ECE2150J Introduction to Circuits

Chapter 12. Three-Phase Circuits

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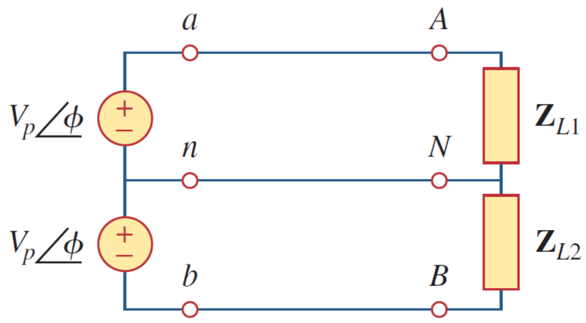
12.1 Introduction

Single phase two wire

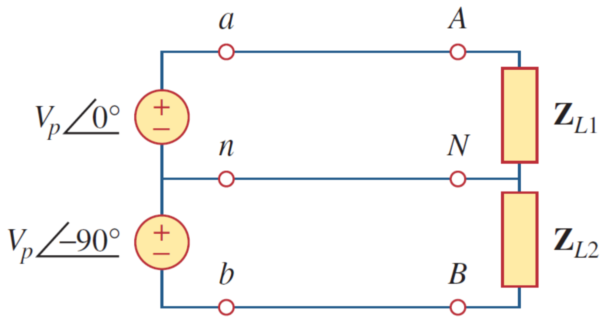


Single phase three wire

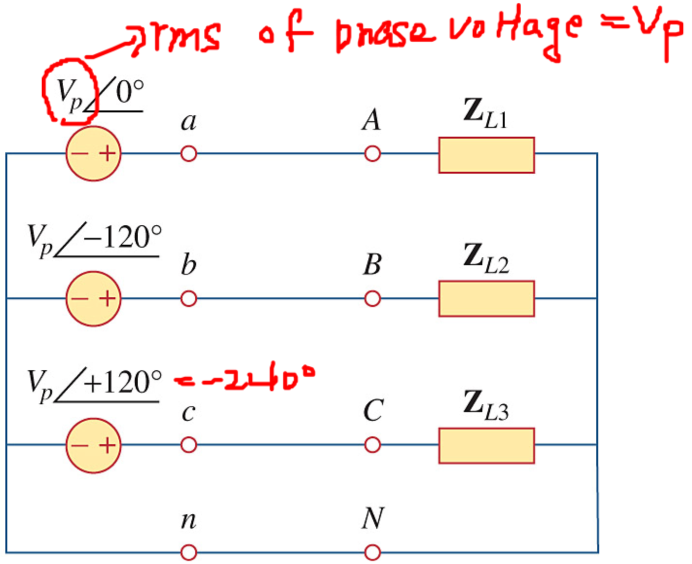
A single-phase ac power system: a generator connected through a pair of wires to a load.

A single-phase three wire system: two identical sources (equal magnitude and the same phase) connected to two loads by two outer wires and the neutral.

Polyphase: AC sources operate at the same frequency but different phases.

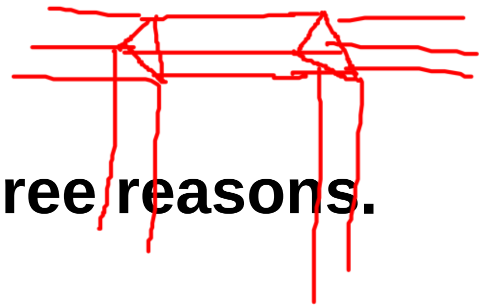


Two-phase three-wire system



Three-phase four-wire system

A three-phase system: Three sources having the same amplitude and frequency but out of phase with each other by 120°. The three-phase system is **by far the most prevalent and most economical polyphase system**.



Three-phase systems are important for at least three reasons.

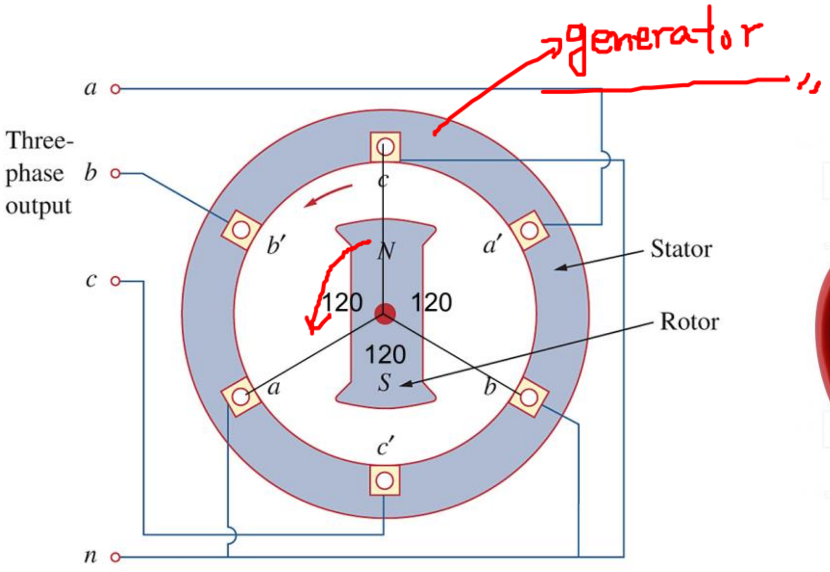
First, nearly all electric power is generated and distributed in three-phase, at the operating frequency of 50 or 60 Hz. **Multiphases** can be generated: from 1-2 to even 48 phases.

Second, the instantaneous power in a three-phase system can be **constant** (not pulsating). This results in uniform power transmission and less vibration of three-phase machines.

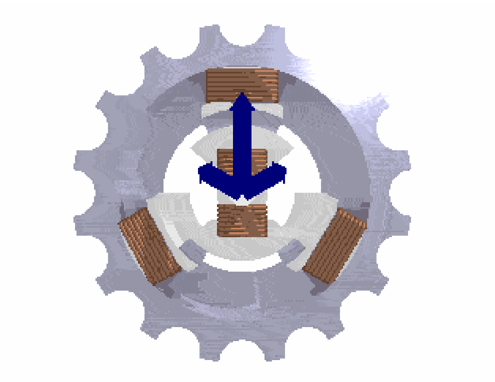
Third, for the same amount of power, the three-phase system is **more economical** than the single phase.

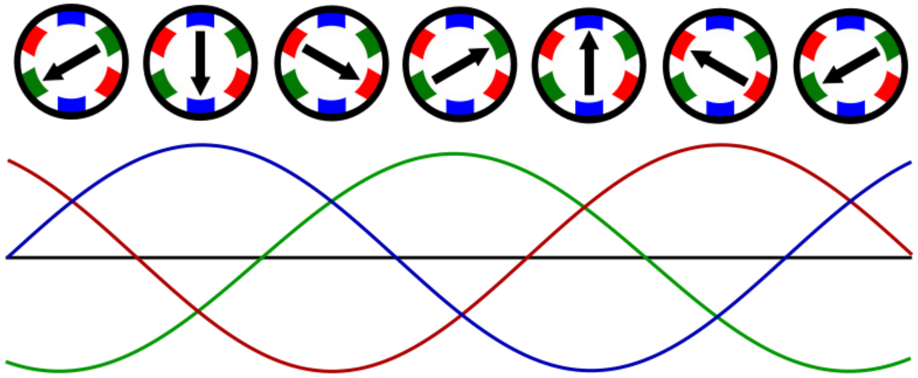
12.2 Balanced Three-Phase Voltages

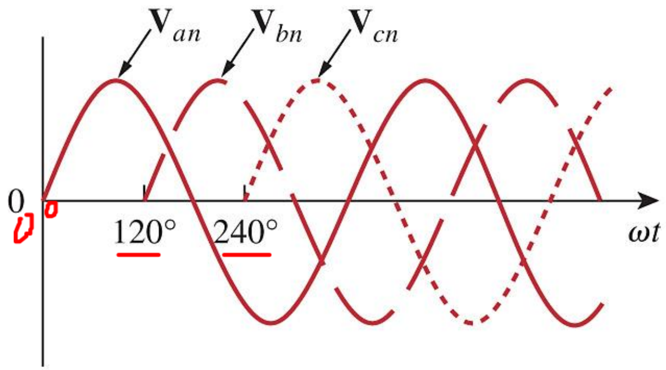
Three-phase voltages are often produced with a three-phase ac generator.



Rotor: a rotating magnet
Stator: a stationary winding







As the rotator rotates, the flux through each coil varies sinusoidally with time, inducing a sinusoidal voltage. Because the coils are placed **120**° apart, the induced voltages are out of phase by **120**°.

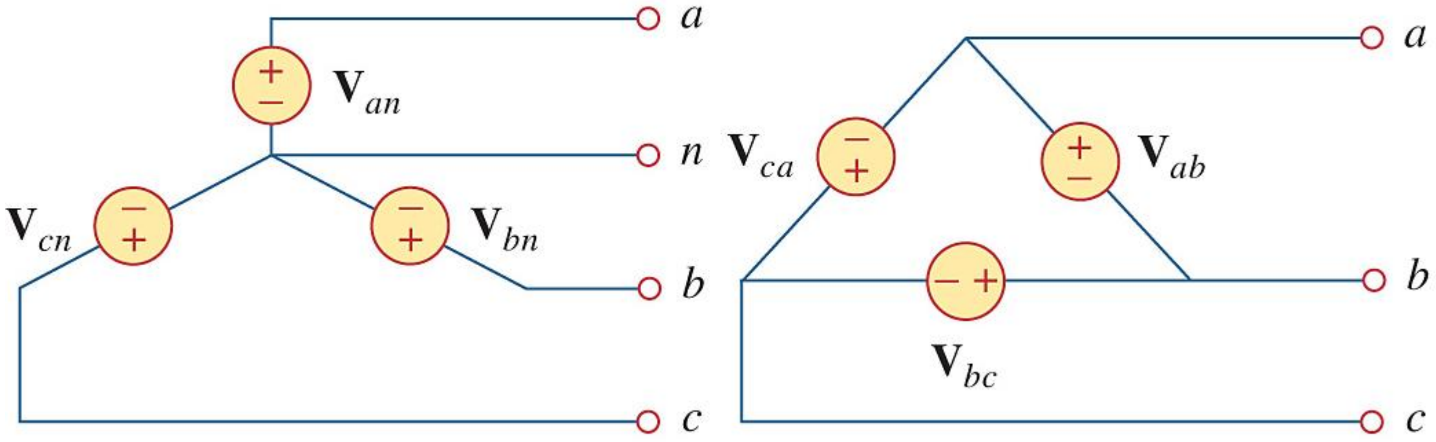
Voltage sources

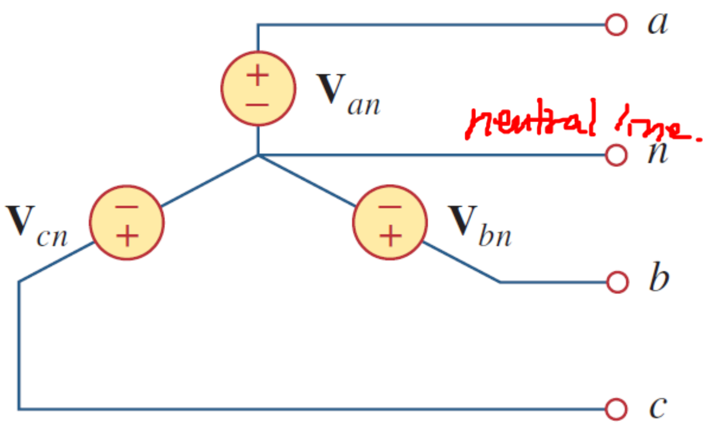
A typical three-phase system consists of three voltage sources connected to loads by three or four wires. A three-phase system is equivalent to three single-phase system. **The voltage sources** can be either **wye- or delta-connected**.

$Z \to Y$ or Δ

Y-Y
Y-Δ
Δ-Y
Δ-Δ

Y Δ





$\mathbf{V}_{an}$, $\mathbf{V}_{bn}$, and $\mathbf{V}_{cn}$ are phase voltages.

V_{ab}, V_{bc}, V_{ac} → line voltages

phase / line currents

I_p I_{ab}

Balanced phase voltages: Equal in magnitude and frequency and are out of phase with each other by 120°. This implies that

(i) $|\mathbf{V}_{an}| = |\mathbf{V}_{bn}| = |\mathbf{V}_{cn}|$

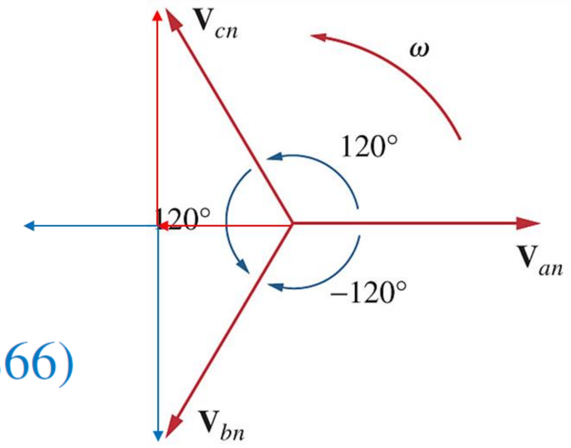
(ii) $\mathbf{V}_{an} + \mathbf{V}_{bn} + \mathbf{V}_{cn} = 0$

−240°

$$= V_p\underline{/0^\circ} + V_p\underline{/-120^\circ} + V_p\underline{/+120^\circ}$$

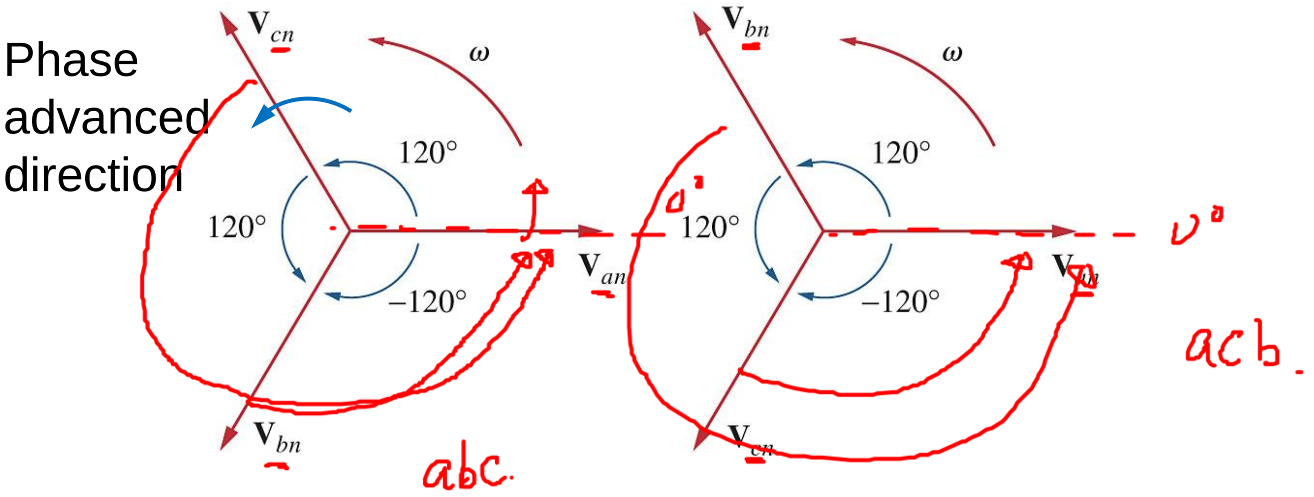
$$= V_p(1.0 - 0.5 - j0.866 - 0.5 + j0.866)$$

$$= 0$$



Phase sequence

abc, acb. 2x2x2 ⇒ 8.



$$\mathbf{V}_{an} = V_p\angle 0^\circ$$
$$\mathbf{V}_{bn} = V_p\angle -120^\circ$$
$$\mathbf{V}_{cn} = V_p\angle -240^\circ = V_p\angle +120^\circ$$

$$\mathbf{V}_{an} = V_p\angle 0^\circ$$
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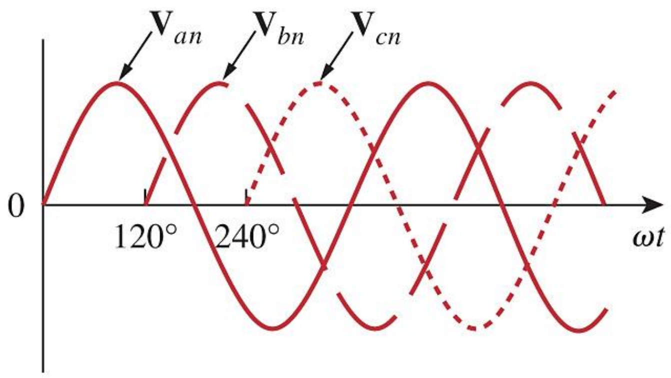
***V_p is the effective (rms)** value of the phase voltage

The phase sequence is the time order in which the voltages pass through their respective maximum values.



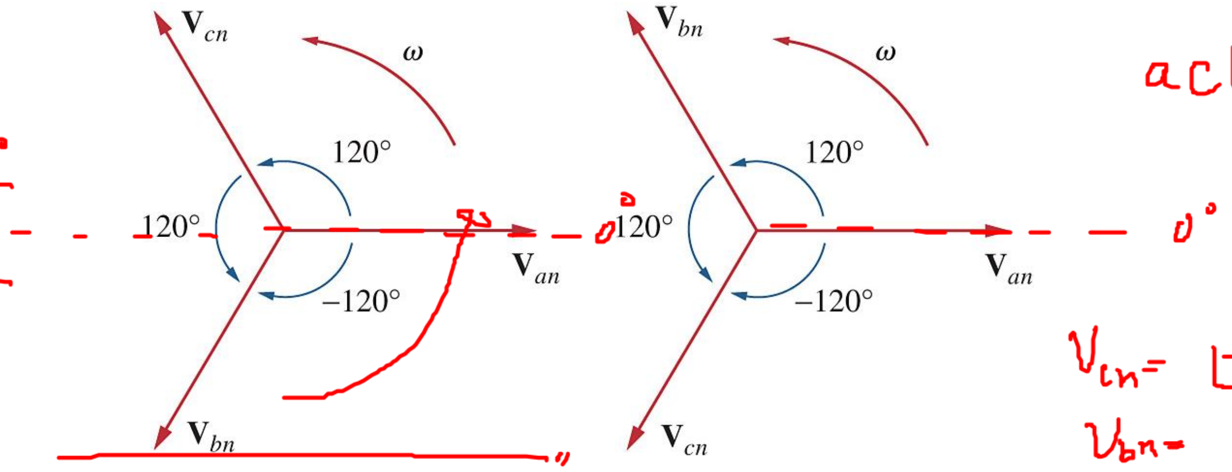
abc: a leads b, b leads c
(i.e., ∠a > ∠ b > ∠c)

abc

$V_{an} = V_p \angle 0^\circ$

$V_{bn} = \angle -120^\circ$

$V_{cn} = \angle -240^\circ$



acb.

$V_{cn} = \angle -120^\circ$

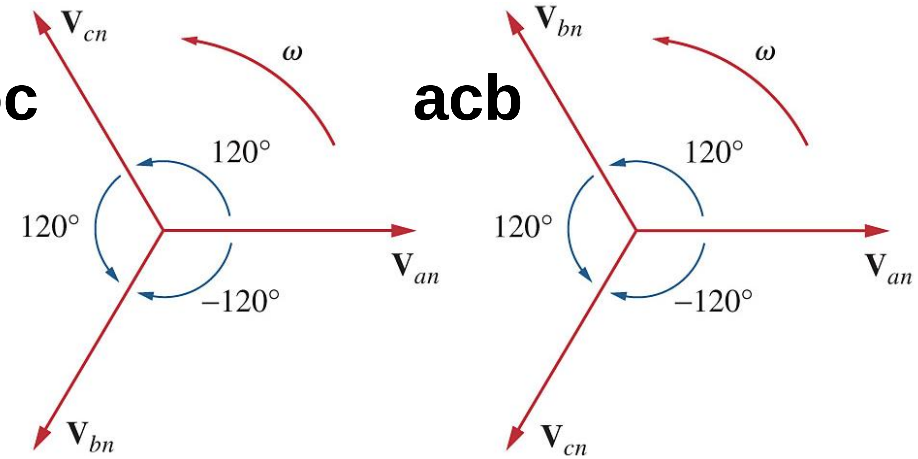
$V_{bn} = \angle -240^\circ$

From which phase the voltage curve above is generated? abc or acb sequence?

The phase sequence is determined **by the order in which the phasors pass through a fixed point** in the phase diagram.

abc

acb



$$\mathbf{V}_{an} = V_p\angle 0^\circ$$
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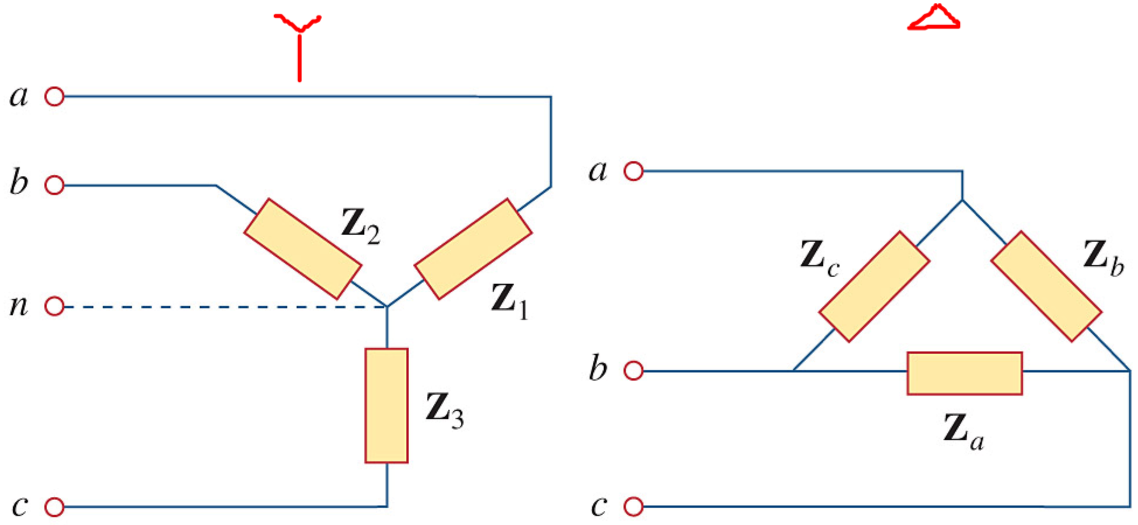
*V_p is the effective (rms) value of the phase voltage

Phase load connection

Similar to the source connections, a three-phase load can be either wye-connected or delta-connected



Balanced Load

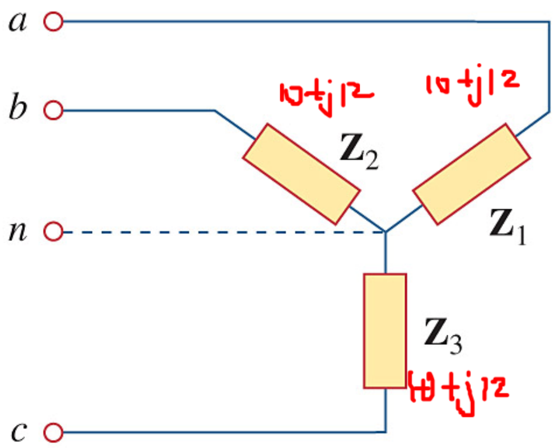
A balanced load is one in which the phase impedances are **equal in magnitude and in phase**.

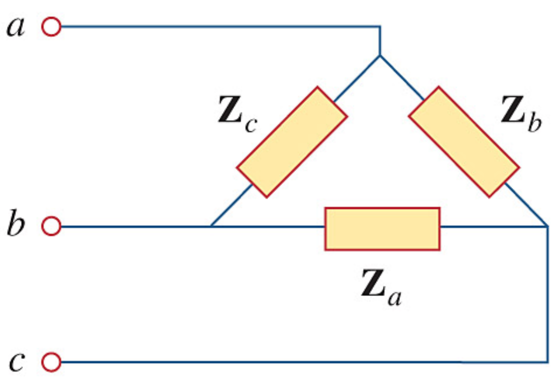
(i) Balanced wye-connected load:

$$\mathbf{Z}_1 = \mathbf{Z}_2 = \mathbf{Z}_3 = \mathbf{Z}_Y$$

(i) Balanced delta-connected load:

$$\mathbf{Z}_a = \mathbf{Z}_b = \mathbf{Z}_c = \mathbf{Z}_\Delta$$





A wye-connected load can be transformed into a delta-connected load, or vice versa.

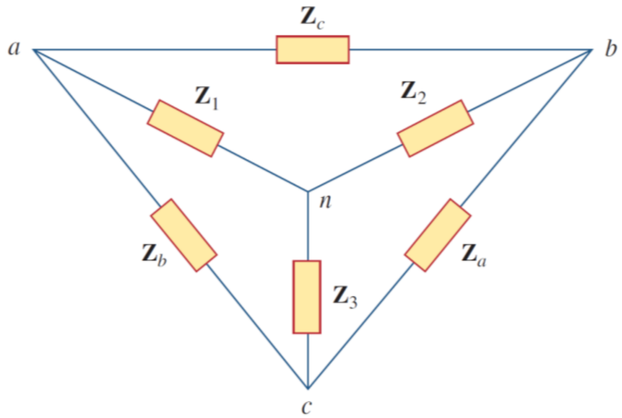
$$\boxed{Z_\Delta = 3Z_Y \text{ or } Z_Y = \frac{1}{3}Z_\Delta}$$

Y-Δ Conversion:

$$\mathbf{Z}_a = \frac{\mathbf{Z}_1\mathbf{Z}_2 + \mathbf{Z}_2\mathbf{Z}_3 + \mathbf{Z}_3\mathbf{Z}_1}{\mathbf{Z}_1}$$

$$\mathbf{Z}_b = \frac{\mathbf{Z}_1\mathbf{Z}_2 + \mathbf{Z}_2\mathbf{Z}_3 + \mathbf{Z}_3\mathbf{Z}_1}{\mathbf{Z}_2}$$

$$\mathbf{Z}_c = \frac{\mathbf{Z}_1\mathbf{Z}_2 + \mathbf{Z}_2\mathbf{Z}_3 + \mathbf{Z}_3\mathbf{Z}_1}{\mathbf{Z}_3}$$



Δ-Y Conversion:

$$\mathbf{Z}_1 = \frac{\mathbf{Z}_b\mathbf{Z}_c}{\mathbf{Z}_a + \mathbf{Z}_b + \mathbf{Z}_c}$$

$$\mathbf{Z}_2 = \frac{\mathbf{Z}_c\mathbf{Z}_a}{\mathbf{Z}_a + \mathbf{Z}_b + \mathbf{Z}_c}$$

$$\mathbf{Z}_3 = \frac{\mathbf{Z}_a\mathbf{Z}_b}{\mathbf{Z}_a + \mathbf{Z}_b + \mathbf{Z}_c}$$

$$\mathbf{Z}_1 = \mathbf{Z}_2 = \mathbf{Z}_3 = \mathbf{Z}_Y$$

$$\mathbf{Z}_a = \mathbf{Z}_b = \mathbf{Z}_c = \mathbf{Z}_\Delta$$

Since both the three-phase source and the three-phase load can be either wye- or delta-connected, we have four possible connections:

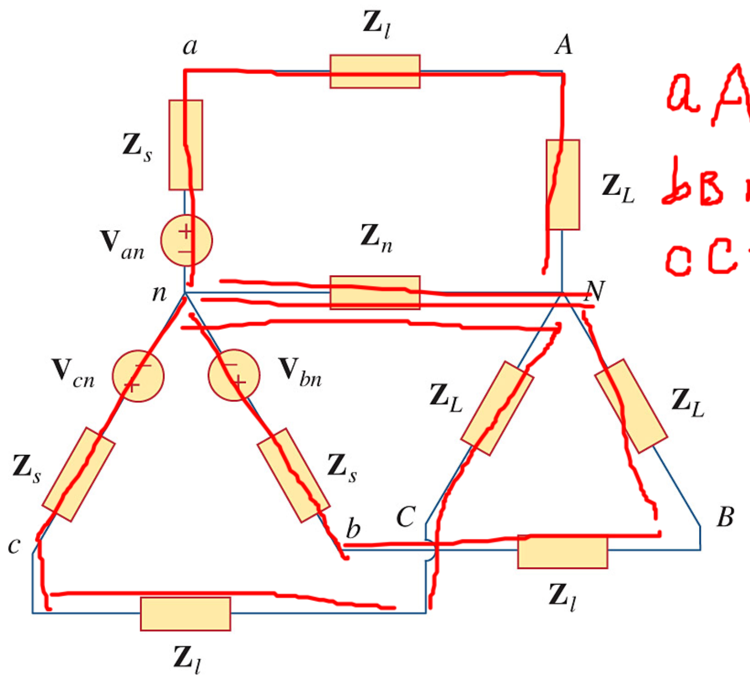
1. Y-Y connection (i.e., Y-connected source with a Y-connected load).
2. Y-Δ connection.
3. Δ-Δ connection.
4. Δ-Y connection.

abc

acb.

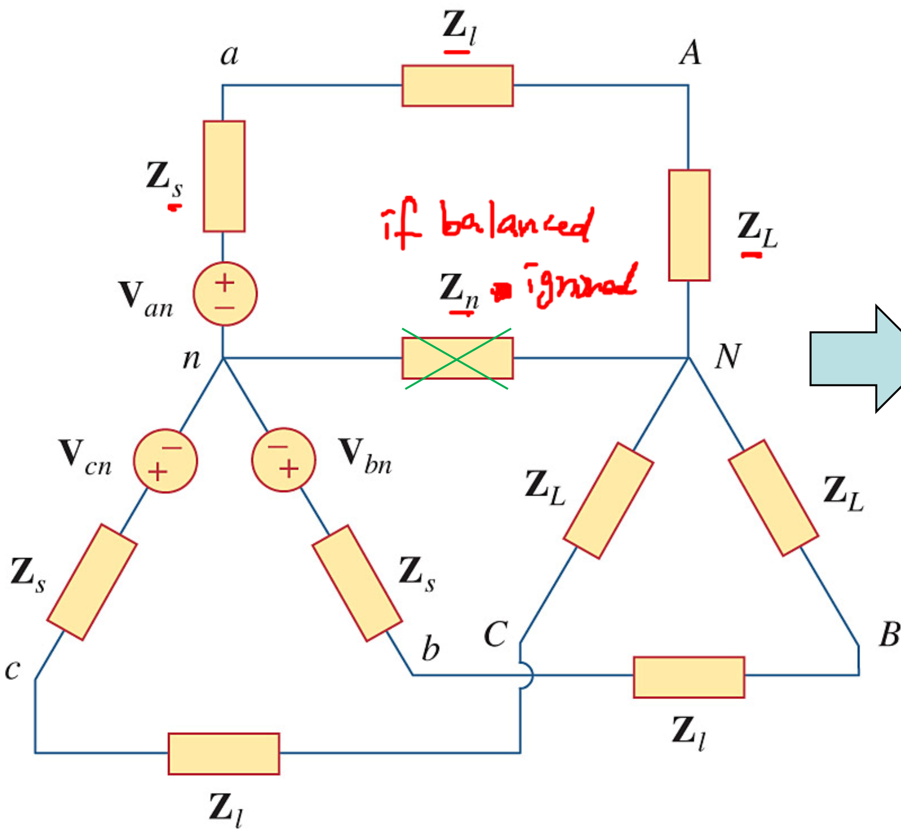
12.3 Balanced Wye-Wye Connection

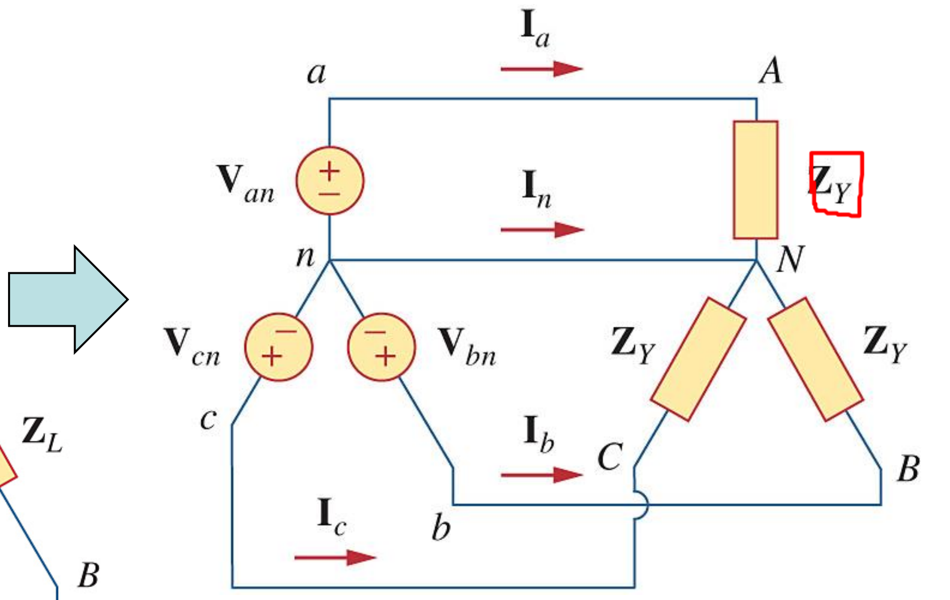
We begin with the Y-Y system, because any balanced three-phase system can be reduced to an equivalent Y-Y system. A balanced Y-Y system is a three-phase system with a balanced Y-connected source and a balanced Y-connected load.



aAn
bBn
cCn.

If balanced, the system can be simplified.

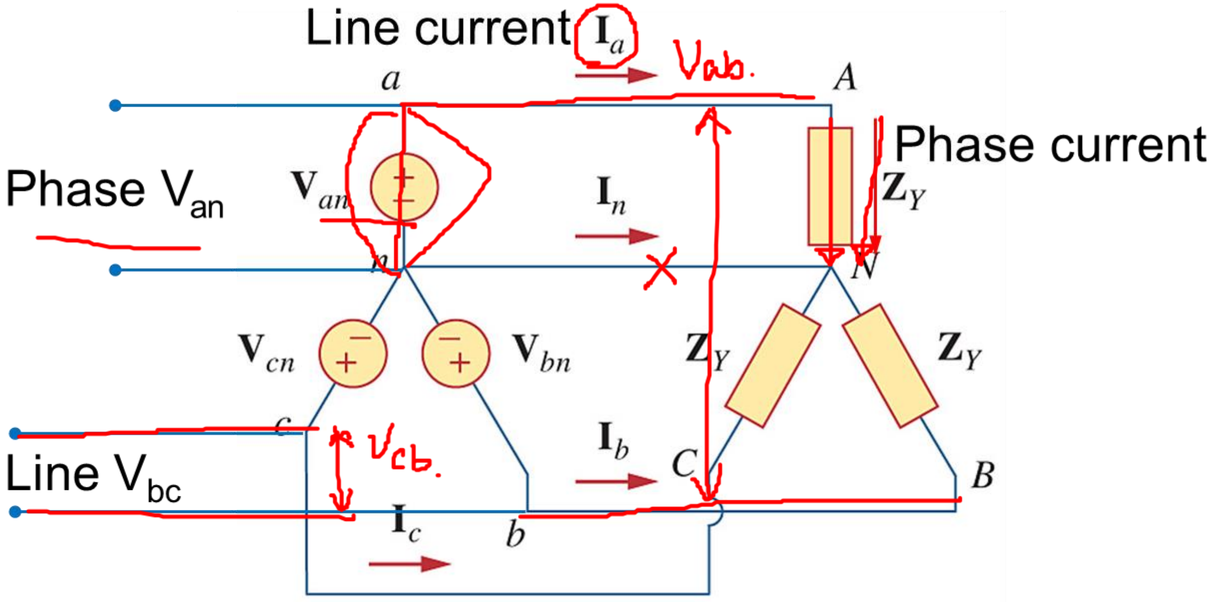


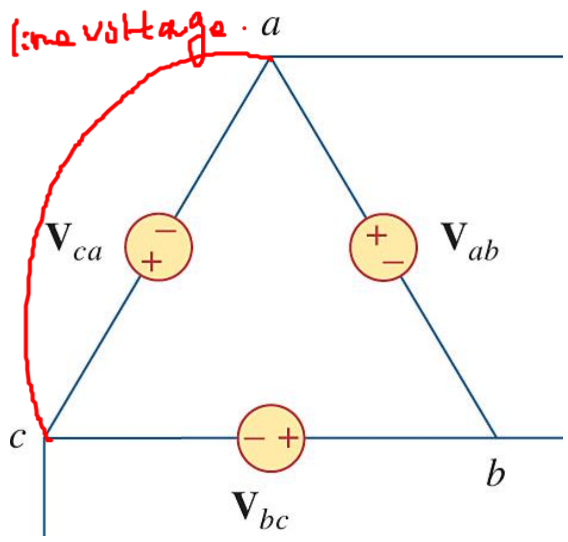


$$\mathbf{Z}_Y = \mathbf{Z}_s + \mathbf{Z}_\ell + \mathbf{Z}_L$$

Phases and Lines?

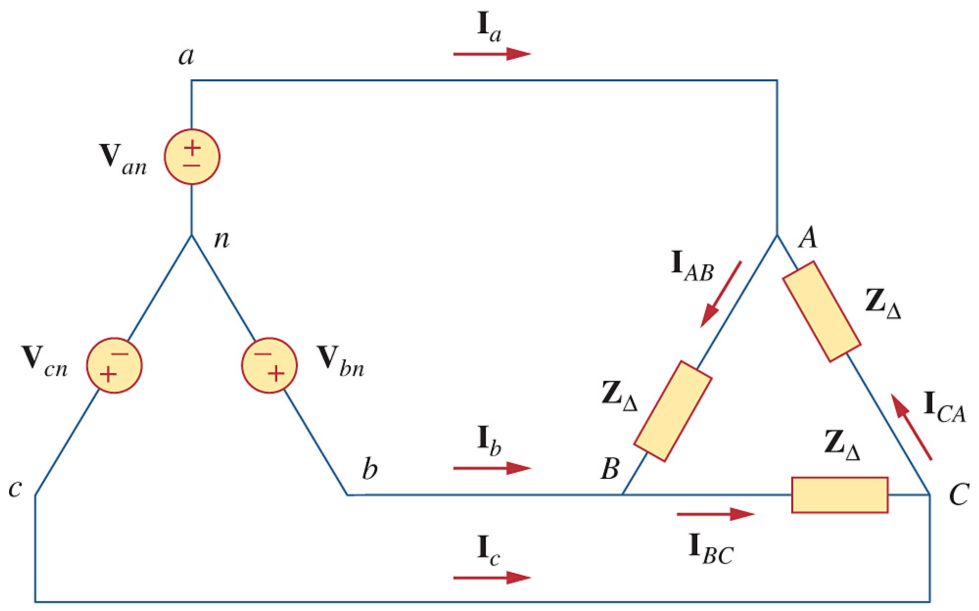
phase vol   phase current
line vol   line current.





The voltage between **any two line** conductors are termed **line voltages** and **the current** that passes along **each line** conductor is termed **a line current**.

Phases are connected **between any pair of line terminals**. **The voltage** appearing across **any phase** is termed a **phase voltage**, and **the current** passing through **any phase** is termed a **phase current**.

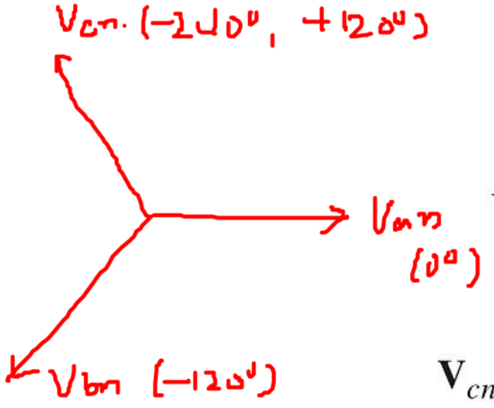


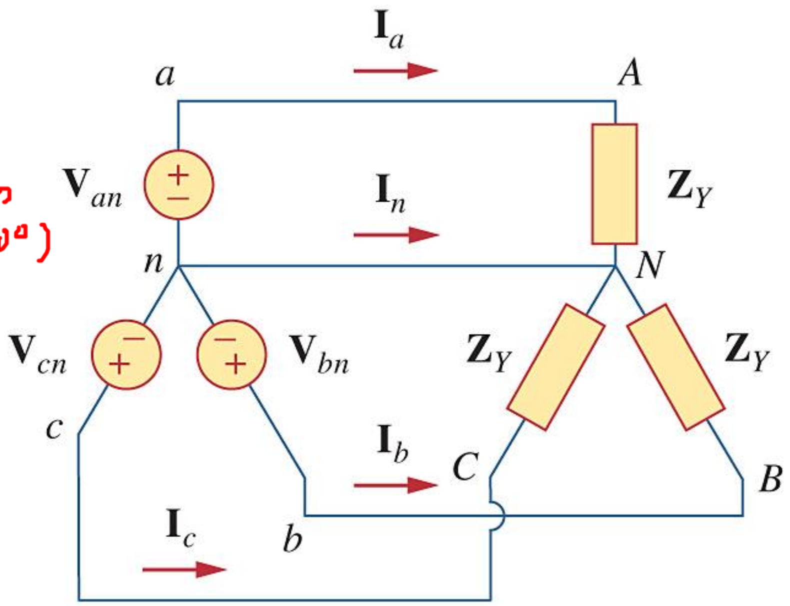
The voltage between **any** **two** **line** conductors are termed **line voltages** and **the current** that passes along **each** **line** conductor is termed **a line current**.

Phases are connected **between any pair of line terminals**. **The voltage** appearing across **any phase** is termed a **phase voltage**, and **the current** passing through **any phase** is termed a **phase current**.

abc.

Assuming the positive sequence, **the phase voltages** (or line-to-neutral voltages) are





rms value phase voltage

$$\tilde{V}_{an} = V_p \angle 0^\circ$$

$$\tilde{V}_{bn} = V_p \angle -120^\circ = V_{an} \angle -120^\circ$$

$$\tilde{V}_{cn} = V_p \angle -240^\circ = V_{an} \angle -240^\circ$$

Balanced source:
Same amplitude and frequency
Out of phase with each other by 120°

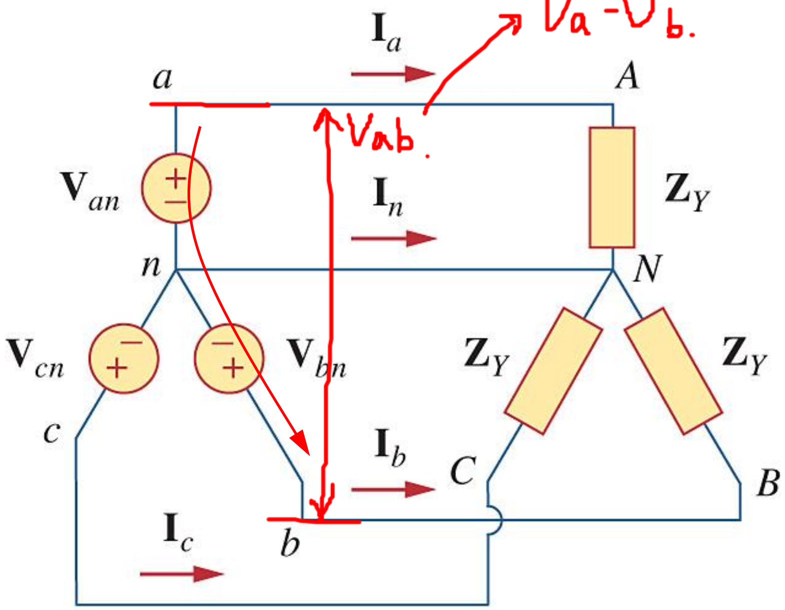
Line voltages

V_{ab}, V_{bc}, V_{ca}

The line voltages (or line-to-line voltages) are

$1.73\ldots\angle 30°$

$V_p\angle 0° - V_p\angle -120° = V_p(1\angle 0° - 1\angle -120°) = \sqrt{3}V_p\angle 30°$



$$\boxed{\tilde{V}_{ab}} = \tilde{V}_{an} - \tilde{V}_{bn} = \sqrt{3}V_p\angle 30°$$

$V_p\angle -120° - V_p\angle -240°$

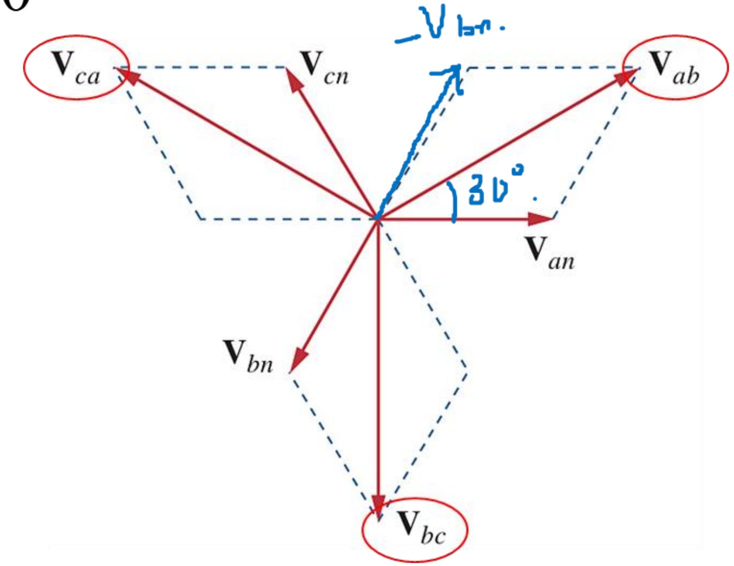
$\sqrt{3}V_p\angle 30°\angle -120°$

V_{ab}

$$\tilde{V}_{bc} = \tilde{V}_{bn} - \tilde{V}_{cn} = \sqrt{3}V_p\angle -90° = \tilde{V}_{ab}\angle -120°$$

$$\tilde{V}_{ca} = \tilde{V}_{cn} - \tilde{V}_{an} = \sqrt{3}V_p\angle -210° = \tilde{V}_{ab}\angle -240°$$

$$\tilde{V}_{ab} + \tilde{V}_{bc} + \tilde{V}_{ca} = 0$$



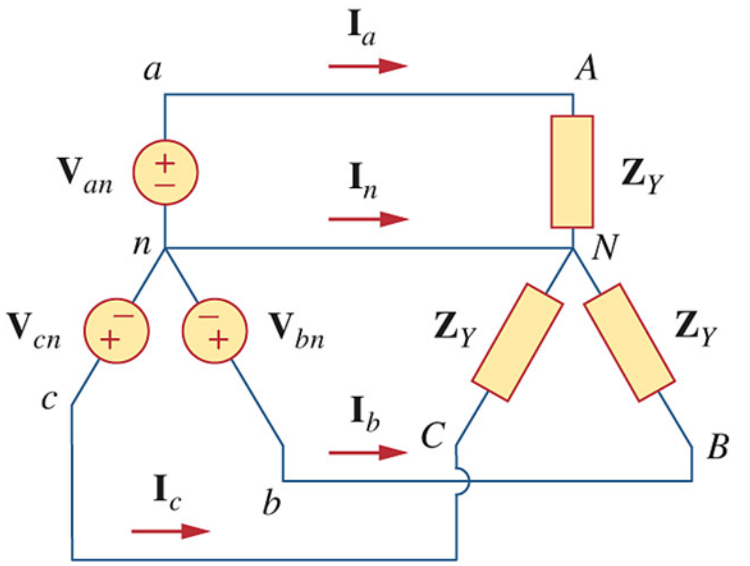
Line voltages are also balanced.

The magnitude of the line voltages is $\sqrt{3}$ times the magnitude of the phase voltages.

$$V_L = \sqrt{3} V_p$$

$$V_p = \left|\widetilde{V}_{an}\right| = \left|\widetilde{V}_{bn}\right| = \left|\widetilde{V}_{cn}\right|$$

$$V_L = \left|\widetilde{V}_{ab}\right| = \left|\widetilde{V}_{bc}\right| = \left|\widetilde{V}_{ca}\right|$$



The line voltages lead their corresponding phase voltages by 30°

$$\tilde{V}_{an} = V_p \angle 0^\circ \qquad \tilde{V}_{ab} = \tilde{V}_{an} - \tilde{V}_{bn} = \sqrt{3} V_p \angle 30^\circ$$

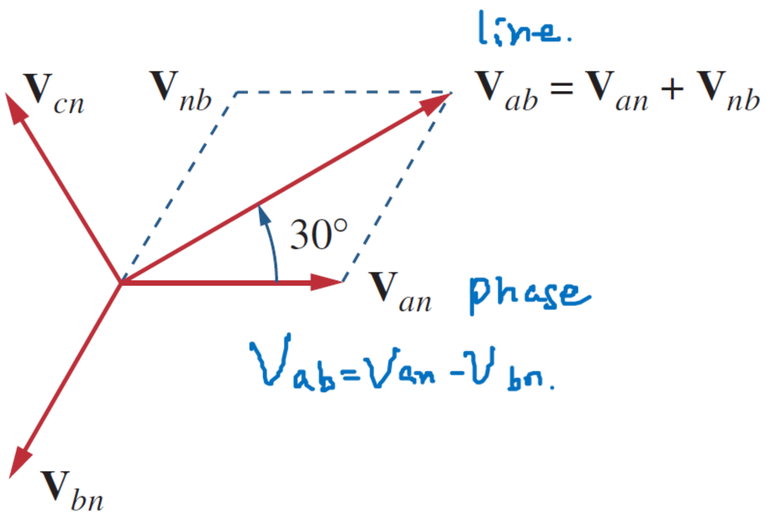
$$\tilde{V}_{bn} = V_p \angle -120^\circ \qquad \tilde{V}_{bc} = \tilde{V}_{bn} - \tilde{V}_{cn} = \sqrt{3} V_p \angle -90^\circ$$

$$\tilde{V}_{cn} = V_p \angle -240^\circ \qquad \tilde{V}_{ca} = \tilde{V}_{cn} - \tilde{V}_{an} = \sqrt{3} V_p \angle -210^\circ$$

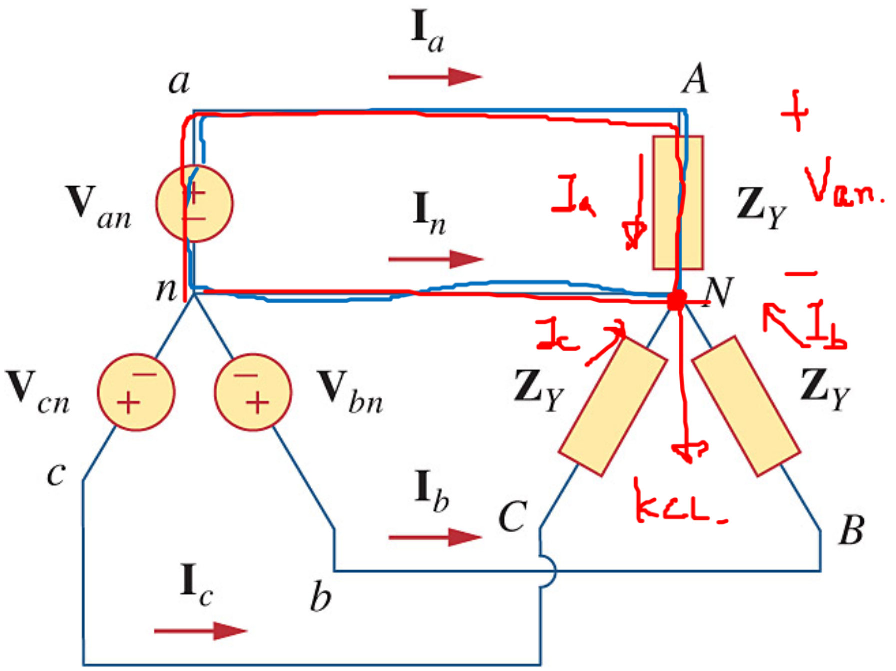
$$\angle \tilde{V}_{ab} = \angle \tilde{V}_{an} + \angle 30^\circ$$

$$\angle \tilde{V}_{bc} = \angle \tilde{V}_{bn} + \angle 30^\circ$$

$$\angle \tilde{V}_{ca} = \angle \tilde{V}_{cn} + \angle 30^\circ$$



Line currents



By KVL at each phase

$$\mathbf{I}_a = \frac{\mathbf{V}_{an}}{\mathbf{Z}_Y},$$

$$\mathbf{I}_b = \frac{\mathbf{V}_{bn}}{\mathbf{Z}_Y} = \frac{\mathbf{V}_{an}\angle -120^\circ}{\mathbf{Z}_Y} = \mathbf{I}_a\angle -120^\circ$$

$$\mathbf{I}_c = \frac{\mathbf{V}_{cn}}{\mathbf{Z}_Y} = \frac{\mathbf{V}_{an}\angle -240^\circ}{\mathbf{Z}_Y} = \mathbf{I}_a\angle -240^\circ$$

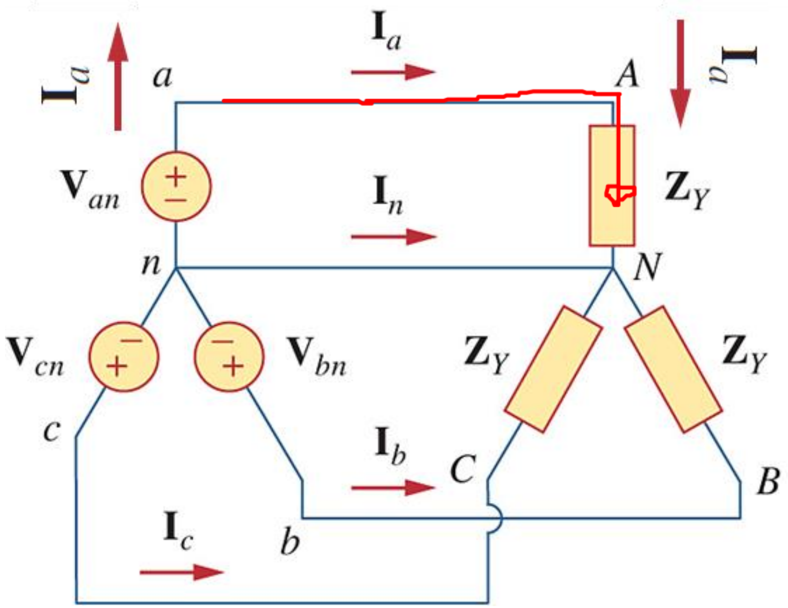
$\Sigma = 0$.

Line currents add up to zero: $\mathbf{I}_a + \mathbf{I}_b + \mathbf{I}_c = 0$

Thus, $\mathbf{I}_n = -(\mathbf{I}_a + \mathbf{I}_b + \mathbf{I}_c) = 0$ and $\mathbf{V}_{nN} = \mathbf{Z}_n \underbrace{\mathbf{I}_n}_{=0.} = 0$

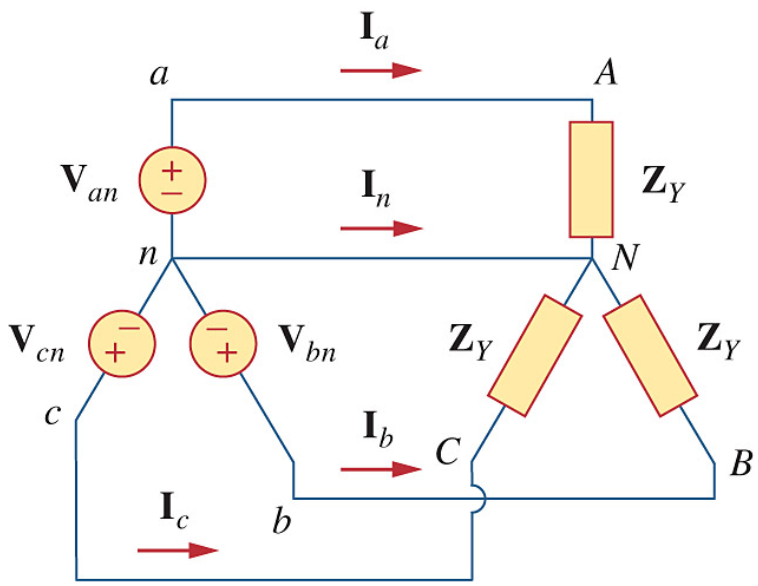
While **the line current** is the current in each line, **the phase current** is the current in each phase of the source or load.

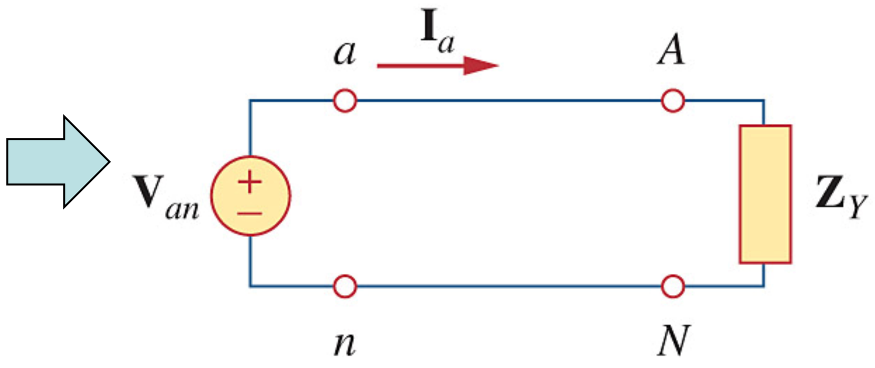
Y-Y → line I = phase I.



In Y-Y connected system, the line current is the same as the phase current.

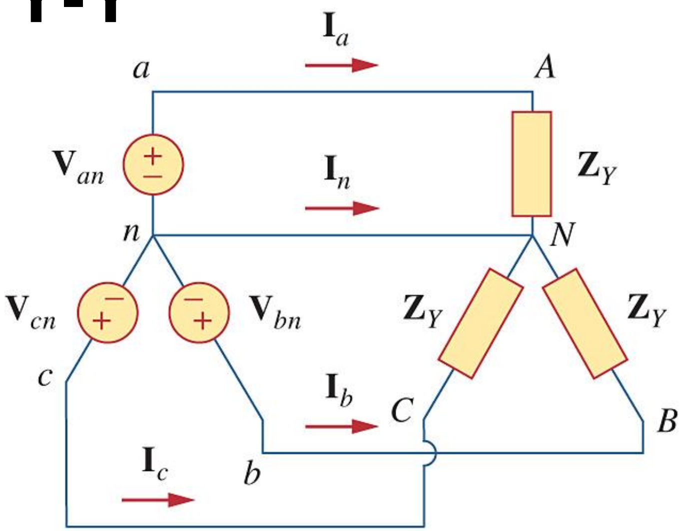
An alternative way of analyzing **a balanced Y-Y system** is to do so on a **per phase basis**.





The single-phase analysis yields the line current $\mathbf{I}_a = \dfrac{\mathbf{V}_{an}}{\mathbf{Z}_Y}$

Summary of balanced Y-Y



Summary of phase and line voltages/currents for balanced three-phase systems.[1]

Connection	Phase voltages/currents	Line voltages/currents
Y-Y	$\mathbf{V}_{an} = V_p\underline{/0^\circ}$	$\mathbf{V}_{ab} = \sqrt{3}V_p\underline{/30^\circ}$
	$\mathbf{V}_{bn} = V_p\underline{/-120^\circ}$	$\mathbf{V}_{bc} = \mathbf{V}_{ab}\underline{/-120^\circ}$
	$\mathbf{V}_{cn} = V_p\underline{/+120^\circ}$	$\mathbf{V}_{ca} = \mathbf{V}_{ab}\underline{/+120^\circ}$
	Same as line currents	$\mathbf{I}_a = \mathbf{V}_{an}/\mathbf{Z}_Y$
		$\mathbf{I}_b = \mathbf{I}_a\underline{/-120^\circ}$
		$\mathbf{I}_c = \mathbf{I}_a\underline{/+120^\circ}$

all are balanced.

abc sequence.

Positive or abc sequence is assumed.

Practice Problem 12.2 A Y-connected balanced three-phase generator with an impedance of $0.4 + j0.3\ \Omega$ per phase is connected to a Y-connected balanced load with an impedance of $24 + j19\ \Omega$ per phase. The line joining the generator and the load has an impedance of $0.6 + j0.7\ \Omega$ per phase. Assuming a positive sequence for the source voltages and that $\tilde{V}_{an} = 120\angle 30°$ V, find the line voltages and the line currents.

Z_s Z_L Z_l

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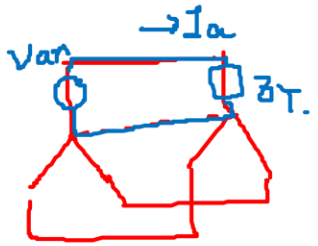
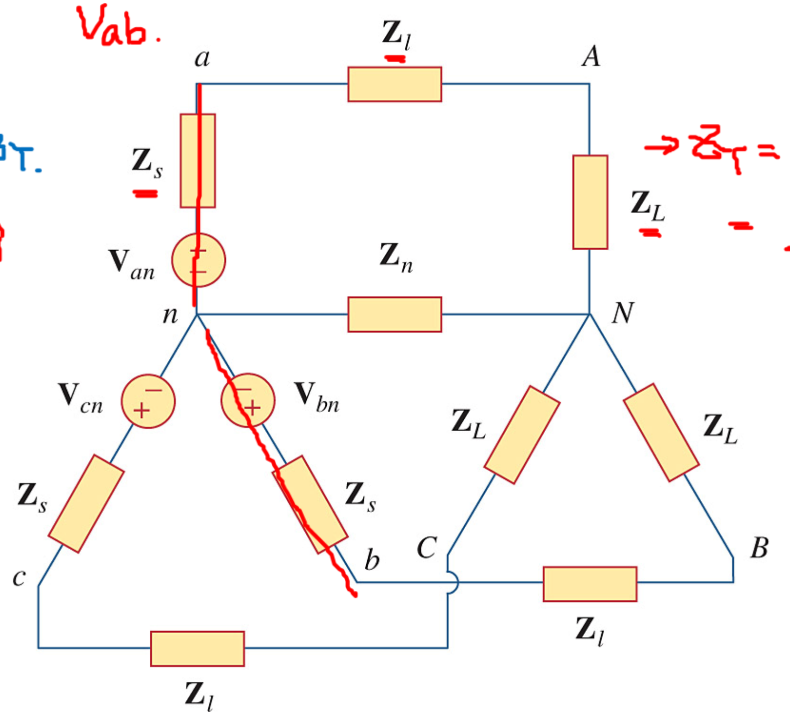


Vab.



$\rightarrow Z_T = Z_s + Z_l + Z_L$

$= 25 + j20.$

$\sqrt{3} \times 120 \angle 30+30$

$\rightarrow V_{an} = 120\angle 30°$

$V_{bn} = 120\angle -90°$

$V_{cn} = 120\angle -210°$

$\rightarrow V_{ab} = V_{an} - V_{bn} = 120\angle 30° - 120\angle -90° = 103.923 + j180$

$= 207.85\angle 60°$

$V_{bc} = 207.85\angle -60°$

$V_{ca} = 207.85\angle -180°$

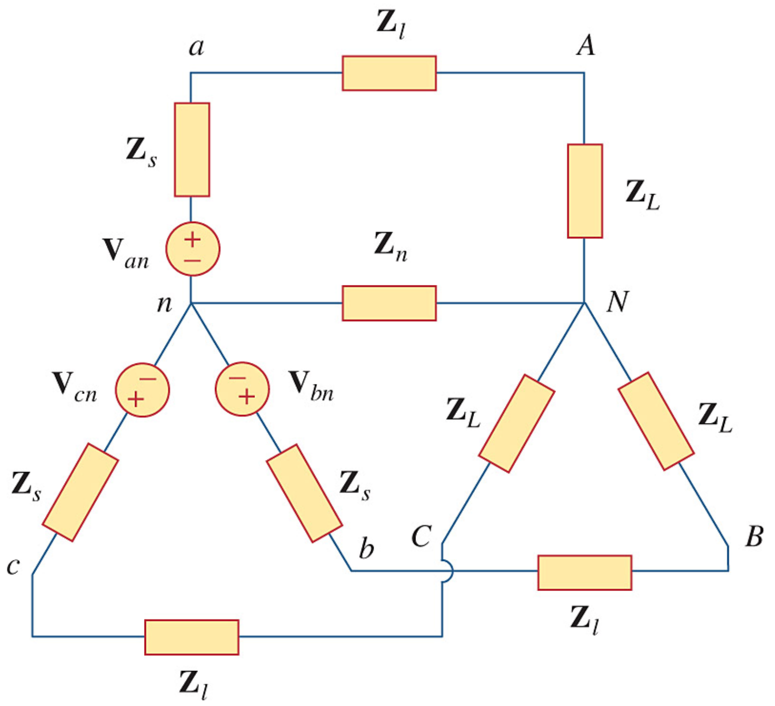
$\rightarrow I_a = \dfrac{120\angle 30°}{25+j20.} = \dfrac{120\angle 30°}{32.01\angle 38.65°} = 3.749\angle -8.65°$

$I_b = 3.75\angle -128.65°$

$I_c = 3.75\angle -248.65°$

Line voltages by follow the definition

Practice Problem 12.2 A Y-connected balanced three-phase generator with an impedance of $0.4 + j0.3\ \Omega$ per phase is connected to a Y-connected balanced load with an impedance of $24 + j19\ \Omega$ per phase. The line joining the generator and the load has an impedance of $0.6 + j0.7\ \Omega$ per phase. Assuming a positive sequence for the source voltages and that $\tilde{V}_{an} = 120\angle 30°$ V, find the line voltages and the line currents.



The "ideal" line voltages are

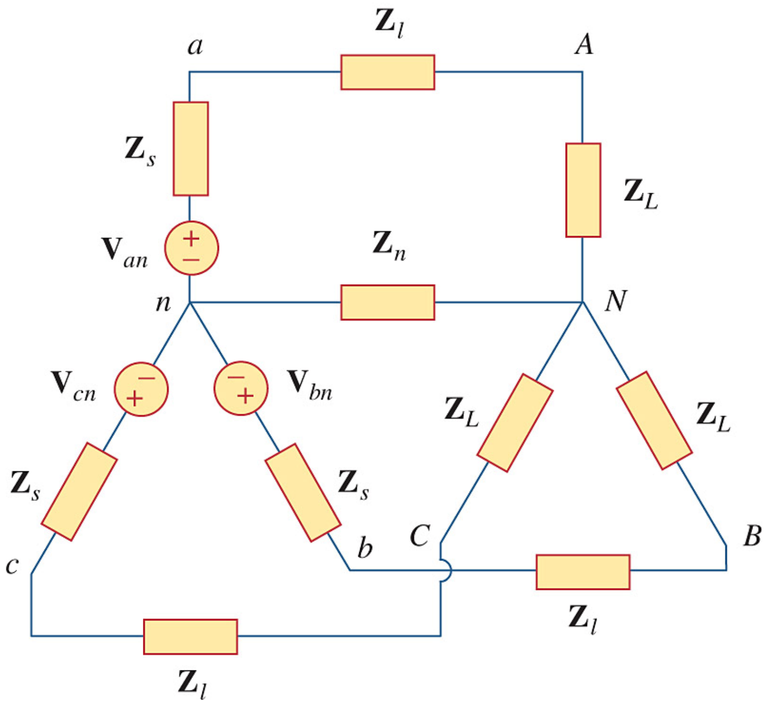
$$\tilde{V}_{ab} = \tilde{V}_{an}\sqrt{3}\angle 30° = 120\angle 30° \times \sqrt{3}\angle 30°$$

$$\approx 207.8461\angle 60°\ (\mathrm{V})$$

$$\tilde{V}_{bc} = \tilde{V}_{ab}\angle -120° = 207.8461\angle -60°\ (\mathrm{V})$$

$$\tilde{V}_{ba} = \tilde{V}_{ab}\angle -240° = 207.8461\angle -180°\ (\mathrm{V})$$

Line currents



$$Z_Y = Z_s + Z_l + Z_L = (0.4 + j0.3) + (24 + j19)$$
$$+(0.6 + j0.7) = 25 + j20\ (\Omega)$$
$$\tilde{I}_a = \frac{\tilde{V}_{an}}{Z_Y} = \frac{120\angle 30^\circ}{25 + j20} \approx \frac{120\angle 30^\circ}{32.0156\angle 38.66^\circ}$$
$$\approx 3.7482\angle -8.66^\circ\ (\text{A})$$
$$\tilde{I}_b = \tilde{I}_a \angle -120^\circ = 3.7482\angle -128.66^\circ\ (\text{A})$$
$$\tilde{I}_c = \tilde{I}_a \angle -240^\circ = 3.7482\angle -248.66^\circ\ (\text{A})$$

Alternatively, by the equations

The "ideal" line voltages are

$$\widetilde{V}_{ab} = \widetilde{V}_{an}\sqrt{3}\angle 30° = 120\angle 30° \times \sqrt{3}\angle 30°$$

$$\approx 207.8461\angle 60° \text{ (V)}$$

$$\widetilde{V}_{bc} = \widetilde{V}_{ab}\angle -120° = 207.8461\angle -60° \text{ (V)}$$

$$\widetilde{V}_{ba} = \widetilde{V}_{ab}\angle -240° = 207.8461\angle -180° \text{ (V)}$$

Note that for a balanced system, the other two voltages/currents can be quickly obtained by their **phase relation**.

Line current

$$Z_Y = Z_s + Z_l + Z_L = (0.4 + j0.3) + (24 + j19)$$

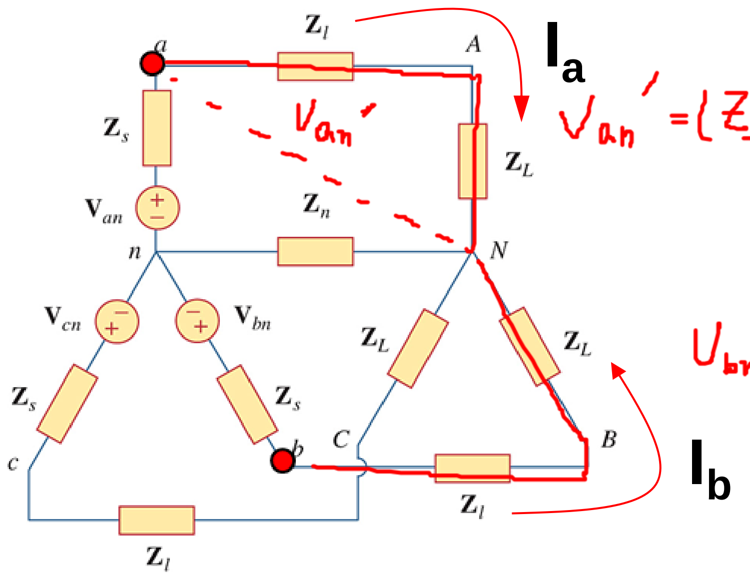
$$+(0.6 + j0.7) = 25 + j20\ (\Omega)$$

$$\widetilde{I}_a = \frac{\widetilde{V}_{an}}{Z_Y} = \frac{120\angle 30^\circ}{25 + j20} \approx \frac{120\angle 30^\circ}{32.0156\angle 38.66^\circ}$$

$$\approx 3.7482\angle -8.66^\circ\ (\mathrm{A})$$

$$\widetilde{I}_b = \widetilde{I}_a\angle -120^\circ = 3.7482\angle -128.66^\circ\ (\mathrm{A})$$

$$\widetilde{I}_c = \widetilde{I}_a\angle -240^\circ = 3.7482\angle -248.66^\circ\ (\mathrm{A})$$



$V_{an}' = (Z_l + Z_L) I_a$.

$V_{bn}' = (Z_l + Z_L) I_b$.

$V_{ab}' = V_{an}' - V_{bn}'$

The line voltages seen from the generator terminals are

$$\tilde{V}_{ab} = \tilde{I}_a (Z_l + Z_L) - \tilde{I}_b (Z_l + Z_L)$$

$$= \tilde{I}_a \sqrt{3} \angle 30° (Z_l + Z_L)$$

$$= \frac{\tilde{V}_{an}}{Z_Y} \sqrt{3} \angle 30° (Z_l + Z_L) = \tilde{V}_{ab} \left(\frac{Z_l + Z_L}{Z_Y} \right)$$

Line voltage V_{ab}

$$= 207.8461\angle 60^\circ \times \left(\frac{24.6 + j19.7}{25 + j20} \right)$$

$$\approx 207.8461\angle 60^\circ \times \frac{31.5159\angle 38.69^\circ}{32.0156\angle 38.66^\circ}$$

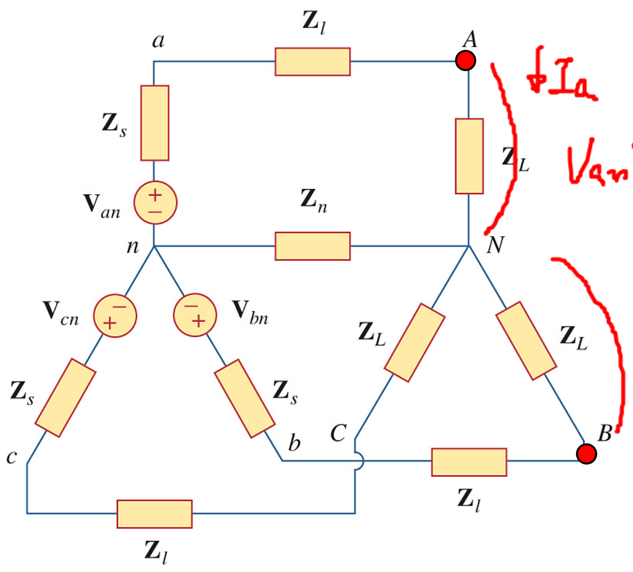
$$\approx 204.6020\angle \underline{60.03}^\circ \text{ (V)}$$

−120 −240°

$$\tilde{V}_{bc} = 204.6020\angle -59.97^\circ \text{ (V)}$$

$$\tilde{V}_{ca} = 204.6020\angle -179.97^\circ \text{ (V)}$$

Slightly lower magnitude and angles compared to the ideal line voltages.



I_a $V_{an}'' = Z_L I_a$

V_{an}''

$V_{bn}'' = Z_L I_b$

$V_{ab}'' = V_{an}'' - V_{bn}''$

The line voltages seen from the load terminals are

$$\tilde{V}_{AB} = \tilde{I}_a Z_L - \tilde{I}_b Z_L$$

$$I_a = 3.7482\angle -8.66$$
$$I_b = 3.7482\angle -8.66$$
$$Z_L = 14 + j19 = 30.61\angle 38.37$$

$$V_{AB} = 198.72\angle 59.71$$
$$V_{BC} = 198.72\angle -60.29$$
$$V_{CA} = 198.72\angle -180.29$$

-120° -240°

The line voltages seen from the load terminals are

$\boxed{V_{AN}-V_{BN}}$ $\boxed{I_a-I_b=I_a\sqrt{3}\angle 30°=V_{an}/Z_Y\sqrt{3}\ \angle 30°=V_{ab}/Z_Y}$

$$\tilde{V}_{AB}=\tilde{I}_a Z_L-\tilde{I}_b Z_L=\tilde{V}_{ab}\frac{Z_L}{Z_Y}$$

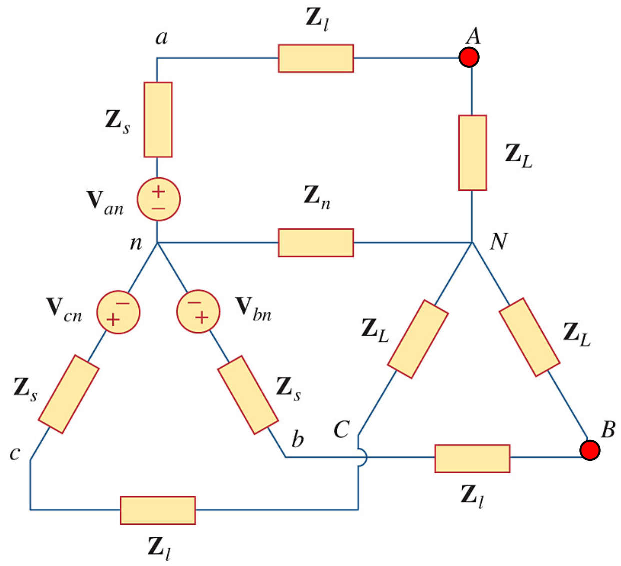
$$=207.8461\angle 60°\times\left(\frac{24+19}{25+j20}\right)$$

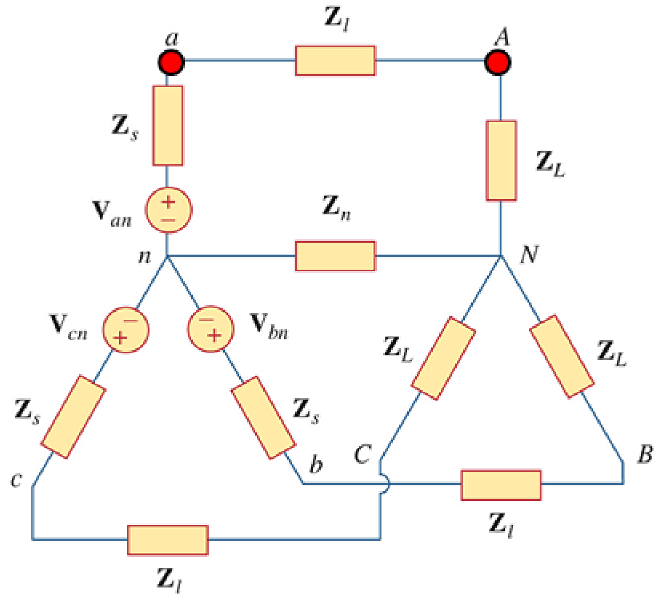
$$\approx 207.8461\angle 60°\times\frac{30.6105\angle 38.37°}{32.0156\angle 38.66°}$$

$$\approx 198.7242\angle 59.71°\ (\mathrm{V})$$

$$\tilde{V}_{BC}\approx 198.7242\angle -60.29°\ (\mathrm{V})$$

$$\tilde{V}_{CA}\approx 198.7242\angle -180.29°\ (\mathrm{V})$$





The line voltage drops are

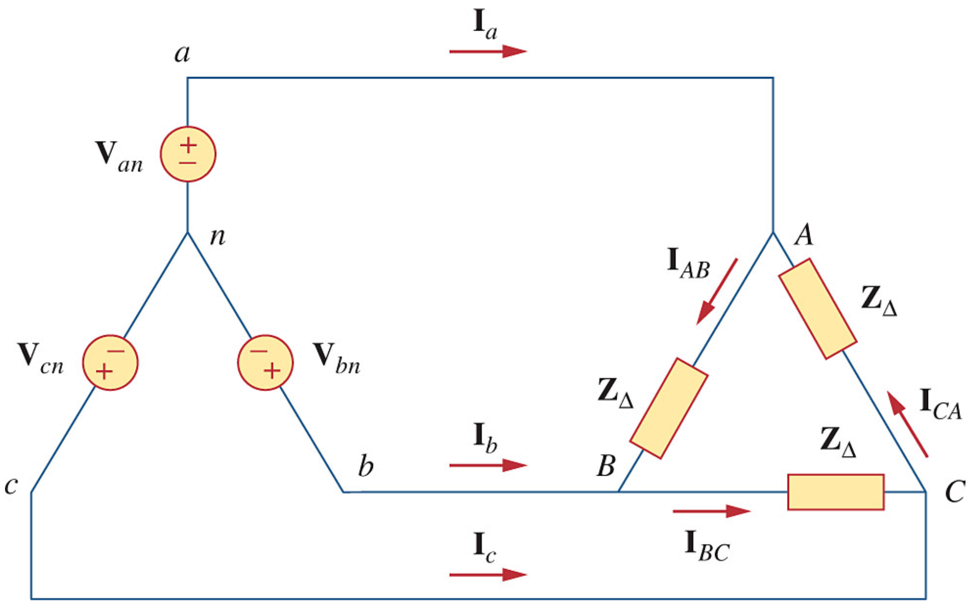
$$\tilde{I}_a Z_l = 3.7482\angle -8.66° \times (0.6 + j0.7)$$

$$\approx 3.4558\angle 40.74° \text{ (V)}$$

$$\tilde{I}_b Z_l = 3.4558\angle -79.26° \text{ (V)}$$

$$\tilde{I}_c Z_l = 3.4558\angle -199.26° \text{ (V)}$$

12.4 Balanced Wye-Delta Connection



A balanced Y-Δ system consists of a balanced Y-connected source feeding a balanced Δ-connected load.

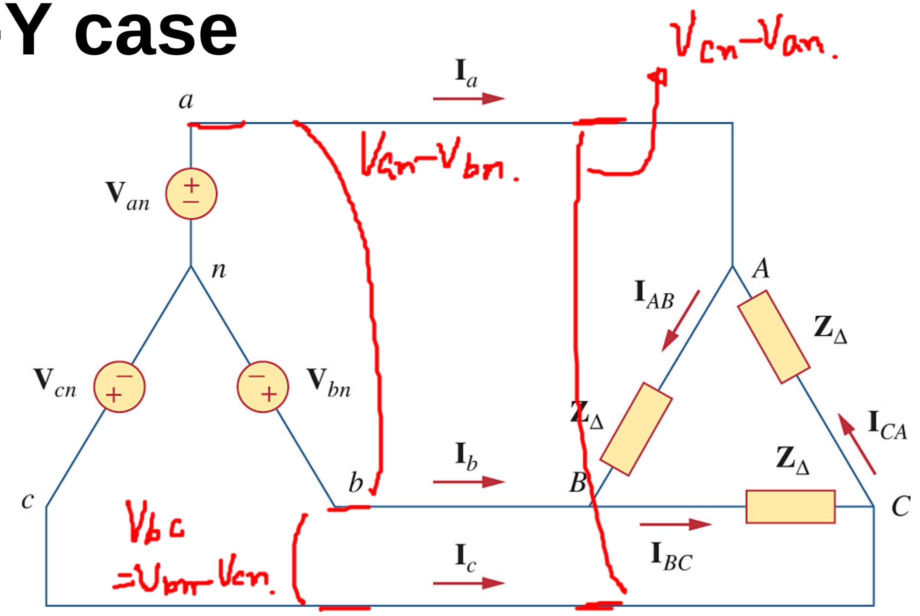
Phase voltages: same as Y-Y case

Assume that

$$\tilde{V}_{an} = V_p \angle 0°$$

$$\tilde{V}_{bn} = V_p \angle -120°$$

$$\tilde{V}_{cn} = V_p \angle -240°$$



The line voltages are

$$\tilde{V}_{ab} = \sqrt{3} V_p \angle 30° = \tilde{V}_{an} \sqrt{3} \angle 30° = \tilde{V}_{AB}$$

$$\tilde{V}_{bc} = \tilde{V}_{ab} \angle -120° = \tilde{V}_{BC}$$

$$\tilde{V}_{ca} = \tilde{V}_{ab} \angle -240° = \tilde{V}_{CA}$$

Phase currents

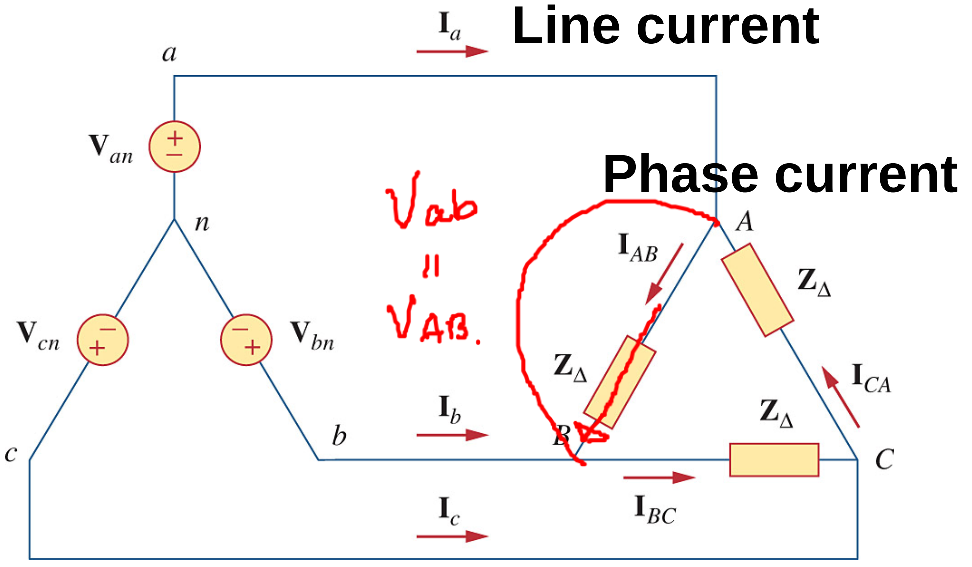
The phase currents are

balanced.

$$\tilde{I}_{AB} = \frac{\tilde{V}_{AB}}{Z_\Delta}$$

$$\tilde{I}_{BC} = \frac{\tilde{V}_{BC}}{Z_\Delta} = \tilde{I}_{AB}\angle\underline{-120°}$$

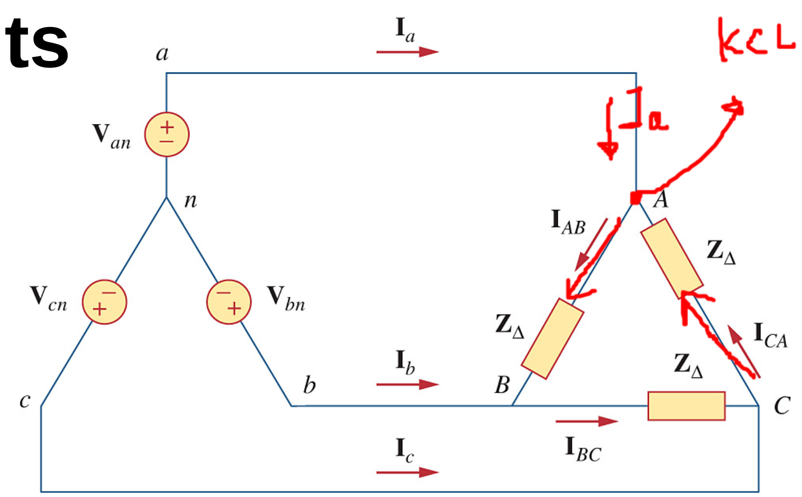
$$\tilde{I}_{CA} = \frac{\tilde{V}_{CA}}{Z_\Delta} = \tilde{I}_{AB}\angle\underline{-240°}$$



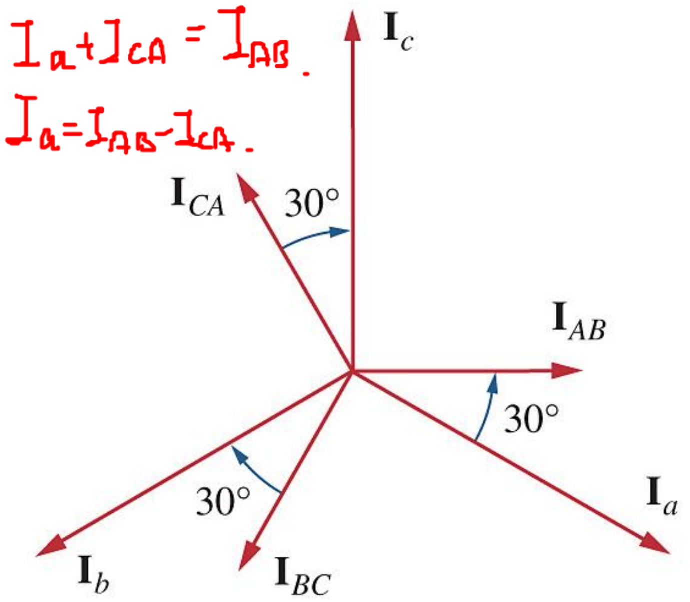
$$Z_Y = \frac{Z_\Delta}{3}$$

While **the line current** is the current in each line, **the phase current** is the current in each phase of the source or load.

Line currents



KCL: $I_a + I_{CA} = I_{AB}$.
$I_a = I_{AB} - I_{CA}$.



The line currents are

$$\tilde{I}_a = \tilde{I}_{AB} - \tilde{I}_{CA} = \tilde{I}_{AB}\sqrt{3}\angle -30^\circ$$

$$\tilde{I}_b = \tilde{I}_{BC} - \tilde{I}_{AB} = \tilde{I}_{BC}\sqrt{3}\angle -30^\circ = \boxed{\tilde{I}_a \angle -120^\circ}$$

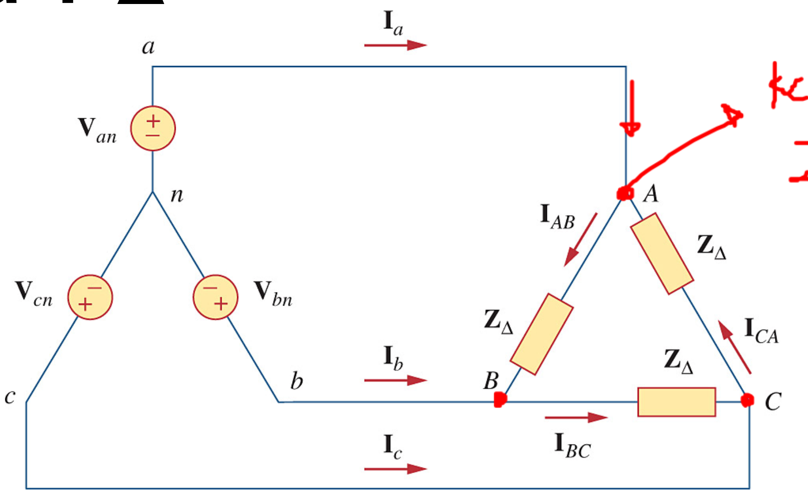
$$\tilde{I}_c = \tilde{I}_{CA} - \tilde{I}_{BC} = \tilde{I}_{CA}\sqrt{3}\angle -30^\circ = \boxed{\tilde{I}_a \angle -240^\circ}$$

$$\boxed{\begin{aligned} \tilde{I}_{AB} &= \frac{\tilde{V}_{AB}}{Z_\Delta} \\ \tilde{I}_{BC} &= \frac{\tilde{V}_{BC}}{Z_\Delta} = \tilde{I}_{AB}\angle -120^\circ \\ \tilde{I}_{CA} &= \frac{\tilde{V}_{CA}}{Z_\Delta} = \tilde{I}_{AB}\angle -240^\circ \end{aligned}}$$

showing that

$$I_L = \sqrt{3} I_p \qquad I_L = \left|\tilde{I}_a\right| = \left|\tilde{I}_b\right| = \left|\tilde{I}_c\right|,\ I_p = \left|\tilde{I}_{AB}\right| = \left|\tilde{I}_{BC}\right| = \left|\tilde{I}_{CA}\right|$$

Summary of balanced Y-Δ



KCL.

$I_a + I_{CA} = I_{AB}$.

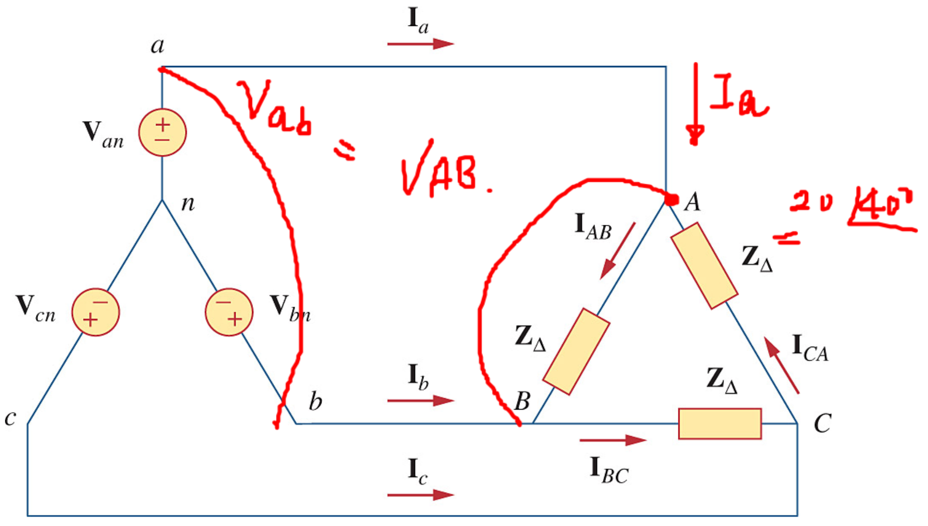
$I_a = I_{AB} - I_{CA}$.

Summary of phase and line voltages/currents for balanced three-phase systems.[1]

Connection	Phase voltages/currents	Line voltages/currents
Y-Δ	$\mathbf{V}_{an} = V_p\angle 0^\circ$	$\mathbf{V}_{ab} = \mathbf{V}_{AB} = \sqrt{3}V_p\angle 30^\circ$
	$\mathbf{V}_{bn} = V_p\angle -120^\circ$	$\mathbf{V}_{bc} = \mathbf{V}_{BC} = \mathbf{V}_{ab}\angle -120^\circ$
	$\mathbf{V}_{cn} = V_p\angle +120^\circ$	$\mathbf{V}_{ca} = \mathbf{V}_{CA} = \mathbf{V}_{ab}\angle +120^\circ$
	$\mathbf{I}_{AB} = \mathbf{V}_{AB}/\mathbf{Z}_\Delta$	$\mathbf{I}_a = \mathbf{I}_{AB}\sqrt{3}\angle -30^\circ$
	$\mathbf{I}_{BC} = \mathbf{V}_{BC}/\mathbf{Z}_\Delta$	$\mathbf{I}_b = \mathbf{I}_a\angle -120^\circ$
	$\mathbf{I}_{CA} = \mathbf{V}_{CA}/\mathbf{Z}_\Delta$	$\mathbf{I}_c = \mathbf{I}_a\angle +120^\circ$

Positive or abc sequence is assumed.

Practice Problem 12.3 One line voltage of a balanced Y-connected source is $\tilde{V}_{AB} = 240\angle -20°$ V. If the source is connected to a Δ-connected load of $20\angle 40°$ Ω, find the phase and line currents. Assume the *abc* sequence.



$$I_{AB} = \frac{240\angle -20°}{20\angle 40°} = 12\angle -60°$$

$-60-30°$

$$I_{BC} = 12\angle -180°$$

$$I_{CA} = 12\angle -300°$$

$$I_b = 20.78\angle -210°$$

$$I_c = 20.78\angle -330°$$

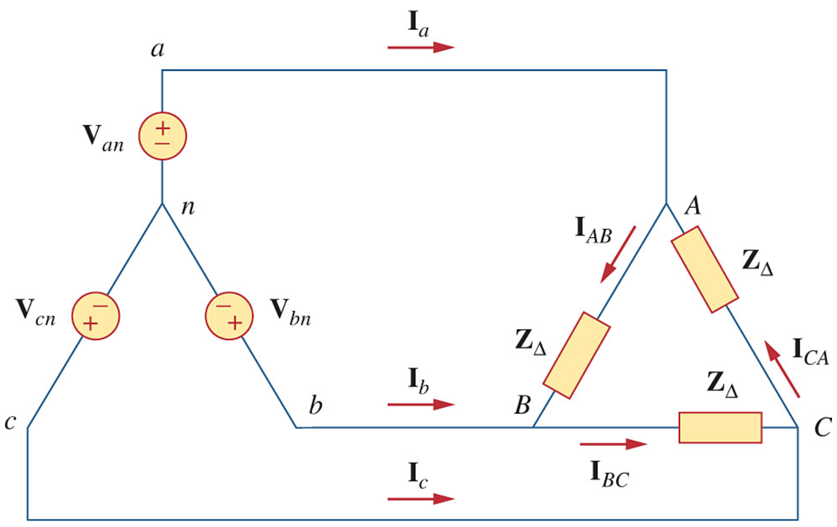
KCL: $I_a + I_{CA} = I_{AB}.$

$$I_a = I_{AB} - I_{CA}.$$

$$= 12\angle -60° - 12\angle -300°$$

$$= \cancel{12}\ 0. - j20.78$$

$$= 20.78\angle -90°$$



$$\tilde{I}_{AB} = \frac{\tilde{V}_{AB}}{Z_\Delta} = \frac{240\angle -20^\circ}{20\angle 40^\circ} = 12\angle -60^\circ \text{ (A)}$$

$$\tilde{I}_{BC} = \tilde{I}_{AB}\angle -120^\circ = 12\angle -180^\circ \text{ (A)}$$

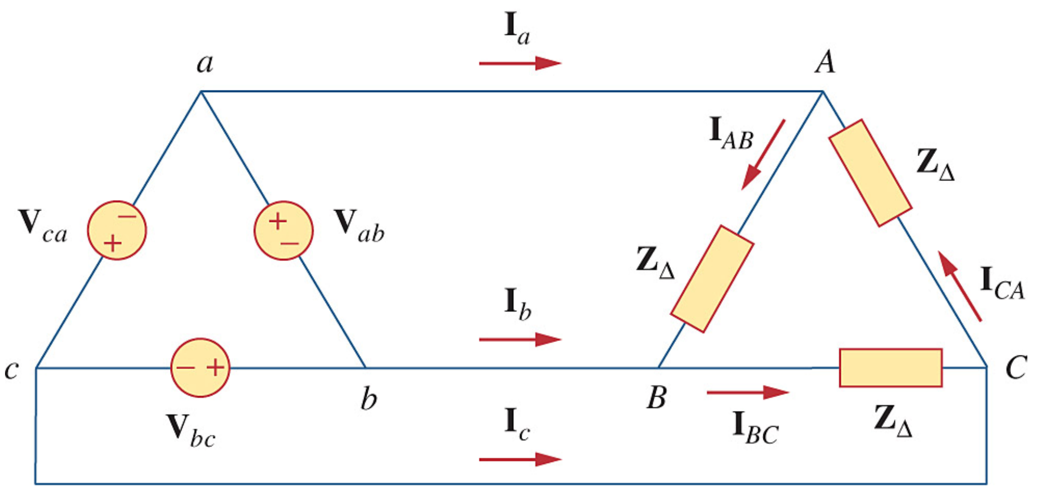
$$\tilde{I}_{CA} = \tilde{I}_{AB}\angle +120^\circ = 12\angle 60^\circ \text{ (A)}$$

$$\tilde{I}_a = \tilde{I}_{AB}\sqrt{3}\angle -30^\circ \approx 20.7846\angle -90^\circ \text{ (A)}$$

$$\tilde{I}_b = \tilde{I}_a\angle +240^\circ = 20.7846\angle 150^\circ \text{ (A)}$$

$$\tilde{I}_c = \tilde{I}_a\angle +120^\circ = 20.7846\angle 30^\circ \text{ (A)}$$

12.5 Balanced Delta-Delta Connection



A balanced Δ-Δ system is one in which both the balanced source and balanced load are Δ-connected.

Phase and line voltages

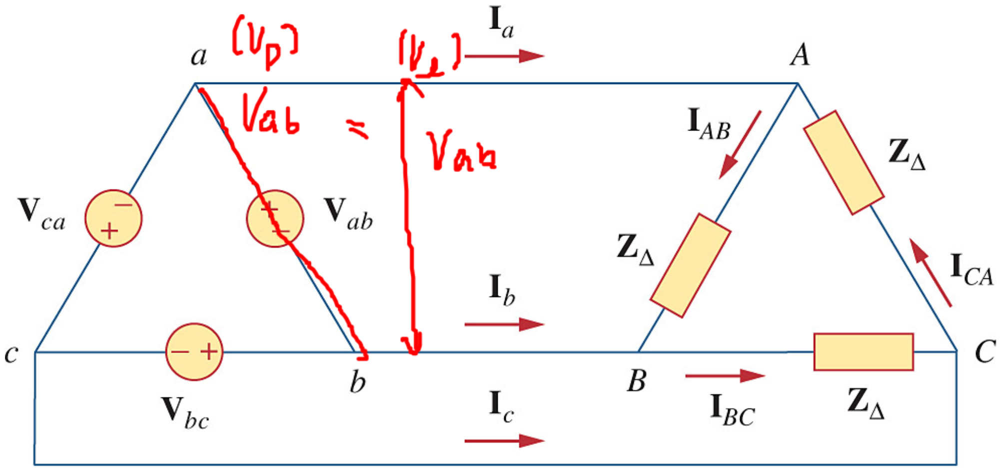
Assume that

$$\tilde{V}_{ab} = V_p \angle 0°$$

$$\tilde{V}_{bc} = V_p \angle -120°$$

$$\tilde{V}_{ca} = V_p \angle +120°$$

(= −240°)

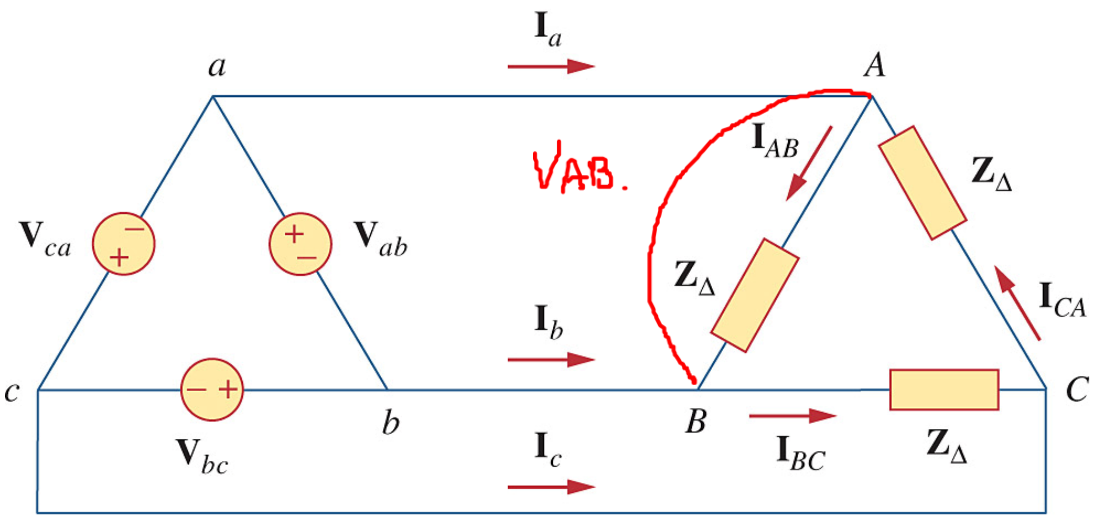


Phase voltage = Line voltage

Phase voltage = Voltage across the impedances

$$\tilde{V}_{ab} = \tilde{V}_{AB}, \ \tilde{V}_{bc} = \tilde{V}_{BC}, \ \tilde{V}_{ca} = \tilde{V}_{CA}$$

Phase current



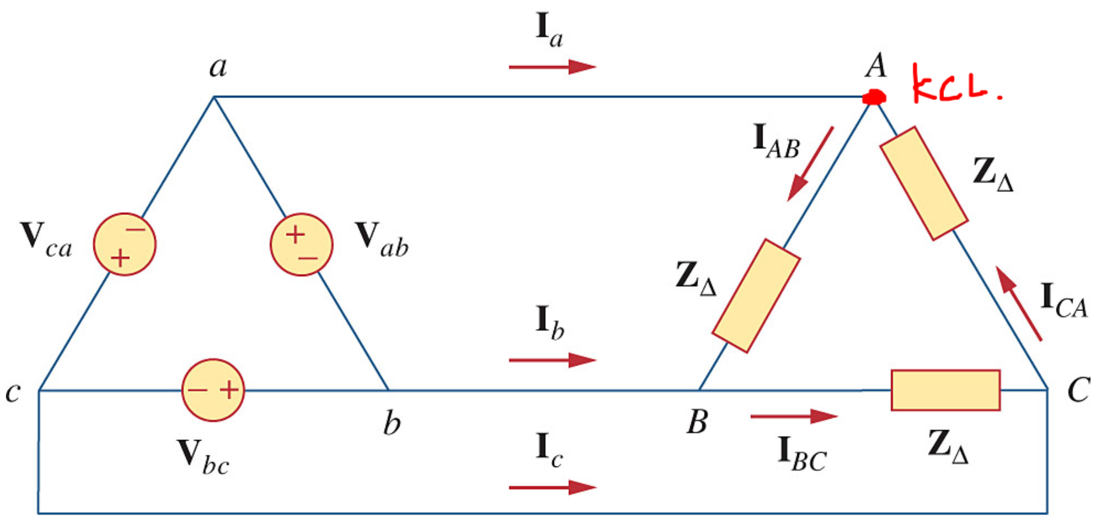
The phase currents are

$$\tilde{I}_{AB} = \frac{\tilde{V}_{AB}}{Z_{\Delta}}$$

$$\tilde{I}_{BC} = \frac{\tilde{V}_{BC}}{Z_{\Delta}} = \tilde{I}_{AB}\angle -120^{\circ}$$

$$\tilde{I}_{CA} = \frac{\tilde{V}_{CA}}{Z_{\Delta}} = \tilde{I}_{AB}\angle +120^{\circ}$$

Line current



The line currents are

balanced

$$\boxed{\tilde{I}_a} = \tilde{I}_{AB} - \tilde{I}_{CA} = \tilde{I}_{AB}\sqrt{3}\angle -30°$$

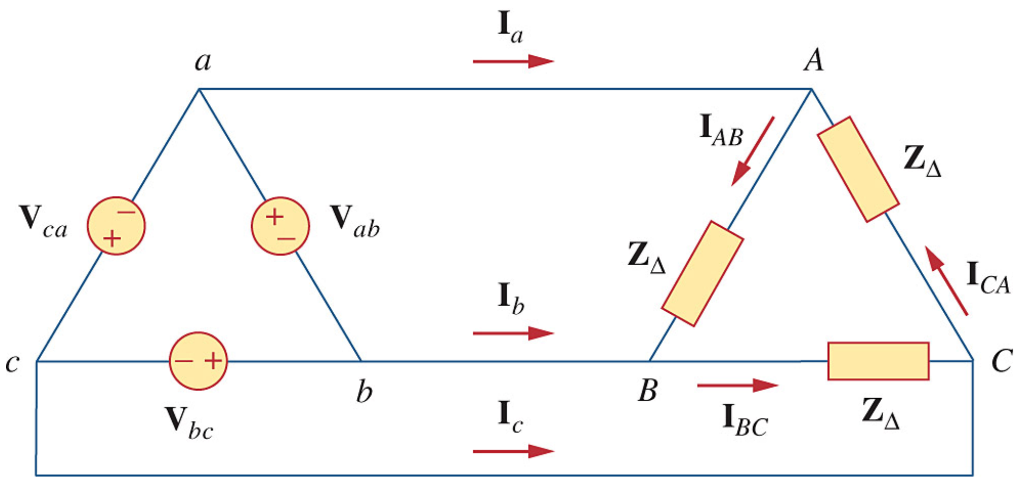
$$\tilde{I}_b = \tilde{I}_{BC} - \tilde{I}_{AB} = \tilde{I}_{BC}\sqrt{3}\angle -30° = \boxed{\tilde{I}_a\angle -120°}$$

$$\tilde{I}_c = \tilde{I}_{CA} - \tilde{I}_{BC} = \tilde{I}_{CA}\sqrt{3}\angle -30° = \boxed{\tilde{I}_a\angle -240°}$$

showing that

$$I_L = \sqrt{3}I_p \qquad I_L = \left|\tilde{I}_a\right| = \left|\tilde{I}_b\right| = \left|\tilde{I}_c\right|,\ I_p = \left|\tilde{I}_{AB}\right| = \left|\tilde{I}_{BC}\right| = \left|\tilde{I}_{CA}\right|$$

Summary of balanced Δ-Δ

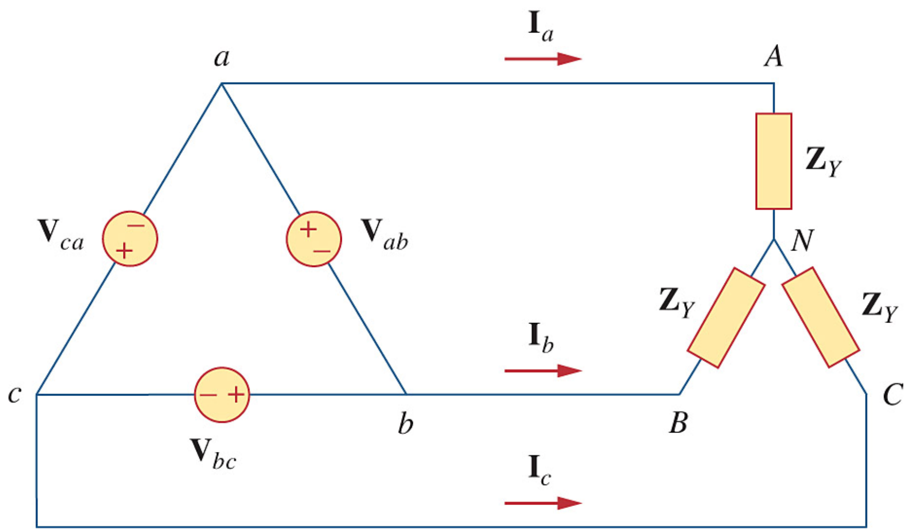


Summary of phase and line voltages/currents for balanced three-phase systems.[1]

Connection	Phase voltages/currents	Line voltages/currents
Δ-Δ	$\mathbf{V}_{ab} = V_p\angle 0^\circ$	Same as phase voltages
	$\mathbf{V}_{bc} = V_p\angle -120^\circ$	
	$\mathbf{V}_{ca} = V_p\angle +120^\circ$	
	$\mathbf{I}_{AB} = \mathbf{V}_{ab}/\mathbf{Z}_\Delta$	$\mathbf{I}_a = \mathbf{I}_{AB}\sqrt{3}\angle -30^\circ$
	$\mathbf{I}_{BC} = \mathbf{V}_{bc}/\mathbf{Z}_\Delta$	$\mathbf{I}_b = \mathbf{I}_a\angle -120^\circ$
	$\mathbf{I}_{CA} = \mathbf{V}_{ca}/\mathbf{Z}_\Delta$	$\mathbf{I}_c = \mathbf{I}_a\angle +120^\circ$

Positive or abc sequence is assumed.

12.6 Balanced Delta-Wye Connection



A balanced Δ-Y system consists of a balanced Δ-connected source feeding a balanced Y-connected load.

***In Δ-connected source:**
Phase voltages = Line voltages

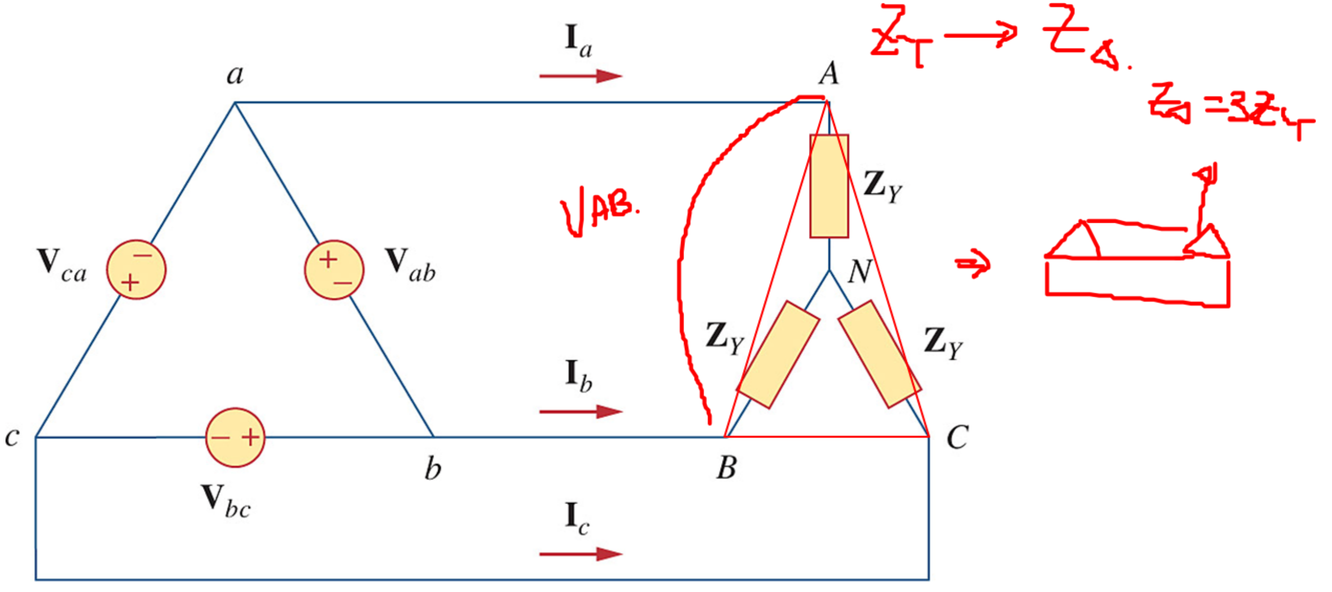
Line current

Assume that

$$\tilde{V}_{ab} = V_p \angle 0°$$

$$\tilde{V}_{bc} = V_p \angle -120°$$

$$\tilde{V}_{ca} = V_p \angle +120°$$



Replace the Y-connected load with its equivalent Δ-connected load. **Line current (e.g. I_a)** in a Δ-connected load is:

" V_{AB}/Z_Δ $= 3Z_Y$.

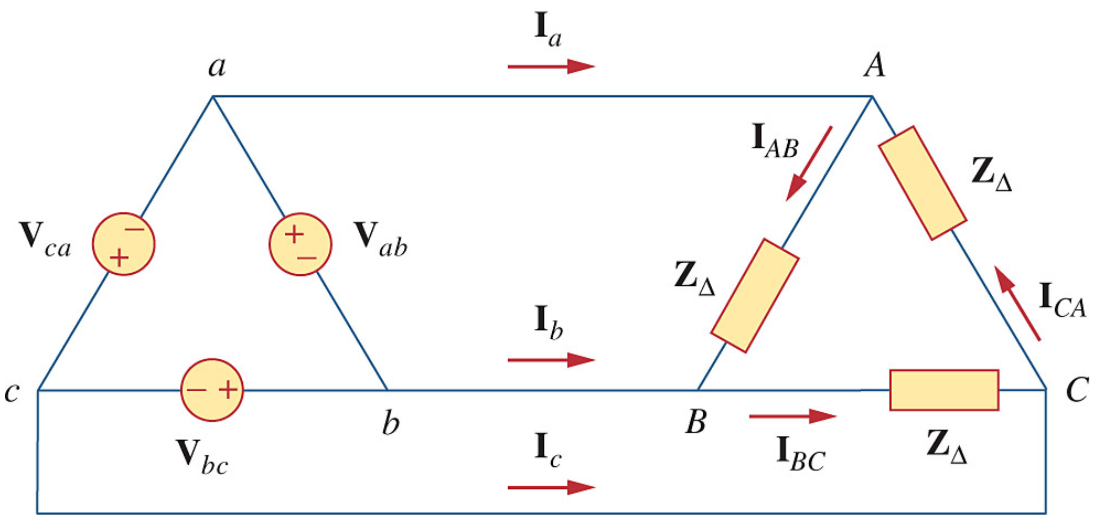
$$\tilde{I}_a = \tilde{I}_{AB}\sqrt{3}\angle -30° = \frac{\tilde{V}_{AB}}{Z_\Delta}\sqrt{3}\angle -30°$$

$$= \frac{\tilde{V}_{ab}}{\cancel{3}Z_Y}\cancel{\sqrt{3}}\angle -30° = \frac{\tilde{V}_{ab}}{\sqrt{3}Z_Y}\angle -30°$$

$\boxed{Z_\Delta = 3Z_Y}$

$Z_Y = Z_\Delta/3$

Recall: Δ-Δ Phase current



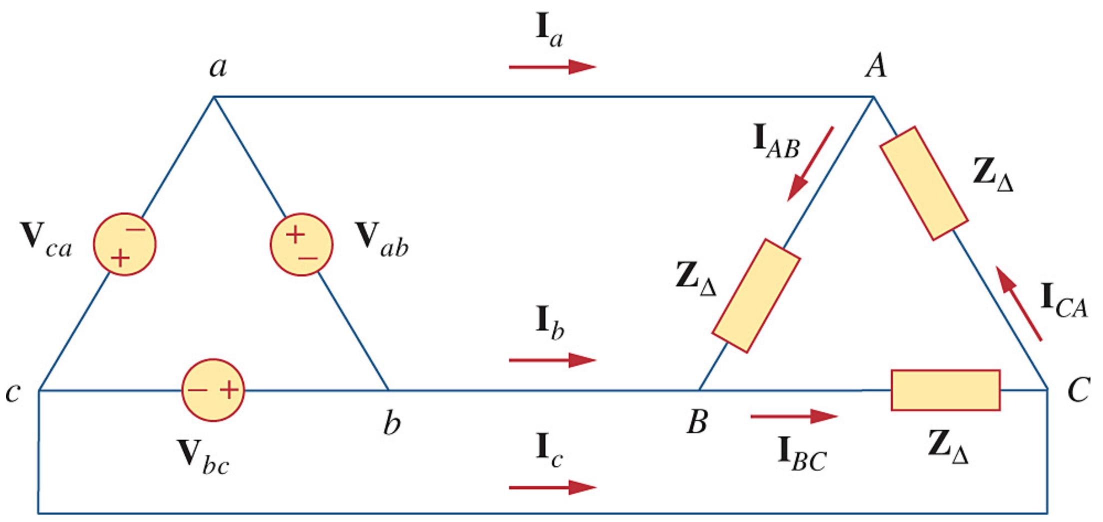
The phase currents are

$$\tilde{I}_{AB} = \frac{\tilde{V}_{AB}}{Z_{\Delta}}$$

$$\tilde{I}_{BC} = \frac{\tilde{V}_{BC}}{Z_{\Delta}} = \tilde{I}_{AB} \angle -120^{\circ}$$

$$\tilde{I}_{CA} = \frac{\tilde{V}_{CA}}{Z_{\Delta}} = \tilde{I}_{AB} \angle +120^{\circ}$$

Recall: Δ-Δ Line current



The line currents are

$$\tilde{I}_a = \tilde{I}_{AB} - \tilde{I}_{CA} = \tilde{I}_{AB}\sqrt{3}\angle -30°$$

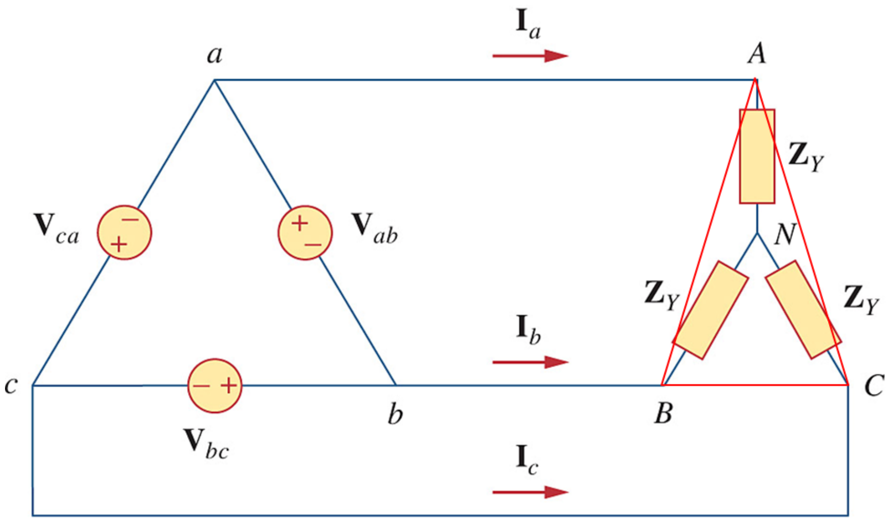
$$\tilde{I}_b = \tilde{I}_{BC} - \tilde{I}_{AB} = \tilde{I}_{BC}\sqrt{3}\angle -30° = \tilde{I}_a\angle -120°$$

$$\tilde{I}_c = \tilde{I}_{CA} - \tilde{I}_{BC} = \tilde{I}_{CA}\sqrt{3}\angle -30° = \tilde{I}_a\angle -240°$$

showing that

$$I_L = \sqrt{3}I_p \qquad I_L = \left|\tilde{I}_a\right| = \left|\tilde{I}_b\right| = \left|\tilde{I}_c\right|, I_p = \left|\tilde{I}_{AB}\right| = \left|\tilde{I}_{BC}\right| = \left|\tilde{I}_{CA}\right|$$

Line current



$$\tilde{V}_{ab} = V_p \angle 0°$$
$$\tilde{V}_{bc} = V_p \angle -120°$$
$$\tilde{V}_{ca} = V_p \angle +120°$$

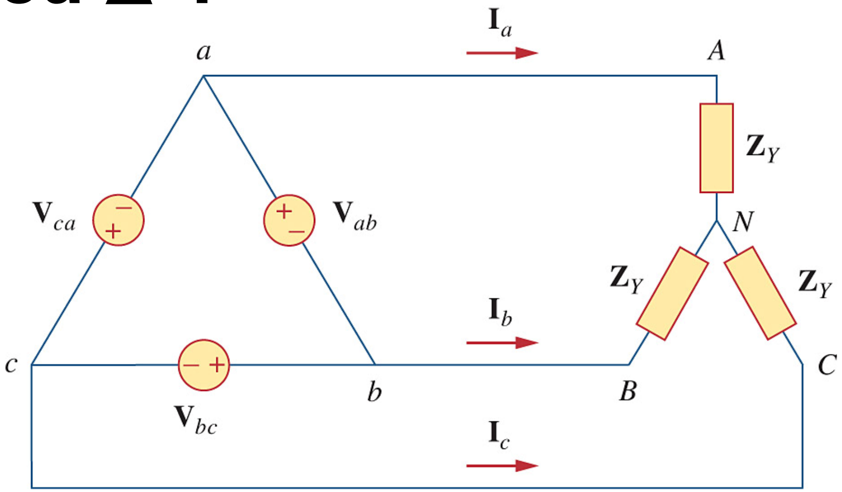
$$\boxed{\tilde{I}_a} = \frac{\tilde{V}_{ab}}{\sqrt{3}Z_Y} \angle -30°$$

$$\tilde{I}_b = \frac{\tilde{V}_{bc}}{\sqrt{3}Z_Y} \angle -30° = \boxed{\tilde{I}_a \angle -120°}$$

$$\tilde{I}_c = \frac{\tilde{V}_{ca}}{\sqrt{3}Z_Y} \angle -30° = \boxed{\tilde{I}_a \angle +120°}$$

In Y-connected load,
Phase currents = Line currents

Summary of balanced Δ-Y



Summary of phase and line voltages/currents for balanced three-phase systems.[1]

Connection	Phase voltages/currents	Line voltages/currents
Δ-Y	$\mathbf{V}_{ab} = V_p\angle 0°$ $\mathbf{V}_{bc} = V_p\angle -120°$ $\mathbf{V}_{ca} = V_p\angle +120°$	Same as phase voltages
	Same as line currents	$\mathbf{I}_a = \dfrac{V_p\angle -30°}{\sqrt{3}\mathbf{Z}_Y}$ $\mathbf{I}_b = \mathbf{I}_a\angle -120°$ $\mathbf{I}_c = \mathbf{I}_a\angle +120°$

Positive or abc sequence is assumed.

Practice Problem 12.5

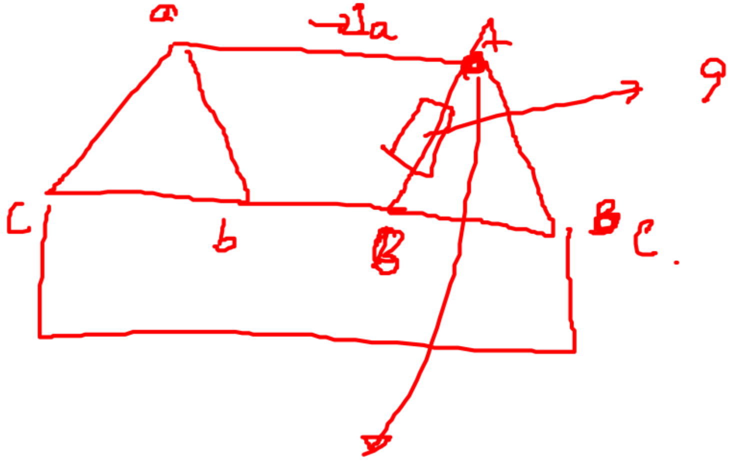
In a balanced Δ-Y circuit, $\mathbf{V}_{ab} = 240\angle 15^\circ$ and $\mathbf{Z}_Y = (12 + j15)\ \Omega$. Calculate the line currents.

-240° -120° -120°

Answer: $7.21\angle -66.34^\circ$ A, $7.21\angle +173.66^\circ$ A, $7.21\angle 53.66^\circ$ A.

$Z_\Delta = 3Z_Y$
$Z_Y = Z_\Delta/3$

Δ-Y → Δ-Δ $\quad Z_\Delta = 3Z_Y = 3(12+j15) = 9(4+j5)$



$$I_{AB} = \frac{V_{AB}}{Z_\Delta} = \frac{240\angle 15^\circ}{9(4+j5)} = \frac{240\angle 15^\circ}{57.63\angle 51.34^\circ}$$

$$= 4.16\angle -36.34^\circ$$

$$I_{BC} = 4.16\angle -36.34 - 120^\circ$$

$$I_{CA} = 4.16\angle -36.34 - 240^\circ$$

KCL: $I_a = I_{AB} - I_{CA}$

$\rightarrow\ = 4.16\angle -36.34^\circ - 4.16\angle -276.34^\circ$

= 2.89156 -j6.59967 = 7.205∠–66.34

$I_b = 7.21\angle -66.34 - 120^\circ$

$I_c = 7.21\angle -66.34 - 240^\circ$

12.7 Power in a Balanced System

Three phase system - Advantage 1:

We begin by examining the **instantaneous power** absorbed by the load (time domain). For a **Y-connected load**, the phase voltages in the abc sequence are

V_p = rms value,   Peak voltage

$$v_{AN} = \underline{\sqrt{2}V_p} \cos \omega t$$

$$v_{BN} = \sqrt{2}V_p \cos(\omega t - 120°)$$

$$v_{CN} = \sqrt{2}V_p \cos(\omega t + 120°)$$

Phase voltage V_p is the rms value

➔ Peak value: $\sqrt{2}V_P$

If $Z_Y = Z\angle\theta$, the phase currents are

$\to$ Peak current

$$i_a = \sqrt{2}I_p \cos(\omega t - \theta)$$

$$i_b = \sqrt{2}I_p \cos(\omega t - \theta - 120°)$$

$$i_c = \sqrt{2}I_p \cos(\omega t - \theta + 120°)$$

✓

I=V/Z
➔ ∠I=∠V−∠Z

p=v·i

The total instantaneous power is

$$p = p_a + p_b + p_c$$

$$= v_{AN}i_a + v_{BN}i_b + v_{CN}i_c$$

$$= 3V_pI_p\cos\theta$$

Constant

$$= 2V_pI_p[\cos\omega t\cos(\omega t - \theta)$$
$$+\cos(\omega t - 120°)\cos(\omega t - \theta - 120°)$$
$$+\cos(\omega t + 120°)\cos(\omega t - \theta + 120°)]$$
$$= 2V_pI_p\{\frac{\cos\theta + \cos(2\omega t - \theta)}{2}$$
$$+\frac{\cos\theta + \cos(2\omega t - \theta - 240°)}{2}$$
$$+\frac{\cos\theta + \cos(2\omega t - \theta + 240°)}{2}]$$
$$= 3V_pI_p\cos\theta$$

$$p = p_a + p_b + p_c \;= 3V_p I_p \cos\theta$$

Thus, **the total instantaneous power** in a balanced three-phase system is **constant** – it does not change with time as the instantaneous power of each phase does.

This result is true whether the load is Y- or Δ-connected. This is one important reason for using a three-phase system to generate and distribute power.

The advantage over a single-phase AC system: **constant p(t)**

Since the total instantaneous power is independent of time,

$Z_Y = Z\angle\theta$ θ is the power factor angle

(i) **Average power** per phase P_p for the Y- or Δ-connected load is $^P/_3$, or $P_p = V_P I_P cos\theta$

(ii) **Reactive power** per phase is $Q_p = V_P I_P sin\theta$

(iii) **Apparent power** per phase is $|S_P| = V_P I_P$

(iv) **Complex power** per phase is $S_P = P_P + jQ_P = \boldsymbol{V_P I_P^*}$

(v) **Total average power** by AC power conservation is $P = P_a + P_b + P_c = 3P_P = 3\underbrace{V_P I_P \cos\theta}_{\text{phases}}$

three

The total average power:

Y-Y For a Y-connected load (with Y-connected source),

$$\boldsymbol{I_L = I_P \ but \ V_L = \sqrt{3} V_P}$$

Δ-Δ For a Δ-connected load (with Δ-connected source),

$$\boldsymbol{I_L = \sqrt{3} I_P \ but \ V_L = V_P}$$

Thus, $\boldsymbol{3V_p I_P cos\theta = \sqrt{3} V_L I_L cos\theta}$

V_p: phase voltage I_p: phase current	V_L: line voltage I_L: line current

The total average power:

P = 3P_P = $3V_p I_P cos\theta = \sqrt{3}V_L I_L cos\theta$

3 × P per phase

The total reactive power:

Q = 3Q_P = $3V_p I_P sin\theta = \sqrt{3}V_L I_L sin\theta$

per Phase

Recall:

$Z_Y = Z\angle\theta$ θ=∠$\mathbf{V_p}$−∠$\mathbf{I_p}$

θ is the power factor angle

The total complex power:

S = 3S_P = $3\boldsymbol{V_p}\boldsymbol{I_P^*} = 3I_P^2 Z_P = \frac{3V_P^2}{Z_P^*}$

where Z_P is the load impedance per phase.

$S = P + jQ = 3V_P I_P \cos\theta + j3V_P I_P \sin\theta = \sqrt{3}V_L I_L \cos\theta + j\sqrt{3}V_L I_L \sin\theta$

$\mathbf{V_P}$, $\mathbf{I_P}$, $\mathbf{V_L}$, and $\mathbf{I_L}$ are **all rms values** and that θ is the angle of the load impedance or the angle between the phase voltage and the phase current.

The total average power:

For a Y-Y connection, $\boldsymbol{I_L = I_P \; but \; V_L = \sqrt{3} V_P}$

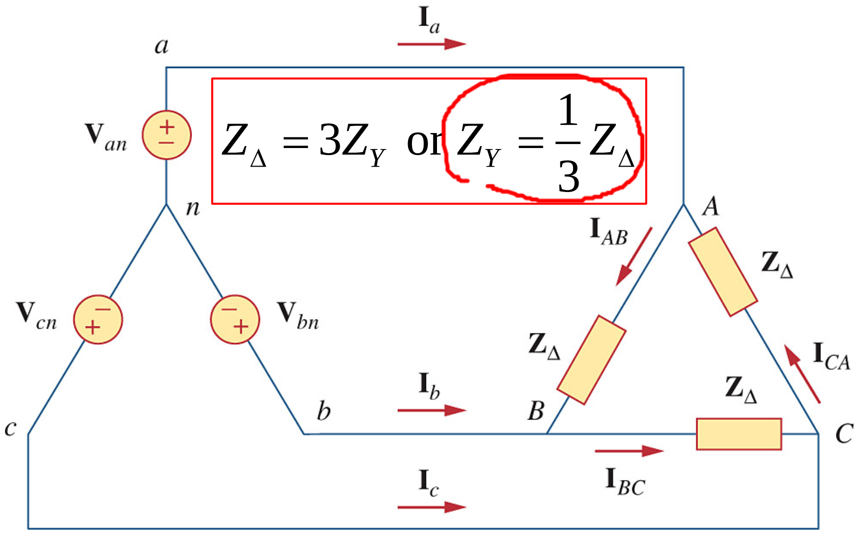
For a Δ-Δ connection, $\boldsymbol{I_L = \sqrt{3} I_P \; but \; V_L = V_P}$

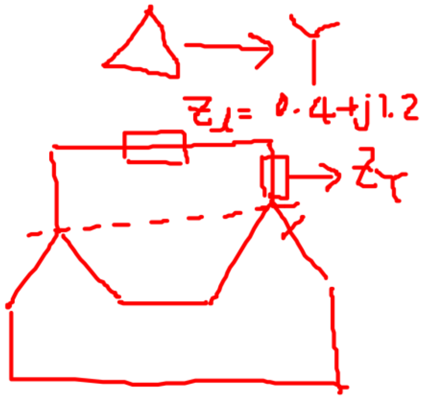
P = 3P_P = $3V_p I_P cos\theta = \sqrt{3} V_L I_L cos\theta$

How about other connections? Y-Δ

Δ-Y.

12.29 A balanced three-phase Y-Δ system has $\mathbf{V}_{an} = 240\underline{/0^\circ}$ V rms and $\mathbf{Z}_\Delta = 51 + j45\ \Omega$. If the line impedance per phase is $0.4 + j1.2\ \Omega$, find the total complex power delivered to the load.





$Z_\Delta \to Z_Y = \frac{1}{3} Z_\Delta$

$= 17 + j15$

$I_a = \frac{240\angle 0^\circ}{17.4 + j16.2} = \frac{240\angle 0^\circ}{23.78\angle 42.95^\circ} = 10.09\angle -42.95^\circ$

$S_p = V_{rms} I_{rms}^* = I_{rms} \cdot Z_Y I_{rms}^* = I_{rms}^2 Z_Y$

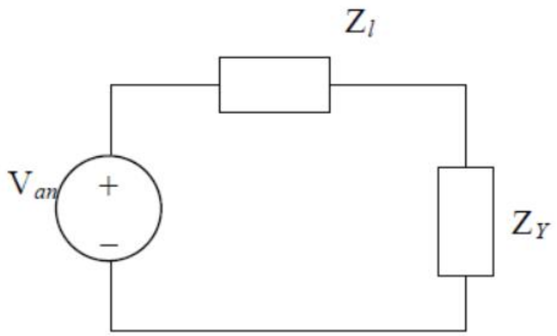
$S = 3 \times S_p = 6924\angle$ ____

$= (10.09)^2 (17 + j15) = 2307.99\angle 41.42^\circ$

$22.67\angle 41.42^\circ$

12.29 A balanced three-phase Y-Δ system has $\mathbf{V}_{an} = 240\angle 0°$ V rms and $\mathbf{Z}_\Delta = 51 + j45\ \Omega$. If the line impedance per phase is $0.4 + j1.2\ \Omega$, find the total complex power delivered to the load.

Replace the delta load with a Y load, $Z_Y = Z_\Delta/3$



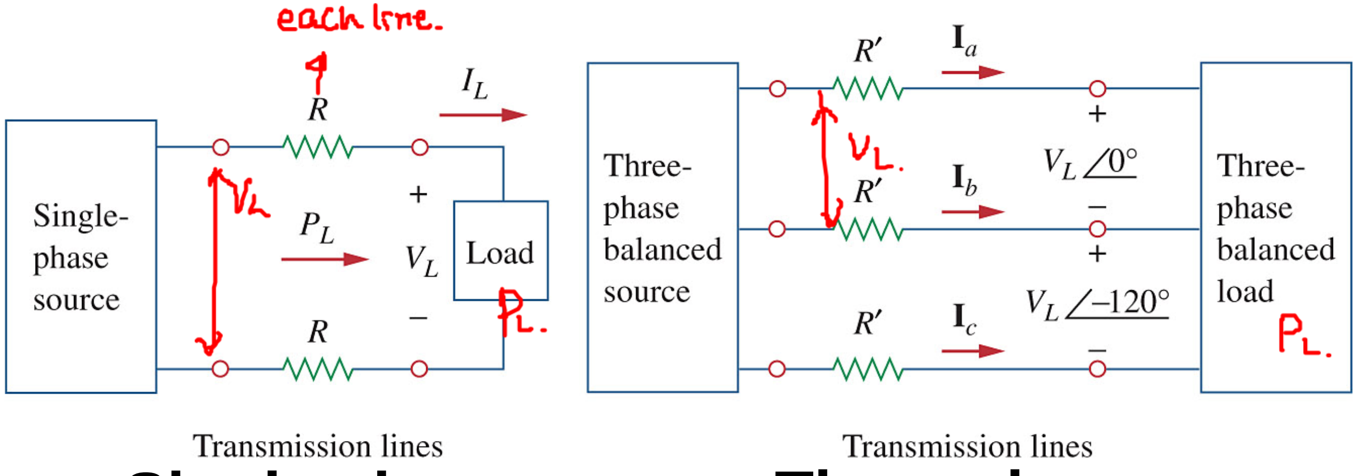
$\mathbf{I_a} = \mathbf{V_{an}}/|\mathbf{Z_Y} + \mathbf{Z_l}| = 240/|17+j15+0.4+j1.2| = 240/|17.4+j16.2| = 240/23.77 = 10.095$

$\mathbf{S} = 3[(I_a)^2(17+j15)] = 3x101.91(17+j15)$

$= \mathbf{[5.197+j4.586]\ kVA}$.

Three phase system - Advantage 2:

The three-phase system uses a lesser amount of wire than the single-phase system for the same line voltage V_L and **the same absorbed power P_L** → Economical

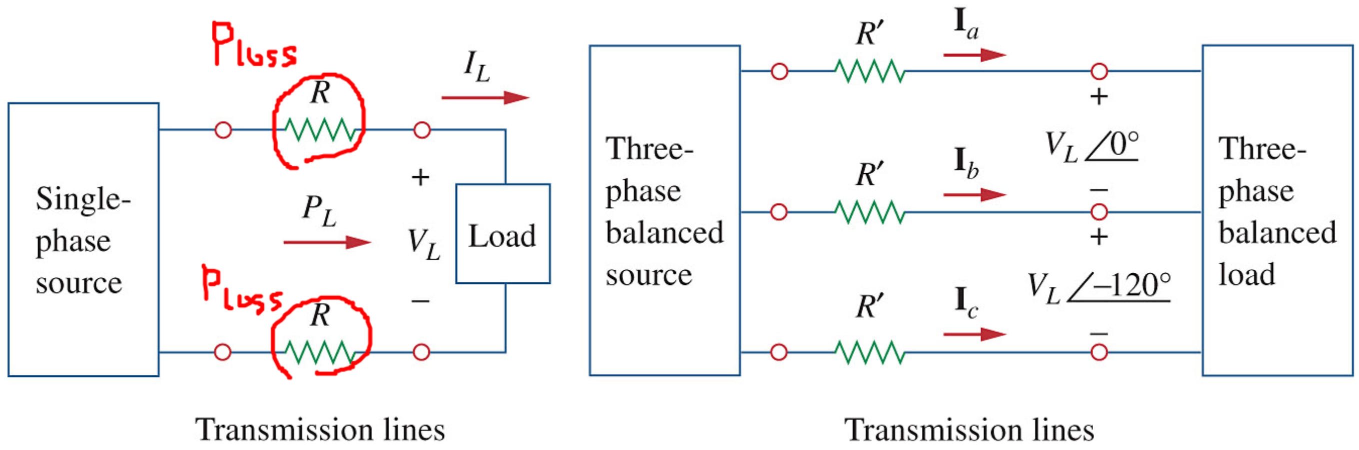


Single phase **Three phases**

1. The same total power delivered P_L
2. The same line voltage V_L

Recall: Average power in the rms form in Chapter 11

$$P = \frac{1}{2}V_m I_m \cos(\theta_v - \theta_i) = V_{rms} I_{rms} \cos(\theta_v - \theta_i)$$



Assume that the load is purely resistive

For the single-phase **two-wire system**, $P_L = V_L I_L$, the power loss in the two wires is

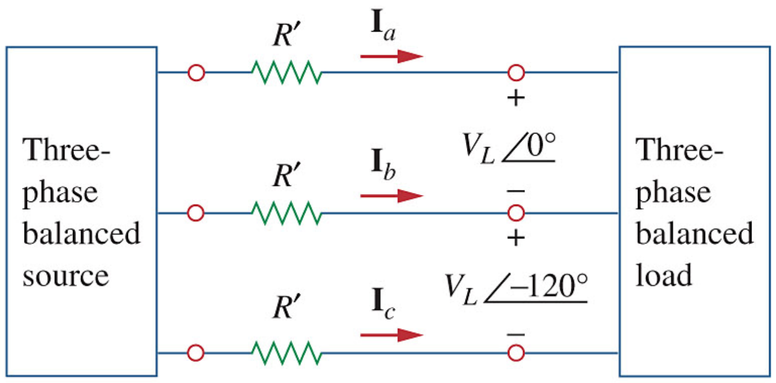
P at R. → fixed for both.

$$P_{loss} = 2\boxed{I_L^2 R} = 2\left(\frac{P_L}{V_L}\right)^2 R$$

2 wires

Recall: Average power in the rms form in Chapter 11

$$P = \frac{1}{2}V_m I_m \cos(\theta_v - \theta_i) = V_{\text{rms}} I_{\text{rms}} \cos(\theta_v - \theta_i)$$



Transmission lines

I′$_L$: line current
R′: line resistance

$$I'_L = |\mathbf{I}_a| = |\mathbf{I}_b| = |\mathbf{I}_c| = P_L / \sqrt{3} V_L$$

3 VpIp.

For the three-phase wire system, $P_L = \sqrt{3} V_L I'_L$, the power loss in **the three wires** is

R.R′

$$P'_{loss} = 3 I_L'^2 R' = 3\left(\frac{P_L}{\sqrt{3}V_L}\right)^2 R' = \boxed{\left(\frac{P_L}{V_L}\right)^2 R'}$$

3 wires

The equations show that for **the same total power delivered P_L** and **the same line voltage V_L**,

$$P_{loss} = 2I_L^2 R = 2\left(\frac{P_L}{V_L}\right)^2 R$$ **2 wires**

$$P'_{loss} = 3I_L'^2 R' = 3\left(\frac{P_L}{\sqrt{3}V_L}\right)^2 R' = \left(\frac{P_L}{V_L}\right)^2 R'$$ **3 wires**

(2)
(3)

$$\frac{P_{loss}}{P'_{loss}} = \frac{2R}{R'} = \frac{2\cancel{\rho}\cancel{l}/(\cancel{\pi}r^2)}{\cancel{\rho}\cancel{l}/(\cancel{\pi}r'^2)} = \frac{2r'^2}{r^2}$$

$$R = \frac{\rho L}{A}$$

ρ = resistivity
L = length
A = cross sectional area

where ρ is resistivity; l is length of transmission line; and r is radius of the transmission line

If we consider **the same power loss** in both systems,

$$\frac{P_{loss}}{P'_{loss}} = \frac{2r'^2}{r^2} = 1 \quad \text{thus, } r^2 = 2r'^2$$

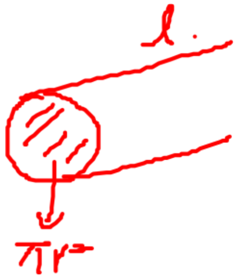
Two wires

Material volume needed

Two wires

Three wires

$$\frac{\text{Material for single-phase}}{\text{Material for three-phase}} = \frac{2(\pi r^2 l)}{3(\pi r'^2 l)} = \frac{2r^2}{3r'^2} = \frac{4}{3}$$



https://www.energy.gov/sites/prod/files/2015/12/f28/united-states-electricity-industry-primer.pdf

The second major advantage of three-phase systems for power distribution: **Economical**

Summary of the advantages of 3-ϕ system

1. The total instantaneous power in a balanced three-phase system is constant.

2. The material (transmission line) to deliver the same power and to tolerate the same loss needed is ¾ times less.

Example 12.8

$$S = P + jQ = 3V_P I_P \cos\theta + j3V_P I_P \sin\theta$$
$$= \sqrt{3}V_L I_L \cos\theta + j\sqrt{3}V_L I_L \sin\theta$$

Two balanced loads are connected to a 240-kV rms 60-Hz line, as shown in Fig. 12.22(a). Load 1 draws 30 kW at a power factor of 0.6 lagging, while load 2 draws 45 kVAR at a power factor of 0.8 lagging. Assuming the *abc* sequence, determine: (a) the complex, real, and reactive powers absorbed by the combined load, (b) the line currents, and (c) the kVAR rating of the three capacitors Δ-connected in parallel with the load that will raise the power factor to 0.9 lagging and the capacitance of each capacitor.

line voltage

$V_L = 240$ kV.

$S = 3V_P I_P^*$

$= \sqrt{3} V_L I_L^*$

30kW
pf=0.6 lagging

45kVAR
pf=0.8 lagging

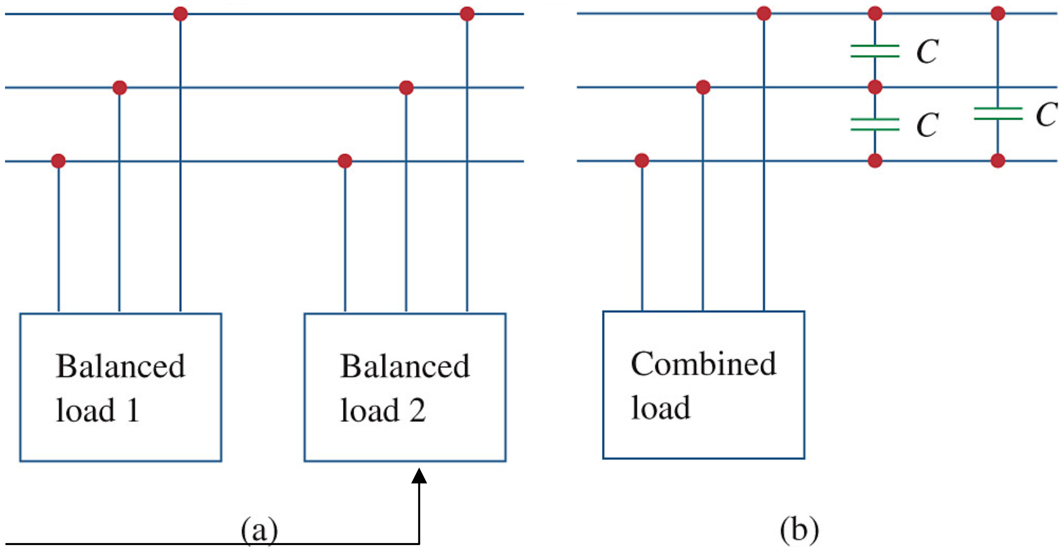
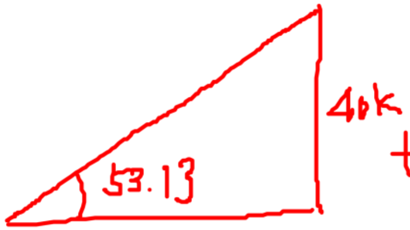


Figure 12.22 (a) The original balanced loads, (b) the combined load with improved power factor.

Load 1:
30kW
pf=0.6 lagging

Load 2:
45kVAR
pf=0.8 lagging

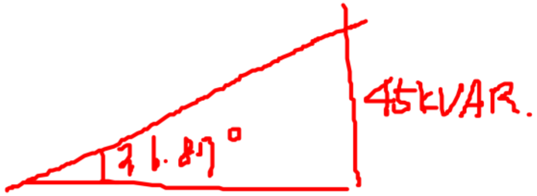
(a)



$\cos^{-1} 0.6 =$

$\tan 53.13 = \frac{Q_1}{P_1}$

$S_1 = 30k + j40k.$



$\cos^{-1} 0.8 = 36.87^\circ$

$\tan 36.87 = \frac{Q_2}{P_2}$ $\quad P_2 = 60k.$

$S_2 = 60k + j45k.$

$S = S_1 + S_2$

$= 90k + j85k.$

(b) $\sqrt{3} V_L I_L^* = 90k + j85k.$ 240kV

$I_L^* = \frac{90k + j85k.}{\sqrt{3} \times 240k}$

$= \frac{123.79 \angle 43.36^\circ}{\sqrt{3} \times 240}$

$= 0.298 \angle 43.36^\circ$

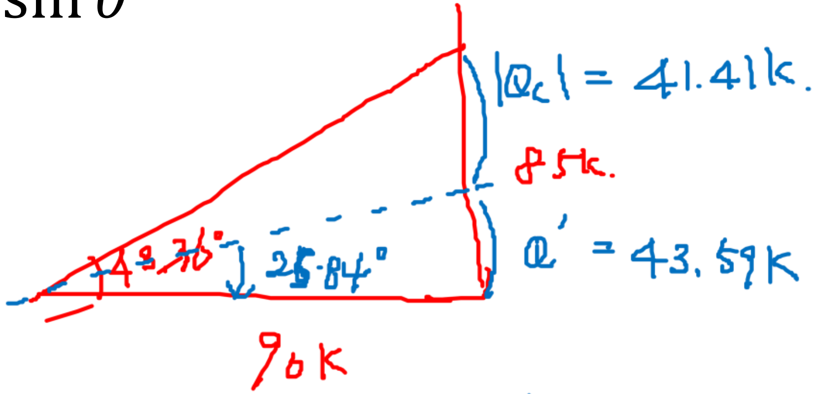
$I_L = 0.298 \angle -43.36^\circ$

$V_L = 240\text{kV}, 60\text{ Hz}$

$S = P + jQ = 3V_P I_P \cos\theta + j3V_P I_P \sin\theta$

$= \sqrt{3}V_L I_L \cos\theta + j\sqrt{3}V_L I_L \sin\theta$

$S = 90k + j85k.$



$C = \frac{1}{j\omega C}.$

$Q = \frac{V^2}{\omega C}.$

$pf = 0.9$ lagging $\rightarrow 25.84° \rightarrow \tan 25.84 = \frac{Q'}{90k}$

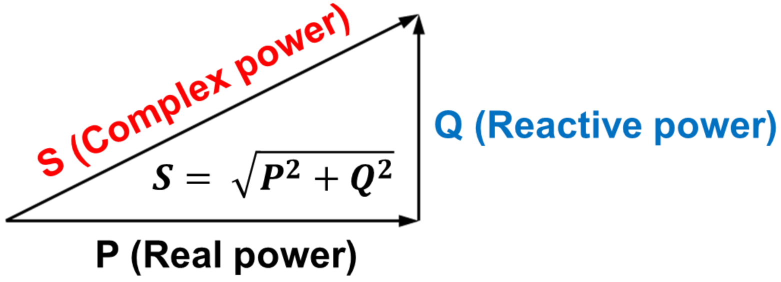
Q_c per Phase $41.41k/3 = 13.80k$ VAR

$Q_c = \omega C V^2 \Rightarrow 2\pi \times 60 \times C \times (240k)^2 = 13.80k.$

C per phase $= \frac{13.80k}{(240k)^2 \times 2\pi \times 60.} = 6.36 \times 10^{-10}$ F

(a) S, P, Q

Load 1: 30kW, pf=0.6 lagging



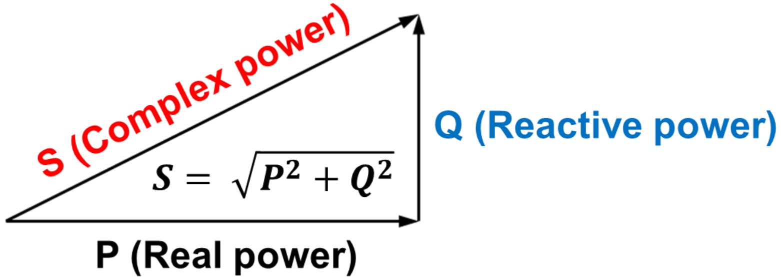
$\cos \theta_1 = 0.6 \rightarrow \theta_1 = 53.13^\circ$

$\tan 53.13^\circ = Q/P$

Thus, Q = 40k [VAR]

$\mathbf{S_1 = 30k + j40k}$ **[VA]**

Load 2: 45kVAR, pf=0.8 lagging



$\cos \theta_2 = 0.8 \rightarrow \theta_2 = 36.87^\circ$

$\tan 36.87^\circ = Q/P$

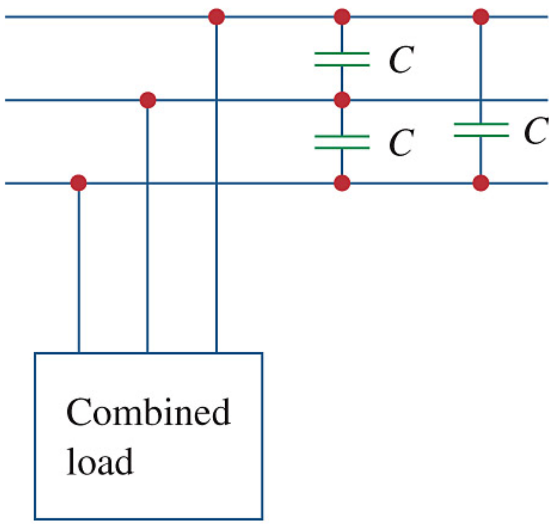
Thus, P = 60k [W]

$\mathbf{S_1 = 60k + j45k}$ **[VA]**

Complex power absorbed by the combined load, therefore, is

S = 90k + j85k [VA] where P = 90kW and Q = 85kVA

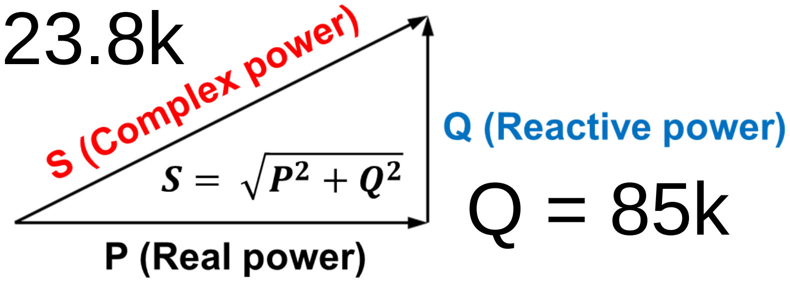
(b) Line currents



240 kV rms 60-Hz line → V_L = 240 kV

S from (a) is 90k + j85k

|S| = 123.8k



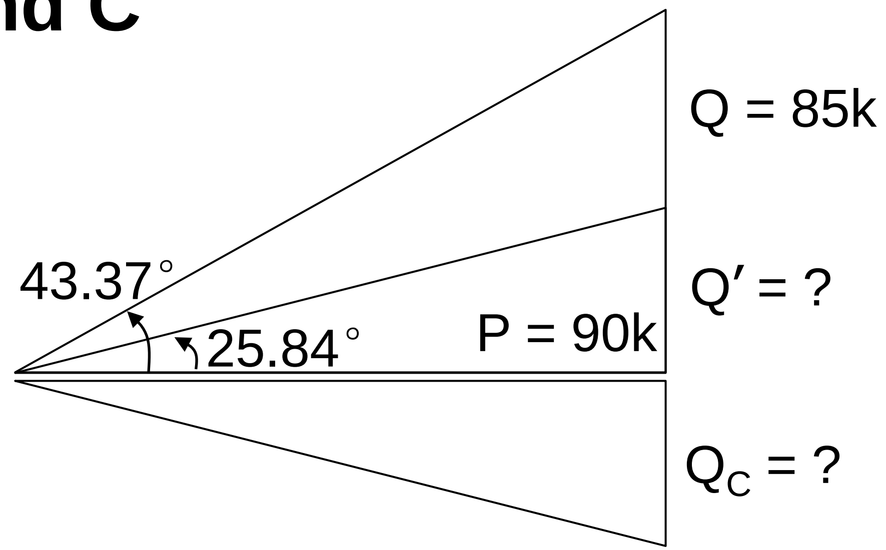
Q = 85k

P = 90k

$$P = \sqrt{3} V_L I_L \cos\theta \rightarrow 90k = \sqrt{3}\, 240k\, I_L\, {}^{90}/_{123.8}$$

Thus, I_L = 0.296 A or 0.296 mA

(c) Q_C and C



pf 0.9 lagging

$$\cos\theta' = 0.9 \rightarrow \theta' = 25.84°$$

$$Q' \rightarrow \tan 25.84 = \frac{Q'}{P(90k)} \rightarrow Q' = 43.56k$$

Q_C = Q – Q′ = 85k – 43.56k = **41.44k VAR**

→ Each capacitor has an effect of 13.81k VAR

$Q_C = I^2X = \omega CV^2$ for purely capacitive case, and thus,

$$C = \frac{Q_C}{\omega(=2\pi f)V^2} = \mathbf{6.36 \times 10^{-10}}[\boldsymbol{F}]$$