Homogenous Transformation Matrix (SEC3) T=[R] of for 3-dimensional space, T is a 4x4 natrix exp: for 1-D,  $T = \begin{bmatrix} \cos\theta & -\sin\theta & \gamma_1 \\ \sin\theta & \cos\theta & \gamma_2 \end{bmatrix}$ \*Important:  $T' \neq T'$   $T' = \begin{bmatrix} R^T - R^TP \end{bmatrix}$   $T' = \begin{bmatrix} R^T - R^TP \end{bmatrix}$ For Tieseco, Treseco, Treseco Title SE(3)
(IiTa) = TicTaT3)
Title SE(3)
Title SE(3)  $T[X] = \begin{bmatrix} R & P \end{bmatrix}[X] \Rightarrow \text{ for a vector } U_b \text{ in from } b$   $\begin{bmatrix} V_s \\ 1 \end{bmatrix} = \begin{bmatrix} R_{sb}P_{bb} \\ 1 \end{bmatrix} = \begin{bmatrix} R_{sb}P_{bb} \\ 0 \end{bmatrix} \begin{bmatrix} V_b \\ 1 \end{bmatrix}$ Proposition: Given T=CR.P) ESEG) and X, y GR 0 || Tx - Ty || = ||x - y|| || || nears norm (1) <Tx-Ty, Ty-Tz>= <x-y, y-2> <x, x> means inner troduct Three uses of SEC3): (1) Represent the configuration (2) Change the frame representation to another frame

(3) A operation of moving a vector Tab = Toa TabTbc = Tac TabUb = Va K When we treat T as a displacement geration, huge difference between fre-multiply and post-multiply. Assume T = Trans (p) Rot (w.0), Tsb & SEG) OTTsb = Trans(p) Rot(w, f) Tsb Rotate first, then monspose, all operation means Esz as main frame (2) TsbT = Tsb Trans(p) Rot (w, p)

Translate first, then rotate, all operation meats {b} as main frome 铝门是先跃压为中心,Tu在后后,就在前推并以下的前一个sub-son种的frame 为基准 Just similar to R'R=[w], T'T=[[w]] Ub]

Just similar to RR=[w], TT=[o]

R'R represent angular velocity, TT represent the combination of angular and linear velocity.

A better way to represent the [Lwb] ub] is to introduce twist V=S0

S, whit screw axis, [w]

0, rate of change

$$U = \begin{bmatrix} W_{S} \\ V_{S} \end{bmatrix} \in \mathbb{R}^{6} \quad [V] = \begin{bmatrix} [W_{S}] \\ V_{S} \end{bmatrix} \in Sec_{2}$$

$$Just like [W_{b}] = \mathbb{R}^{5}b [W_{S}] \mathbb{R}^{5}b$$

$$[V_{b}] = \mathbb{R}^{5}b [V_{S}] \mathbb{R}^{5}b$$

$$[V_{b}] = \mathbb{R}^{5}b [V_{b}] \mathbb{R}^{5}b = \mathbb{R}^{5}[W_{b}]\mathbb{R}^{5} - \mathbb{R}[W_{b}]\mathbb{R}^{5}p + \mathcal{R}V_{b}]$$

$$[V_{S}] = \mathbb{R}^{5}b [V_{b}] \mathbb{R}^{5}b = \mathbb{R}^{5}[W_{b}]\mathbb{R}^{5} - \mathbb{R}[W_{b}]\mathbb{R}^{5}p + \mathcal{R}V_{b}]$$

Like RIWIRT = [Rw], [WP = - IP] w, we have

[WS] = [R] (Wb)

[VS] = [IP]R R (Vb)

[VS] Adjoint / Matrix (Vb)

[XS] (6x6)

For a T=CR, p) e SEC=), its odjoint motivix is

[Add] = [P] O

[P] R

Us = [AdTsb] Up = AdTsb(Ub)

For Ti, Tz & SEC3) and V = Cw, w, we have:

Adti(AdtzCv)) = [Adti][Adtz] V = AdtitzCv)=[Adtitz]v

Adti(Adtz(v)) = Adtitz(v) = Adt(v)

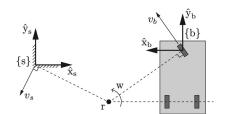


Figure 3.18: The twist corresponding to the instantaneous motion of the chassis of a three-wheeled vehicle can be visualized as an angular velocity w about the point r.

w = 2 rad/s about an axis out of the page at the point r in the plane. Inspecting the figure, we can write r as  $r_s=(2,-1,0)$  or  $r_b=(2,-1.4,0)$ , w as  $\omega_s=(0,0,2)$  or  $\omega_b=(0,0,-2)$ , and  $T_{sb}$  as

$$T_{sb} = \left[ egin{array}{ccc} R_{sb} & p_{sb} \ 0 & 1 \end{array} 
ight] = \left[ egin{array}{cccc} -1 & 0 & 0 & 4 \ 0 & 1 & 0 & 0.4 \ 0 & 0 & -1 & 0 \ 0 & 0 & 0 & 1 \end{array} 
ight].$$

From the figure and simple geometry, we get

$$v_s = \omega_s \times (-r_s) = r_s \times \omega_s = (-2, -4, 0),$$
  
 $v_b = \omega_b \times (-r_b) = r_b \times \omega_b = (2.8, 4, 0),$ 

and thus obtain the twists  $V_s$  and  $V_b$ :

$$v_{s} = \begin{bmatrix} \omega_{s} \\ v_{s} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 2 \\ -4 \\ 0 \end{bmatrix}, \quad v_{b} = \begin{bmatrix} \omega_{b} \\ v_{b} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ -2 \\ 2.8 \\ 4 \\ 0 \end{bmatrix}. \quad \text{Twist in \{s\} and \{b\}}$$

point r is in (2,-1,0) in  $\{s\}$  and (2,-1,0) in  $\{b\}$   $V_s = W \times (-\tau) = \begin{bmatrix} 0 \\ 1 \end{bmatrix} \times \begin{bmatrix} -2 \\ 1 \end{bmatrix} \times 2$   $= \begin{bmatrix} 0 \\ 1 \end{bmatrix} \times \begin{bmatrix} -2 \\ 1 \end{bmatrix} \times 2$   $V_b = \begin{bmatrix} 0 \\ 1 \end{bmatrix} \times \begin{bmatrix} -2 \\ 1 \end{bmatrix} = \begin{bmatrix} 2.8 \\ 4 \end{bmatrix}$ 

Representation of twist using screw axis  $0 \{9, \hat{s}, h\}$ , q is a point on  $\hat{s}$  axis h is notion of linear velocity to matter velocity  $V = \begin{bmatrix} w \\ v \end{bmatrix} = \begin{bmatrix} \hat{s} \hat{\theta} \\ -\hat{s} \hat{\theta} \times 9 + h \hat{s} \hat{\theta} \end{bmatrix}$ 

Screw Axis, S can be regarded as normalized version of twist, S=V/11w11 = V/0

If w=0, means no rotational motion, only linear h=linear velocity/rotational velocity, goes to version = 0, ||Sv||=1

If w=0, ||Sv||=1, ||Sv||=1

Some as twist 
$$V$$
,  $[S] = \begin{bmatrix} [w] & v \\ 0 & 0 \end{bmatrix}$   
 $Sa = [AdTab]Sb$ 

If a joint has a fitch property means it provides extra linear velocity in direction of screw notation axis.

OCalculate Sw and Sv as before, use  $v = -w \times r$  get the linear velocity given by rotation

Freat pitch as an extra component with linear velocity only in direction of screw rotation direction

3 Add together

Exp: 
$$Sw = [0], p=[0], \theta=1, pitch=3$$

$$0 Sv = -Sw \times r = [0]$$

$$v_1 = [Sw] \times \theta = [0]$$

3 
$$V = V_1 + V_2 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

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