- Linear-phase FIR filters with narrow transition bands are of very high order, and as a result have a very long group delay that is about half the filter order
- By relaxing the linear-phase requirement, it is possible to design an FIR filter of lower order thus reducing the overall group delay and the computational cost

- A very simple method of minimum-phase
   FIR filter is described next
- Consider an arbitrary FIR transfer function of degree *N*:

$$H(z) = \sum_{n=0}^{N} h[n]z^{-n} = h[0] \prod_{k=1}^{N} (1 - \xi_k z^{-1})$$

• The mirror-image polynomial to H(z) is given by

$$\hat{H}(z) = z^{-N} H(z^{-1})$$

$$= \sum_{n=0}^{N} h[N-n] z^{-n} = h[N] \prod_{k=1}^{N} (1-z^{-1}/\xi_k)$$

• The zeros of  $\hat{H}(z)$  are thus at  $z = 1/\xi_k$ , i.e., are reciprocal to the zeros of H(z) at  $z = \xi_k$ 

• As a result,

$$G(z) = H(z)\hat{H}(z) = z^{-N}H(z)H(z^{-1})$$

has zeros exhibiting mirror-image symmetry in the *z*-plane and is thus a Type 1 linear-phase transfer function of order 2*N* 

• Moreover, if H(z) has a zero on the unit circle,  $\hat{H}(z)$  will also have a zero on the unit circle at the conjugate reciprocal position

- Thus, unit circle zeros of G(z) occur in pairs
- On the unit circle we have

$$\left| H(e^{j\omega}) \right|^2 = \breve{G}(\omega)$$

$$\breve{G}(\omega) \ge 0$$

• Moreover, the amplitude response  $\check{G}(\omega)$  has double zeros in the frequency range  $[0,\pi]$ 

- Design Procedure –
- Step 1: Design a Type 1 linear-phase transfer function F(z) of degree 2N satisfying the specifications:

$$1 - \delta_p^{(F)} \le \breve{F}(\omega) \le 1 + \delta_p^{(F)} \quad \text{for } \omega \in [0, \omega_p]$$
$$-\delta_s^{(F)} \le \breve{F}(\omega) \le \delta_p^{(F)} \quad \text{for } \omega \in [\omega_s, \pi]$$

• Note that F(z) has single unit circle zeros

• Step 2: Determine the linear-phase transfer function

$$G(z) = \delta_s^{(F)} z^{-N} + F(z)$$

Its amplitude response satisfies

$$1 + \delta_s^{(F)} - \delta_p^{(F)} \le \breve{G}(\omega) \le 1 + \delta_s^{(F)} + \delta_p^{(F)}$$

$$\text{for } \omega \in [0, \omega_p]$$

$$0 \le \breve{G}(\omega) \le 2\delta_s^{(F)}$$

$$\text{for } \omega \in [\omega_s, \pi]$$

- Note that G(z) has double zeros on the unit circle and all other zeros are situated with a mirror-image symmetry
- Hence, it can be expressed in the form

$$G(z) = z^{-N} H_m(z) H_m(z^{-1})$$

where  $H_m(z)$  is a minimum-phase transfer function containing all zeros of G(z) that are inside the unit circle and one each of the unit circle double zeros

- Step 3: Determine  $H_m(z)$  from G(z) by applying a spectral factorization
- The passband ripple  $\delta_p^{(F)}$  and the stopband ripple  $\delta_s^{(F)}$  of F(z) must be chosen to ensure that the specified passband ripple  $\delta_p$  and the stopband ripple  $\delta_s$  of  $H_m(z)$  are satisfied

It can be shown

$$\delta_p^{(F)} = \sqrt{1 + \frac{\delta_p}{1 + \delta_s}} - 1, \quad \delta_s^{(F)} = \sqrt{\frac{2\delta_s}{1 + \delta_s}}$$

- An estimate of the order N of  $H_m(z)$  can be found by first estimating the order of F(z) and then dividing it by 2
- If the estimated order of F(z) is an odd integer, it should be increased by 1

- Order Estimation -
- Kaiser's Formula:

$$N \cong \frac{-20\log_{10}(\sqrt{\delta_p \delta_s})}{14.6(\omega_s - \omega_p)/2\pi}$$

• Note: Filter order N is inversely proportional to transition band width  $(\omega_s - \omega_p)$  and does not depend on actual location of transition band

• Hermann-Rabiner-Chan's Formula:

$$N \cong \frac{D_{\infty}(\delta_p, \delta_s) - F(\delta_p, \delta_s) [(\omega_s - \omega_p)/2\pi]^2}{(\omega_s - \omega_p)/2\pi}$$

#### where

$$D_{\infty}(\delta_{p}, \delta_{s}) = [a_{1}(\log_{10}\delta_{p})^{2} + a_{2}(\log_{10}\delta_{p}) + a_{3}]\log_{10}\delta_{s} + [a_{4}(\log_{10}\delta_{p})^{2} + a_{5}(\log_{10}\delta_{p}) + a_{6}]$$

$$F(\delta_{p}, \delta_{s}) = b_{1} + b_{2}[\log_{10}\delta_{p} - \log_{10}\delta_{s}]$$
with  $a_{1} = 0.005309, a_{2} = 0.07114, a_{3} = -0.4761$ 

$$a_{4} = 0.00266, a_{5} = 0.5941, a_{6} = 0.4278$$

$$b_{1} = 11.01217, b_{2} = 0.51244$$

- Formula valid for  $\delta_p \ge \delta_s$
- For  $\delta_p < \delta_s$ , formula to be used is obtained by interchanging  $\delta_p$  and  $\delta_s$
- Both formulas provide only an estimate of the required filter order *N*
- Frequency response of FIR filter designed using this estimated order may or may not meet the given specifications
- If specifications are not met, increase filter order until they are met

• MATLAB code fragments for estimating filter order using Kaiser's formula

```
num = - 20*log10(sqrt(dp*ds)) - 13;
den = 14.6*(Fs - Fp)/FT;
N = ceil(num/den);
```

• M-file firpmord implements Hermann-Rabiner-Chan's order estimation formula

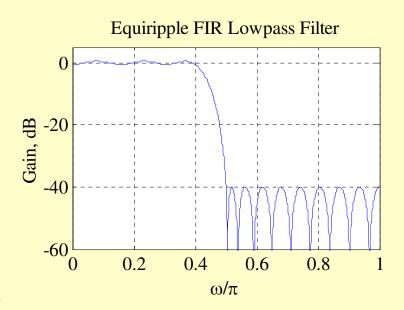
- For FIR filter design using the Kaiser window, window order is estimated using the M-file kaiserord
- The M-file kaiserord can in some cases generate a value of *N* which is either greater or smaller than the required minimum order
- If filter designed using the estimated order *N* does not meet the specifications, *N* should either be gradually increased or decreased until the specifications are met

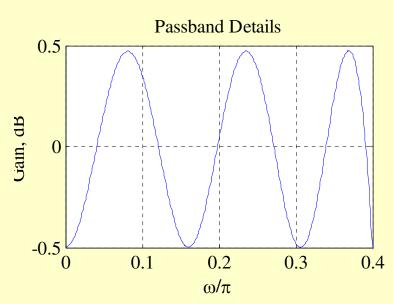
- The M-file firpm can be used to design an equiripple FIR filter using the Parks-McClellan algorithm
- Example Design an equiripple FIR filter with the specifications:  $F_p = 0.8$  kHz,  $F_s = 1$  kHz,  $F_T = 4$  kHz,  $\alpha_p = 0.5$ dB,  $\alpha_s = 40$  dB
- Here,  $\delta_p = 0.0559$  and  $\delta_s = 0.01$

MATLAB code fragments used are

```
[N, fpts, mag, wt] =
firpmord(fedge, mval, dev, FT);
b = firpm(N, fpts, mag, wt);
where fedge = [800     1000],
mval = [1 0], dev = [0.0559     0.01],
and FT = 4000
```

- The computed gain response with the filter order obtained (N = 28) does not meet the specifications ( $\alpha_p = 0.6 \, \mathrm{dB}, \alpha_s = 38.7 \, \mathrm{dB}$ )
- Specifications are met with N = 30





- Example Design a linear-phase FIR bandpass filter of order 26 with a passband from 0.3 to 0.5, and stopbands from 0 to 0.25 and from 0.55 to 1
- The pertinent input data here are

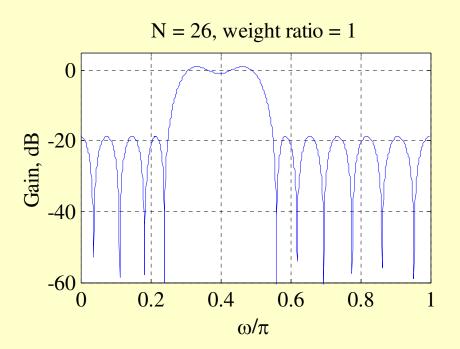
```
N = 26

fpts = [0 0.25 0.3 0.5 0.55 1]

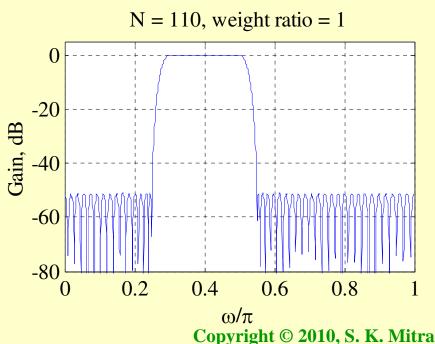
mag = [0 0 1 1 0 0]

wt = [1 1 1]
```

• Computed gain response shown below where  $\alpha_p = 1$  dB,  $\alpha_s = 18.7$  dB



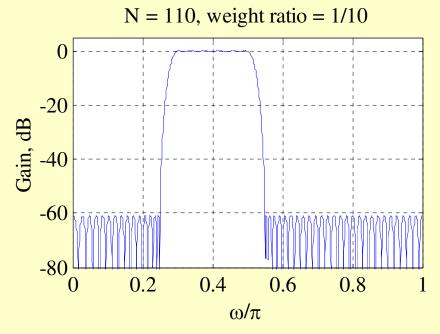
- We redesign the filter with order increased to 110
- Computed gain response shown below where  $\alpha_p = 0.024 \text{ dB}$ ,  $\alpha_s = 51.2 \text{ dB}$
- Note: Increase in order improves gain response at the expense of increased computational complexity



•  $\alpha_s$  can be increased at the expenses of a larger  $\alpha_p$  by decreasing the relative weight

ratio  $W(\omega) = \delta_p / \delta_s$ 

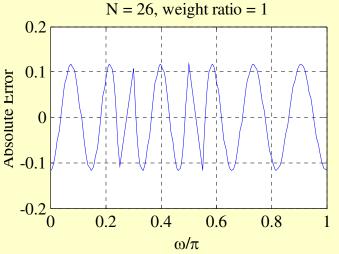
Gain response of bandpass filter of order 110 obtained with a weight vector [1 0.1 1]



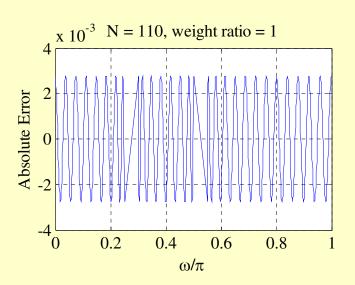
• Now  $\alpha_p = 0.076 \, dB$ ,  $\alpha_s = 60.86 \, dB$ 

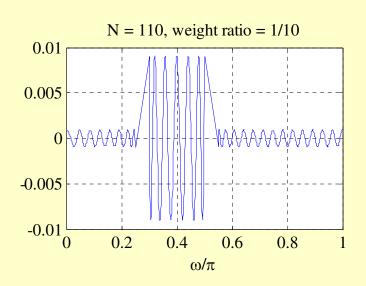
- Plots of absolute error for 1st design
- Absolute error has same peak value in all bands
- As L=13, and there on the at most are 4 band edges, there can be at most
- Error plot exhibits 17 extrema

L-1+6=18 extrema



- Absolute error has same peak value in all bands for the 2nd design
- Absolute error in passband of 3rd design is 10 times the error in the stopbands





- Example Design a linear-phase FIR bandpass filter of order 60 with a passband from 0.3 to 0.5, and stopbands from 0 to 0.25 and from 0.6 to 1 with unequal weights
- The pertinent input data here are

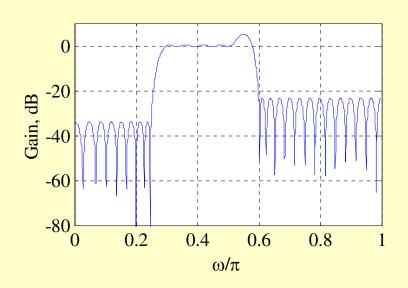
```
N = 60

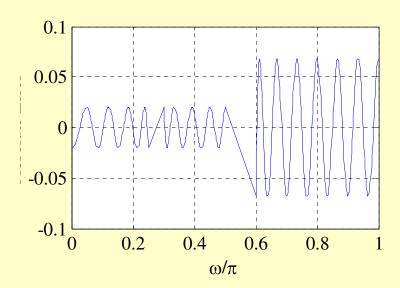
fpts = [0 0.25 0.3 0.5 0.6 1]

mag = [0 0 1 1 0 0]

wt = [1 1 0.3]
```

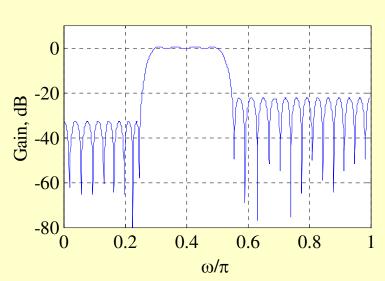
 Plots of gain response and absolute error shown below





- Response in the second transition band shows a peak with a value higher than that in passband
- Result does not contradict alternation theorem
- As N = 60, M = 30, and hence, there must be at least M + 2 = 32 extremal frequencies
- Plot of absolute error shows the presence of 32 extremal frequencies

- If gain response of filter designed exhibits a nonmonotonic behavior, it is recommended that either the filter order or the bandedges or the weighting function be adjusted until a satisfactory gain response has been obtained
- Gain plot obtained by moving the second stopband edge to 0.55



 A lowpass differentiator has a bandlimited frequency response

$$H_{DIF}(e^{j\omega}) = \begin{cases} j\omega, & 0 \le |\omega| \le \omega_p \\ 0, & \omega_s \le |\omega| \le \pi \end{cases}$$

where  $0 \le |\omega| \le \omega_p$  represents the passband and  $\omega_s \le |\omega| \le \pi$  represents the stopband

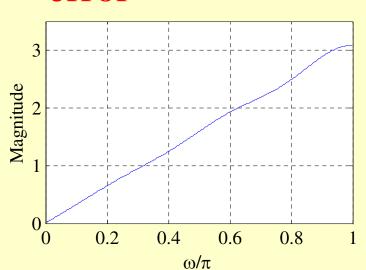
• For the design phase we choose

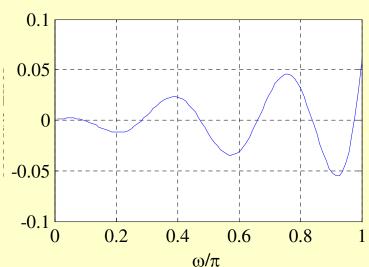
$$W(\omega) = 1/\omega$$
,  $D(\omega) = 1$ ,  $0 \le |\omega| \le \omega_p$ 

- The M-file firpmord cannot be used to estimate the order of an FIR differentiator
- Example Design a full-band  $(\omega_p = \pi)$  differentiator of order 11
- Code fragment to use

```
b =
firpm(N,fpts,mag, 'differentiator');
where N = 11
    fpts = [0    1]
    mag = [0    pi]
```

Plots of magnitude response and absolute error





• Absolute error increases with  $\omega$  as the algorithm results in an equiripple error of the function  $\left[\frac{A(\omega)}{\omega}-1\right]$ 

- Example Design a lowpass differentiator of order 50 with  $\omega_p = 0.4\pi$  and  $\omega_s = 0.45\pi$
- Code fragment to use

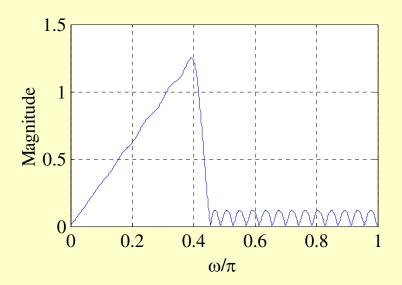
```
b =
firpm(N, fpts, mag'differentiator');
where
```

```
N = 50

fpts = [0   0.4   0.45   1]

mag = [0   0.4*pi   0   0]
```

 Plot of the magnitude response of the lowpass differentiator



## Equiripple FIR Hilbert Transformer Design Using MATLAB

• Desired amplitude response of a bandpass Hilbert transformer is

$$D(\omega) = 1, \quad \omega_L \le |\omega| \le \omega_H$$

with weighting function

$$W(\omega) = 1, \quad \omega_L \le |\omega| \le \omega_H$$

• Impulse response of an ideal Hilbert transformer satisfies the condition

$$h_{HT}[n] = 0$$
, for  $n$  even

which can be met by a Type 3 FIR filter

## Equiripple FIR Hilbert Transformer Design Using MATLAB

• Example - Design a linear-phase bandpass FIR Hilbert transformer of order 20 with  $\omega_L = 0.1\pi$ ,  $\omega_H = 0.9\pi$ 

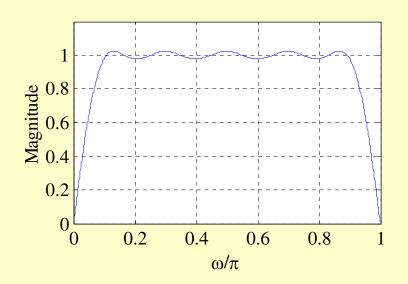
Code fragment to use

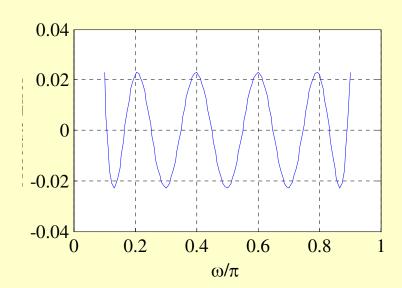
```
b = firpm(N, fpts, mag, 'Hilbert');
where
```

```
N = 20
fpts = [0.1 0.9]
mag = [1 1]
```

## Equiripple FIR Hilbert Transformer Design Using MATLAB

Plots of magnitude response and absolute error





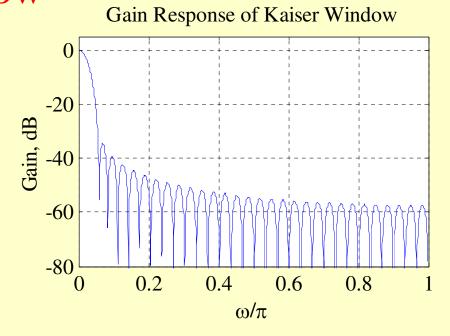
Window Generation - Code fragments to use

```
w = blackman(L);
w = hamming(L);
w = hanning(L);
w = chebwin(L, Rs);
w = kaiser(L, beta);
where window length L is odd
```

- Example Kaiser window design for use in a lowpass FIR filter design
- Specifications of lowpass filter:  $\omega_p = 0.3\pi$ ,  $\omega_s = 0.4\pi$ ,  $\alpha_s = 50$  dB  $\Rightarrow \delta_s = 0.003162$
- Code fragments to use

```
[N, Wn, beta, ftype] = kaiserord(fpts, mag,dev);
w = kaiser(N+1, beta);
where fpts = [0.3 0.4]
mag = [1 0]
dev = [0.003162 0.003162]
```

Plot of the gain response of the Kaiser window



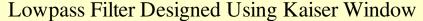
- M-files available are fir1 and fir2
- fir1 is used to design conventional lowpass, highpass, bandpass, bandstop and multiband FIR filters
- fir2 is used to design FIR filters with arbitrarily shaped magnitude response
- In fir1, Hamming window is used as a default if no window is specified

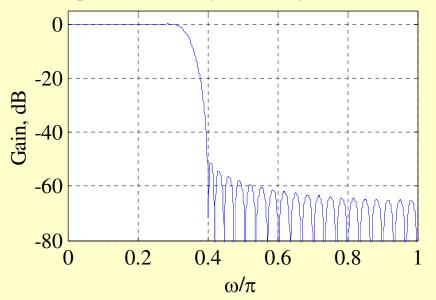
• Example - Design using a Kaiser window a lowpass FIR filter with the specifications:  $\omega_p = 0.3\pi$ ,  $\omega_s = 0.4\pi$ ,  $\delta_s = 0.003162$ 

Code fragments to use

```
[N, Wn, beta, ftype] = kaiserord(fpts, mag, dev);
b = fir1(N, Wn, kaiser(N+1, beta));
where fpts = [0.3 0.4]
mag = [1 0]
dev = [0.003162 0.003162]
```

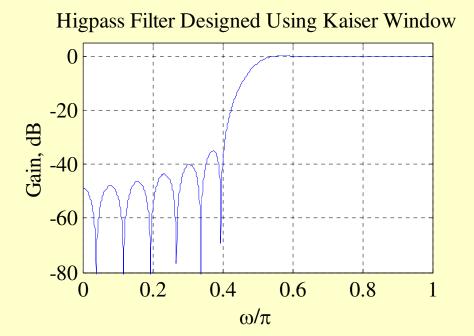
Plot of gain response





- Example Design using a Kaiser window a highpass FIR filter with the specifications:  $\omega_p = 0.55\pi$ ,  $\omega_s = 0.4\pi$ ,  $\delta_s = 0.02$
- Code fragments to use
- [N, Wn, beta, ftype] = kaiserord(fpts, mag, dev);
   b = fir1(N, Wn, 'ftype', kaiser(N+1, beta));
   where fpts = [0.4 0.55]
   mag = [0 1]
   dev = [0.02 0.02]

Plot of gain response



• Example - Design using a Hamming window an FIR filter of order 100 with three different constant magnitude levels: 0.3 in the frequency range [0, 0.28], 1.0 in the frequency range [0.3, 0.5], and 0.7 in the frequency range [0.52, 1.0]

Code fragment to use

```
b = fir2(100, fpts, mval);
where fpts = [0 0.28 0.3 0.5 0.52 1];
mval = [0.3 0.3 1.0 1.0 0.7 0.7];
```

