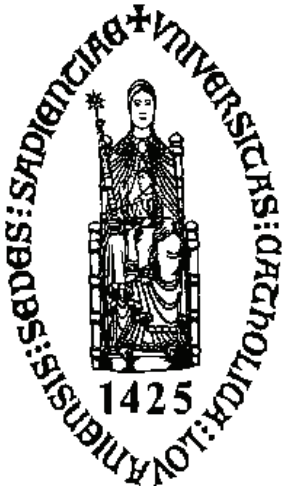


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---

# Low-Noise Amplifiers



**Willy Sansen**

**KULeuven, ESAT-MICAS**  
**Leuven, Belgium**

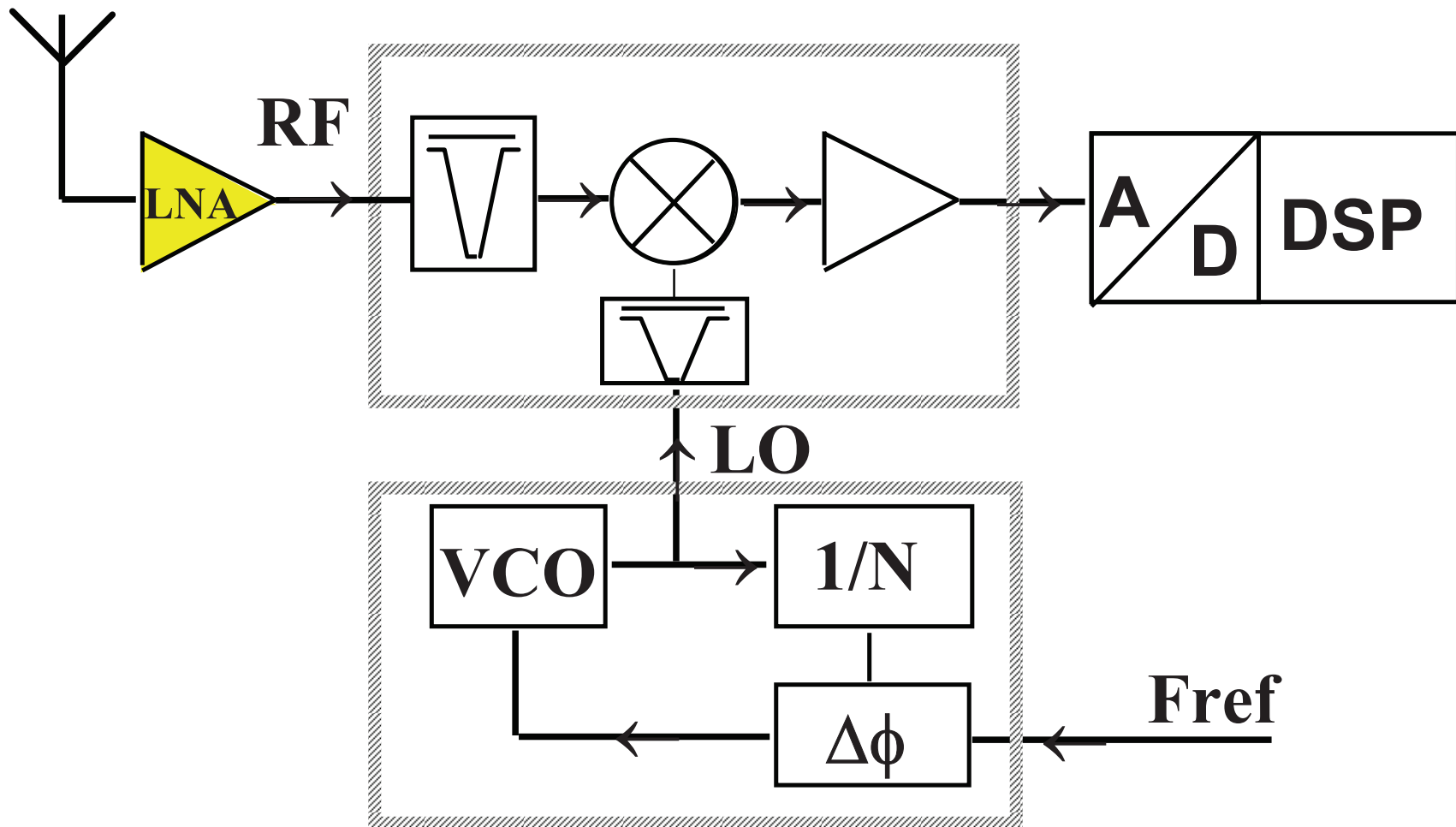
[willy.sansen@esat.kuleuven.be](mailto:willy.sansen@esat.kuleuven.be)



---

# Receiver Topology

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## Table of contents

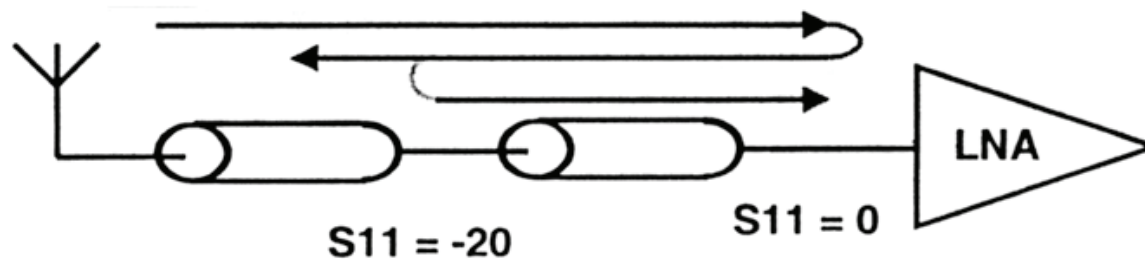
---

- **Noise Figure and Impedance Matching**
- **LNA specifications and linearity**
- **Input amplifier or cascode**
- **Non-quasi-static MOST model**
- **More realizations**
- **Inductive ESD protection**

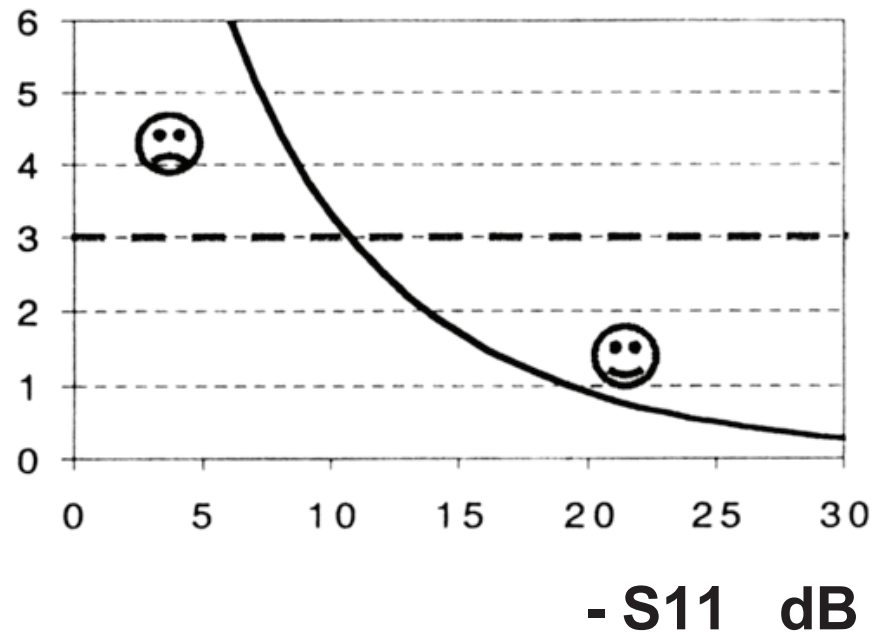
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# Transmission line effects

---



**Unwanted Signal  
over Signal in -dB**



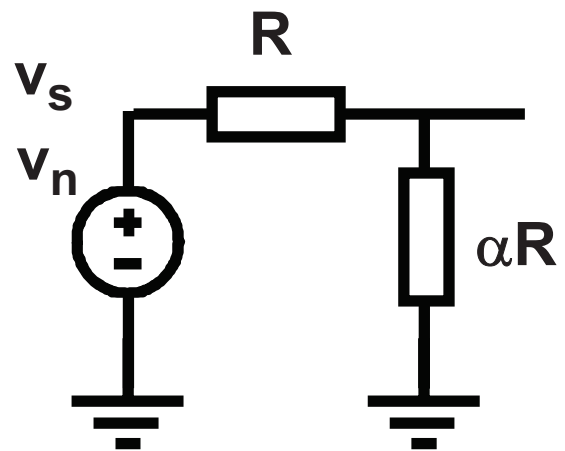
---

# Noise Figure

---

$$V_n = \sqrt{4RkTB}$$

$$V_s = \sqrt{4R.S}$$



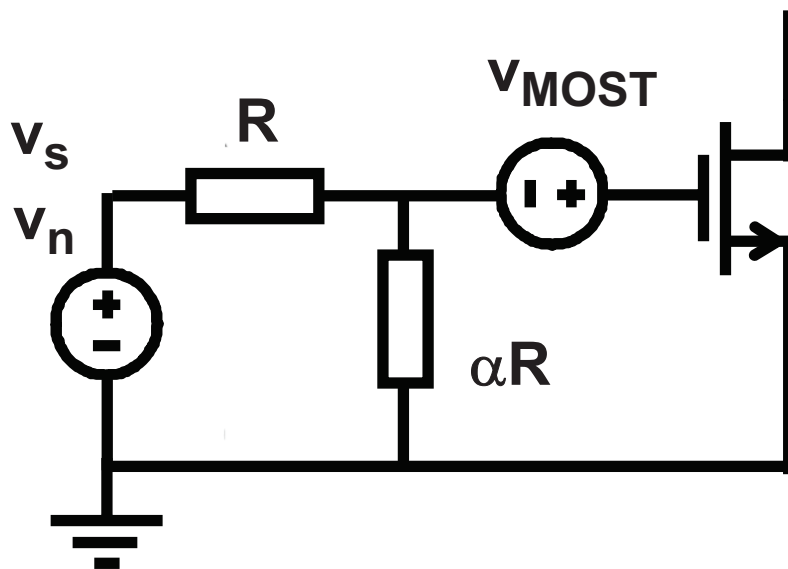
$$NF = \frac{\text{total output noise power}}{\text{output noise due to input source}}$$

$$NF = \frac{4kTB\left[\frac{\alpha}{(1+\alpha)^2} + \frac{1}{(1+\alpha)^2}\right]}{4kTB\frac{\alpha}{(1+\alpha)^2}}$$

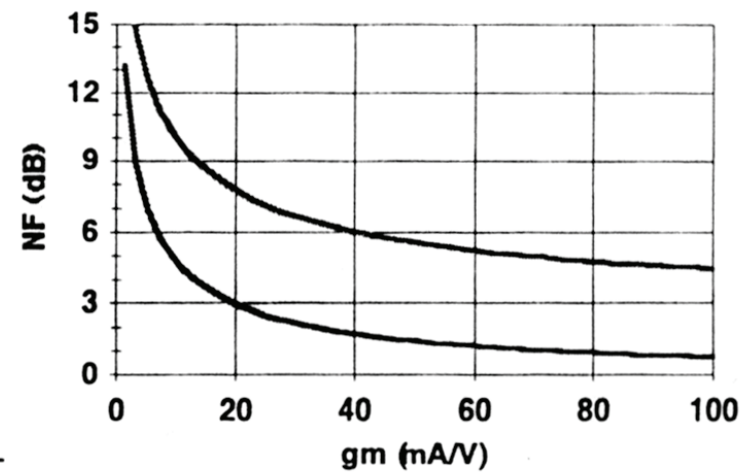
$$NF = \frac{1+\alpha}{\alpha}$$

**Resistive match :  $\alpha = 1$  :  $NF = 3$  dB**

# MOST amplifier with Resistive termination



$$V_{MOST} = 4kT \frac{2}{3 g_m}$$



$$NF = \frac{1 + \alpha}{\alpha} + \left(\frac{1 + \alpha}{\alpha}\right)^2 \frac{1}{g_m \cdot R}$$

$\alpha = 1$  (Matched):

$\alpha = \infty$  (Open circuit):

$NF = 2 + \frac{4}{g_m \cdot R}$
$NF = 1 + \frac{1}{g_m \cdot R}$

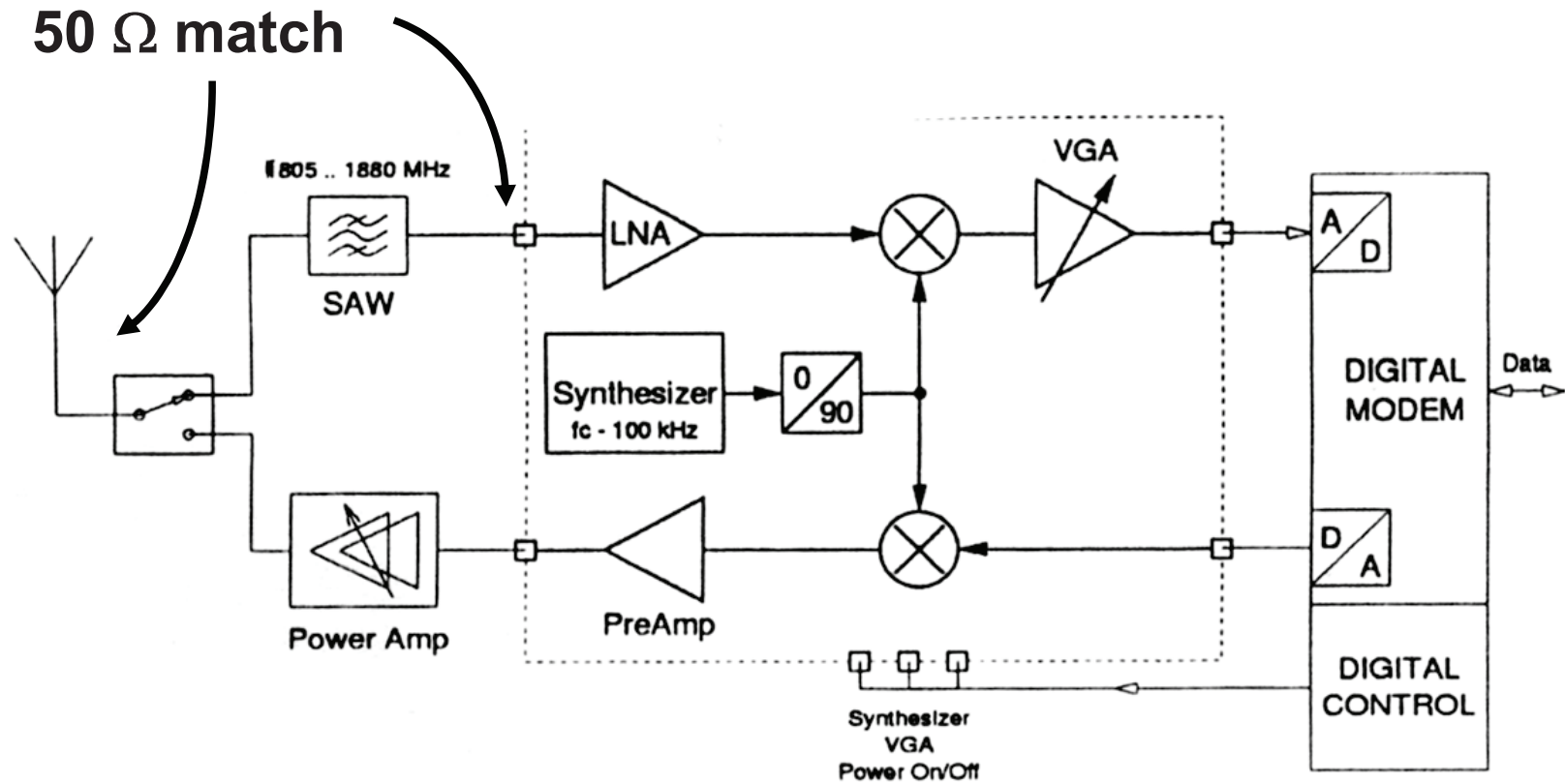
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## Table of contents

---

- Noise Figure and Impedance Matching
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# Transceiver





---

## Minimum NF and IIP3 for DCS-1800

---

Sensitivity -100 dBm

SNR 9 dB

Input noise -109 dBm

kT = -174 dBm

Bandwidth (200 kHz) + 53 dB

NF :  $-109 - (-174 + 53) =$  12 dB

Attenuating blocking filter : 3 dB **NF < 9 dB**

+ 3 dB Sensitivity -97 dBm

SNR (-49 dBm sine) 9 dB

IIP3 =  $-49 + (-49 - (-106/2)) =$  -20.5 dBm

With attenuating blocking filter : 3 dB **IIP3 < -23.5 dBm**

---

# Linearity CMOS amplifier

---

Velocity saturation

$$v_{\max} \approx 10^7 \text{ cm/s}$$

$$\Theta L \approx 0.2 \text{ } \mu\text{m/V}$$

$$I_{ds} = \frac{\mu_0 C_{ox}}{2n} \cdot \frac{W}{L} \cdot \frac{(V_{GS} - V_T)^2}{1 + \Theta \cdot (V_{GS} - V_T)}$$

$$\Theta = \theta + \frac{\mu_0}{L_{eff} \cdot v_{\max} \cdot n}$$

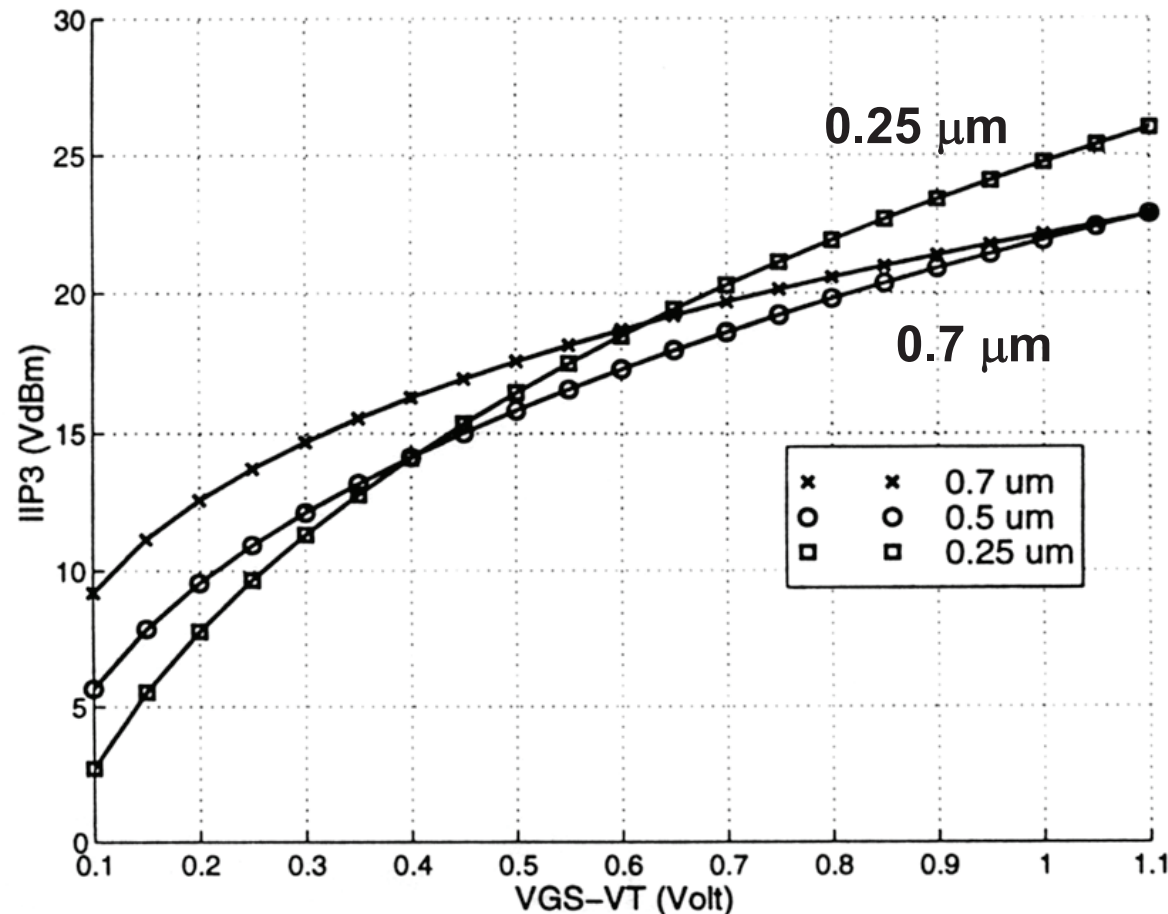
$$IM2 = \frac{v}{V_{GS} - V_T} \cdot \frac{1}{(1 + r) \cdot (2 + r)}$$

$$r = \Theta \cdot (V_{GS} - V_T)$$

$$IM3 = \frac{3}{4} \frac{v^2}{(V_{GS} - V_T)} \cdot \frac{\Theta}{(1 + r)^2 \cdot (2 + r)}$$

$$IIP3 \cong 11.25 + 10 \cdot \text{Log}_{10} \left( (V_{GS} - V_T) \cdot (1 + r)^2 \cdot (2 + r) / \Theta \right)$$

# IIP3 for different CMOS technologies



Velocity saturation

$v_{\text{max}} \approx 10^7 \text{ cm/s}$

$\Theta L \approx 0.2 \mu\text{m/V}$

$L = 0.7 \mu\text{m} \quad \Theta \approx 0.5 \text{ V}^{-1}$

$L = 0.25 \mu\text{m} \quad \Theta \approx 1.2 \text{ V}^{-1}$

---

# Table of contents

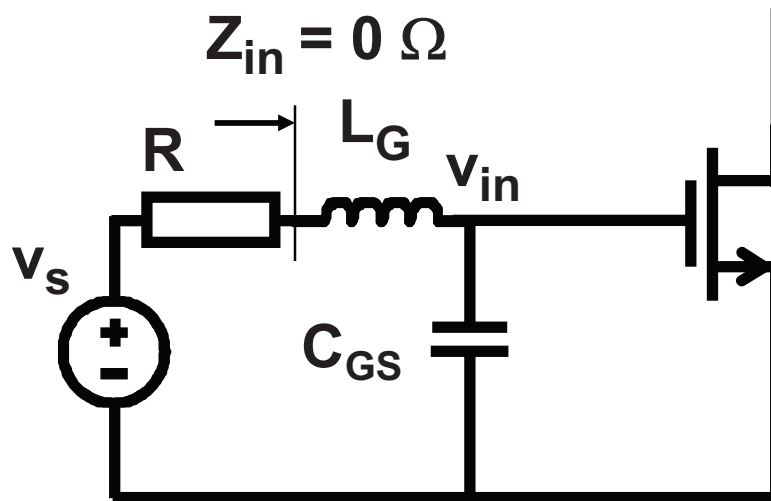
---

- **Noise Figure and Impedance Matching**
- **LNA specifications and linearity**
- **Input amplifier or cascode**
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- **More realizations**
- **Inductive ESD protection**

---

## Inductive input : gain

---



$$Z_{in} = \frac{1}{j\omega C_{GS}} + j\omega L_G$$

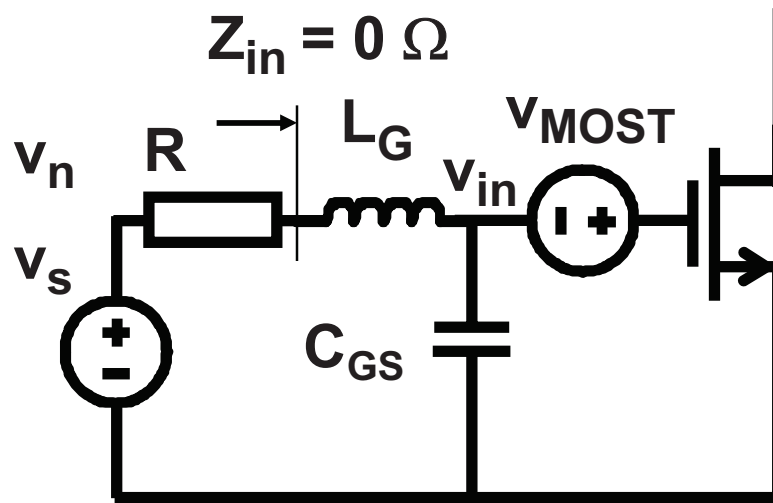
$$\textcircled{1} \quad L_G = \frac{1}{C_{GS} \omega_{in}^2}$$

$$\text{At } f_{in} = \frac{1}{2\pi \sqrt{L_G C_{GS}}} \quad \textcircled{2} \quad \frac{v_{in}}{v_s} = \frac{1}{R \sqrt{C_{GS} / L_G}} = \frac{1}{2\pi R C_{GS} \omega_{in}}$$

Extra Gain  $\approx 10$  dB

$$L_G = 15 \text{ nH}; C_{GS} = 0.5 \text{ pF}; f_{in} = 1.8 \text{ GHz}; R = 50 \Omega;$$

## Inductive input : noise



$$v_{MOST} = 4kT \frac{2}{3 g_m}$$

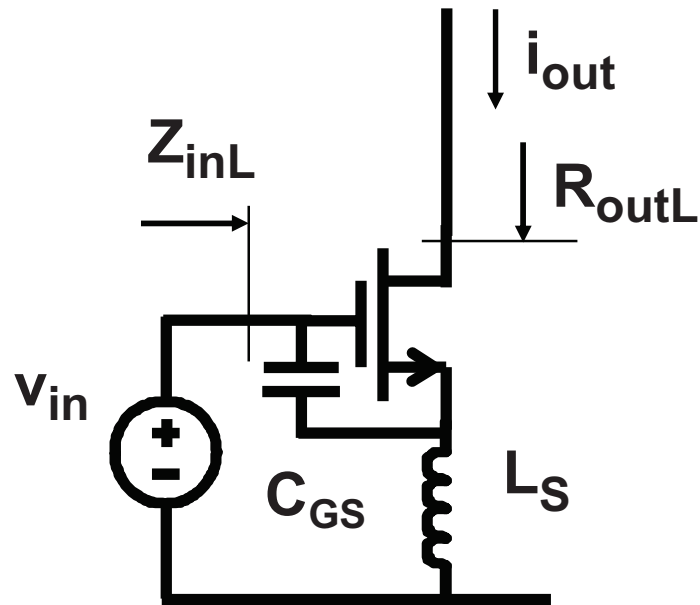
$$\frac{v_{in}}{v_s} = \frac{1}{R \sqrt{C_{GS} / L_G}}$$

$$NF = 1 + \frac{(R \sqrt{C_{GS} / L_G})^2}{g_m R} = 1 + \frac{R C_{GS}}{g_m L_G} = 1 + g_m R \left( \frac{\omega_{in}}{\omega_T} \right)^2$$

$$NF_{g_m R=1} \approx 0.4 \text{ dB}$$

$$L_G = 15 \text{ nH}; C_{GS} = 0.5 \text{ pF}; f_{in} = 1.8 \text{ GHz}$$

# Inductive degeneration in the Source



$$g_{mL} = \frac{g_m}{1 + g_m L_S s}$$

$$R_{outL} = r_{DS} (1 + g_m L_S s)$$

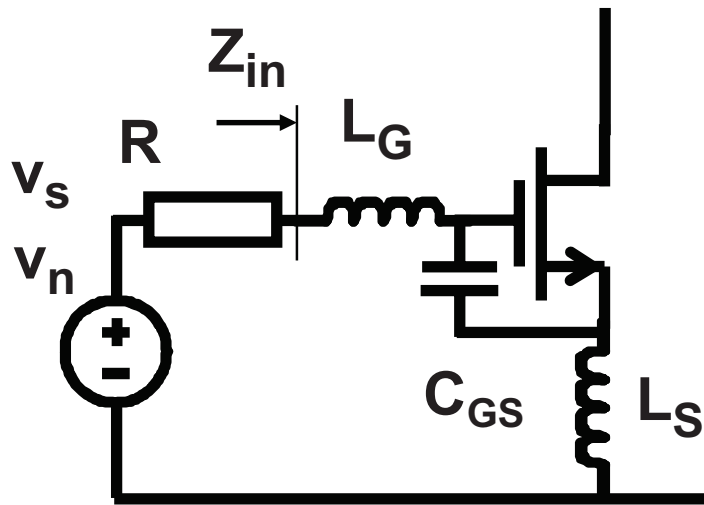
$$Z_{inL} = g_m \frac{L_S}{C_{GS}} + \frac{1 + L_S C_{GS} s^2}{s C_{GS}}$$

$$Z_{inL} = L_S \omega_T + L_S s + \frac{1}{s C_{GS}}$$

---

## Inductive degeneration in Source and Gate

---



$$Z_{in} = \frac{1}{j\omega C_{GS}} + j\omega (L_G + L_S) + \omega_T L_S$$

$$\textcircled{1} \quad L_G + L_S = \frac{1}{C_{GS} \omega_{in}^2}$$

$$\textcircled{2} \quad L_S = \frac{R C_{GS}}{g_m} = \frac{R}{\omega_T}$$

**Impedance Match :**

**$\text{Re}(Z_{in}) = R_{in} = R$  at  $\omega_{in}$**

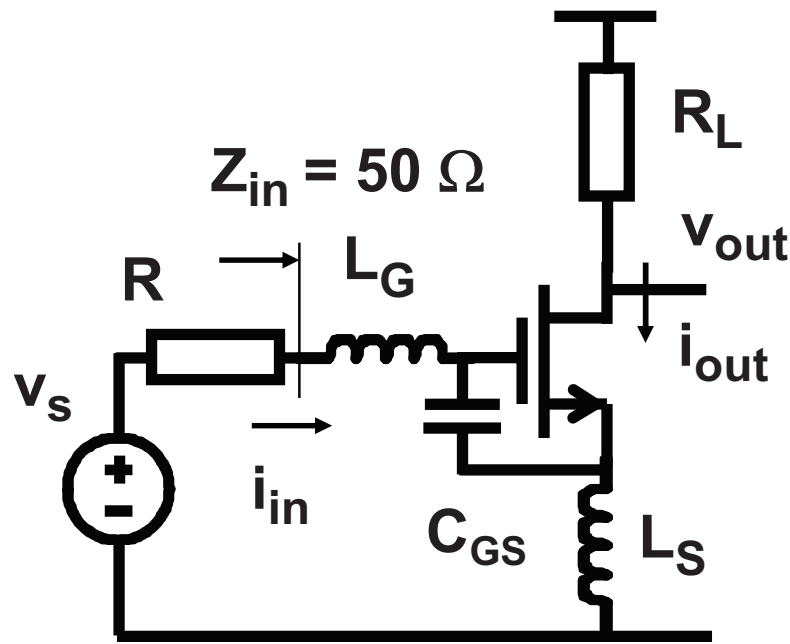
**$\text{Im}(Z_{in}) = 0$**



---

## Inductive degeneration : gain

---



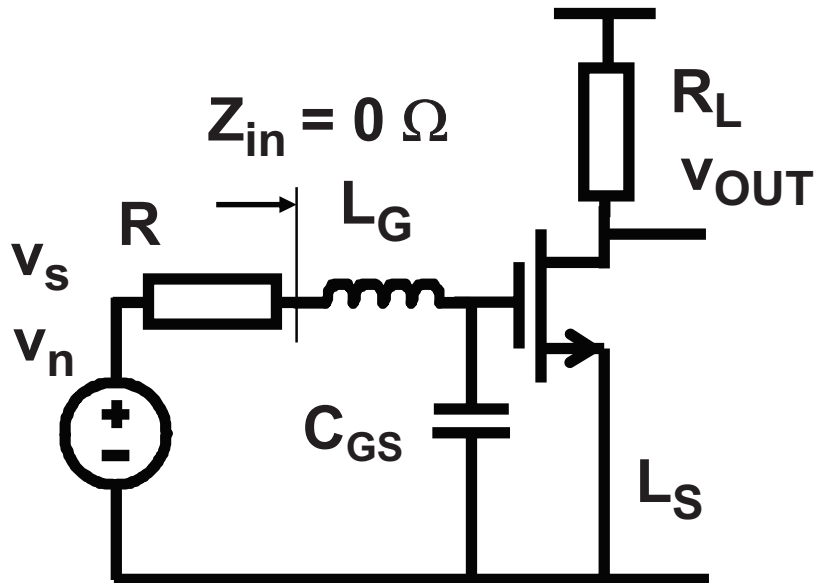
Under matching :

$$\frac{i_{out}}{i_{in}} = \frac{\omega_T}{\omega_{in}}$$

$$\frac{v_{out}}{v_{in}} = \frac{i_{out}}{i_{in}} \frac{R_L}{2R}$$

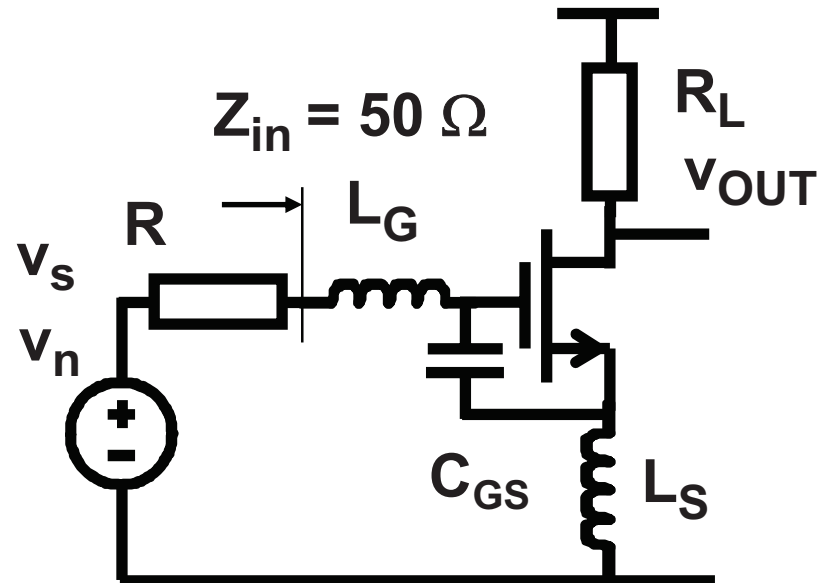
$$G_P = \frac{P_{out}}{P_{in}} = \left( \frac{\omega_T}{\omega_{in}} \right)^2 \frac{R_L}{2R}$$

# Inductive degeneration : gain



$$G_v = \frac{g_m}{\sqrt{C_{GS} / L_G}} \frac{R_L}{R}$$

$$G_v / G_{v,R=50\Omega} = 2x$$



$$G_v = \frac{g_m}{\sqrt{C_{GS} / (L_G + L_S)}} \frac{R_L}{2R}$$

---

## Inductive degeneration : Noise Figure

---

$$NF = 1 + \frac{dv_{in}^2}{dv_R^2} = 1 + \frac{R C_{GS}}{g_m (L_G + L_S)}$$

$$dv_{in}^2 = 4kT \frac{2/3}{g_m} df \approx 4kT \frac{1}{g_m} df$$

$$dv_R^2 = 4kT R df$$

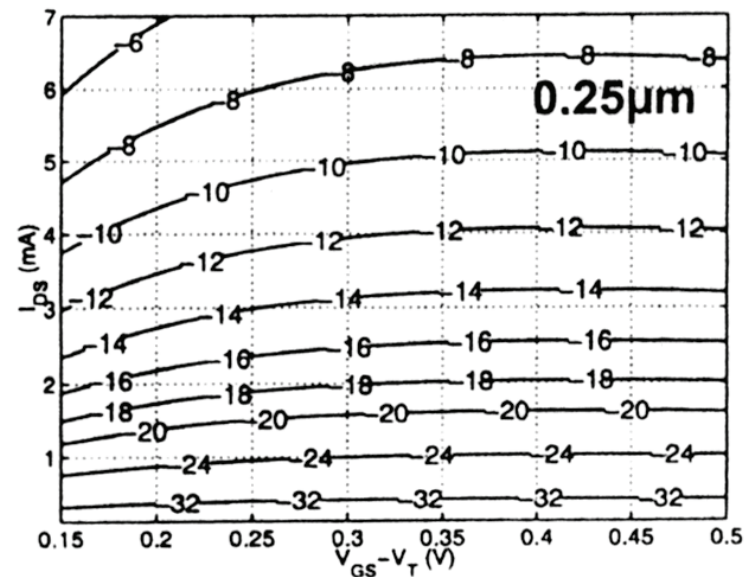
$$NF = 1 + g_m R \left( \frac{\omega_{in}}{\omega_T} \right)^2$$

# Inductive degeneration : IIP3 vs IDS

$$IIP3 \approx 11.25 + 20 \log_{10} \left( \underbrace{\sqrt{\frac{V_{gst}(2+r)^2(1+r)}{\Theta}} \frac{1 + \Theta V_{gst}}{V_{gst}^2}}_{\approx Cst} \cdot \omega_{in} \frac{100}{\mu_0} I_D L^2 \right)$$

$$IIP3 \approx Cst + 20 \log_{10} \left( \frac{\omega_{in} I_D L^2}{\mu_0} \right)$$

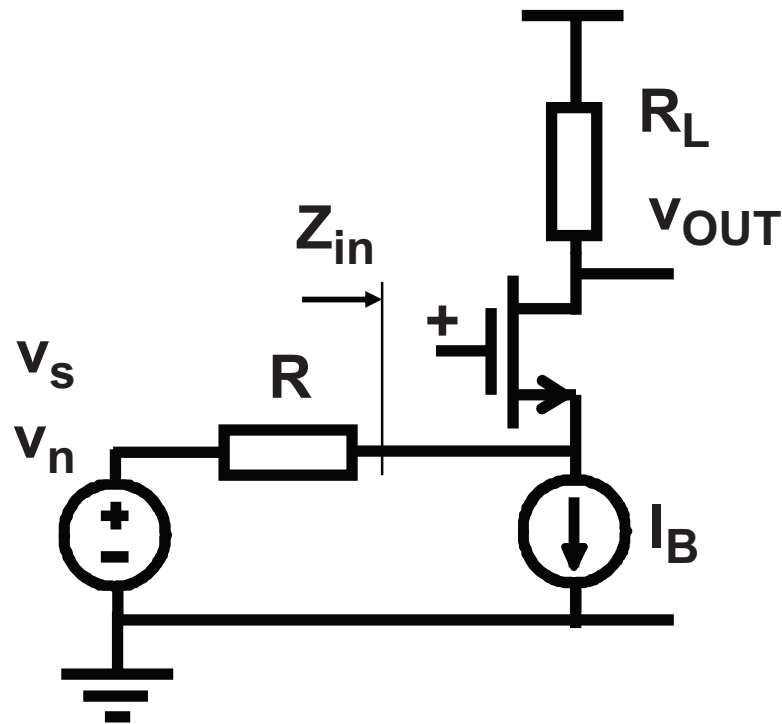
$$r = \Theta V_{gst} = \Theta (V_{GS} - V_T)$$



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## Cascode or current input : $Z_{in}$

---



$$R_{in} = \frac{1}{g_m}$$

$$= 50 \, \Omega \text{ at } 20 \text{ mS}$$

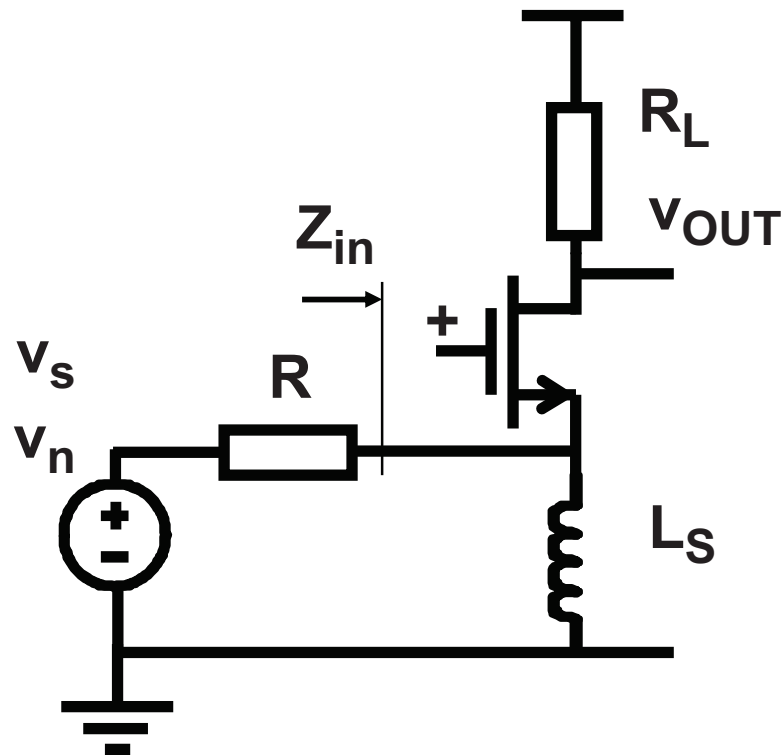
$$R_{in} = \frac{1}{g_m} \frac{1}{n} \left( 1 - \frac{R_L}{2r_{DS}} \right)$$

Depends on  $r_{DS}$  !

---

## Cascode or current input : Gain & NF

---



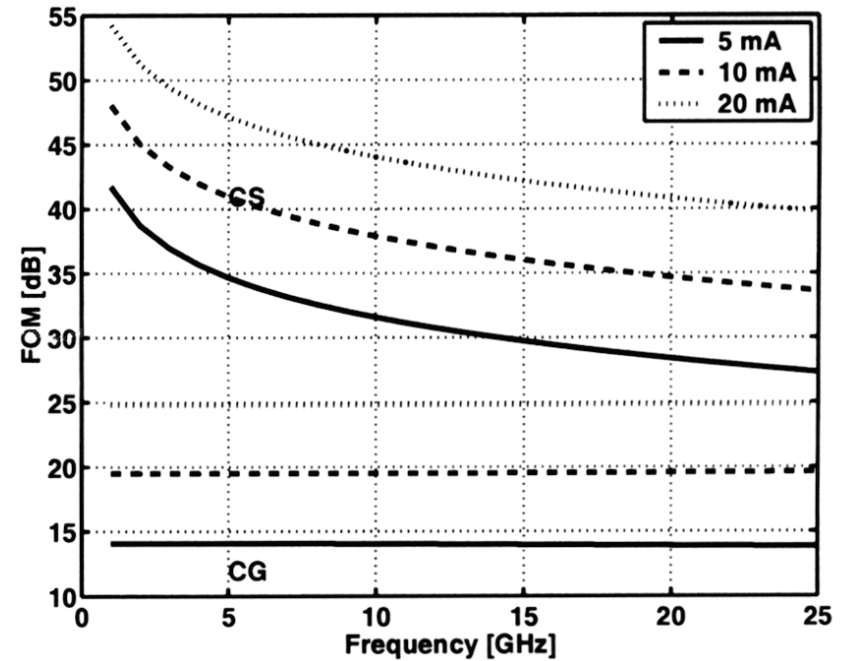
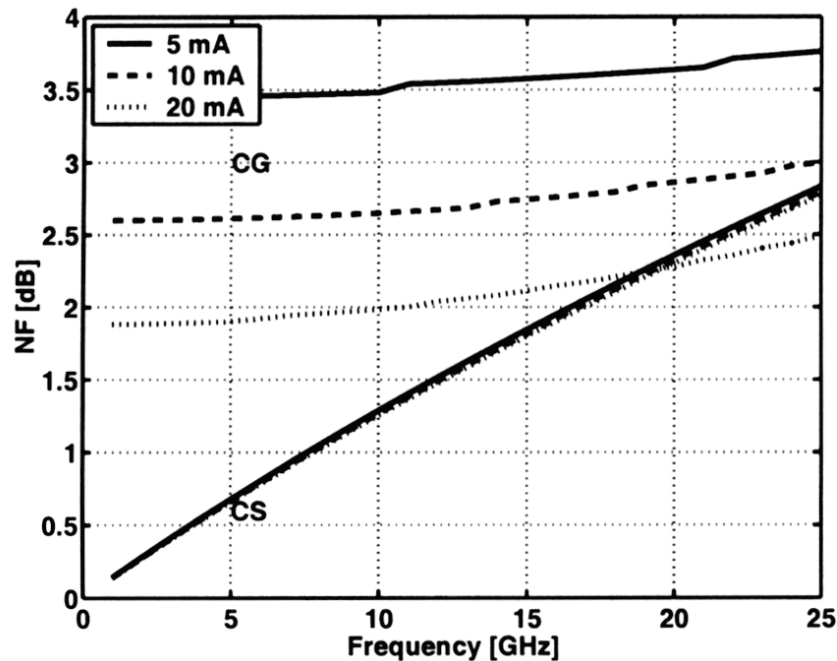
$$\frac{i_{out}}{i_{in}} = 1$$

$$G_P = \frac{P_{out}}{P_{in}} = \frac{R_L}{4R}$$

$$NF = 1 + \frac{1}{g_m R}$$

Match : NF = 3 dB

# LNA : amplifier versus cascode



$$\text{FOM} = \frac{G_P \text{ IIP3}}{\text{NF} - 1}$$

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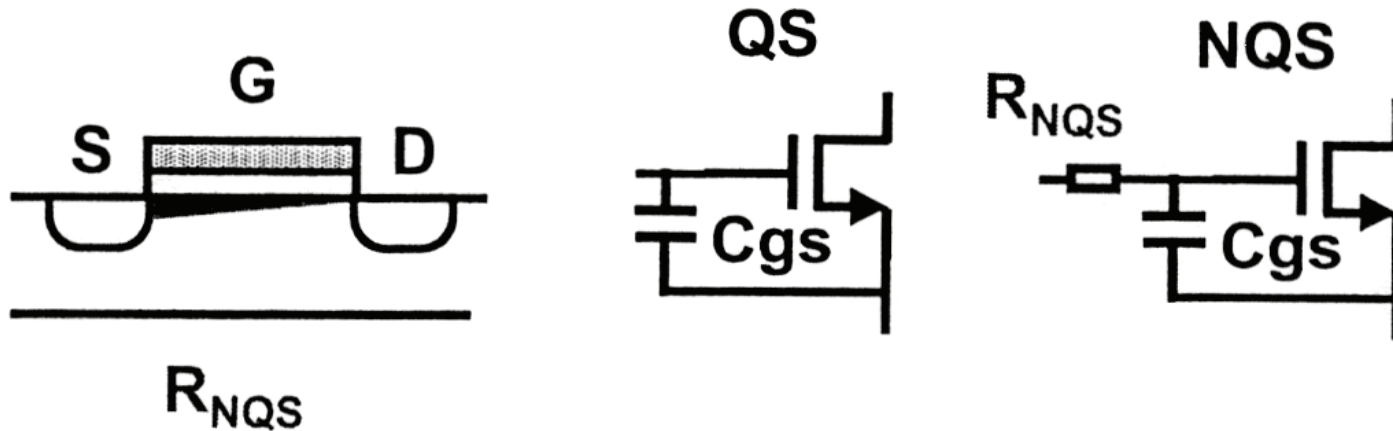
- **Noise Figure and Impedance Matching**
- **LNA specifications and linearity**
- **Input amplifier or cascode**
- **Non-quasi-static MOST model**
- **More realizations**
- **Inductive ESD protection**



---

## Non-quasi static MOST model

---



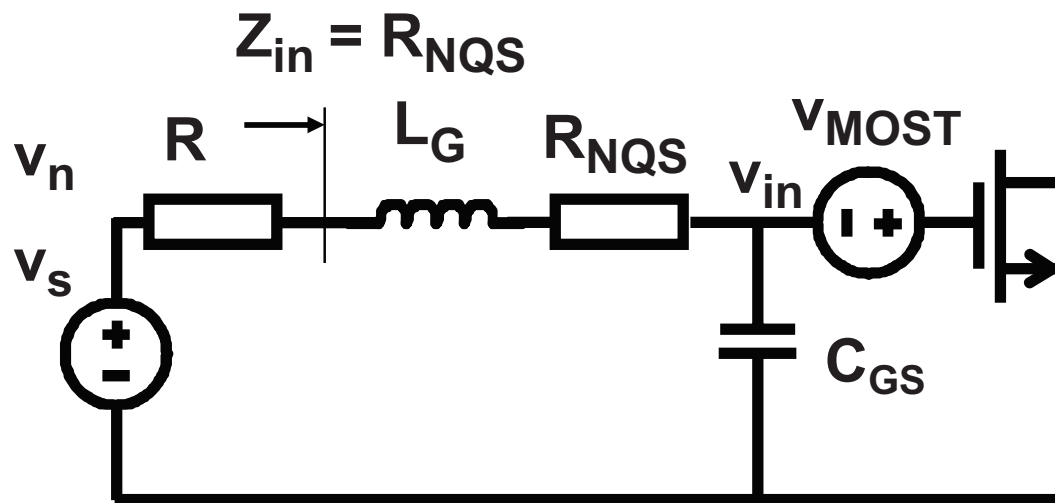
$$R_{NQS} = \frac{1}{5 g_m}$$

Normally important for  $f > f_T / 5$

$C_{GS}$  is tuned out by  $L_G$  !!

Ref.Janssens, ACD 1998

## Inductor in input

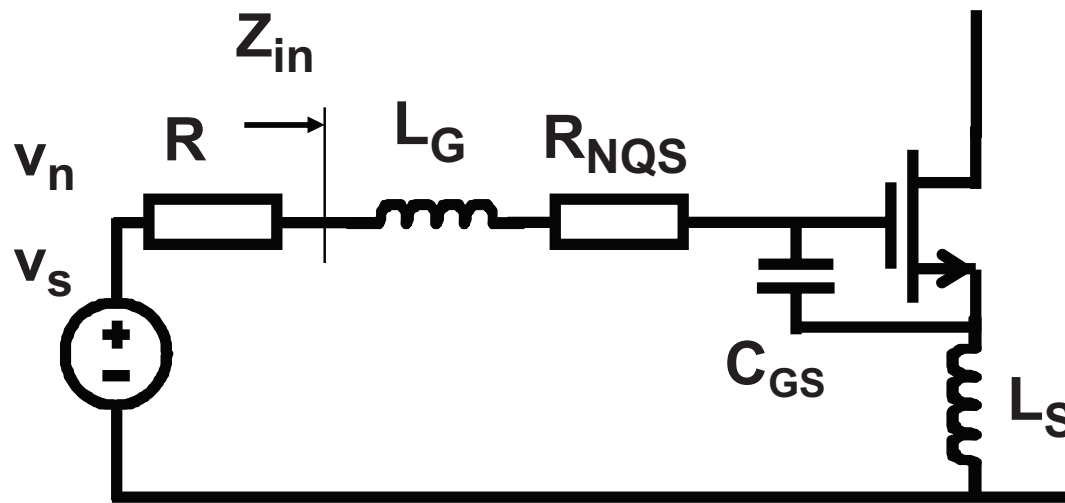


$$NF = 1 + \frac{R \cdot C_{gs}}{g_m \cdot L_g} \left(1 + \frac{R_{NQS}}{R}\right)^2 + \frac{R_{NQS}}{R}$$

$$NF_{g_m=20\text{mS}} = 1.2 \text{ dB}$$

$$NF = 1 + \frac{R \cdot C_{gs}}{g_m \cdot L_g} \left(1 + \frac{1}{5g_m R}\right)^2 + \frac{1}{5g_m R}$$

# Inductive degeneration with NQS model



$$\omega^2 C_{gs}(L_g + L_s) = 1$$

$$L_s = \frac{(R - R_{NQS})C_{gs}}{g_m}$$

$$NF = 1 + \frac{R.C_{gs}}{g_m(L_g + L_s)} \left(1 + \frac{R_{NQS}}{R}\right)^2 + \frac{R_{NQS}}{R}$$

$$NF_{gm=20mS} = 1.2 \text{ dB}$$

---

## Noise matching

---

$$NF = 1 + \frac{R.C_{gs}}{g_m.(L_g + L_s)} \left(1 + \frac{1}{5g_m R}\right)^2 + \frac{1}{5g_m R}$$

Optimum

$$R = \frac{1}{5g_m} \cdot \sqrt{1 + \frac{5.(L_g + L_s)g_m^2}{C_{gs}}} = 80\Omega$$

$$NF \approx 1 \text{ dB} \quad (g_m = 20 \text{ mS})$$

$$L_G + L_S = 15 \text{ nH}; C_{GS} = 0.5 \text{ pF}; f = 1.8 \text{ GHz}$$

---

# Noise matching (Optimum design)

---

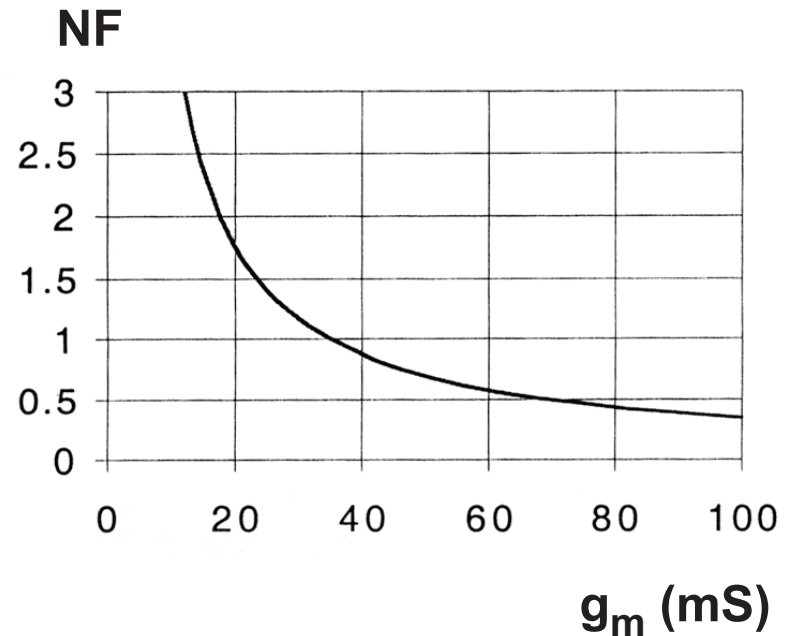
$$NF = 1 + \frac{R.C_{gs}}{gm.(Lg + Ls)} \left(1 + \frac{1}{5gmR}\right)^2 + \frac{1}{5gmR}$$

**Opt.**  $C_{gs} = \frac{5.(Lg + Ls)gm^2}{(5.Rgm)^2 - 1}$

$$NF = 1 + \frac{5gmR}{(5gmR)^2 - 1} \left(1 + \frac{1}{5gmR}\right)^2 + \frac{1}{5gmR}$$

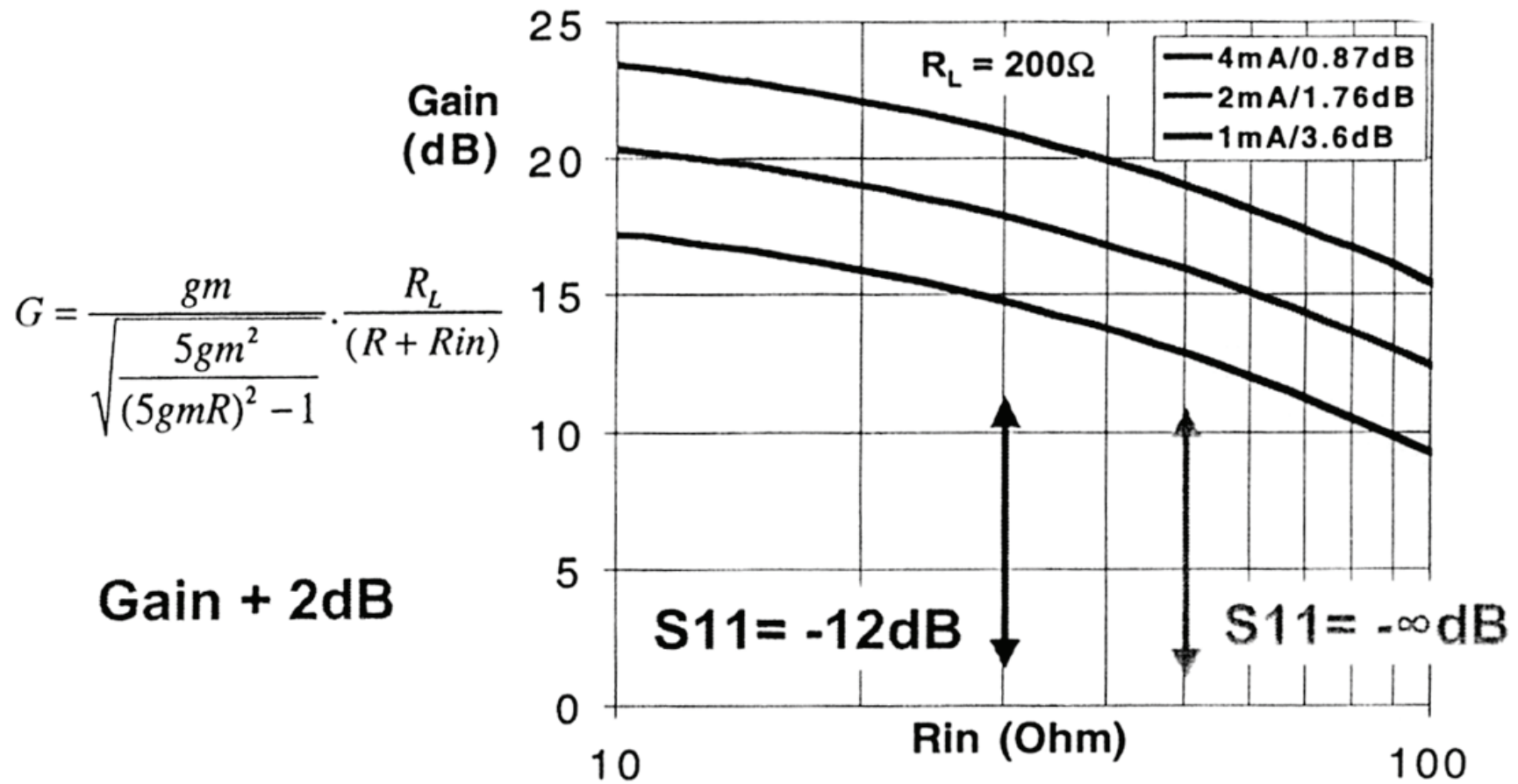
$$NF \approx 1 + \frac{2}{5gmR}$$

$$g_m R > 1$$



**Lower NF requires more power !**

# Gain vs Rin for optimal NF



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## Table of contents

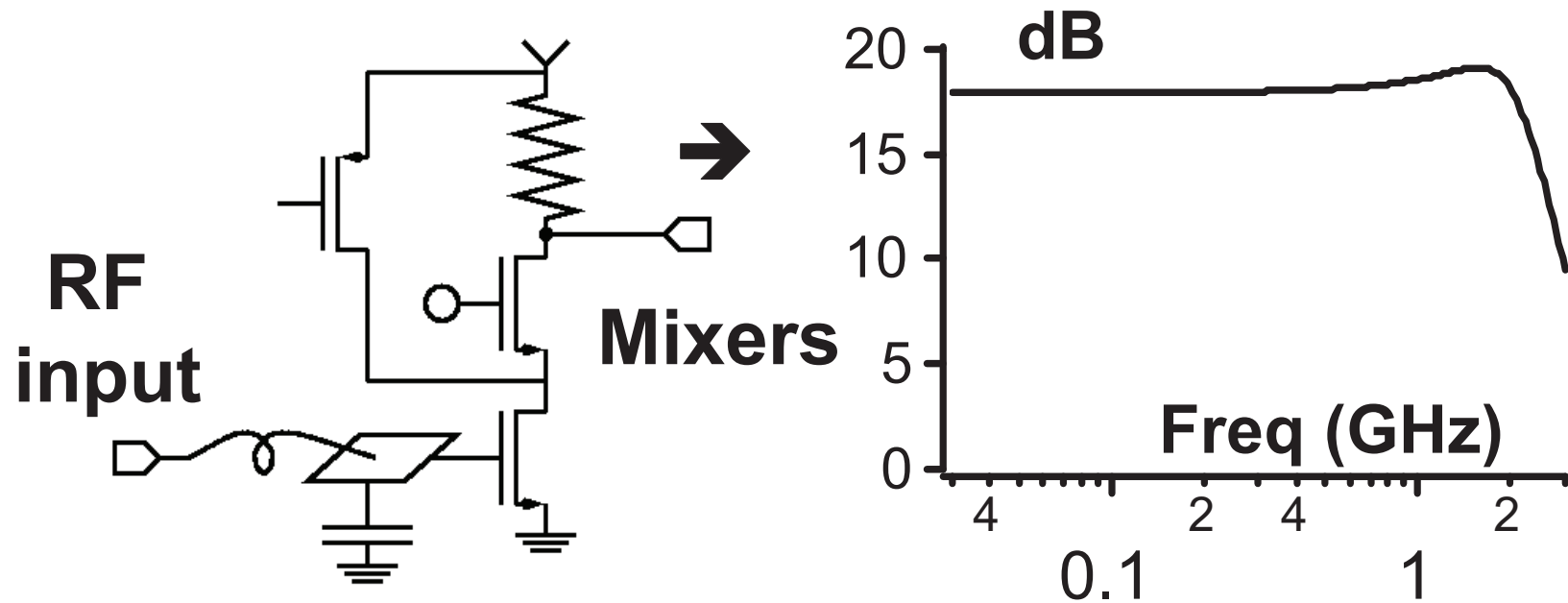
---

- **Noise Figure and Impedance Matching**
- **LNA specifications and linearity**
- **Input amplifier or cascode**
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---

# Low-noise amplifier

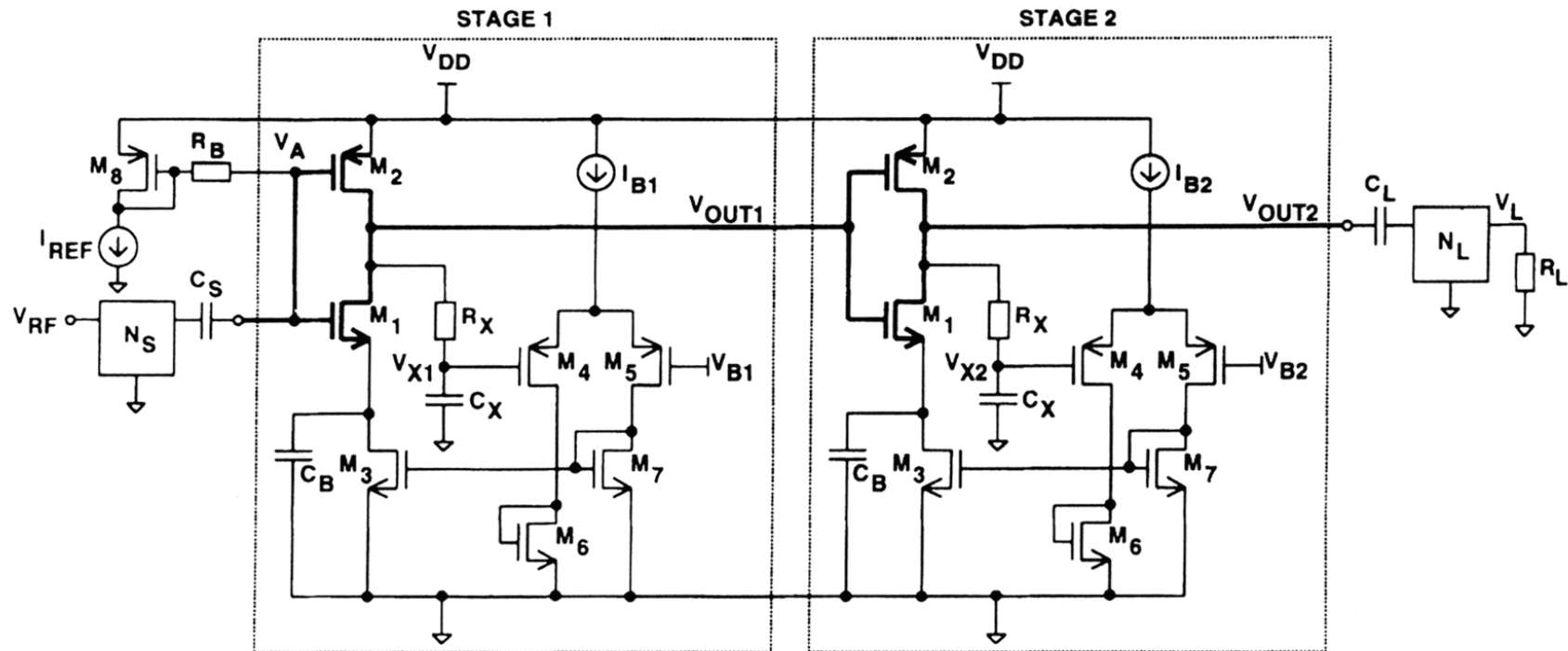
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**Broad-Band Topology : multi-mode possible**



# LNA 900 MHz with reuse



**NF = 2.2 dB**

**G = 15.6 dB**

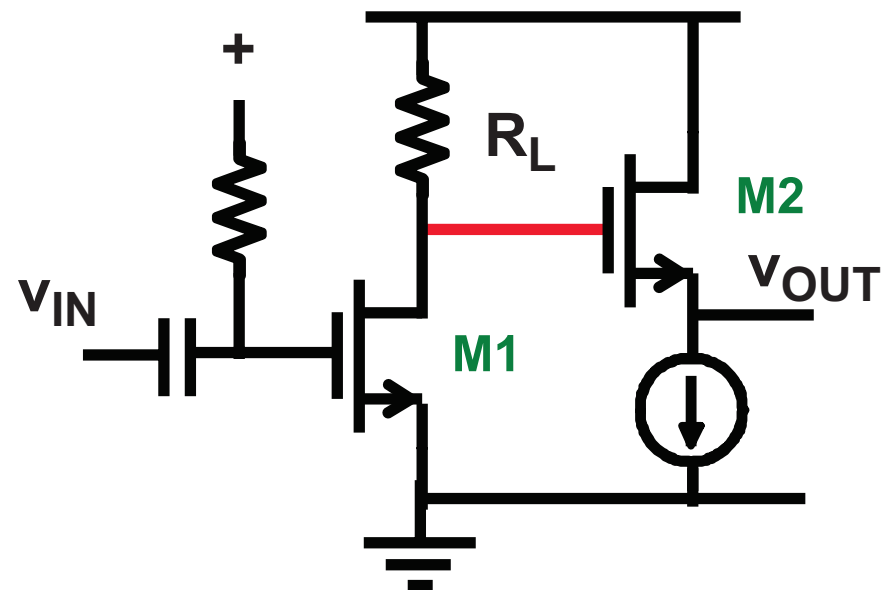
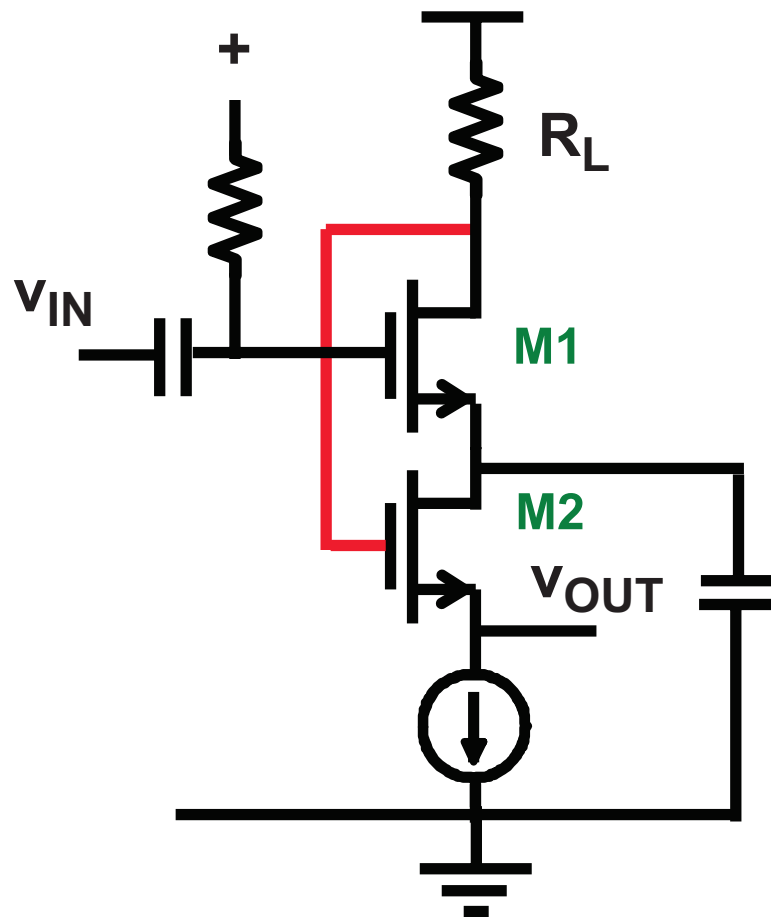
**P = 20 mW (2.7 V)**

Karanicolas, JSSC Dec 96, 1939-1944

---

## LNA with reuse

---

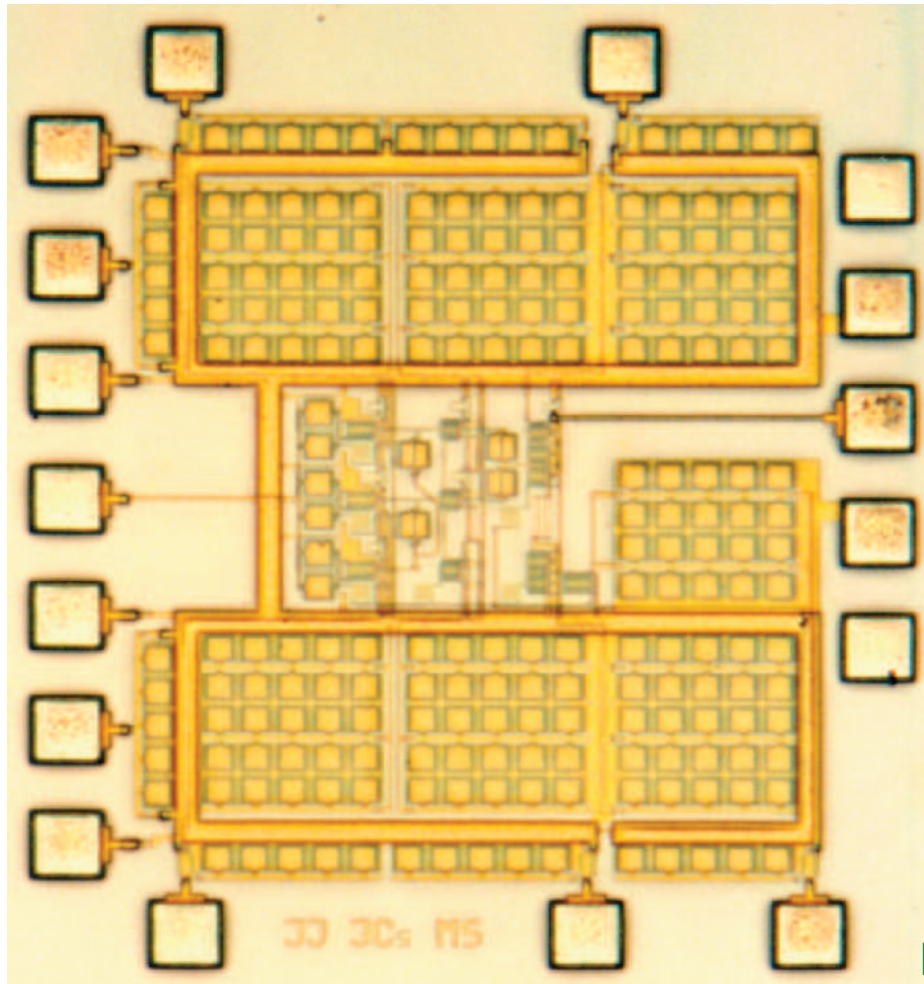




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## CMOS LNA with reuse

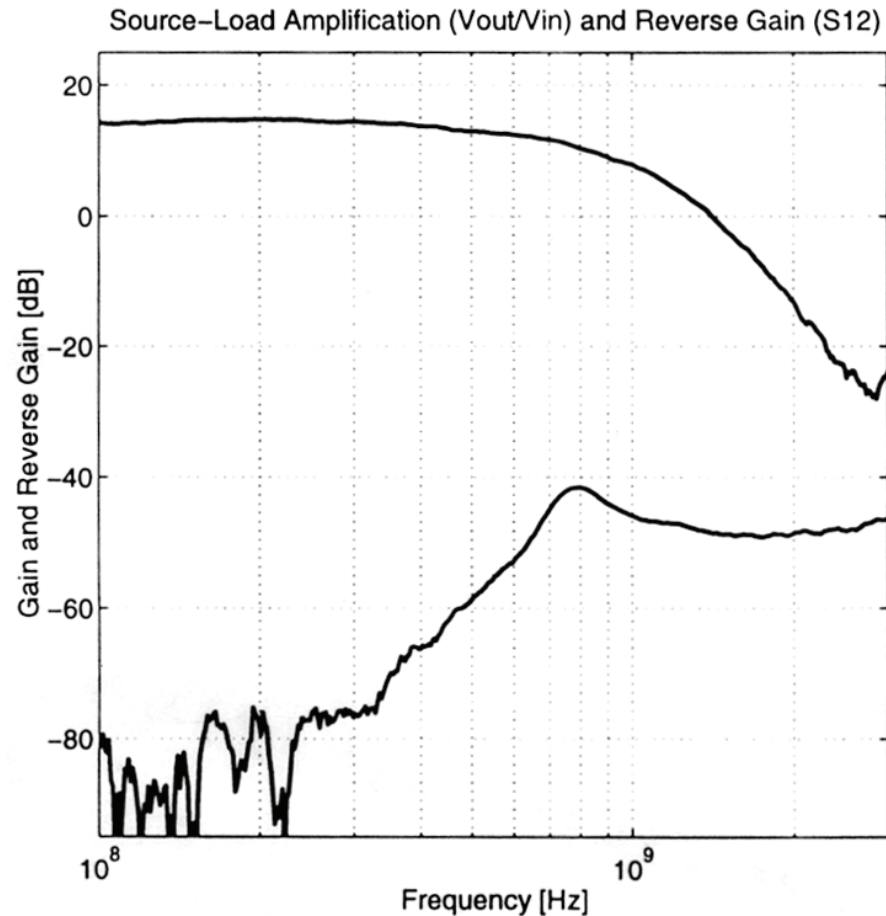
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<b>Fin</b>	<b>900 MHz</b>
<b>Power</b>	<b>10 mW</b>
<b>NF</b>	<b>2.3-3.3 dB</b>
<b>Gain</b>	<b>14.8 dB</b>
<b>IIP3</b>	<b>-4.7 VdBm</b>
<b>S11</b>	<b>-7 dB</b>
<b>Area</b>	<b>0.12 mm<sup>2</sup></b>

Ref. Janssens, M. Steyaert, CICC'98

# Measurements - 1



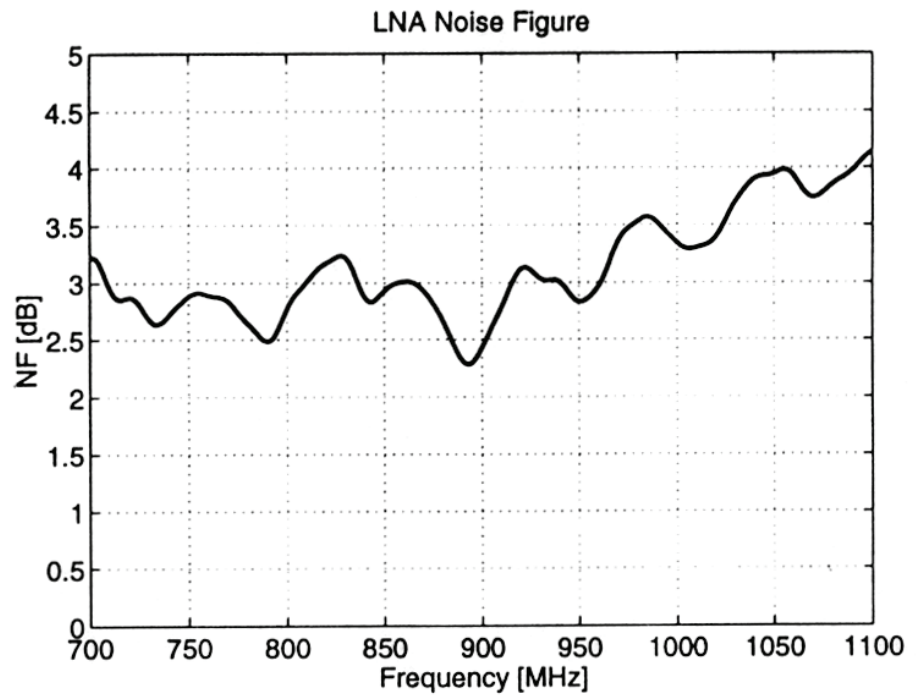
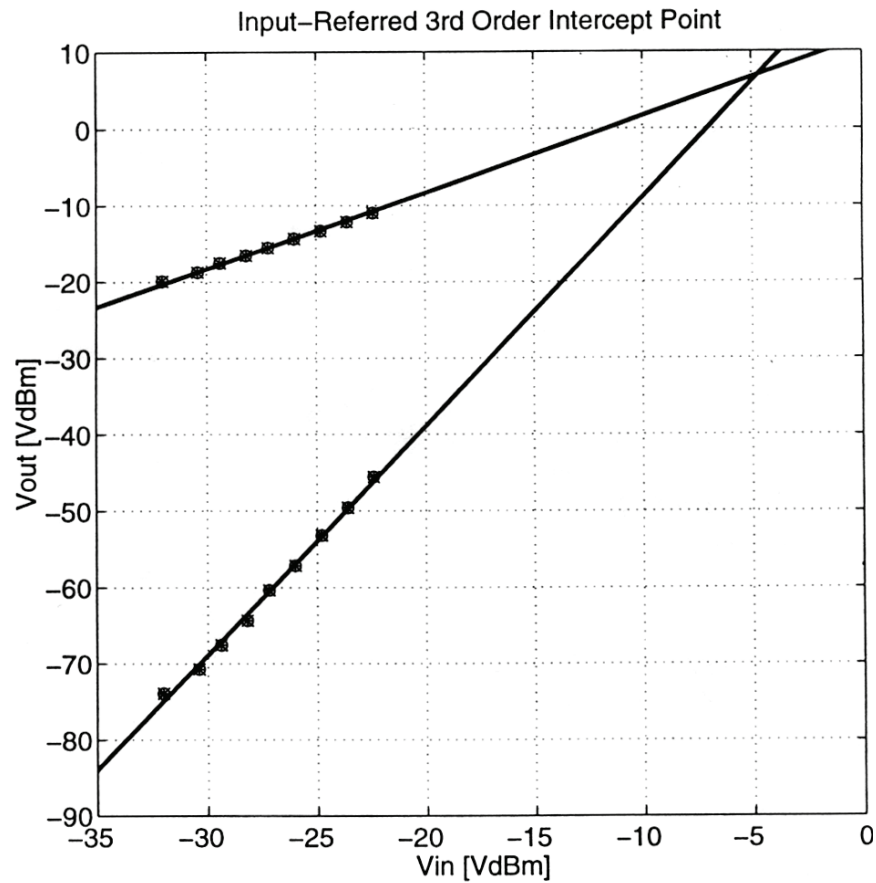
## Forward & Reverse gain

Parameter	Value
Supply voltage	3.0 Volt
Power dissipation	10 mW
-3dB band	50 - 700 MHz
Noise figure	2.3 - 3.3 dB
In-band gain	14.8 dB
Gain at 900 MHz	9 dB
Reverse isolation	> 41 dB
Input IP3	-4.7 VdBm
Die area	1.0 x 1.2 mm <sup>2</sup>

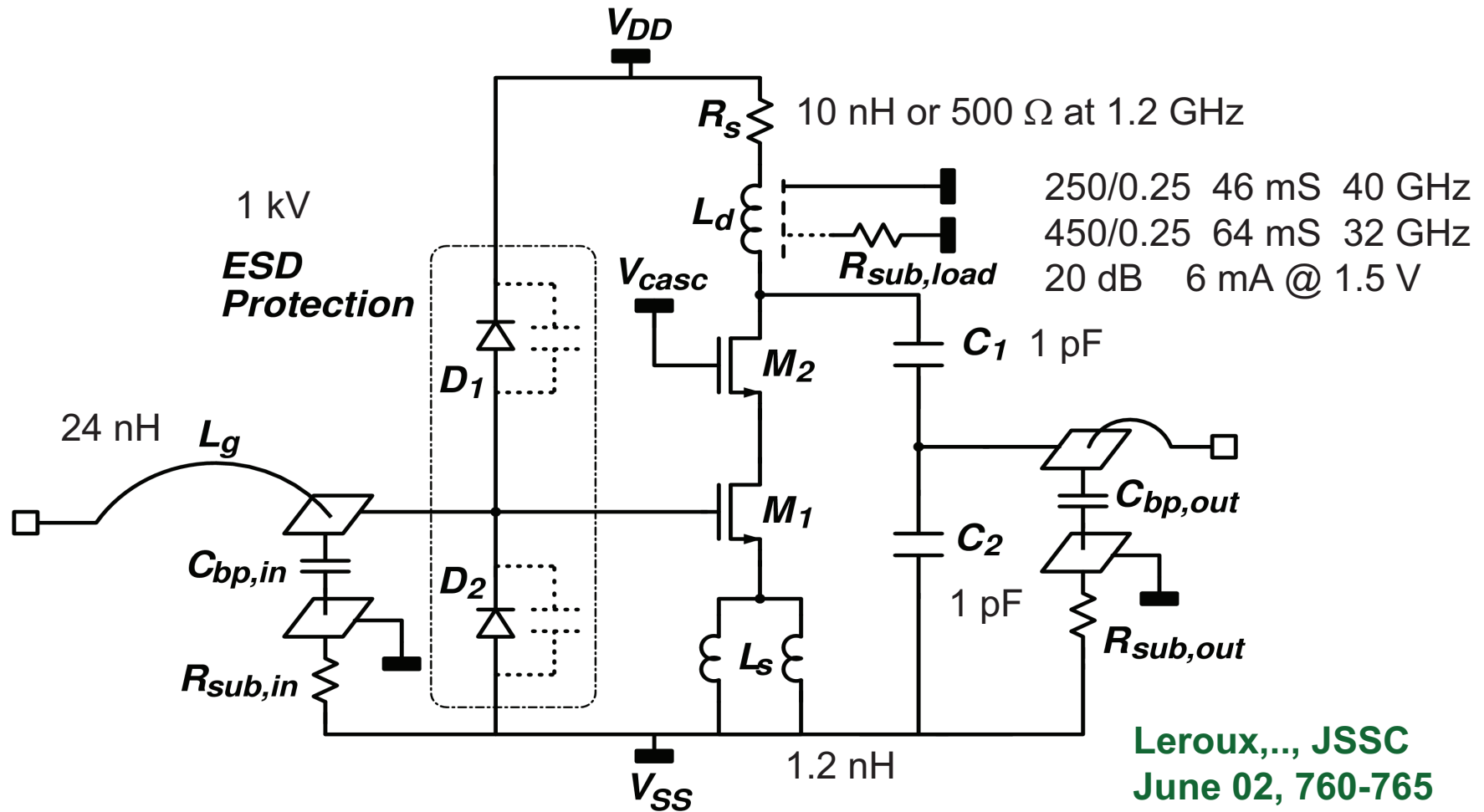
---

# Measurements - 2

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# 1.2 GHz LNA with C-ESD protection

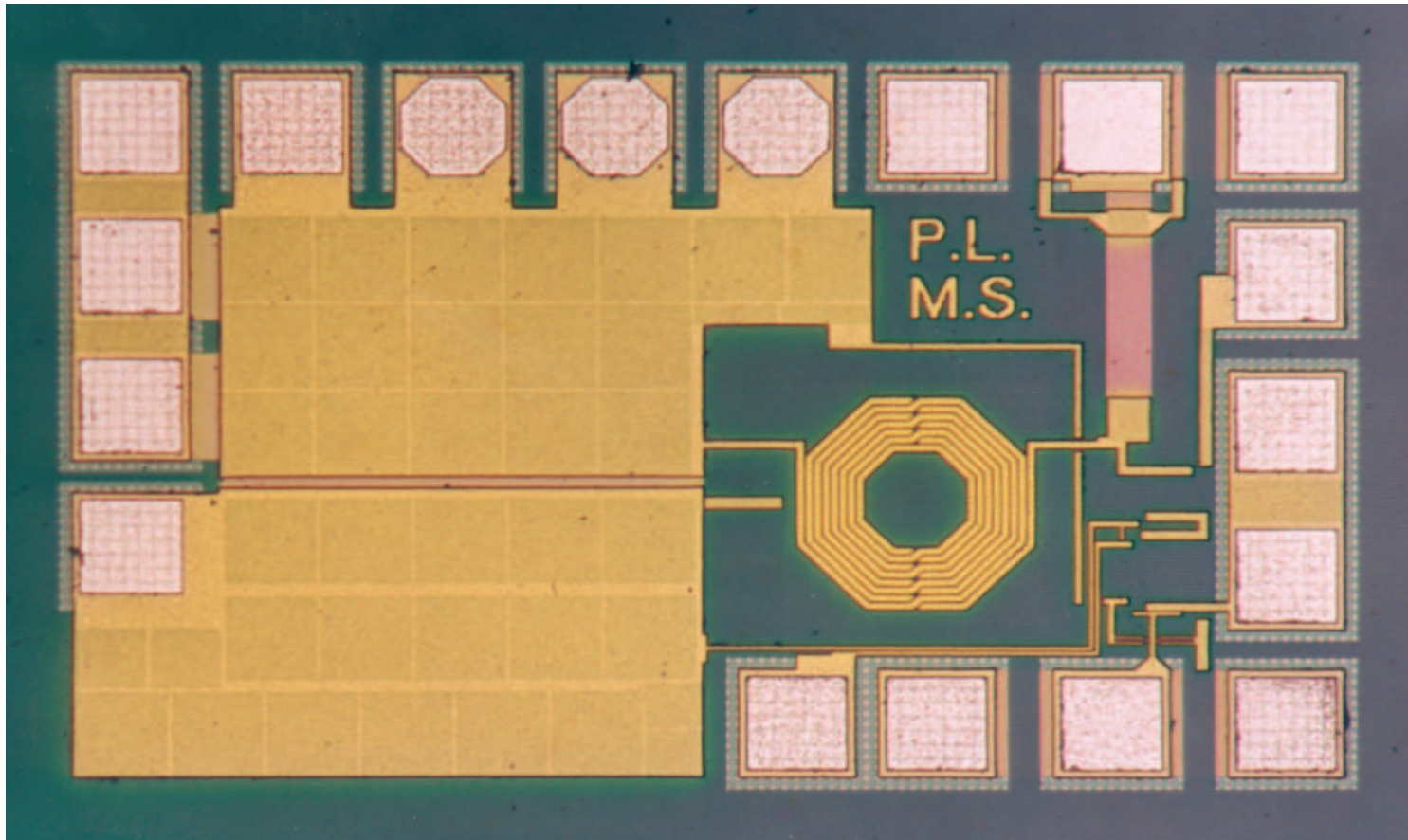




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# LNA Micrograph

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Leroux,..., JSSC June 02, 760-765

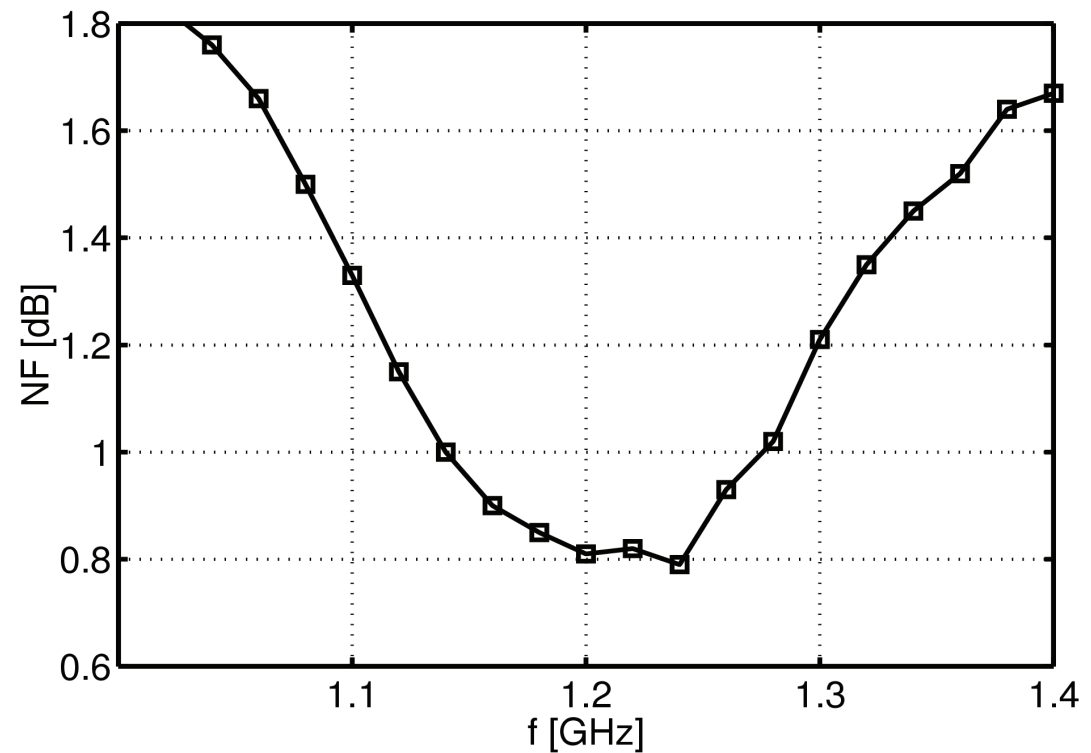


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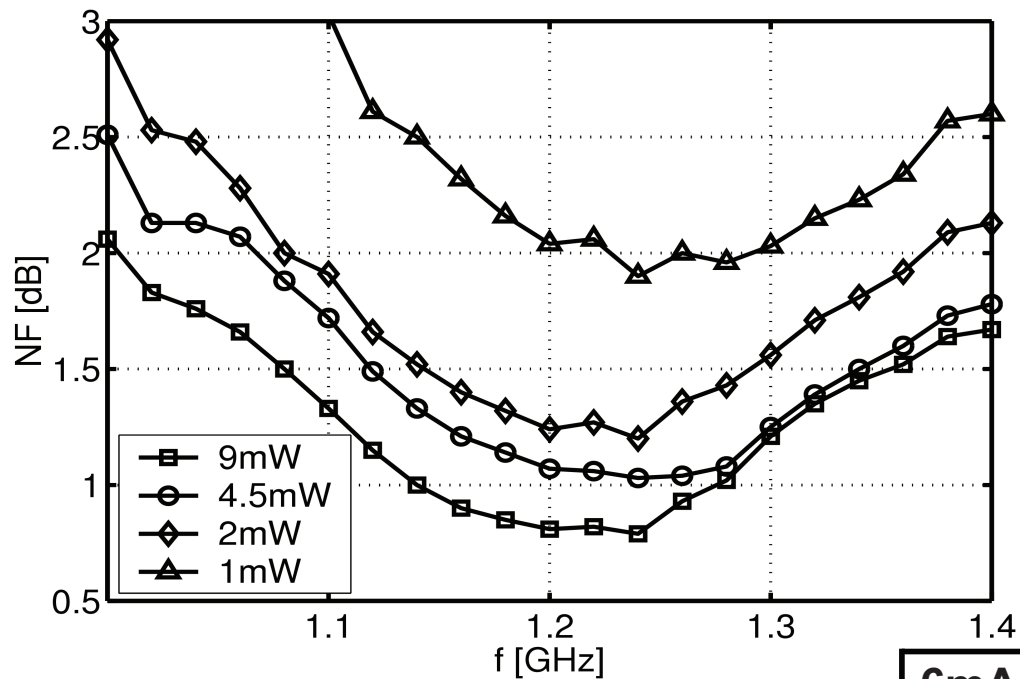
# Noise Figure

---

- Min. NF = 0.8 dB
- BW (NF<1dB) = 130 MHz



# Noise Figure



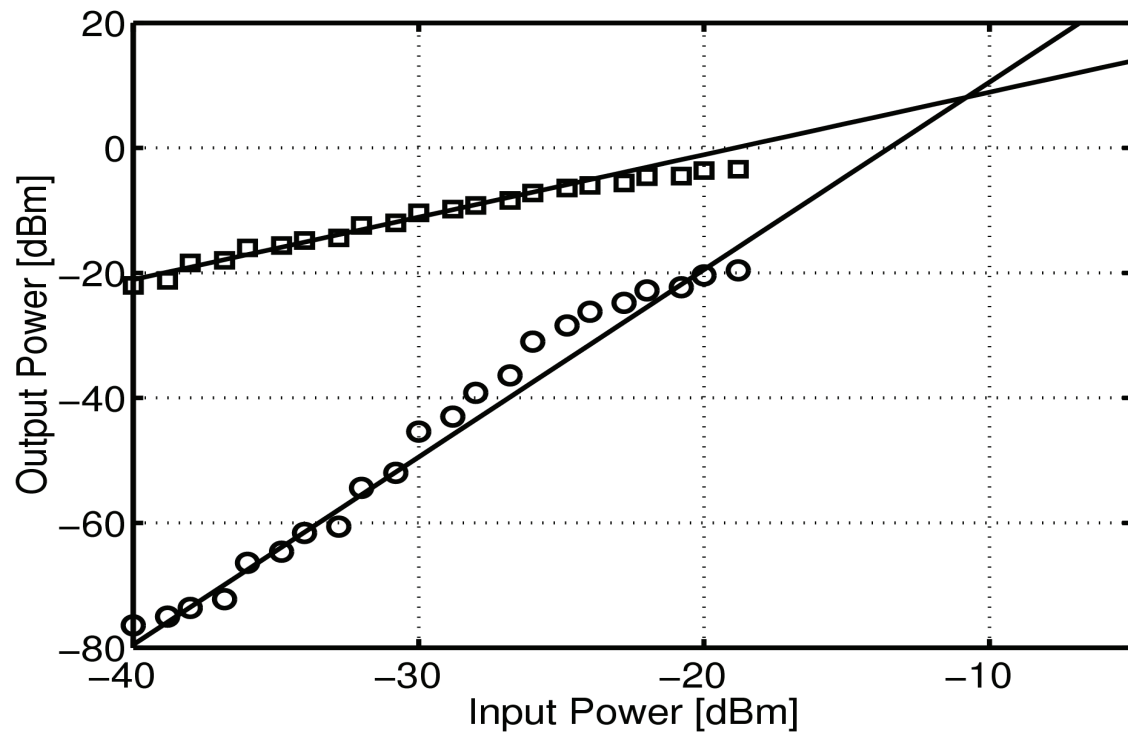
	NF @ min
6mA @ 1.5V	0.8dB
3mA @ 1.5V	1 dB
2mA @ 1V	1.2dB
1mA @ 1V	1.9dB

---

# Linearity performance

---

- Input IP3 = -10.8 dBm
- Input 1dBCp = -24 dBm



---

## Performance summary

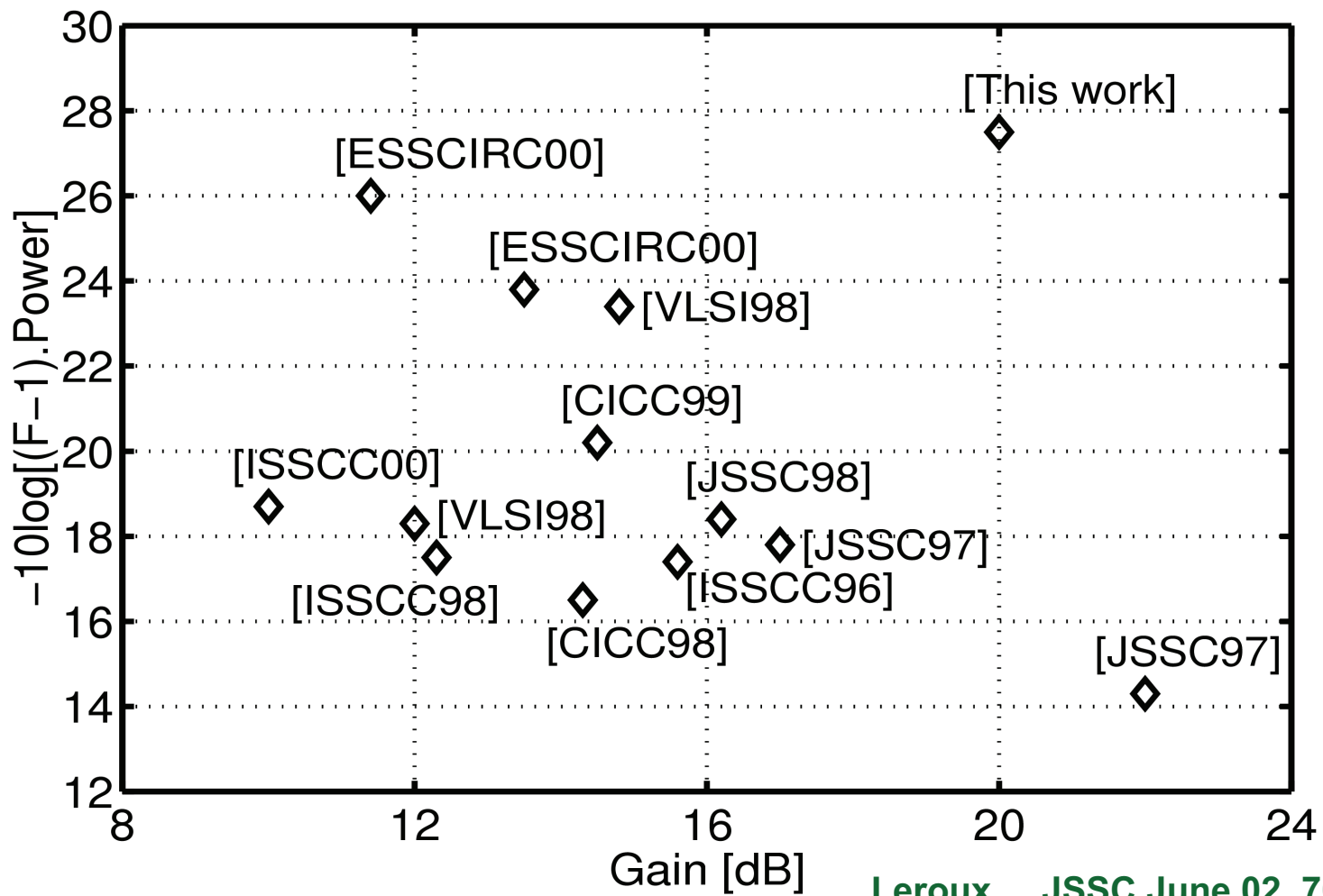
---

<i><b>Parameter</b></i>	<i><b>Specification</b></i>	<i><b>Measurement</b></i>
<b>Supply voltage</b>	<b>1.5 Volt</b>	<b>1.5 Volt</b>
<b>Power dissipation</b>	<b>10 mW</b>	<b>9 mW</b>
<b>Noise figure</b>	<b>1 dB</b>	<b>0.79 dB</b>
<b>Power gain @ 1.23 GHz</b>	<b>Max.</b>	<b>20 dB</b>
<b>S11 at 1.23 GHz</b>	<b>-10 dB</b>	<b>-11 dB</b>
<b>S22 at 1.23 GHz</b>	<b>-10 dB</b>	<b>-11 dB</b>
<b>Reverse isolation</b>	<b>30 dB</b>	<b>31 dB</b>
<b>Input IP3</b>	<b>-20 dBm</b>	<b>-10.8 dBm</b>
<b>HBM ESD-protection</b>	<b>0.5 kV</b>	<b>0.6 kV / -1.4 kV</b>
<b>Die area</b>	<b>-</b>	<b>0.6 x 1.1 mm<sup>2</sup></b>

---

# Performance comparison

---

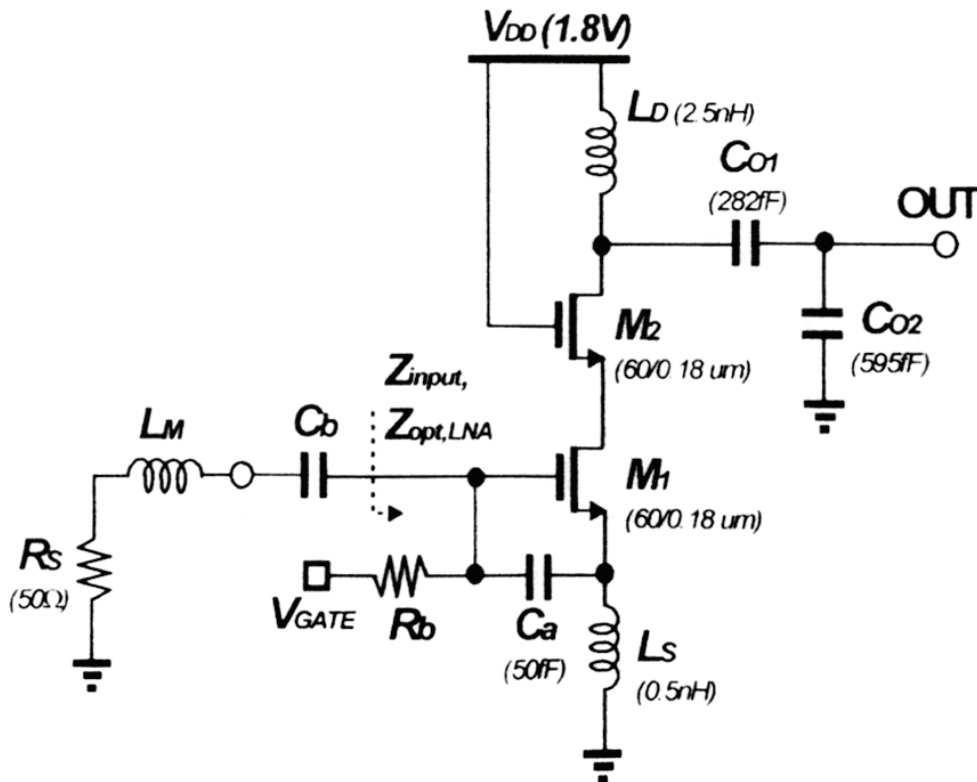


Leroux,..., JSSC June 02, 760-765

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## 5.2 GHz LNA

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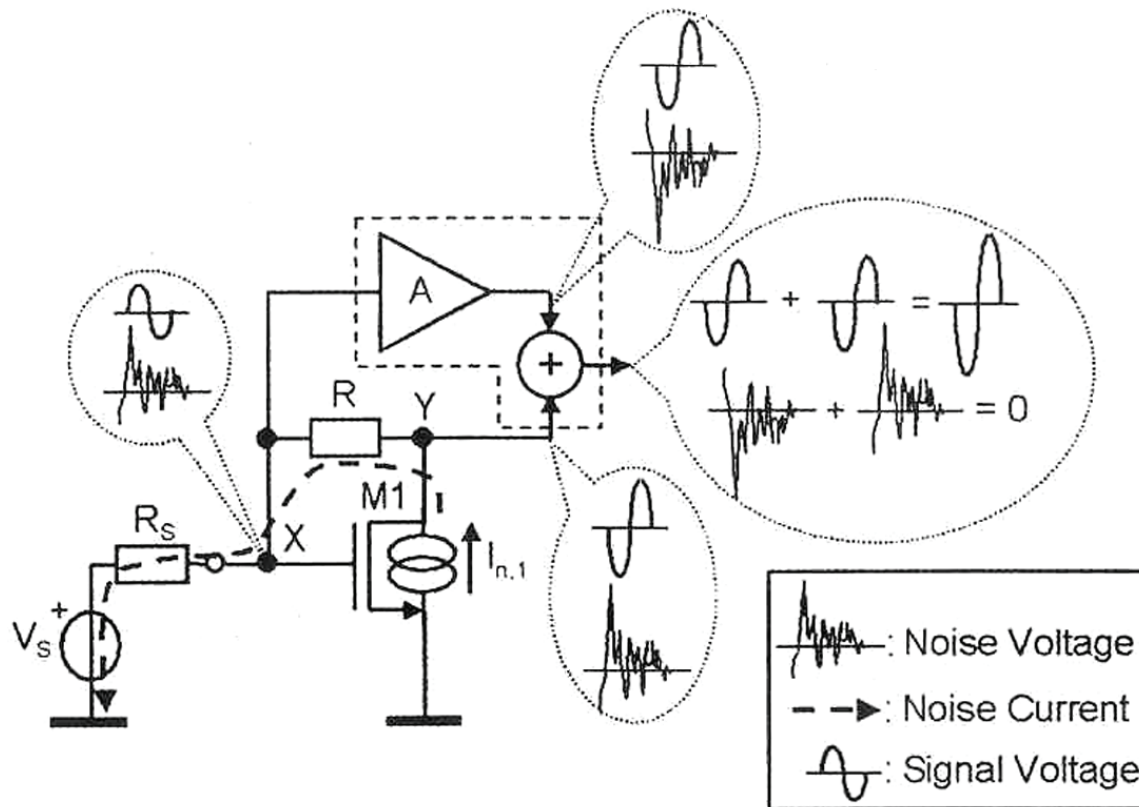


**5.2 GHz**  
**Gain 16 dB**  
**NF 1.1 dB**

**1.8 V**  
**12.4 mW**

Han,..., JSSC March 05, 726-735

# Noise-cancellation principle



$$v_X = \frac{R_S I_{n,1}}{1 + g_{m1} R_S}$$

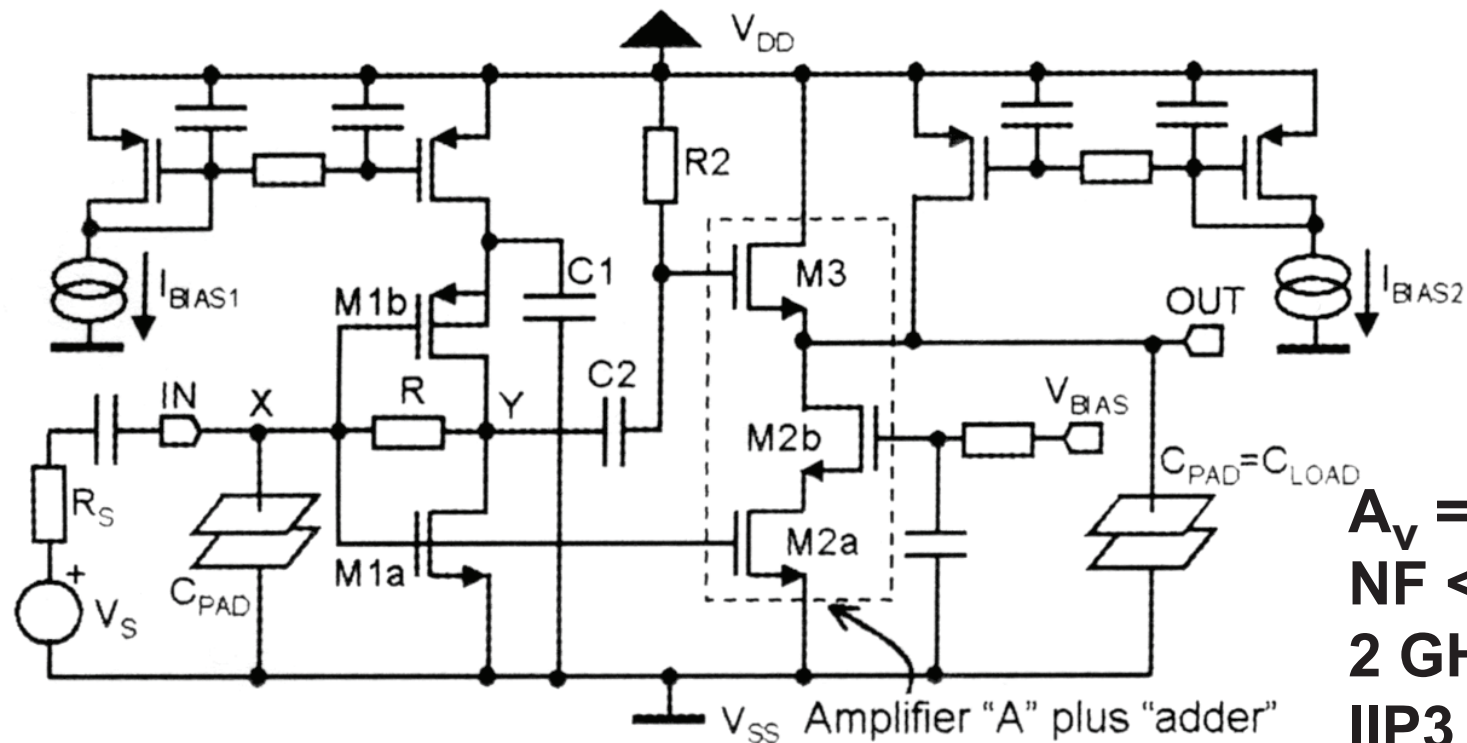
$$v_Y = \frac{(R + R_S) I_{n,1}}{1 + g_{m1} R_S}$$

$$v_{OUT} = Av_X + v_Y$$

**cancels the noise**

Bruccoli, ..., JSSC Febr.04, 275-282

# Noise-cancelling LNA



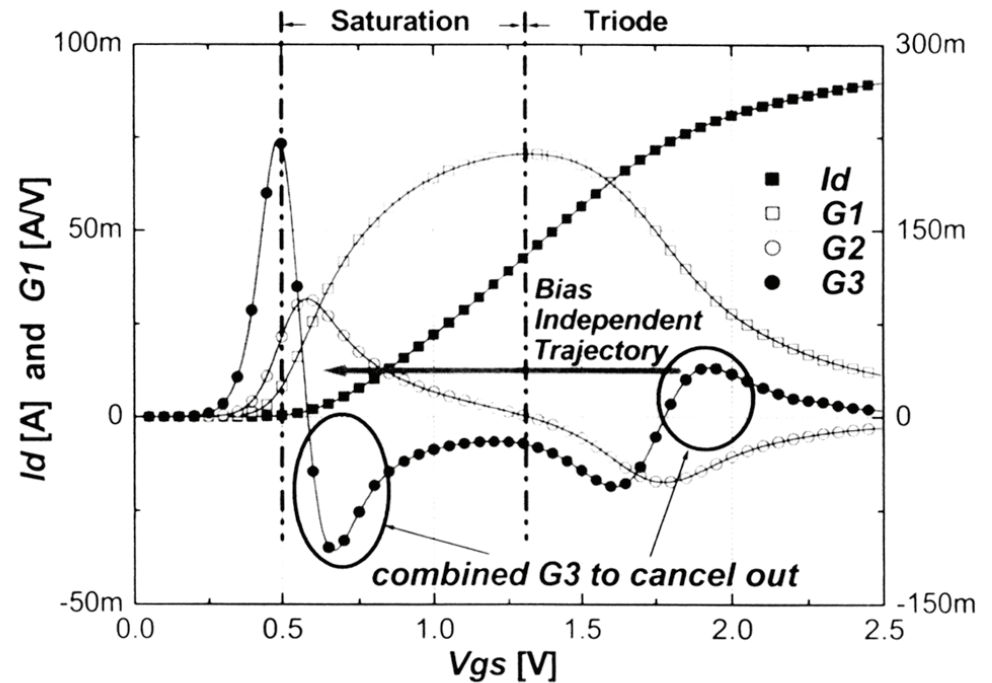
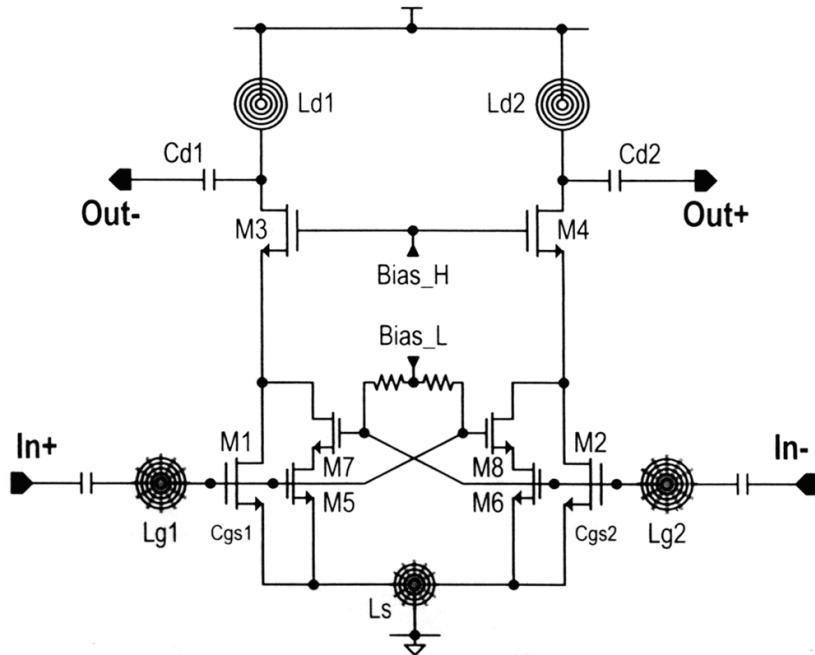
$A_v = 14$  dB  
 $NF < 2.4$  dB  
 $2$  GHz  
 $IIP3$   $0$  dBm  
 $14$  mA  $2.5$  V

Noise cancelling condition :  $\frac{g_{m2}}{g_{m3}} = \frac{R + R_S}{R_S}$

Bruccoleri, Nauta,  
 JSSC Febr.04,  
 275-282



# Differential LNA in 0.25 $\mu\text{m}$ CMOS : 2.4 GHz

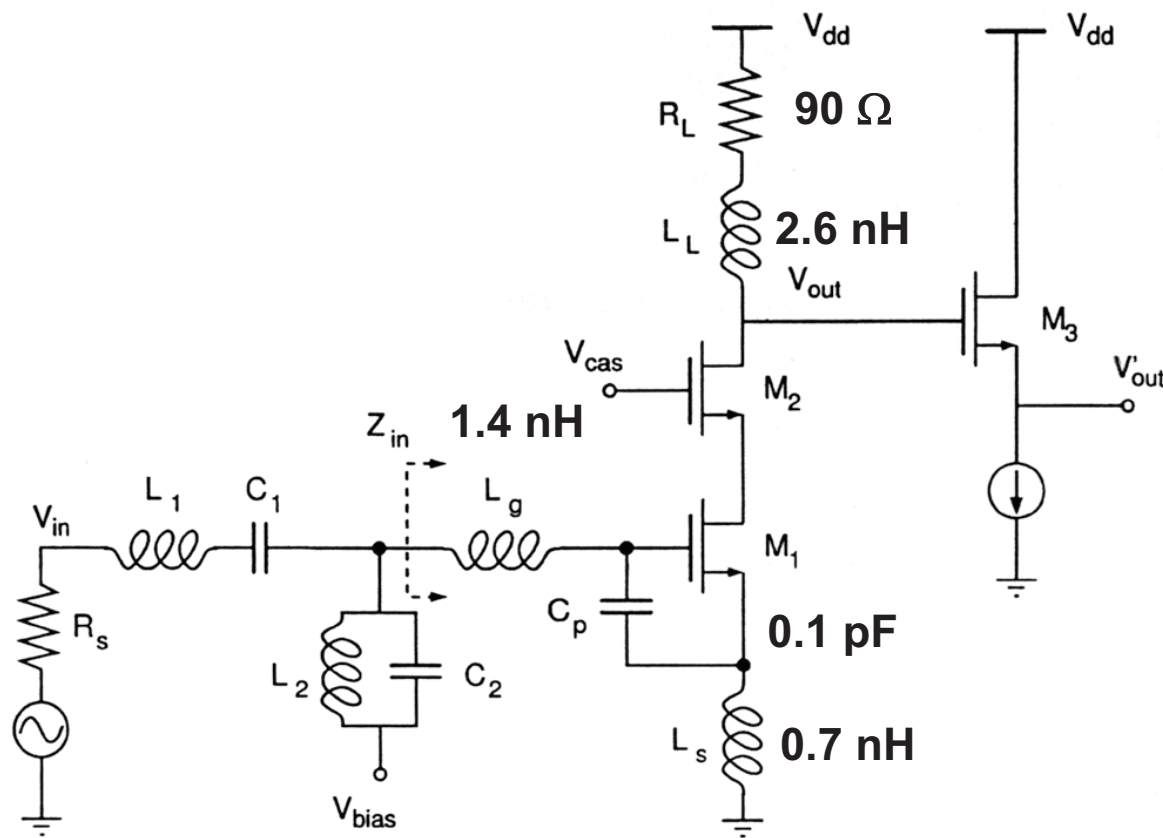


17 % More output power : 23.5 mW or +16 dBm

For same  $P_{-1\text{dB}} = -5$  dBm

Youn,..., ISSCC 03, 406-407

# LNA for UWB (3 - 10 GHz)



$$A_v = 9.3 \text{ dB}$$

$$NF < 4 \text{ dB}$$

$$IIP3 = 6.7 \text{ dBm}$$

$$1.5 \text{ V } 5 \text{ mA}$$

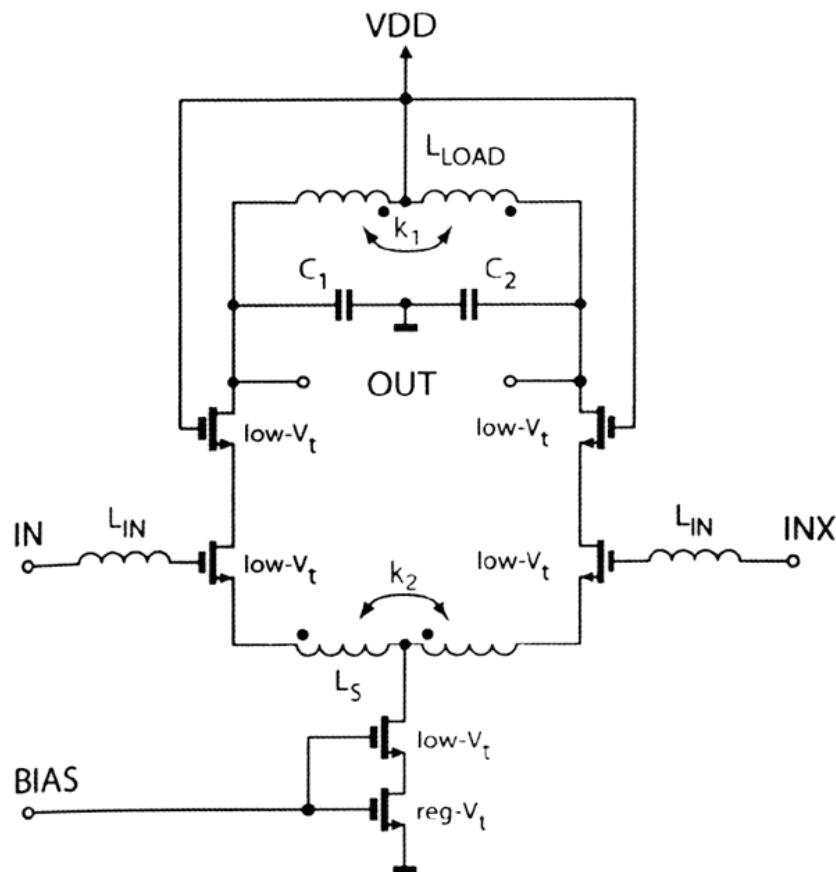
$$0.18 \mu\text{m CMOS}$$

Bevilacqua,..., JSSC Dec.01, 2259-2268

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# Differential LNA at 17 GHz

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**WLAN ISM 17 GHz**

**$A_v = 25.8$  dB**

**NF < 10 dB**

**IIP3 = -40 dBm**

**1.5 V**

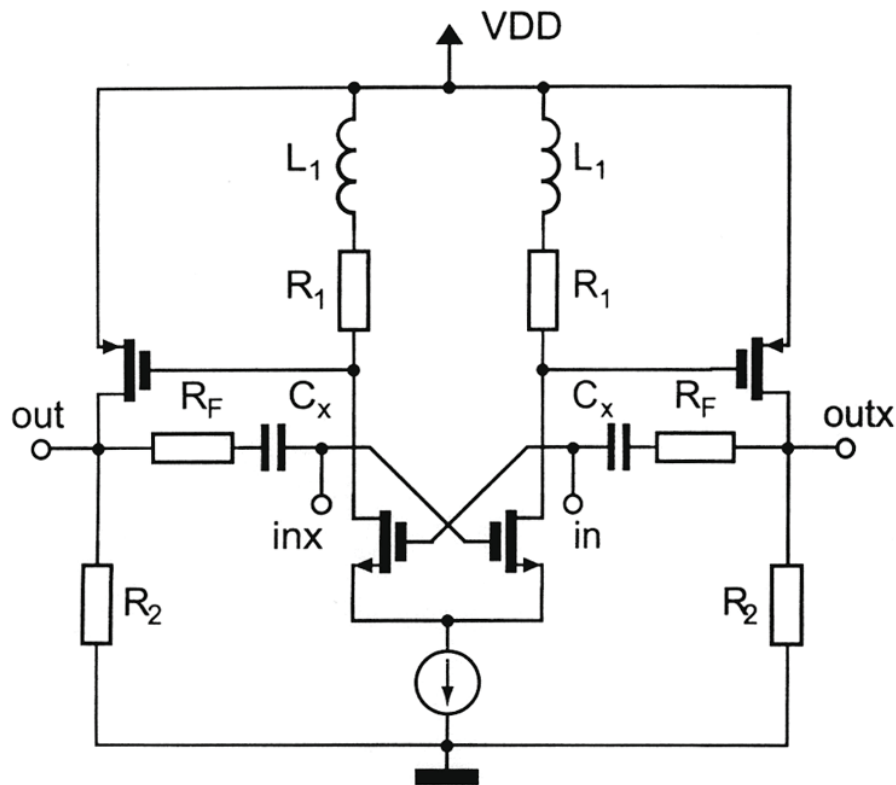
**0.13  $\mu$ m CMOS**

Kienmayer,..., ESSCIRC 2005, 133-136

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# Differential LNA at 5 GHz

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**UWB 3 - 5 GHz**  
 **$A_v = 25.8$  dB**  
**NF < 3.6 dB**  
**IIP3 = -22.7 dBm**  
**1.5 V 45 mW**  
**HBM ESD 1.5 kV**

Salerno,..., ESSCIRC 2005, 219-222

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- **Noise Figure and Impedance Matching**
- **LNA specifications and linearity**
- **Input amplifier or cascode**
- **Non-quasi-static MOST model**
- **More realizations**
- **Inductive ESD protection**

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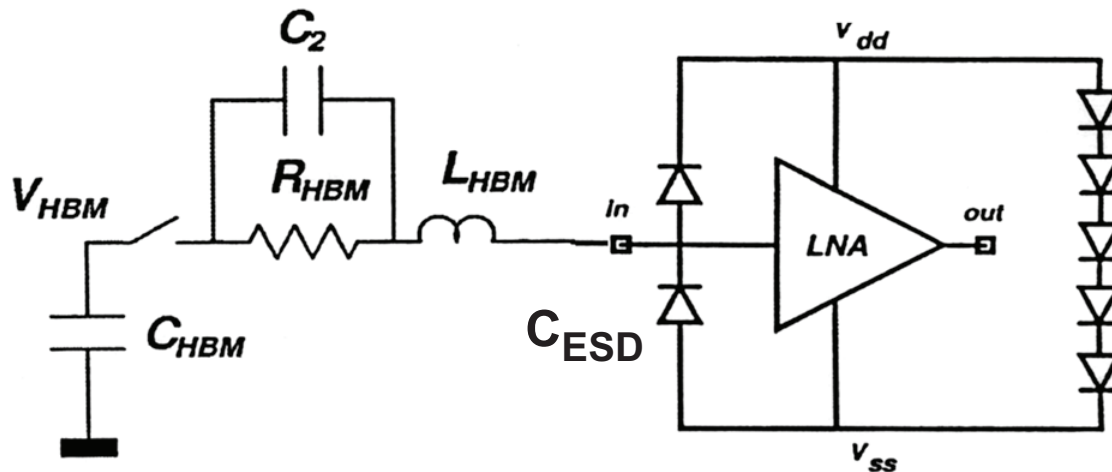
## ESD protection : Human Body model

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- CMOS requires ESD protection
- Protection network deteriorates RF performance
- Standards for testing : Human Body Model

Transmission Line Pulse ...

- Human Body Model :



$$C_{HBM} = 100 \text{ pF}$$

$$R_{HBM} = 1.5 \text{ k}\Omega$$

$$V_{HBM} =$$

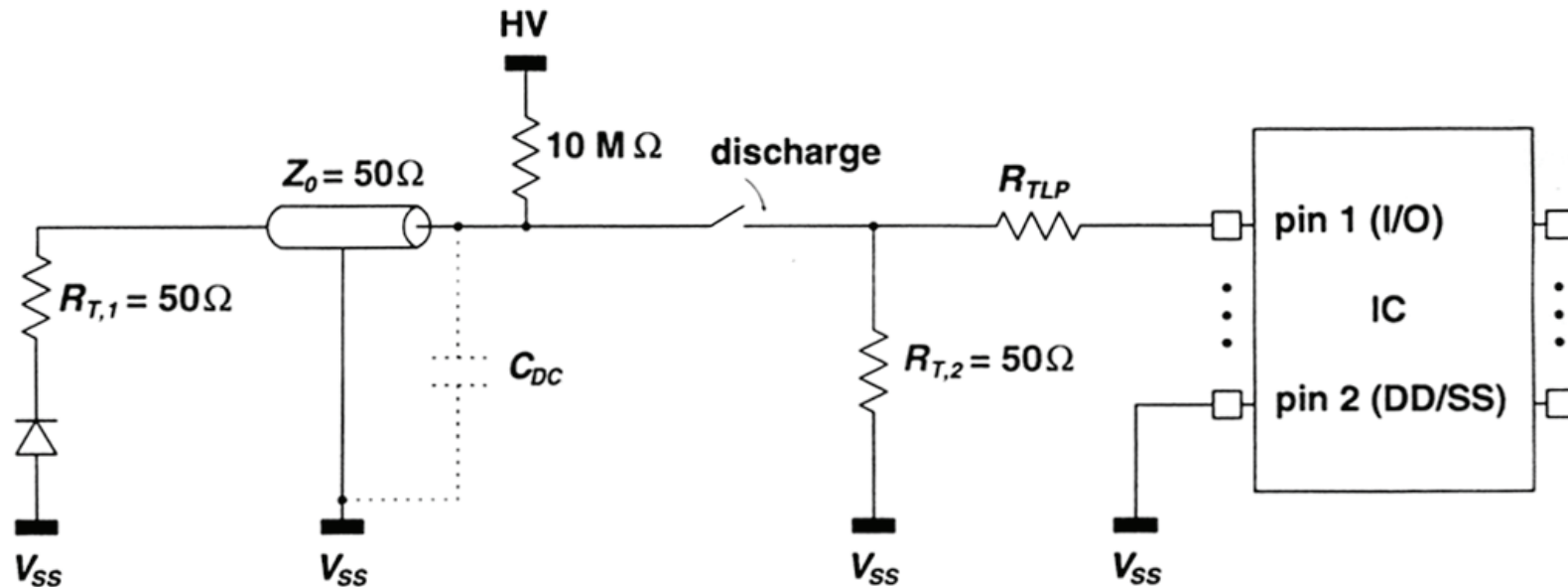
$$I_{\max} = 0.67 \text{ A / kV}$$

Required 2 kV !!

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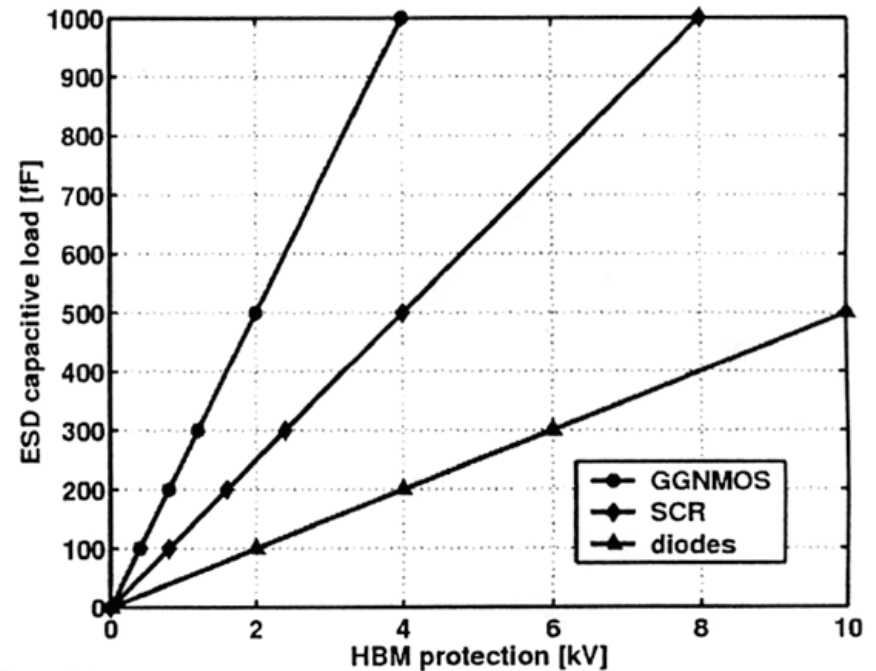
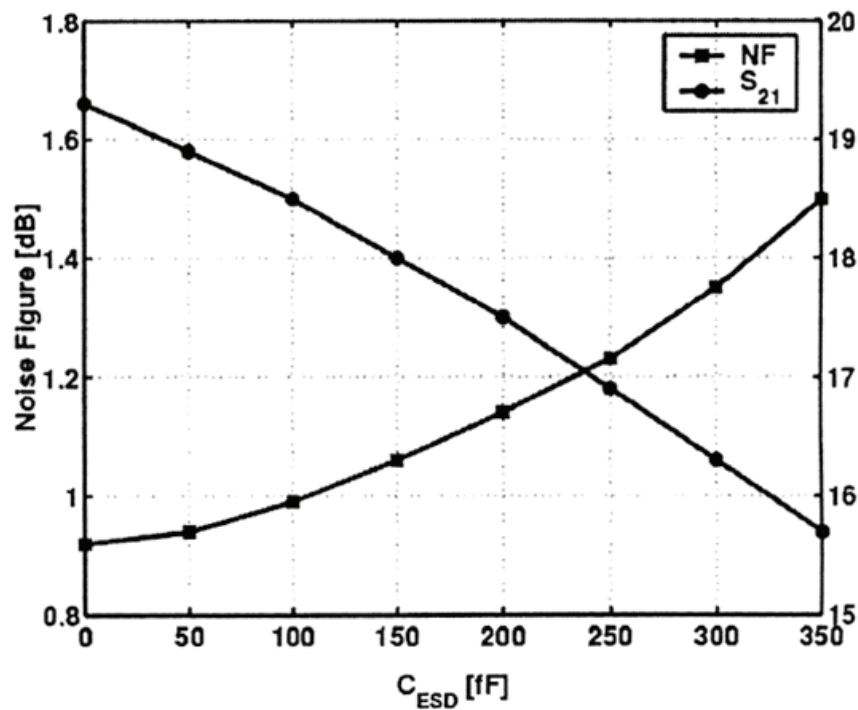
# ESD protection : Transmission Line Pulse

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HV : High Voltage : kV's

# Simulated deterioration by ESD diodes

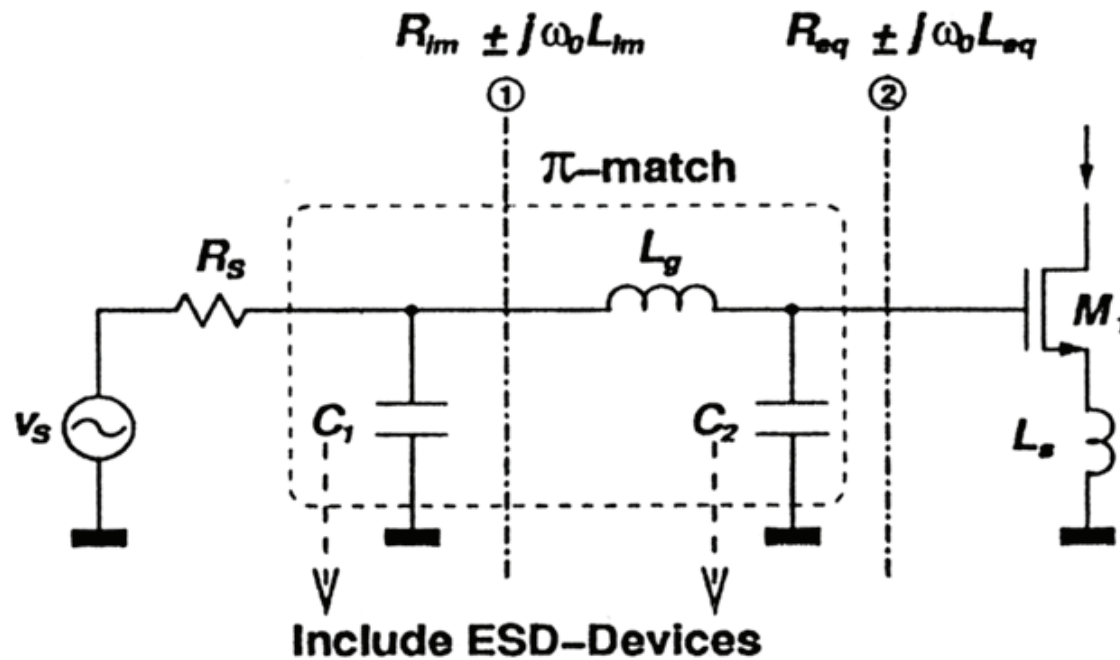




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# $\Pi$ -network with Capacitive ESD protection

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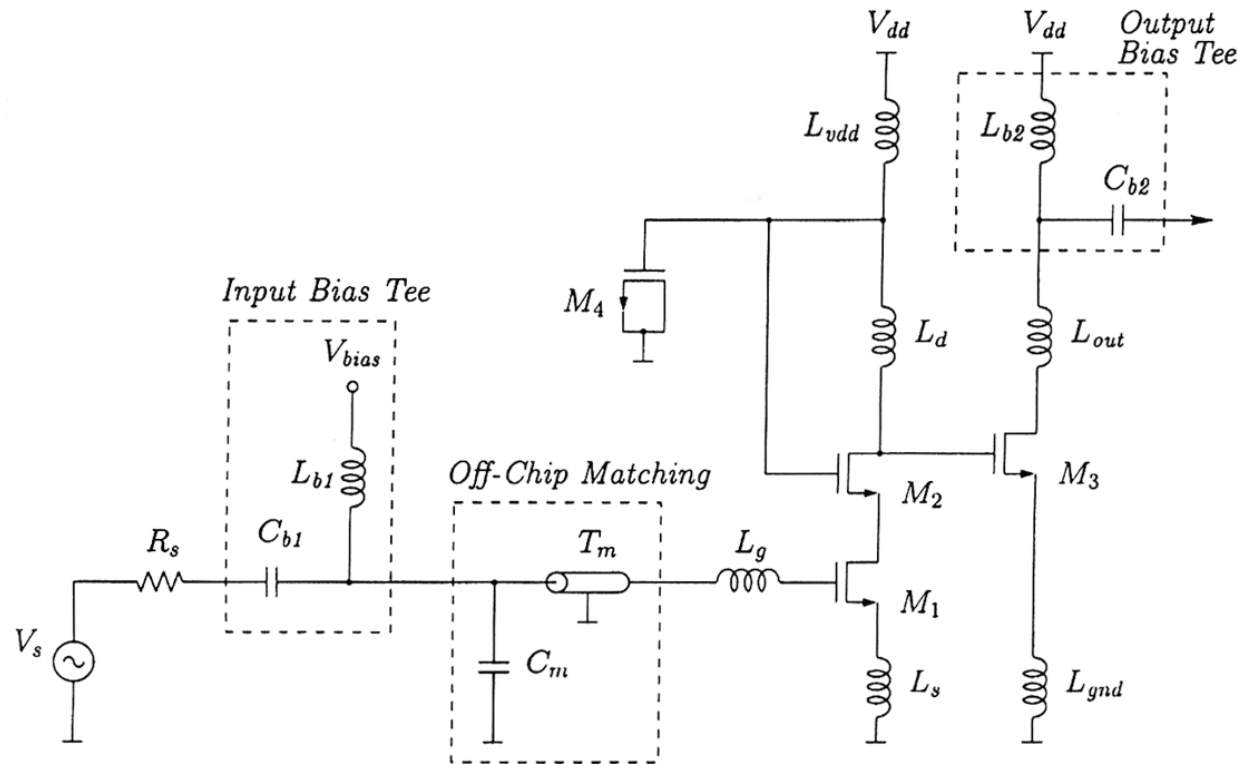
Requires on-chip inductor !

Leroux,.., Kluwer 2005

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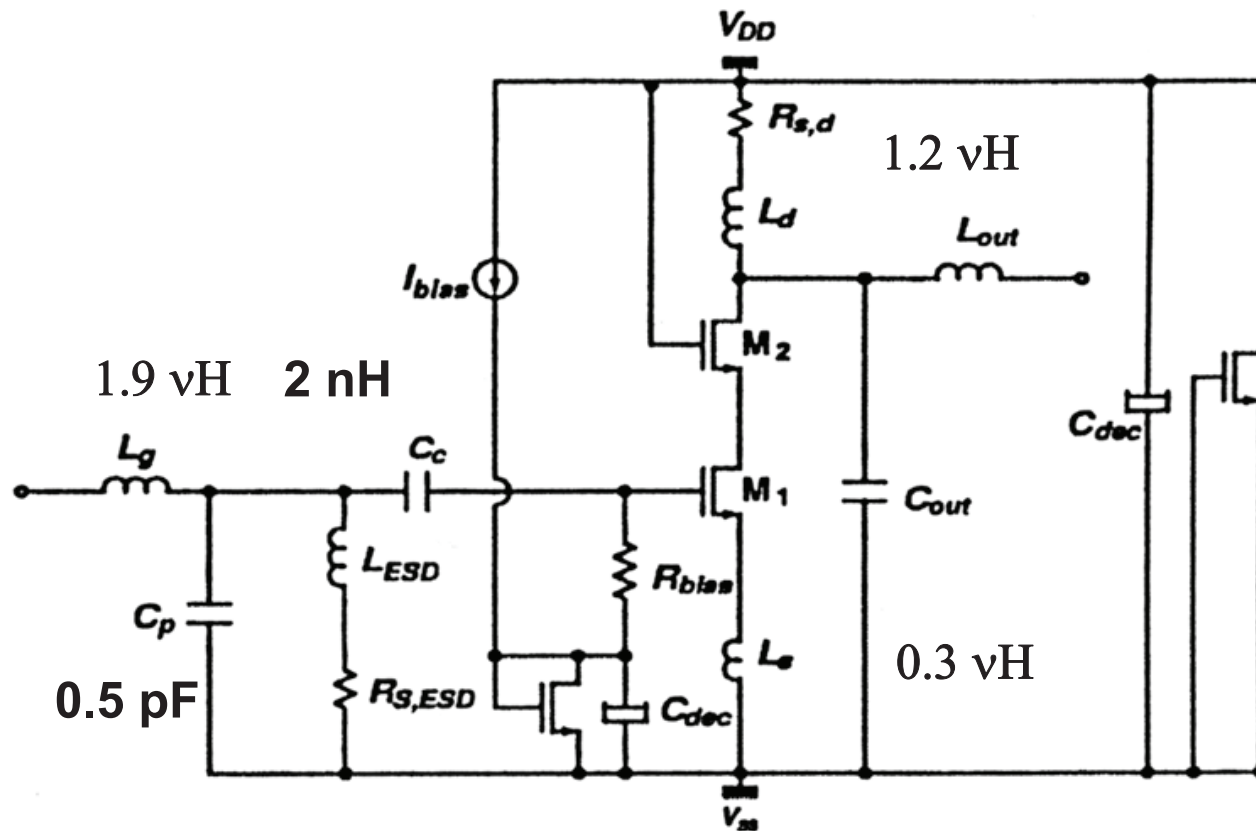
# 1.5 V 1.5 GHz LNA

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Schaeffer,.. JSSC May 97, 745-759

# LNA with L-ESD protection for 5 GHz LNA



5 GHz  
24 MHz  
NF < 10 dB  
IIP3 > -10dBm

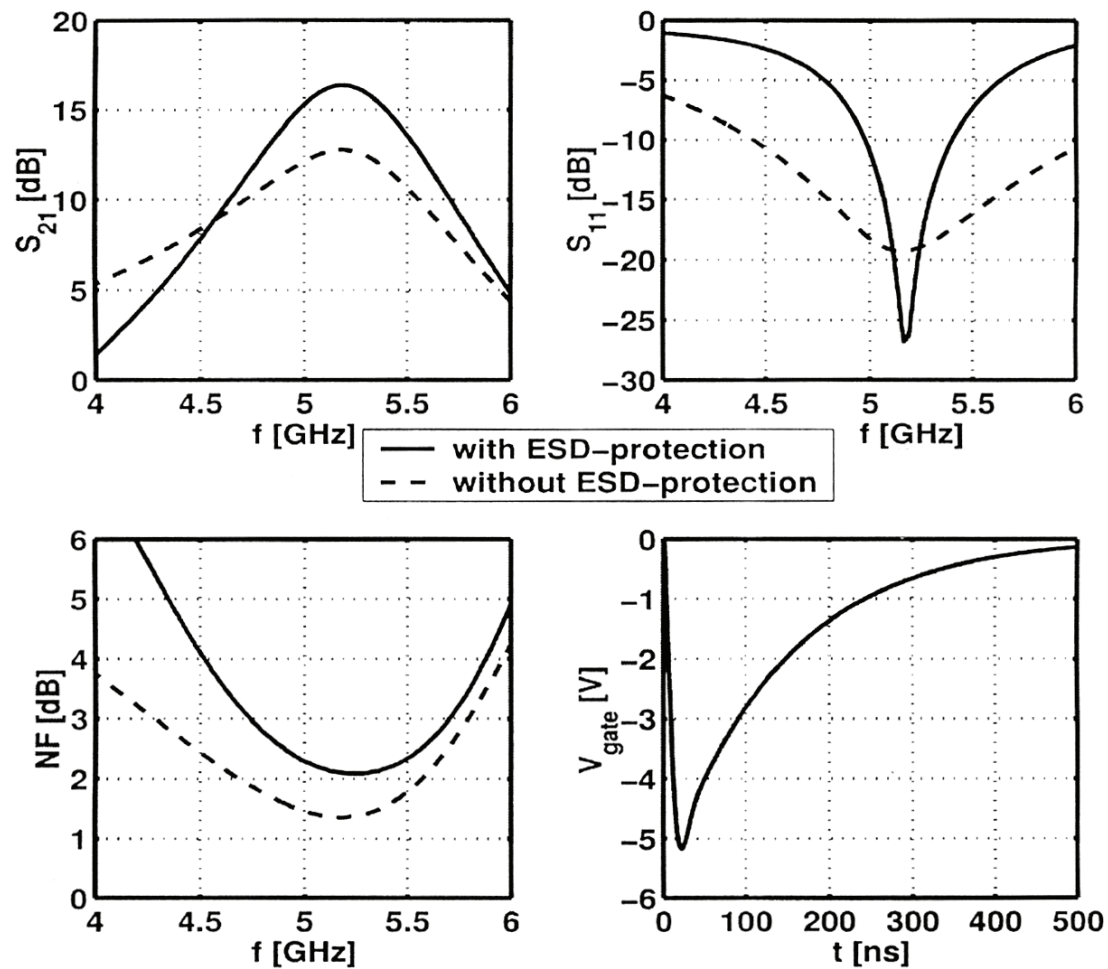
0.18  $\mu$ m CMOS  
8 mA/1.5 V  
3 kV ESD-prot.

Leroux,..., AACD 2003, 207-225

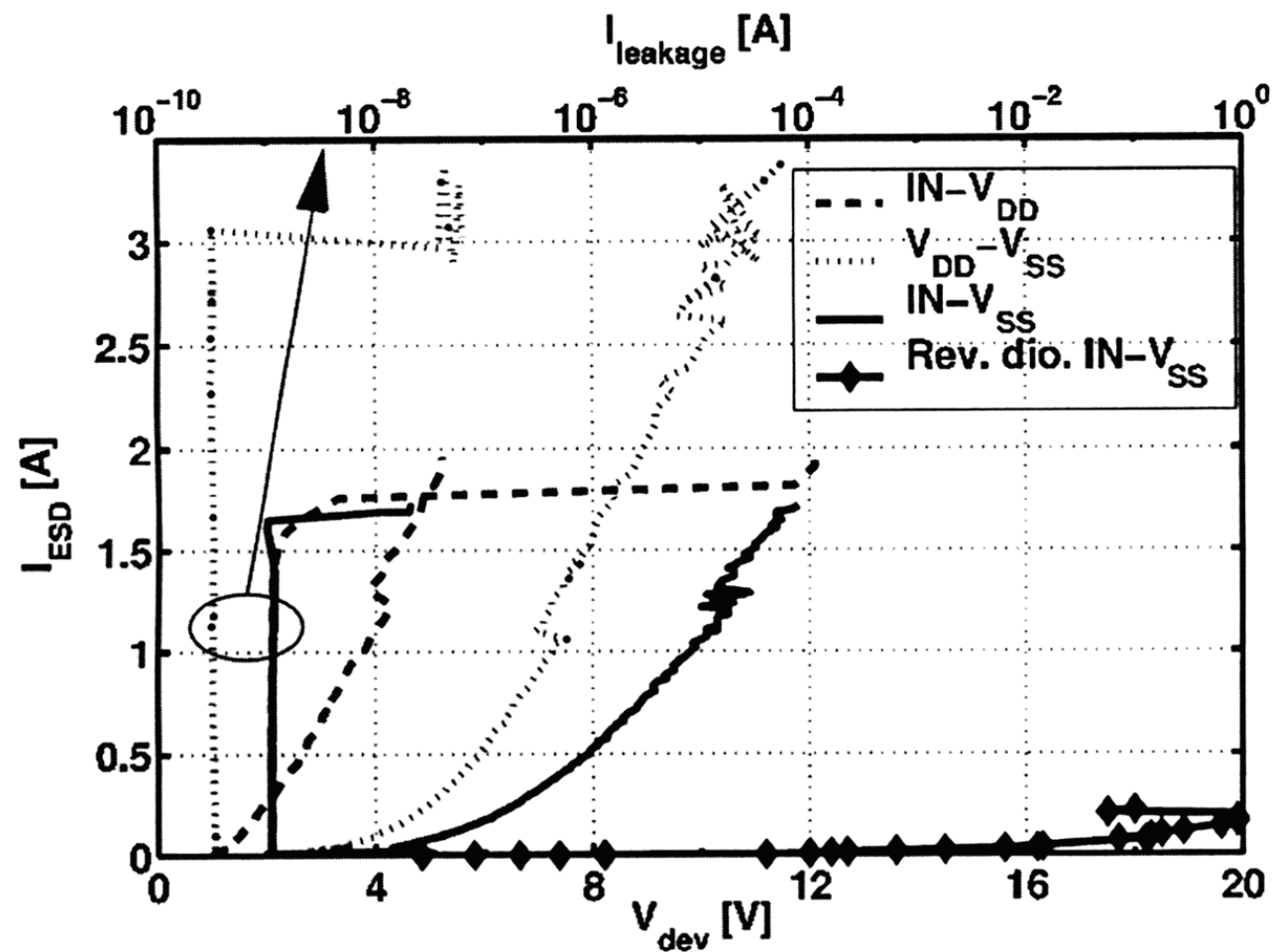
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# Effect of ESD on performance

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# TLP Characteristics



Transmission  
Line Pulse

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