

Introduction to Robotics

[ME_639]

Mini-Project

[Task_0]

Submitted by:

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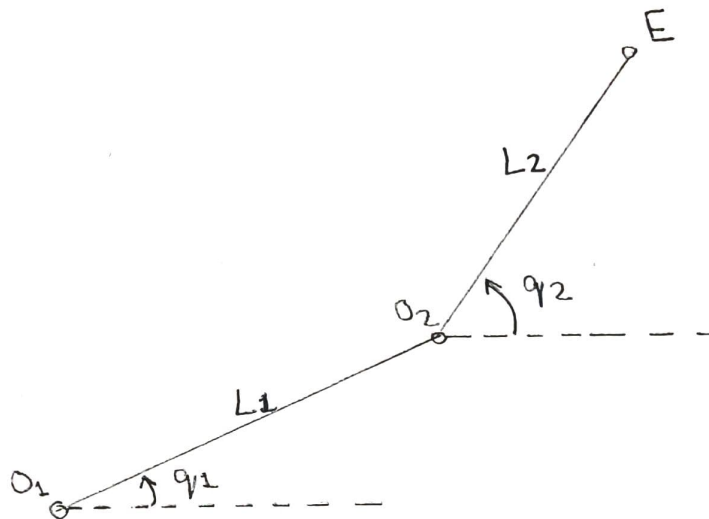
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M.Tech (Mechanical)

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⇒ Task-0

Consider the diagram of a 2R manipulator as shown in the figure below;

⇒ Equation-1 (Forward Kinematics)

Let O_1 be the origin of the 2-R manipulator (elbow manipulator)

For Link-1;

$d_1 \rightarrow$ length of the link-1

$m_1 \rightarrow$ mass of link-1

$I_1 \rightarrow$ Inertia of the link-1

For Link-2;

$d_2 \rightarrow$ length of the link-2

$m_2 \rightarrow$ mass of the link-2

$I_2 \rightarrow$ Inertia of the link-2

At O_2 ;

$$O_{2x} = d_1 \cos(q_1)$$

[1-a]

$$O_{2y} = d_1 \sin(q_1)$$

[1-b]

Similarly,

At End Effector (E);

$$E_x = O_2x + l_2 \cos(q_1 + q_2)$$

Using eq (1-a), we get;

$$\rightarrow E_x = l_1 \cos(q_1) + l_2 \cos[q_1 + q_2] \quad [1-c]$$

$$E_y = O_2y + l_2 \sin[q_1 + q_2]$$

Using eq(1-b), we get;

$$\rightarrow E_y = l_1 \sin(q_1) + l_2 \sin[q_1 + q_2] \quad [1-d]$$

Let's call the coordinates of the end effector as X & Y;

∴

$$\begin{aligned} E_x = X &= l_1 \cos(q_1) + l_2 \cos[q_1 + q_2] \\ E_y = Y &= l_1 \sin(q_1) + l_2 \sin[q_1 + q_2] \end{aligned} \rightarrow \text{Equation-1}$$

Equation-1 gives the forward kinematics of the end effector (E) of the 2-R manipulator.

⇒ Equation-2 [Velocity of End Effector]

Differentiating Equation-1; we get;

$$\dot{X} = -l_1 \sin q_1 \cdot \dot{q}_1 - l_2 \sin[q_1 + q_2] \cdot [\dot{q}_1 + \dot{q}_2]$$

$$\dot{Y} = l_1 \cos q_1 \cdot \dot{q}_1 + l_2 \cos[q_1 + q_2] \cdot [\dot{q}_1 + \dot{q}_2]$$

Therefore,

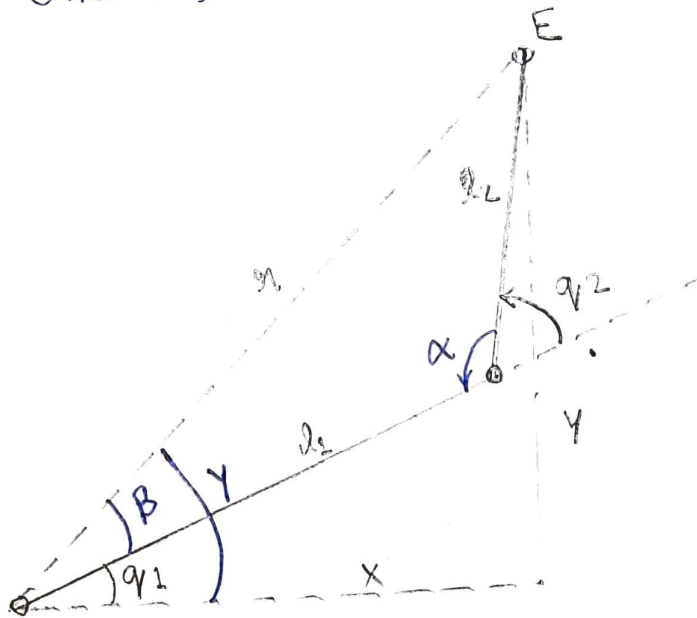
Equation of End-Effector Velocity can be written as;

$$\begin{bmatrix} \dot{x} \\ \dot{y} \end{bmatrix} = \begin{bmatrix} -l_1 \sin q_1 & -l_2 \sin(q_1 + q_2) \\ l_1 \cos q_1 & l_2 \cos(q_1 + q_2) \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \end{bmatrix}$$

→ Equation-2

⇒ Equation-3 [Inverse Kinematics]

The distance from the end effector to the robot base (shoulder joint) is d_1 and can be written in terms of x & y using Pythagoras theorem;



$$d_1^2 = x^2 + y^2 \quad [3-a]$$

Using Law of Cosines, we get;

$$d_1^2 = l_1^2 + l_2^2 - 2l_1 l_2 \cos(\alpha) \quad [3-b]$$

$$\therefore \alpha = \pi - q_2 \quad [3-c]$$

$$x^2 + y^2 = l_1^2 + l_2^2 - 2l_1l_2 \cos(\alpha)$$

$$x^2 + y^2 = l_1^2 + l_2^2 - 2l_1l_2 \cos[\pi - q_2] \quad [3-d]$$

$$2l_1l_2 \cos[\pi - q_2] = l_1^2 + l_2^2 - [x^2 + y^2]$$

$$\cos[\pi - q_2] = \frac{l_1^2 + l_2^2 - [x^2 + y^2]}{2l_1l_2} \quad [3-e]$$

$$\therefore \cos[\pi - q_2] = -\cos(q_2)$$

$$\therefore \cos q_2 = \frac{x^2 + y^2 - [l_1^2 + l_2^2]}{2l_1l_2}$$

$$\therefore q_2 = \cos^{-1} \left[\frac{x^2 + y^2 - [l_1^2 + l_2^2]}{2l_1l_2} \right] \quad [3-f]$$

$$\text{Also, } \beta = \tan^{-1} \left(\frac{l_2 \sin(q_2)}{l_1 + l_2 \cos(q_2)} \right) \quad [3-g]$$

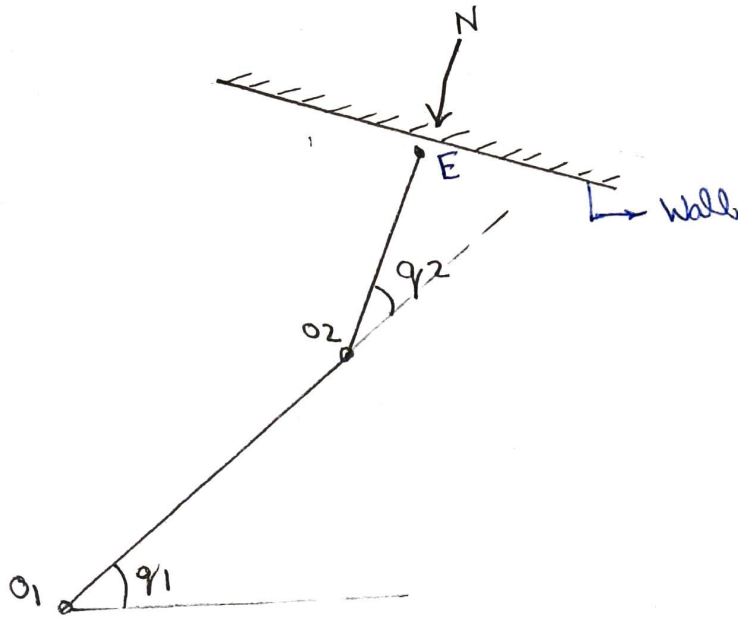
$$\gamma = q_1 + \beta \quad [3-h]$$

$$q_1 = \gamma - \beta$$

$$\therefore q_1 = \tan^{-1} \left(\frac{y}{x} \right) - \tan^{-1} \left[\frac{l_2 \sin(\theta_1)}{l_1 + l_2 \cos(\theta_1)} \right] \quad [3-i]$$

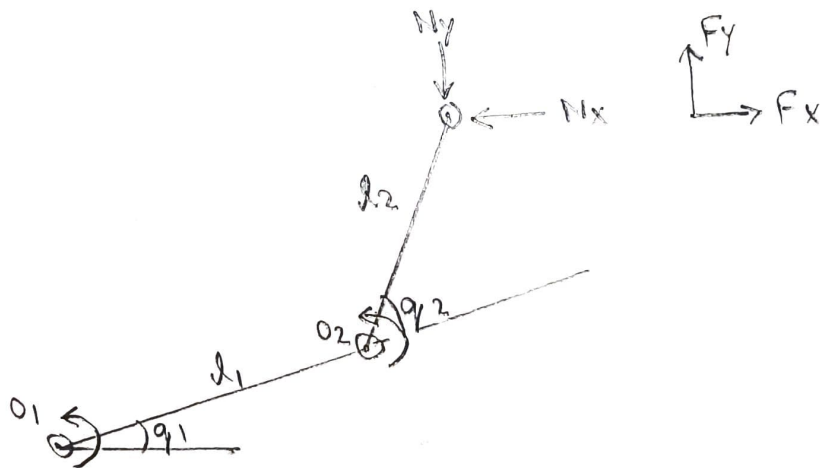
Equation (3-f) & (3-i) combined together constitute Equation-3 of Inverse Kinematics of the end effector of 2R Manipulator.

⇒ Equation-4 [Force Control]



Consider the free diagram of the 2-R manipulator as shown in the figure above;

FBD :-



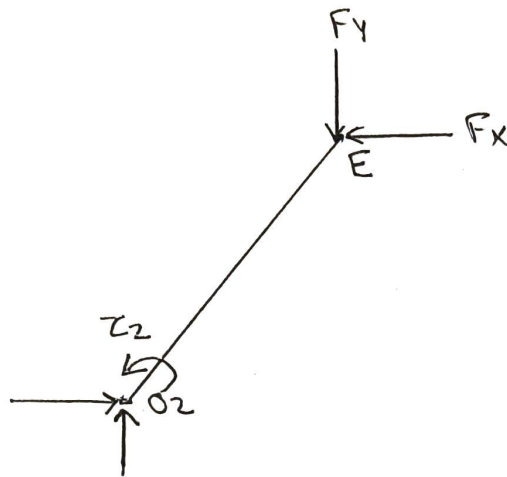
Considering static equilibrium;

$$\sum M_{O_1} = 0$$

$$\sum M_{O_2} = 0$$

Now, we will analyze each link separately;

FBD of Link-2;

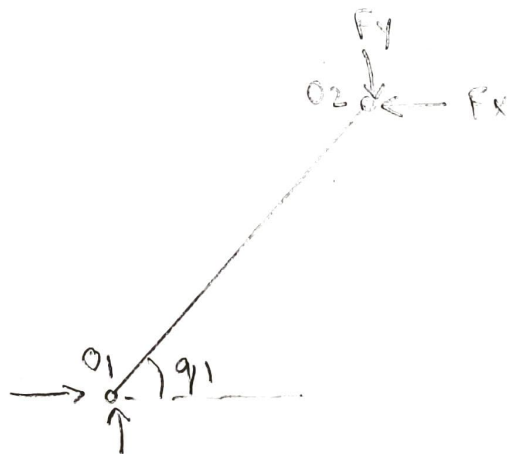


$$\sum M_{O2} = 0$$

$$F_y l_2 \cos \theta_2 - F_x l_2 \sin \theta_2 = \tau_2$$

[4-a]

FBD of Link-1;



$$\sum M_{O1} = 0$$

$$F_y l_1 \cos \theta_1 - F_x l_1 \sin \theta_2 = \tau_1$$

[4-b]

Combining eq-[4-a] and [4-b], we get Equation-4.

Equation - 5; [Lagrange's Equation]

Lagrange's equation is given by;

$$L = \text{Kinetic Energy } [K] - \text{Potential Energy } [V]$$

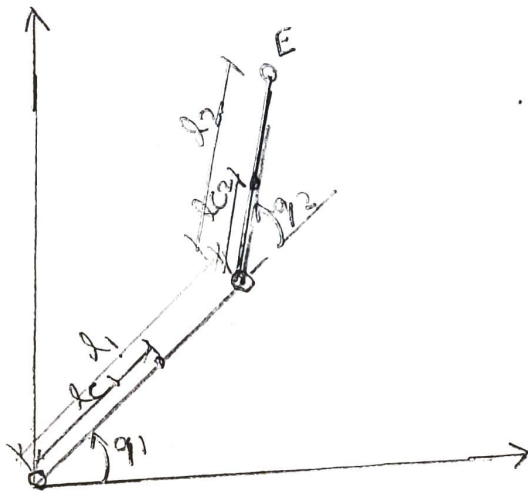
$$\therefore L = K - V$$

Also;
$$\frac{d}{dt} \left[\frac{\partial L}{\partial \dot{q}_i} \right] - \left[\frac{\partial L}{\partial q_i} \right] = Q_i'$$

Q_i' is generalized forces obtained using principle of Virtual work.

Equation - 6; [Dynamics Equation]

Consider a 2-R manipulator as shown in figure below;



Kinetic energy term;

$$K = \frac{1}{2} m_1 \dot{V}_{c1}^T \dot{V}_{c1} + \frac{1}{2} m_2 \dot{V}_{c2}^T \dot{V}_{c2} = \frac{1}{2} \dot{q} [m_1 J_{Vc1}^T J_{K1} + m_2 J_{Vc2}^T J_{Vc2}] \dot{q}$$

Angular velocity terms;

$$\omega_1 = \dot{q}_1, \quad \omega_2 = [\dot{q}_1 + \dot{q}_2] K$$

Rotational energy term;

$$\frac{1}{2} \dot{q}^T \left[I_1 \begin{bmatrix} 1 & 0 \\ 0 & 0 \end{bmatrix} + I_2 \begin{bmatrix} 1 & 1 \\ 1 & 1 \end{bmatrix} \right] \dot{q}$$

Now, Inertia Matrix;

$$D(q) = m_1 J_{Vc1}^T J_{Vc1} + m_2 J_{Vc2}^T J_{Vc2} + \begin{bmatrix} I_1 + I_2 I_2 \\ I_2 & I_2 \end{bmatrix}$$

Carrying out the multiplications of the above equations and using the standard trigonometric identities;

$$d_{11} = m_1 l_{c1}^2 + m_2 [l_1^2 + l_{c2}^2 + 2l_1 l_{c2} \cos q_2] + I_1 + I_2$$

$$d_{12} = d_{21} = m_2 [l_{c2}^2 + l_1 l_{c2} \cos q_2] + I_2$$

$$d_{22} = m_2 l_{c2}^2 + I_2$$

$$C_{111} = \frac{1}{2} \frac{\partial d_{11}}{\partial q_1} = 0$$

$$C_{121} = C_{211} = \frac{1}{2} \frac{\partial d_{11}}{\partial q_2} = -m_2 l_1 l_{c2} \sin q_2 = h$$

$$C_{221} = \frac{\partial d_{12}}{\partial q_2} = \frac{1}{2} \frac{\partial d_{22}}{\partial q_1} = h$$

$$C_{112} = \frac{\partial d_{21}}{\partial q_1} = \frac{1}{2} \frac{\partial d_{11}}{\partial q_2} = -h$$

$$C_{122} = C_{212} = \frac{1}{2} \frac{\partial d_{22}}{\partial q_1} = 0$$

$$C_{222} = \frac{1}{2} \frac{\partial d_{22}}{\partial q_2} = 0$$

For each link, potential energy is just its mass multiplied by the gravitational acceleration and the height of its centre of mass.

Then,

$$V_1 = m_1 g l_{c1} \sin q_1$$

$$V_2 = m_2 g [l_{c2} \sin q_1 + l_{c2} \sin [q_1 + q_2]]$$

$$\begin{aligned} V &= V_1 + V_2 \\ &= [m_1 l_{c1} + m_2 l_1] g \sin q_1 + m_2 l_{c2} g \sin [q_1 + q_2] \end{aligned}$$

Now,

$$\phi_1 = \frac{\partial V}{\partial q_1} = [m_1 l_{c1} + m_2 l_1] g \cos q_1 + m_2 l_{c2} g \cos [q_1 + q_2]$$

$$\phi_2 = \frac{\partial V}{\partial q_2} = m_2 l_{c2} g \cos [q_1 + q_2]$$

\therefore

$$\begin{aligned} d_{11} \ddot{q}_1 + d_{12} \ddot{q}_2 + c_{121} \dot{q}_1 \dot{q}_2 + c_{211} \dot{q}_2 \dot{q}_1 + c_{221} \dot{q}_2^2 + \phi_1 &= \tau_1 \\ d_{21} \ddot{q}_1 + d_{22} \ddot{q}_2 + c_{112} \dot{q}_1^2 + \phi_2 &= \tau_2 \end{aligned}$$

→ Equation-6