

VE311 RC4 MOSFET

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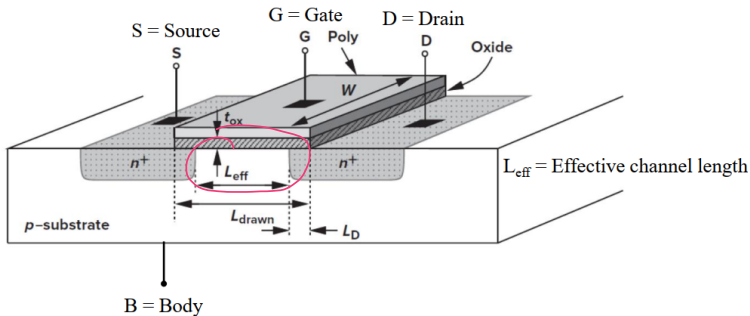
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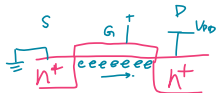
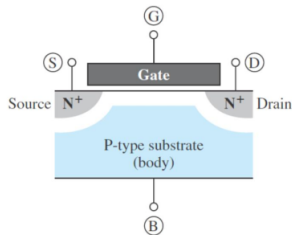
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- 1 MOSFET Physics
- 2 Second Order Effects
- 3 Small-Signal Model
- 4 Exercise

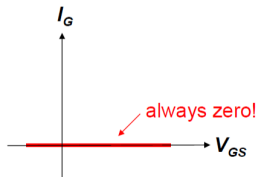
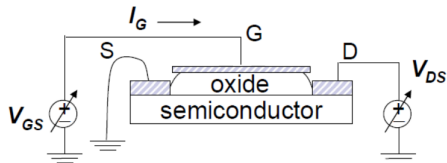


- ▶ $L_{eff} = L_{drawn} - 2L_D$
- ▶ If not specify L , we assume it is L_{eff}



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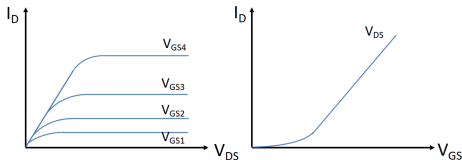
- ▶ $V_{GS} < 0$, attract holes to surface: Accumulation, not we want
- ▶ $V_{GS} > V_T$, induce electrons: Inversion, form channel
- ▶ If not apply V_{DS} , no current
- ▶ How to distinct Source (S) and Drain (D)
 - ▶ Since both S and D are doped with same concentration, it depends on how you apply voltage
 - ▶ Electrons flow from source to drain. Current I_{DS} or I_D , drain to source
 - ▶ Positive voltage: Drain $V_{DS} > 0$
 - ▶ S and D can switch by changing voltage

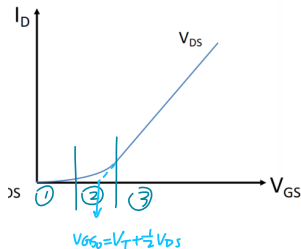


- Gate is insulated from the semiconductor, always 0

$$I_D = \begin{cases} 0 & V_{GS} - V_T < 0 \\ \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_T)^2 & 0 \leq V_{GS} - V_T < V_{DS} \\ \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_T - \frac{1}{2} V_{DS}) V_{DS} & V_{GS} - V_T \geq V_{DS} \end{cases}$$

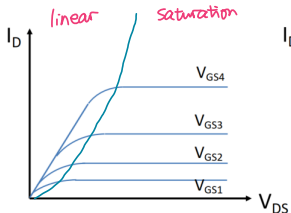
Summary of I_D





► Fixed V_{DS}

1. When $V_{GS} < V_T$, no current, $I_D = 0$
2. When $0 < V_{GS} - V_T < V_{DS}$, $I_D = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_T)^2$, I_D and V_{GS} follows **quadratic** relation.
3. When $V_{GS} - V_T > V_{DS}$, $I_D = \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_T - \frac{1}{2} V_{DS}) V_{DS}$, I_D and V_{GS} follows **linear** relation, the interception with x axis is $V_T + \frac{1}{2} V_{DS}$



► Fixed V_{GS} for each curve

1. When $0 < V_{DS} < V_{GS} - V_T$, $I_D = \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_T - \frac{1}{2} V_{DS}) V_{DS}$

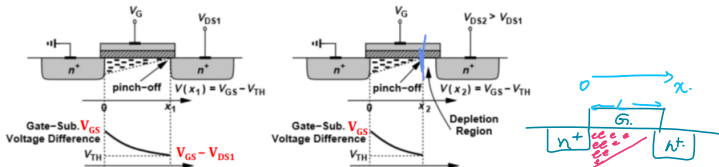
► When $0 < V_{DS} \ll 2(V_{GS} - V_T)$, V_{DS}^2 can be ignored. Then

$I_D = \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_T) V_{DS}$, I_D and V_{DS} follows **linear** relationship. We call this **Linear/ Triode/ Resistive** region

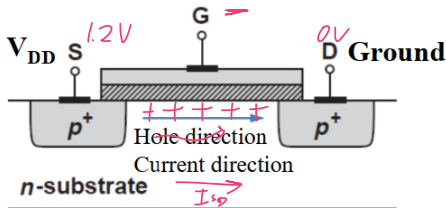
► S to D can be represented by a linear $R_o = \frac{1}{\mu_n C_{ox} \frac{W}{L} (V_{GS} - V_T)}$


2. When $V_{DS} > V_{GS} - V_T$, $I_D = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_T)^2$, I_D has no relation with V_{DS} , current saturate. We call this **Saturation** region.

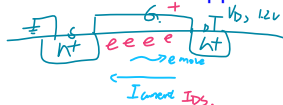
*How does saturation happen - Pinch off



- ▶ $I_D = WQ_n(x)v$. $Q_n(x)$ is charge per unit area. $v = \mu_n E$
 - ▶ Inversion layer charge density $|Q_n(x)| = C_{ox}(V_{GS} - V_T - V(x))$, where $V(x) = \frac{V_{DS}}{L}x$
 - ▶ When x increases, $|Q_n(x)|$ decreases
1. When $0 < V_{DS} < V_{GS} - V_T$: At L , $|Q_n(x)| > 0$, still has electrons, **no pinch off**
 2. When $V_{DS} = V_{GS} - V_T$: At L , $|Q_n(x)| = 0$, **start to pinch off**
 3. When $V_{DS} > V_{GS} - V_T$: Before L , $|Q_n(x)| = 0$, **pinch off**. MOSFET reaches **saturation** region, even if we increase V_D , I_D will not change since $|Q_n(x)|$ will not change.
- ▶ Electrons can still pass through the pinch-off region because of E_{bi}

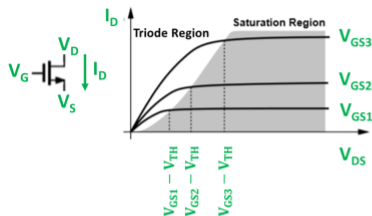
$$V_{SD} > 0 \text{ or } V_{DS} < 0$$


- ▶ $V_{GS} < 0$, attract holes as channel.
 - ▶ In PMOS, V_T is usually smaller than 0. To turn on the device, $V_{GS} < V_T$
 - ▶ Holes from source to drain. Current I_{SD} , source to drain
 - ▶ Positive voltage: Source. $V_{SD} > 0$. Current direction is opposite from NMOS (I_{DS})
- 



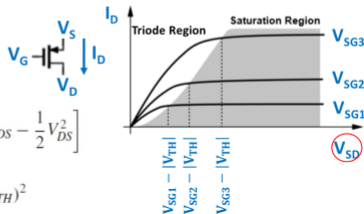
From slides

NMOS vs PMOS



$$\text{Triode region: } I_D = \mu_n C_{ox} \frac{W}{L_{eff}} \left[(V_{GS} - V_{TH}) V_{DS} - \frac{1}{2} V_{DS}^2 \right]$$

$$\text{Saturation region: } I_D = \frac{1}{2} \mu_n C_{ox} \frac{W}{L'} (V_{GS} - V_{TH})^2$$



$$\text{Triode region: } I_D = -\mu_p C_{ox} \frac{W}{L} \left[(V_{GS} - V_{TH}) V_{DS} - \frac{1}{2} V_{DS}^2 \right]$$

$$\text{Saturation region: } I_D = -\frac{1}{2} \mu_p C_{ox} \frac{W}{L'} (V_{GS} - V_{TH})^2$$

NMOS and PMOS IMPORTANT!

To simplify the equation, we can use the following universal formula by simply adding $| \quad |$ on I_D , $V_{GS} - V_T$, and V_{DS} .

This equation is valid for both NMOS and PMOS, and either V_T is positive or negative.

$$I_D = \begin{cases} 0 & |V_{GS}| - |V_T| < 0 \\ \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (|V_{GS} - V_T|)^2 & 0 \leq |V_{GS} - V_T| < |V_{DS}| \\ \mu_n C_{ox} \frac{W}{L} (|V_{GS} - V_T| - \frac{1}{2}|V_{DS}|)|V_{DS}| & |V_{GS} - V_T| \geq |V_{DS}| \end{cases}$$

Universal Formula

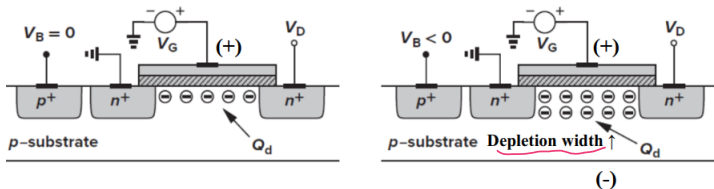
► Usually defined in saturation region. $I_D = \frac{1}{2}\mu_n C_{ox} \frac{W}{L} (V_{GS} - V_T)^2$

✳ $g_m = \frac{dI_D}{dV_{GS}} = \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_T) = \sqrt{2\mu_n C_{ox} \frac{W}{L} I_D} = \frac{2I_D}{V_{GS} - V_T}$

► High g_m , small change in V_{GS} will lead to large change in I_D . High sensitivity.

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Second Order Effects - Body Effect



- Initially $V_B = 0$, now $V_B < 0$. Attract more holes to bottom, leaving more electrons to surface. Wider depletion region. V_{TH} increases.

- $V_{TH} = V_{TH0} + \gamma(\sqrt{|2\Phi_F + V_{SB}|} - 2\sqrt{|2\Phi_F|})$

- $\gamma = 0$, no body effect

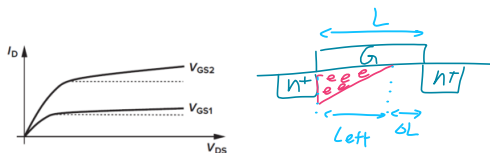
define:

- $g_{mb} = \frac{dI_D}{dV_{BS}} = \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_T)^{\frac{\gamma}{2}} \frac{1}{\sqrt{|2\Phi_F + V_{SB}|}} = g_m \eta.$

- $\Delta I_D = \Delta V_{BS} * g_{mb}$, when $V_{BS} (> 0)$ increases (V_{SB} becoming more negative), I_D increases

- $g_m = \frac{dI_D}{dV_{GS}} = \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_T) = \sqrt{2\mu_n C_{ox} \frac{W}{L} I_D} = \frac{2I_D}{V_{GS} - V_T}.$

- $\Delta I_D = \Delta V_{GS} * g_m$, when $V_{GS} (> 0)$ increases, I_D increases



- ▶ After reaching saturation region, when $\Delta L \ll L_{eff}$ is not satisfied, the effect of V_{DS} on I_D cannot be ignored. Now we use $L' = L_{eff} - \Delta L$, where ΔL is the pinch-off length.
- ▶ $I_D = \frac{1}{2} \mu_n C_{ox} \frac{W}{L'} (V_{GS} - V_T)^2 = \frac{1}{2} \mu_n C_{ox} \frac{W}{L_{eff}} (V_{GS} - V_T)^2 (1 + \frac{\Delta L}{L_{eff}}) = \frac{1}{2} \mu_n C_{ox} \frac{W}{L_{eff}} (V_{GS} - V_T)^2 (1 + \lambda V_{DS})$, λ is the slope

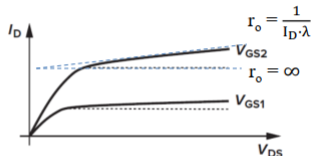
With the channel-length modulation,

$$I_D = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH})^2 (1 + \lambda V_{DS})$$

$$g_m = \frac{\partial I_D}{\partial V_{GS}} = \mu_n C_{ox} \frac{W}{L_{eff}} (V_{GS} - V_{TH}) (1 + \lambda V_{DS})$$

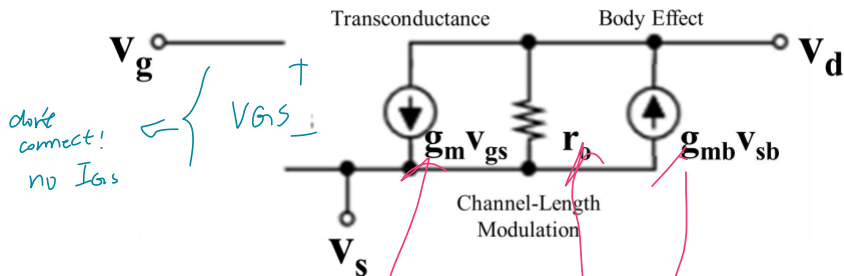
$$r_o = \frac{\partial V_{DS}}{\partial I_D} = 1 / \frac{\partial I_D}{\partial V_{DS}} = \frac{1}{\frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH})^2 \cdot \lambda}$$

$$\approx \frac{1}{I_D \cdot \lambda}$$



Channel-length modulation is reflected in g_m and r_o by λ

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- ▶ $\Delta I_D = g_m \Delta V_{GS} \rightarrow i_d = g_m V_{gs}$, add voltage controlled current source
- ▶ Consider channel length modulation ($\lambda \neq 0$): $r_o = \frac{dV_{DS}}{dI_D} \rightarrow i_d = \frac{V_{DS}}{r_o}$, add a resistor r_o
- ▶ Consider body effect ($\gamma \neq 0$): $g_{mb} = \frac{dI_D}{dV_{BS}} \rightarrow i_d = g_{mb} V_{bs}$, add voltage controlled current source. If $V_{SB} > 0$, we reverse the direction of the current source to make each term positive value
- ▶ This small-signal diagram is the same for PMOS

- ▶ For DC analysis, we are required to calculate I or V .
- ▶ If the question specify which region the MOSFET is now working in, apply the equation for I directly
- ▶ If not, assume the MOSFET is in saturation region, because the equation for I is much easier. $|V_{DS}| > |V_{GS} - V_T| \leftarrow \text{pMOS.}$
- ▶ Apply the formula $I_D = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_T)^2$ to calculate I and V
- ▶ Check whether $|V_{DS}| > |V_{GS} - V_T|$ is indeed true
 - ▶ If indeed true, then it is in saturation region, you get the answer
 - ▶ If not, it is in linear region, and use $I_D = \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_T) V_{DS}$ to calculate I and V again

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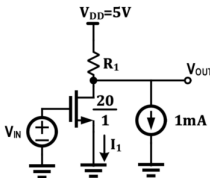
Exercise 1

For the following problems, assume: $\mu_n C_{ox} = 100 \mu A/V^2$, $V_{TH} = 1 V$.

Problem 1: For the circuit below, perform the following calculations:

See solution.

- Find I_1 when $V_{IN} = 1.2 V$ and $R_1 = 2 k\Omega$.
- If W/L of the transistor is changed to $W/L = 80/1$, compute the new value of overdrive voltage (V_{OV}) such the current I_1 remains the same as in part (a).
- Find the maximum value of R_1 which ensures that the transistor remains in saturation.
- Determine the minimum value of supply voltage V_{DD} to bias the transistor in saturation.



- ▶ b): $V_{ov} = V_{GS} - V_{TH}$
- ▶ c): $V_{IN} = 1.2 V$
- ▶ d): $V_{IN} = 1.2 V$, $R_1 = 2 k\Omega$

ANS

Exercise 2

$$\mu_n C_{ox} = 100 \mu A/V^2, V_{TH} = 1V$$

Problem 2: Consider the circuit below. For $R_D = 5 k\Omega$ and $R_S = 1 k\Omega$, find I_D , V_D , and V_S .

Step 1. Suppose it is in saturation.

$$I = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{th})^2$$

$V_{GS} = V_{GS} - V_{th}$
 $V_D \geq V_G - 1 = 1V$
 V_S unknown.

$$I = \frac{V_S}{R_S}$$

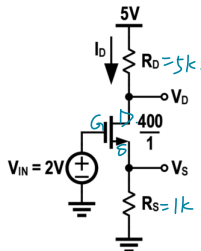
$$V_S = 1.25V \text{ or } 0.8V.$$

Decision:
 $V_{GS} - V_{th} > 0$
 $2 - V_S - 1 > 0$
 $V_S < 1V$

$$I = \frac{V_S}{R_S} = \frac{0.8}{1k} = 0.8 mA$$

$$V_D = 5 - I R_D = 5 - 0.8 mA \times 5k = 1V$$

indeed in saturation.



ANS

Exercise 3

$$\mu_n C_{ox} = 100 \mu A/V^2, V_{TH} = 1V$$

Problem 3: For the circuit below $V_{IN} = 2.8V$, find the value of I_D and V_{OUT} .

★ self-bias first. M2:

$$V_{D2} = V_{G2}$$

$$V_{GS2} > V_{GS1} - V_{th}$$

M1 is in saturation.

$$I_2 = \frac{1}{2} \mu_n C_{ox} \left(\frac{W}{L} \right)_2 (V_{GS2} - V_{th})^2 \quad (1)$$

Step 1. suppose M1 is in saturation

$$V_{DS1} > V_{GS1} - V_{th}$$

$$V_D > V_{G1} - V_{th} = 2.8 - 1 = 1.8V$$

$$I_1 = \frac{1}{2} \mu_n C_{ox} \left(\frac{W}{L} \right)_1 (V_{GS1} - V_{th})^2 \quad (2)$$

$$(1) = (2)$$

$$V_{GS1} - V_{th} = V_{GS2} - V_{th}$$

$$V_{GS1} - V_{th} = \frac{V_{GS1} - V_{S1}}{2.8}$$

$$V_{S1} = V_{D2} = V_{G2}$$

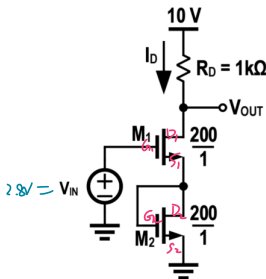
$$V_{GS2} = 2.8 - V_{G2}$$

$$V_{GS1} = 1.4V = V_{D2} = V_{S1}$$

$$I_1 = 1.6mA$$

$$V_{D1} = V_{GS1} - I_1 R_D = 1.4 - 1.6mA \times 1k = -0.4V \Rightarrow \text{indeed in saturation.}$$

||
V_{out}



Step 2
check.

ANS

- Analyze the self-bias stage M2 first