



Closed Loop Response – 2

- *Concept of Resonant Peak*
- *Closed Loop Bandwidth*



ω - Domain Physical Parameters

We know that **time domain** is the real **physical** domain in which the **dynamics** of any system **evolves**.

However, **s-domain**, though **synthetic** in nature, does involve ' ζ ' and ' ω_d ' which are physically **measurable**.

ω - domain, a special case of **s-domain**, also contains **closed loop response features** e.g. GCO, PCO, GM, PM.



ω - Domain Physical Parameters

Here, it is **worth** noting that while **GCO & PM** are related to ' ζ ' and ' ω_n ', and, hence, to **time response** features, by themselves, these **do not** have any physical **interpretation**.

In **view** of the above, we need **features** of closed loop in ω - **domain**, which can have **physical** connotations.

In this regard, we consider **resonant peak**, **bandwidth** as two **possible** features that not only have **physical** meaning but also can be **extracted** from closed loop **response**.



ω - Domain Physical Parameters

Resonant peak is the maximum **amplitude** that a system shows in its **frequency** response and is **indicative** of behaviour in **relation** to time domain **inputs**.

Similarly, **bandwidth** is frequency up to which the **system** will show a **significant** response (i.e. $> 70\%$).

Therefore, we can **extract** these features from **closed loop** response and **assess** the possible **time** domain **behaviour**.



Resonant Frequency and Peak



Resonant Frequency & Amplitude

Closed loop systems, comprising **2nd order** factors, exhibit the **resonance** when subjected to **sinusoidal** inputs.

This has **given** rise to the concepts of **resonant** frequency & amplitude, which are important **figures of merit** of the closed loop frequency **response**.

The resonant **frequency** is the frequency at which the **closed** loop system gives **maximum** output.

We know that **peak** magnitude directly impacts the peak **overshoot** if resonant **frequency** is present in the **input**.



Amplitude Formulation

We can **obtain** closed loop **frequency response** as follows.

$$\frac{C(j\omega)}{R(j\omega)} = \frac{\omega_n^2}{-\omega^2 + j2\zeta\omega_n\omega + \omega_n^2} = Me^{j\alpha}$$
$$M = \frac{1}{\sqrt{\left(1 - \frac{\omega^2}{\omega_n^2}\right)^2 + \left(2\zeta \frac{\omega}{\omega_n}\right)^2}}; \quad \alpha = -\tan^{-1} \left(\frac{2\zeta \frac{\omega}{\omega_n}}{1 - \frac{\omega^2}{\omega_n^2}} \right)$$



Resonance Solution

Maximum value of 'M' is obtained as follows.

$$\frac{d}{d\omega} \left(\left(1 - \frac{\omega^2}{\omega_n^2} \right)^2 + \left(2\zeta \frac{\omega}{\omega_n} \right)^2 \right) = 0 \rightarrow 1 - \frac{\omega_r^2}{\omega_n^2} = 2\zeta^2$$

$$\omega_r = \omega_n \sqrt{1 - 2\zeta^2}; \quad M_r = \frac{1}{2\zeta \sqrt{1 - \zeta^2}}; \quad \alpha_r = -\tan^{-1} \left(\frac{\sqrt{1 - 2\zeta^2}}{\zeta} \right)$$



Resonance Solution Attributes

We note that **resonant peak** is directly related to ' ζ ' while resonant **frequency** is dependent on both ' ζ ' & ' ω_n '.

Hence, we can obtain the **dominant** pole location, so also the time **response** features, from **resonance** condition.

We further see that for $\zeta = 1/\sqrt{2}$, $\omega_r = 0$, indicating that there is **no resonance** beyond this damping **value**.

Lastly, we see that at this **damping**, phase angle is **zero**.



Resonance Solution Attributes

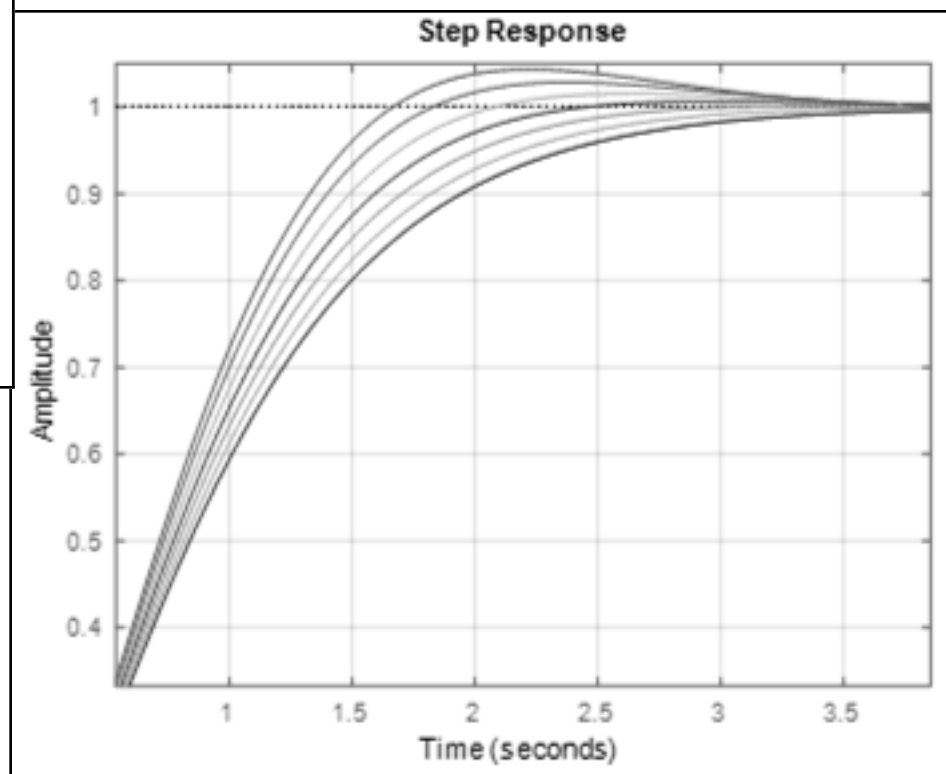
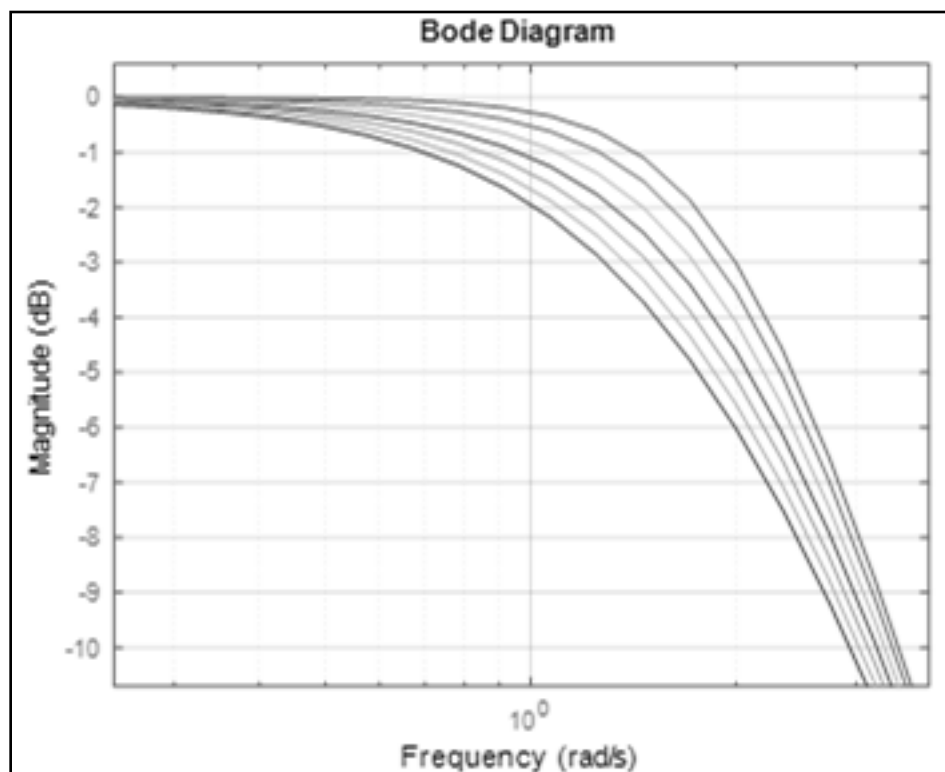
We find that we can get the **same** solution by putting $M_r = 1$, indicating **no** resonance.

We also find that as ' ζ ' increases beyond **0.707**, the system shows a **1st** order type frequency **response**, even **though** the poles in **s-domain** are **complex conjugate**.

Above behaviour of ' M_r ' is found to be **correlated** with the variation of ' M_p ' with ' ζ ' and is **commonly** used as **indicator** of the time **response** directly.



$M_r - M_p$ Correlation





Summary

Closed loop response is typically **specified** through resonant **peak**, which correlates **well** with the **peak overshoot** of time response.



Cut-off Frequency & Bandwidth



Bandwidth As Response Attribute

In addition to **GCO**, ω_n and ω_d , **bandwidth** of closed loop system is also an **important** response feature that is strongly **correlated** to time response.

It is worth noting that **bandwidth** indicates that closed loop **time response** will be **substantial** at all those **frequencies** which are **within** the bandwidth and present in the **input**.



Cut-off Frequency & Bandwidth

Most physical **systems** are described using a **proper** transfer function so that $|G(j\omega)| \rightarrow 0$ as $\omega \rightarrow \infty$.

Therefore, it is clear that **high frequency** input will generate **negligible output**.

This behaviour is **commonly** quantified through the concepts of **cut-off** frequency and **bandwidth**.



Cut-off Frequency & Bandwidth

Bandwidth is actually an **indicator** of the frequencies of input **signals** that the system is **capable** of tracking.

In this context, it is **worth noting** that all inputs in **time domain** can be represented through an **infinite series** of harmonic components, also called the '**Fourier Series**'.

Thus, it is clear that a **specific input** will not be tracked **correctly**, unless the system **bandwidth** contains all the frequencies that **comprise** that input.

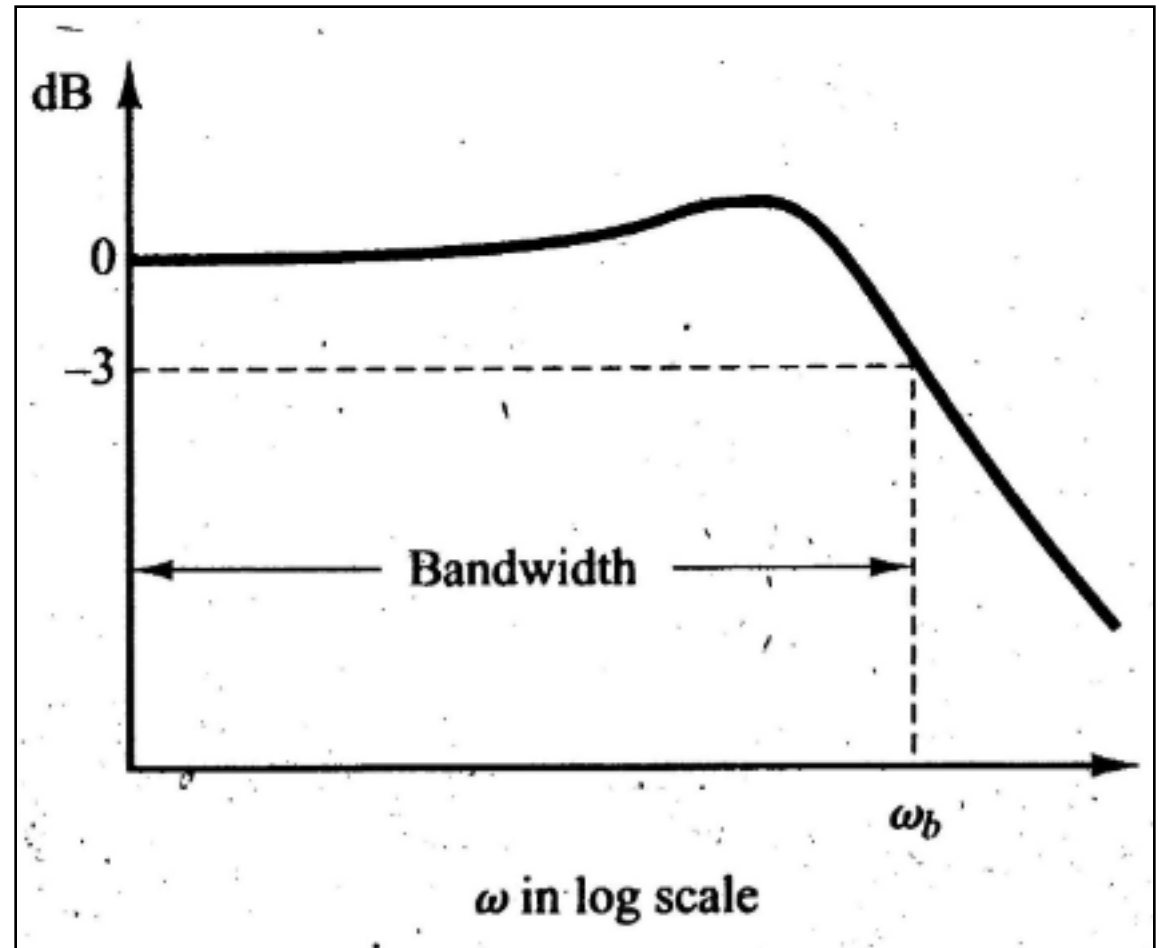


Cut-off Frequency & Bandwidth

Cut-off frequency is defined as **frequency** above which, **bode magnitude** is **below '0' dB** by 3 dB or more.

Cut-off frequency indicates that beyond this value, $P_o \leq 0.5P_i$ (Half-power point).

Bandwidth is range of **frequencies** up to the **cut-off frequency**.





Bandwidth as Response Feature

We can use closed loop **bandwidth** as a response feature, which is **related** to ' ω_n ', ' ζ ', and is derived **as follows**.

$$20 \log_{10} \left| \frac{C(j\omega_b)}{R(j\omega_b)} \right| = -3dB \rightarrow \bar{\omega}_b = \frac{\omega_b}{\omega_n}; \quad \frac{1}{\sqrt{(1 - \bar{\omega}_b^2)^2 + (2\zeta\bar{\omega}_b)^2}} = \frac{1}{\sqrt{2}}$$
$$(1 - \bar{\omega}_b^2)^2 + (2\zeta\bar{\omega}_b)^2 = 2 \rightarrow \omega_b = \omega_n \sqrt{\sqrt{(1 - 2\zeta^2)^2 + 1} + (1 - 2\zeta^2)}$$

We **note** that for $\zeta = 1/\sqrt{2}$, $\omega_b = \omega_n$.



ω - Domain Specification Example

Determine the **frequency domain** equivalent of the following **time domain** specifications.

1. Peak overshoot = **12%**, Settling time = **4 sec** (2%)

s-Domain Parameters: $\zeta = 0.56$, $\omega_n = 1.786$, $\omega_d = 1.48$

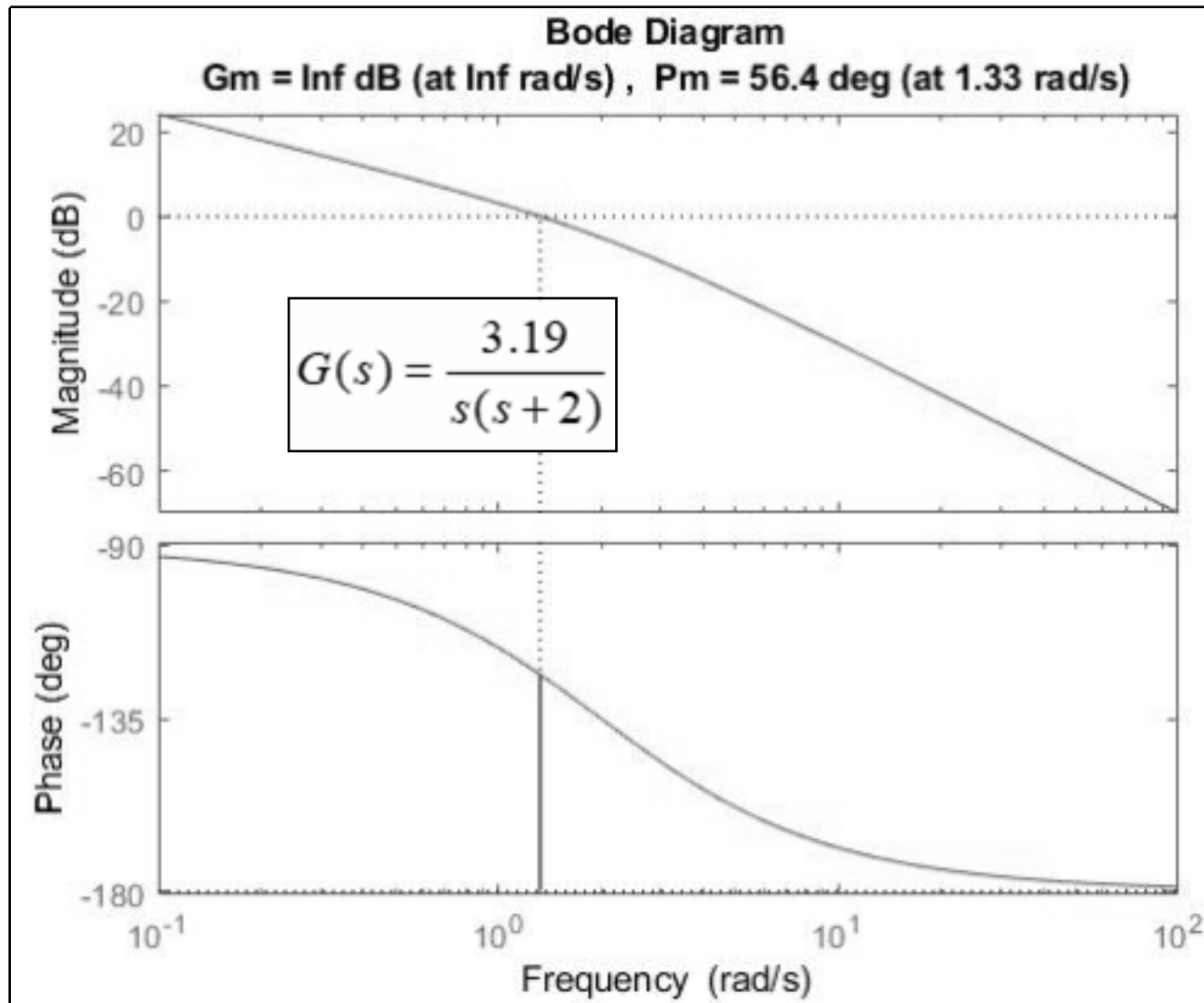
GCO & PM: $\omega_{GCO} = 1.328$, $PM = 56.4^\circ$

Resonant Frequency & Peak: $\omega_r = 1.09$, $M_r = 1.078$

Bandwidth: $\omega_b = 2.14$

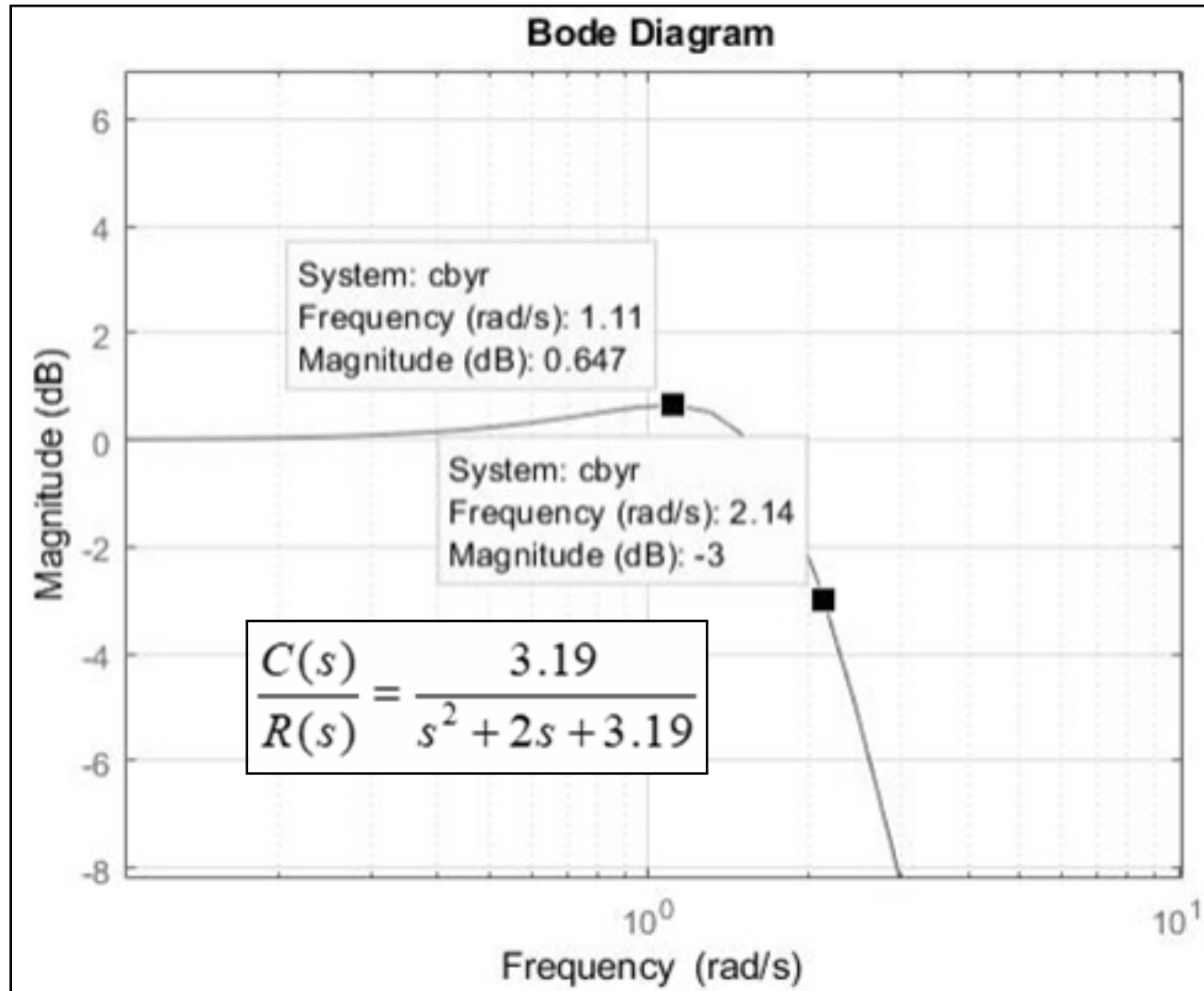


Verification of GCO, PM





Verification of M_r , ω_r and ω_b





Summary

Bandwidth is an important response **attribute** which is closely correlated to **speed** of response in time domain and **undamped** natural frequency in **Laplace** domain.