(3)

1. Determine the phase crossover frequency and gain margin for the following plant.

$$G(s) = \frac{20}{s(s+1)(s+5)}$$

$$\angle G(j\omega) = -90 - \tan^{-1}\omega - \tan^{-1}0.2\omega = -180 \to \tan(\tan^{-1}\omega + \tan^{-1}0.2\omega) = \infty$$

$$\frac{1.2\omega}{1 - 0.2\omega^{2}} = \infty \to 1 - 0.2\omega^{2} = 0 \to \omega_{PCO} = \sqrt{5} = 2.236$$

$$|G(j\omega_{PCO})| = \left|\frac{20}{\omega \times \sqrt{1 + \omega^{2}} \times \sqrt{25 + \omega^{2}}}\right|_{\omega = 2.236} = 0.667 \to GM = 1.5 \text{ or } 3.52dB$$

Further, if it is known that phase margin is 8.9°, and real closed loop pole is at -5.74, determine the location of closed loop dominant poles.

$$PM^o = 8.9 = 100\zeta \rightarrow \zeta = 0.089;$$
  $D(s) = s^3 + 6s^2 + 5s + 20$   
 $s^2 + 2\zeta\omega_n s + \omega_n^2 = \frac{D(s)}{(s+5.74)} = s^2 + 0.26s + 3.51 \rightarrow \omega_n = 1.87$   
 $\sigma = \zeta\omega_n = 0.13;$   $s_{1,2} = -0.13 \pm j1.86$  or  $-0.17 \pm j1.86$ 

2. Derive the expressions for peak time and peak overshoot in respect of a standard 2<sup>nd</sup> order closed loop transfer function, whose unit step response expression is as given below. (2)

$$c(t) = 1 - \frac{1}{\sqrt{1 - \zeta^2}} e^{-\zeta \omega_n t} \sin\left(\omega_d t + \tan^{-1} \frac{\sqrt{1 - \zeta^2}}{\zeta}\right)$$

$$\phi = \tan^{-1} \frac{\sqrt{1 - \zeta^2}}{\zeta} \rightarrow \tan \phi = \frac{\sqrt{1 - \zeta^2}}{\zeta}; \quad \sin \phi = \sqrt{1 - \zeta^2}; \quad \cos \phi = \zeta$$

$$\frac{dc(t)}{dt} = -\frac{1}{\sqrt{1 - \zeta^2}} e^{-\zeta \omega_n t} \left[-\zeta \omega_n \sin\left(\omega_d t + \phi\right) + \omega_d \cos\left(\omega_d t + \phi\right)\right] = 0$$

$$\tan\left(\omega_d t + \phi\right) = \frac{\omega_d}{\zeta \omega_n} = \frac{\sqrt{1 - \zeta^2}}{\zeta} = \tan \phi \rightarrow \frac{\tan(\omega_d t) + \tan \phi}{1 - \tan(\omega_d t) \tan \phi} = \tan \phi \rightarrow \tan(\omega_d t) \left[1 + \tan^2 \phi\right] = 0$$

$$\omega_d t = \pi \rightarrow t_p = \frac{\pi}{\omega_d}; \quad M_p = -\frac{1}{\sqrt{1 - \zeta^2}} e^{-\zeta \omega_n \times \pi/\omega_d} \left[\sin\left(\pi + \phi\right)\right] = \frac{1}{\sqrt{1 - \zeta^2}} e^{-\zeta \omega_n \times \pi/\omega_d} \sin \phi = e^{-\pi/2} \left[-\zeta/2\right]$$

3. Derive the expression for bandwidth of a standard  $2^{nd}$  order closed loop transfer function, as given below, in terms of  $\zeta$  and  $\omega_n$ .

$$G(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

$$|G(j\omega)| = \frac{\omega_n^2}{-\omega^2 + 2j\zeta\omega_n\omega + \omega_n^2} = \frac{\omega_n^2}{\sqrt{(\omega_n^2 - \omega^2)^2 + (2\zeta\omega_n\omega)^2}} = \frac{1}{\sqrt{2}}$$

$$(\omega_n^2 - \omega^2)^2 + (2\zeta\omega_n\omega)^2 = 2\omega_n^4 \to \omega^4 - 2(1 - 2\zeta^2)\omega_n^2\omega^2 - \omega_n^4 = 0$$

$$\omega^2 = \frac{2(1 - 2\zeta^2)\omega_n^2 + \sqrt{[2(1 - 2\zeta^2)\omega_n^2]^2 + 4\omega_n^4}}{2}$$

$$\omega^2 = (1 - 2\zeta^2)\omega_n^2 + \omega_n^2\sqrt{1 + (1 - 2\zeta^2)^2}; \quad \omega = \omega_n\sqrt{(1 - 2\zeta^2) + \sqrt{1 + (1 - 2\zeta^2)^2}}$$

4. Consider the following plant.

$$G(s) = \frac{K(s+1)}{s(s+2)(s+3)}$$

Determine the value of parameter, K'(>0), for which dominant pole(s) of unity feedback closed loop system is (are) at -0.5 and determine the nature of the dominant pole(s). (2)

$$1+G(s) = 1 + \frac{K(s+1)}{s(s+2)(s+3)} = \frac{s^3 + 5s^2 + (6+K)s + K}{s^3 + 5s^2 + 6s} = 0$$

$$s = z - 0.5; \quad D(z) = (z - 0.5)^3 + 5(z - 0.5)^2 + (6+K)(z - 0.5) + K = 0$$

$$D(z) = z^3 + 3.5z^2 + (1.75 + K)s + (0.5K - 1.875)$$

$$1.75 + K$$

$$3.5 \qquad 0.5K - 1.875$$

$$\frac{3K + 8}{3.5} \qquad 0$$

$$0.5K - 1.875$$

5. Determine the benchmark  $2^{nd}$  order closed loop transfer function which has a rise time of 1 sec and 2% ripple settling time of 2.5 sec. (Hint: You may use the following relations as applicable). (1)

$$t_{r} = \frac{1}{\omega_{d}} \tan^{-1} \left(\frac{\omega_{d}}{-\sigma}\right); \quad t_{s}(2\%) = \frac{4}{\sigma}$$

$$t_{s}(2\%) = \frac{4}{\sigma} = 2.5 \to \sigma = 1.6; \quad t_{r} = \frac{1}{\omega_{d}} \tan^{-1} \left(\frac{\omega_{d}}{-1.6}\right) = 1$$

$$\tan \omega_{d} = \frac{\omega_{d}}{-1.6} \to \omega_{d} = 1.6 \tan(\pi - \omega_{d}) \to \omega_{d} = 2.2$$

$$\zeta \omega_{n} = 1.6; \quad \omega_{n} \sqrt{1 - \zeta^{2}} = 2.2 \to \frac{1 - \zeta^{2}}{\zeta^{2}} = 1.89 \to \zeta = 0.59$$

$$\omega_{n} = 2.72; \quad \frac{C(s)}{R(s)} = \frac{7.4}{s^{2} + 3.2s + 7.4}$$

6. Derive the equation of constant 'M' trajectories for the unity negative feedback closed loop frequency response of a plant having  $G(j\omega)$  as its frequency response. (Hint: M is the magnitude of closed loop frequency response. You may use the following relation as applicable.). (1)

$$G(i\omega) = X(\omega) + iY(\omega)$$

$$G(j\omega) = X(\omega) + jY(\omega); \quad \frac{C(j\omega)}{R(j\omega)} = \frac{G(j\omega)}{1 + G(j\omega)} = \frac{X + jY}{(1 + X) + jY}$$

$$M = \left| \frac{C(j\omega)}{R(j\omega)} \right| = \left| \frac{X + jY}{(1 + X) + jY} \right| = \frac{\left| X + jY \right|}{\left| (1 + X) + jY \right|} \rightarrow M^2 = \frac{X^2 + Y^2}{(1 + X)^2 + Y^2}$$

$$M \neq 1 \rightarrow X^2 \left( 1 - M^2 \right) - 2M^2 X - M^2 + \left( 1 - M^2 \right) Y^2 = 0$$

$$X^2 + \frac{2M^2}{M^2 - 1} X + \frac{M^2}{M^2 - 1} + Y^2 = 0 \rightarrow \left( X + \frac{M^2}{M^2 - 1} \right)^2 + Y^2 = \frac{M^2}{\left( M^2 - 1 \right)^2}$$
Circle with  $R = \frac{M}{\left( M^2 - 1 \right)}$ ; Centre:  $\left( -\frac{M^2}{M^2 - 1}, 0 \right)$ ;  $M = 1 \rightarrow X = -\frac{1}{2}$ 

7. Consider the plant given below.

$$G(s) = \frac{2(s-1)}{(s+1)}$$

Determine the cascade controller,  $G_c$  to achieve a closed loop damping of  $1/\sqrt{2}$  and undamped natural frequency of  $\sqrt{2}$  for the benchmark  $2^{nd}$  order response to a unit step input and determine its order and stability. (1)

$$\frac{C(s)}{R(s)} = \frac{2}{s^2 + 2s + 2}; \quad G_{eq} = \frac{2}{s(s+2)}; \quad G_c = \frac{G_{eq}}{G} = \frac{(s+1)}{s(s-1)(s+2)}$$

3rd order, type '1' unstable controller.

PAPER ENDS