

High-Order Data Reconstruction In 1D Hydrodynamics

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Computational Astrophysics

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1D Hydro Code and the Test Problem

The 1 dimensional Hydro code

- MUSCL-Hancock scheme
- HLLC Riemann solver
- Test problem: Sod shock tube, acoustic wave
- Compare results with the analytical solution at end time $T=0.1$

Initial condition	
Left state	Right state
$\begin{bmatrix} \rho_L \\ v_L \\ P_L \end{bmatrix} = \begin{bmatrix} 1.0 \\ 0.0 \\ 1.0 \end{bmatrix}$	$\begin{bmatrix} \rho_R \\ v_R \\ P_R \end{bmatrix} = \begin{bmatrix} 0.125 \\ 0.0 \\ 0.1 \end{bmatrix}$

Data Reconstruction Method

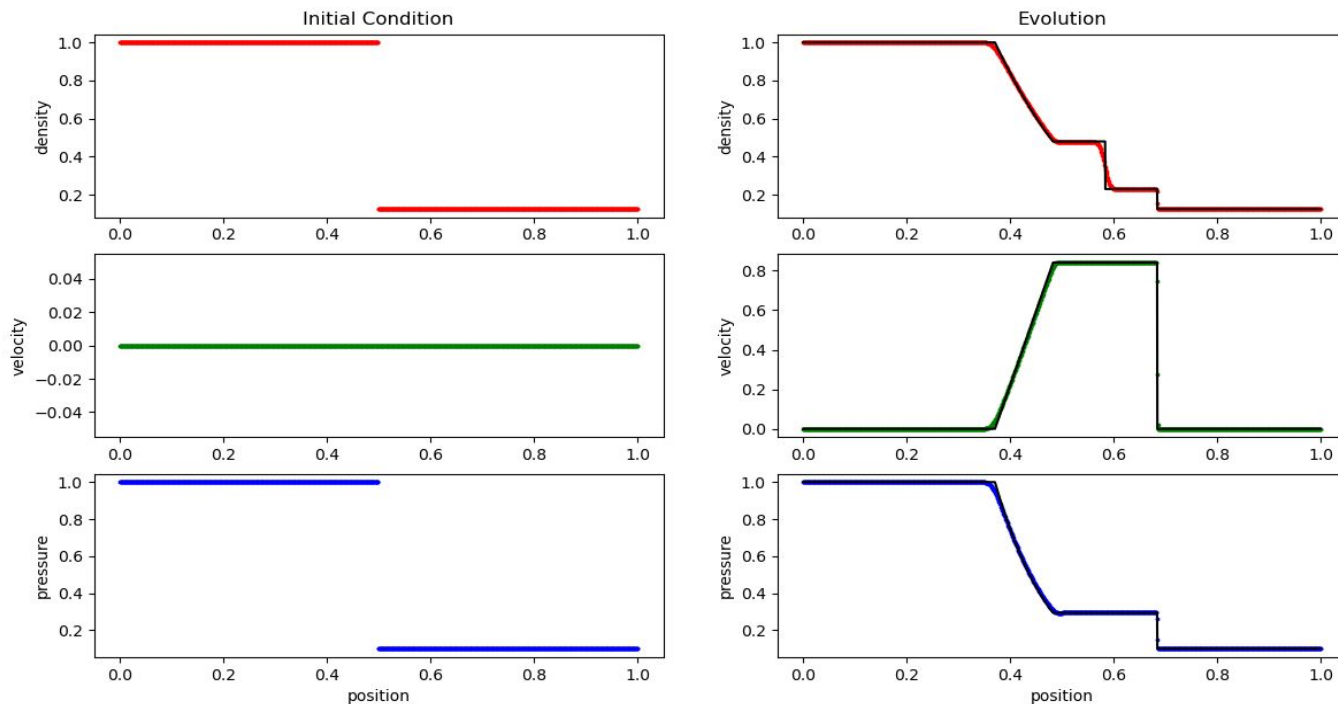
- Piecewise constant method (PCM): the original Godunov method
 - First order accurate
- Piecewise linear method (PLM):
 - with van Leer slope limiter to avoid new local extrema
 - should be second order accurate
- Piecewise parabolic method (PPM)
 - should be third order accurate
- Gaussian Process (GP)

Parallel computation

- Use OpenMP `# pragma omp parallel for`
- Parallelize the part for calculating Riemann flux, and other minor functions (e.g., computation of sound speed, limited slope, etc).
- For large N (e.g., 1000 or 2000), using 2 threads can cut the wall-clock time in half. However, using 4 threads isn't faster.
(Note: Depends on how many CPU cores are in the computer)

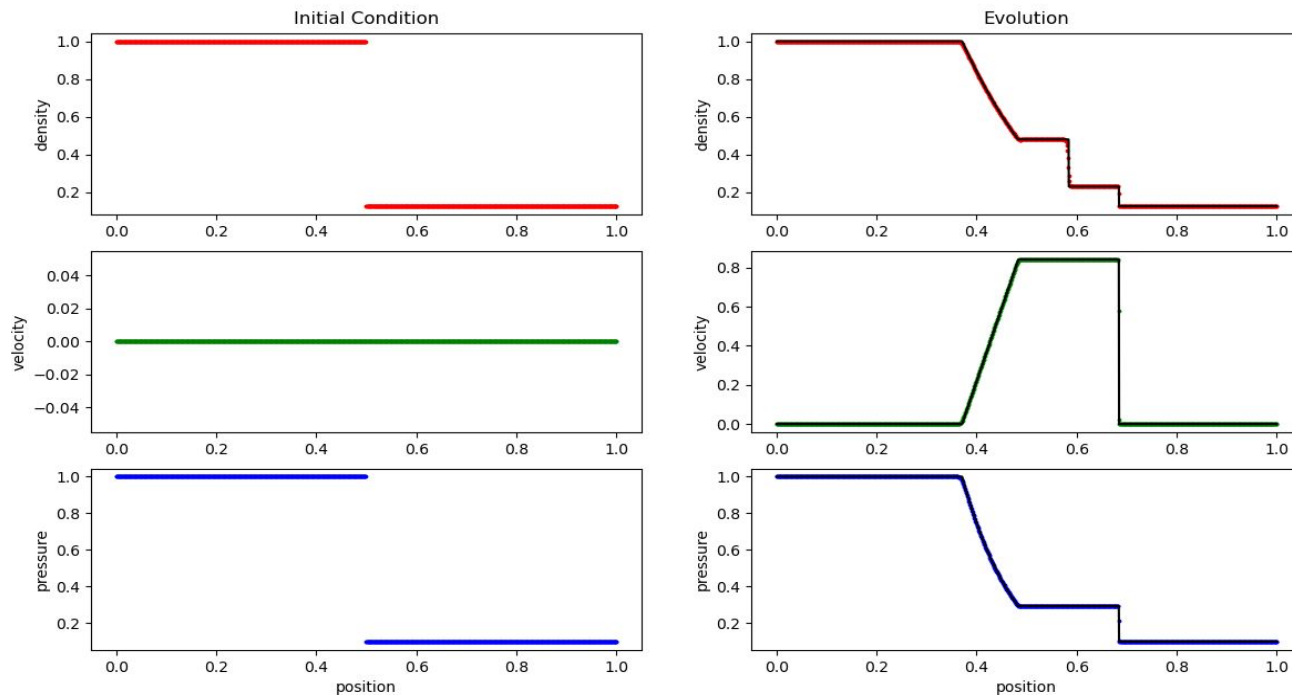
Piecewise constant method (PCM) result

Evolution of 1D Hydro tube



Piecewise linear method (PLM) result

Evolution of 1D Hydro tube



Piecewise Parabolic Method (PPM)

Implementation

- Convert conserved variables to primitive variables. Calculate the slope of each cell $\delta \mathbf{w}_i^m$ with van Leer limiter, as in the PLM method.
- Use parabolic interpolation to compute values at the left- and right-side of each cell cell:

$$\mathbf{w}_{L,i} = (\mathbf{w}_i + \mathbf{w}_{i-1})/2 - (\delta \mathbf{w}_i^m + \delta \mathbf{w}_{i-1}^m)/6$$

$$\mathbf{w}_{R,i} = (\mathbf{w}_{i+1} + \mathbf{w}_i)/2 - (\delta \mathbf{w}_{i+1}^m + \delta \mathbf{w}_i^m)/6$$

Implementation

- Monotonicity constraints: Ensure the values on the left- and right-side of cell center lie between neighboring cell-centered values.

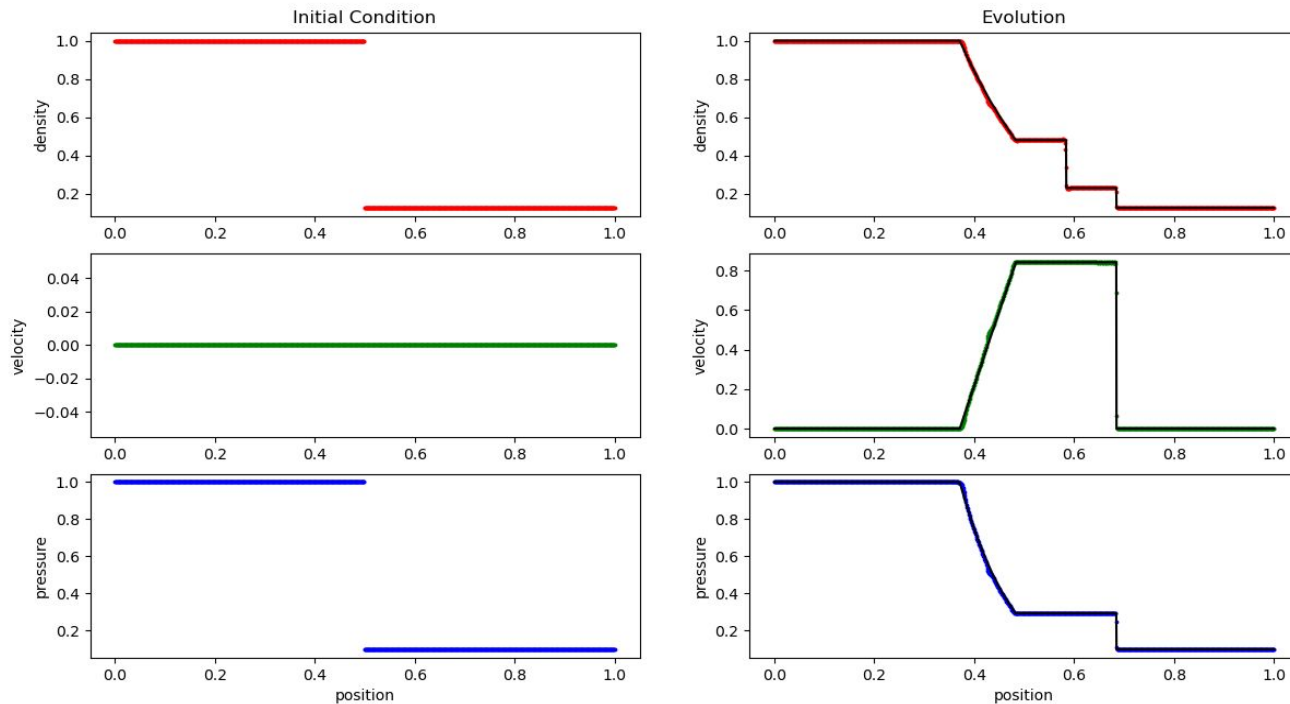
$$\text{if } (\mathbf{w}_{R,i} - \mathbf{w}_i)(\mathbf{w}_i - \mathbf{w}_{L,i}) \leq 0 : \mathbf{w}_{L,i} = \mathbf{w}_i, \mathbf{w}_{R,i} = \mathbf{w}_i$$

$$\text{if } 6(\mathbf{w}_{R,i} - \mathbf{w}_{L,i})(\mathbf{w}_i - (\mathbf{w}_{L,i} + \mathbf{w}_{R,i})/2) > (\mathbf{w}_{R,i} - \mathbf{w}_{L,i})^2 : \mathbf{w}_{L,i} = 3\mathbf{w}_i - 2\mathbf{w}_{R,i}$$

$$\text{if } 6(\mathbf{w}_{R,i} - \mathbf{w}_{L,i})(\mathbf{w}_i - (\mathbf{w}_{L,i} + \mathbf{w}_{R,i})/2) < -(\mathbf{w}_{R,i} - \mathbf{w}_{L,i})^2 : \mathbf{w}_{R,i} = 3\mathbf{w}_i - 2\mathbf{w}_{L,i}$$

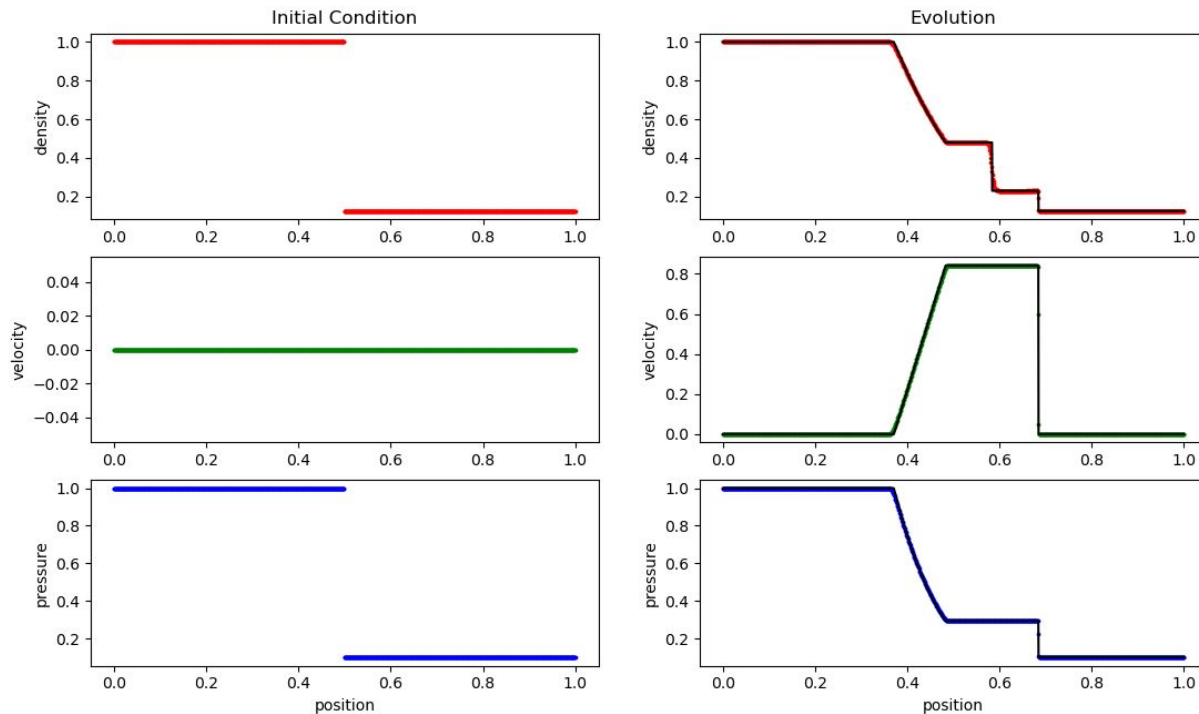
Piecewise parabolic method (PPM) result

Evolution of 1D Hydro tube



NEW: Piecewise parabolic method (PPM) result

Evolution of 1D Hydro tube



Fix the bug
that cause
errors at the
rarefaction
wave.

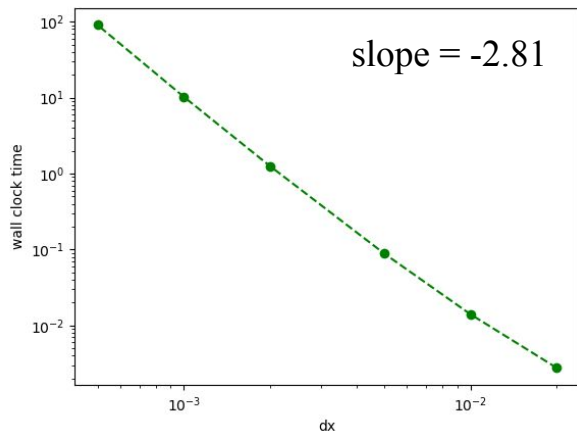
Performance: wall-clock time

threads	PCM	PLM	PPM
1	119.303281	115.460185	115.977558
2	66.330743	64.517736	64.743422
4	57.220275	56.637502	56.538886

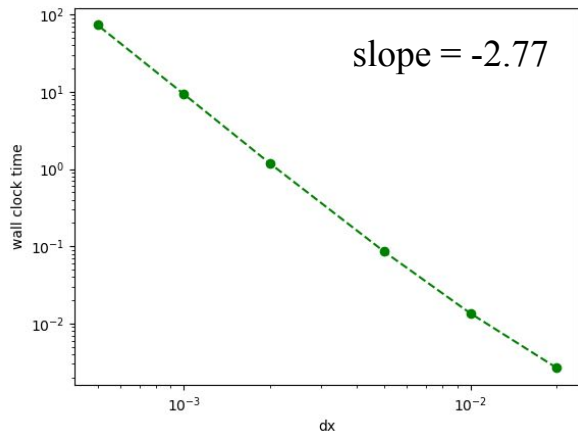
Unit: second

with the number of cells $N = 2000$

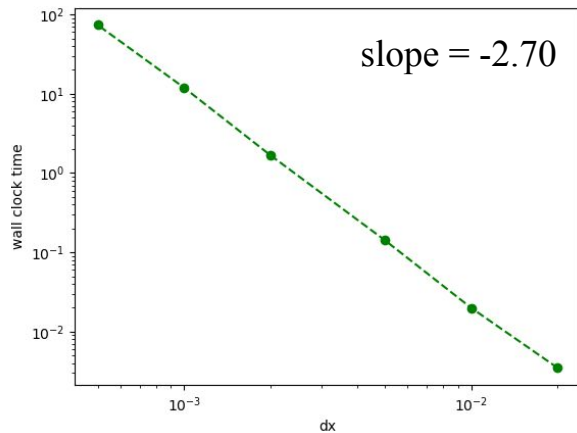
Performance



PCM

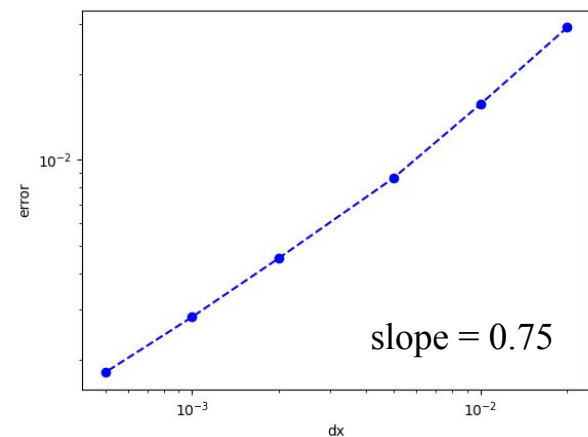


PLM

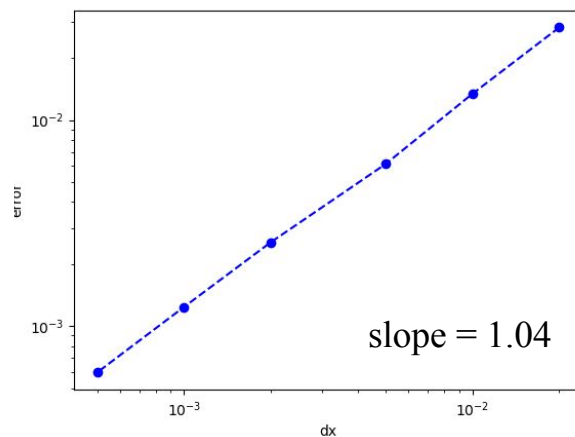


PPM

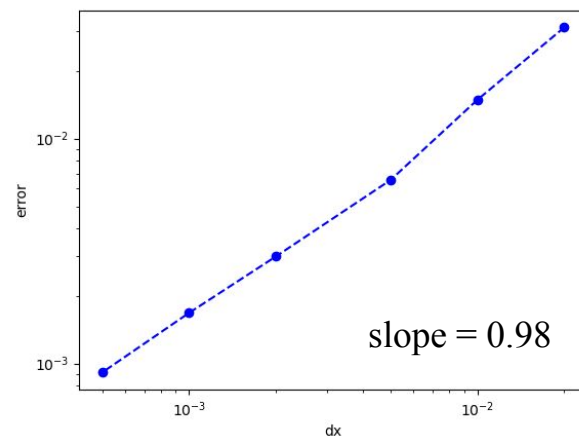
Accuracy (shock tube problem)



PCM



PLM



PPM

Current Problem

- PLM and PPM show only first order accuracy.
- According to Stone et al. (2018), it's probably because of our HLLC Riemann solver. An additional correction term is required to fix it to second order accurate.
- Will it be better with characteristic tracing step?

Characteristic tracing

- Implement the entire section 4.2.3 in Stone et al. (2018).
- Calculate the data on the left and right side of the “interface”, i.e. $\mathbf{W}_{L,i+1/2}$ and $\mathbf{W}_{R,i-1/2}$, instead of $\mathbf{W}_{L,i}$ and $\mathbf{W}_{R,i}$.
- Construct the eigenvalues and eigenvectors of the linearized equations in the primitive variables, use them to obtain the face-centered data.

Characteristic tracing

- Compute the left- and right-interface values using monotonized parabolic interpolation (similar to Colella & Woodward 1984).

$$\hat{\mathbf{w}}_{L,i+1/2} = \mathbf{w}_{R,i} - \lambda^{\max} \frac{\delta t}{2\delta x} \left[\delta \mathbf{w}_i^m - \left(1 - \lambda^{\max} \frac{2\delta t}{3\delta x} \right) \mathbf{w}_{6,i} \right]$$

$$\hat{\mathbf{w}}_{R,i-1/2} = \mathbf{w}_{L,i} + \lambda^{\min} \frac{\delta t}{2\delta x} \left[\delta \mathbf{w}_i^m + \left(1 - \lambda^{\min} \frac{2\delta t}{3\delta x} \right) \mathbf{w}_{6,i} \right]$$

$$\lambda = (v_x - a, v_x, v_x, v_x, v_x + a) \quad \delta \mathbf{w}_i^m = \mathbf{w}_{R,i} - \mathbf{w}_{L,i}, \quad \mathbf{w}_{6,i} = 6(\mathbf{w}_i - (\mathbf{w}_{L,i} + \mathbf{w}_{R,i})/2)$$

Characteristic tracing

- Subtract the part of each wave family (characteristics) that does not reach the interface in $dt/2$.

$$\mathbf{w}_{L,i+1/2} = \hat{\mathbf{w}}_{L,i+1/2} + \sum_{\lambda^\alpha > 0} [\mathbf{L}^\alpha (A(\delta \mathbf{w}_i^m - \mathbf{w}_{6,i}) + B \mathbf{w}_{6,i})] \mathbf{R}^\alpha$$

$$\mathbf{w}_{R,i+1/2} = \hat{\mathbf{w}}_{R,i+1/2} + \sum_{\lambda^\alpha < 0} [\mathbf{L}^\alpha (C(\delta \mathbf{w}_i^m + \mathbf{w}_{6,i}) + D \mathbf{w}_{6,i})] \mathbf{R}^\alpha$$

$$\mathbf{R} = \begin{bmatrix} 1 & 1 & 0 & 0 & 1 \\ -a/\rho & 0 & 0 & 0 & a/\rho \\ 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 \\ a^2 & 0 & 0 & 0 & a^2 \end{bmatrix}$$

where in the above

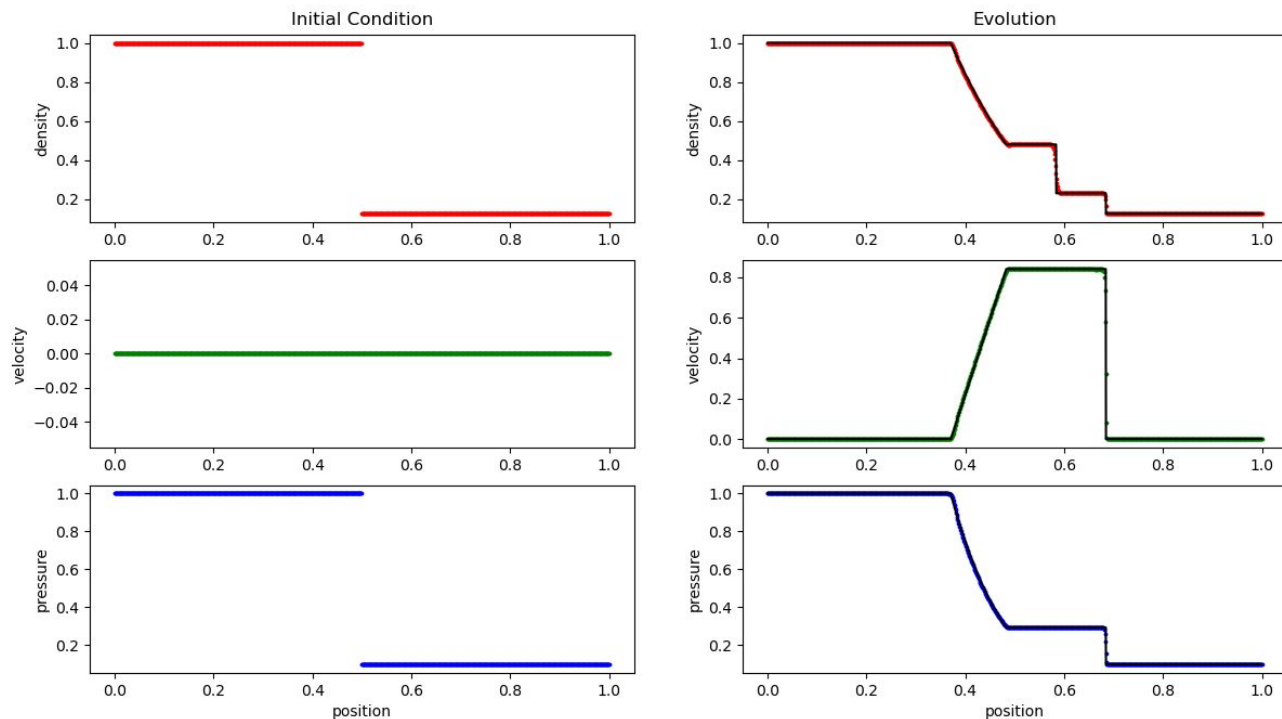
$$A = \frac{\delta t}{2\delta x}(\lambda^M - \lambda^\alpha) \quad B = \frac{1}{3} \left[\frac{\delta t}{\delta x} \right]^2 (\lambda^M \lambda^M - \lambda^\alpha \lambda^\alpha)$$

$$C = \frac{\delta t}{2\delta x}(\lambda^0 - \lambda^\alpha) \quad D = \frac{1}{3} \left[\frac{\delta t}{\delta x} \right]^2 (\lambda^0 \lambda^0 - \lambda^\alpha \lambda^\alpha)$$

$$\mathbf{L} = \begin{bmatrix} 0 & -\rho/(2a) & 0 & 0 & 1/(2a^2) \\ 1 & 0 & 0 & 0 & -1/a^2 \\ 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 \\ 0 & \rho/(2a) & 0 & 0 & 1/(2a^2) \end{bmatrix}_{19}$$

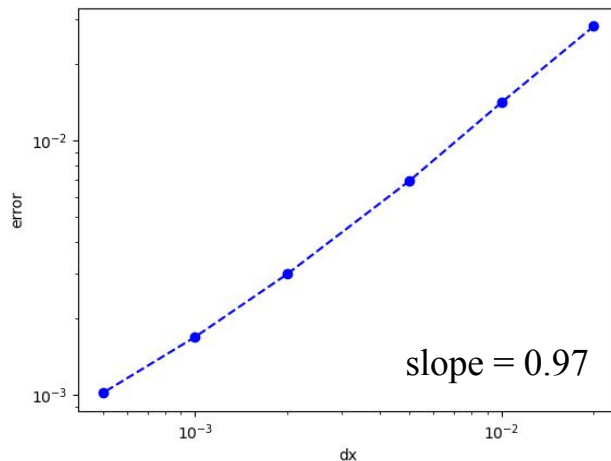
With characteristic tracing

Evolution of 1D Hydro tube



Characteristic tracing

- Still first order accurate. The result is not better than the original PPM.
- Maybe adding the correction term for HLLC Riemann solver will be better?



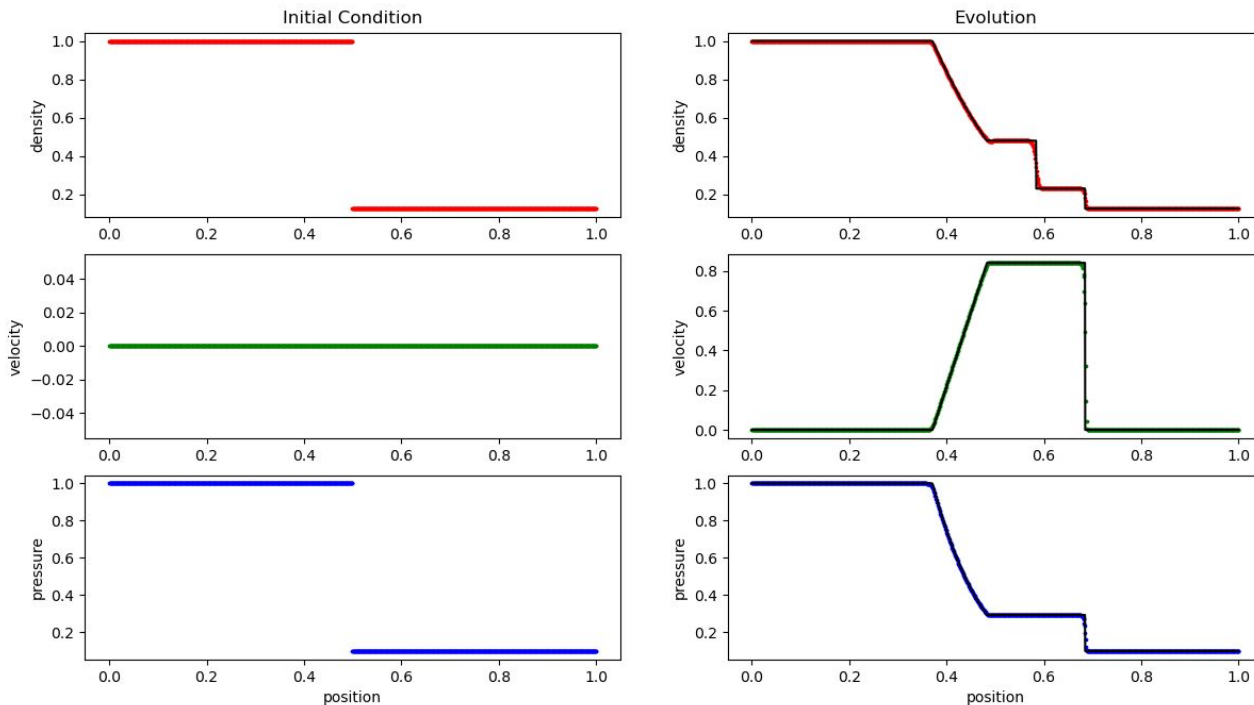
Correction term for HLL family solver

- For approximate Riemann solvers (like HLLC) that average over intermediate states.
- Include a correction for waves which propagate away from the interface in order to make the algorithm higher than first-order.

$$\Delta \mathbf{w}_{L,i+1/2} = -\frac{\delta t}{2\delta x} \sum_{\lambda^\alpha < 0} ((\lambda_i^\alpha - \lambda_i^M) \mathbf{L}^\alpha \cdot \delta \mathbf{w}_i^m) \mathbf{R}^\alpha$$
$$\Delta \mathbf{w}_{R,i-1/2} = -\frac{\delta t}{2\delta x} \sum_{\lambda^\alpha > 0} ((\lambda_i^\alpha - \lambda_i^0) \mathbf{L}^\alpha \cdot \delta \mathbf{w}_i^m) \mathbf{R}^\alpha$$

With characteristic tracing + correction

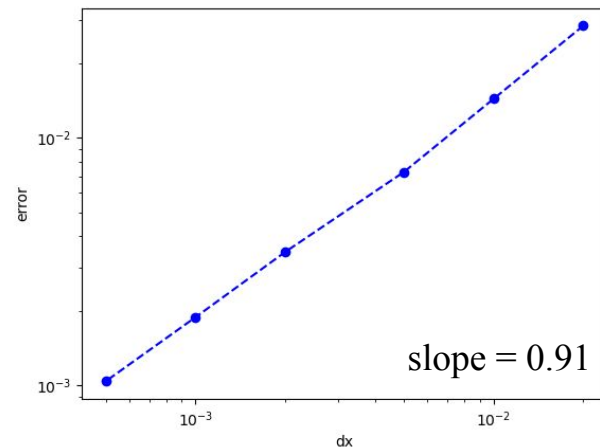
Evolution of 1D Hydro tube



worse???

Characteristic tracing + correction

- The correction term doesn't fix the code to second order accurate.
- Possible reason: bug...?

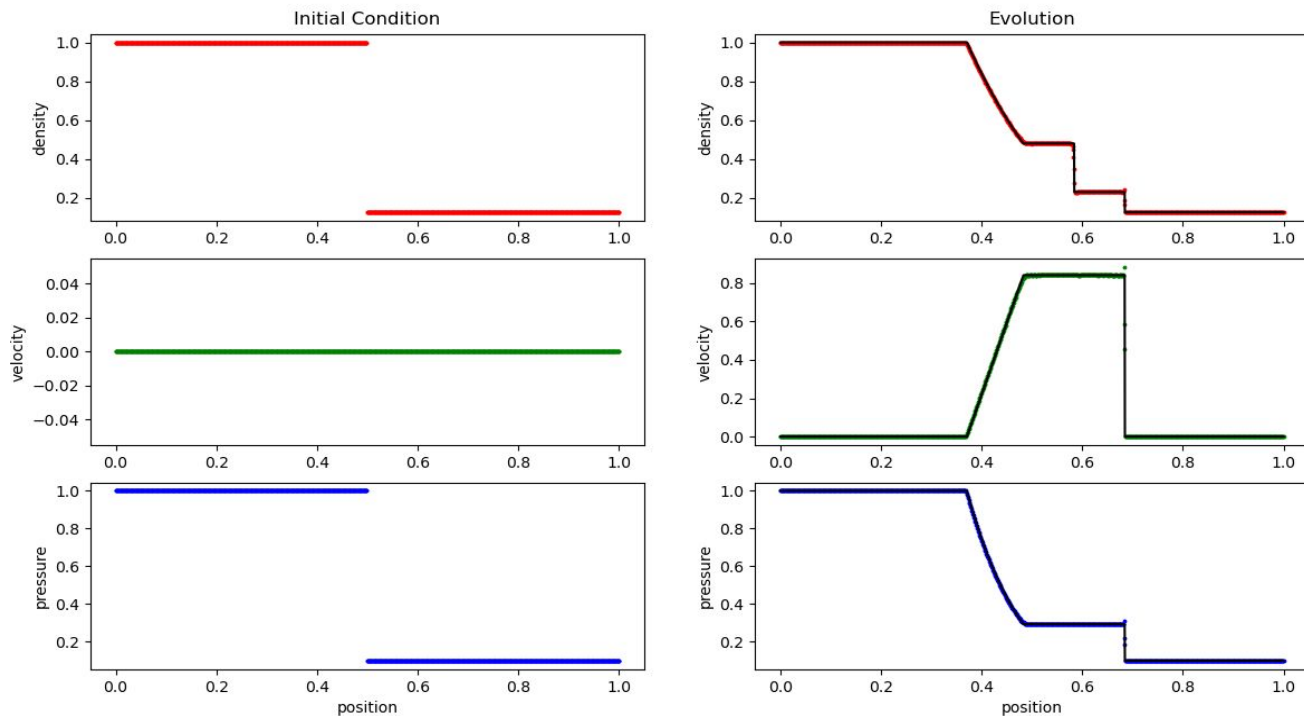


Another PPM implementation

- From section 1 + 3 in the paper of Colella & Woodward (1984).
- Calculate the data on the left and right side of the “interface”, i.e. $\mathbf{W}_{L,i+1/2}$ and $\mathbf{W}_{R,i-1/2}$, instead of $\mathbf{W}_{L,i}$ and $\mathbf{W}_{R,i}$.
- Construct the eigenvalues and eigenvectors of the linearized equations in the primitive variables, use them to obtain the face-centered data.
- Should be second order accurate according to the paper.

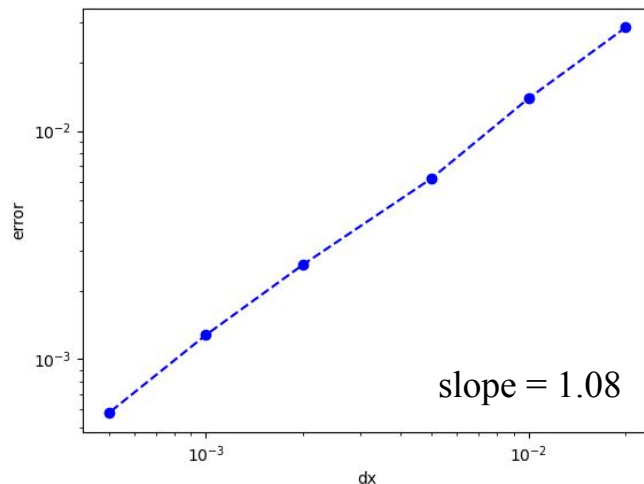
PPM of Colella & Woodward (1984) result

Evolution of 1D Hydro tube



PPM of Colella & Woodward (1984) result

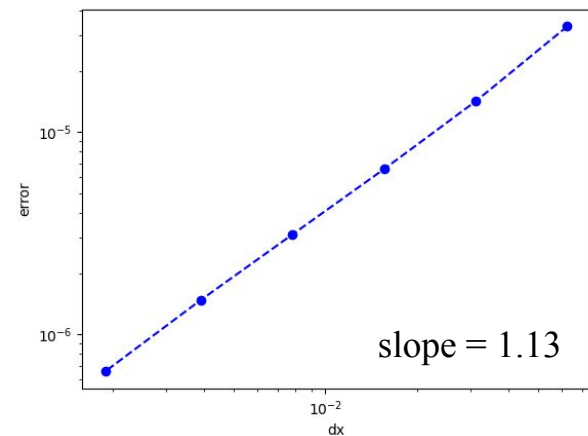
- Can't capture the shock very well. Need further modification.
- This method is first order accurate, too. The error is close to the original PPM method (slightly better).



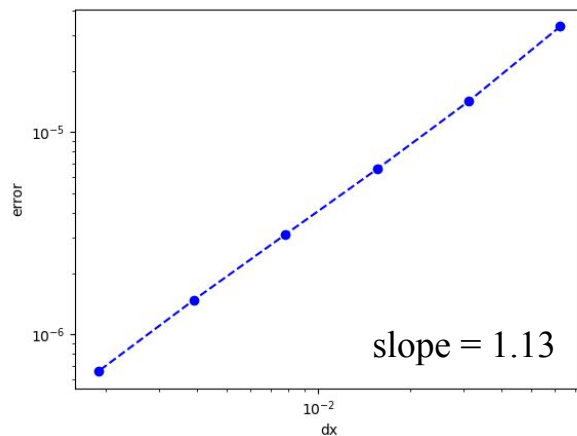
Density error comparison

N	PCM	PLM	PPM	PPM + tracing	PPM + correction	PPM CW
1000	2.815e-3	1.239e-3	1.677e-3	1.687e-3	1.883e-3	1.275e-3
2000	1.799e-3	5.959e-4	9.112e-4	1.015e-3	1.037e-3	5.802e-4

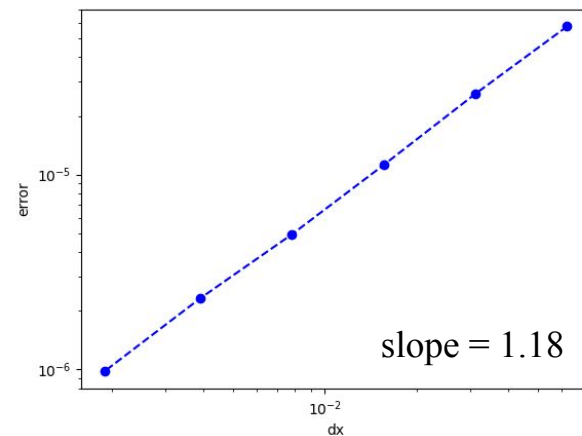
NEW: Accuracy test with acoustic wave problem



PLM



PPM (bug
fixed)



PPM with
characteristic
tracing

Gaussian Process (GP)

Gaussian Process

- Reference: Reyes, A., Lee, D., Graziani, C. et al. A New Class of High-Order Methods for Fluid Dynamics Simulations Using Gaussian Process Modeling: One-Dimensional Case. J Sci Comput 76, 443–480 (2018).
- Use the predictive GP to produce a “data-informed” prediction.

Gaussian Process

Updated posterior mean function:

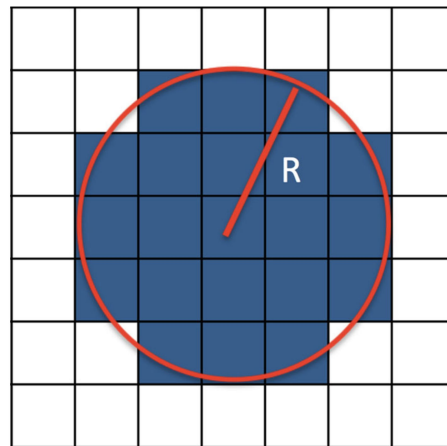
$$\tilde{f}_* \equiv \bar{f}(\mathbf{x}_*) + \mathbf{k}_*^T \mathbf{K}^{-1} \cdot (\mathbf{f} - \bar{\mathbf{f}})$$

$$k_{*,i} = K(\mathbf{x}_*, x_i)$$

$$K(\mathbf{x}, \mathbf{y}) \equiv \Sigma^2 \exp \left[-\frac{(\mathbf{x} - \mathbf{y})^2}{2\ell^2} \right]$$

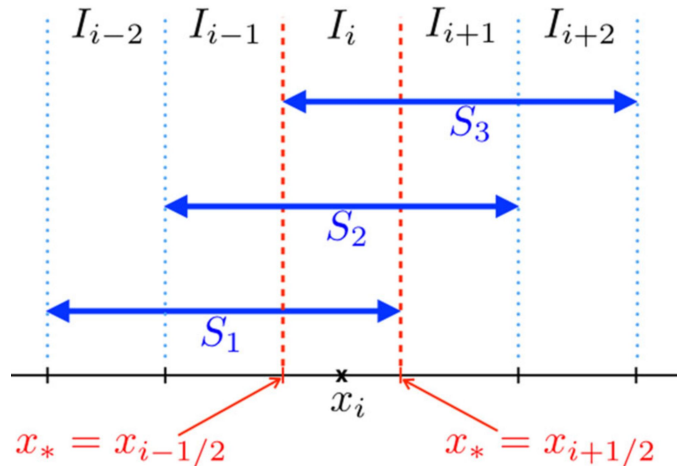
Gaussian Process

- R : stencil radii for Gaussian process
- l : hyperparameter for SE kernel
- Advantage:
 - Directional unbiased reconstruction
 - Solution accuracy can be tuned by kernel hyperparameters



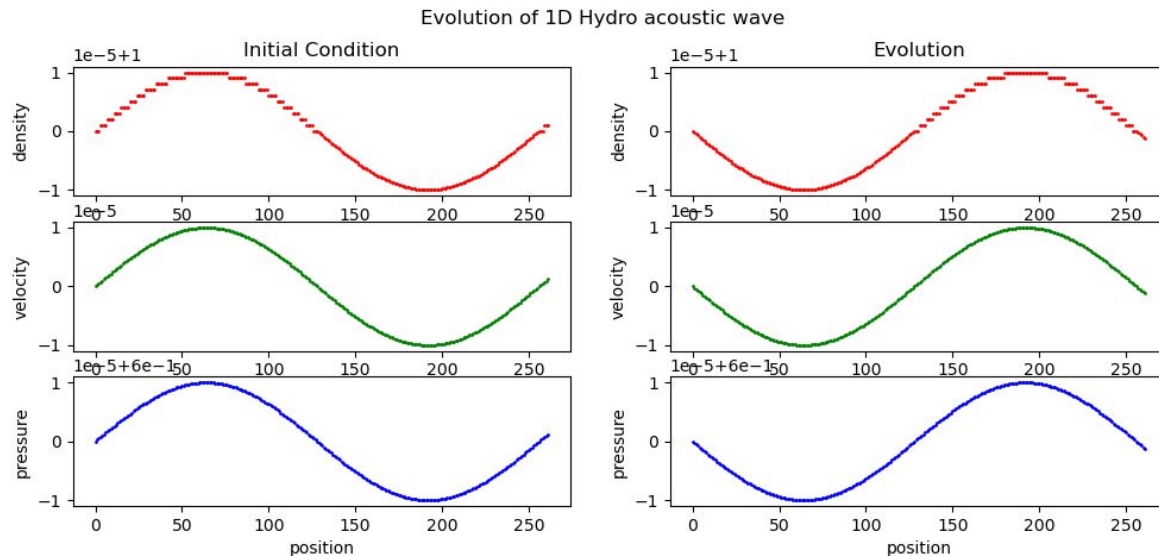
Gaussian Process

- Only applied to smooth wave
- GP-WENO — smooth indicator



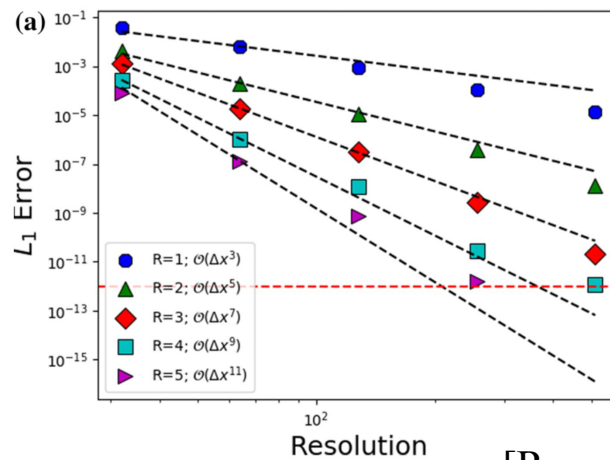
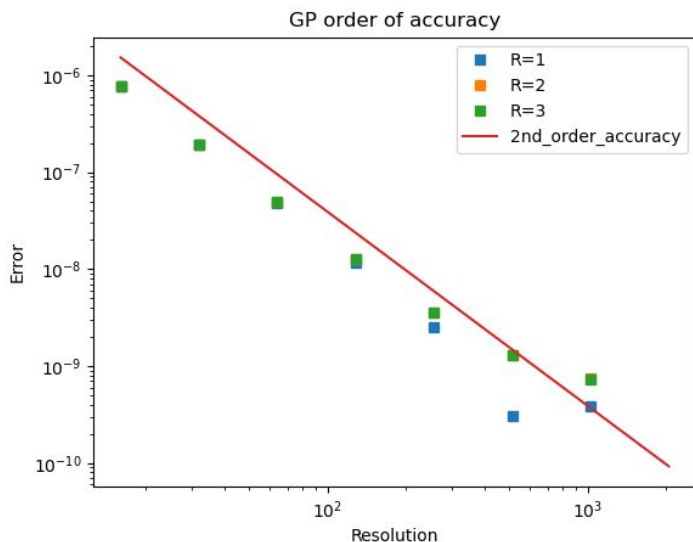
Gaussian Process

- acoustic wave test



Gaussian Process

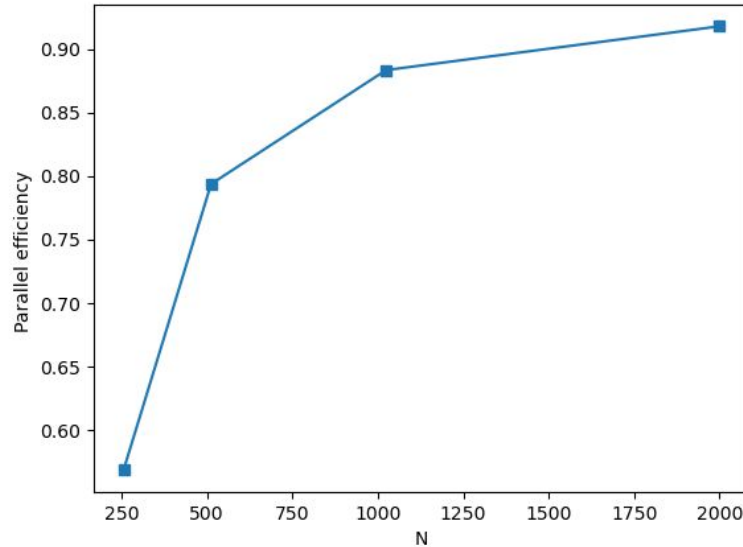
- acoustic wave test



[Reyes 2018]

OpenMP

- Parallel efficiency



Reference

- Colella, P., & Woodward, P.R., 1984. J. Comp. Phys., 54, 174,
<https://www.sciencedirect.com/science/article/pii/0021999184901438>
- Colella, P., & Sekora, M., 2007. J. Comp. Phys,
<https://www.sciencedirect.com/science/article/pii/S0021999108001435>
- Stone et al., ApJS, 178, 137 (2008), <https://arxiv.org/abs/0804.0402>
- Reyes, A., Lee, D., Graziani, C. et al. J Sci Comput 76, 443–480 (2018).
<https://doi.org/10.1007/s10915-017-0625-2>