



This report is part of Dynamics of Non linear Robotic Systems [DNIRS] course for first year master students at Innopolis University. In this report you can find the full Derivation of the dynamic model for Mitsubishi robot RV-1A while the implementation is available on [GitHub](#).

# 1 Introduction

Derivation of the dynamic model of a manipulator plays an important role for simulation of motion, analysis of manipulator structures, and design of control algorithms. In this report we will use Euler-lagrange method in order to derive the dynamic model of the mitsubishi robot RV-1A. As it is shown in (Figure 1) we have a 6 DOF arm manipulator. I am assuming all

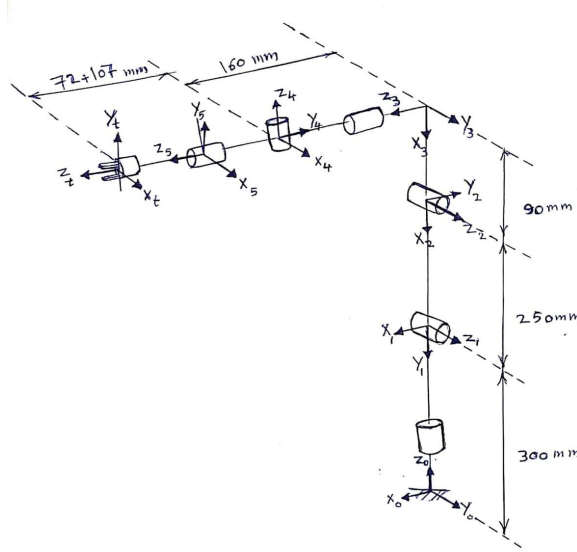


Figure 1: Mitsubishi robot RV-1A scheme.

of masses ( $M_1, M_2, M_3, M_4, M_5, M_6$ ) exist at the end of links for simplicity. six actuators exist at each joint, and directly actuate the torques ( $u_1, u_2, u_3, u_4, u_5, u_6$ ). The manipulator kinematics is governed by six joint angles ( $q_1, q_2, q_3, q_4, q_5, q_6$ ).

# 2 Theoretical Background

The dynamic model of a manipulator provides a description of the relationship between the joint actuator torques and the motion of the structure. With lagrange formulation, the equations of motion can be derived in a systematic way independently of the reference coordinate frame. lagrangian of the mechanical system can be defined as a function of the generalized coordinates. The general dynamic equation is obtained by:

$$\frac{d}{dt} \left( \frac{\partial T}{\partial \dot{q}_j} \right) - \frac{\partial T}{\partial q_j} + \frac{\partial V}{\partial q_j} = P_j \quad (1)$$

Where,  $T$  is the total kinetic energy,  $V$  is the total potential energy of the system.  $P_j$  is the generalized force,  $t$  is time,  $q_j$  is the generalized coordinates and  $\dot{q}_j$  is the generalized velocity.

### 3 Dynamic model usg the Euler-lagrange approach

#### 3.1 Math Matrix $M(q)$ :

First of all, we need to determine the center of mass - which in our case in the end of each link - and write the equations of each link projected on each axes.

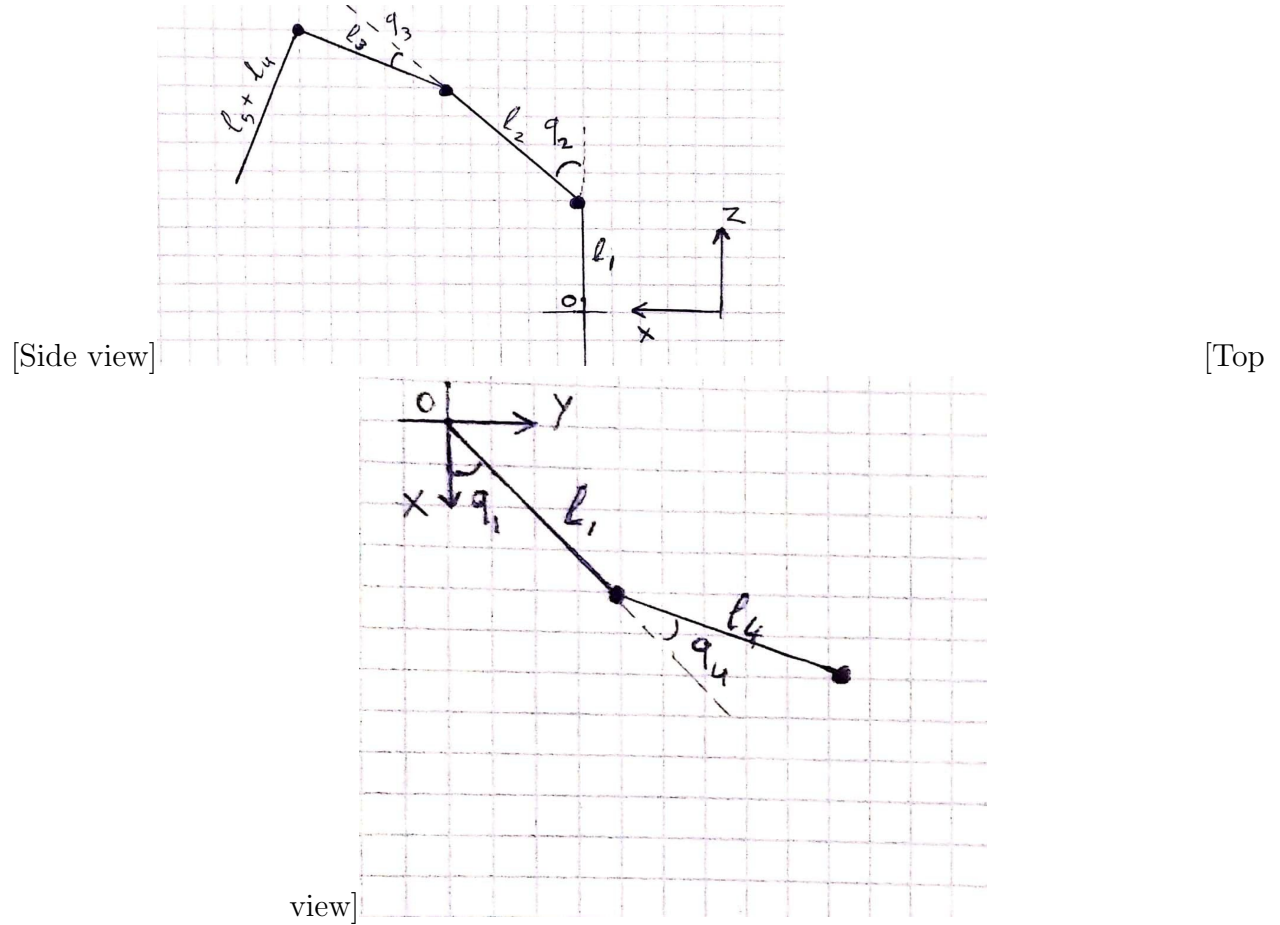


Figure 2: Mitsubishi robot RV-1A Top and Side views

$$\begin{aligned}
 x_1 &= l1.c1 \\
 x_2 &= l1.c1 + l2.c2 \\
 x_3 &= l1.c1 + l2.c2 + l3.c(q_2 + q_3) \\
 x_4 &= l1.c1 + l2.c2 + l3.c(q_2 + q_3) + l4.c(q_1 + q_4) \\
 x_5 &= l1.c1 + l2.c2 + l3.c(q_2 + q_3) + l4.c(q_1 + q_4) \\
 x_6 &= l1.c1 + l2.c2 + l3.c(q_2 + q_3) + l4.c(q_1 + q_4) + l6.c(q_1 + q_4 + q_6) \\
 y_1 &= l1.s1
 \end{aligned}$$

$$\begin{aligned}
y_2 &= l1.s1 \\
y_3 &= l1.s1 \\
y_4 &= l1.s1 + l4.s(q_1 + q_4) \\
y_5 &= l1.s1 + l4.s(q_1 + q_4) + l5.c5 \\
y_6 &= l1.s1 + l4.s(q_1 + q_4) + l5.c5 + l6.s(q_1 + q_4 + q_6)
\end{aligned}$$

$$\begin{aligned}
z_1 &= 0 \\
z_2 &= l2.s2 \\
z_3 &= l2.s2 + l3.c(q_2 + q_3) \\
z_4 &= l2.s2 + l3.c(q_2 + q_3) \\
z_5 &= l2.s2 + l3.c(q_2 + q_3) + l5.s5 \\
z_6 &= l2.s2 + l3.c(q_2 + q_3) + l5.s5
\end{aligned}$$

Now we have to compute translation and rotation jacobian matrices in order to compute  $M(q)$ .

let us compute the translation jacobians:

$$\mathbb{J}_v^i = \begin{bmatrix} \frac{\partial x_i}{\partial y_1} & \cdots & \frac{\partial x_i}{\partial y_6} \\ \frac{\partial y_i}{\partial y_1} & \cdots & \frac{\partial y_i}{\partial y_6} \\ \frac{\partial z_i}{\partial y_1} & \cdots & \frac{\partial z_i}{\partial y_6} \end{bmatrix} \quad (2)$$

$$\begin{aligned}
\mathbb{J}_v^1 &= \begin{bmatrix} -l1.s1 & 0 & 0 & 0 & 0 & 0 \\ l1.c1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix} \\
\mathbb{J}_v^2 &= \begin{bmatrix} -l1.s1 & -l2.s2 & 0 & 0 & 0 & 0 \\ l1.c1 & 0 & 0 & 0 & 0 & 0 \\ 0 & l2.c2 & 0 & 0 & 0 & 0 \end{bmatrix} \\
\mathbb{J}_v^3 &= \begin{bmatrix} -l1.s1 & -l3.s23 - l2.s2 & -l3.s23 & 0 & 0 & 0 \\ l1.c1 & 0 & 0 & 0 & 0 & 0 \\ 0 & l2.c2 - l3.s23 & -l3.s23 & 0 & 0 & 0 \end{bmatrix} \\
\mathbb{J}_v^4 &= \begin{bmatrix} -l4.s14 - l1.s1 & -l3.s23 - l2.s2 & -l3.s23 & -l4.s14 & 0 & 0 \\ l4.c14 + l1.c1 & 0 & 0 & l4.c14 & 0 & 0 \\ 0 & l2.c2 - l3.s23 & -l3.s23 & 0 & 0 & 0 \end{bmatrix} \\
\mathbb{J}_v^5 &= \begin{bmatrix} -l4.s14 - l1.s1 & -l3.s23 - l2.s2 & -l3.s23 & -l4.s14 & 0 & 0 \\ l4.c14 + l1.c1 & 0 & 0 & l4.c14 & -l5.s5 & 0 \\ 0 & l2.c2 - l3.s23 & -l3.s23 & 0 & l5.c5 & 0 \end{bmatrix} \\
\mathbb{J}_v^6 &= \begin{bmatrix} -l4.s14 - l1.s1 - l6.s146, & -l3.s23 - l2.s2 & -l3.s23 & -l4.s14 - l6.s146 & 0 & 0 \\ l4.c14 + l1.c1 + l6.c146 & 0 & 0 & 0 & l4.c14 + l6.c146 & 0 \\ -l4.s14 - l1.s1 - l6.s146 & -l3.s23 - l2.s2 & -l3.s23 & -l4.s14 - l6.s146 & -l4.s14 - l6.s146 & 0 \end{bmatrix}
\end{aligned}$$

and now we will move to the rotation jacobian:

$$\begin{aligned}\mathbb{J}_w^1 &= \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 & 0 \end{bmatrix} \quad \mathbb{J}_w^2 = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix} \quad \mathbb{J}_w^3 = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix} \\ \mathbb{J}_w^4 &= \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \end{bmatrix} \quad \mathbb{J}_w^5 = \begin{bmatrix} 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix} \quad \mathbb{J}_w^6 = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}\end{aligned}$$

now we can compute  $M(q)$  matrix, by using the following formula:

$$M(q) = \sum_{i=1}^6 m_i \mathbb{J}_v^i T \mathbb{J}_v^i + \mathbb{J}_w^i T R_i I R_i^T \mathbb{J}_w^i \quad (3)$$

where  $m_i$  is the mass of the  $i^{th}$  joint, and  $I$  is the inertia matrix in which we will consider it as a unit matrix for simplicity (but we can change it whenever we want regarding our model)

$$I = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \quad (4)$$

so, our  $M(q)$  matrix will be in the following form:

$$M(q) = \begin{bmatrix} m_{11} & m_{12} & m_{13} & m_{14} & m_{15} & m_{16} \\ m_{21} & m_{22} & m_{23} & m_{24} & m_{25} & m_{26} \\ m_{31} & m_{32} & m_{33} & m_{34} & m_{35} & m_{36} \\ m_{41} & m_{42} & m_{43} & m_{44} & m_{45} & m_{46} \\ m_{51} & m_{52} & m_{53} & m_{54} & m_{55} & m_{56} \\ m_{61} & m_{62} & m_{63} & m_{64} & m_{65} & m_{66} \end{bmatrix} \quad (5)$$

Then we calculate  $C(q, \dot{q})$  matrix, by using the following formula:

$$C_{ij} = \sum_{k=1}^6 c_{ijk} \dot{q}_k \quad (6)$$

and we will also get a matrix as following:

$$C(q, \dot{q}) = \begin{bmatrix} c_{11} & c_{12} & c_{13} & c_{14} & c_{15} & c_{16} \\ c_{21} & c_{22} & c_{23} & c_{24} & c_{25} & c_{26} \\ c_{31} & c_{32} & c_{33} & c_{34} & c_{35} & c_{36} \\ c_{41} & c_{42} & c_{43} & c_{44} & c_{45} & c_{46} \\ c_{51} & c_{52} & c_{53} & c_{54} & c_{55} & c_{56} \\ c_{61} & c_{62} & c_{63} & c_{64} & c_{65} & c_{66} \end{bmatrix} \quad (7)$$

and the  $g(q)$  matrix is:

$$g = \sum_{k=1}^6 (\mathbb{J}_{wi}^k)^T g_0 \quad (8)$$

finally we can derive the dynamic model by using Euler-Lagrange approach by substituting in the next formula:

$$M(q) + C(q, \dot{q})\dot{q} + g(q) = \tau \quad (9)$$

you can find the code and implementation on [GitHub](#).