin \frac{\theta}{2} \\
 &= 11.25 \sin \frac{\theta}{2}
 \end{aligned}$$

$$\begin{aligned}
 \int (\nabla \cdot \vec{D}) dv &= \int_{z=0}^{5} \int_{\theta=0}^{\pi} \int_{p=0}^{1.8} 11.25 \sin \frac{\theta}{2} p d\theta dz dp \\
 &= 11.25 \left[\frac{p^2}{2} \right]_{0}^{1.8} \left[-\cos \frac{\theta}{2} \right]_{0}^{\pi} \cancel{[11.25 \times 0]} \times 2 \\
 &= 11.25 \times \frac{4}{2} \times 1 \times 0.75 \times 2 \\
 &= 225 \text{ C.}
 \end{aligned}$$

$$\text{Qn: If } \vec{D} = 15\rho^2 \sin^2\theta \hat{\rho} + 10\rho^2 \cos^2\theta \hat{\theta} \text{ C/m}^2, \text{ evaluate}$$

both sides of divergence theorem for the region :

$$1 < \rho < 2 \text{ m}, \quad 1 < \theta < 2 \text{ rad}, \quad 1 < z < 2 \text{ m}.$$

[Ans: - 6.93C]

~~Qn: Evaluate both sides of the divergence theorem for the region:~~

~~Ans:~~

$$\text{Ans: } \frac{16}{\pi} \cos 2\theta \hat{\alpha}_\theta \text{ C/m}^2,$$

~~Qn: Given the flux density, $\frac{16}{\pi} \cos 2\theta \hat{\alpha}_\theta \text{ C/m}^2$, evaluate both sides of divergence theorem for the region: $1 < r < 2 \text{ m}, \quad 1 < \theta < 2 \text{ rad}, \quad 1 < z < 2 \text{ m}$.~~

~~Ans: - 3.91C~~

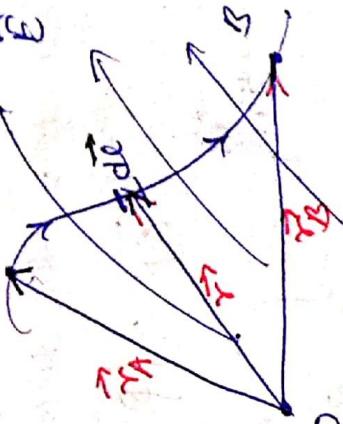
Electric Potential & Work (Potential field of a point charge)

If a charge q is placed in an electric field \vec{E} , then the force due to electric field is given by $\vec{F} = q\vec{E}$ [Coulomb's Law]. Suppose we wish to move a point charge from point A to point B in an electric field \vec{E} as in figure. Then, the work done in moving the charge q in electric field \vec{E} for a displacement A to B is

$$\text{d}W = -\vec{F} \cdot \vec{d}\ell = -q\vec{E} \cdot \vec{d}\ell$$

The -ve sign indicates that the work is being done by an external agent. Thus the total work done, or the potential energy required in moving q from A to B is

$$W = -q \int_A^B \vec{E} \cdot d\vec{\ell}$$



$$\begin{aligned} d\vec{\ell} &= dx \hat{i}_x + dy \hat{i}_y + dz \hat{i}_z \\ d\vec{\ell} &= ds \hat{a}_s + pd\theta \hat{a}_\theta + rd\phi \hat{a}_\phi \\ d\vec{\ell} &= dr \hat{a}_r + r d\theta \hat{a}_\theta + r \sin\theta d\phi \hat{a}_\phi \end{aligned}$$

$$\text{Again, } \frac{W}{q} = V_{BA} = - \int_A^B \vec{E} \cdot d\vec{\ell}$$

This is the potential energy per unit charge, denoted by V_{BA} and also known as potential difference bet. points A & B.

B.

Note:

- 1.) In determining V_{BA} , A is the initial point while B is final point.
- 2.) If V_{BA} is -ve, there is a loss in potential energy in moving q from A to B; this implies that the work done is by the field. However, if V_{BA} is +ve, there is a gain in potential energy in the movement; an external agent performs the work.
- 3.) V_{BA} is independent of the path taken.
- 4.) V_{BA} is measured in joules per coulomb, commonly as volts(V).

(84) → Work done by external source against field → +ve
→ Work done by field → -ve

We have, from Coulomb's Law, the field \vec{E} due to point charge Q located at origin is

$$\vec{E} = \frac{Q}{4\pi\epsilon_0 r^2} \hat{ar}$$

Potential difference is defined as the workdone (by an external source) in moving a unit positive charge from one point to another in an electric field.

$$\text{Then, } V_{BA} = - \int_A^B \frac{Q}{4\pi\epsilon_0 r^2} \hat{ar} \cdot dr \hat{ar}$$

$$\text{or, } V_{BA} = \frac{Q}{4\pi\epsilon_0} \left[\frac{1}{r_B} - \frac{1}{r_A} \right].$$

or, $V_{BA} = V_B - V_A$
 where, V_B and V_A are the potentials (or absolute potentials) at B and A, respectively. Thus the potential difference V_{BA} may be regarded as the potential at B with reference to choose infinity as reference point. That is, we assume the potential at infinity is zero. Thus, if $V_A = 0$ as $r_A \rightarrow \infty$, then the potential at any point ($r_B \rightarrow r$) due to a point charge Q located at the origin is.

If reference is not at infinity then $V = \frac{Q}{4\pi\epsilon_0 r} + C_1$, C_1 is potential at the reference point (\vec{ar}), any contribution since, \vec{E} points in the radial direction in θ or ϕ direction it wiped out by the from a displacement $\vec{E} \cdot d\vec{l} = E \cos\theta dl = Edr$. Hence, potential difference is independent of the path.

The potential at any point is the potential difference betw. that point and a chosen point at which the potential is zero.

(85) In other words, by assuming zero potential at ∞ , the potential at a distance r from the point charge is the work done per unit charge by an external agent in moving a test charge from infinity to that point.

$$\text{i.e. } V = - \int_{\infty}^r \vec{E} \cdot d\vec{l}$$

If a point charge q is not located at origin but at a point whose position vector is \vec{r}' , then, the potential $V(x, y, z)$ or $V(\vec{r})$ at \vec{r} becomes:

$$V(\vec{r}) = \frac{q}{4\pi\epsilon_0 |\vec{r} - \vec{r}'|}$$

Then, for n point charges, q_1, q_2, \dots, q_n located at points with position vectors $\vec{r}_1, \vec{r}_2, \dots, \vec{r}_n$, the potential at \vec{r} is

$$V(\vec{r}) = \frac{q_1}{4\pi\epsilon_0 |\vec{r} - \vec{r}_1|} + \frac{q_2}{4\pi\epsilon_0 |\vec{r} - \vec{r}_2|} + \dots + \frac{q_n}{4\pi\epsilon_0 |\vec{r} - \vec{r}_n|}$$

$$\text{or, } V(\vec{r}) = \frac{1}{4\pi\epsilon_0} \sum_{k=1}^n \frac{q_k}{|\vec{r} - \vec{r}_k|}$$

Now, for line, surface & volume charges

$$V(\vec{r}) = \frac{1}{4\pi\epsilon_0} \int_L \frac{\rho_L(\vec{r}') dl'}{|\vec{r} - \vec{r}'|}$$

$$V(\vec{r}) = \frac{1}{4\pi\epsilon_0} \int_S \frac{\sigma_s(\vec{r}') ds'}{|\vec{r} - \vec{r}'|}$$

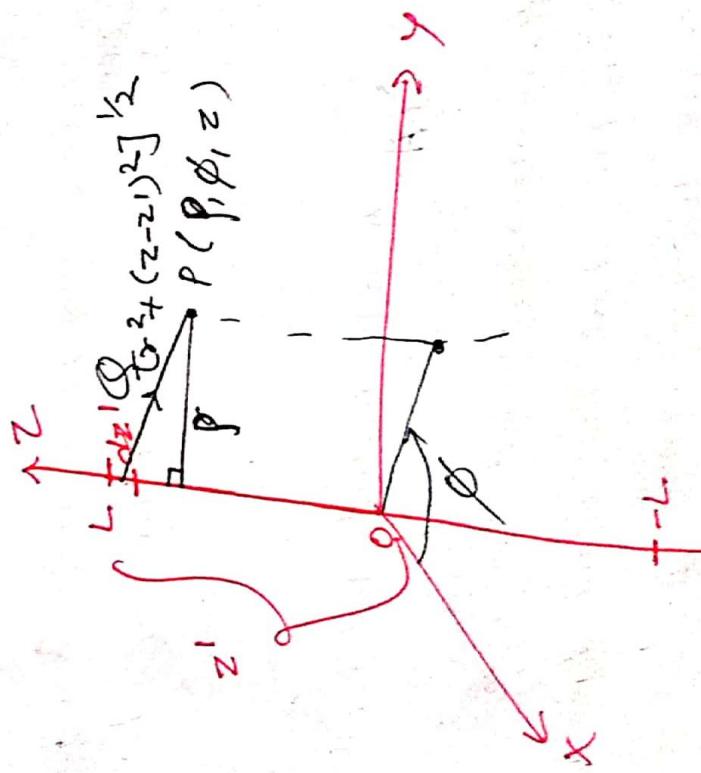
$$V(\vec{r}) = \frac{1}{4\pi\epsilon_0} \cdot \int_{Vol.} \frac{\rho_v(\vec{r}') dv'}{|\vec{r} - \vec{r}'|}$$

Finite length line charge

Consider the uniform distribution of line charge ρ_L of finite length $2L$ centered on the z -axis. Distinguishing betwⁿ position of charge element $dq = \rho_L dz'$ at z' and the field point at co-ordinate z , the distance betwⁿ source and field is

$$\sqrt{\rho^2 + (z - z')^2}$$

$$\begin{aligned} \text{then, } V &= \int_{-L}^{L} \frac{\rho_L dz'}{4\pi\epsilon_0 (\rho^2 + (z - z')^2)^{1/2}} \\ &= -\frac{\rho_L}{4\pi\epsilon_0} \ln \left(\frac{z - L + (\rho^2 + (z - L)^2)^{1/2}}{z + L + (\rho^2 + (z + L)^2)^{1/2}} \right) \\ &= -\frac{\rho_L}{4\pi\epsilon_0} \left[\sinh^{-1} \frac{\rho}{L+z} - \sinh^{-1} \frac{\rho}{L-z} \right] \end{aligned}$$



Qn: If we take a reference, for potential at infinity find the potential at $(0, 0, 2)$ caused by this charge configuration in free space: (a) 12 nC/m on the line $P = 2.5m, z=20$

- (b) point charge of 18 nC at $(1, 2, -1)$ (c) 12 nC/m on the line $y = 2.5$, $z=0$, $-1.0 < x < 1.0$. [Ans: 529 V; 43.2 V, 66.41 V]

Soln:

(a) For line charge

$$\begin{aligned} V \text{ at } (0, 0, 2) &= \int_0^{2\pi} \frac{\rho L \cdot \rho d\phi}{4\pi \epsilon_0 \sqrt{\rho^2 + z^2}} \\ &= \int_0^{2\pi} \frac{12 \times 10^{-9} \times 2.5 \times d\phi}{4\pi \epsilon_0 \sqrt{2.5^2 + 2^2}} \\ &= \frac{108 \times 2.5 \times 2\pi}{\sqrt{2.5^2 + 2^2}} \\ &= 529.885 \text{ V} \end{aligned}$$

$$\begin{aligned} &\therefore V = \int \frac{\rho_L d\phi}{4\pi \epsilon_0 \sqrt{z^2 + \rho^2}} \\ &= \int_0^{2\pi} \frac{\rho_L d\phi}{4\pi \epsilon_0 \sqrt{2.5^2 + \rho^2}} \\ &= \rho_L = \rho \frac{d\phi}{2\pi} \end{aligned}$$

(b) For point charge

$$\begin{aligned} V \text{ at } (0, 0, 2) &= \frac{Q}{4\pi \epsilon_0 r} = \frac{18 \times 10^{-9}}{36\pi \epsilon_0} \times \frac{1}{\sqrt{(0-1)^2 + (0-2)^2 + (2+1)^2}} \\ &= \frac{18 \times 9}{\sqrt{14}} \\ &= 43.2 \text{ V} \end{aligned}$$

(c) For line charge

$$\begin{aligned} V \text{ at } (0, 0, 2) &= \int_{-1}^1 \frac{\rho_L dx}{4\pi \epsilon_0 \sqrt{\rho^2 + x^2}} \\ &= \frac{12 \times 10^{-9}}{36\pi \epsilon_0} \cdot \ln \left(x + \sqrt{\rho^2 + x^2} \right) \Big|_{-1}^1 \\ &= 108 \times \left[\ln(1 + \sqrt{1 + 10 \cdot 25}) - \ln(-1 + \sqrt{1 + 10 \cdot 25}) \right] = 66.41 \text{ V} \end{aligned}$$

$$\begin{aligned} &\text{where, } \rho = \sqrt{(0-0)^2 + (0-2)^2 + (2+1)^2} \\ &= \sqrt{2.5^2 + 2^2} \\ &= 3.20156 \end{aligned}$$

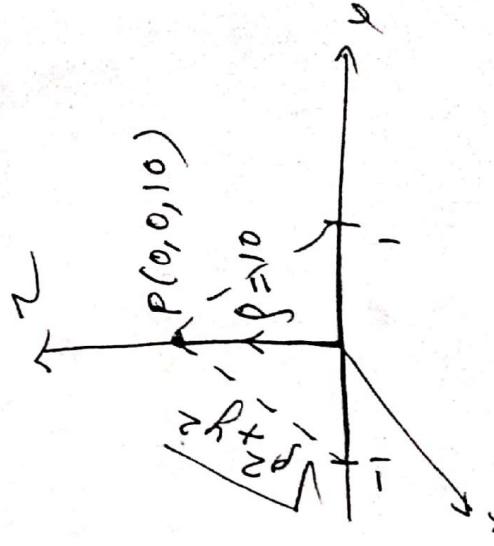
Qn: Assume a zero reference at infinity. Find the potential at $P(0, 0, 10)$ that is caused by this charge configuration in free space :
 ① 20 nC at the origin ; ② 10 nC/m along the line $x=0$, $z=0$, $-1 \leq y \leq 1$; ③ 10 nC/m along the line $x=0, y=0$, $1 \leq z \leq 11$.

Ans : ① 17.98 V ② 13.95 V ③ 18.04 V

Sol: ① For point charge

$$V_p = \frac{q}{4\pi\epsilon_0 r_p} \quad \text{where, } r_p = \sqrt{(0-0)^2 + (0-0)^2 + (10-0)^2} = 10$$

$$\therefore V_p = \frac{20 \times 10^{-9}}{4\pi\epsilon_0 \times 10^9 \times 10} = 18 \text{ V or } 17.98 \text{ if } \epsilon_0 = 8.85 \times 10^{-12}$$



$$\begin{aligned} ② V_p &= \int_{-1}^1 \frac{\rho_L dy}{4\pi\epsilon_0 \int s^2 ds} \\ &= \int_{-1}^1 \frac{10x 10^{-9}}{4\pi\epsilon_0 \frac{1}{3} \pi s^3} \frac{dy}{\sqrt{s^2 + y^2}} \\ &= 90x \left[\int_{-1}^1 \frac{dy}{\sqrt{s^2 + y^2}} \right] \Big|_1^1 \quad \text{where } p = 10 \\ &= 90 \left[\ln(1 + \sqrt{100+1}) - \ln(-1 + \sqrt{100+1}) \right] \end{aligned}$$

$$= 17.97 \text{ V}$$

86:

Work done is independent of Path taken (or Physical interpretation of line integral)

The workdone in moving a point charge q from one point to another is given by

$$W = -q \int_{\text{Initial}}^{\text{Final}} \vec{E} \cdot d\vec{l}$$

where, $d\vec{l}$ = differential vector path length.

$$= -q \int_{\text{Initial}}^{\text{Final}} \vec{E}_L dl$$

where, E_L is the component of \vec{E} along $d\vec{l}$.

Consider a region having uniform electric field intensity as shown in figure. we have to calculate the workdone in carrying a charge q from B to A.

From above workdone value in integral form, we can calculate the total workdone but if the path B to A is divided into very small segments and calculate the workdone for each segments by multiplying \vec{E} by $d\vec{l}$ along the path directions then we can get total workdone by adding all segments workdone as:

$$W = -q (E_{L_1} \Delta l_1 + E_{L_2} \Delta l_2 + \dots + E_{L_N} \Delta l_N + \dots)$$

$$E_{L_N} \Delta l_N)$$

Using vector notation

$$W = -q (\vec{E}_1 \cdot \vec{\Delta l}_1 + \vec{E}_2 \cdot \vec{\Delta l}_2 + \dots + \vec{E}_N \cdot \vec{\Delta l}_N)$$

since, $\vec{E}_1 = \vec{E}_2 = \vec{E}_3 = \dots = \vec{E}_N = \vec{E}$ for Uniform field

(8) then,

$$W = -q \vec{E} \cdot (\vec{L}_{L_1} + \vec{L}_{L_2} + \vec{L}_{L_3} + \cdots + \vec{L}_{L_N}) = \vec{L}_{BA}$$

= a vector directed from initial point to final point.

Since, the vector from initial point to final point will be same whether the path is different, the work done in moving a point charge from initial point to final point is independent of the path taken.

$$\therefore W = -q \vec{E} \cdot \vec{L}_{BA}$$

This shows that work done is independent of the path taken.

Work done in carrying a charge Q around a circular path of radius, a in presence of the field due to a uniform line charge at center of the circular

Path.

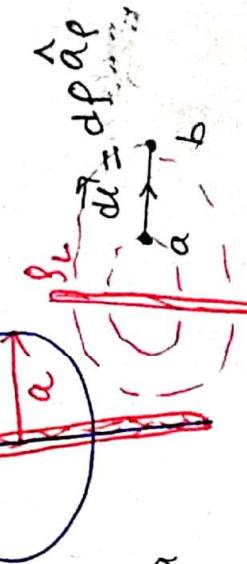
Here, a uniform line charge of density ρ_L is placed in the center of circular path if placed in the center of circular path $d\vec{E} = q d\rho \hat{\alpha}$ where q charge, ρ is moved from one point to another.

From previous derivations

\vec{E} due to uniform line charge at a

point is

$$\vec{E} = \frac{\rho_L}{2\pi\epsilon_0 r} \hat{\alpha}_r$$



Let us take a differential displacement $d\vec{l}$ = a $d\hat{\alpha}_\theta$ in cylindrical Co-ordinate systems.

Then : the work done is given by

$$W = -Q \int_{\text{initial}}^{\text{final}} \vec{E} \cdot d\vec{l}$$

$$= -Q \int_0^{2\pi} \frac{p_L}{2\pi\epsilon_0} \hat{a}_p \cdot a \, d\theta \, \hat{a}_\theta \\ = 0 \quad [\hat{a}_p \cdot \hat{a}_\theta = 0]$$

i.e the work done in moving the point charge q , in circular path is zero.

Again, if we choose the differential displacement in the path $p=a$ to $p=b$ in radial path then

$$d\vec{l} = dp \hat{a}_p \quad \text{and} \quad W = -Q \int_{\text{initial}}^{\text{final}} \frac{p_L}{2\pi\epsilon_0} \hat{a}_p \cdot dp \, \hat{a}_\theta$$

$$\text{or } W = -Q \int_a^b \frac{p_L}{2\pi\epsilon_0} \, dp$$

$$\therefore W = -Q \frac{p_L}{2\pi\epsilon_0} \ln\left(\frac{b}{a}\right)$$

since, b is greater than a so the value $\ln\left(\frac{b}{a}\right)$ becomes +ve & work done, W will be -ve i.e by field.

Conservative field: Any field that satisfies $\vec{E} \cdot d\vec{l} = 0$ (no work is done in carrying the unit charge around any closed path) is said to be a conservative field. i.e no work is done (or the energy is conserved) around a closed path.

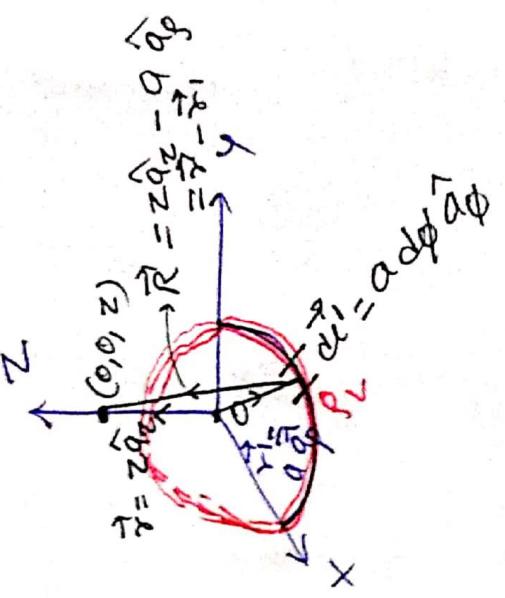
(Q) The gravitational field is also conservative for any energy expended in moving (raising) an object against the field is recovered exactly when the object is returned (lowered) to its original position.

(Qn): Find the electric potential at a point on the z-axis due to a line charge ρ_L in the form of a circular ring of radius 'a' placed on the xy-plane ($z=0$ plane).

Sol:

we have,

$$\begin{aligned}
 V &= \frac{\int \rho_L' dr'}{4\pi\epsilon_0 |\vec{r} - \vec{r}'|} \\
 &= \int_{\rho=0}^{2\pi} \frac{\rho_L a d\phi}{4\pi\epsilon_0 \sqrt{a^2 + z^2}} \\
 &= \frac{2\pi a \rho_L}{4\pi\epsilon_0 \sqrt{a^2 + z^2}} \\
 &= \frac{a \rho_L}{2\epsilon_0 \sqrt{a^2 + z^2}}
 \end{aligned}$$



Equipotential Surface

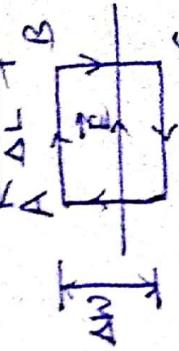
The surface over which the potential is same at all the points is known as equipotential surface.

If A and B are two points in the equipotential surface then

$$V_A - V_B = 0$$

i.e From figure

$$\oint_{\text{closed loop}} \vec{E} \cdot d\vec{l} = \int_A^B \vec{E} \cdot d\vec{l} + \int_B^C \vec{E} \cdot d\vec{l} + \int_C^A \vec{E} \cdot d\vec{l} + \int_A^A \vec{E} \cdot d\vec{l}$$



$$= \epsilon_0 E \cdot d\vec{l} + 0 - \nabla \phi \cdot \vec{l} + 0$$

i.e. $\oint E \cdot d\vec{l} = 0$ [It is only applicable for static fields]

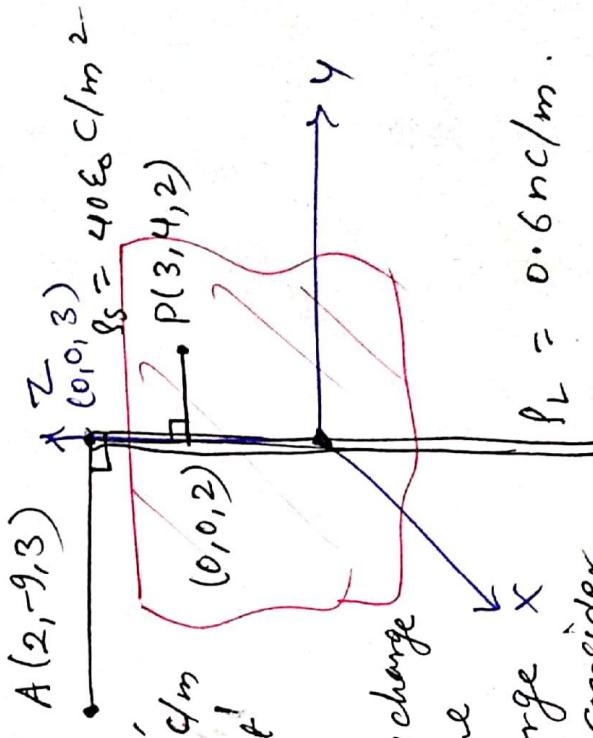
These surfaces for which $\oint \vec{E} \cdot d\vec{l} = 0$ is known as equipotential surface. \vec{E} is known as conservative field.

Qn: A uniform sheet of charge, $\sigma_s = 40 \epsilon_0 \text{ C/m}^2$ is located in the plane $x=0$ in free space. A uniform line charge ρ_L of 0.6 nC/m lies along the z -axis in free space. Find the potential at point $P(3,4,2)$ if $V=5V$ at $A(2,-9,3)$.
Sol:

Given,

uniform sheet charge,

$\sigma_s = 40 \epsilon_0 \text{ C/m}^2$ at $x=0$ plane,
uniform line charge, $\rho_L = 0.6 \text{ nC/m}$
along z -axis and $V=5V$ at
 $A(2,-9,3)$.



Since, the field due to line charge & sheet charge affects the movement of the unit charge in the field, we need to consider the potential due to line charge field & sheet charge field.

Now, Potential at P due to line charge is

$$V_P = -\frac{\rho_L}{2\pi\epsilon_0} \ln(s_p) + C_1$$

$$\text{where, } s_p = \sqrt{(3-0)^2 + (4-0)^2 + (2-2)^2} = 5$$

(Q) Again, potential at p due to sheet charge is

$$V_{P_5} = -\frac{\rho_s}{2\epsilon_0} x_p + C_2$$

where, $x_p = 3$

Then,

total potential at P, $V_P = V_{P_2} + V_{P_5}$

$$\begin{aligned} &= -\frac{\rho_L}{2\pi\epsilon_0} \ln(5) + \left(\frac{-\rho_s}{2\epsilon_0} \cdot 3\right) + C_1 \\ &= -\frac{0.6 \times 10^{-9}}{2\pi \times 10^{-9}} \cdot \ln(5) - \frac{40\epsilon_0}{2\epsilon_0} \times 3 + C \end{aligned}$$

$$\text{or, } V_P = -0.6 \times 12 \times 1.61 - 20 \times 3 + C$$

$$\text{or, } V_P = -77.39 + C$$

where, $C = C_1 + C_2$

since, $V_A = 5V$

$$\text{or, } -\frac{\rho_L}{2\pi\epsilon_0} \ln(9_A) - \frac{\rho_s}{2\epsilon_0} x_A + C = 5$$

$$\text{or, } -\frac{0.6 \times 10^{-9}}{2\pi \times 10^{-9}} \ln(9_A) - \frac{40\epsilon_0}{2\epsilon_0} x_A + C = 5$$

$$\text{where, } \rho_A = \sqrt{(2-0)^2 + (-9-0)^2 + (3-3)^2}$$

$$\begin{aligned} &= \sqrt{4+81} \\ &= \sqrt{85} \end{aligned}$$

$$x_A = 2$$

$$Qx_1 - 0.6 \times 18 \ln(\frac{1}{\sqrt{5}}) - 20x_2 + c = 5$$

$$0x_1 - 18.98 - 40 + c = 5$$

$$\therefore 0x_1 - 18.98 - 40 + c = 5$$

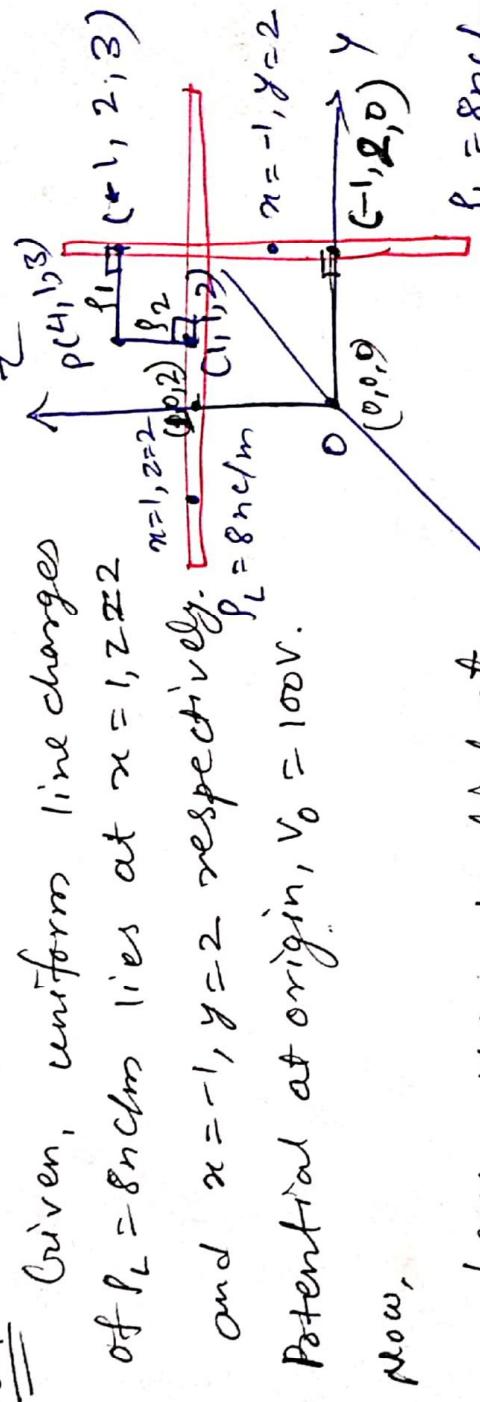
Now,

$$V_p = -77.39 + 68.98$$

$$V_p = -77.39 + c = -8.4V$$

Qn: Two uniform line charges 8nC/m each are located at $x=1, z=2$ and at $x=-1, y=2$ in free space. If the potential at the origin is 100V , find V at $P(4, 1, 3)$. [2011 Jhawar]

Sol:



Now,

$$p_L = 8\text{nC/m}.$$

we have, the potential at

Point $P(4, 1, 3)$ is due to

two line charges : So,

$$V_p = -\frac{p_L}{2\pi\epsilon_0} \ln(p_1) - \frac{p_L}{2\pi\epsilon_0} \ln(p_2) + c.$$

$$= -\frac{8 \times 10^{-9}}{2\pi \times 10^{-9}} \cdot \ln(p_1) - \frac{8 \times 10^{-9}}{2\pi \times 10^{-9}} \cdot \ln(p_2) + c$$

$$= -8 \times 18 \ln(p_1) - 8 \times 18 \ln(p_2) + c$$

(93) where, $\beta_1 = \sqrt{(4+1)^2 + ((-2)^2 + (3-3)^2)}$

$$= \sqrt{26}$$

$$\text{& } \beta_2 = \sqrt{(4-1)^2 + ((-1)^2 + (3-3)^2)} \\ = \sqrt{10}$$

$$\therefore V_p = -144 \ln(\sqrt{26}) - 144 \ln(\sqrt{10}) + C$$

$$\text{or, } V_p = -234.58 - 165.786 + C$$

$$\text{or, } V_p = -400.37 + C$$

Again,

$$V_0 = 100 \text{ V}$$

$$\text{or, } \frac{(-\beta_1)}{2\pi\epsilon_0} \ln(\beta_{1,0}) + \frac{(-\beta_2)}{2\pi\epsilon_0} \ln(\beta_{2,0}) + C = 100$$

$$\text{or, } -8 \times 18 \ln(\beta_{1,0}) - 8 \times 18 \ln(\beta_{2,0}) + C = 100$$

$$\text{where, } \beta_{1,0} = \sqrt{(-1)^2 + (0-0)^2} = \sqrt{1} \\ \text{& } \beta_{2,0} = \sqrt{(0+1)^2 + (0-2)^2 + (0-0)^2} = \sqrt{5}$$

$$\therefore -144 \ln(\sqrt{5}) - 144 \ln(\sqrt{5}) + C = 100$$

$$\text{or, } -288 \ln(\sqrt{5}) + C = 100$$

$$\text{or, } -231.76 + C = 100$$

$$\text{or, } 81 = 331.76 \Rightarrow V_p = -400.37 + 331.76 = -68.61 \text{ V}$$

Potential due to point charge

$$V = -\frac{q}{4\pi\epsilon_0} \int_A^B \vec{dr} \cdot d\vec{r}$$

$$= -\frac{q}{4\pi\epsilon_0} \int_A^B \frac{1}{r^2} dr \cdot d\vec{r}$$

$$= -\frac{qQ'}{4\pi\epsilon_0 r} \Big|_A^B$$

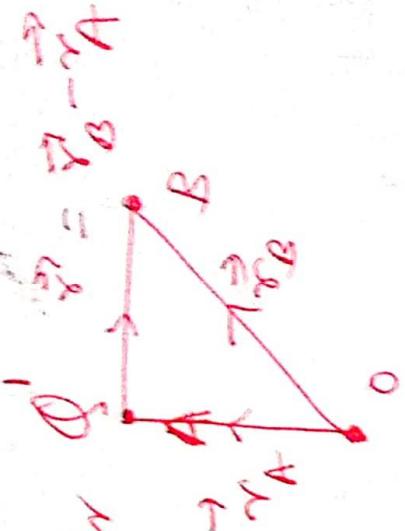
$$= \frac{qQ'}{4\pi\epsilon_0} \left[\frac{1}{r_B} - \frac{1}{r_A} \right]$$

$$= \frac{q}{4\pi\epsilon_0 r_B} - \frac{q}{4\pi\epsilon_0 r_A}$$

$$\text{or, } \frac{W}{q} = V_{BA} = V_B - V_A \Rightarrow$$

where, $V_B = \frac{Q}{4\pi\epsilon_0 r_B} + C$ \rightarrow reference point

$V_A = \frac{Q}{4\pi\epsilon_0 r_A} + C$ \rightarrow reference point



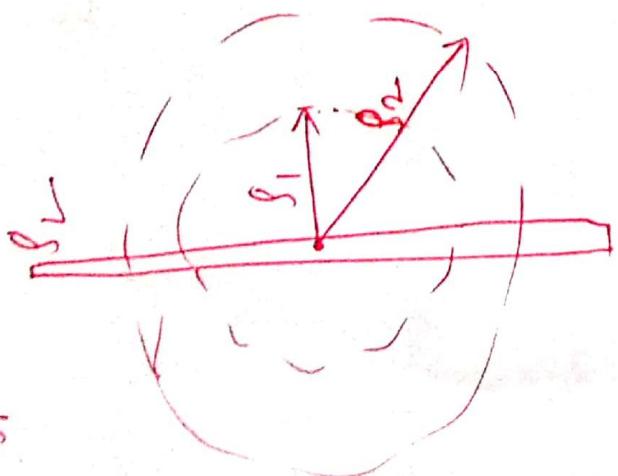
$$\frac{q}{4\pi\epsilon_0 r} = 880$$

If $C = 0$

$$V_B = \frac{Q}{4\pi\epsilon_0 r_B} + C$$

line charge

$$W = -Q \int_{\rho_1}^{\rho_2} \int_{\rho_1}^{\rho_2} \frac{\rho_2}{2\pi\epsilon_0} \hat{r} d\rho_2 d\rho_1$$



$$= -Q \frac{\rho_L}{2\pi\epsilon_0} \left[\ln(\rho_2) - \ln(\rho_1) \right]$$

$$= -Q \frac{\rho_L}{2\pi\epsilon_0} \ln\left(\frac{\rho_2}{\rho_1}\right)$$

$$\text{or, } \frac{W}{Q} = -\frac{\rho_L}{2\pi\epsilon_0} \ln\left(\frac{\rho_2}{\rho_1}\right)$$

$$\text{or, } V_{\rho_2} = -\frac{\rho_L}{2\pi\epsilon_0} \ln\left(\frac{\rho_2}{\rho_1}\right)$$

$$= -\frac{\rho_L}{2\pi\epsilon_0} \ln(\rho_2) + \frac{\rho_L \cdot \rho_1}{2\pi\epsilon_0}$$

$$= V_{\rho_2} - V_{\rho_1}$$

i.e., $V_{\rho_1} = -\frac{\rho_L}{2\pi\epsilon_0} \ln(\rho_1) + C_1$

& $V_{\rho_2} = -\frac{\rho_L}{2\pi\epsilon_0} \ln(\rho_2) + C_2$

point is at $\rho = 0$
if not, if $C_1 = 0$
then C_2

For sheet charge

$$W = -Q \int_A^B \vec{E} \cdot d\vec{l}$$

$$= -Q \int_A^B \frac{\rho_s}{2\epsilon_0} \cdot \hat{q}_A \cdot d\hat{q}_A$$

$$= -Q \frac{\rho_s}{2\epsilon_0} \cdot [V_B - V_A]$$



$$\text{or, } \frac{W}{Q} = V_{BA} = \frac{-\rho_s}{2\epsilon_0} [V_B - V_A] \quad V_B - V_A$$

$$\text{or, } V_{BA} = V_B - V_A$$

$$V_B = \frac{-\rho_s}{2\epsilon_0} V_B + c_1$$

$$V_A = \frac{-\rho_s}{2\epsilon_0} V_A + c_2$$

point referred
with other
if at C₂
 $c_1 = 0 \neq c_2$

(4) Qn: An electric field is expressed in Cartesian Co-ordinate system
 $\vec{E} = 6x^2\hat{a}_x + 6y\hat{a}_y + 4z\hat{a}_z$ v/m. find (i) V_m if points M & N
 are specified by M(2, 6, -1) and N(-3, -3, 2) (ii) V_m if $V_\infty = 0$ at
 $\vec{Q}(4, -2, -3)$ (iii) V_m if $V=2$ at P(1, 2, -4).

Soln Given, $\vec{E} = 6x^2\hat{a}_x + 6y\hat{a}_y + 4z\hat{a}_z$ v/m.

$$\begin{aligned}
 @ V_{M,N} &= - \int_M^N (6x^2\hat{a}_x + 6y\hat{a}_y + 4z\hat{a}_z) \cdot (dx\hat{a}_x + dy\hat{a}_y + dz\hat{a}_z) \\
 &= - \int_{-3}^2 6x^2 dx - 6 \int_{-3}^6 y dy - 4 \int_2^{-1} dz \\
 &= - \frac{6}{3} [(2)^3 - (-3)^3] - \frac{6}{2} [6^2 - (-3)^2] - 4 (-1 - 2) \\
 &= -139 \text{ V}.
 \end{aligned}$$

Again,

(b) $V_Q = 0$ at $\vec{Q}(4, -2, -3)$ then

$$V_{M,Q} = - \int_M^Q \vec{E} \cdot d\vec{l}$$

$$\begin{aligned}
 &= - \int_Q^M (6x^2\hat{a}_x + 6y\hat{a}_y + 4z\hat{a}_z) \cdot (dx\hat{a}_x + dy\hat{a}_y + dz\hat{a}_z) \\
 &= - \int_4^2 6x^2 dx - 6 \int_{-2}^6 y dy - 4 \int_{-3}^{-1} dz \\
 &= - \frac{6}{3} [(2)^3 - 4^3] - \frac{6}{2} [6^2 - (-2)^2] - 4 [-1 + 35] \\
 &= -120 \text{ V}
 \end{aligned}$$

Now,

$$\begin{aligned}
 V_{M,Q} &= V_m - V_Q \\
 \text{or, } -120 &= V_m - 0 \Rightarrow V_m = -120 \text{ V}
 \end{aligned}$$

$$Q) \text{ At } P(1, 2, -4), V_p = 2V$$

then,

$$V_{kp} = - \int_P^k \vec{E} \cdot d\vec{l}$$

$$= - \int_P^k (6x^2 \hat{a}_x + 6y \hat{a}_y + 4 \hat{a}_z) \cdot (dx \hat{a}_x + dy \hat{a}_y + dz \hat{a}_z)$$

$$= -6 \int_1^{-3} x^2 dx - 6 \int_2^{-3} dy - 4 \int_{-4}^2 dz$$

$$= -\frac{6}{3} [(-3)^3 - 1^3] - \frac{6}{2} [(-3)^2 - 2^2] - 4 [2 + 4]$$

$$= 17V$$

now,

$$V_{kp} = V_k - V_p$$

$$\text{or, } 17 = V_k - 2$$

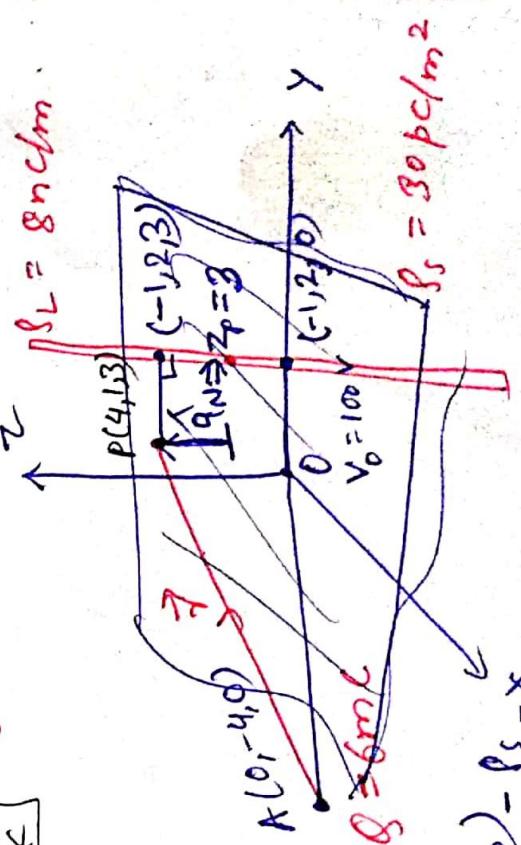
$$\text{or, } V_k = 19V$$

Qn: A line charge of 8 nC/m is located at $x = -1, y = 2$, a point charge of 6 mC at $y = -4$ and a surface charge of 30 pC/m^2 charge of 30 pC/m^2 at $z = 0$. If the potential at origin is 100 V , find the potential at $P(4, 1, 3)$. [2012 KARTHIK]

$$\text{Sol'n} \quad V_p = \frac{\theta}{4\pi\epsilon_0 r_p} + \frac{(-\rho_L)}{2\pi\epsilon_0} \ln(r_p)$$

$$+ \frac{(-\rho_S)}{2\epsilon_0} z_p + C$$

$$= \frac{8 \times 10^{-3}}{4\pi \times 10^{-9} \frac{r_p}{36\pi}} - \frac{8 \times 10^{-9}}{2\pi \times 10^{-9}} \ln(\frac{r_p}{r_0}) - \frac{\rho_S z_p}{2\epsilon_0} + C$$



$$\rho_S = 30 \text{ pC/m}^2$$

(Q) where, $V_p = \sqrt{(4-0)^2 + (1+4)^2 + (3-0)^2}$

$$= \sqrt{16+25+9}$$

$$= \sqrt{50}$$

$$\rho_p = \sqrt{(4+1)^2 + (1-2)^2 + (3-3)^2}$$

$$= \sqrt{25+1}$$

$$= \sqrt{26}$$

$$Z_p = 3$$

so, $V_p = \frac{54 \times 10^6}{\sqrt{50}} - 144 \ln(\sqrt{26}) - \frac{30 \times 10^{-12}}{2 \times 10^{-9}} \times 3 + C$

$$\text{or, } V_p = 7.64 \times 10^6 - 234.58 - 5.089 + C$$

$$\text{or, } V_p = 7639.760331 + C$$

Again,

$$V_0 = 100V$$

$$\text{or, } \frac{6 \times 10^{-3}}{4 \pi \times 10^{-9} r_0} - \frac{8 \times 10^{-9}}{2 \pi \times 10^{-9}} \ln(r_0) - \frac{30 \times 10^{-12}}{36 \pi} \cdot Z_0 + C = 100$$

$$\text{or, } \frac{564 \times 10^6}{r_0} - 144 \ln(r_0) - 15 \times 36 \pi \times 10^{-3} Z_0 + C = 100$$

$$\text{where, } r_0 = 4, \quad \rho_0 = \sqrt{(0+1)^2 + (0-2)^2 + (0-0)^2} = \sqrt{5}$$

$$Z_0 = 0$$

$$\text{or, } \frac{54 \times 10^6}{4} - 144 \ln(\sqrt{5}) - 0 + C = 100$$

$$\text{or, } 13.5 \times 10^6 - 115.88 + C = 100$$

$$V_p = -13499784.12$$

Now,

$$V_p = 7639760.331 - 13499784.12$$

$$= -586023.739$$

$$= -5.86 \times 10^6 \text{ V}$$

$$= -5860 \text{ kV.}$$

Qn: Given a surface charge density of 8 nC/m^2 on the plane $x=2$, a line charge density of 80 nC/m on the line $x=1, y=2$ and a $1 \mu\text{C}$ point charge at $P(-1, -1, 2)$, find V_{AB} for points A(3, 4, 0) and B(4, 0, 1). [Ans: $-V_{AB} = 193 \text{ V}$]

$$\begin{aligned} & \text{Scri.} \\ V_A &= \frac{\rho_L}{4\pi\epsilon_0 r} - \frac{\rho_S}{2\pi\epsilon_0} \ln(\rho_A) - \frac{\rho_S}{2\pi\epsilon_0} L_A + C \\ V_B &= \frac{\rho_L}{4\pi\epsilon_0 r_B} - \frac{\rho_L}{2\pi\epsilon_0} \ln(r_B) - \frac{\rho_S}{2\pi\epsilon_0} (L_B + C) \\ \therefore V_A - V_B &= \frac{\rho_L}{4\pi\epsilon_0} \left[\frac{1}{r_A} - \frac{1}{r_B} \right] + \frac{\rho_S}{2\pi\epsilon_0} \left[\ln\left(\frac{\rho_B}{\rho_A}\right) \right] + \frac{\rho_S}{2\pi\epsilon_0} [L_B - L_A] \\ &= 193 \text{ V} \end{aligned}$$

Qn: Let a uniform surface charge density of 8 nC/m^2 be present at the $z=0$ plane, a uniform line charge density of 8 nC/m be located at $x=0, z=4$ and a point charge of $2 \mu\text{C}$ be present at $P(2, 0, 0)$. If $V=0$ at $M(0, 1, 0)$ then find V at N(1, 2, 3).

Scri.

$$\begin{aligned} V_M &= 0 = \frac{\rho_L}{4\pi\epsilon_0 r_M} - \frac{\rho_L}{2\pi\epsilon_0} \ln(\rho_M) - \frac{\rho_S}{2\pi\epsilon_0} L_M + C \\ V_N &= \frac{\rho_L}{4\pi\epsilon_0 r_N} - \frac{\rho_L}{2\pi\epsilon_0} \ln(\rho_N) - \frac{\rho_S}{2\pi\epsilon_0} L_N + C = 1.98 \text{ kV} \end{aligned}$$

Potential Gradient

विद्युत काल्पनिक

Consider a region as shown in figure, when both \vec{E} and V change from point to point, we have

$$V = - \int_{\text{Initial}}^{\text{Final}} \vec{E} \cdot d\vec{l}$$

Let us assume the small incremental length Δl where \vec{E} is almost uniform & constant.

Then, $\Delta V = - \vec{E} \cdot \Delta l$

which is the incremental potential difference bet. "initial & final points of Δl ". If Δl makes an angle θ with \vec{E} as shown in figure, then

$$\Delta V = - E \cos \theta \Delta l$$

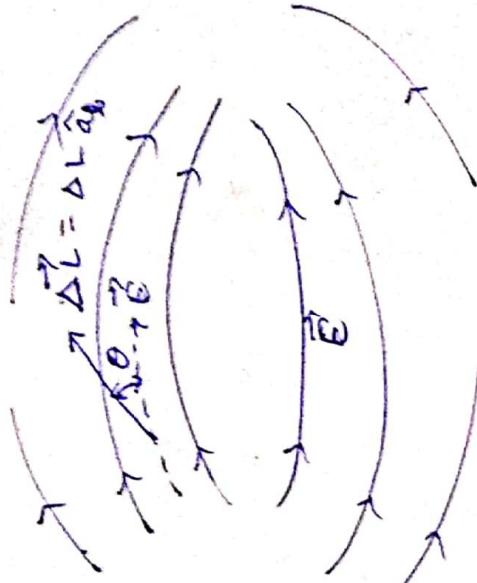
$$\text{or, } \frac{\Delta V}{\Delta l} = - E \cos \theta$$

Here, V may be interpreted as a function $V(x, y, z)$. If we assume a specified starting point or zero reference and then let our end point be (x, y, z) , then the result of the integration is a unique function of the end point (x, y, z) because \vec{E} is a conservative field. Using limit we get

$$\lim_{\Delta l \rightarrow 0} \frac{\Delta V}{\Delta l} = - E \cos \theta$$

$$\text{or, } \frac{dV}{dl} = - E \cos \theta$$

Here, the value of \vec{E} is a definite value at the point at which we need to calculate & is independent of the direction of $d\vec{l}$. The magnitude Δl is also constant, and the variable is \vec{E} only the unit vector showing the direction of $d\vec{l}$. From above expression, maximum increment of potential, ΔV_{\max} will occur when $\cos \theta = -1$, or $d\vec{l}$ points in the direction opposite to \vec{E} .



Initial & Final

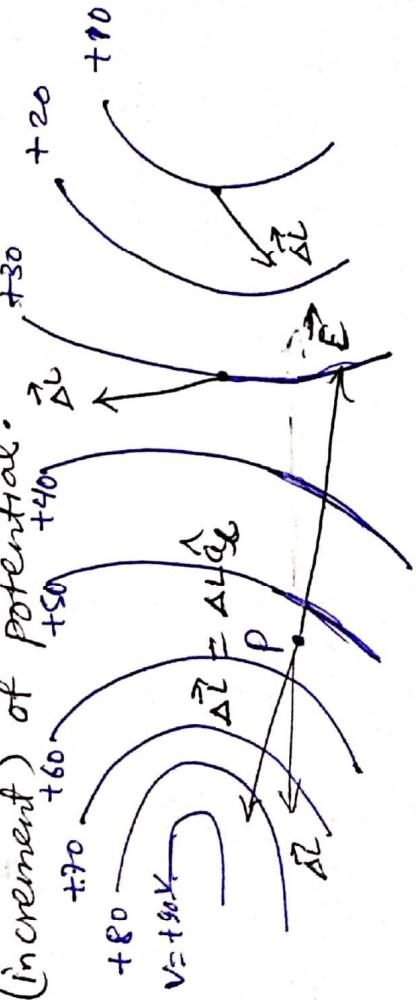
For this,

$$\frac{dV}{dr} \Big|_{\text{max}} = +E$$

This shows that,

- ① the magnitude of the electric field intensity is given by the maximum value of the rate of change of potential with distance.
- ② the direction of \vec{E} is exactly opposite to \vec{E} or the dir. of \vec{E} is opposite to the dir. in which the potential is increasing the most rapidly.

Hence, the dir. of \vec{E} is opposite of maximum positive change in (increment) of potential.



The above figure is showing the equipotential surfaces. At any point the \vec{E} field is normal to the equipotential surface passing through that point and is directed toward the more negative surfaces in which the potential is increasing the most rapidly.
Let us assume a point P as in figure and assume a small incremental distance Δr in various directions, hunting for that dir. in which the potential is increasing the most rapidly.
From the sketch, the dir. of max. increasing of potential appears to be left and slightly upward. It seems that the dir. of \vec{E} is opposite to the max. increment of potential.

Also, the dir. in which the potential is increasing the most rapidly is perpendicular to the equipotential surfaces.
so, if \vec{E} has dir. along equipotential surface then $\nabla V = 0$.

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$$\text{i.e. } \nabla V = -\vec{E} \cdot \hat{n} \vec{U} = 0$$

since, neither \vec{E} nor \hat{n} is zero, \vec{E} must be perpendicular to \hat{n} or perpendicular to the equipotential surfaces. Then, assuming \vec{U} was the unit vector along normal to the equipotential surface and directed toward the higher potentials.

$$\therefore \vec{E} = -\frac{dv}{dx} \hat{i} + \frac{dv}{dy} \hat{j}$$

which shows that the magnitude of \vec{E} is given by the max. rate of change of V and the direction of \vec{E} is normal to the equipotential surface (in the dir. of decreasing potential).

Since, $\frac{dv}{dx}$ occurs in \hat{i} occurs in \hat{i} , we may write as:

$$\frac{dv}{dx} / \max = \frac{dv}{dV} \quad \& \quad \vec{E} = -\frac{\partial V}{\partial \vec{U}} \hat{a}_V$$

The operation on V by which $-\vec{E}$ is obtained is known as gradient and the gradient of a scalar field T is defined as

$$\text{Gradient of } T = \text{grad } T = \frac{\partial T}{\partial \vec{U}} \hat{a}_U$$

where, \hat{a}_U is a unit vector normal to the equipotential surfaces, and that normal is chosen which points in the dir. of increasing values of T .

Now,

$$\boxed{\vec{E} = -\text{grad } V}$$

Since, V is a unique function of $x, y \& z$, we may take its total differential

$$dv = \frac{\partial V}{\partial x} dx + \frac{\partial V}{\partial y} dy + \frac{\partial V}{\partial z} dz$$

Also, we have,

$$dv = -\vec{E} \cdot \vec{U} = -E_x dx - E_y dy - E_z dz$$

(Q) Since both expressions are true for any dx, dy & dz

$$E_x = -\frac{\partial V}{\partial x}$$

$$E_y = -\frac{\partial V}{\partial y}$$

$$E_z = -\frac{\partial V}{\partial z}$$

$$\therefore \vec{E} = - \left(\frac{\partial V}{\partial x} \hat{i}_x + \frac{\partial V}{\partial y} \hat{i}_y + \frac{\partial V}{\partial z} \hat{i}_z \right)$$

$$\text{Since grad. } V = \frac{\partial V}{\partial x} \hat{i}_x + \frac{\partial V}{\partial y} \hat{i}_y + \frac{\partial V}{\partial z} \hat{i}_z = \nabla V$$

The gradient of any scalar gives the maximum rate of change of that scalar w.r.t. distance and also indicates where that max. rate of change w.r.t. distance is taking place. This is physical interpretation of gradient.

$$\boxed{\vec{E} = -\nabla V}$$

example

Assuming reference at infinity the potential at any point due to the field of point charge q is

$$V = \frac{q}{4\pi\epsilon_0 r}$$

Now, $\vec{E} = -\nabla V$
 $= -\frac{\partial V}{\partial r} \hat{i}_r \quad [\because \vec{E} \text{ is only function of } r]$

$$\begin{aligned} &= -\frac{\partial}{\partial r} \left(\frac{q}{4\pi\epsilon_0 r} \right) \hat{i}_r \\ &= \frac{q}{4\pi\epsilon_0 r^2} \hat{i}_r \end{aligned}$$

$$\therefore \boxed{\vec{E} = \frac{q}{4\pi\epsilon_0 r^2} \hat{i}_r}$$

Sol. 1: A potential field is given as $V = 100 e^{-5x} \sin y \cos 4z$.
 Let point P $(0.1, \frac{\pi}{12}, \frac{\pi}{24})$ be located at a conductor-free space boundary. At point P, find the magnitude of \vec{E} .

$$\text{Sol. 1} \quad \text{④ } V \text{ at } P(0.1, \frac{\pi}{12}, \frac{\pi}{24}) = V_p = 100 e^{-0.05} \sin\left(\frac{\pi x}{12}\right) \cdot \cos\left(4 \times \frac{\pi z}{24}\right)$$

$$= 37.142 \text{ V}$$

$$\text{⑤ } \vec{E} = -\nabla V = 500 e^{-5x} \sin y \cos 4z \hat{a}_x - 300 e^{-5x} \cos y \cos 4z \hat{a}_y + 400 e^{-5x} \sin y \cdot \sin 4z \hat{a}_z$$

Substituting co-ordinates of P in \vec{E} , we get

$$\vec{E} \text{ at } P = \vec{E}_P = 185.711 \hat{a}_x + 111.427 \hat{a}_y + 85.226 \hat{a}_z \text{ V/m}$$

- Ques: Within the cylinder $\rho = 2$, $0 < z < 1$ the potential given by: $V = 100 + 50\rho + 150 \sin \theta$ find:
 ① Electric field Intensity (\vec{E}) at $P(1, 60^\circ, 0.5)$ in free space
 ② Potential gradient $\left(\frac{dV}{dr}\right)$
 ③ Volume Charge Density at $P(1, 60^\circ, 0.5)$ in free space
 ④ How much charge lies within the cylinder?
Sol. 2

Given, potential within the cylinder is

$$V = 100 + 50\rho + 150 \sin \theta$$

$$\text{① } \vec{E} \text{ at } P(1, 60^\circ, 0.5) \text{ is}$$

$$\vec{E}_P = -\nabla V = -\frac{\partial V}{\partial \rho} \hat{a}_\rho - \frac{1}{\rho} \frac{\partial V}{\partial \theta} \hat{a}_\theta - \frac{\partial V}{\partial z} \hat{a}_z$$

$$= [E_{\rho} - 150 \sin \theta] \hat{a}_\rho - \frac{1}{\rho} [150 \rho \cos \theta] \hat{a}_\theta \hat{a}_z$$

$$= -[50 + 150 \sin \theta] \hat{a}_\rho - 150 \cos \theta \hat{a}_z$$

(b) Substituting value of $\rho(1, 60^\circ, 0, \phi)$

$$\vec{E}_p = -[50 + 150 \sin 60^\circ] \hat{a}_p - 150 \cos 60^\circ \hat{a}_\theta \\ = -199.9 \hat{a}_p - 75 \hat{a}_\theta \text{ V/m}$$

Again,

④ Potential Gradient $\left(\frac{dV}{ds}\right) = +\sqrt{(\vec{E}^2)} = +\sqrt{(-199.9)^2 + (-75)^2}$
 $= 2104.90 \text{ V/m}$

Also,

⑤ $P_V = \nabla \cdot \vec{D}_p$ [From Maxwell's first Equation]
 $= \epsilon_0 \nabla \cdot \vec{E}_p$
 $= \epsilon_0 \left[\frac{1}{r} \frac{\partial}{\partial r} \{q(-50 - 150 \sin \phi)\} + \frac{1}{r} \frac{\partial}{\partial \phi} \{150 \cos \phi\} \right]$
 $= \epsilon_0 \cdot [(-50 + \frac{1}{r} 150 \sin \phi + \frac{1}{r} 150 \sin \phi)]$
 $= -\frac{50}{r} \epsilon_0$
 Substituting $\rho(1, 60^\circ, 0, \phi)$

$$P_V = -\frac{50}{1} \times 8.85 \times 10^{-12} \\ = -442.5 \text{ PC/m}^3.$$

⑥ For the cylinder, $\rho = 2$, $0 < z < 4$, the charge within the cylinder will be

$$Q = \int_{\text{vol.}} P_V dv = \int_{\rho=0}^{2} \int_{z=0}^{2\pi} \int_{r=0}^1 -\frac{50}{r} \epsilon_0 \vec{S} d\phi dr dz$$

104) $\oint \vec{B} \cdot d\vec{s} = \int_{P=0}^2 \int_{\phi=0}^{2\pi} (-50 \epsilon_0) d\rho d\phi$

$$\rho = 0 \quad \phi = 0$$

$$= \int_{P=0}^2 -50 \epsilon_0 \cdot 2\pi d\rho$$

$$= -50 \times 2\pi \epsilon_0 \times 2$$

$$= -2.78 \text{ nC} \times 2$$

$$= -5.56 \text{ nC}$$

- Qn: Given the potential field $V = \frac{100x z}{x^2 + 4}$ Volts in free space:
- (a) Find \vec{B} at the surface $z=0$
 - (b) Show that the $z=0$ surface is an equipotential surface
 - (c) Assume that the $z=0$ surface is a conductor and find the total charge on that portion of the conductor defined by $0 < x < 2$, $-3 \leq y \leq 0$. [2019 Chairita]

Sol: Given the potential field

$$V = \frac{100x z}{x^2 + 4} \text{ Volts.}$$

$$\begin{aligned} \text{(a)} \quad \vec{E} &= -\nabla V \\ &= -\left(\frac{\partial}{\partial x} \hat{A}_x + \frac{\partial}{\partial y} \hat{A}_y + \frac{\partial}{\partial z} \hat{A}_z\right) \left(\frac{100x z}{x^2 + 4}\right) = \frac{-100x z}{x^2 + 4} \hat{A}_x \text{ V/m} \end{aligned}$$

$$\text{&} \quad \vec{D} = \epsilon_0 \vec{E} \quad (\text{Put } z=0) = -\frac{100 \epsilon_0 x}{x^2 + 4} \hat{A}_x \text{ C/m}^2.$$

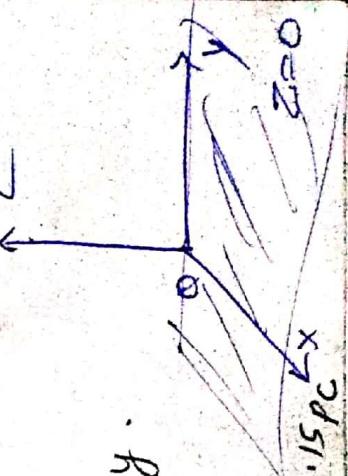
- (b) To show $z=0$ surface is an equipotential surface

$$V = \frac{100x z}{x^2 + 4} = 0 \text{ V}$$

since, V is constant for any value of x & y .

- (c) Total charge within that conductor is

$$\Phi = \oint \vec{B} \cdot d\vec{s} = \int_{y=0}^{y=2} \int_{x=0}^{x=2} (-50 \epsilon_0) dz = -9.20 \cdot 15 \text{ pC} = -9.20 \cdot 15 \text{ pC}$$



$$= -g \cdot 20.15 \text{ pc}$$

$$= -\frac{300 \epsilon_0}{2} \cdot \ln(2x^2 + 4) \Big|_0^2 = -150 \epsilon_0 \times 0.693$$

$$x=0$$

$$= - \int_0^2 \frac{\log x}{x^2+4} (x+3) dx$$

$$x=0, y=-3.$$

$$= \int_0^2 \frac{-\log x}{x^2+4} dy$$

$$\Phi = \int_0^2 \vec{B} \cdot d\vec{s} = \left(-100 \pi x \cdot \hat{i}_2 \right) \cdot \left(\sin y \hat{i}_2 \right)$$

$$\vec{B} = -\frac{100 \pi}{x^2+4} \hat{j}_2 \quad c/m^2$$

$$-i \vec{E} = -\frac{100 \pi}{x^2+4} \hat{j}_2 \quad V/m$$

$$\text{Put } z=0$$

$$= - \int_{2001}^{(x^2+4)} \frac{\frac{1}{2}x}{(x^2+4)^2} - x \cdot 2x \cdot \int_{2001}^{(x^2+4)} \frac{x}{e} dx$$

$$\textcircled{2} \quad \left[\frac{3}{8} \left(\frac{1}{2}x^2 \right) \frac{ze}{e} + \left(\frac{1}{8} \left(\frac{1}{2}x^2 \right) \right) \frac{ze}{e} \right] = \frac{3}{8} \left(\frac{1}{2}x^2 \right) \frac{ze}{e} + \left(\frac{1}{8} \left(\frac{1}{2}x^2 \right) \right) \frac{ze}{e}$$

$$\int \frac{x}{x^2+a^2} dx = \frac{1}{2} \ln(x^2+a^2) + C$$

$$\frac{d(\mu_A)}{dx} = \frac{\mu_A}{x^2} - \frac{\mu_B}{x^2}$$

$$\int_0^{\frac{\pi}{2}} \sin^n x dx = \frac{\sqrt{n}}{2} \frac{\Gamma\left(\frac{n+1}{2}\right)}{\Gamma\left(\frac{n}{2} + 1\right)}$$

Integrals Using Beta Gamma function

$$\int_0^{\frac{\pi}{2}} \sin\theta \cdot \cos^q \theta d\theta = \frac{1}{2} \beta\left(\frac{p+1}{2}, \frac{q+1}{2}\right)$$

$$\beta(m,n) = \frac{\Gamma(m) \cdot \Gamma(n)}{\Gamma(m+n)}$$

$$\frac{1}{\sqrt{m-1+1}} = \sqrt{m-1} \quad \text{and} \quad \frac{1}{\sqrt{m-1}} = \sqrt{m-1}$$

$$\sqrt{1 - (1 - c)^n} = \sqrt{n}c$$

$$\sqrt{\frac{5}{2}} = \sqrt{\left(\frac{3}{2} + 1\right)} = \sqrt{\frac{3}{2}}$$

$$= \frac{3}{2} \sqrt{\left(\frac{1}{2}\right)^2 + \left(\frac{1}{2}\right)^2} = \frac{3}{2} \times \frac{1}{2} \times \sqrt{\frac{1}{2}} = \frac{3}{4} \sqrt{\frac{1}{2}} = \frac{3}{4} \sqrt{\frac{2}{4}} = \frac{3}{4} \times \frac{1}{2} \times \sqrt{2}$$

$$\sqrt{4} = 2$$

(Q-825) Qn: For a potential field $V = r^2 z^2 \sin\phi$ at point $P(1, 45^\circ, 1)$ in cylindrical co-ordinate system. Determine (a) Potential V
(b) Electric field \vec{E} . (c) Electric flux density, \vec{D} (d) Volume charge density ρ_v and (e) unit vector in direction of \vec{E} .

[2068 shown]

Qn: Given the potential $V = \frac{10}{r^2} \sin\phi \cos\theta$; find the electric flux density \vec{D} at $(2, \frac{\pi}{2}, 0)$. [2073 Chaitra]

Electric Dipole

An electric dipole is formed when two point charges of equal magnitude but opposite sign are separated by a small distance. The distance bet' two charges is very small compared to the distance to the point at which we want to know the electric and potential fields.

Consider an electric dipole of magnitude Q is placed on the Z -axis.

The +ve charge $+Q$ is placed at $(0, 0, \frac{d}{2})$ and -ve charge $-Q$ is placed at $(0, 0, -\frac{d}{2})$. i.e. two charges are separated by d distance as shown in figure.

Let us take the point P where we need to find the electric field intensity due to the electric dipole.

Let the point P be described in spherical co-ordinate system as $P(r, \theta, \phi)$

Now, the potential at point P due to field of dipole, assuming reference at infinity is given by

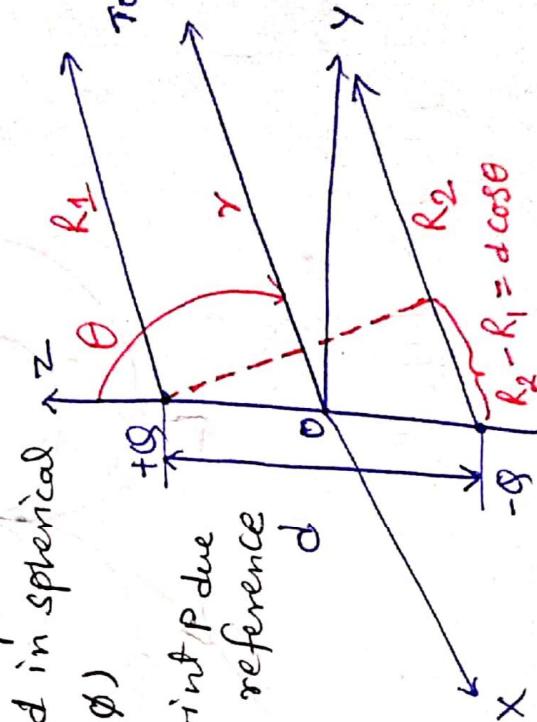
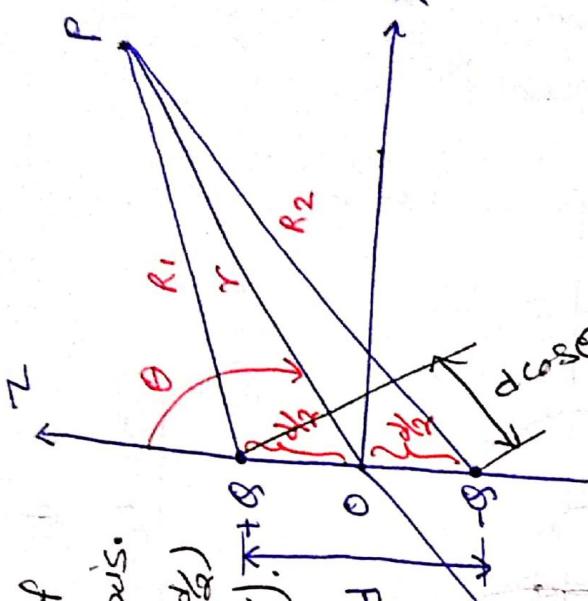
$$V = \frac{Q}{4\pi\epsilon_0 R_1} + \frac{(-Q)}{4\pi\epsilon_0 R_2}$$

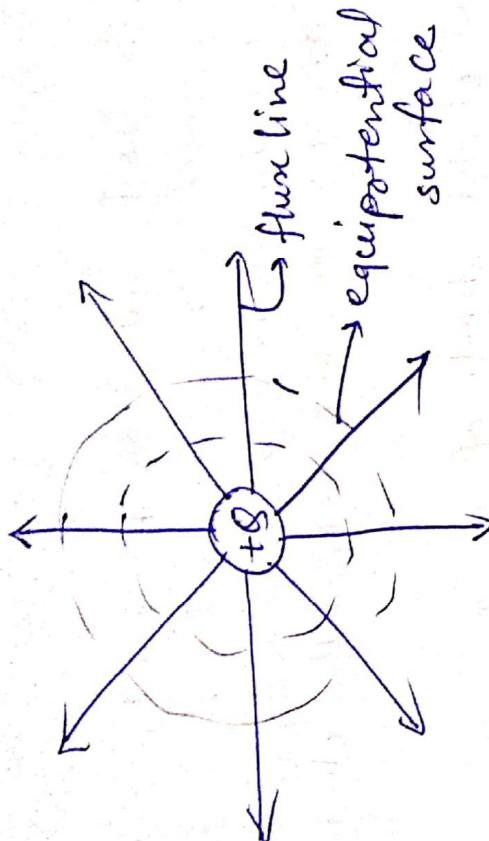
$$= \frac{Q}{4\pi\epsilon_0} \left[\frac{1}{R_1} - \frac{1}{R_2} \right]$$

$$= \frac{Q}{4\pi\epsilon_0} \left[\frac{R_2 - R_1}{R_1 R_2} \right]$$

where, R_1 = distance bet' P & $+Q$.

& R_2 = distance bet' P & $-Q$

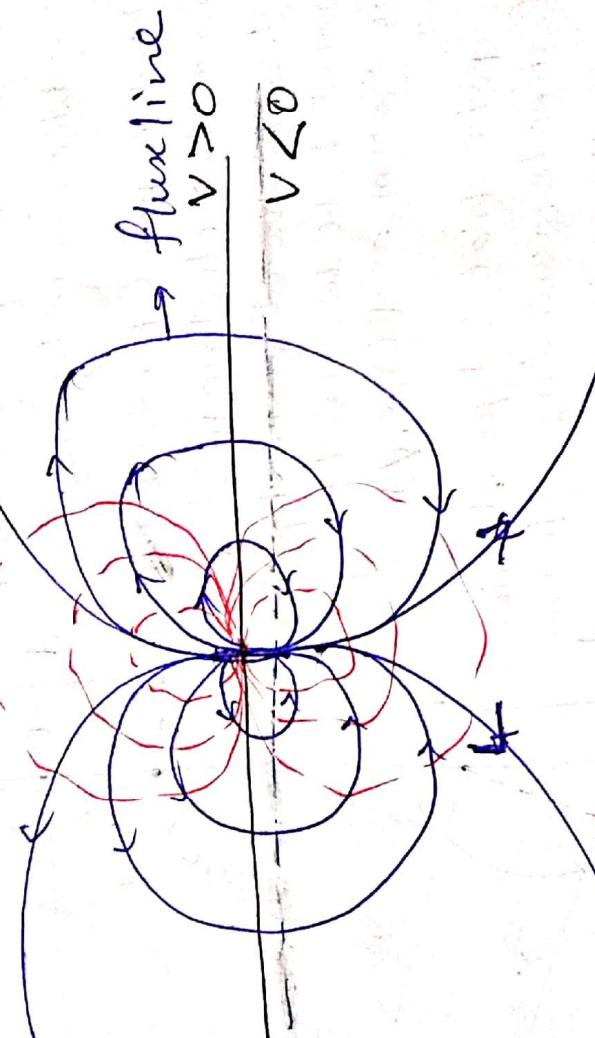




Point charge

Equipotential Surface

flux line



Electric Dipole

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If point P is very far and $r \gg d$ then

$$R_2 = R_1 = r, \quad R_2 - R_1 \approx d \cos\theta \text{ and } R_2 \cdot R_1 \approx r^2$$

$$\text{So, } V = \frac{Q}{4\pi\epsilon_0} \left[\frac{R_2 - R_1}{r^2} \right] = \frac{Q}{4\pi\epsilon_0} \cdot \frac{d \cos\theta}{r^2}$$

Now, since, $d \cos\theta = \vec{d} \cdot \hat{a}_x$, where $\vec{d} = \hat{d} \hat{a}_z$, we define

$$\vec{P} = Q \vec{d}$$

where \vec{P} = the dipole moment, directed from $-Q$ to $+Q$.

$$\text{Then, } V = \frac{Q}{4\pi\epsilon_0} \cdot \frac{d \cos\theta}{r^2} = \frac{Q \cdot \vec{d} \cdot \hat{a}_x}{4\pi\epsilon_0 r^2} = \frac{\vec{P} \cdot \hat{a}_x}{4\pi\epsilon_0 r^2}$$

If the dipole center is not at the origin but at \vec{r}'

Then,

$$V(\vec{r}) = \frac{\vec{P} \cdot (\vec{r} - \vec{r}')}{4\pi\epsilon_0 | \vec{r} - \vec{r}' |^3}$$

Again, where, \vec{r} locates the field point & \vec{r}' locates the center of dipole.

The electric field due to the dipole with center at the origin is given by

$$\begin{aligned} \vec{E} &= -\nabla V = - \left[\frac{\partial V}{\partial r} \hat{a}_r + \frac{1}{r} \frac{\partial V}{\partial \theta} \hat{a}_\theta + \frac{1}{r \sin\theta} \frac{\partial V}{\partial \phi} \hat{a}_\phi \right] \\ &= \frac{Q d \cos\theta}{2\pi\epsilon_0 r^3} \hat{a}_r + \frac{Q d \sin\theta}{4\pi\epsilon_0 r^3} \hat{a}_\theta \\ \therefore \vec{E} &= \frac{p}{4\pi\epsilon_0 r^3} [Q \cos\theta \hat{a}_r + Q \sin\theta \hat{a}_\theta] \text{ V/m.} \end{aligned}$$

This is the electric field intensity due to the dipole.

$$\text{where, } p = |\vec{P}| = Qd$$

Qn: A dipole for which $\vec{P} = 3\hat{a}_x - 5\hat{a}_y + 10\hat{a}_z \text{ nC.m}$ is located at origin. Find \vec{E} at point $(1, 2, -4)$. Find \vec{E} at P. [2012 Chaitra]

Soln.

$$\text{Given, } \vec{P} = 3\hat{a}_x - 5\hat{a}_y + 10\hat{a}_z \text{ nC.m.}$$

The electric field intensity due to the dipole is

$$\vec{E} = \frac{\mu_0}{4\pi\epsilon_0 r^3} [2\cos\theta\hat{a}_r + \sin\theta\hat{a}_\theta]$$

Since, \vec{E} is in spherical coordinate system, we need to change $P(1, 2, -4)$ to spherical coordinate system.

$$r = \sqrt{1^2 + 2^2 + (-4)^2} = \sqrt{21}$$

$$\theta = \tan^{-1}\left(\frac{\sqrt{21}}{2}\right) = \tan^{-1}\left(\frac{\sqrt{5}}{4}\right) = 180^\circ - 29.2^\circ = 150.79^\circ$$

$$\phi = \tan^{-1}\left(\frac{y}{x}\right) = \tan^{-1}\left(\frac{-4}{2}\right) = 63.43^\circ$$

Now, $|P| = p = \sqrt{3^2 + (-5)^2 + 10^2} = 11.575 \text{ nC.m.}$

$$\vec{E} = \frac{11.575 \times 10^{-9}}{4\pi \times 10^{-9} \times (21)^{3/2}} \left[2\cos(150.79^\circ)\hat{a}_r + \sin(150.79^\circ)\hat{a}_\theta \right]$$

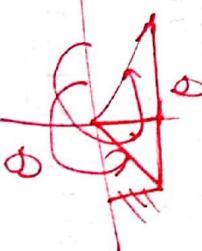
$$= 1.0825 \left[2 \cdot 7457 \hat{a}_r + (+0.488)\hat{a}_\theta \right]$$

$$= [-1.889 \hat{a}_r + 0.528 \hat{a}_\theta] \text{ V/m}$$

$$= 180^\circ + 23.578^\circ \text{ or } 860^\circ - 23.578^\circ$$

$$\theta = \sin^{-1} \left(-\frac{3}{5} \right)$$

$\theta = 3.528^\circ$



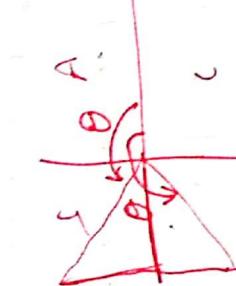
$$\theta = \cos^{-1} \left(-\frac{3}{5} \right)$$

$\theta = 336.42^\circ$

$$= 180^\circ - 69.38^\circ \text{ or } 180^\circ + 69.38^\circ$$



$$\Rightarrow 11^2 - 6^2 = 8$$

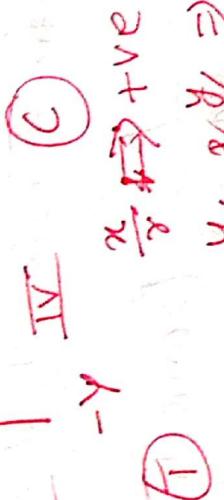


$$\text{eg: } \cos \theta = -\frac{5}{13}$$

$$\frac{dy}{dx} < 0$$

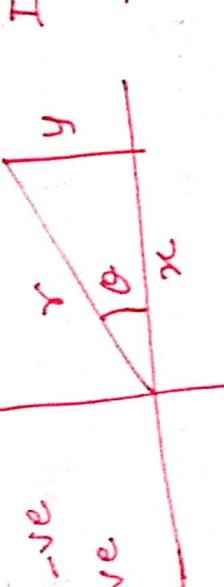
$$\frac{dy}{dx} > 0 \Rightarrow \text{increasing}$$

$$\{ 360^\circ - \theta \}$$



$$\frac{dy}{dx} < 0 \Rightarrow \text{decreasing}$$

sharper (x is always +ve)



sharper \Rightarrow +ve

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sharper \Rightarrow +ve

(S)

II

sharper \Rightarrow +ve



sharper \Rightarrow +ve

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sharper \Rightarrow +ve

C

sharper \Rightarrow +ve

D

sharper \Rightarrow +ve

E

sharper \Rightarrow +ve

F

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Qn: A dipole of moment $\vec{p} = 6\hat{a}_z$ n.C.m is located at the origin in freespace. ① Find V at P(r=4, $\theta=20^\circ$, $\phi=0^\circ$) ② Find \vec{E} at P.

Sol:

$$\text{Given, } \vec{p} = 6\hat{a}_z$$

Converting it to spherical co-ordinate

$$\begin{aligned}\vec{p}_{\text{sph.}} &= 6\cos\theta\hat{a}_r + 6(\sin\theta)\hat{a}_\theta \\ &= [6\cos\theta\hat{a}_r - 6\sin\theta\hat{a}_\theta] \text{ n.C.m}\end{aligned}$$

$$@ \text{ so, } V = \frac{\vec{p} \cdot \hat{a}_r}{4\pi\epsilon_0 r^2}$$

$$= \frac{[6\cos\theta\hat{a}_r - 6\sin\theta\hat{a}_\theta] \cdot \hat{a}_r}{4\pi\epsilon_0 r^2}$$

$$= \frac{6\cos\theta}{4\pi\epsilon_0 r^2}$$

Now,

at P ($r=4$, $\theta=20^\circ$, $\phi=0^\circ$)

$$V_p = \frac{6\cos 20^\circ \times 10^{-9}}{4\pi \times 10^{-9} \times 4^2 \times 36\pi} = 3.17 \text{ V}$$

Again,

$$② \vec{E} \text{ at P} = \vec{E}_p = \frac{\vec{p}}{4\pi\epsilon_0 r^2} [2\cos\theta\hat{a}_r + \sin\theta\hat{a}_\theta]$$

$$= \frac{6 \times 10^{-9}}{4\pi \times 10^{-9} \times 4^2} [2\cos 20^\circ \hat{a}_r + \sin 20^\circ \hat{a}_\theta]$$

$$= [1.585 \hat{a}_r + 0.288 \hat{a}_\theta] \text{ V/m.}$$

(Q9) Qn: A dipole having a moment $\vec{P} = 3\hat{a}_x - 5\hat{a}_y + 10\hat{a}_z$ nC.m is located at Q(1, 2, -4) in free space. Find V at P(2, 3, 4) ~~at P~~

Sol. Given,

$$\vec{P} = 3\hat{a}_x - 5\hat{a}_y + 10\hat{a}_z \text{ nC.m at point Q(1, 2, -4)}$$

We have,

$$V = \frac{\vec{P} \cdot (\vec{r} - \vec{r}')}{4\pi\epsilon_0 |\vec{r} - \vec{r}'|^3}$$

$$\text{where, } \vec{r}' = \hat{a}_x + 2\hat{a}_y - 4\hat{a}_z$$

$$\vec{r} = 2\hat{a}_x + 3\hat{a}_y + 4\hat{a}_z$$

$$\text{so, } \vec{r} - \vec{r}' = -\hat{a}_x + \hat{a}_y + 8\hat{a}_z$$

$$\therefore |\vec{r} - \vec{r}'| = \sqrt{1+1+64} = \sqrt{66}$$

$$\text{Then, } V_p = \frac{(3\hat{a}_x - 5\hat{a}_y + 10\hat{a}_z) \cdot (-\hat{a}_x + \hat{a}_y + 8\hat{a}_z)}{4\pi \times 10^{-9} \times \frac{36\pi}{(66)^{3/2}}} \times 10^{-9}$$

$$= \frac{(3 - 5 + 80) \times 9}{(66)^{3/2}}$$

$$= 1.31 \text{ V}$$

Energy Density in Electrostatic field.

To determine the energy present in a system of charges, we must find the work done by an external source in assembling the charges.

Let us consider an empty universe and position the point charges brought from infinity. For initial condition, there is no charge in universe so, the work done in bringing point charge Q_1 from infinity to that universe is zero. Then, the work done in bringing & positioning charge Q_2 from outside into that universe requires an amount of work against the field due to charge Q_1 which is given by $V_{2,1}$. Q_2 where, $V_{2,1}$ is the potential at point P_2 due to the charge Q_1 at point P_1 .

$$\text{Work done in positioning } Q_2 = Q_2 V_{2,1}$$
$$\text{Work done in positioning } Q_3 = Q_3 V_{3,1} + Q_3 V_{3,2}$$
$$\text{Work done in positioning } Q_4 = Q_4 V_{4,1} + Q_4 V_{4,2} + Q_4 V_{4,3}$$

So, total work done to position the N charges = potential energy of field = $W_E = Q_2 V_{2,1} + Q_3 V_{3,1} + Q_3 V_{3,2} + Q_4 V_{4,1} + Q_4 V_{4,2} + \dots + Q_N V_{N,1} + Q_N V_{N,2} + \dots + Q_N V_{N,N-1}$

$$\therefore W_E = Q_2 V_{2,1} + Q_3 (V_{3,1} + V_{3,2}) + \dots + Q_N (V_{N,1} + \dots + V_{N,N-1})$$

(ii) Also, we have,

$$Q_3 V_{3,1} = Q_2 \cdot \frac{Q_1}{4\pi\epsilon_0 R_{13}} = \frac{Q_1 Q_3}{4\pi\epsilon_0 R_{13}}$$

where, R_{13} & R_{31} each represent the scalar distance bet. Q_1 & Q_3 .

Then, the total workdone in positioning different charges in reverse order is

$$WE = Q_1 V_{1,2} + Q_1 V_{1,3} + Q_2 V_{2,3} + Q_1 V_{1,4} + \dots + V_{1,N}$$

Adding the two energy expressions.

$$\begin{aligned} 2WE &= Q_1 (V_{1,2} + V_{1,3} + V_{1,4} + \dots) + Q_2 (V_{2,1} + V_{2,3} + V_{2,4} + \dots) \\ &\quad - \dots + Q_{N-1} (V_{1,N} + V_{2,N}) + \dots \end{aligned}$$

Each sum of potentials in parenthesis is the combined potential due to all the charges except for the charge at the point where this combined potential is being found i.e. $V_{1,2} + V_{1,3} + V_{1,4} + \dots + V_{1,N} = V_1$

$$V_{2,1} + V_{2,3} + V_{2,4} + \dots + V_{2,N} = V_2$$

— — — — —

Therefore,

$$WE = \frac{1}{2} (Q_1 V_1 + Q_2 V_2 + Q_3 V_3 + \dots)$$

$$\therefore WE = \frac{1}{2} \sum_{m=1}^{m=N} Q_m V_m \quad \text{For discrete charges.}$$

In order to obtain an expression for the energy stored in a region of continuous charge distribution, each charge is replaced by $\int_V dv$ and the summation becomes an integral.

$$W_E = \frac{1}{2} \cdot \int_{\text{vol.}} V \cdot V \, d\omega$$

From Maxwell's first equation

$$\rho_V = \nabla \cdot \vec{B}$$

So,

$$W_E = \frac{1}{2} \int_{\text{vol.}} (\nabla \cdot \vec{B}) V \, d\omega$$

Again, from vector identity

$$\nabla \cdot (\nabla \vec{B}) = V(\nabla \cdot \vec{B})$$

$$(\nabla \cdot \vec{B}) V = \nabla (V \cdot \vec{B}) - \vec{B} \cdot (\nabla V)$$

$$\text{So, } W_E = \frac{1}{2} \int_{\text{vol.}} [V(\nabla \cdot \vec{B}) - \vec{B} \cdot (\nabla V)] \, d\omega$$

from divergence theorem.

$$\int_{\text{vol.}} (\nabla \cdot \vec{B}) \, d\omega = \oint_S \vec{B} \cdot d\vec{s}$$

$$\text{So, } \oint_S V \cdot d\vec{s} = \int_{\text{vol.}} \nabla \cdot (V \vec{B}) \, d\omega.$$

$$\therefore W_E = \frac{1}{2} \oint_S (V \vec{B}) \cdot d\vec{s} - \frac{1}{2} \int_{\text{vol.}} \vec{B} \cdot (\nabla V) \, d\omega.$$

Here, in $\frac{1}{2} \oint_S V \cdot d\vec{s}$, \vec{B} varies with $\frac{1}{S_2}$ and $d\vec{s}$ varies with $\frac{1}{S_2}$ ~~and~~ V varies with $\frac{1}{S_2}$. So, the effect of variation with $\frac{1}{S_2}$ is cancelled but effect due to $\frac{1}{S_2}$ is remained & if $r \rightarrow \infty$ then $\frac{1}{S_2} \rightarrow 0$

So, $\frac{1}{2} \oint_S V \vec{B} \cdot d\vec{s} = 0$ as we are bringing the charges from infinity to an empty universe

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$$\therefore W_E = -\frac{1}{2} \int_{\text{vol.}} \vec{B} \cdot (\nabla V) d\sigma$$

Again, from potential gradient, we have

$$\vec{E} = -\nabla V$$

The W_E becomes,

$$\begin{aligned} W_E &= \frac{1}{2} \int_{\text{vol.}} \vec{B} \cdot (\vec{E}) d\sigma \\ &= \frac{1}{2} \int_{\text{vol.}} (\epsilon_0 \vec{E}) \cdot \vec{E} d\sigma \end{aligned}$$

$$\boxed{\therefore W_E = \frac{1}{2} \int_{\text{vol.}} \epsilon_0 E^2 d\sigma}$$

$$\text{Again, from, } W_E = \frac{1}{2} \int_{\text{vol.}} (\vec{D} \cdot \vec{E}) d\sigma$$

We can use, the differential form as:

$$dW_E = \frac{1}{2} \vec{D} \cdot \vec{E} d\sigma$$

$$\boxed{\text{or, } \frac{dW_E}{d\sigma} = \frac{1}{2} \vec{D} \cdot \vec{E}} - \text{This is called Energy density in electrostatic field.}$$

It has the dimension of Energy density or Joules per cubic meter. If we integrate this energy over the entire field containing volume, the result is the total energy present in that volume.

$$\text{Also, } W_E = \frac{dW_E}{d\sigma} = \frac{1}{2} \vec{D} \cdot \vec{E} = \frac{1}{2} \epsilon_0 E^2 = \frac{D^2}{2\epsilon_0}$$

$$\star W_E = \int_{\text{vol.}} \epsilon_0 E^2 d\sigma$$

density

Energy stored in the electrostatic field of section of a coaxial cable or capacitor of length L .

$$\text{We have, } \vec{E} = \frac{\alpha s}{\epsilon_0 p} \hat{a}_p$$

$$2\pi \vec{D} = \frac{\alpha s}{p} \hat{a}_p$$

where, s_s = surface charge density on the inner conductor.

Thus,

$$\begin{aligned} W_E &= \frac{1}{2} \int_{\text{Vol.}} \vec{D} \cdot \vec{E} \, dV = \frac{1}{2} \int_{\text{Vol.}} \epsilon_0 E^2 \, dV \\ &= \frac{1}{2} \int_0^L \int_0^{2\pi} \int_0^\pi \epsilon_0 \frac{\alpha^2 s_s^2}{\epsilon_0 p^2} p \, dp \, d\theta \, d\phi \\ &= \frac{\pi L a^2 s_s^2}{\epsilon_0} \ln\left(\frac{b}{a}\right) \end{aligned}$$

If we choose the outer conductor as zero potential reference then the potential of the inner conductor is

$$V_a = - \int_b^a \frac{q}{\epsilon_0 p} \, dp = - \int_b^a \frac{q s_s}{\epsilon_0 p} \, dp = \frac{q s_s}{\epsilon_0} \ln\left(\frac{b}{a}\right)$$

Qn: An electric dipole located at the origin in free space has a moment $\vec{P} = 3\hat{a}_x - 2\hat{a}_y + \hat{a}_z \text{ n C} \cdot \text{m}$ @ Find value

P_A (2,3,4) ⑥ Find V at r = 2.5, θ = 30°; φ = 40°.

Ans: ⑧ 230 V, 1.973 V

Qn: Find the energy stored in free space for the region $0 < \rho < a$, $0 < \phi < \pi$, $0 < z < 2$, given the potential field $V = V_0 (\rho/a) v_1 + V_0 (\rho/a) \cos^2 \theta V_1$

Sol:

① we have, $V = V_0 (\rho/a)$

$$\vec{E} = -\nabla V = -\left[\frac{\partial V}{\partial \rho} \hat{\rho} \right] = \frac{\partial V}{\partial \rho} \left(\frac{V_0 \rho}{a} \right) \hat{\rho} = -\frac{V_0}{a} \hat{\rho}$$

$$\therefore |\vec{E}| = E = \frac{V_0}{a}$$

Now, we have, the energy stored is given by

$$W_E = \frac{1}{2} \int_{\text{vol.}} \epsilon_0 E^2 dV$$

$$= \frac{1}{2} \int_{\text{vol.}} \epsilon_0 \left(\frac{V_0}{a} \right)^2 dV$$

$$= \frac{1}{2} \frac{\epsilon_0 V_0^2}{a^2} \int_{\text{vol.}} d\rho d\phi dz$$

$$= \frac{\epsilon_0 V_0^2}{2a^2} \int_0^a \int_0^\pi \int_0^2 \rho d\rho d\phi dz$$

$$\begin{aligned} &\quad \rho=0 \quad \phi=0 \quad z=0 \\ &\quad \rho=a \quad \phi=\pi \quad z=2 \end{aligned}$$

$$= \frac{\epsilon_0 V_0^2}{2a^2} \cdot \int_0^a \rho (\pi - 0) \cdot (2 - 0) d\rho$$

$$= \frac{2\pi \epsilon_0 V_0^2}{2a^2} \cdot \left. \frac{\rho^2}{2} \right|_0^a$$

$$= \frac{\epsilon_0 V_0^2 \pi}{a^2} \cdot \frac{a^2}{2}$$

$$= \frac{\pi \epsilon_0 V_0^2}{2} = 1.571 \epsilon_0 V_0^2 \pi //$$

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Again, $V = V_0 \left(\frac{r}{a}\right) \cdot \cos^2 \phi$

$$\text{⑥ } \vec{\epsilon} = -\nabla V = -\left[\frac{\partial}{\partial r} \left(\frac{V_0 r \cos^2 \phi}{a} \right) \hat{a}_r + \frac{1}{r} \frac{\partial}{\partial \phi} \left(\frac{V_0 r \cos^2 \phi}{a} \right) \hat{a}_\phi \right]$$

$$= -\frac{V_0}{a} (\cos^2 \phi \hat{a}_r - 2 \sin \phi \cos \phi \hat{a}_\phi)$$

$$\therefore E = |\vec{E}| = \frac{V_0}{a} \sqrt{(\cos^2 \phi)^2 + (-2 \sin \phi \cos \phi)^2}$$

$$= \frac{V_0}{a} \cos \phi \sqrt{\cos^2 \phi + 4 \sin^2 \phi}$$

$$= \frac{V_0}{a} \cos \phi \sqrt{1 + 3 \sin^2 \phi}$$

Now,

$$\begin{aligned} W_E &= \frac{\epsilon_0}{2} \int_{\text{vol.}} E^2 dV \\ &= \frac{\epsilon_0}{2} \int_0^a \int_0^\pi \int_0^{2\pi} \frac{V_0^2}{a^2} \cos^2 \phi (1 + 3 \sin^2 \phi) \rho d\rho d\phi d\theta \\ &= \frac{\epsilon_0 V_0^2}{2 a^2} \left[\frac{g^2}{2} \right]_0^a \left[\frac{1}{2} (\phi + \frac{\sin 2\phi}{2}) + \frac{3}{8} (\phi - \frac{\sin 4\phi}{4}) \right]_0^{2\pi} \end{aligned}$$

$$= \frac{\epsilon_0 V_0^2}{2 a^2} \times \frac{a^2}{2} \times 2 \cdot 24 \theta \times \frac{1}{2}$$

$$= 1.374 \epsilon_0 V_0^2 J.$$

Qn: Find the energy stored in free space for the region
 $2\text{ mm} < r < 3\text{ mm}$, $0 < \theta < 90^\circ$; $0 < \phi < 90^\circ$, given the potential

$$\text{field } V =: \textcircled{1} \frac{200}{r} V, \textcircled{2} \frac{300 \cos \theta}{\delta^2} V.$$

$$\text{Ans: } \cancel{1.391 \mu\text{J}}, 36.7 \mu\text{J}, \\ 46.4 \mu\text{J}$$

↳ corrected in 8th edition.

Current and Current Density

Current (in amperes) through a given area is the electric charge passing through the area per unit time. Also, the rate of movement of charge passing a given reference point (or crossing a given reference plane) of one coulomb per second. Current is symbolized by I and given by

$$I = \frac{dQ}{dt}$$

current is thus defined by the motion of positive charges, even though conduction in metals takes place through the motion of electrons.

Thus, in a current of one ampere, charge is being transferred at a rate of one Coulomb per second.

Current density is the current per unit area measured in Ampere per meter square and represented by J .

If ΔI current flows through a surface ΔS , the current density is

$$J_A = \frac{\Delta I}{\Delta S}$$

$$\text{or, } \Delta I = J_A \Delta S$$

assuming that the current density is perpendicular to the surface. If current density is not normal to the surface then,

$$\Delta I = J \cdot \vec{\Delta S}$$

Then, total current is obtained by integrating

$$I = \int_S J \cdot d\vec{S}$$

17) Current density may be related to the velocity of volume charge density at a point.

Let us consider the element of charge

$$\Delta Q = \rho_v \Delta v = \rho_v \Delta S \Delta l \text{ as shown in figure.}$$

If the element of charge is moved a distance Δx in a time interval Δt we will find that $\Delta Q = \rho_v \Delta S \Delta x$

charge has been moved through a reference plane perpendicular to the direction of motion.

So, resultant current is

$$\Delta I = \frac{\Delta Q}{\Delta t} = \rho_v \Delta S \frac{\Delta x}{\Delta t}$$

Taking the limit with respect to time

$$\Delta I = \rho_v \Delta S v_x$$

where v_x represents the ΔS x -component of the velocity \vec{v} . In terms of current density, so,

$$J_x = \rho_v v_x$$

and in general

$$\boxed{\vec{J} = \rho_v \vec{v}}$$

This shows that the change in motion constitutes the current and this type of current is called convection current and J or \vec{J} is the convection current density. Depending on how I is produced, there are different kinds of current densities: convection current density, conductive current density and displacement current density.

Continuity of Current (Continuity Equation)

Conservation of charge — The principle of conservation of charge states that charges can be neither created nor destroyed although equal amounts of positive and negative charge may be simultaneously created, obtained by separation, destroyed or lost by recombination.

The continuity equation follows the conservation of charge principle when any region bounded by a closed surface is considered. The current through closed surface is given by

$$I = \oint_S \vec{J} \cdot d\vec{s}$$

This is the outflow of positive charge from the closed surface and must be balanced by the decrease of positive charge (or increase of negative charge) within the closed surface. If the change inside the closed surface is denoted by δi , then the rate of decrease of charge is $-\frac{d\delta i}{dt}$ and the principle of conservation of charge requires,

$$I = \oint_S \vec{J} \cdot d\vec{s} = -\frac{d\delta i}{dt}$$

The sign of $-\frac{d\delta i}{dt}$ depends on the type of charge; for +ve it is -ve & for -ve charge it is +ve. The above current is the outward flowing current. The above equation is integral form of continuity equation and the point or differential form is obtained by using the divergence theorem.

$$\oint_S \vec{J} \cdot d\vec{s} = \int_{\text{Vol.}} (\nabla \cdot \vec{J}) dV$$

Also, we can use the volume charge density for Φ_i as:

$$\Phi_i = \int_{V_{\text{tot}}} \rho_i dV$$

So,

$$\int_{V_{\text{tot}}} (\nabla \cdot \vec{J}) dV = -\frac{d}{dt} \int_{V_{\text{tot}}} \Phi_i dV$$

If the surface is kept constant the derivative becomes a partial derivative and

$$\int_{V_{\text{tot}}} (\nabla \cdot \vec{J}) dV = \int_{V_{\text{tot}}} -\frac{\partial \Phi_i}{\partial t} dV$$

Since, the expression is true for any volume, however small it is also true for an incremental or differential volume.

So,

$$(\nabla \cdot \vec{J}) \Delta V = -\frac{\partial \Phi_i}{\partial t} \Delta V$$

$$\nabla \cdot (\vec{J}) = -\frac{\partial \Phi_i}{\partial t}$$

This is the point form of continuity Equations. This indicates that the current or charge per second, diverging from a small volume per unit volume is equal to the time rate of decrease of charge per unit volume at every point.

Let us consider a current density that is directed radially outward and decreases exponentially with time,

$$\vec{J} = \frac{1}{r} e^{-t} \hat{a}_r A/m^2$$

Selecting an instant of time $t = 1s$, we may calculate the total outward current at $r = 5m$:

$$I = J_r \cdot S = \left(\frac{1}{5} e^{-1}\right) (4\pi s^2) = 23.1 A$$

For $r = 6m$ & $t = 1s$,

$$I = J_r \cdot S = \left(\frac{1}{6} e^{-1}\right) (4\pi s^2) = 27.7 A$$

Then, from continuity Eq:

$$-\frac{\partial \rho_v}{\partial t} = \nabla \cdot \vec{J} = \nabla \cdot \left(\frac{1}{r} e^{-t} \hat{a}_r \right) = \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{1}{r} e^{-t} \right) = \frac{1}{r^2} e^{-t}$$

Integrating w.r.t. t :

$$\rho_v = - \int \frac{1}{r^2} e^{-t} dt + k(r) = \frac{1}{r^2} e^{-t} + k(r)$$

If we assume that $\rho_v \rightarrow 0$ as $t \rightarrow \infty$ then $k(r) = 0$

$$\therefore \boxed{\rho_v = \frac{1}{r^2} e^{-t} C/m^3}$$

Now, we may use $\vec{J} = \rho_v \vec{V}$ to find velocity

$$V_r = \frac{J_r}{\rho_v} = \frac{\frac{1}{r} e^{-t}}{\frac{1}{r^2} e^{-t}} m/s = \propto m/s.$$

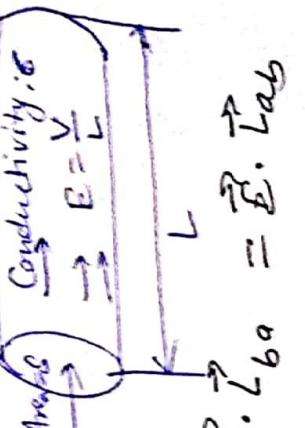
Point form of Ohm's Law

For any metallic conductors, the relation bet. \vec{J} and \vec{E} is given by $\vec{J} = \sigma \vec{E}$ or $J = \rho A E$ - This is the point form of Ohm's law where, σ = Conductivity of that metallic conductor

$$= \frac{e n e}{l}$$

$n e$ is free electron charge density & l is mobility of the electron.

Let us consider for any cylindrical metallic conductor, J & E are uniform. Then the current through the metallic conductor is given by

$$\text{Area } A = \int_S \vec{J} \cdot d\vec{S} = JS$$


$$\text{and } V_{ab} = - \int_b^a \vec{E} \cdot d\vec{l} = - \vec{E} \cdot \int_b^a dl = - \vec{E} \cdot L_{ba} = - \vec{E} \cdot L \hat{a}_x$$

$$\text{or, } V = EL$$

$$\text{So, } J = \frac{I}{S} = \sigma E = \sigma \frac{V}{L}$$

$$\text{or } R = \frac{L}{\sigma S} I$$

The ratio of the potential difference bet. two ends of the cylinder to the current entering the more positive end is the resistance of the cylinder and hence

$$V = IR$$

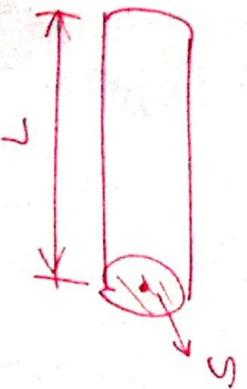
For non uniform fields

$$R = \frac{V_{ab}}{I} = \frac{- \int_b^a \vec{E} \cdot d\vec{l}}{\int_S \sigma \vec{E} \cdot d\vec{S}}$$

where, $R = \frac{L}{\sigma S}$

Point form of Ohm's law (Derivation)

$$\text{Resistivity, } \sigma = \frac{1}{\rho} = \frac{R \cdot S}{L} \quad \text{(1)}$$



where, σ = conductivity of the conductor

$$\text{so, } \sigma = \frac{I}{RS} \quad \text{(2)}$$

Again, Assuming that the field \vec{E} & current density \vec{J} for metallic conductors are uniform, then,

Potential difference bet. two ends of the conductor is given by

$$V = EL \quad [\because V_{ab} = - \int_b^a \vec{E} \cdot d\vec{l} = \vec{E} \cdot [\vec{l}]_{ab}] \quad \text{(3)}$$

& the current passing through the conductor is

$$I = JS \quad [\because I = \int_s \vec{J} \cdot d\vec{s} = JS] \quad \text{(4)}$$

Again, from Ohm's Law

$$V = IR$$

$$\text{or, } EL = JS \cdot R$$

$$\text{or, } J = \frac{L}{R \cdot S} E$$

so, in vector form $\vec{J} = \sigma \vec{E}$

This is point form of Ohm's Law.

Relaxation Time

Let us consider any conductor containing charge. When we see the charge on any conductor they will appear at the surface as surface charge. Initially, when we introduce the charge into the conductor the charge will be seen at every point of the conductor. After some time it will move towards surface and finally all charge will be seen at the surface. So, the time taken to move the charge from the point in conductor to the surface of conductor is termed as the relaxation constant for that conductor.

Now, from ohm's law (point form)

$$\vec{J} = \sigma \vec{E}$$

and from continuity equation (point form)

$$\nabla \cdot \vec{J} = - \frac{\partial \rho_v}{\partial t}$$

in which \vec{J} & ρ_v both involve only free charges.

$$\nabla \cdot \sigma \vec{E} = - \frac{\partial \rho_v}{\partial t}$$

$$\text{or, } \nabla \cdot \frac{\epsilon}{\epsilon_0} \vec{D} = - \frac{\partial \rho_v}{\partial t} \quad \left[\because \epsilon = \epsilon_0 \epsilon_r \right]$$

↳ permittivity of conductor.

If we assume that the medium is homogeneous, so that σ & ϵ are not functions of position.

$$\nabla \cdot \vec{D} = - \frac{\epsilon}{\epsilon_0} \frac{\partial \rho_v}{\partial t}$$

$$\text{or, } \rho_v = - \frac{\epsilon}{\epsilon_0} \frac{\partial \rho_v}{\partial t} \quad \text{using maxwell's first}$$

$$\text{Equation } \nabla \cdot \vec{D} = \rho_v$$

Relaxation time or rearrangement time

It is the time it takes a charge placed in the interior of a material to drop to $e^{-1} = 36.8$ percent of its initial value.

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If we assume that σ is not a function of r , then we will get the solution as:

$$J_V = J_0 e^{-(6/\epsilon)t}$$

where, J_0 = charge density at $t=0$. This shows an exponential decay of charge density at every point with a time constant of $\epsilon/6$; which is called relaxation time.

i.e. Relaxation time = $\frac{\epsilon}{6}$

For distilled water,

$$\frac{\epsilon}{6} = \frac{80 \times 8.854 \times 10^{-12}}{2 \times 10^{-4}} = 3.54 \text{ μs.}$$

Qn: Let $\vec{J} = \frac{400 \sin \theta}{r^2 + 4} \hat{A}/\text{m}^2$ ② Find the total current flowing through that portion of the spherical surface $r=0.8$ bounded by $\theta = 0.1\pi$, $\phi = 0.3\pi$, $0 \leq \rho \leq 2\pi$ ③ Find the average value of \vec{J} over the defined area.

Soln: Given,

$$\vec{J} = \frac{400 \sin \theta}{r^2 + 4} \hat{A} \text{ A/m}^2$$

② Spherical surface $r=0.8$, bounded by $0.1\pi \leq \theta \leq 0.3\pi$, $0 \leq \phi \leq 2\pi$. Then,

the current flowing through that portion, $I = \int_S \vec{J} \cdot d\vec{s}$.

$$= \int_S \vec{J} \cdot (r^2 \sin \theta d\phi d\theta) \hat{A} = \int_0^{2\pi} \int_0^{0.3\pi} \frac{400 \sin \theta}{(0.8)^2 + 4} \cdot (0.8)^2 \sin \theta d\theta d\phi$$

(12.3)

$$= \frac{400(0.8)^2 2\pi}{4 \cdot 84} \int_{\theta=0}^{0.3\pi} \sin^2 \theta d\theta$$

$$\theta = 0.1\pi$$

$$= 346.5 \int_{\theta=0}^{0.3\pi} \frac{1}{2} [1 - \cos 2\theta] d\theta$$

$$= 77.4 A$$

⑥ The area is given by

$$\begin{aligned} \text{Area} &= \int_{\phi=0}^{2\pi} \int_{\theta=0}^{0.3\pi} (0.8)^2 \sin \theta d\theta d\phi \\ &= 1.46 \text{ m}^2 \end{aligned}$$

The average current density is thus

$$\vec{J}_{\text{avg}} = \frac{\mathcal{I}}{\text{Area}} \hat{a}_r = \frac{77.4}{1.46} \hat{a}_r = 53.0 \hat{a}_r \text{ A/m}^2$$

Qn: The current density in certain region is approximated by $\vec{J} = \left(\frac{0.1}{r}\right) e^{-10t} \hat{a}_r \text{ A/m}^2$ in spherical co-ordinates.

⑦ How much current is crossing the surface $r = 50 \text{ cm}$, at $t = 1 \mu\text{s}$? Find $J_r(r, t)$ assuming that $\theta_r \rightarrow 0$ as $t \rightarrow \infty$.

Sol: Given, $\vec{J} = \frac{0.1}{r} e^{-10t} \hat{a}_r \text{ A/m}^2$

⑧ The current crossing the surface $r = 50 \text{ cm}$ at $t = 1 \mu\text{s}$ is

$$\begin{aligned} \mathcal{I} &= J_r \cdot S = \left(\frac{0.1}{0.5} e^{-10 \times 10^{-6}} \right) \cdot 4\pi \times (0.5)^2 \\ &= \frac{1}{5} e^{-1} \cdot 4\pi \times 0.25 \times 0.2 \times 0.3678 \times 4\pi \times 0.25 \\ &= 0.231 A \end{aligned}$$

again, (6) we have, From continuity Eq: $-\frac{\partial \rho_v}{\partial t} = (\nabla \cdot \vec{J})$

$$\rho_v(r, t) = - \int \frac{0.1}{r^2} e^{-10^6 t} dt$$

$$= - \frac{0.1}{r^2} \cdot (-10^6) \cdot e^{-10^6 t} + K(r)$$

$$= \frac{10^7}{r^2} e^{-10^6 t} + K(r)$$

If $r \rightarrow 0$ as $t \rightarrow \infty$

then, $K(r) = 0$

$$\text{so, } \rho_v(r, t) = \frac{10^7}{r^2} e^{-10^6 t}$$

For, $r = 50 \text{ cm. as } t = 1 \mu s.$

$$\rho_v = \frac{10^5}{0.5} e^{-10^6 \times 10^{-6}}$$

$$= \frac{10^5 \times 0.3678}{0.5}$$

$$= 73560 \times 10^3 \text{ C/m}^3$$

Qn: A current density in certain region is given as:

$$\vec{J} = 20 \sin\theta \cos\phi \hat{a}_r + \frac{1}{r} \hat{a}_\theta A/m^2, \text{ Find:}$$

(i) The average value of \vec{J} over the surface $r=1, 0 < \theta < \pi/2$

$$0 < \phi < \pi/2 \quad [2073 \text{ Shrawan}]$$

$$(ii) \frac{\partial \rho_r}{\partial t} = ?$$

$$\text{Soln: Given, } \vec{J} = 20 \sin\theta \cos\phi \hat{a}_r + \frac{1}{r} \hat{a}_\theta A/m^2$$

$$(i) \text{ Area} = \int_S r^2 \sin\theta d\phi$$

$$= \int_{\theta=0}^{\pi/2} \int_{\phi=0}^{\pi/2} (r^2 \sin\theta) d\phi$$

$$= \frac{\pi}{2} [-\cos\phi]_0^{\pi/2}$$

$$= \frac{\pi}{2} \cdot 1$$

$$= \frac{\pi}{2} m^2$$

$$\text{& } (ii) I = \int_S \vec{J} \cdot d\vec{s} = \int_S (20 \sin\theta \cos\phi \hat{a}_r + \frac{1}{r} \hat{a}_\theta A). (r^2 \sin\theta \cdot d\phi \hat{a}_\theta)$$

$$= \int_{\theta=0}^{\pi/2} \int_{\phi=0}^{\pi/2} 20 \sin^2\theta \cdot \cos\phi \cdot d\phi \cdot d\theta$$

$$\text{So, } \vec{J}_{\text{avg}} = \frac{I}{\text{Area}} \hat{a}_r = \dots \hat{a}_r A/m^2$$

(iii)

$$\frac{\partial \rho_r}{\partial t} = - \nabla \cdot \vec{J} = - \left(\frac{1}{r^2} \frac{\partial}{\partial \theta} (r^2 J_r) + \frac{1}{r \sin\theta} \frac{\partial (r^2 J_\theta)}{\partial \phi} \right) + \frac{1}{r \sin\theta} \frac{\partial J_z}{\partial \theta}$$

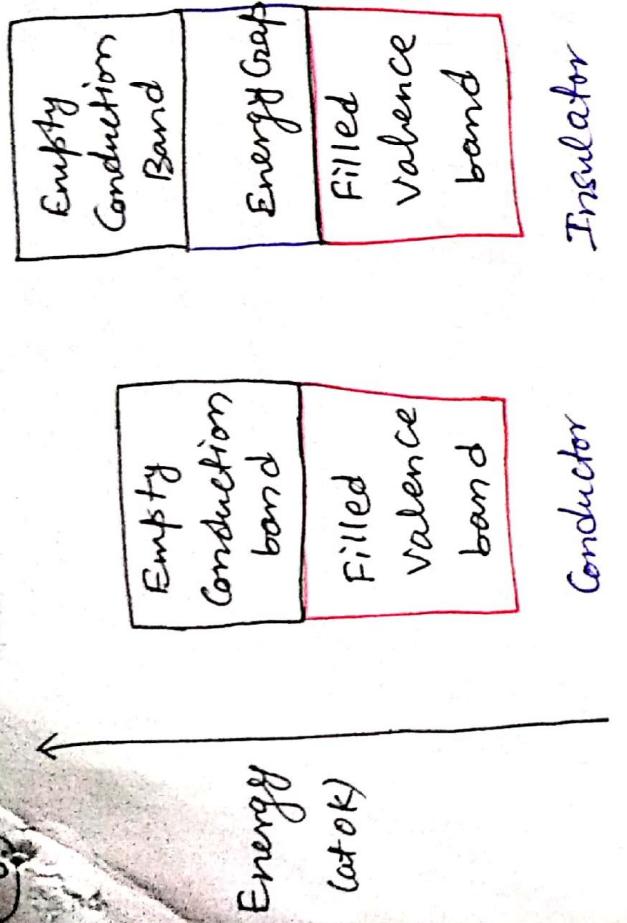
Electric Properties of Material Mediums

As electric fields can exist in free space, they can exist in material media. Materials are broadly classified in terms of their electrical properties as conductors and non conductors. Non conducting materials are usually referred to as insulators or dielectrics.

In a broad sense materials may be classified in terms of their conductivity σ , in mhos per meter (Ω^{-1}/m) or siemens per meter (S/m), as conductors and non conductors, or technically as metals and insulators (or dielectrics). The conductivity of a material usually depends on temperature and frequency. A material with high conductivity ($\sigma \gg 1$) is referred to as a metal whereas one with low conductivity ($\sigma < 1$) is referred to as an insulator. A material whose conductivity lies some where 'bet.' those of metals and insulators is called semiconductor. Copper and aluminium are metals, silicon and germanium as semiconductors and glass and rubber are insulators. The conductivity of metals generally increases with decrease in temperature. At temperatures near absolute zero ($T=0^\circ K$), some conductors exhibit infinite conductivity and are called superconductors. Lead and aluminium are typical examples of such metals. The major difference bet. a metal and an insulator lies in the amount of electrons available for conduction of current in contrast to metals, which have an abundance of free electrons.

For conductors, current is due to movement of electrons. and with field \vec{E} due to charge $q = -e$

$$\text{Force, } \vec{F} = -e\vec{E}.$$



In free space, the electrons would accelerate and continuously increase its velocity (and energy); in the crystalline material the progress of the electron is impeded by continual collisions with the thermally excited crystalline lattice structure, and a constant average velocity is soon attained. The velocity v_d is termed as the drift velocity and linearly related to the electric field intensity by the mobility of the electron in the given material.

$$\therefore \vec{v}_d = \mu_e \vec{E}$$

where, μ_e = mobility of an electron and is positive by definition.

$$\text{Also, } \vec{J} = -\sigma_e \vec{v}_d \vec{E}$$

where, σ_e = free electron charge density, a -ve value.

Free and Bound Charges

Free Charges: It is the one that moves freely in space i.e without an external electromagnetic field. Any electric charge that can be placed on a conductor or on or within a dielectric. e.g. - Electrons in a conductor, which are free to move throughout the material. Electrons or ions in a vacuum are also free charges.

Bound charges :- It is one that cannot move freely or will move only in response to the external electromagnetic force. Charges on the surface of an insulator are an example. Also, the electric charge that is bound to an atom or molecule is bound charges.

Polar Molecules :- The molecules that have a permanent displacement existing betⁿ the centers of gravity of the positive and negative charges, and each pair of charges acts as dipole.

Non polar Molecules :- Does not have the dipole arrangement until after a field is applied. i.e sufficiently strong field is required to produce an additional displacement betⁿ the positive and negative charges.

Polarization

When the atoms of a material are under the influence of the electric field, the electrons shift their positions and the atoms are said to be polarized; the phenomenon being is called polarization. The direction of polarization is from -ve to +ve charges or in the dirn. of \vec{E} .

Also, polarization is the dipole moment per unit volume.

$$\text{i.e } \vec{P} = \lim_{\Delta V \rightarrow 0} \frac{1}{\Delta V} \sum_{i=1}^{n \Delta V} \vec{p}_i$$

where, \vec{p}_i = dipole moment

& given by $\vec{p} = Q \vec{d}$; \vec{d} = vector from -ve to +ve charges

$$\vec{P}_{\text{total}} = \sum_{i=1}^{n \Delta V} \vec{p}_i = \text{total dipole moment}$$

If there is n dipoles per unit volume, or ΔV then there will be $n \Delta V$ dipoles.

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Let us consider the dielectric containing non polar molecules. A molecule has a dipole moment, and $\vec{P} = 0$ throughout the material.

Somewhere in the interior of dielectric let us select an incremental surface element $\Delta \vec{s}$ as shown in figure; and apply the electric field \vec{E} . The field \vec{E} produces a dipole moment $\vec{P} = Q\vec{d}$ in each molecule such that \vec{P} is at an angle θ with $\Delta \vec{s}$.

Let us inspect the movement of bound charges across $\Delta \vec{s}$. Each of the charges associated with the creation of a dipole must have moved a distance $\frac{d}{2} \cos \theta$ in the direction perpendicular to $\Delta \vec{s}$. Thus, any positive charges initially lying below the surface $\Delta \vec{s}$ and within the distance $\frac{d}{2} \cos \theta$ of the surface must have crossed $\Delta \vec{s}$ going upward. Also, any negative charges initially lying above the surface and within that distance ($\frac{d}{2} \cos \theta$) from $\Delta \vec{s}$ must have crossed $\Delta \vec{s}$ going downward. Therefore since there are n molecules/m³, the net total charge which crosses the elemental surface in an upward direction is equal to $n Q \cos \theta \Delta \vec{s}$ or $\Delta Q_b = n Q d \vec{i} \cdot \Delta \vec{s}$

where, ΔQ_b = bound charge.

Now, in terms of polarization

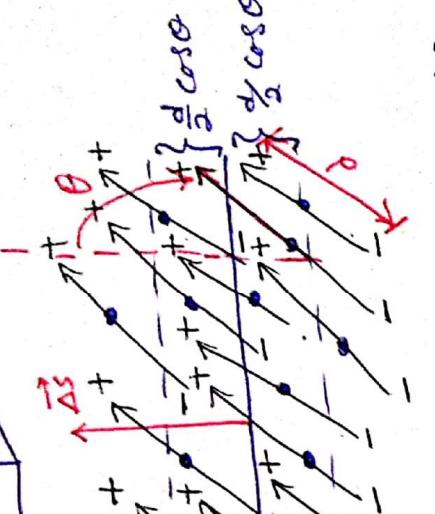
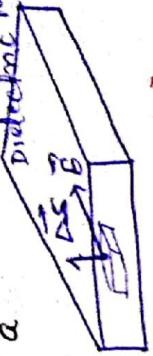
$$\Delta Q_b = \vec{P} \cdot \Delta \vec{s}$$

If we interpret $\Delta \vec{s}$ as an element of a closed surface inside the dielectric material, then the dir' of $\Delta \vec{s}$ is outward, and the net increase in the bound charge within the closed surface is obtained through the integral

$$Q_b = - \oint_S \vec{E}_0 \cdot d\vec{s}$$

Similar expression from Gauss's Law

$$Q_T = \oint_S \vec{E}_0 \cdot d\vec{s} \quad \text{where, } Q_T = Q_b + Q$$



and \mathcal{Q} is the total free charge enclosed by the surfaces,

Now, $\mathcal{Q} = \delta_T - \delta_E = \int_S (\epsilon_0 \vec{E} + \vec{P}) \cdot d\vec{s}$

we may define \vec{D} in more general terms as:

$$\boxed{\vec{D} = \epsilon_0 \vec{E} + \vec{P}}$$

Thus, for polarizable material the added \vec{P} (polarization) is present in the relation

$$\mathcal{Q} = \int_S \vec{D} \cdot d\vec{s}.$$

where, \mathcal{Q} = free charge enclosed.

Isotropic materials — The materials in which \vec{E} & \vec{P} are linearly related. The \vec{E} & \vec{P} are always parallel, regardless of the orientation of the field.

Nonisotropic or Anisotropic Materials — The materials in which \vec{E} and \vec{P} are non linearly related and \vec{E} & \vec{P} does not have same direction.

Relative Permittivity (ϵ_R)

for ferroelectric materials the relationship bet? \vec{P} & \vec{E} is not only nonlinear, but also shows hysteresis effects; that is the polarization produced by a given electric field intensity depends on the past history of the sample. e.g.: barium titanate used in ceramic capacitors.

The linear relationship bet? \vec{P} and \vec{E} is

$$\boxed{\vec{P} = \chi_e \epsilon_0 \vec{E}}$$

(where, χ_e) is the dimensionless quantity called the electric susceptibility of the material.

Dielectric Strength - It is the maximum electric field that a dielectric can tolerate or withstand without breakdown.

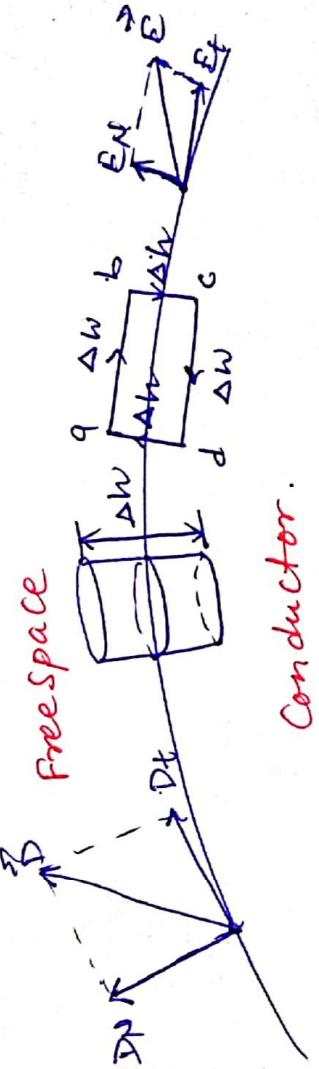
(30)

$$\text{Now, } \vec{D} = \epsilon_0 \vec{E} + \vec{P} = \epsilon_0 \vec{E} + \chi_e \epsilon_0 \vec{E} = (\chi_e + 1) \epsilon_0 \vec{E} = \epsilon_r \epsilon_0 \vec{E}$$

where, $\boxed{\epsilon_r = \chi_e + 1}$ is the dimensionless quantity known as relative permittivity or dielectric constant of the material.
 $\therefore \vec{D} = \epsilon_0 \epsilon_r \vec{E} = \epsilon \vec{E}$
where, $\boxed{\epsilon = \epsilon_0 \epsilon_r}$ is the permittivity of dielectric material.

Electric Boundary Conditions

① Boundary Conditions between freespace and Conductor



Conductor.

Let us consider the boundary of free space and the conductor. Since, all the charges resides on the exterior surface of the conductor the charge density within the conductor is zero. For static conditions in which no current may flow, the electric field intensity within the conductor is zero from Ohm's Law.

Let us consider \vec{E} be the external fields to the charge on the surface of the conductor then it can be decomposed to the tangential component and normal component to the conductor surface. The tangential component E_T is seen to be zero. If it is not zero then it would be applied to the elements of the surface charge, resulting in their motion and nonstatic conditions. Since, static condition is assumed, the tangential electric field intensity and electric flux density are zero.

13:

For the region interior to conductor the both fields are zero in the conductor.

For tangential components,

$$\oint \vec{E} \cdot d\vec{l} = 0 \text{ around the small closed path abeda.}$$

$$\int_a^b + \int_b^c + \int_c^d + \int_d^a = 0$$

Since, $\vec{E} = 0$ within the conductor, $ab = cd = \Delta w \neq bc = da = \Delta h$

then,

$$E_t \Delta w - E_N,_{ab} \cdot \frac{1}{2} \Delta h + E_N,_{cd} \frac{1}{2} \Delta h = 0$$

As, $\Delta h \rightarrow 0$ to approach zero, keeping Δw small but finite we get

$$E_t \Delta w = 0$$

$$\boxed{E_t = 0}$$

The Condition on the normal field is found most readily by considering Ds rather than E_N and choosing a small cylinder of the Gaussian surface. Let the height be Δh & the area of the top and bottom faces be Ds . Again, if Δh tends to zero, the top and bottom faces be Ds .

$$\oint_s \vec{B} \cdot d\vec{s} = \emptyset$$

$$\text{or, } \int_{\text{top}} + \int_{\text{bottom}} + \int_{\text{sides}} = \emptyset.$$

Since, no fields within conductor & tangential components of fields are zero $\int_{\text{bottom}} \vec{B} \cdot d\vec{s} = \int_{\text{sides}} \vec{B} \cdot d\vec{s} = 0$.

$$\therefore \int_{\text{top}} \vec{B} \cdot d\vec{s} = \emptyset$$

$$\delta r, D_N \Delta S = \varphi = \rho_s \Delta S$$

$$\text{or, } D_N = \rho_s$$

So, the desired boundary conditions for the conductor-free space boundary in electrostatics are:

$$\boxed{D_t = E_t = 0}$$

$$\& D_N = \epsilon_0 E_N = \rho_s$$

~~(2)~~ Boundary Conditions for Perfect Dielectric Materials

Let us consider the interface between two dielectrics having permittivities $\epsilon_1 \neq \epsilon_2$ and occupying regions 1 & 2 as shown in figure. We first examine the tangential components by using $\vec{E} \cdot \vec{d} = 0$ [No work is done in closed path] around the small closed path A-B-C-D on the left as:

$$\int_A^B \vec{E} \cdot \vec{d} + \int_B^C \vec{E} \cdot \vec{d} + \int_C^D \vec{E} \cdot \vec{d} + \int_D^A \vec{E} \cdot \vec{d} = 0$$

$$\text{or, } E_{tang} \Delta w - E_{tang} \Delta w = 0$$

$$\text{or, } E_{tan1} = E_{tan2}$$

Since, the normal component of \vec{E} along the sections of length Δw becomes negligible as Δw decreases and the closed path crowds the surface.

If the tangential electric field intensity is continuous across the boundary then tangential \vec{E} is discontinuous

(33) i.e

$$\frac{D_{\text{tan}1}}{\epsilon_1} = \frac{D_{\text{tan}2}}{\epsilon_2}$$

$$\text{or, } \frac{D_{N1}}{D_{N2}} = \frac{\epsilon_1}{\epsilon_2}$$

Now, the boundary conditions on the normal components are found by applying Gauss's Law to the small "pill box". The sides are again very short, and the flux leaving the top & bottom surfaces is the difference

$$D_{N1}\Delta S - D_{N2}\Delta S = \Delta \phi = \rho_s \Delta S$$

$$\text{or, } D_{N1} - D_{N2} = \rho_s$$

Assuming $\rho_s = 0$ in the interface betw. two perfect dielectrics

Then,

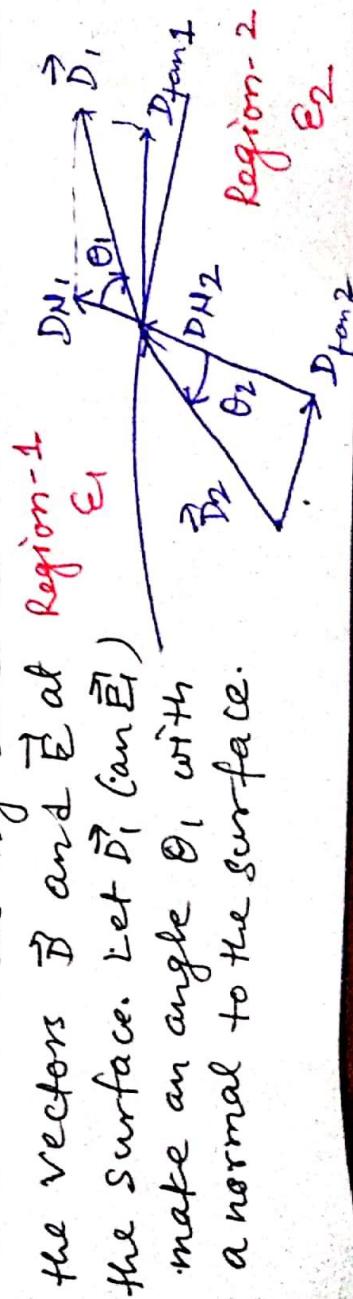
$$D_{N1} = D_{N2}$$

or the normal component of \vec{D} is continuous &

$$\epsilon_1 E_{N1} = \epsilon_2 E_{N2}$$

$$\text{or, } \frac{E_{N1}}{E_{N2}} = \frac{\epsilon_2}{\epsilon_1}$$

normal component of \vec{E} is discontinuous.
These conditions may be combined to show the change in



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Since the normal components of \vec{D} are continuous,

$$D_{N_1} = D_1 \cos \theta_1 = D_2 \cos \theta_2 = D_{N_2} \quad \text{--- } (a)$$

& the ratio of tangential component is given by

$$\frac{D_{\tan 1}}{D_{\tan 2}} = \frac{D_1 \sin \theta_1}{D_2 \sin \theta_2} = \frac{\epsilon_1}{\epsilon_2}$$

$$\text{or, } \epsilon_2 D_1 \sin \theta_1 = \epsilon_1 D_2 \sin \theta_2 \quad \text{--- } (b)$$

Now, dividing (b) by (a) we get

$$\frac{\tan \theta_1}{\tan \theta_2} = \frac{\epsilon_1}{\epsilon_2}$$

Since, we have assumed $\epsilon_1 > \epsilon_2$ and therefore $\theta_1 > \theta_2$.
Direction of \vec{E} on each side of the boundary is identical
with the \vec{B} , because $\vec{D} = \epsilon \vec{E}$.

The magnitude of \vec{D} in region 2 may be

$$D_2 = D_1 \sqrt{\cos^2 \theta_1 + \left(\frac{\epsilon_2}{\epsilon_1}\right)^2 \sin^2 \theta_1} \quad (*)$$

and the magnitude of \vec{E}_2 is

$$E_2 = E_1 \sqrt{\sin^2 \theta_1 + \left(\frac{\epsilon_1}{\epsilon_2}\right)^2 \cos^2 \theta_1} \quad (**)$$

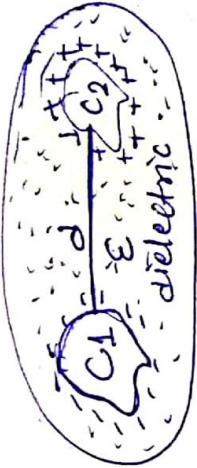
(*) Since, $D_{N_2} = D_1 \cos \theta_1$ & $D_{\tan 2} = \frac{\epsilon_2}{\epsilon_1} D_1 \sin \theta_1$

Also, $E_{N_2} = \frac{\epsilon_1}{\epsilon_2} E_1 \cos \theta_1$ & $E_{\tan 2} = \frac{\epsilon_1}{\epsilon_2} \sin \theta_1$

$$\therefore E_2 = \sqrt{E_{N_2}^2 + E_{\tan 2}^2} = \sqrt{\left(\frac{\epsilon_1}{\epsilon_2}\right)^2 \cos^2 \theta_1 + \left(\frac{\epsilon_1}{\epsilon_2}\right)^2 \sin^2 \theta_1} = \sqrt{\epsilon_1^2 \cos^2 \theta_1 + \epsilon_1^2 \sin^2 \theta_1} = \epsilon_1 \sqrt{\cos^2 \theta_1 + \sin^2 \theta_1} = \epsilon_1$$

Capacitance - It is the ratio of the magnitude of total charge on either conductor to the magnitude of the potential difference bet' 2 conductors where, two conductors with equal charges but in opposite signs are separated by small distance and a dielectric is placed in bet' the two conductors.

$$i.e. C = \frac{Q}{V_0}$$



Also, we define Q by a surface integral over the positive conductors and find V_0 by carrying unit positive charge from the -ve to +ve surface,

$$C = \frac{\int_S \epsilon E^2 \cdot d\vec{S}}{- \int_{-ve}^{+ve} \vec{E} \cdot d\vec{l}}$$

Gauss law

Capacitance is measured in Farads (F) and is a function of only the physical dimensions of the system of conductors and of the permittivity of the homogeneous dielectric.

① Capacitance of the parallel plate capacitor

Let us consider two metallic conductors are separated by the distance d . Let the space is filled with dielectric material of permittivity, ϵ and a uniform surface charge of s is placed on conductor at $z=0$ & $-s$ charge density is placed on conductor at $z=d$. Then, the electric field intensity will be generated from +ve to -ve charges as shown in figure.

As we know, the electric field intensity in bet' two plates is

$$\vec{E} = \frac{\rho c}{\epsilon} \hat{q}_x = \frac{\rho s}{\epsilon} \hat{q}_x$$

C : since z-axis is considered in figure.

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Now, from definition of capacitance,

$$C = \frac{\oint_s E \vec{E} \cdot d\vec{l}}{-\int_{-ve}^{+ve} E \cdot d\vec{l}} = \frac{Q}{V_0} = \frac{Q}{-\int_{-ve}^{+ve} E \cdot d\vec{l}}$$

$$\begin{aligned}
 &= \frac{\rho_s \cdot S}{-\int_0^d \frac{\rho_s}{\epsilon} dr} \\
 &\quad z=d \\
 &= \frac{\rho_s \cdot S}{\epsilon [0-d]} \\
 &= \frac{\rho_s S}{\epsilon d} \\
 &= \frac{\epsilon S}{d} \\
 &= \frac{\epsilon S}{d} \cdot \frac{S}{d} \\
 &= \frac{\epsilon S^2}{d^2} \\
 &\therefore C = \frac{\epsilon S}{d} \quad \text{where, } S = \text{Area of the conductors} \\
 &\quad \& d = \text{separations b/w conductors}
 \end{aligned}$$

② Capacitance of the Co-axial Capacitor

Let us consider two cylindrical metallic conductors of length L , inner radius a and outer radius b are separated by certain distance as shown in figure. Let the space b/w two conductors is filled with dielectric material of ϵ permittivity. Then, the electric field intensity is produced from +ve charge to -ve charge & given by.

$$\vec{E} = \frac{\rho_s q}{\epsilon r} \hat{a}_r \quad \text{where, } \rho = \text{radius in betw. } a \& b.$$

$$\text{Then, } C = \frac{Q}{V} = \frac{\rho_s \cdot 2\pi aL}{-\int_{-ve}^{+ve} \epsilon r dr}$$

$$\text{or, } C = \frac{\rho_s 2\pi a L}{-\int_b^a \frac{\rho_s q}{\epsilon} \hat{q} p \cdot d\hat{q}}$$

$$= \frac{\rho_s \cdot 2\pi a L}{-\frac{\rho_s q \ln(p)}{\epsilon} \Big|_b^a}$$

$$= \frac{2\pi a L \epsilon}{-\ln(a) + \ln(b)}$$

$$= \frac{2\pi a L \epsilon}{\ln(\frac{b}{a})}$$

$$\therefore C = \boxed{\frac{2\pi a L \epsilon}{\ln(\frac{b}{a})}}$$

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इन्डियर

Graphical Field Plotting (Curvilinear squares)

It is the basic and first mapping method. The method to be described is applicable only to fields in which no variation exists in the direction normal to the plane of the sketch. The procedure is based on several facts given as:

- ① A conductor boundary is an equipotential surface.
- ② The electric field intensity and electric flux density are both perpendicular to the equipotential surfaces.
- ③ \vec{E} & \vec{D} are therefore perpendicular to the conductor boundaries and possess zero tangential values.
- ④ The lines of electric flux, or streamlines, begin and terminate on charge and hence, in a charge free, homogeneous dielectric, begin and terminate only on the conductor boundaries.

Equipotentials.

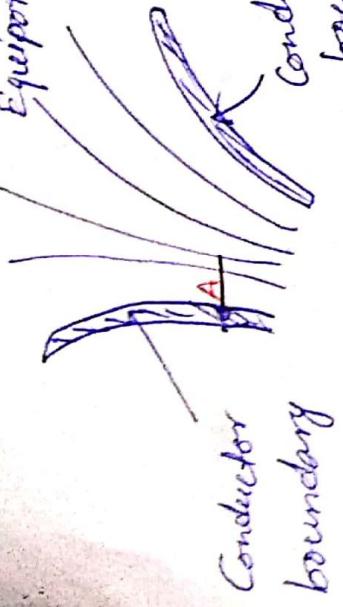
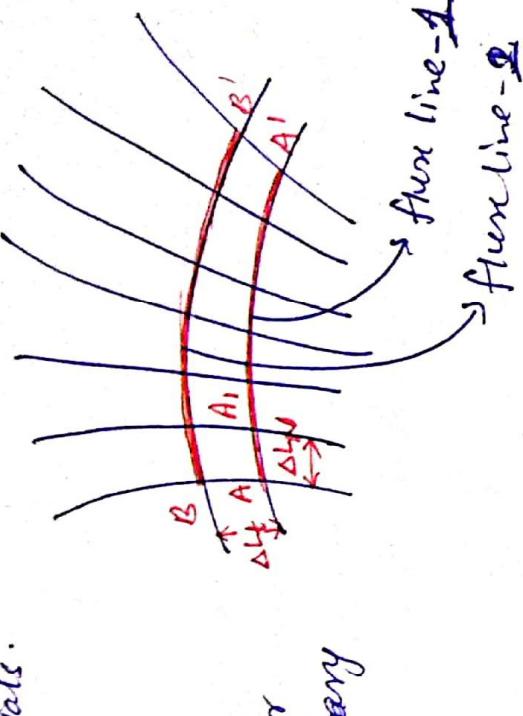


fig. sketch of equipotential surfaces betⁿ two conductors.



Let us construct the equipotential surfaces betⁿ two conductors as shown in figure. Let the flux line-1 is drawn from A to A' & another flux line-2 drawn from B to B' as shown in figure. During the construction of AA' & BB' flux lines the perpendicularity is maintained betⁿ equipotential surfaces & the flux lines. Here, the electric field intensity at the midpoint of the line joining A to B may be found approximately by assuming a value for the flux in the tube AB, say $\Delta \psi$, so electric flux density is $\frac{\Delta \psi}{\Delta L}$, where the depth of the tube into the paper is 1 m and ΔL is ΔL the length of the line joining A to B

Magnitude of E is

$$E = \frac{1}{\epsilon} \cdot \frac{\Delta \psi}{\Delta L}$$

However, we may find the magnitude of the electric field intensity by dividing the potential difference betⁿ points A & A₁, lying on two adjacent equipotential surfaces, by the distance from A to A₁. If A to A₁ is ΔL_1 and ΔV is increment of potential betⁿ equipotentials. then,

$$E = \frac{\Delta V}{\Delta L_1}$$

The value applies most accurately to the point at the middle of the line segment from A to A₁ while previous was most accurate at the midpoint of the line segment from A to B. If the two adjacent equipotential surfaces are close together and the two streamline s are close together ($\Delta \psi$ small), the two values for E must be equal approximately.

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$$\text{i.e. } \frac{1}{\epsilon} \cdot \frac{\Delta \psi}{\Delta L_H} = \frac{\Delta V}{\Delta L_H}$$

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Throughout the sketch a homogeneous medium is considered (ϵ -constant), a constant increment of potential bet' equipotentials (ΔV constant) and a constant amount of flux per tube ($\Delta \psi$ constant). To satisfy all these conditions,

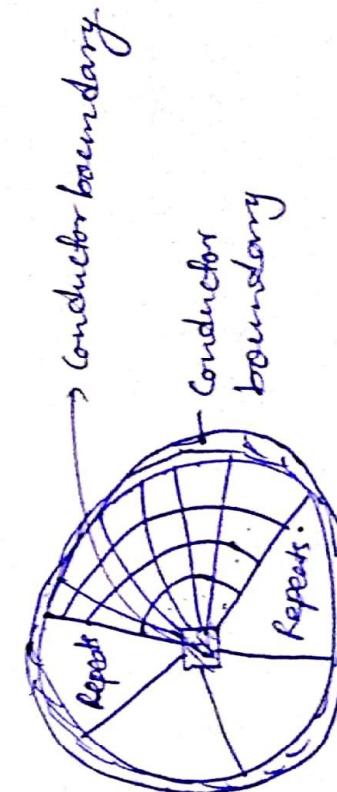
$$\frac{\Delta L_H}{\Delta L_H} = \text{constant} = \frac{1}{\epsilon} \cdot \frac{\Delta \psi}{\Delta V}$$

A similar argument might be made at any point of the sketch, and we are therefore led to a conclusion that a constant ratio must be maintained bet' the distance bet' streamlines as measured along an equipotential and the distance bet' equipotentials as measured along the streamline. It is the ratio which must have the same value at every point.

Again, the capacitance is found from $C = \frac{Q}{V_0}$ by replacing Q by $NQ \Delta \psi$, where NQ is number of flux tubes joining the two conductors and letting $V_0 = N \Delta V$, where N is the number of potential increments bet' conductors.

$$C = \frac{NQ \Delta \psi}{N \Delta V}$$

$$\text{or, } C = \frac{NQ}{N \Delta V} \epsilon \frac{\Delta L_H}{\Delta L_H} = \epsilon \frac{NQ}{N \Delta V} \text{ if } \frac{\Delta L_H}{\Delta L_H} = 1$$



$$C = \epsilon \frac{8 \times 3.25}{4} \text{ PF/m.s.} \quad N_V = 4 \quad N_Q = 6 \times 3.25$$

e 0

J

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Numerical Integration (The Iteration Method)

In potential problems where the potential is completely specified on the boundaries of a given region, particularly problems in which the potential does not vary in one direction (i.e. two dimensional potential distributions) there exist a repetitive method yielding desired accuracy. It can not be found with mapping method. So, digital computers should be used.

The iterative method is well suited for digital computers. Let us assume a two dimensional problem in which the potential does not vary with the z-co-ordinate and divide the interior of a cross section of the region where the ~~region~~ potential is desired into squares of length h on each side.

The unknown values of the potential at five adjacent points are indicated as V_0 , V_1 , V_2 , V_3 and V_4 as shown in figure. If the region is charge free and contains a homogeneous dielectric then

$$\nabla \cdot \vec{D} = 0 \text{ & } \nabla \cdot \vec{E} = 0, \text{ from which}$$

we have

$$\frac{\partial E_x}{\partial x} + \frac{\partial E_y}{\partial y} = 0$$

But the gradient operation gives

Fig:- two dimensional potential field region with squares of sides h.

$$E_x = -\frac{\partial V}{\partial x} \text{ & } E_y = -\frac{\partial V}{\partial y}$$

$$\text{So, } \frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} = 0$$

Approximate values for these partial derivatives may be obtained in terms of the assumed potentials at

$$\left. \frac{\partial V}{\partial x} \right|_c = \frac{V_0 - V_3}{h}$$

$$\left. \frac{\partial V}{\partial y} \right|_c = \frac{V_1 - V_3}{h}$$

(14) From which,

$$\frac{\partial^2 V}{\partial x^2} \Big|_0 = \frac{\partial V}{\partial x} \Big|_0 - \frac{\partial V}{\partial x} \Big|_0 = \frac{V_1 - V_0 - V_0 + V_3}{h}$$

Similarly,

$$\frac{\partial^2 V}{\partial y^2} \Big|_0 = \frac{V_2 - V_0 - V_0 + V_4}{h}$$

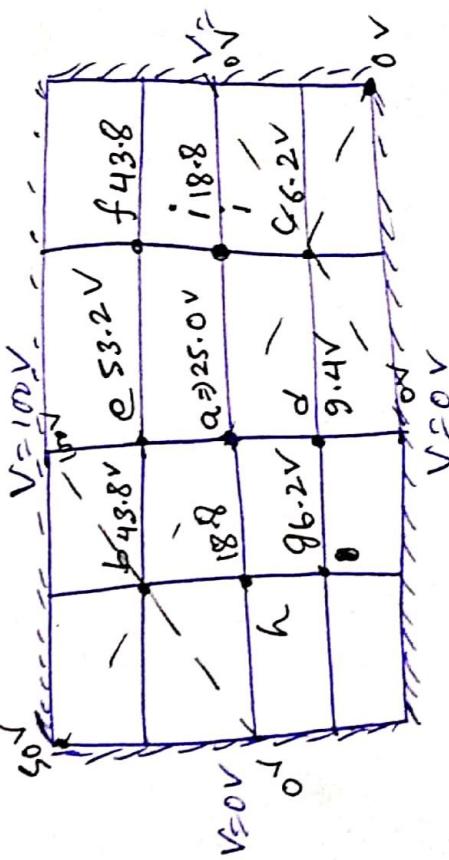
Combining,

$$\frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} = \frac{V_1 + V_2 + V_3 + V_4 - 4V_0}{h} = 0$$

$$\text{or, } \frac{(V_1 + V_2 + V_3 + V_4)}{4} = V_0$$

The expression becomes exact as h tends to zero.

e.g:-



$$\begin{aligned} \text{for } d, \\ V_d &= \frac{1}{4} (25 + 6.2 + 6.2 + 0) \\ &= 9.4 \text{ V} \\ \text{for } e, \\ V_e &= \frac{1}{4} (43.8 + 43.8 + 100 + 25) \\ &= 53.2 \text{ V} \end{aligned}$$

At first for a,

$$V_a = \frac{1}{4} (0 + 100 + 0 + 0) = 25.0 \text{ V}$$

Again, for b,

$$V_b = \frac{1}{4} (25 + 100 + 50 + 0) = 43.0 \text{ V}$$

$$\text{for } c, \quad V_c = \frac{1}{4} (25 + 0 + 0 + 0) = 6.2 \text{ V}$$

$$\begin{aligned} \text{for } h, \\ V_h &= \frac{1}{4} (0 + 25 + 6.2 + 43.8) \\ &= 18.8 \text{ V} \end{aligned}$$

Ques: Let the region $z < 0$ be composed of a uniform dielectric material for which $\epsilon_R = 3.2$, while the region $z > 0$ is characterized by $\epsilon_R = 2$. Let $\vec{D}_1 = -30\hat{a}_x + 50\hat{a}_y + 70\hat{a}_z \text{ nC/m}^2$ and find (a) D_{N1} by $\vec{E}_R = 2$ (b) \vec{P}_1 (c) D_{t1} (d) D_{N2} (e) \vec{B}_1 (f) \vec{B}_2 (g) D_{t2} (h) D_{N2}

Sol: Given,

$$\vec{D}_1 = -30\hat{a}_x + 50\hat{a}_y + 70\hat{a}_z \text{ nC/m}^2$$

since, the two dielectric boundary lies in $z=0$

we have,

(a) Normal component of \vec{D}_1 is

$$D_{N1} = 70 \text{ nC/m}^2$$

$$D_{N1} = |\vec{D}_{N1}| = 70 \text{ nC/m}^2$$

$$\text{& (b)} \quad \vec{D}_{N1} = \vec{D}_{t1} = \vec{D}_1 - \vec{D}_{N1} = -30\hat{a}_x + 50\hat{a}_y + 70\hat{a}_z - 70\hat{a}_z$$

$$= -30\hat{a}_x + 50\hat{a}_y \text{ nC/m}^2$$

$$(c) \quad D_{t1} = |\vec{D}_{t1}| = \sqrt{(-30)^2 + (50)^2} = 58.3 \text{ nC/m}^2$$

$$(d) \quad D_1 = |\vec{D}_1| = \sqrt{(-30)^2 + (50)^2 + (70)^2} = 91.1 \text{ nC/m}^2$$

$$(e) \quad \text{we have,} \quad \Rightarrow \quad \vec{D}_{N1} \cdot \vec{D}_1 = |\vec{D}_{N1}| |\vec{D}_1| \cos \theta_1 \\ D_{N1} = D_1 \cos \theta_1$$

$$\text{or, } \theta_1 = \cos^{-1} \left(\frac{D_{N1}}{D_1} \right) = \cos^{-1} \left(\frac{70}{91.1} \right) = 39.8^\circ$$

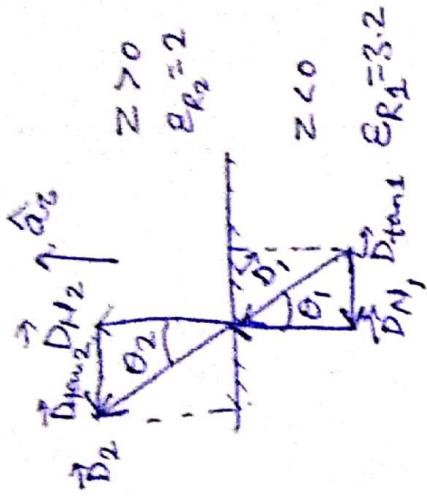
(f) we have,

$$\vec{P}_1 = \chi_e \epsilon_0 \vec{E}_1 \quad \text{and} \quad \vec{D}_1 = \epsilon_R \epsilon_0 \vec{E}_1$$

$$\text{or, } \vec{P}_1 = \frac{\chi_{e1} (\epsilon_0 \epsilon_{R1} \vec{E}_1)}{\epsilon_{R1}} = \frac{\chi_{e1}}{\epsilon_{R1}} \cdot \vec{D}_1$$

and $\epsilon_{R1} = \chi_{e1} t_1$

$$\text{or, } \chi_{e1} = \epsilon_{R1} - 1 = 3.2 - 1 = 2.2$$



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$$\text{so, } \vec{P}_1 = \frac{\epsilon_0}{3.2} (-30\hat{a}_x + 50\hat{a}_y + 70\hat{a}_z)$$

$$= -20.6\hat{a}_x + 34.4\hat{a}_y + 48.1\hat{a}_z \text{ nc/m}^2$$

② From boundary conditions

$$\vec{D}_{N_1} = \vec{D}_{N_2} = 70\hat{a}_z \text{ nc/m}^2$$

③ Also, From boundary conditions.

$$\vec{E}_{t2} = \vec{E}_{t2}$$

$$\text{or, } \frac{\epsilon_{R_1}\epsilon_0 \vec{E}_{t1}}{\epsilon_{R_1}} = \frac{\epsilon_{R_2}\epsilon_0 \vec{E}_{t2}}{\epsilon_{R_2}}$$

$$\text{or, } \frac{\vec{D}_{t1}}{\epsilon_{R_1}} = \frac{\vec{D}_{t2}}{\epsilon_{R_2}}$$

$$\text{or, } \vec{B}_{t2} = \frac{\epsilon_{R_2}}{\epsilon_{R_1}} \vec{B}_{t1} = \frac{2}{3.2} (-30\hat{a}_x + 50\hat{a}_y) \\ = -18.75\hat{a}_x + 31.25\hat{a}_y \text{ nc/m}^2$$

$$\text{i) } \vec{D}_2 = \vec{D}_{N_2} + \vec{D}_{t2} = 70\hat{a}_z - 18.75\hat{a}_x + 31.25\hat{a}_y \\ = -18.75\hat{a}_x + 31.25\hat{a}_y + 70\hat{a}_z \text{ nc/m}^2$$

$$\text{j) } \vec{P}_2 = \kappa_{e_2} \epsilon_0 \vec{E}_2$$

$$\text{or, } \vec{D}_2 = \kappa_{e_2} \epsilon_0 \vec{E}_2$$

$$\text{i.e. } \vec{P}_2 = \frac{\kappa_{e_2}}{\epsilon_{R_2}} \vec{D}_2 \text{ where, } \kappa_{e_2} = \epsilon_{R_2} - 1 = 2 - 1 = 1$$

$$\text{or, } \vec{P}_2 = \frac{1}{2} (-18.75\hat{a}_x + 31.25\hat{a}_y + 70\hat{a}_z)$$

$$= -9.38\hat{a}_x + 15.63\hat{a}_y + 35\hat{a}_z \cdot \text{nc/m}^2$$

$$\text{Again, } \theta_2 = \cos^{-1} \left(\frac{D_{N_2}}{D_2} \right) = \cos^{-1} \left(\frac{70}{\sqrt{(-18.75)^2 + (31.25)^2 + (70)^2}} \right) = 227.5^\circ$$

14.4 Qn: The region $z < 0$ contains a dielectric material for which $\epsilon_{r2} = 4$.

$E_r1 = 2.5$ while the region $z > 0$ is characterized by $\epsilon_{r1} = 4$.
 Let $\vec{E}_1 = -30\hat{a}_x + 50\hat{a}_y + 70\hat{a}_z \text{ V/m}$. Find: ② \vec{E}_2 ③ D_2

④ Polarization in Region 2 (P_2)

[2073 shrawan]

Soln:

$$\vec{E}_1 = -30\hat{a}_x + 50\hat{a}_y + 70\hat{a}_z \text{ V/m.}$$

Since, the boundary of two dielectric medium is at $z = 0$

$$\vec{E}_{N1} = 70\hat{a}_z \text{ V/m.}$$

$$\& \vec{D}_{N1} = \epsilon_{r1}\epsilon_0 \cdot \vec{E}_{N1} = 6.175\hat{a}_z \text{ C/m}^2$$

$$\text{Also, } \vec{E}_{t1} = \vec{E}_1 - \vec{E}_{N1} = -30\hat{a}_x + 50\hat{a}_y \text{ V/m.}$$

$$\& \vec{D}_{t1} = \epsilon_0 \epsilon_{r1} \vec{E}_{t1} = \epsilon_0 (-75\hat{a}_x + 125\hat{a}_y) \text{ C/m}^2.$$

From boundary conditions.

$$\vec{E}_{t2} = \vec{E}_{N1} = -30\hat{a}_x + 50\hat{a}_y \text{ V/m.}$$

$$\text{A/150, } \vec{D}_{N2} = \vec{D}_{N1} = 175\epsilon_0 \hat{a}_z \text{ C/m}^2$$

$$\text{or, } \epsilon_0 \epsilon_{r2} \vec{E}_{N2} = 175 \frac{\epsilon_0}{\epsilon_{r2}} \hat{a}_z$$

$$\text{or, } \vec{E}_{N2} = \frac{175}{4} \hat{a}_z = 43.75\hat{a}_z \text{ V/m}$$

$$\therefore \text{② } \vec{E}_2 = \vec{E}_{t2} + \vec{E}_{N2} = -30\hat{a}_x + 50\hat{a}_y + 43.75\hat{a}_z \text{ V/m.}$$

Again, $\vec{D}_2 = \epsilon_0 \cdot \epsilon_{r2} \vec{E}_2 = 8.85 \times 10^{-12} \times 4 (-30\hat{a}_x + 50\hat{a}_y + 43.75\hat{a}_z)$

$$\text{③ } \vec{D}_2 = 1.062 \hat{a}_x + 1.77 \hat{a}_y + 1.55 \hat{a}_z \text{ nC/m}^2$$

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Now, for polarization, \vec{P}_2

$$\text{we have, } \vec{P}_2 = \kappa_r \epsilon_0 \vec{E}_2 \quad \text{and} \quad \vec{D}_2 = \epsilon_{r_2} \epsilon_0 \vec{E}_2, \quad \chi_{r_2} - 1 = 4 - 1 = 3$$

So,

$$\textcircled{C} \quad \vec{P}_2 = 3 \times 8.85 \times 10^{-12} (-30 \hat{a}_x + 50 \hat{a}_y + 48.75 \hat{a}_z) \\ = -0.796 \hat{a}_x + 1.327 \hat{a}_y + 1.161 \hat{a}_z \text{ nC/m}^2$$

Qn: The region $x < 0$ is composed of a uniform dielectric material for which $\epsilon_{r_1} = 3.2$, while the region $x > 0$ is characterized by $\epsilon_{r_2} = 2$. The electric flux density at region $x < 0$ is $\vec{D}_1 = -30 \hat{a}_x + 50 \hat{a}_y + 70 \hat{a}_z \text{ nC/m}^2$. Then find polarization (\vec{P}) and electric field intensity (\vec{E}) in both regions. [$\vec{P}_1, \vec{P}_2, \vec{E}_1 \& \vec{E}_2 = ?$] [2068 cbutra]

Sol:

$$\text{Given, } \vec{D}_1 = -30 \hat{a}_x + 50 \hat{a}_y + 70 \hat{a}_z \text{ nC/m}^2 \quad \epsilon_{r_1} = 3.2 \quad \epsilon_{r_2} = 2$$

Since, the boundary of two dielectrics is in $x=0$ plane

$$\vec{D}_{H1} = -30 \hat{a}_x \text{ nC/m}^2, \quad = \vec{D}_{H2}$$

$$\text{So, } \vec{E}_{H1} = \frac{\vec{D}_{H1}}{\epsilon_{r_1} \epsilon_0} = \frac{-30 \times 10^{-9} \hat{a}_x}{3.2 \times 8.85 \times 10^{-12}} = -1059 \hat{a}_x \text{ V/m.} \quad \times < 0$$

$$\text{Also, } \vec{E}_1 = \frac{\vec{D}_1}{\epsilon_{r_1} \epsilon_0} = \frac{(-30 \hat{a}_x + 50 \hat{a}_y + 70 \hat{a}_z) \times 10^{-9}}{3.2 \times 8.85 \times 10^{-12}} \\ = -1059 \hat{a}_x + 1765 \hat{a}_y + 2471 \hat{a}_z \text{ V/m}$$

Again,

$$\chi_{r_1} - 1 = \epsilon_{r_1} - 1 = 2.2$$

$$\textcircled{*} \quad \vec{P}_1 = \frac{\kappa_{r_1}}{\epsilon_{r_1}} \vec{D}_1 = \frac{2.2}{3.2} (-30 \hat{a}_x + 50 \hat{a}_y + 70 \hat{a}_z) \text{ nC/m}^2 \\ = -20.625 \hat{a}_x + 34.4 \hat{a}_y + 48.1 \hat{a}_z \text{ nC/m}^2$$

$$\text{Now, } \vec{E}_{r_1} = \vec{E}_1 - \vec{E}_{H1} = 1765 \hat{a}_y + 2471 \hat{a}_z \text{ V/m.}$$

From boundary conditions,

$$\vec{E}_{t_2} = \vec{E}_{t_1} = 17.65 \hat{a}_y + 24.71 \hat{a}_z \text{ V/m.}$$

$$\text{and, } \vec{E}_{H_2} = \frac{\vec{D}_{H_2}}{\epsilon_{r_2} \epsilon_0} = \frac{-30 \hat{a}_x - 10^{-9}}{2 \times 8.85 \times 10^{-12}} = -1694.92 \hat{a}_x \text{ V/m.}$$

$$\therefore \vec{E}_2 = \vec{E}_{t_2} + \vec{E}_{H_2} = -1695 \hat{a}_x + 17.65 \hat{a}_y + 24.71 \hat{a}_z \text{ V/m.}$$

Now,

$$\vec{P}_2 = \chi_{e_2} \epsilon_0 \vec{E}_2 \quad \text{where, } \chi_{e_2} = \epsilon_{r_2} - 1 = 2 - 1 = 1$$

$$\therefore \vec{P}_2 = 1 \times 8.85 \times 10^{-12} (-1695 \hat{a}_x + 17.65 \hat{a}_y + 24.71 \hat{a}_z) \\ = -15 \hat{a}_x + 15.62 \hat{a}_y + 21.87 \hat{a}_z \text{ nC/m}^2$$

(iii): Use boundary condition to find \vec{E}_2 in the medium 2 with boundary located at plane $z=0$. Medium 1 is perfect dielectric characterized by $\epsilon_{r_1}=2.5$, medium 2 is perfect dielectric characterized by $\epsilon_{r_2}=5$, electric field in medium 1 is $\vec{E}_1 = \hat{a}_x + 3 \hat{a}_y + 3 \hat{a}_z \text{ V/m.}$ [2069 Ashad]

$$\begin{aligned} \vec{D}_{H_2} &= \vec{D}_{H_1}, \quad \vec{E}_{t_2} = \vec{E}_{t_1} \\ \therefore \vec{E}_{H_2} &= \frac{\epsilon_{r_2} \epsilon_0}{\epsilon_{r_1} \epsilon_0} \cdot \vec{D}_{H_1} \\ \therefore \vec{E}_2 &= \vec{E}_{t_2} + \vec{E}_{H_2} \end{aligned}$$

(iv): Consider the region $y < 0$ be composed of a uniform dielectric material for which the relative permittivity (ϵ_{r_2}) is 3.2 while the region $y > 0$ is characterized by $\epsilon_{r_2} = 2$. Let the flux density in region 1 be $\vec{D}_1 = -30 \hat{a}_x + 50 \hat{a}_y + 70 \hat{a}_z \text{ nC/m}^2$. Find: (a) Magnitude of flux density (D_2) & electric field intensity at region 2 (E_2) (b) Polarization in region 1 & 2 (P_1 & P_2)

$$\text{Soln: } \chi_{e_1} = \epsilon_{r_1} - 1, \quad \chi_{e_2} = \epsilon_{r_2} - 1 \quad \vec{P}_2 = \frac{\epsilon_{r_2} - 1}{\epsilon_{r_1}} \vec{D}_1, \quad \vec{P}_2 = \frac{\epsilon_{r_2} - 1}{\epsilon_{r_2}} \vec{D}_2$$

Boundary Value Problems

The procedure for determining the electric field \vec{E} are defined in many ways; using graphical plotting, Coulomb's law, Gauss's law when charge distribution is known; or using $\vec{E} = -\nabla V$ when the potential V is known throughout the region. In most practical situations, however, neither the charge distribution nor the potential distribution is known. So, for practical situations there will be only electrostatic conditions (charge & potential) at some boundaries are known and it is desired to find \vec{E} & V throughout the region. Such problems are usually solved using Poisson's or Laplace's equation or the image method, and they are usually referred to as boundary value problems.

Poisson's and Laplace's Equation

Poisson's and Laplace's equations are easily derived from Gauss's law (for a linear material medium). From point form of Gauss's Law or Maxwell's first equation,

$$\nabla \cdot \vec{D} = \rho_v \quad \text{--- (a)}$$

again, we have from definition of \vec{D}

$$\vec{D} = \epsilon \vec{E}$$

and gradient relationship is,

$$\vec{E} = -\nabla V$$

Substituting in (a)

$$\nabla \cdot (\epsilon \vec{E}) = \rho_v$$

$$\text{or, } \nabla \cdot [\epsilon (-\nabla V)] = \rho_v$$

(14)

$$\text{or } \nabla \cdot \nabla V = -\frac{\rho_V}{\epsilon}$$

This is a Poisson's Equation; where ϵ is constant for homogeneous region.

Again, from definition of gradient & divergence, we get

$$\begin{aligned} \nabla \cdot \vec{A} &= \frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z} \\ \&\nabla V = \frac{\partial V}{\partial x} \hat{a}_x + \frac{\partial V}{\partial y} \hat{a}_y + \frac{\partial V}{\partial z} \hat{a}_z \end{aligned} \quad \left. \begin{array}{l} \text{Cartesian} \\ \text{coordinates.} \end{array} \right\}$$

Therefore,

$$\begin{aligned} \nabla \cdot \nabla V &= \frac{\partial}{\partial x} \left(\frac{\partial V}{\partial x} \right) + \frac{\partial}{\partial y} \left(\frac{\partial V}{\partial y} \right) + \frac{\partial}{\partial z} \left(\frac{\partial V}{\partial z} \right) \\ &= \frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} + \frac{\partial^2 V}{\partial z^2} \\ \text{So, } \nabla \cdot \nabla V &= \nabla^2 V = \frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} + \frac{\partial^2 V}{\partial z^2} = -\frac{\rho_V}{\epsilon} \end{aligned}$$

If $\rho_V = 0$, indicating zero volume charge density, but allowing point charges, line charges, and surface charge density to exist at singular locations as sources of the field, then:

$$\boxed{\nabla^2 V = 0}$$

This is the Laplace's Equation. The ∇^2 (del squared) operation is called Laplacian of V . In Cartesian co-ordinates Laplace's Equation is

$$\boxed{\nabla^2 V = \frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} + \frac{\partial^2 V}{\partial z^2} = 0}$$

(149) Similarly, in cylindrical and spherical coordinates the Laplace's Eqn is given as:

$$\text{Cylindrical} - \nabla^2 V = \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial V}{\partial r} \right) + \frac{1}{r^2} \left(\frac{\partial^2 V}{\partial \theta^2} \right) + \frac{\partial^2 V}{\partial z^2} = 0$$

$$\text{Spherical} - \nabla^2 V = \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial V}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial V}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 V}{\partial \phi^2} = 0$$

Laplace's equation is applicable for the region where volume charge density is zero; it states that every conceivable configuration of electrodes or conductors produces the field for which $\nabla^2 V = 0$. All these fields are different, with different potential values and different spatial rates of change, yet for each of them $\nabla^2 V = 0$. To certain boundary conditions we must solve the Laplace's equation.

Every physical problem must contain at least one conducting boundary and usually contains two or more. The potentials on these boundaries are assigned values, perhaps V_0, V_1, \dots , or perhaps numerical values. These definite equipotential surfaces will provide the boundary conditions for the type of problem to be solved.

Example of solution of Laplace's Equation

Let us assume that V is a function of x only and we have to need for boundary conditions to get exact value. So, Laplace's equation reduces to

$$\frac{\partial^2 V}{\partial x^2} = 0$$

(150) and the partial derivative may be replaced by ordinary derivative, since, v is not a function of y & z ,

$$\frac{d^2v}{dx^2} = 0$$

Integrating twice, we get

$$\frac{dv}{dx} = c_1$$

$$\text{and } v = c_1 x + c_2$$

where, c_1 & c_2 are constants of integration and are determined from boundary conditions.

let $v = v_0$ at $x = x_0$ and $v = v_1$ at $x = x_1$, then

$$v_0 = c_1 x_0 + c_2 \quad v_1 = c_1 x_1 + c_2$$

$$\text{so, } c_1 = \frac{v_0 - v_1}{x_0 - x_1} \quad c_2 = \frac{v_1 x_0 - v_0 x_1}{x_0 - x_1}$$

$$\text{and } v = \frac{v_0(x - x_1) - v_1(x - x_0)}{x_0 - x_1}$$

If we assume a simple boundary condition as:

$v = 0$ at $x = 0$ & $v = v_0$ at $x = d$ then

$$c_1 = \frac{v_0}{d} \quad c_2 = 0$$

$$\text{and } v = \frac{v_0 x}{d}$$

15.1

Uniqueness Theorem - If a solution to Laplace's equation can be found that satisfies the boundary conditions, then the solution is unique.

Ay solution of Laplace's Equation which satisfies the same boundary conditions must be the only solution regardless of the method used. This is known as the uniqueness theorem. The theorem applies to any solution of Poisson's or Laplace's equation in a given region or closed surface.

The theorem is proved by contradiction.

Proof:

Let us assume that we have two solutions of Laplace's equation, V_1 & V_2 , both are general functions of the coordinates used. Therefore,

$$\nabla^2 V_1 = 0$$

$$\text{and } \nabla^2 V_2 = 0$$

from which, we get

$$\nabla^2 (V_1 - V_2) = 0$$

Each solution must also satisfy the boundary conditions and if we assume the given potential values on the boundary are by V_b then the value of V_1 on the boundary V_{1b} and the value of V_2 on the boundary V_{2b} must both be identical to V_b ,

$$V_{1b} = V_{2b} = V_b$$

$$\text{or, } V_{1b} - V_{2b} = 0$$

From vector identity

$$\nabla \cdot (\nabla \vec{B}) = \nabla (\nabla \cdot \vec{B}) + \vec{B} \cdot (\nabla \nabla)$$

which holds for any scalar V and any vector \vec{B} .

(152) For present condition we assume $v_1 - v_2$ as the scalar & $\nabla(v_1 - v_2)$ as the vector, resulting

$$\nabla \cdot [(v_1 - v_2) \nabla(v_1 - v_2)] = (v_1 - v_2) (\nabla \cdot \nabla(v_1 - v_2)) +$$

$$\nabla(v_1 - v_2) \cdot \nabla(v_1 - v_2)$$

Integrating throughout the volume enclosed by the boundary surfaces specified:

$$\begin{aligned} & \int_{\text{vol.}} \nabla \cdot [(v_1 - v_2) \nabla(v_1 - v_2)] d\tau + \int_{\text{vol.}} \nabla(v_1 - v_2) \cdot \nabla(v_1 - v_2) d\tau \\ &= \int_{\text{vol.}} (v_1 - v_2) [\nabla \cdot \nabla(v_1 - v_2)] d\tau + \int_{\text{vol.}} [\nabla(v_1 - v_2)]^2 d\tau \end{aligned}$$

From divergence theorem we can replace the volume integral on the left side of the equation by the closed surface integral over the surface surrounding the volume. This surface consists of the boundaries already specified on which $v_{1b} = v_{2b}$ and therefore.

$\int_{\text{vol.}} \nabla \cdot [(v_1 - v_2) \nabla(v_1 - v_2)] d\tau = \int_S (v_{1b} - v_{2b}) \nabla(v_{1b} - v_{2b}) \cdot d\vec{s} = 0$

One of the factors of the first integral on the right side of above equation is $\nabla \cdot \nabla(v_1 - v_2)$ or $\nabla^2(v_1 - v_2)$, which is zero by hypothesis, and therefore that integral is zero. Hence, the remaining integral must be zero.

$$\int_{\text{vol.}} [\nabla(v_1 - v_2)]^2 d\tau = 0$$

There are two reasons for an integral to be zero; either the integral (the quantity under the integral sign) is

(153) everywhere zero, or the integrand is positive in some regions and negative in others, and the contributions cancel algebraically. In this case, the first reason must hold because $\nabla(V_1 - V_2)]^2$ can not be negative. Therefore

$$[\nabla(V_1 - V_2)]^2 = 0$$

$$\text{and } \nabla(V_1 - V_2) = 0$$

Finally, if the gradient of $V_1 - V_2$ is everywhere zero, then $V_1 - V_2$ cannot change with any co-ordinates and

$$V_1 = V_2 = \text{constant}.$$

The constant is evaluated by considering a point on the boundary. Here, $V_1 - V_2 = V_{1b} - V_{2b} = 0$ & we see that the constant is zero and therefore

$$V_1 = V_2$$

giving two identical solutions. It is applied to Poisson's equation also, where $\nabla^2 V_1 = -\frac{\rho_V}{\epsilon}$ & $\nabla^2 V_2 = -\frac{\rho_V}{\epsilon}$ when $\nabla^2(V_1 - V_2) = 0$ as before (Laplace's equation).

Capacitance of parallel plate capacitor

रैल्फ एन्ड लेट

Capacitance is given by the ratio of charge to potential difference. The potential difference is fixed as V_0 by choosing the potential of one plate zero and the other V_0 . The locations of these plates are made as simple as possible by letting $V = 0$ at $x = 0$.

Steps to find Capacitance after choosing $V=0$ at $x=0$.

- ① Given, V , use $\vec{E} = -\nabla V$ to find \vec{E}
- ② Use $\vec{D} = \epsilon \vec{E}$ to find \vec{D}
- ③ Evaluate \vec{D} at either capacitor plate, $\vec{D} = \vec{D}_S = D_N \hat{a}_N$.
- ④ Recognize that $S_S = D_N$
- ⑤ Find Q by a surface integration over the capacitor plate, $Q = \int_S Q ds$.

Then, we will have

$$V = \frac{V_0}{d} x \quad [\text{solution of Laplace's eq?}]$$

$$\vec{E} = -\frac{V_0}{d} \hat{a}_m$$

$$\vec{D} = -\epsilon \frac{V_0}{d} \hat{a}_m$$

$$\vec{D}_S = \vec{D} \Big|_{x=0} = -\epsilon \frac{V_0}{d} \hat{a}_m \quad \text{and} \quad \hat{a}_m = \hat{a}_x$$

$$D_N = -\epsilon \frac{V_0}{d} = S_S$$

$$Q = S_S - \frac{\epsilon V_0}{d} S_S = -\epsilon \frac{V_0 S}{d}$$

and the capacitance is

$$C = \frac{1/2}{V_0} = \frac{\epsilon S}{d}$$

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Capacitance of Co-axial Cable

Let us consider a cylindrical co-axial cable filled with dielectric of permittivity ϵ in between two cylindrical conductor plates.

Let 'a' be the radius of inner conductor where the potential $V = V_0$ at $p = a$ and 'b' be the radius of the outer conductor where the potential $V = 0$ at $p = b$ ($b > a$).

From the figure, we can see that the variation of potential is seen only in p direction. so, from laplace equation.

$$\nabla^2 V = 0$$

$$\text{or, } \frac{1}{p} \frac{\partial}{\partial p} \left(p \frac{\partial V}{\partial p} \right) + \frac{1}{p^2} \frac{\partial^2 V}{\partial \phi^2} + \frac{\partial^2 V}{\partial z^2} = 0$$

$$\text{As } \frac{1}{p^2} \frac{\partial^2 V}{\partial \phi^2} = 0 \text{ & } \frac{\partial^2 V}{\partial z^2} = 0$$

we have,

$$\frac{1}{p} \frac{\partial}{\partial p} \left(p \frac{\partial V}{\partial p} \right) = 0$$

$$\text{or, } \frac{1}{p} \frac{d}{dp} \left(p \frac{\partial V}{\partial p} \right) = 0 \quad [\text{from ordinary derivative}]$$

$$\text{or, } \frac{d}{dp} \left(p \frac{\partial V}{\partial p} \right) = 0$$

Integrating both sides w.r.t. p

$$p \frac{\partial V}{\partial p} = C_1$$

$$(156) \text{ or, } \frac{dV}{dp} = C_1$$

Again, Integrating both sides w.r.t. p , we get

$$V = C_1 \ln(p) + C_2$$

Now, using boundary conditions $V=V_0$ at $p=a$ & $V=0$ at $p=b$ for $b>a$. Then

$$V_0 = C_1 \ln(a) + C_2 \quad 0 = C_1 \ln(b) + C_2$$

$$V_0 = C_1 \ln(\frac{a}{b})$$

$$\text{Or, } C_1 = \frac{V_0}{\ln(\frac{a}{b})}$$

$$\text{Again, } C_2 = -\frac{\ln(b) \cdot V_0}{\ln(\frac{a}{b})}$$

$$\begin{aligned} \text{Therefore, } V &= \frac{V_0}{\ln(\frac{a}{b})} \cdot \ln(p) - \frac{\ln(b) \cdot V_0}{\ln(\frac{a}{b})} \\ &= \frac{V_0 \ln(\frac{p}{b})}{\ln(\frac{a}{b})} \\ \therefore V &= \boxed{\frac{V_0 \ln(\frac{p}{b})}{\ln(\frac{b}{a})}} \end{aligned}$$

$$\text{Now, } \vec{E} = -\nabla V = \frac{V_0}{p} \cdot \frac{1}{\ln(\frac{b}{a})} \hat{ap}$$

$$D_{\text{in}}(r=a) = \frac{\epsilon V_0}{a \ln(b/a)}$$

$$\therefore C = \frac{\epsilon V_0 2\pi aL}{a \ln(b/a)}$$

$$\therefore C = \boxed{\frac{2\pi \epsilon L}{\ln(b/a)}}$$

Capacitance of Spherical Capacitor

Let us assume a spherical capacitor with inner plate of radius a & potential difference $V = V_b$ at $r=a$ and outer plate of radius b & potential difference $V=0$ at $r=b$. ($b>a$). Then, from Laplace's Eqn:

$$\nabla^2 V = 0$$

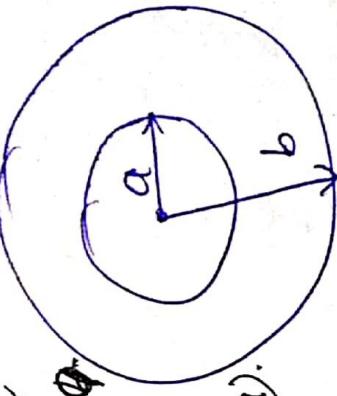
$$\text{or, } \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial V}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial V}{\partial r} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 V}{\partial \phi^2} = 0$$

As, V only varies with r .

$$\text{or, } \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial V}{\partial r} \right) = 0$$

$$\text{or, } \frac{d}{dr} \left(r^2 \frac{\partial V}{\partial r} \right) = 0$$

Integrating twice we get



$$\frac{dV}{dx} = \frac{C_1}{x^2}$$

$$\text{or, } V = -\frac{C_1}{x} + C_2$$

Now, using boundary conditions, we get

$$V = V_0 \frac{\frac{1}{x} - \frac{b}{a}}{\frac{1}{a} - \frac{1}{b}}$$

$$\text{For capacitance, } C = \frac{4\pi\epsilon}{\frac{1}{a} - \frac{1}{b}}$$

Example of solution of Poisson's Equation

Let us assume the p-n junction between two halves of a semi-conductor bar extending in the x -dir. Assuming the region for $x < 0$ is doped p-type and that region for $x > 0$ is n-type and the degree of doping is identical on each side of the junction. Then, the charge distribution is given as

$$\rho_V = 2\rho_{V_0} \operatorname{sech} \frac{\pi}{a} \tan h \frac{\pi}{a}$$

which has a maxm charge density ρ_{V_0} at $x=0$ that occurs at $x=0.881a$. As the maxm charge density is related to the acceptor and donor concentrations N_A & N_D as:

$$\rho_{V_0} = eN_A = eN_D$$

We got from poisson's eqn.

$$\nabla^2 V = -\frac{\rho_V}{\epsilon}$$

Then,

$$\frac{d^2 V}{dx^2} = -\frac{2\rho_{V_0}}{\epsilon} \operatorname{sech}^2 \frac{\pi}{a} \tanh \frac{\pi}{a}$$

1.5.9 Integrating both sides.

$$\frac{dv}{dx} = \frac{2\varphi_{v_0} a}{\epsilon} \operatorname{sech}^2 \frac{x}{a} + C_1$$

and obtain the electric field intensity.

$$E_x = -\frac{2\varphi_{v_0} a}{\epsilon} \operatorname{sech} \frac{x}{a} - C_1$$

To evaluate the constant of integration C_1 , we note that no net charge density and no fields can exist far from the junction. Thus, as $x \rightarrow \pm \infty$, E_x must approach zero. Therefore, $C_1 = 0$, and

$$E_x = -\frac{2\varphi_{v_0} a}{\epsilon} \operatorname{sech} \frac{x}{a}$$

Integrating again

$$V = \frac{4\varphi_{v_0} a^2}{\epsilon} \tan^{-1} e^{x/a} + C_2$$

Assuming arbitrarily select our zero reference of potential at the center of the junction, $x=0$

$$0 = \frac{4\varphi_{v_0} a^2}{\epsilon} \cdot \frac{\pi}{4} + C_2$$

and finally

$$V = \frac{4\varphi_{v_0} a^2}{\epsilon} \left(\tan^{-1} e^{x/a} - \frac{\pi}{4} \right)$$

The potential difference V_0 across the junction is obtained from

$$V_0 = V_{x \rightarrow \infty} - V_{x \rightarrow -\infty} = \frac{2\pi \varphi_{v_0} a^2}{\epsilon}$$

Total positive charge is

$$Q = \int_0^{\infty} 2\varphi_{v_0} \operatorname{sech} \frac{x}{a} \tanh \frac{x}{a} dx = 2\varphi_{v_0} a^2.$$

16.9. where, S = area of the junction cross section.

$$\text{then, } \Phi = S \sqrt{2\pi V_0 \epsilon V_0} \quad F.a = \left[\frac{\sqrt{V_0 \epsilon}}{2\pi V_0} \right]$$

Since, total charge is a function of potential difference, we get

$$T = \frac{d\Phi}{dt} = C \frac{dv_0}{dt}$$

$$\therefore C = \frac{d\Phi}{dv_0}$$

Differentiating w.r.t v_0

$$C = \sqrt{\frac{8\pi V_0 \epsilon}{2\pi V_0}} \cdot S = \frac{\epsilon S}{2\pi a}$$