



# Principles of Engineering Sciences

Dept. of Mechanical-Mechatronics Engineering

Type: UG core

Branch: All

Semester: 3<sup>rd</sup>

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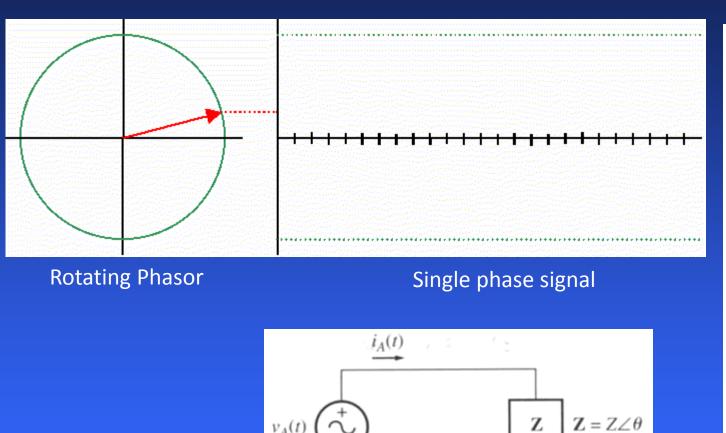
### Syllabus:

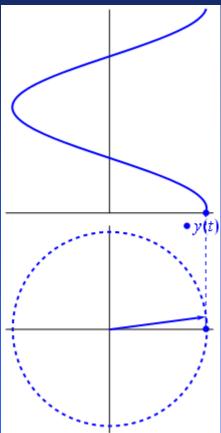
- Three phase systems: Generation of three phase voltagesadvantages of three phase systems, star and delta connection, 3 wire and four wire systems, relation between line and phase voltages & currents.
- Transformers: construction, types, emf equation, losses and efficiency
- DC Machines: DC generator- construction, types, emf equation, D.C motor- types, characteristics, applications.
- AC machines: Three phase induction motor, single phase induction motor, three-phase alternator- construction, principle of operation, characteristics, methods of starting.

### **Text Books**

- 1. Thereja B. L., Fundamentals of Electrical Engineering and Electronics —I, S. Chand & Co, New Delhi, 2012.
- 2. Chakrabarti A., et.al, *Basic Electrical Engineering*, TMH, 2012.
- 3. Hughes, *Electrical and Electronic Technology*, Pearson Education South Asia, 2011

# Single-Phase signal

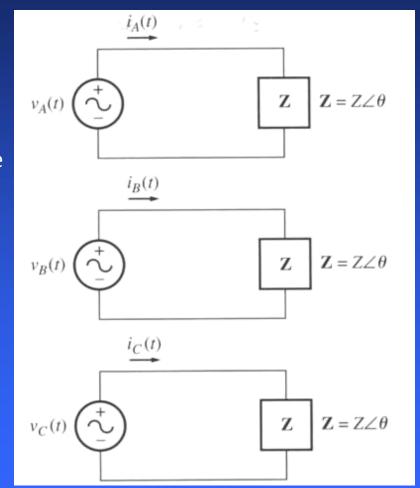


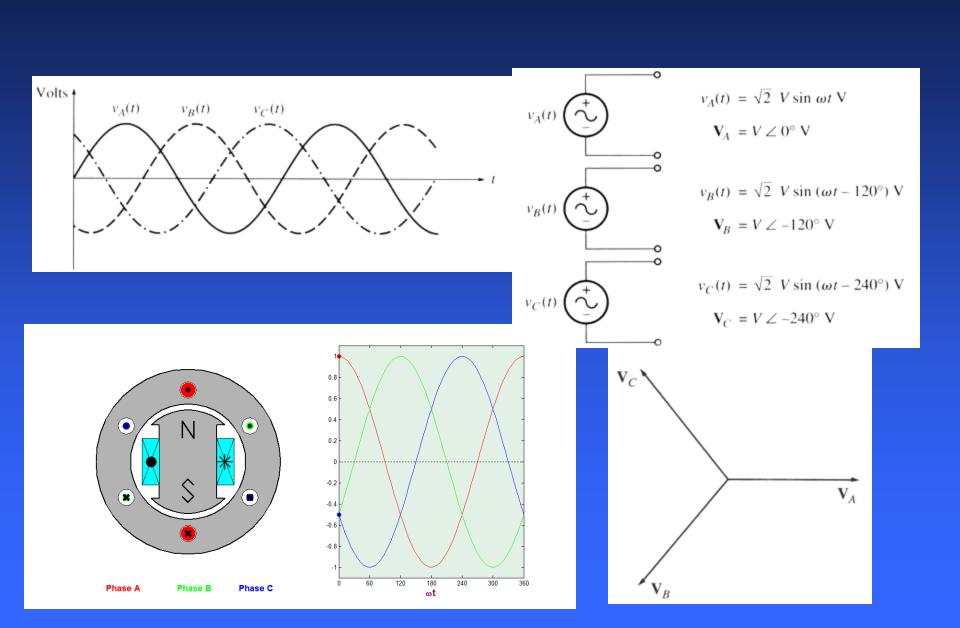


# Generating three-phase

#### **Applying constraints**

- 1. Amplitude of  $v_A v_B v_C$  are equal.
- 2. The voltages have a 120 ° phase difference between each other.
- 3. Connect identical loads to each supply.





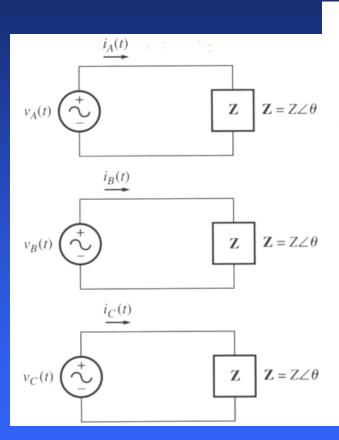
The current flowing to each load can be found as I = V/Z

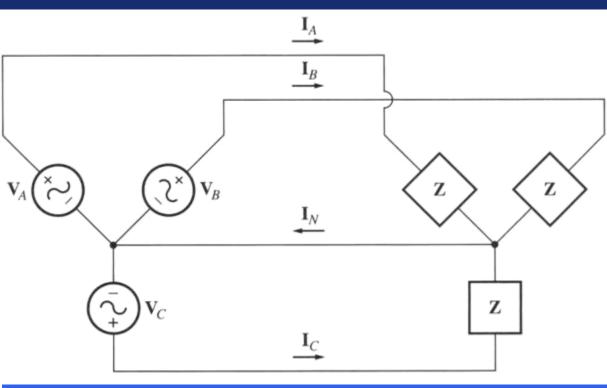
$$I_{A} = \frac{V \angle 0^{0}}{Z \angle \theta} = I \angle -\theta$$

$$I_{B} = \frac{V \angle -120^{0}}{Z \angle \theta} = I \angle -120 - \theta$$

$$I_{A} = \frac{V \angle -240^{0}}{Z \angle \theta} = I \angle -240 - \theta$$

Connect the grounds together using a single wire so the 3 circuits will have a single return path.





Therefore,  $I_N = I_A + I_B + I_C$ 

 $I_N = ?$ 

$$\begin{split} I_{N} &= I_{A} + I_{B} + I_{C} = I \angle -\theta + I \angle -\theta - 120^{0} + I \angle -\theta - 240^{0} \\ &= I \cos(-\theta) + jI \sin(-\theta) + I \cos(-\theta - 120^{0}) + jI \sin(-\theta - 120^{0}) + I \cos(-\theta - 240^{0}) + jI \sin(-\theta - 240^{0}) \\ &= I \Big[ \cos(-\theta) + \cos(-\theta - 120^{0}) + \cos(-\theta - 240^{0}) \Big] + jI \Big[ \sin(-\theta) + \sin(-\theta - 120^{0}) + \sin(-\theta - 240^{0}) \Big] \\ &= I \Big[ \cos(-\theta) + \cos(-\theta) \cos(120^{0}) + \sin(-\theta) \sin(120^{0}) + \cos(-\theta) \cos(240^{0}) + \sin(-\theta) \sin(240^{0}) \Big] \\ &+ jI \Big[ \sin(-\theta) + \sin(-\theta) \cos(120^{0}) - \cos(-\theta) \sin(120^{0}) + \sin(-\theta) \cos(240^{0}) - \cos(-\theta) \sin(240^{0}) \Big] \end{split}$$

$$\begin{split} I_N &= I \left[ \cos(-\theta) - \frac{1}{2}\cos(-\theta) + \frac{\sqrt{3}}{2}\sin(-\theta) - \frac{1}{2}\cos(-\theta) - \frac{\sqrt{3}}{2}\sin(-\theta) \right] \\ &+ jI \left[ \sin(-\theta) - \frac{1}{2}\sin(-\theta) + \frac{\sqrt{3}}{2}\cos(-\theta) - \frac{1}{2}\sin(-\theta) - \frac{\sqrt{3}}{2}\cos(-\theta) \right] \\ &= 0 \end{split}$$

The current through the neutral line can be found as zero as long as the load is balanced.

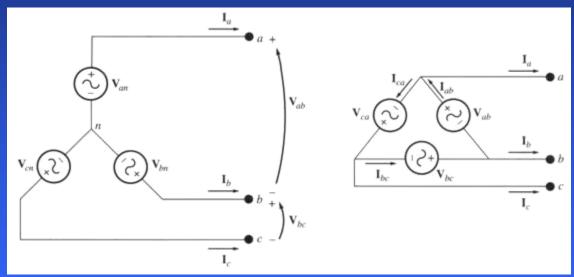
Therefore is the neutral line necessary?

In a balanced system, neutral is unnecessary!

### **Definitions**

- Represented as 3Ф
- 4 wires
  - 3 "active" phases, A(R), B(Y), C(B)
  - 1 "ground", or "neutral"
- Color Code
  - Phase A Red
  - Phase B Yellow
  - Phase CBlue
  - Neutral Black
- Phase sequence(RYB) order of phases in which individual voltages peak.

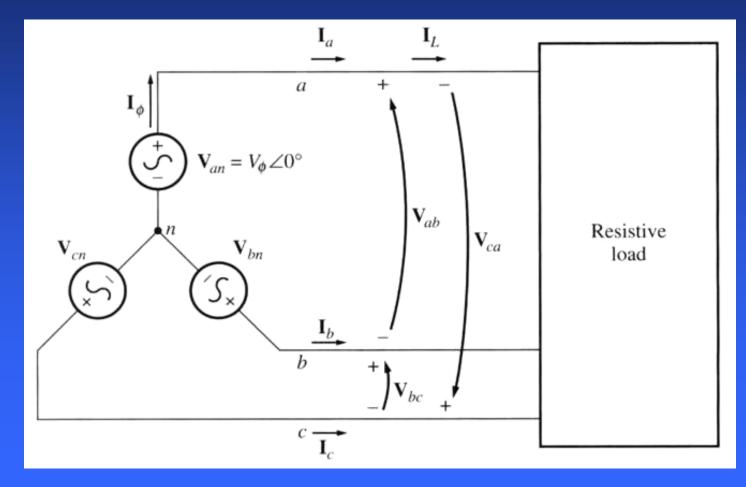
 There are two types of connections in threephase circuits: Y (star) and Δ (delta)



Phase quantities - voltages and currents in a given phase. Line quantities - voltages between the lines and currents in the lines connected to the generators.

#### 1. Y-connection

Assuming a resistive load...



### 1. Y-connection (cont)

$$V_{an} = V_{\phi} \angle 0^{0}$$

$$V_{bn} = V_{\phi} \angle -120^{0}$$

$$V_{cn} = V_{\phi} \angle -240^{0}$$

#### Since we assume a resistive load:

$$I_a = I_{\phi} \angle 0^0$$

$$I_b = I_{\phi} \angle -120^0$$

$$I_c = I_{\phi} \angle -240^0$$

#### 1. Y-connection (cont 2)

The current in any line is the same as the current in the corresponding phase.

$$oxed{I_L = I_{\phi}}$$

#### Voltages are:

$$V_{ab} = V_a - V_b = V_{\phi} \angle 0^0 - V_{\phi} \angle -120^0 = V_{\phi} - \left(-\frac{1}{2}V_{\phi} - j\frac{\sqrt{3}}{2}V_{\phi}\right) = \frac{3}{2}V_{\phi} + j\frac{\sqrt{3}}{2}V_{\phi}$$
$$= \sqrt{3}V_{\phi}\left(\frac{\sqrt{3}}{2} + j\frac{1}{2}\right) = \sqrt{3}V_{\phi} \angle 30^0$$

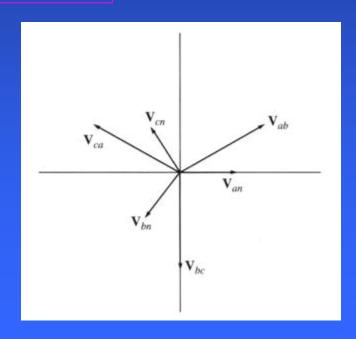
### 1. Y-connection (cont 3)

Magnitudes of the line-to-line voltages and the line-to-neutral voltages are related as:

$$V_{LL} = \sqrt{3}V_{\phi}$$

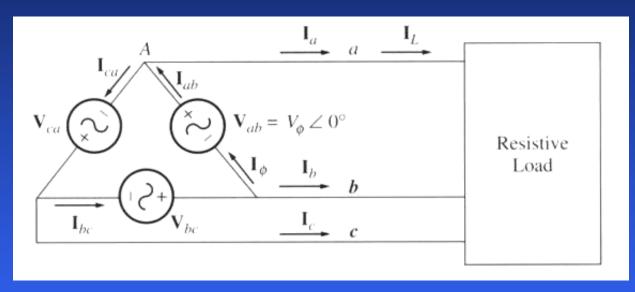
In addition, the line voltages are shifted by 30° with respect to the phase voltages.

In a connection with *abc* sequence, the voltage of a line **leads** the phase voltage.



#### 1. $\Delta$ -connection

assuming a resistive load:



$$V_{ab} = V_{\phi} \angle 0^{0}$$

$$V_{bc} = V_{\phi} \angle -120^{0}$$

$$V_{ca} = V_{\phi} \angle -240^{0}$$

$$I_{ab} = I_{\phi} \angle 0^{0}$$

$$I_{bc} = I_{\phi} \angle -120^{0}$$

$$I_{ca} = I_{\phi} \angle -240^{0}$$

#### 1. $\Delta$ -connection (cont)

$$V_{\scriptscriptstyle LL} = V_{\scriptscriptstyle \phi}$$

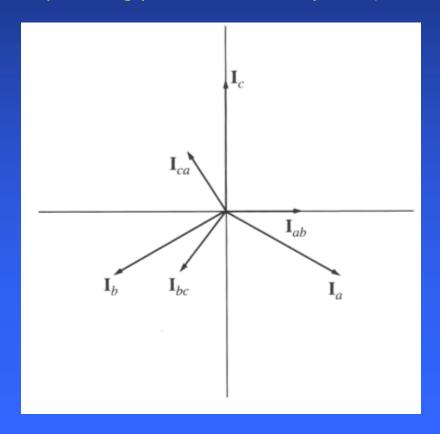
The currents are:

$$I_{a} = I_{ab} - I_{ca} = I_{\phi} \angle 0^{0} - I_{\phi} \angle 240^{0} = I_{\phi} - \left(-\frac{1}{2}I_{\phi} + j\frac{\sqrt{3}}{2}I_{\phi}\right)$$
$$= \frac{3}{2}I_{\phi} - j\frac{\sqrt{3}}{2}I_{\phi} = \sqrt{3}I_{\phi}\left(\frac{\sqrt{3}}{2} - j\frac{1}{2}\right) = \sqrt{3}I_{\phi} \angle -30^{0}$$

The magnitudes:

$$I_L = \sqrt{3}I_{\phi}$$

For the connections with the *abc* phase sequences, the current of a line lags the corresponding phase current by 30° (see Figure below).



For a balanced Y-connected load with the impedance  $Z_{\phi} = Z \angle \theta$ :

#### and voltages:

$$v_{an}(t) = \sqrt{2V} \sin \omega t$$

$$v_{bn}(t) = \sqrt{2V}\sin(\omega t - 120^{\circ})$$

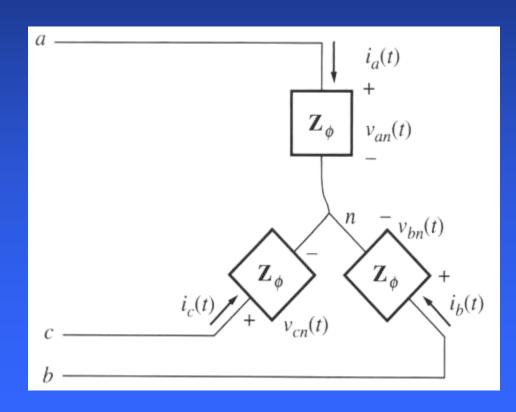
$$v_{cn}(t) = \sqrt{2V}\sin(\omega t - 240^{\circ})$$

#### The currents can be found:

$$i_a(t) = \sqrt{2}I\sin(\omega t - \theta)$$

$$i_b(t) = \sqrt{2}I\sin(\omega t - 120^0 - \theta)$$

$$i_c(t) = \sqrt{2}I\sin(\omega t - 240^0 - \theta)$$



The instantaneous power is:

$$p(t) = v(t)i(t)$$

Therefore, the instantaneous power supplied to each phase is:

$$p_{a}(t) = v_{an}(t)i_{a}(t) = 2VI\sin(\omega t)\sin(\omega t - \theta)$$

$$p_{b}(t) = v_{bn}(t)i_{b}(t) = 2VI\sin(\omega t - 120^{0})\sin(\omega t - 120^{0} - \theta)$$

$$p_{c}(t) = v_{cn}(t)i_{c}(t) = 2VI\sin(\omega t - 240^{0})\sin(\omega t - 240^{0} - \theta)$$

Since

$$\sin \alpha \sin \beta = \frac{1}{2} [\cos(\alpha - \beta) - \cos(\alpha + \beta)]$$

#### Therefore

$$p_{a}(t) = VI \left[ \cos \theta - \cos(2\omega t - \theta) \right]$$

$$p_{b}(t) = VI \left[ \cos \theta - \cos(2\omega t - 240^{0} - \theta) \right]$$

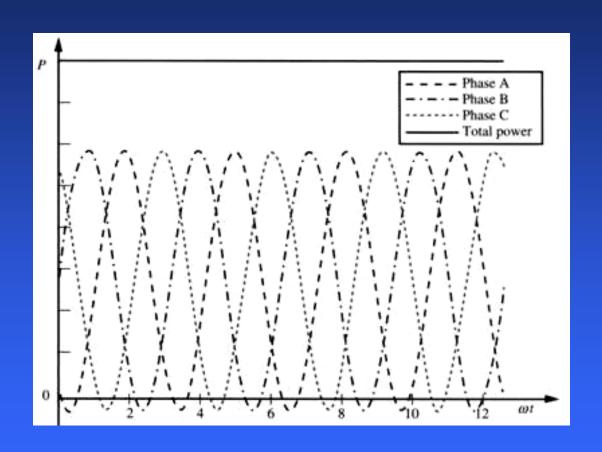
$$p_{c}(t) = VI \left[ \cos \theta - \cos(2\omega t - 480^{0} - \theta) \right]$$

The total power on the load

$$p_{tot}(t) = p_a(t) + p_b(t) + p_c(t) = 3VI \cos \theta$$

The instantaneous power in phases.

The total power supplied to the load is constant.



Line quantities: Y-connection.

Power consumed by a load:  $P = 3V_{\phi}I_{\phi}\cos\theta$ 

Since for this load  $I_L = I_\phi \ \ and \ \ V_{LL} = \sqrt{3} V_\phi$ 

Therefore:  $P = 3\frac{V_{LL}}{\sqrt{3}}I_L \cos \theta$ 

Finally:  $P = \sqrt{3}V_{LL}I_L \cos\theta$ 

Note: these equations are valid for balanced loads only.

Line quantities:  $\Delta$ -connection.

Power consumed by a load:  $P = 3V_{\phi}I_{\phi}\cos\theta$ 

Since for this load  $I_L = \sqrt{3}I_\phi \ \ and \ \ V_{LL} = V_\phi$ 

Therefore:  $P = 3\frac{I_L}{\sqrt{3}}V_{LL}\cos\theta$ 

Finally:  $P = \sqrt{3}V_{LL}I_L \cos\theta$ 

Same as for a Y-connected load!

Note: these equations were derived for a balanced load.

# Problems