



# **EE340: Communications Laboratory**



## **Prelab Material**

### **Lab 6: Non-linearity and its effects in communication systems**



# Non-linear Systems

- Linear Systems: Satisfy superposition principle
- However, any practical system is non-linear (amount of non-linearity may vary)
- Non-linearity results in generation of “new frequency components” – i.e. frequency components that are not there at the input of the system.

- Memoryless non-linearity can be modeled as:

$$y(t) = a_1 x(t) + a_2 x^2(t) + a_3 x^3(t) + a_4 x^4(t) \dots$$

- Memoryless means present output depends only on the present output (also see Appendix – last slide)

# Effects of Non-Linearity

Consider a simplified non-linear system described by

$$y(t) = a_1 x(t) + a_2 x^2(t) + a_3 x^3(t)$$

For  $x(t) = A \cos(\omega t)$ ,

$$y(t) = \frac{1}{2} a_2 A^2 + \left( a_1 + \frac{3}{4} a_3 A^2 \right) A \cos(\omega t) + \frac{1}{2} a_2 A^2 \cos(2\omega t) + \frac{1}{4} a_3 A^3 \cos(3\omega t)$$

**Important observations:**

- **Second order non-linearity**  
**( $a_2$  coefficient):**

**Adds DC + 2<sup>nd</sup> harmonic**

$$\frac{1}{2} a_2 A^2 (1 + \cos(2\omega t))$$

- **Third order non-linearity**  
**( $a_3$  coefficient):**

**Adds 3<sup>rd</sup> harmonic and Gain becomes**  
**input amplitude (A) dependent**

**Also,  $a_3$  is generally negative**

**=> gain compression**

**with increasing A**

$$\left( a_1 + \frac{3}{4} a_3 A^2 \right) A \cos(\omega t) + \frac{1}{4} a_3 A^3 \cos(3\omega t)$$

Gain :  $\left( a_1 + \frac{3}{4} a_3 A^2 \right)$

# Second Order Non-Linearity

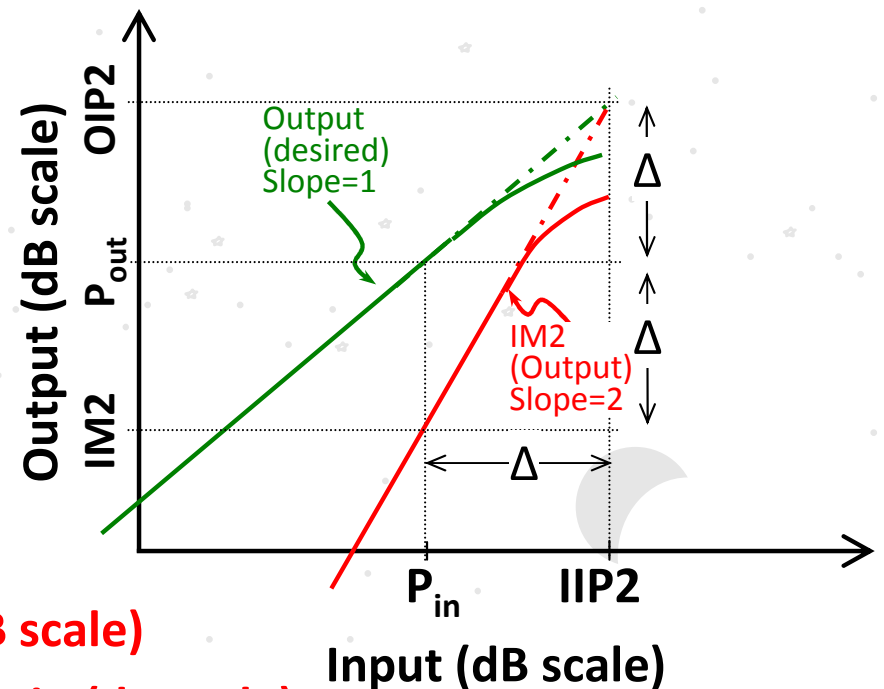
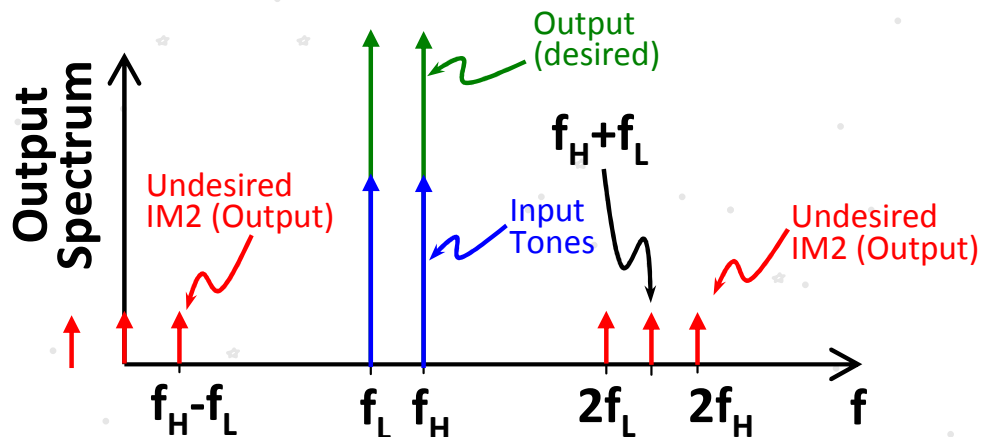
Consider a non-linear system described by

$$y(t) = a_1 x(t) + a_2 x^2(t); \quad \Rightarrow \text{For } x = A(\cos \omega_1 t + \cos \omega_2 t):$$

$$y(t) = a_2 A^2 + a_1 A(\cos(\omega_1 t) + \cos(\omega_2 t)) + a_2 A^2 \left( \frac{\cos(2\omega_1 t) + \cos(2\omega_2 t)}{2} + \cos((\omega_1 - \omega_2)t) + \cos((\omega_1 + \omega_2)t) \right)$$

The undesired spectral components generated due to the second order non-linearity coefficient  $a_2$  at frequencies 0,  $2\omega_1$ ,  $2\omega_2$ ,  $2(\omega_1 - \omega_2)$  and  $2(\omega_1 + \omega_2)$  are called IM2 (Inter-Modulation products due to 2<sup>nd</sup> order non-linearity) components

## Observations:

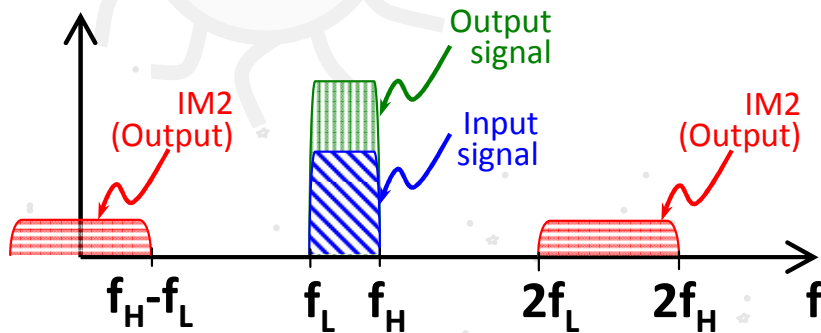


$$IIP2 = P_{in} + \Delta \text{ (dB scale)}$$

$$OIP2 = P_{in} + \Delta + \text{Gain (dB scale)}$$

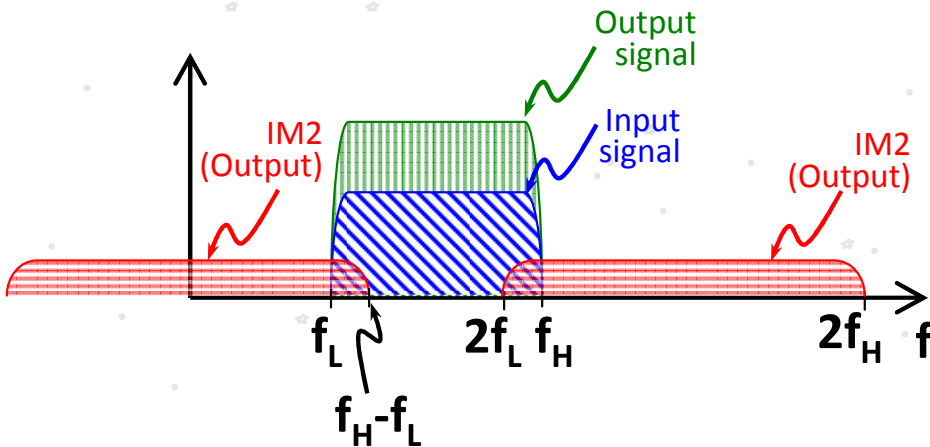
# Second Order Non-Linearity

## More observations:



**Sub-octave:**  $f_H < 2f_L$  (i.e.  $BW < f_L$ )

- No in-band IM2 distortion –out-of-band IM2 components can easily be filtered out
- DC components can sometimes cause amplifier saturation



**Multi-octave:**  $f_H > 2f_L$  (i.e.  $BW > f_L$ )

- In-band IM2 distortion present, can't be filtered out
- DC components may cause amplifier saturation

# Third Order Non-Linearity

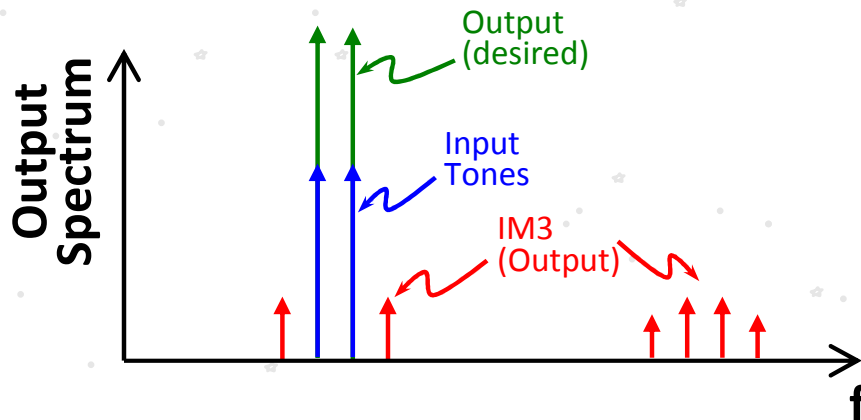
Consider a non-linear system described by

$$y(t) = a_1 x(t) + a_3 x^3(t); \quad \Rightarrow \text{For } x(t) = A \cos(\omega_1 t) + A \cos(\omega_2 t):$$

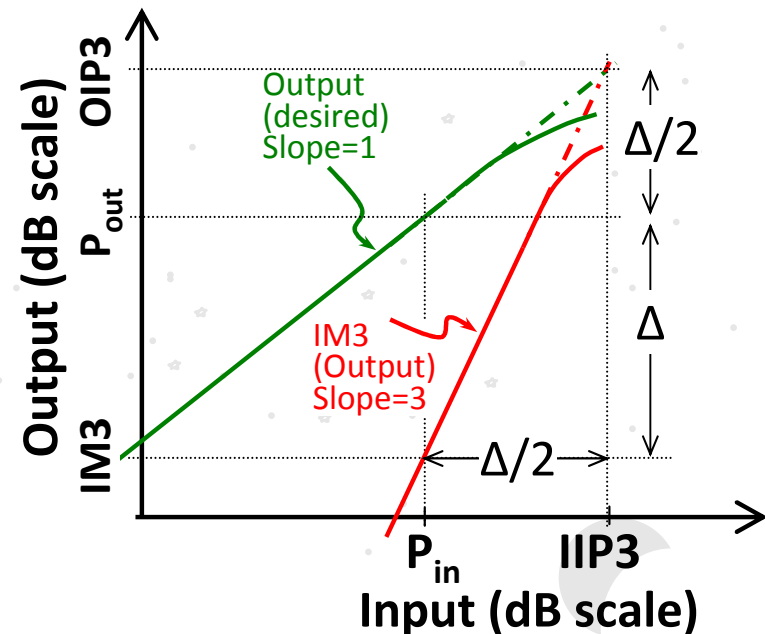
$$y(t) = A \left( a_1 + \frac{9a_3 A^2}{4} \right) (\cos(\omega_1 t) + \cos(\omega_2 t)) + \frac{1}{4} a_3 A^3 (\cos(3\omega_1 t) + \cos(3\omega_2 t))$$

$$+ \frac{3}{4} a_3 A^3 [\cos((2\omega_1 - \omega_2)t) + \cos((2\omega_1 + \omega_2)t) + \cos((2\omega_2 - \omega_1)t) + \cos((2\omega_2 + \omega_1)t)]$$

Observations:



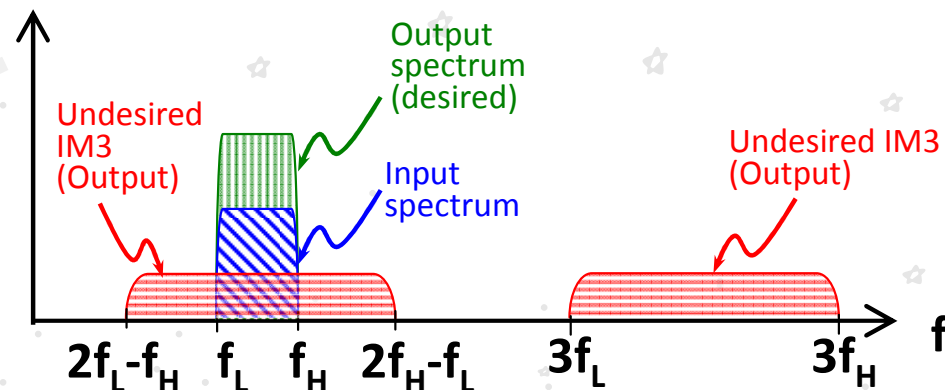
Generates in-band/adjacent band, out-of-band components, but no DC



$$IIP3 = P_{in} + \Delta/2 \text{ (dB scale)}$$

$$OIP3 = P_{in} + \Delta/2 + \text{Gain (dB scale)}$$

# Third Order Non-linearity

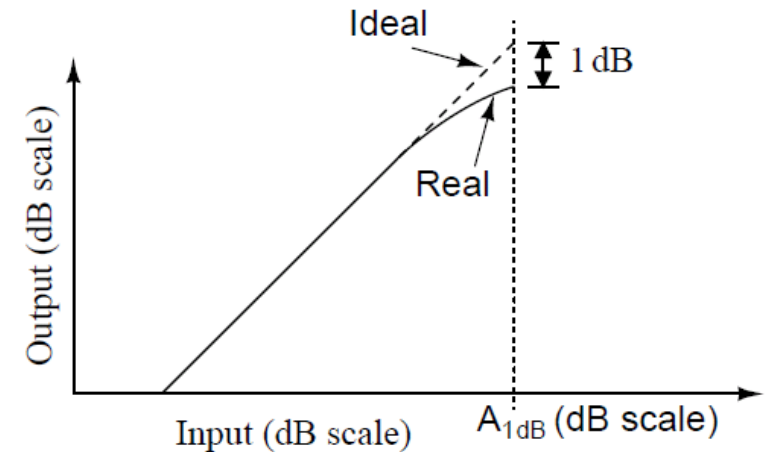


- The figure above shows the undesired spectrum generated by 3<sup>rd</sup> order non-linearity (i.e. due to non-zero  $a_3$  co-efficient)
- The undesired spectrum generated is called IM3 component, i.e. Inter-Modulation products due to 3<sup>rd</sup> order non-linearity component.
- Due to 3<sup>rd</sup> or odd order non-linearities (unlike 2<sup>nd</sup> or even order non-linearities), part of the spectrum is in-band and hence CANNOT be removed by filtering even for narrow-band inputs.
- Therefore, effects of 3<sup>rd</sup> (or odd) order non-linearities are more difficult to remove in general (then of even order non-linearities).

# Compression Point and Jamming

**1-dB compression point: Amplitude ( $A_{-1dB}$ ) at which gain decreases by 1-dB (without interferer) – because  $a_3$  is “almost always” negative.**

$$20 \log \left[ \frac{\left( a_1 + \frac{3}{4} a_3 A_{-1dB}^2 \right) A_{-1dB}}{a_1 A_{-1dB}} \right] = -1 \text{ dB} \Rightarrow A_{-1dB} \approx 0.40 \sqrt{\frac{a_1}{a_3}}$$



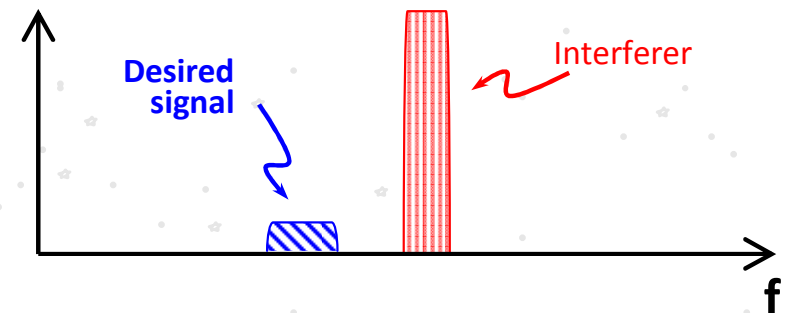
## Jamming / Blocking / Desensitization

Desired signal

Interferer

For  $x(t) = A \cos(\omega t) + B \cos(\omega_i t)$ ,

$$y(t) = \left( a_1 + \frac{3}{4} a_3 A^2 + \frac{3}{2} a_3 B^2 \right) A \cos(\omega t) + \text{other terms}$$



- Therefore, if interferer amplitude  $B \gg A$ , the receiver is jammed
- The transmitter can jam the receiver if they are operating concurrently, for example in full duplex systems (and isolation is poor)



# APPENDIX: Real Systems are not memory-less or linear: Non-linear dynamical behaviour

## Transfer function of a dynamic non-linear system

- Very complex, commonly expressed as the Volterra series

$$y(t) = a_0 + \sum_{n=1}^{\infty} \frac{1}{n!} \int_0^{\infty} \dots \int_0^{\infty} a_n(\tau_1, \tau_2, \dots, \tau_n) x(t - \tau_1) x(t - \tau_2) \dots x(t - \tau_n) d\tau_1 d\tau_2 \dots d\tau_n$$

$a_n$  is called the  $n^{\text{th}}$  order Volterra kernel

Therefore, a 2<sup>nd</sup> order dynamic non-linear system can be modeled as

$$y(t) = a_0 + \int_0^{\infty} a_1(\tau_1) x(t - \tau_1) d\tau_1 + \frac{1}{2} \int_0^{\infty} \int_0^{\infty} a_2(\tau_1, \tau_2) x(t - \tau_1) x(t - \tau_2) d\tau_1 d\tau_2$$