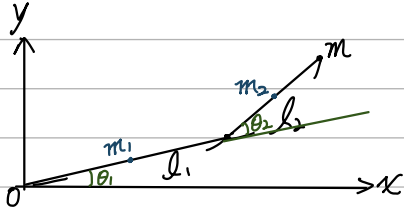
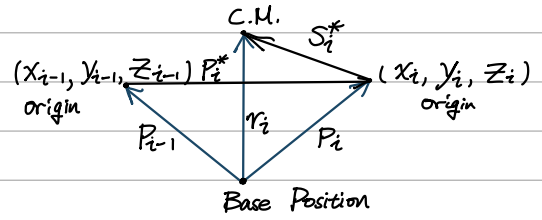


Linearity Velocity: $V_{i+1} = W_{i+1} \times P_{i+1}^* + V_i \rightarrow V_{i+1} = \dot{W}_{i+1} \times P_{i+1}^* + W_{i+1} \times (W_{i+1} \times P_{i+1}^*) + V_i$

Newton's equation: $F_i = \frac{d}{dt}(m_i \cdot V_{ci}) = m_i \cdot \dot{V}_{ci}$ V_{ci} is the velocity of center of mass (C.M.)

Euler's equation: $N_i = \frac{d}{dt}(J_i \cdot W_i) = J_i \cdot \dot{W}_i + W_i \times (J_i \cdot W_i)$

$$\begin{cases} f_i = F_i + f_{i+1} \\ n_i = N_i + n_{i+1} + P_i^* \times f_{i+1} + (P_i^* + S_i) \times F_i \\ \tau_i = n_i^T \bar{Z}_{i-1}, R \\ \tau_i = f_i^T \bar{Z}_{i-1}, P \end{cases}$$



For the 2-link robot manipulator example in the class with CM shift to the middle of each link and with a load m held at the top of the second link.

$$W_{1z} = \dot{\theta}_1 \quad \dot{V}_1 = \dot{W}_1 \times P_1^* + W_1 \times (W_1 \times P_1^*) + \dot{V}_0 \quad \text{where } \dot{V}_0 = [0 \ 0 \ 0]^T$$

$$\dot{W}_{1z} = \ddot{\theta}_1 \Rightarrow \dot{V}_1 = \dot{W}_1 \times [l_1 C_1 \ l_1 S_1 \ 0]^T + W_1 \times \{W_1 \times [l_1 C_1 \ l_1 S_1 \ 0]^T\} + \dot{V}_0$$

$$= [-l_1 S_1 \ddot{\theta}_1 - l_1 C_1 \dot{\theta}_1^2 \ l_1 C_1 \ddot{\theta}_1 - l_1 S_1 \dot{\theta}_1^2 + \dot{\theta}_1 \ 0]^T$$

$$V_{ci} = W_i \times S_i + V_i \rightarrow \dot{V}_{ci} = \dot{W}_i \times S_i + W_i \times (W_i \times S_i) + \dot{V}_i, \quad \text{where } S_i = -\frac{1}{2} P_i^*$$

$$\dot{V}_{c1} = \begin{bmatrix} -\frac{1}{2} l_1 S_1 \ddot{\theta}_1 - \frac{1}{2} l_1 C_1 \dot{\theta}_1^2 \\ \frac{1}{2} l_1 C_1 \ddot{\theta}_1 - \frac{1}{2} l_1 S_1 \dot{\theta}_1^2 + \dot{\theta}_1 \\ 0 \end{bmatrix} \quad F_1 = m_1 \dot{V}_{c1}, \quad J_1 = \begin{bmatrix} \frac{1}{4} m_1 l_1^2 & 0 & 0 \\ 0 & \frac{1}{4} m_1 l_1^2 & 0 \\ 0 & 0 & \frac{1}{4} m_1 l_1^2 \end{bmatrix} \quad N_1 = J_1 \dot{W}_1 + W_1 \times (J_1 W_1)$$

$$W_2 = \dot{\theta}_1 + \dot{\theta}_2 \quad \dot{W}_2 = \ddot{\theta}_1 + \ddot{\theta}_2$$

$$\dot{V}_2 = \dot{W}_2 \times P_2^* + W_2 \times (W_2 \times P_2^*) + \dot{V}_1$$

$$= \begin{bmatrix} 0 \\ 0 \\ \dot{\theta}_1 + \dot{\theta}_2 \end{bmatrix} \times \begin{bmatrix} l_2 C_2 \\ l_2 S_2 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ \dot{\theta}_1 + \dot{\theta}_2 \end{bmatrix} \times \left(\begin{bmatrix} 0 \\ 0 \\ \dot{\theta}_1 + \dot{\theta}_2 \end{bmatrix} \times \begin{bmatrix} l_2 C_2 \\ l_2 S_2 \\ 0 \end{bmatrix} \right) \times \dot{V}_1 = \begin{bmatrix} -l_2 S_2 (\ddot{\theta}_1 + \ddot{\theta}_2) - l_2 C_2 (\dot{\theta}_1 + \dot{\theta}_2)^2 - l_1 S_1 \ddot{\theta}_1 - l_1 C_1 \dot{\theta}_1^2 \\ l_2 C_2 (\ddot{\theta}_1 + \ddot{\theta}_2) - l_2 S_2 (\dot{\theta}_1 + \dot{\theta}_2)^2 + l_1 C_1 \ddot{\theta}_1 - l_1 S_1 \dot{\theta}_1^2 + \dot{\theta}_1 \\ 0 \end{bmatrix}$$

$$\dot{V}_{2c} = \dot{W}_2 \times S_2 + W_2 \times (W_2 \times S_2) + \dot{V}_2 = \begin{bmatrix} -\frac{1}{2} l_2 S_2 (\ddot{\theta}_1 + \ddot{\theta}_2) - \frac{1}{2} l_2 C_2 (\dot{\theta}_1 + \dot{\theta}_2)^2 - l_1 S_1 \ddot{\theta}_1 - l_1 C_1 \dot{\theta}_1^2 \\ \frac{1}{2} l_2 C_2 (\ddot{\theta}_1 + \ddot{\theta}_2) - \frac{1}{2} l_2 S_2 (\dot{\theta}_1 + \dot{\theta}_2)^2 + l_1 C_1 \ddot{\theta}_1 - l_1 S_1 \dot{\theta}_1^2 + \dot{\theta}_1 \\ 0 \end{bmatrix}$$

where $S_2 = -\frac{1}{2} P_2^*$

$$F_2 = m_2 \dot{V}_{2c}, \quad J_2 = \begin{bmatrix} \frac{1}{4} m_2 l_2^2 & 0 & 0 \\ 0 & \frac{1}{4} m_2 l_2^2 & 0 \\ 0 & 0 & \frac{1}{4} m_2 l_2^2 \end{bmatrix}, \quad N_2 = J_2 \dot{W}_2 + W_2 \times (J_2 W_2)$$

$$f_2 = F_2 + f_3, \quad \text{where } f_3 = [0 \ mg \ 0]^T$$

$$\Rightarrow n_2 = n_3 + P_2^* \times f_3 + (P_2^* + S_2) \times F_2 + N_2, \quad n_3 = 0 \text{ (zero vector)}$$

$$= \begin{bmatrix} l_2 C_{12} \\ l_2 S_{12} \\ 0 \end{bmatrix} \times \begin{bmatrix} 0 \\ mg \\ 0 \end{bmatrix} + \begin{bmatrix} \frac{1}{2} l_2 C_{12} \\ \frac{1}{2} l_2 S_{12} \\ 0 \end{bmatrix} \times m_2 \dot{V}_{2c} + N_2$$

$$\text{due to } N_2 \rightarrow \tau_2 = n_2^T \bar{Z}_1, \quad \bar{Z}_1 = [0 \ 0 \ 1]^T \quad f_1 = F_1 + f_2 = m_1 \dot{V}_{c1} + m_2 \dot{V}_{c2} + [0 \ mg \ 0]^T$$

$$n_1 = n_2 + P_1^* \times f_2 + (P_1^* + S_1) \times F_1 + N_1$$

$$= n_2 + \begin{bmatrix} l_1 C_1 \\ l_1 S_1 \\ 0 \end{bmatrix} \times (m_2 \dot{V}_{c2} + \begin{bmatrix} 0 \\ mg \\ 0 \end{bmatrix}) + \begin{bmatrix} \frac{1}{2} l_1 C_1 \\ \frac{1}{2} l_1 S_1 \\ 0 \end{bmatrix} \times m_1 \dot{V}_{c1} + N_1$$

$$= n_2 + \begin{bmatrix} l_1 C_1 \\ l_1 S_1 \\ 0 \end{bmatrix} \times \begin{bmatrix} -\frac{1}{2} m_2 l_2 S_{12} (\ddot{\theta}_1 + \ddot{\theta}_2) - \frac{1}{2} m_2 l_2 C_{12} (\dot{\theta}_1 + \dot{\theta}_2)^2 - m_2 l_1 S_1 \ddot{\theta}_1 - m_2 l_1 C_1 \dot{\theta}_1^2 \\ \frac{1}{2} m_2 l_2 C_{12} (\dot{\theta}_1 + \dot{\theta}_2) - \frac{1}{2} m_2 l_2 S_{12} (\dot{\theta}_1 + \dot{\theta}_2)^2 + m_2 l_1 C_1 \ddot{\theta}_1 - m_2 l_1 S_1 \dot{\theta}_1^2 + (m_2 - m_1) g \\ 0 \end{bmatrix} + \begin{bmatrix} \frac{1}{2} l_1 C_1 \\ \frac{1}{2} l_1 S_1 \\ 0 \end{bmatrix} \begin{bmatrix} -\frac{1}{2} m_1 l_1 S_1 \ddot{\theta}_1 - \frac{1}{2} m_1 l_1 C_1 \dot{\theta}_1^2 \\ \frac{1}{2} m_1 l_1 C_1 \ddot{\theta}_1 - \frac{1}{2} m_1 l_1 S_1 \dot{\theta}_1^2 + m_1 g \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ \frac{1}{4} m_1 l_1^2 \ddot{\theta}_1 \end{bmatrix}$$

$$\tau_1 = n_1^T \vec{Z}_0, \quad \vec{Z}_0 = [0 \ 0 \ 1]^T$$

在此系統內將 load m 以 $x-y$ 方向的力 mg 替代, 得 $\tau_1 = \tau_2$, 從方程式的推導中可以看到 load m 以一個力 f_3 代表, 因此若從方程式回推系統的動態結構, 並無法區別 f_3 是 load m or external force $-mg$.

$$\begin{aligned} \dot{W}_0 &= 0 & W_1 &= [0 \ 0 \ \dot{\theta}_1]^T & W_2 &= [0 \ 0 \ \dot{\theta}_1 + \dot{\theta}_2]^T & P_1^* &= [l_1 C_1 \ l_1 S_1 \ 0]^T \\ \dot{W}_1 &= [0 \ 0 \ \ddot{\theta}_1]^T & \dot{W}_2 &= [0 \ 0 \ \ddot{\theta}_1 + \ddot{\theta}_2]^T & P_2^* &= [l_2 C_{12} \ l_2 S_{12} \ 0]^T \\ S_1^* &= -\frac{1}{2} P_1^* = \begin{bmatrix} -\frac{1}{2} l_1 C_1 \\ -\frac{1}{2} l_1 S_1 \\ 0 \end{bmatrix} & S_2^* &= -\frac{1}{2} P_2^* = \begin{bmatrix} -\frac{1}{2} l_2 C_{12} \\ -\frac{1}{2} l_2 S_{12} \\ 0 \end{bmatrix} & f_3 &= \begin{bmatrix} 0 \\ mg \\ 0 \end{bmatrix} \end{aligned}$$