

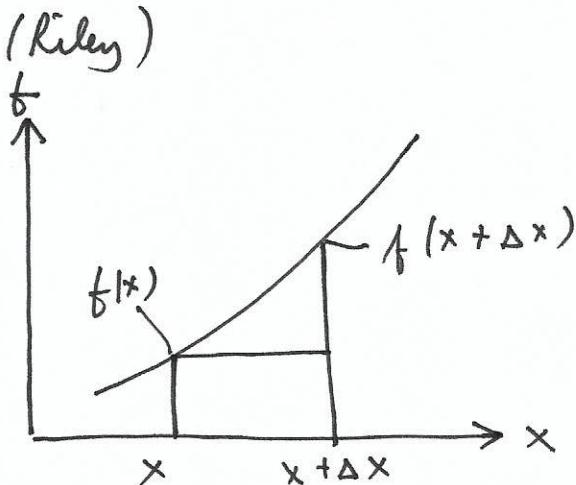
Vector Calculus

1. Differentiation (^{mostly} review)

1.1 Ordinary differentiation

notation used here usually (Riley)

$f = f(x)$
 ↑ ↑ ↗
 dependent function independent variable



Derivative $\frac{df}{dx} = \lim_{\Delta x \rightarrow 0} \frac{f(x + \Delta x) - f(x)}{\Delta x}$

Differential $df = \frac{df}{dx} dx$ two different meanings!

df is the "target approximation to the change in f "
 (Boas, standard)

alternatively (Leibniz) dx is "infinitesimal"
 df is change in f (Riley, nonstandard, useful)

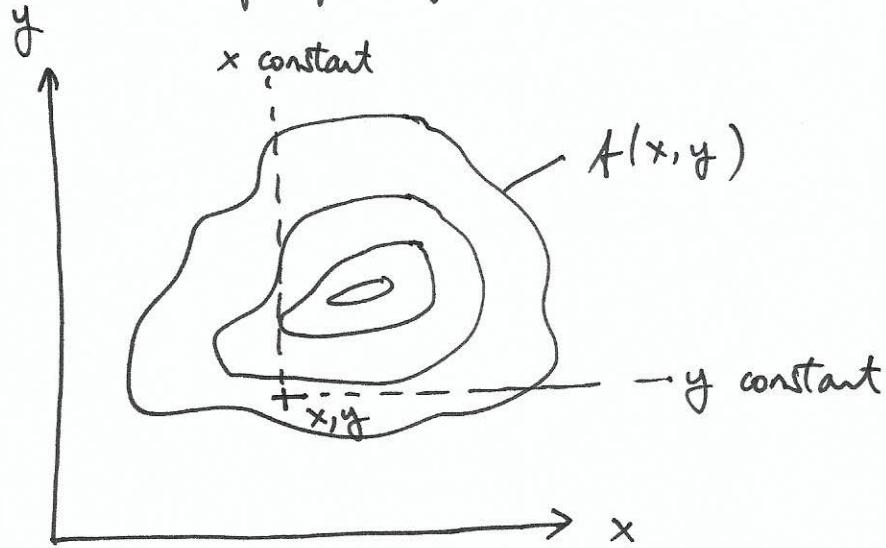
Chain rule $f = f(x(t))$

$$\frac{df}{dt} = \frac{df}{dx} \frac{dx}{dt}$$

1.2 Partial differentiation of scalar fields

More than one independent variable

$f = f(x, y)$ a scalar field e.g. temperature



Partial derivative

$$\frac{\partial f}{\partial x} = \left(\frac{\partial f}{\partial x} \right)_y = \lim_{\Delta x \rightarrow 0} \frac{f(x + \Delta x, y) - f(x, y)}{\Delta x}$$

implicit
↑
y is constant

use when needed
for clarity

Total differential

$$df = \frac{\partial f}{\partial x} dx + \frac{\partial f}{\partial y} dy$$

THE KEY EQUATION

is the "tangent-plane" approximation to Δf
(or the change in f for infinitesimal changes dx, dy)

[no assumption x, y are orthogonal, only independent]

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example

$$f(x,y) = x^2 e^y + y^3$$

calculate the first and second partial derivatives

$$\frac{\partial f}{\partial x} = 2x e^y$$

$$\frac{\partial f}{\partial y} = x^2 e^y + 3y^2$$

 $\frac{\partial}{\partial y}$

$$\frac{\partial}{\partial x} \left(\frac{\partial f}{\partial x} \right) = \frac{\partial^2 f}{\partial x^2} = 2e^y$$

$$\frac{\partial^2 f}{\partial y^2} = x^2 e^y + 6y$$

$$\frac{\partial}{\partial x} \left(\frac{\partial f}{\partial y} \right) = \frac{\partial^2 f}{\partial x \partial y} = 2x e^y$$

$$\frac{\partial^2 f}{\partial y \partial x} = 2x e^y$$

$$\frac{\partial^2 f}{\partial x \partial y} = \frac{\partial^2 f}{\partial y \partial x} \quad \text{Claviault's theorem}$$

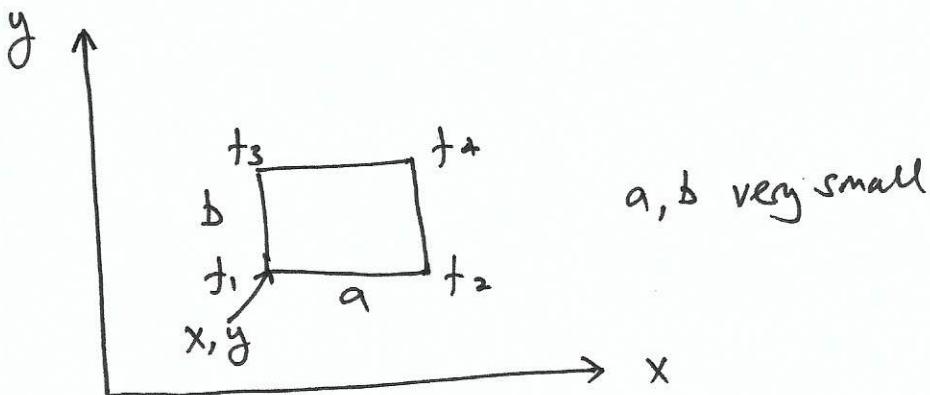
always true provided 1st + 2nd derivatives are continuous

Clairaut's theorem

very rough, not rigorous, to show the idea

means, not
examinable

3 A



$$\frac{\partial f}{\partial x} \approx \frac{f_2 - f_1}{a}$$

$$\frac{\partial f}{\partial y} \approx \frac{f_3 - f_1}{b}$$

$$\frac{\partial}{\partial y} \left(\frac{\partial f}{\partial x} \right) \approx \frac{\frac{(f_4 - f_3)}{a} - \frac{(f_2 - f_1)}{a}}{b} = \frac{f_1 + f_4 - (f_2 + f_3)}{ab}$$

$$\frac{\partial}{\partial x} \left(\frac{\partial f}{\partial y} \right) \approx \frac{\frac{(f_4 - f_2)}{b} - \frac{(f_3 - f_1)}{b}}{a} = \frac{f_1 + f_4 - (f_2 + f_3)}{ab}$$

$$\frac{\partial^2 f}{\partial y \partial x} = \frac{\partial^2 f}{\partial x \partial y}$$

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1.3 Partial differentiation of vector fields

2 D vector field defines a vector at every x, y

$$\underline{A}(x, y) = A_x(x, y) \hat{i} + A_y(x, y) \hat{j} \quad (\text{e.g. velocity})$$

$$\text{e.g. } \underline{A} = xy \hat{i} + x^2 y^2 \hat{j}$$



2 components defined by 2 scalar fields

By analogy define partial derivative

$$\frac{\partial \underline{A}}{\partial x} = \lim_{\Delta x \rightarrow 0} \frac{\underline{A}(x + \Delta x, y) - \underline{A}(x, y)}{\Delta x}$$

$$= \lim_{\Delta x \rightarrow 0} \frac{A_x(x + \Delta x, y) \hat{i} + A_y(x + \Delta x, y) \hat{j} - A_x(x, y) \hat{i} - A_y(x, y) \hat{j}}{\Delta x}$$

$$\frac{\partial \underline{A}}{\partial x} = \frac{\partial A_x}{\partial x} \hat{i} + \frac{\partial A_y}{\partial x} \hat{j} \quad \text{i.e. partial derivative of each component}$$

$$\underline{\text{differential}} \quad d\underline{A} = \frac{\partial \underline{A}}{\partial x} dx + \frac{\partial \underline{A}}{\partial y} dy$$

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1.4 Exact differential

Really a total differential that needs to be recognised!

From before, the total differential is $df = \frac{\partial f}{\partial x} dx + \frac{\partial f}{\partial y} dy$

Now a particular differential

$$A(x, y) dx + B(x, y) dy \quad (1)$$

is a total differential of some parent function f

if $\frac{\partial A}{\partial y} = \frac{\partial B}{\partial x}$ (because $\frac{\partial^2 f}{\partial y \partial x} = \frac{\partial^2 f}{\partial x \partial y}$)

This condition is sufficient.

∴ so we say (1) is an exact differential.

Example !

is $2xy dx + x^2 dy$ exact?

$$\begin{matrix} A \\ \uparrow \\ 2xy \end{matrix} \quad \begin{matrix} B \\ \uparrow \\ x^2 \end{matrix}$$

$$\frac{\partial A}{\partial y} = 2x = \frac{\partial B}{\partial x} \quad \text{yes, exact}$$

What is the parent function?

$$\frac{\partial f}{\partial x}(x, y) = 2xy$$

$$\therefore f = x^2y + g(y) \Rightarrow \frac{\partial f}{\partial y} = x^2 + \frac{\partial g}{\partial y} \quad \frac{dg}{dy}$$

$$\therefore \frac{dg}{dy} = 0 \quad \therefore g = \text{const}^+$$

$$\therefore \text{parent function } f = x^2y + \text{const}$$

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Example 2

$$2xy \, dx - x^2 \, dy \quad (2)$$

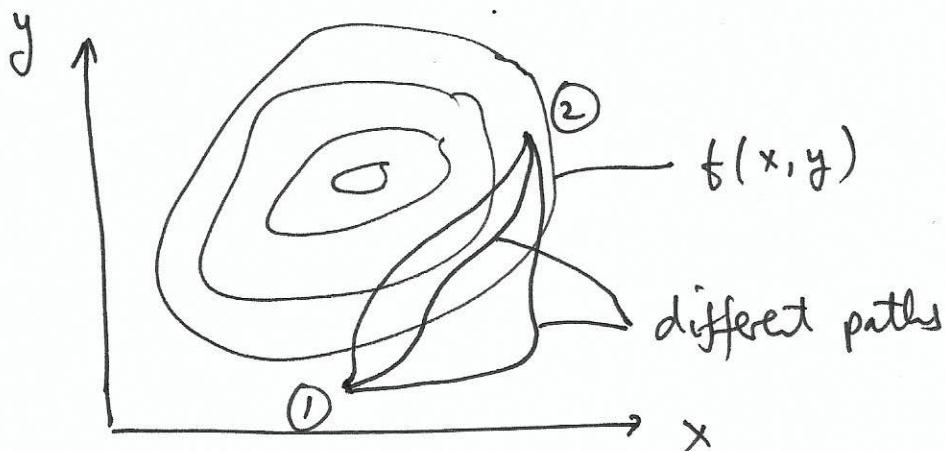
A B

$$\frac{\partial A}{\partial y} = 2x \neq \frac{\partial B}{\partial x} \quad \underline{\text{not exact}}$$

(1 bet) you can't find a parent function of which (2)
is the total differential

- * The integral of an exact differential between two end states is independent of the path

$$\int_{(1)}^{(2)} df = \int_{(1)}^{(2)} A \, dx + \int_{(1)}^{(2)} B \, dy = f_{(2)} - f_{(1)}$$



1.5 Chain rule with partial differentiation

$$f = f(x, y)$$

Look at 3 cases

① $y = y(x)$ only one independent variable (x or y)

② $x = x(t), y = y(t)$
only one independent variable (t)

③ $x = x(u, v), y = y(u, v)$

Case ① $y = y(x)$, what is $\frac{df}{dx}$?

e.g. $f(x, y) = x^2 + y^2$
 $y = 3x^2$

If you can substitute:

$$f(x) = x^2 + 9x^4$$

$$\frac{df}{dx} = 2x + 36x^3$$

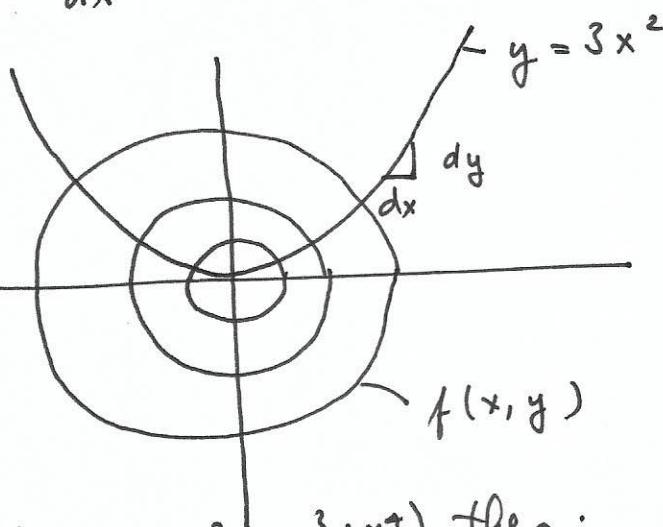
maybe can't substitute ~~unless~~ (e.g. $y + y^2 = x^3 + x^4$) then:

$$df = \frac{\partial f}{\partial x} dx + \frac{\partial f}{\partial y} dy \quad \text{but } dy = \frac{dy}{dx} dx$$

$$df = \frac{\partial f}{\partial x} dx + \frac{\partial f}{\partial y} \frac{dy}{dx} dx$$

$$\boxed{\frac{df}{dx} = \frac{\partial f}{\partial x} + \frac{\partial f}{\partial y} \frac{dy}{dx}}$$

check $\frac{df}{dx} = 2x + 2y \cdot 6x = 2x + 6x^2 \cdot 6x = 2x + 36x^3$ ✓



Case (2) $x = x(t)$ $y = y(t)$

$$dx = \frac{dx}{dt} dt \quad dy = \frac{dy}{dt} dt$$

$$df = \frac{\partial f}{\partial x} \frac{dx}{dt} dt + \frac{\partial f}{\partial y} \frac{dy}{dt} dt$$

$$\frac{df}{dt} = \frac{\partial f}{\partial x} \frac{dx}{dt} + \frac{\partial f}{\partial y} \frac{dy}{dt}$$

using same example as before

$$f(x, y) = x^2 + y^2$$

$$x(t) = 2t \quad y(t) = 12t^2$$

(this is same curve $y = 3x^2$)

$$\begin{aligned} \frac{df}{dt} &= 2x \cdot 2 + 2y \cdot 24t \\ &= 8t + 576t^3 \end{aligned}$$

same path, so check

$$\begin{aligned} \frac{df}{dt} &= \frac{df}{dx} \frac{dx}{dt} = (2x + 36x^3)^2 \\ &= 2x + 72x^3 \\ &= 8t + 576t^3 \quad \checkmark \end{aligned}$$

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Case 3

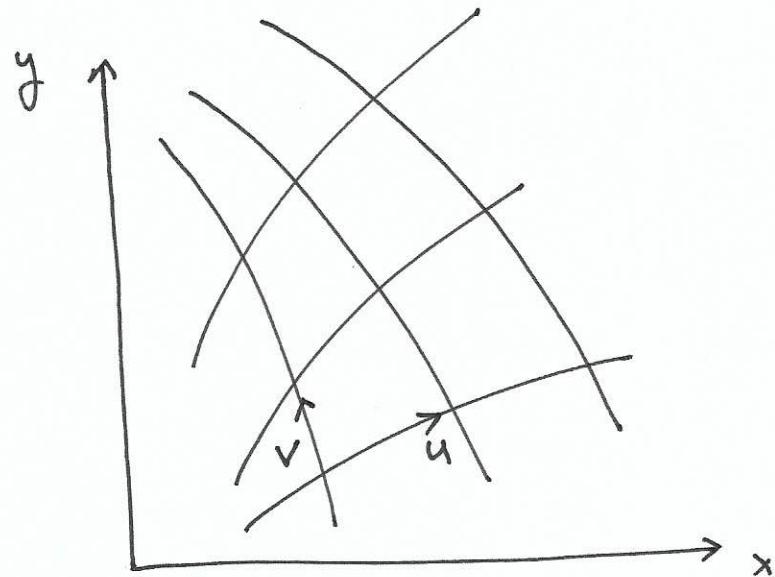
$$x = x(u, v) \quad y = y(u, v)$$

$$df = \frac{\partial f}{\partial x} dx + \frac{\partial f}{\partial y} dy$$

now:

$$dx = \frac{\partial x}{\partial u} du + \frac{\partial x}{\partial v} dv$$

$$dy = \frac{\partial y}{\partial u} du + \frac{\partial y}{\partial v} dv$$

Keeping v constant

$$df = \frac{\partial f}{\partial x} \frac{\partial x}{\partial u} du + \frac{\partial f}{\partial y} \frac{\partial y}{\partial u} du$$

$$\left(\frac{\partial f}{\partial u} \right)_v = \left(\frac{\partial f}{\partial x} \right)_y \left(\frac{\partial x}{\partial u} \right)_v + \left(\frac{\partial f}{\partial y} \right)_x \left(\frac{\partial y}{\partial u} \right)_v$$

similarly

$$\frac{\partial f}{\partial v} = \frac{\partial f}{\partial x} \frac{\partial x}{\partial v} + \frac{\partial f}{\partial y} \frac{\partial y}{\partial v}$$

(subscripts implicit)

Sometimes referred
to as
"change of variables"

Example plane polar coordinates

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$$x(\rho, \phi), y(\rho, \phi)$$

$$\text{find } \left(\frac{\partial f}{\partial \rho} \right), \left(\frac{\partial f}{\partial \phi} \right)_\rho$$

$$\text{e.g. } f = x^2 + y^2$$

~~$x = \rho \cos \phi$~~

$$\text{Now of course } f = x^2 + y^2 = \rho^2$$

$$\text{so directly } \frac{\partial f}{\partial \rho} = 2\rho, \frac{\partial f}{\partial \phi} = 0$$

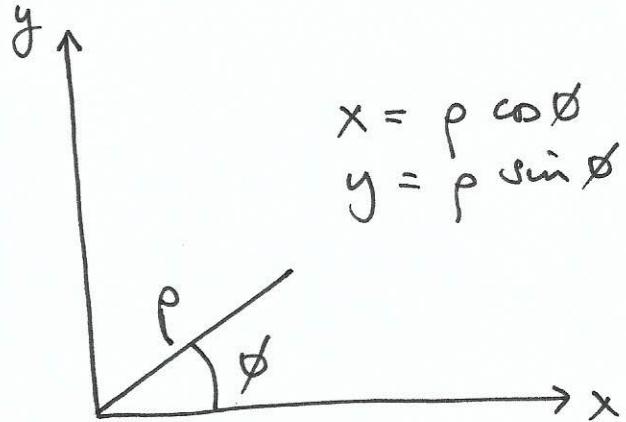
Formally:

$$\begin{aligned} \frac{\partial f}{\partial \rho} &= \frac{\partial f}{\partial x} \frac{\partial x}{\partial \rho} + \frac{\partial f}{\partial y} \frac{\partial y}{\partial \rho} \\ &= 2x \cos \phi + 2y \sin \phi \\ &= 2\rho \cos^2 \phi + 2\rho \sin^2 \phi \end{aligned}$$

$$\frac{\partial f}{\partial \rho} = 2\rho$$

$$\begin{aligned} \frac{\partial f}{\partial \phi} &= \frac{\partial f}{\partial x} \frac{\partial x}{\partial \phi} + \frac{\partial f}{\partial y} \frac{\partial y}{\partial \phi} \\ &= 2x \rho (-\sin \phi) + 2y \rho \cos \phi \\ &= 2\rho \cos \phi \rho (-\sin \phi) + 2\rho \sin \phi \rho \cos \phi \end{aligned}$$

$$\cancel{\frac{\partial f}{\partial \phi}} \frac{\partial f}{\partial \phi} = 0 \quad \text{as expected}$$



$$\begin{aligned} x &= \rho \cos \phi \\ y &= \rho \sin \phi \end{aligned}$$

2. 2 D integration

2.1 1D integration (review)

Integral over interval

a to b of $f(x)$ is limit of Riemann sum

$$S = \sum_{i=1}^n f(x_i)(\xi_i - \xi_{i-1})$$

x_i is any point between ξ_{i-1} and ξ_i

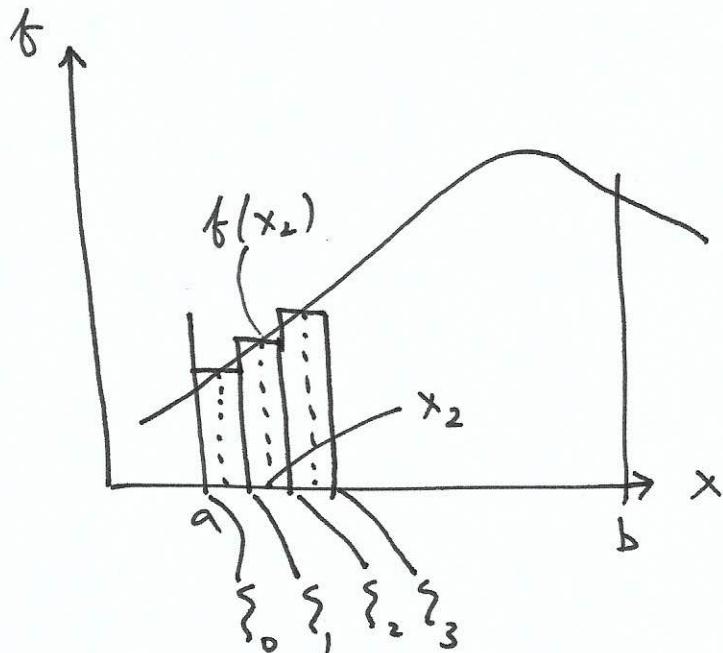
$\int_a^b f(x)dx$ is limit of S as $n \rightarrow \infty$

and width of each strip $\xi_i - \xi_{i-1} \rightarrow 0$ (if sum exists)

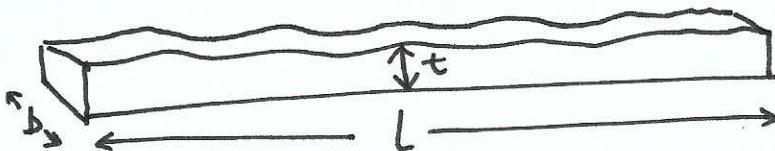
Note that widths do not have to be uniform.

1D integral is 'area under curve'.

Better to consider as 'weighted sum' because of many different uses of integration.



example : a rod of uniform density ρ , width b ,
 varying thickness $t(x)$
 mass per unit length $\lambda(x) = \rho b t(x)$



$$\text{length } l = \int_0^L dx$$

$$\text{mass } m = \int_0^L \lambda(x) dx \quad \text{0th moment of } \lambda$$

$$\text{c of grav } \bar{x} = \frac{1}{m} \int_0^L \lambda(x) x dx \quad \text{1st moment of } \lambda$$

$$\text{radius of gyration } x_r^2 = \frac{1}{m} \int_0^L \lambda(x) x^2 dx \quad \text{2nd moment of } \lambda$$

all weighted sums

Fundamental theorem of calculus (integration from first principles is hard)
 provides connection between integration and differentiation

$$F(b) - F(a) = \int_a^b f(x) dx \quad \text{where } f = \frac{dF}{dx}$$

(simple proof e.g. Riley)

F is the anti-derivative of f .

Many possible functions F that differ by a constant.

Often we don't need to find limit of a sum, we just
 need to find a function that differentiates to $f(x)$.

* This is the first of several integral theorems we will meet *

2.2 2 D integrals

The 2D integral of $f(x, y)$ over a region R

$\iint_R f(x, y) dA$ is the limit
of Riemann sum

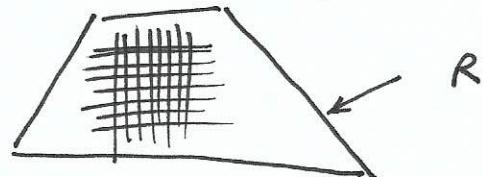
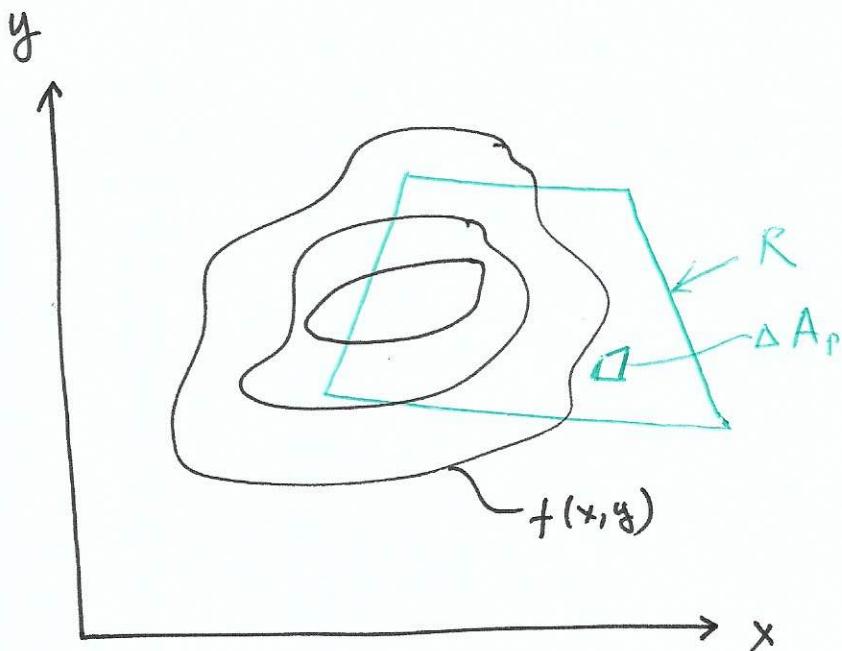
$$S = \sum_{p=1}^n f(x_p, y_p) \Delta A_p$$

as $n \rightarrow \infty$, area $\Delta A_p \rightarrow 0$

the shape and relative sizes of ΔA_p do not matter.

2D integral is like "volume under surface", but generally is a weighted sum.

Could use uniform grid $\Delta x \Delta y$. Then as $n \rightarrow \infty$
area elements are infinitesimal $dA = dx dy$



Example

$$f(x, y) = x + y$$

R is region bounded by $x=0, y=0, y=2-x$

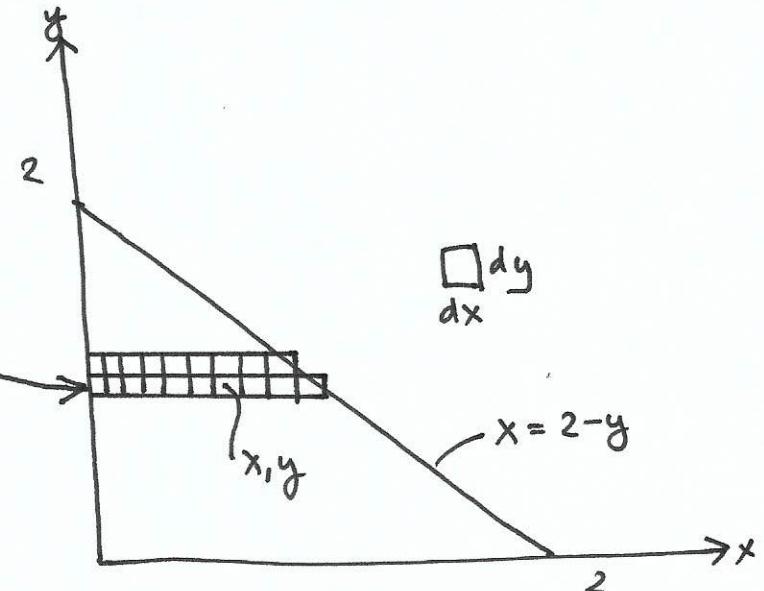
We want $\sum f(x, y) dx dy$

Consider sum for a single slice at fixed y

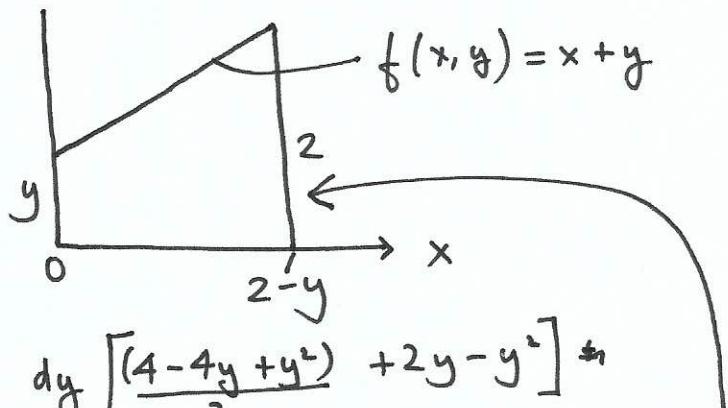
$$dV = \sum f(x, y) dx dy$$

$$= dy \sum f(x, y) dx$$

$$= dy \int_{x=0}^{2-y} (x+y) dx \quad (y \text{ fixed})$$



Cross section looks like:



$$dV = dy \left[\frac{x^2}{2} + yx \right]_0^{2-y} = dy \left[\frac{(4-4y+y^2)}{2} + 2y - y^2 \right]$$

$$dV = dy \left[2 - \frac{y^2}{2} \right] = A(y) dy \quad A(y) \equiv \text{cross section of slice}$$

Now sum up slices

$$V = \sum dV = \int_{y=0}^2 \left(2 - \frac{y^2}{2} \right) dy = \left[2y - \frac{y^3}{6} \right]_0^2 = 4 - \frac{4}{3} = \frac{8}{3}$$

more compactly.

$$V = \int_0^2 \left[\int_{x=0}^{2-y} (x+y) dx \right] dy$$

↑
y = 0
write limits explicitly

"iterated integral"
not needed. Convention
is inner integral first.

N.B. Convention used here "inner to outer" is Boas convention. Others (Riley) use "right to left". Watch out!

Check going the other way, doing the y integral first.

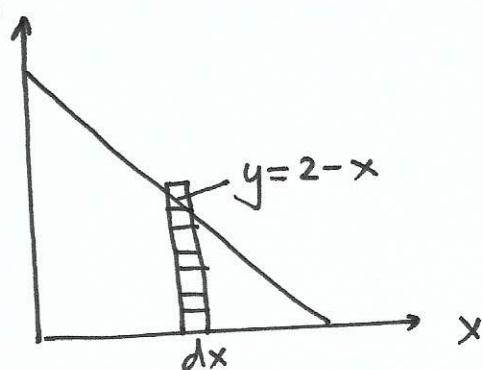
$$V = \int_{x=x_{\min}}^{x_{\max}} \int_{y=y_{\min}}^{y_{\max}} f(x,y) dy dx$$

$x = x_{\min}$ $y = y_{\min}$

$$= \int_{x=0}^2 \int_{y=0}^{2-x} (x+y) dy dx$$

$$= \int_{x=0}^2 \left[xy + \frac{y^2}{2} \right]_0^{2-x} dx = \int_0^2 2 - \frac{x^2}{2} dx$$

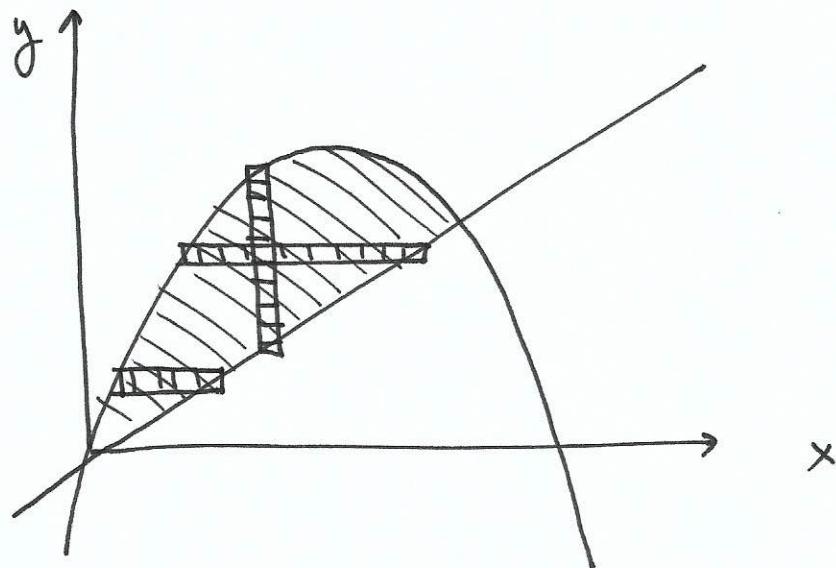
$$= \left[2x - \frac{x^3}{6} \right]_0^2 = \frac{8}{3} \quad \underline{\text{as before}}$$



* * the limits on the integrals for x, y depend on the order you do the integrals !!!.

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always choose the order of integration to make your life easy
example :



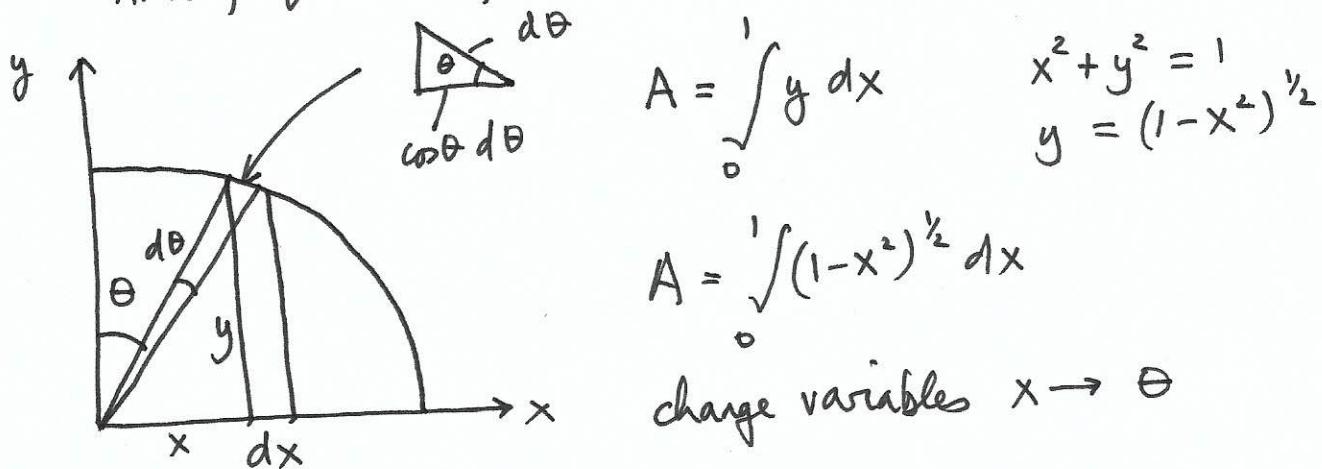
integrate $f(x, y)$ over the shaded area .

This one: do the y integral first (convince yourself)

2.3 Change of variables in 2D integrals - The Jacobian

Reminder: change of variables in 1D integration

Area of quadrant of a circle, radius 1. Expect $\frac{\pi}{4}$.



* Remember: change 3 things

① the integrand: express $f(x)$ as $f(x(\theta))$

$$x = \sin \theta \quad f(x(\theta)) = (1 - \sin^2 \theta)^{1/2} = \cos \theta$$

② the limits $0 < x < 1 \equiv 0 < \theta < \frac{\pi}{2}$

③ the differential

$$dx = \frac{dx}{d\theta} d\theta$$

$$x = \sin \theta \quad \frac{dx}{d\theta} = \cos \theta$$

Put it all together:

$$A = \int_0^{\pi/2} (1-x^2)^{1/2} \, dx = \int_0^{\pi/2} \cos \theta \cdot \cos \theta \, d\theta = \int_0^{\pi/2} \frac{1}{2} [\cos 2\theta + 1] \, d\theta = \left[\frac{\theta}{2} \right]_0^{\pi/2} = \frac{\pi}{4}$$

$$dx = \frac{dx}{d\theta} d\theta$$

is "how much x changes as θ changes by $d\theta$ "

unevenly spaced!

same num, different spacing

1D Jacobian

Now: change of variables in 2D integrals

$$\iint_R f(x,y) dx dy \rightarrow \iint_{R'} f(x(u,v), y(u,v)) |J| du dv$$

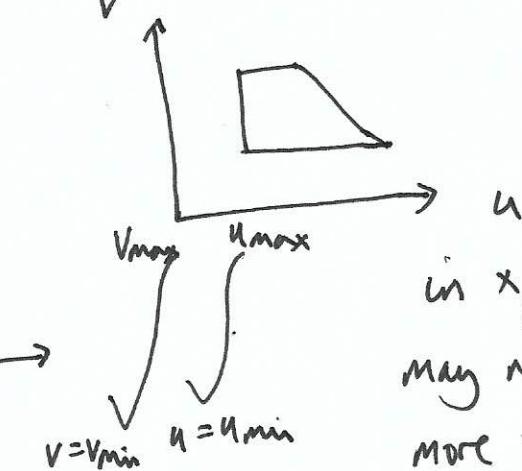
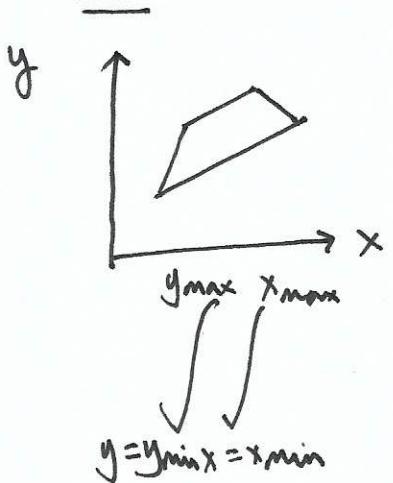
↑
Jacobain

Change 3 things

① the integrand: express $f(x,y)$ as $f(x(u,v), y(u,v))$

② the limits

Draw (yes!) R_{xy} as R'_{uv}



in xy or uv you
may need to split into
more than one integral

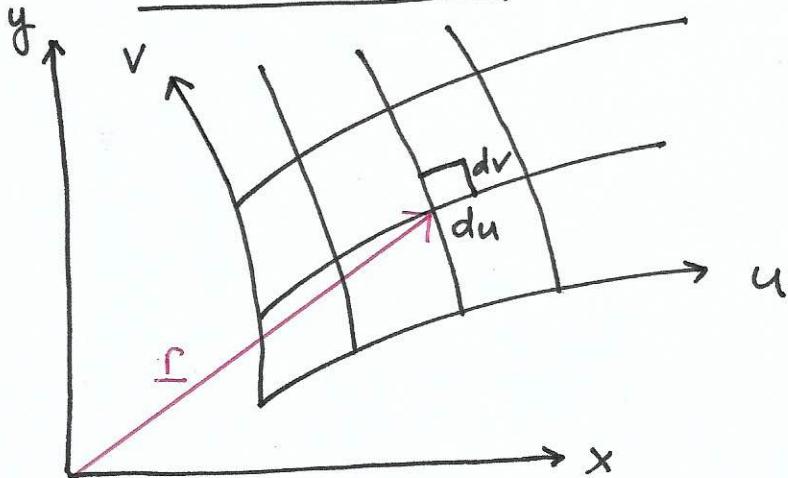
③ transform the differential

$$dx dy \rightarrow |J| du dv$$

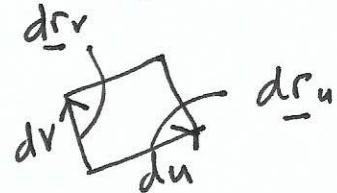
What area in the x,y plane does infinitesimal
change $du dv$ cover?

* There isn't an automatic way (analytic) way
to do step ② - you really do need to draw it!
(see example later in this lecture)

The Jacobian



what is area in x, y plane for element $du \, dv$?



position vector is a vector field $\underline{r} = x \hat{i} + y \hat{j}$

$$\text{then } d\underline{r} = \frac{\partial \underline{r}}{\partial u} du + \frac{\partial \underline{r}}{\partial v} dv = d\underline{r}_u + d\underline{r}_v$$

area of parallelogram is $dA = |d\underline{A}|$

$$d\underline{A} = d\underline{r}_u \times d\underline{r}_v = \boxed{\frac{\partial \underline{r}}{\partial u} \times \frac{\partial \underline{r}}{\partial v} du \, dv}$$

$$d\underline{r}_u = \frac{\partial}{\partial u} (x \hat{i} + y \hat{j}) du = \left(\frac{\partial x}{\partial u} \hat{i} + \frac{\partial y}{\partial u} \hat{j} \right) du$$

$$d\underline{r}_v = \left(\frac{\partial x}{\partial v} \hat{i} + \frac{\partial y}{\partial v} \hat{j} \right) dv$$

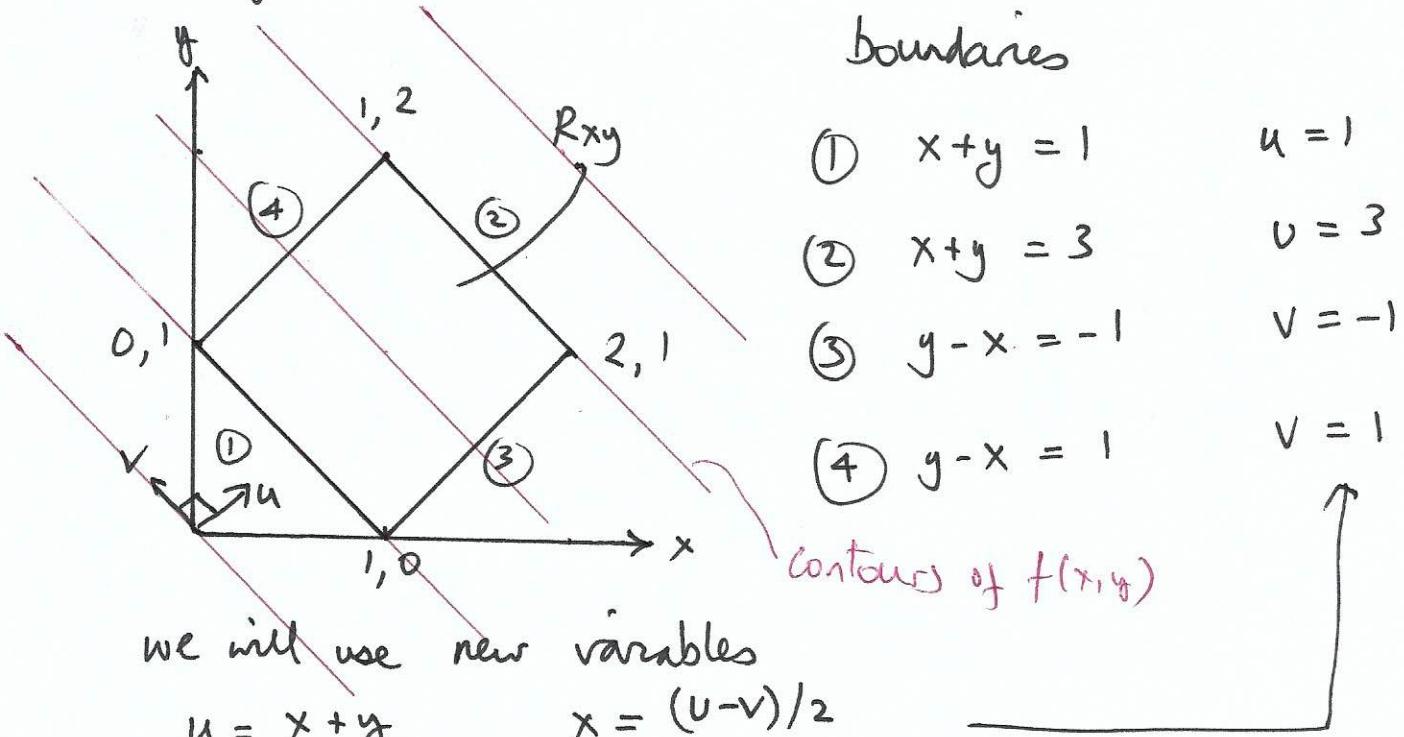
$$d\underline{A} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial x}{\partial u} & \frac{\partial y}{\partial u} & 0 \\ \frac{\partial x}{\partial v} & \frac{\partial y}{\partial v} & 0 \end{vmatrix} \quad dudv = \hat{k} \begin{vmatrix} \frac{\partial x}{\partial u} & \frac{\partial y}{\partial u} \\ \frac{\partial x}{\partial v} & \frac{\partial y}{\partial v} \end{vmatrix} du \, dv$$

determinant
 $J = \text{Jacobian}$

$$dA = |J| du \, dv$$

absolute value

Sometimes written $J = \frac{\partial(x, y)}{\partial(u, v)}$

Example 2D integral and JacobianIntegrate $f(x,y) = x+y$ over diamond region

we will use new variables

$$\begin{aligned} u &= x+y \\ v &= y-x \end{aligned}$$

$$x = (u-v)/2$$

$$y = (u+v)/2$$

check the following 2D integral using x, y

$$I = \iint f(x,y) dx dy$$

 R_{xy}

$$= \int_{x=0}^1 \int_{y=1-x}^{1+x} (x+y) dy dx + \int_{x=1}^2 \int_{y=x-1}^{3-x} (x+y) dy dx$$

$$x=0 \quad y=1-x \qquad x=1 \quad y=x-1$$

$$= \int_0^1 \left[xy + \frac{y^2}{2} \right]_{1-x}^{1+x} dx + \int_1^2 \left[xy + \frac{y^2}{2} \right]_{x-1}^{3-x} dx$$

2 integrals,
long!

$$= \int_0^1 2x^2 + 2x dx + \int_1^2 4 + 2x - 2x^2 dx$$

$$= \frac{5}{3} + \frac{7}{3} = \boxed{4 = I}$$

Integral using u, v .

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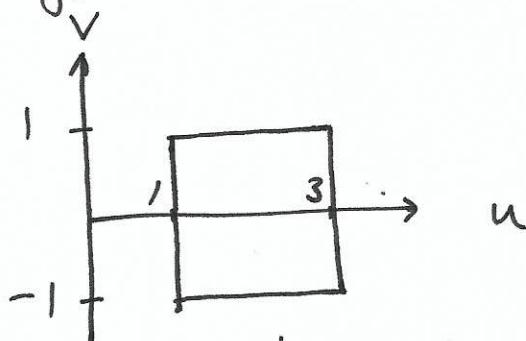
Remember 3 steps

① Transform integrand

$$f(x, y) \rightarrow f(x(u, v), y(u, v))$$

$$f(x, y) \rightarrow f(u) \quad x + y \rightarrow u$$

② Change limits. Draw R_{xy} in the u, v plane



③ Transform the differential

$$dx dy = |J| du dv$$

$$J = \begin{vmatrix} \frac{\partial x}{\partial u} & \frac{\partial x}{\partial v} \\ \frac{\partial y}{\partial u} & \frac{\partial y}{\partial v} \end{vmatrix} = \begin{vmatrix} \frac{1}{2} & \frac{1}{2} \\ -\frac{1}{2} & \frac{1}{2} \end{vmatrix} = \frac{1}{2} \quad (\text{analytic})$$

* I wrote this wrong
in the lecture

Put it all together :

$$I = \iint f(x(u, v), y(u, v)) |J| du dv$$

$$= \int_{v=-1}^{R_{uv}} \int_{u=1}^3 u \cdot \frac{1}{2} \cdot du dv = \int_{-1}^1 \left[\frac{u^2}{4} \right]_1^3 dv$$

$$= \int_{-1}^1 2 dv = \left[2v \right]_{-1}^1 = 4 \quad (\text{as before})$$

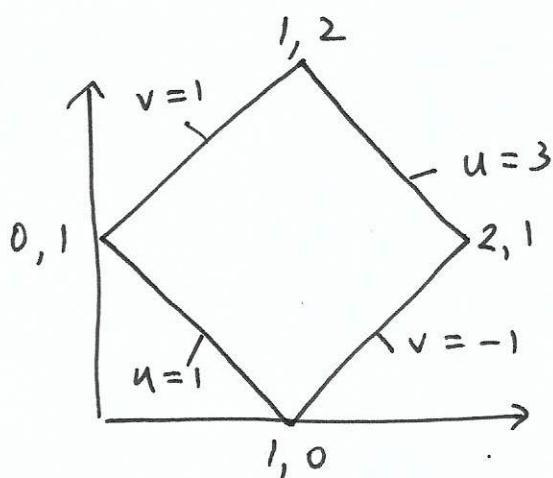
Note: u, v the natural coordinates for this problem

We derived the Jacobian analytically.

But we could do it geometrically.

The question is what is the area in the x,y plane for changes du, dv

Consider the diamond



area of diamond
in x,y plane is

$$\sqrt{2} \times \sqrt{2} = 2$$

area in u,v plane is
 $2 \times 2 = 4$

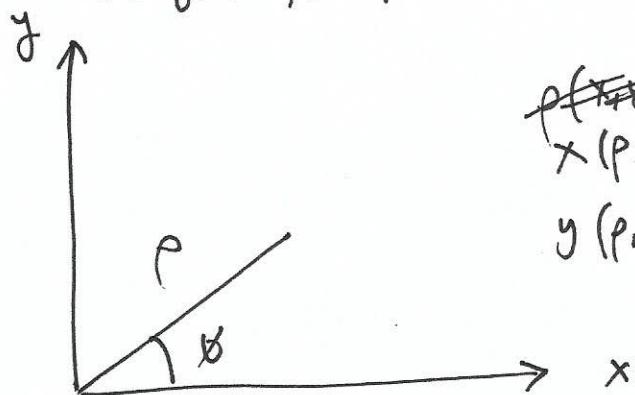
so an element $du dv$ covers
an area $\frac{1}{2} du dv$ in the x,y plane

$$|J|$$

(as we found)

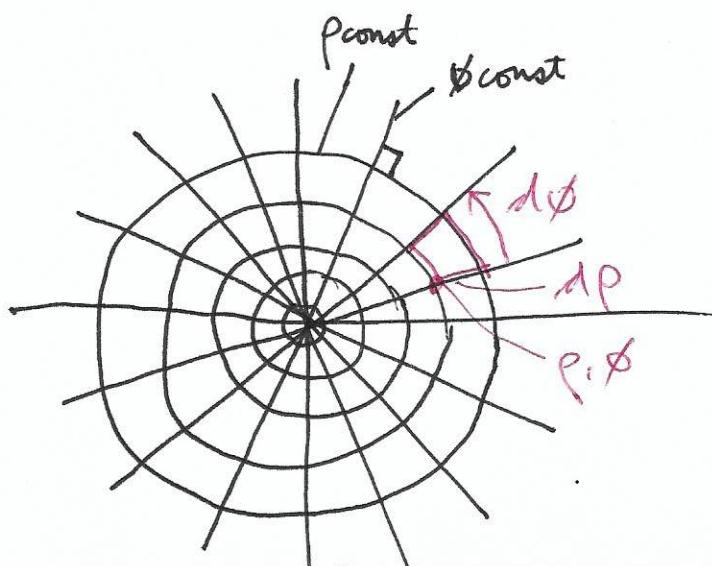
2.4 Plane-polar coordinates

Useful for problems with circular symmetry



$$\begin{aligned} x(p, \phi) &= p \cos \phi & \rho(x, y) &= (x^2 + y^2)^{1/2} \\ y(p, \phi) &= p \sin \phi & \phi(x, y) &= \tan^{-1}(y/x) \end{aligned}$$

The coordinates are orthogonal (!)



what is dA for charges $d\rho, d\phi$?

geometric derivation



$$dA = \rho \, d\rho \, d\phi = |J| \, d\rho \, d\phi$$

i.e. $J = \rho$

analytic derivation

$$J = \begin{vmatrix} \frac{\partial x}{\partial \rho} & \frac{\partial x}{\partial \phi} \\ \frac{\partial y}{\partial \rho} & \frac{\partial y}{\partial \phi} \end{vmatrix} = \begin{vmatrix} \cos \phi & \sin \phi \\ -\sin \phi & \rho \cos \phi \end{vmatrix} = \rho (\cos^2 \phi + \sin^2 \phi) = \rho$$

$J = \rho \quad \text{agrees}$

Example

(24)

A disk of radius R has surface mass density $\sigma(x, y) = \frac{B}{\sqrt{x^2 + y^2}}$.

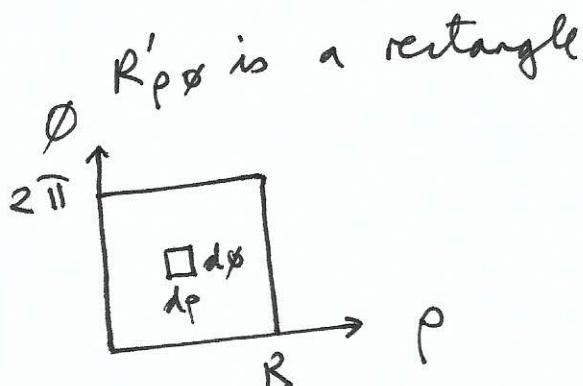
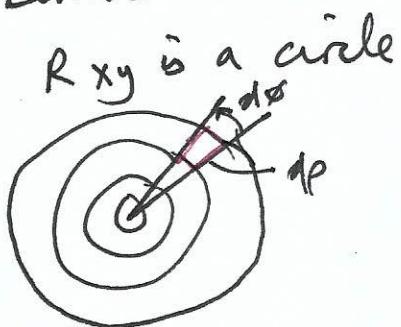
What is the mass of the disk?

Difficult in Cartesian coords.

Problem has circular symmetry — use plane-polar coordinates

$$\textcircled{1} \quad f(x, y) \rightarrow \sigma(x(p, \phi), y(p, \phi)) = \frac{B}{p}$$

\textcircled{2} Limits



$$\textcircled{3} \quad |J| = p$$

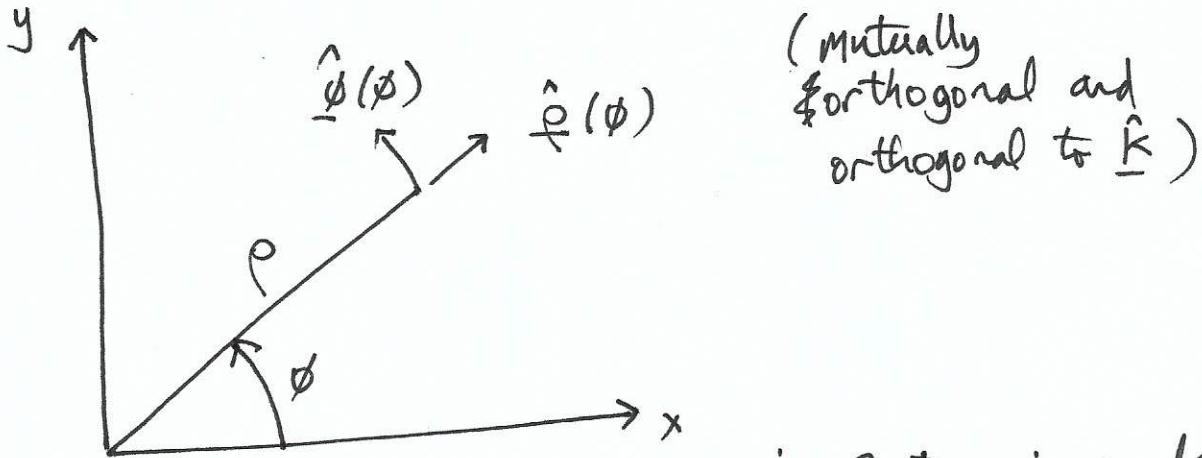
$$\begin{aligned} I &= \int_0^{2\pi} \int_0^R \frac{B}{p} p \, dp \, d\phi \\ &= \int_0^{2\pi} \left[Bp \right]_0^R \, d\phi = BR \left[\phi \right]_0^{2\pi} = 2\pi BR \end{aligned}$$

easy

2.5 Unit vectors in plane-polar coordinates

Differentiating vector fields in plane-polar coords is more difficult!

Useful to define unit vectors in radial \hat{r} and tangential $\hat{\theta}$ directions. They both depend on ϕ !



(Mutually orthogonal and orthogonal to \hat{k})

To differentiate unit vectors, write in Cartesian coords

$$\begin{aligned}\hat{r} &= \cos \phi \hat{i} + \sin \phi \hat{j} \\ \hat{\theta} &= -\sin \phi \hat{i} + \cos \phi \hat{j}\end{aligned}$$

Then $\frac{\partial \hat{r}}{\partial \phi} = -\sin \phi \hat{i} + \cos \phi \hat{j} = \hat{\theta}$

$$\frac{\partial \hat{\theta}}{\partial \phi} = -\cos \phi \hat{i} - \sin \phi \hat{j} = -\hat{r}$$

$$\frac{\partial \hat{r}}{\partial p} = 0 \quad \frac{\partial \hat{\theta}}{\partial p} = 0$$

* *
REMEMBER!

Differentiating vector fields using plane-polar coords.

We will differentiate the position vector $\underline{r} = \rho \hat{f}$

to derive the Jacobian for plane-polar

Generally $d\underline{r} = \frac{\partial \underline{r}}{\partial \rho} d\rho + \frac{\partial \underline{r}}{\partial \phi} d\phi$ ($\rho \equiv u, \phi \equiv v$)

and the Jacobian is

$$J = \left| \frac{\partial \underline{r}}{\partial \rho} \times \frac{\partial \underline{r}}{\partial \phi} \right| \text{ modulus}$$

$$\frac{\partial \underline{r}}{\partial \rho} (\rho, \phi) = \frac{\partial}{\partial \rho} (\rho \hat{f}) = \frac{\partial \rho}{\partial \rho} \hat{f} + \rho \cancel{\frac{\partial \hat{f}}{\partial \rho}} = \hat{f}$$

$$\frac{\partial \underline{r}}{\partial \phi} (\rho, \phi) = \frac{\partial}{\partial \phi} (\rho \hat{f}) = \cancel{\frac{\partial \rho}{\partial \phi}} \hat{f} + \rho \frac{\partial \hat{f}}{\partial \phi} = \rho \hat{\phi}$$

orthogonal $\therefore J = \rho$

or write

$$\frac{\partial \underline{r}}{\partial \rho} \times \frac{\partial \underline{r}}{\partial \phi} = \begin{vmatrix} \hat{f} & \hat{\phi} & \hat{k} \\ 1 & 0 & 0 \\ 0 & \rho & 0 \end{vmatrix} = \rho \hat{k} \quad |J| = \rho$$

generally: write vector field $\underline{A} = A_f \hat{f} + A_\phi \hat{\phi}$ $A_f(\rho, \phi) \hat{f} + A_\phi(\rho, \phi) \hat{\phi}$
 then e.g. $\frac{\partial \underline{A}}{\partial \phi} = \frac{\partial}{\partial \phi} (A_f \hat{f} + A_\phi \hat{\phi})$

Generally: write vector field

$$\underline{A} = A_f(\rho, \phi) \hat{f}(\phi) + A_\phi(\rho, \phi) \hat{\phi}(\phi)$$

then e.g. $\frac{\partial \underline{A}}{\partial \phi} = \frac{\partial (A_f \hat{f})}{\partial \phi} + \frac{\partial (A_\phi \hat{\phi})}{\partial \phi}$ and use product rule

3. 3D integrals3.1 Cartesian coordsExample

Integrate $f(x, y, z) = \alpha x$
over tetrahedron bounded by planes

$$\begin{aligned}x &= 0 \\y &= 0 \\z &= 0 \\x+y+z &= 1\end{aligned}$$

Let us integrate in order

$$I = \int_{x=0}^1 \int_{y=0}^{1-x} \int_{z=0}^{1-x-y} \alpha x \, dz \, dy \, dx$$

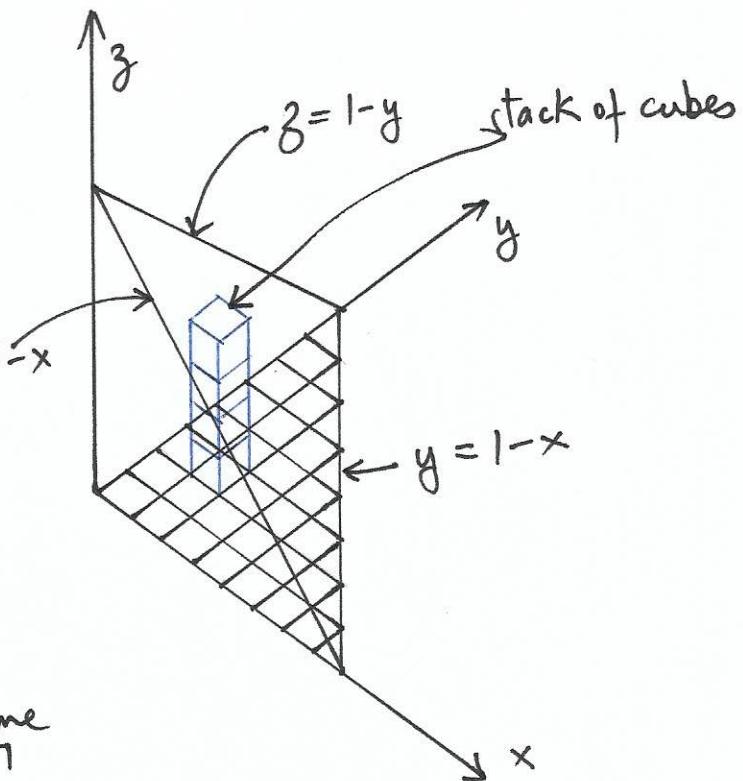
"weight"
cube volume
weight for 2D x,y integral

1st integral x, y constant

$$I = \int_{x=0}^1 \int_{y=0}^{1-x} [\alpha x z]_0^{1-x-y} dy dx = \alpha \int_{x=0}^1 \int_{y=0}^{1-x} x - x^2 - xy \, dy \, dx$$

$$I = \alpha \int_{x=0}^1 \left[x(1-x)y - \frac{x^2 y^2}{2} \right]_0^{1-x} dx = \alpha \int_{x=0}^1 \frac{x((1-x)^2)}{2} dx$$

$$I = \frac{\alpha}{2} \left[\frac{x^2}{2} - \frac{2x^3}{3} + \frac{x^4}{4} \right]_0^1 = \frac{\alpha}{24}$$



2nd integral x constant

$$\text{area of slice at constant } x$$

Now: you really must try this integral in order y, x, z
or x, z, y to get same answer

3.2 Jacobian in 3D

$$I = \iiint_{R_{xyz}} f(xyz) dx dy dz \Rightarrow \iiint_{R'_{uvw}} f(x(uvw), y(uvw), z(uvw)) |J| du dv dw$$

If $x(uvw)$, $y(uvw)$, $z(uvw)$ the differential of the position vector is

$$d\vec{r} = \frac{\partial \vec{r}}{\partial u} du + \frac{\partial \vec{r}}{\partial v} dv + \frac{\partial \vec{r}}{\partial w} dw = d\vec{r}_u + d\vec{r}_v + d\vec{r}_w$$

Since $\vec{r} = x \hat{i} + y \hat{j} + z \hat{k}$

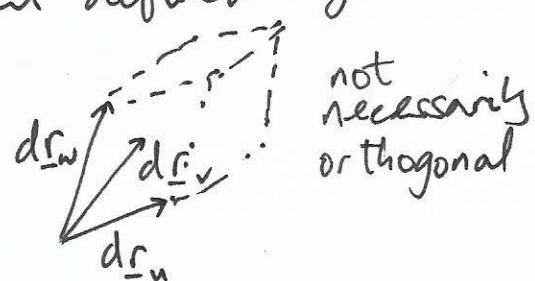
then e.g. $d\vec{r}_u = \left(\frac{\partial x}{\partial u} \hat{i} + \frac{\partial y}{\partial u} \hat{j} + \frac{\partial z}{\partial u} \hat{k} \right) du$

We want the volume of the little element defined by

the 3 little vectors $d\vec{r}_u$, $d\vec{r}_v$, $d\vec{r}_w$

Recall vol. of parallelepiped is $a \cdot b \times c$

i.e. $d\vec{r}_u \cdot d\vec{r}_v \times d\vec{r}_w$



$$dV_{uvw} = \left(\frac{\partial x}{\partial u} \hat{i} + \frac{\partial y}{\partial u} \hat{j} + \frac{\partial z}{\partial u} \hat{k} \right) \cdot \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial x}{\partial v} & \frac{\partial y}{\partial v} & \frac{\partial z}{\partial v} \\ \frac{\partial x}{\partial w} & \frac{\partial y}{\partial w} & \frac{\partial z}{\partial w} \end{vmatrix} du dv dw$$

$$dV_{uvw} = \begin{vmatrix} \frac{\partial x}{\partial u} & \frac{\partial y}{\partial u} & \frac{\partial z}{\partial u} \\ \frac{\partial x}{\partial v} & \frac{\partial y}{\partial v} & \frac{\partial z}{\partial v} \\ \frac{\partial x}{\partial w} & \frac{\partial y}{\partial w} & \frac{\partial z}{\partial w} \end{vmatrix} du dv dw$$

3D Jacobian
sometimes written $\frac{\partial (x, y, z)}{\partial (u, v, w)}$

We want the absolute value $|J|$

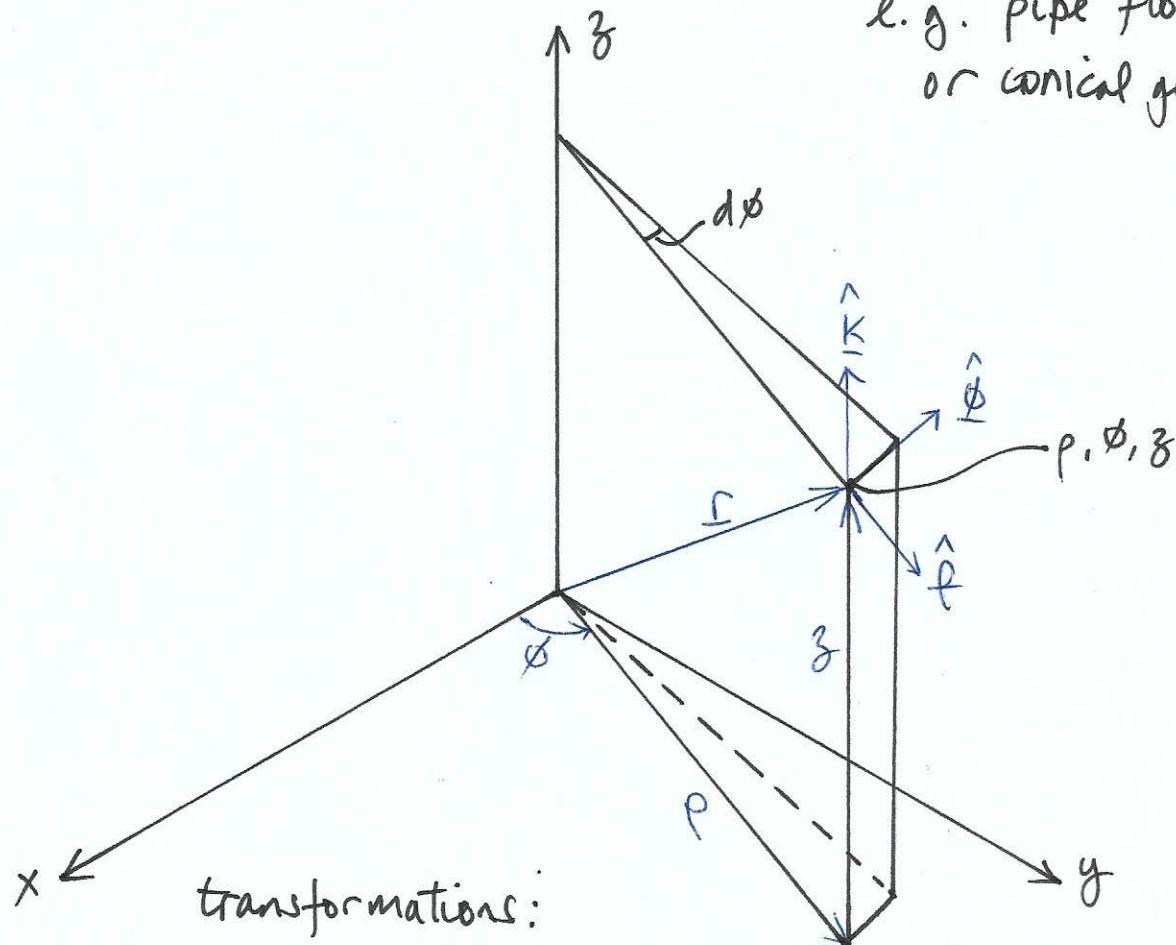
3.3 Cylindrical polar coordinates

(29)

Same as plane polar + z axis

Useful for problems with circular symmetry + variation in z

e.g. pipe flow,
or conical geometry



transformations:

$$\begin{aligned}x &= \rho \cos \phi & \rho &= \sqrt{x^2 + y^2} \\y &= \rho \sin \phi & \phi &= \tan^{-1}(y/x)\end{aligned}$$

$$z = z$$

$$z = z$$

$$\text{position vector } \underline{r}(\rho, \phi, z) = \rho \hat{r}(\phi) + z \hat{k}$$

$\hat{r}(\phi), \hat{\theta}(\phi), \hat{k}$ orthogonal, no dependence on ρ or z

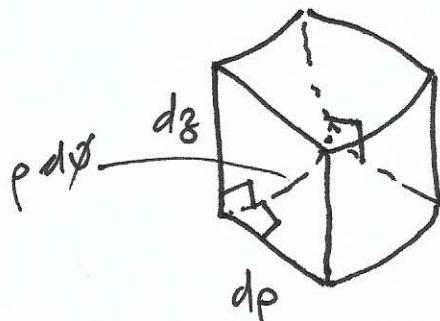
when differentiating a vector field in cylindrical coords
remember $\hat{r}, \hat{\theta}$ depend on ϕ

$$\frac{\partial \hat{r}}{\partial \phi} = \hat{\theta} \quad \frac{\partial \hat{\theta}}{\partial \phi} = -\hat{r}$$

Volume element $|J| d\rho d\phi dz$

(30)

Geometrically What is the volume produced by small changes $d\rho, d\phi, dz$.



$$dV = \rho d\rho d\phi dz$$

Analytically write force from Jacobian (using Cartesian coords)

$$J = \begin{vmatrix} \frac{\partial x}{\partial \rho} & \frac{\partial x}{\partial \phi} & \frac{\partial x}{\partial z} \\ \frac{\partial y}{\partial \rho} & \frac{\partial y}{\partial \phi} & \frac{\partial y}{\partial z} \\ \frac{\partial z}{\partial \rho} & \frac{\partial z}{\partial \phi} & \frac{\partial z}{\partial z} \end{vmatrix} = \begin{vmatrix} \cos\phi & \sin\phi & 0 \\ -\sin\phi & \rho\cos\phi & 0 \\ 0 & 0 & 1 \end{vmatrix} = \rho$$

as expected

$$dV = |J| d\rho d\phi dz = \rho d\rho d\phi dz$$

More elegantly using differential of position vector using $\hat{i}, \hat{\theta}, \hat{k}$

$$\underline{r} = \rho \hat{i}(\phi) + z \hat{k} \quad d\underline{r} = \frac{\partial r}{\partial \rho} d\rho + \frac{\partial r}{\partial \phi} d\phi + \frac{\partial r}{\partial z} dz$$

$$\text{charge } d\rho \quad d\underline{r}_\rho = \frac{\partial r}{\partial \rho} d\rho = \underline{i}\rho \hat{i}$$

$$\text{charge } d\phi \quad d\underline{r}_\phi = \frac{\partial r}{\partial \phi} d\phi = \rho \underline{i}\phi \hat{\theta}$$

$$\text{charge } dz \quad d\underline{r}_z = \frac{\partial r}{\partial z} dz = dz \hat{k}$$

orthogonal

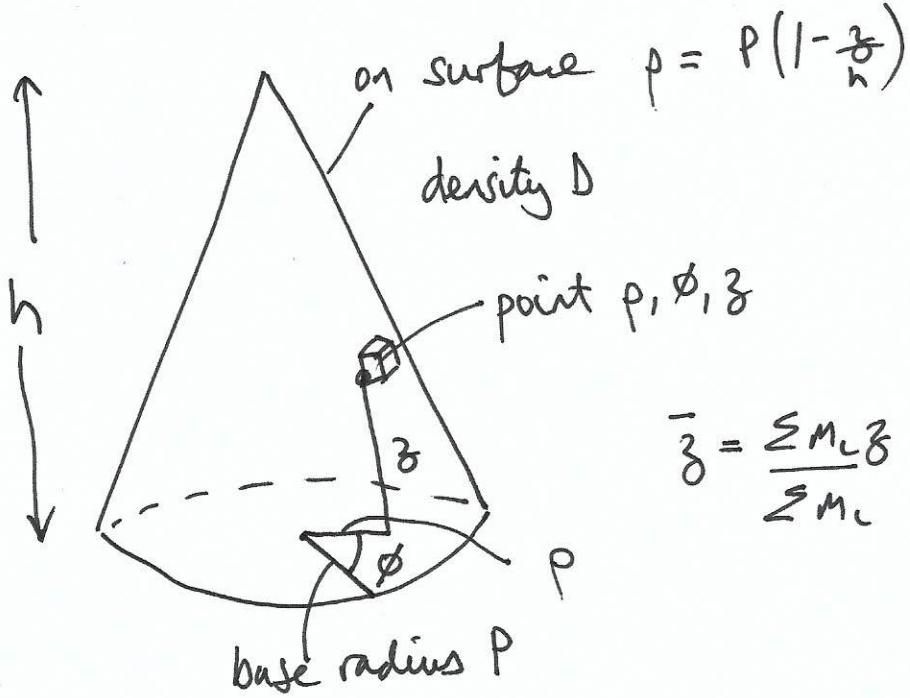
$$dV = d\underline{r}_\rho \cdot d\underline{r}_\phi \times d\underline{r}_z$$

$$= \rho d\rho d\phi dz$$

(determinant not needed)

Example: (vertical) centre of gravity of solid cone

(31)



$$\bar{z} = \frac{\sum m_i z_i}{\sum m_i} = \frac{\iiint z \Delta dV}{\iiint \Delta dV}$$

$$= \frac{\text{1st moment of vol}}{\text{0th moment of vol}}$$

denominator $V = \frac{1}{3} \text{base} \times h = \frac{\pi P^2 h}{3}$ (prove later)

numerator $I = \int_{z=0}^h \int_{\rho=0}^{P(1-\frac{z}{h})} \int_{\phi=0}^{2\pi} z \rho d\phi d\rho dz = 2\pi \int_{z=0}^h z \left[\frac{\rho^2}{2} \right]_0^{P(1-\frac{z}{h})} dz$

differentiate

$$I = \pi \int_{z=0}^h z P^2 \left(1 - \frac{z}{h}\right)^2 dz \quad (1)$$

$$= \pi P^2 \left[\frac{z^2}{2} - \frac{2z^3}{3h} + \frac{z^4}{4h^2} \right]_0^h = \frac{\pi P^2 h^2}{12}$$

... algebra ...

$$\text{based on (1)} \quad V = \pi \int_{z=0}^h P^2 \left[1 - \frac{z}{h}\right]^2 dz \quad \dots \text{algebra} \dots = \frac{\pi P^2 h}{3}$$

$$\bar{z} = \frac{I}{V} = \frac{\pi P^2}{\pi P^2} \frac{h^2}{12} \frac{3}{h} = \frac{h}{4}$$

TOP INTEGRAL
NOW TRY IN A
DIFFERENT ORDER
DO z FIRST!

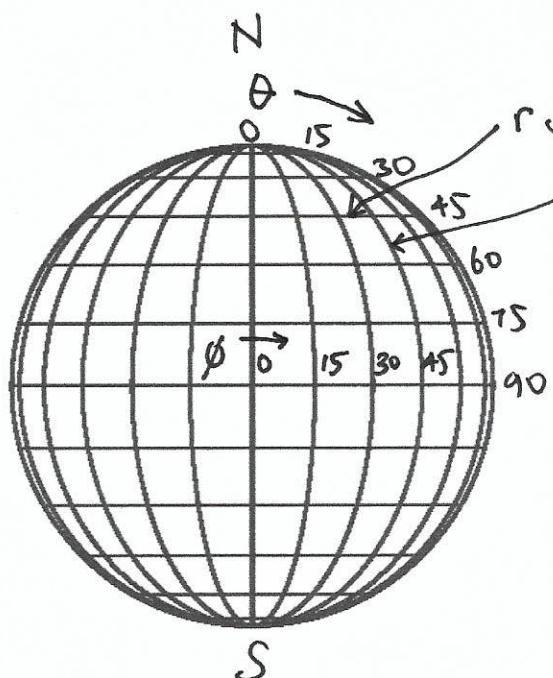
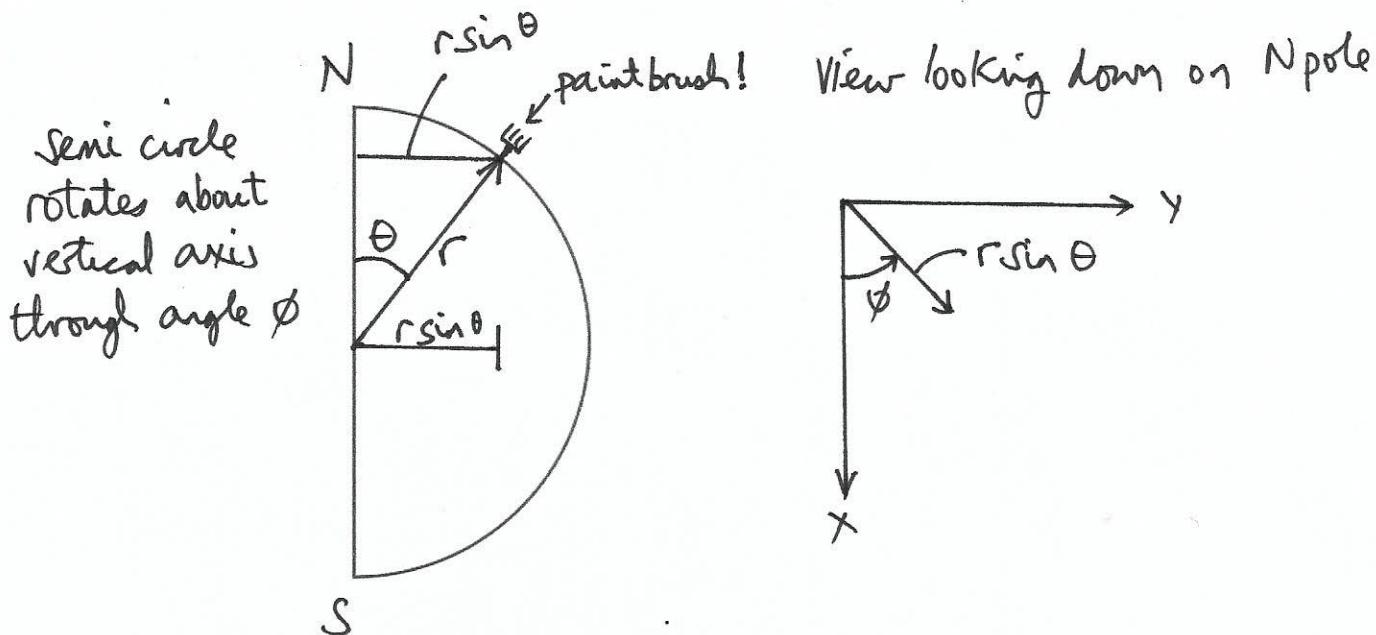
3.4 Spherical polar coordinates

Coordinates are r, θ, ϕ

"latitude" "longitude" (correct but said wrong in lecture)

These are orthogonal

Imagine glass sphere, radius r . We are going to paint inside lines of constant θ and ϕ

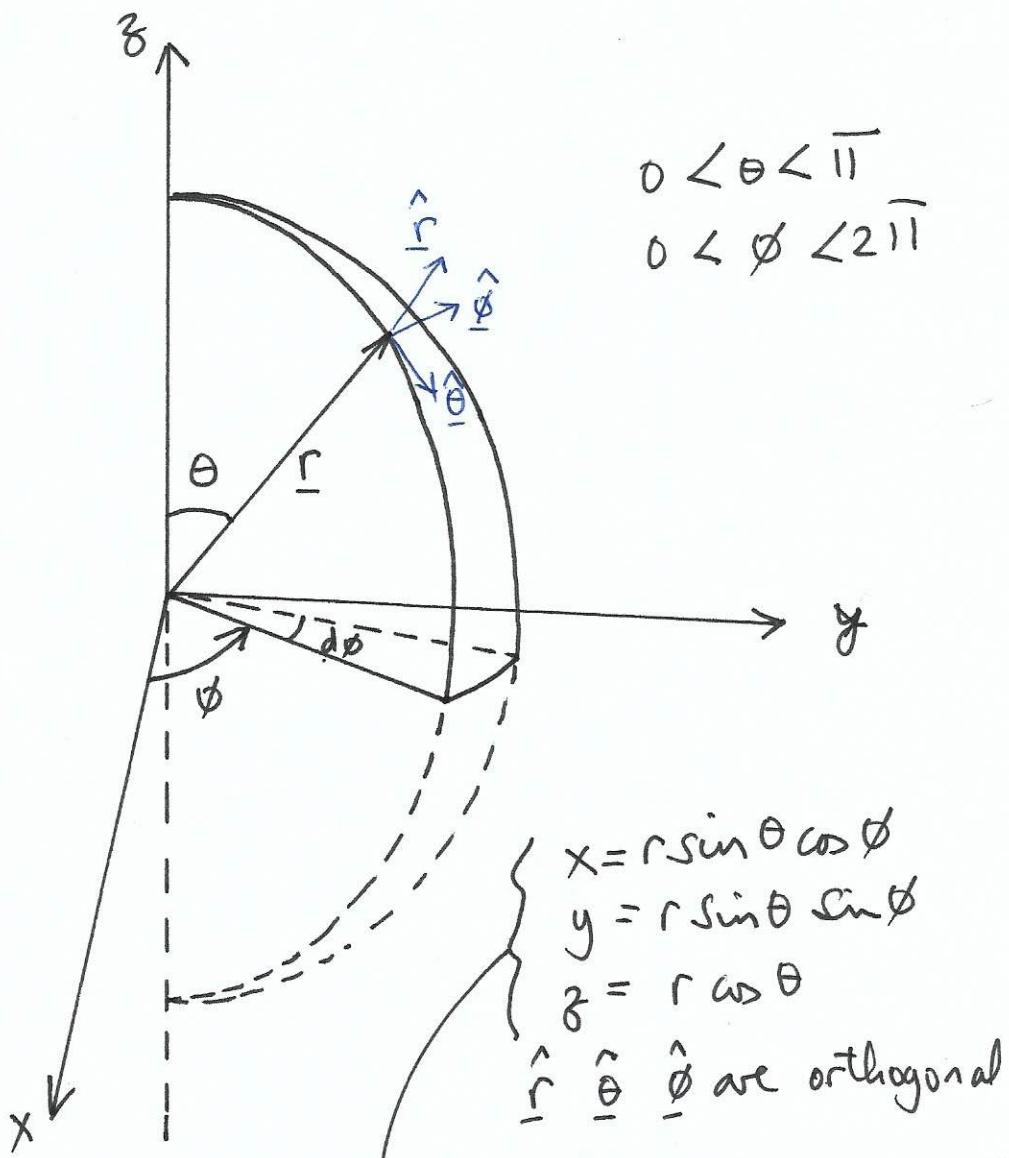


from geometry

$$dV = r \sin \theta d\phi r d\theta dr$$

$$dV = r^2 \sin \theta dr d\theta d\phi$$

(33)



use these to get the Jacobian
and check the volume element

recall ~~the~~^{to} differentiate unit vectors, express using $\hat{i}, \hat{j}, \hat{k}$

(34)

$$\hat{r}(\theta, \phi) = \sin \theta \cos \phi \hat{i} + \sin \theta \sin \phi \hat{j} + \cos \theta \hat{k}$$

$$\hat{\theta}(\theta, \phi) = \cos \theta \cos \phi \hat{i} + \cos \theta \sin \phi \hat{j} - \sin \theta \hat{k}$$

$$\hat{\phi}(\phi) = -\sin \phi \hat{i} + \cos \phi \hat{j}$$

you should be able to figure these out

use these to derive derivatives of unit vectors as needed.

position vector $r = r \hat{r}(\theta, \phi)$

so we need $\frac{\partial \hat{r}}{\partial \theta}$ and $\frac{\partial \hat{r}}{\partial \phi}$

$$\frac{\partial \hat{r}}{\partial \theta} = \cos \theta \cos \phi \hat{i} + \cos \theta \sin \phi \hat{j} - \sin \theta \hat{k} = \hat{\theta} \quad] * \text{REMEMBER}$$

$$\frac{\partial \hat{r}}{\partial \phi} = -\sin \theta \sin \phi \hat{i} + \sin \theta \cos \phi \hat{j} = \sin \theta \hat{\phi}$$

Now derive volume element from differential:

$$dr = \frac{\partial r}{\partial r} dr + \frac{\partial r}{\partial \theta} d\theta + \frac{\partial r}{\partial \phi} d\phi$$

charge dr $dr_r = \frac{\partial r}{\partial r} dr = dr \hat{r}$

charge $d\theta$ $d\theta_r = \frac{\partial r}{\partial \theta} d\theta = r d\theta \hat{\theta}$

charge $d\phi$ $d\phi_r = \frac{\partial r}{\partial \phi} d\phi = r \sin \theta d\phi \hat{\phi}$

$$\therefore dV = \text{product} = r^2 \sin \theta dr d\theta d\phi$$

} orthogonal

3.5 Surface integrals

On a surface in 3D define infinitesimal element of area $d\bar{S}$, a vector of area $|d\bar{S}|$, with direction normal to the surface
 (Warning: direction in/out, up/down is a matter of choice/convention)



Used for computing e.g.

$$1. \text{ area } \iint_S |d\bar{S}|$$

3D surface

$$2. \text{ total scalar e.g. charge } \iint_S \sigma |d\bar{S}| \quad \begin{matrix} \sigma \text{ is surface} \\ \text{density} \end{matrix}$$

$$3. \text{ "flux" through surface } \iint_S \mathbf{F} \cdot d\bar{S}$$

\mathbf{F} is any vector field.

e.g. far from Sun \mathbf{F} defines direction and rate of flow of energy per unit area $\perp r$ to \mathbf{F} .

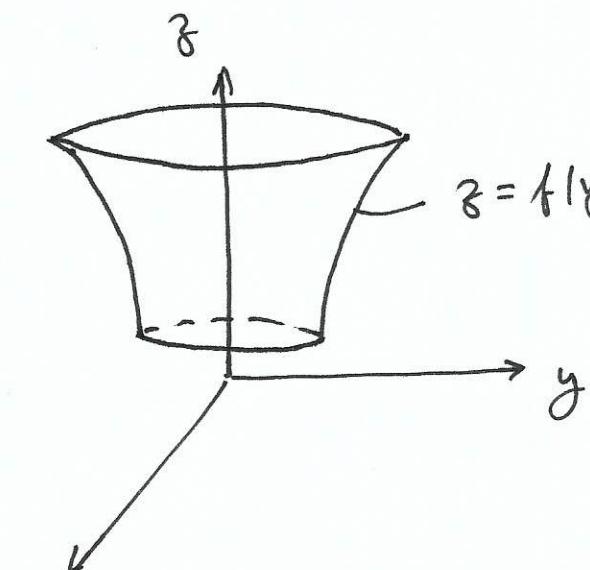
Then $\mathbf{F} \cdot d\bar{S}$ is the rate of flow of energy - the flux - through $d\bar{S}$.



Simple case: Surface of revolution (revision)

(36)

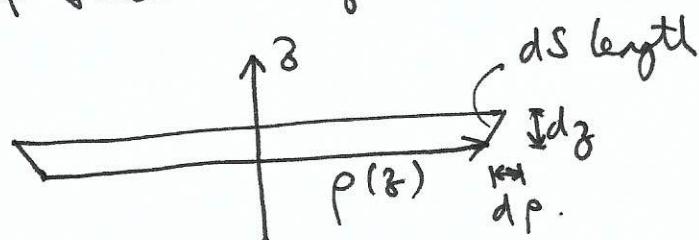
A curve rotated about an axis e.g. z



$z = f(y)$ rotated i.e. $z = f(\rho)$

e.g. curve $z = y^{\frac{1}{2}}$
rotated $z = \rho^{\frac{1}{2}}$ (cylindrical
coords)
or invert $\rho = z^2$

A slice in z



volume:

$$dV = \pi \rho^2(z) dz$$

$$V = \pi \int \rho^2(z) dz$$

Surface area of loop

$$dA = 2\pi \rho(z) ds$$

ds , not $d\rho$ or dz !

now $ds^2 = d\rho^2 + dz^2 = d\rho^2 \left(1 + \frac{dz^2}{d\rho^2}\right) = dz^2 \left(1 + \frac{d\rho^2}{dz^2}\right)$

$$\therefore ds = d\rho \left(1 + \left(\frac{d\rho}{dz}\right)^2\right)^{\frac{1}{2}} = dz \left(1 + \left(\frac{d\rho}{dz}\right)^2\right)^{\frac{1}{2}}$$

choose one

e.g. $A = 2\pi \int_{z=z_{\min}}^{z_{\max}} \rho(z) \left[1 + \left(\frac{d\rho}{dz}\right)^2\right]^{\frac{1}{2}} dz$

use this one in the Seminar

General method

Big idea: the position vector \underline{r} of a point on a surface may be expressed using only 2 coordinates

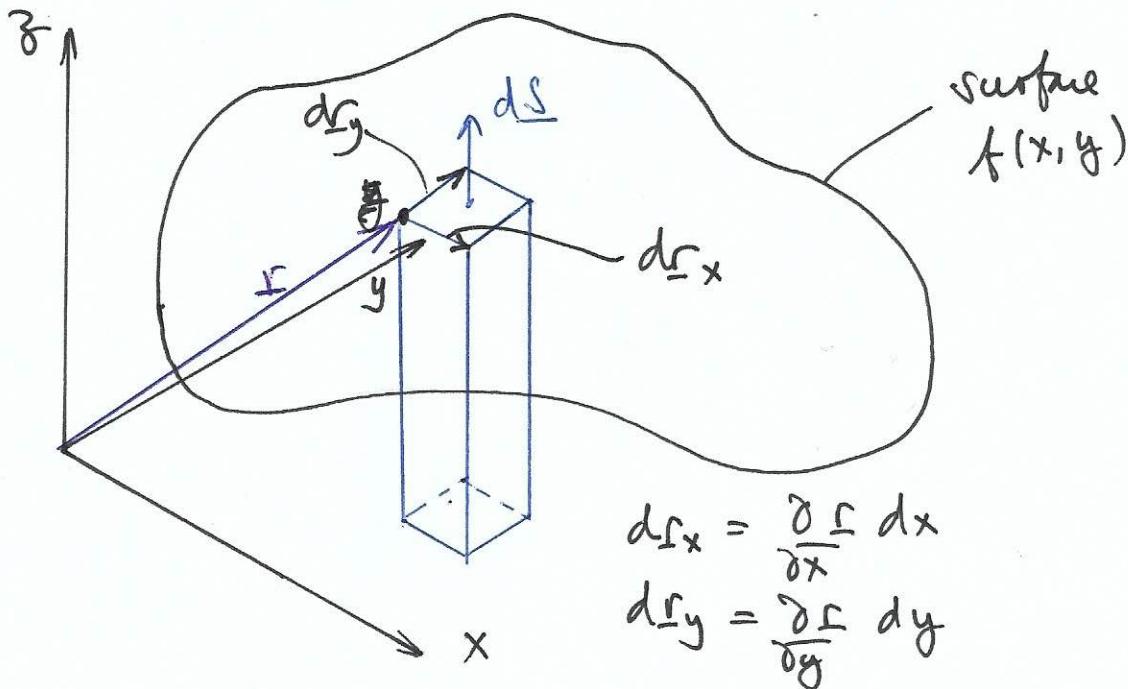
e.g. in Cartesian coords,

$$\text{position vector } \underline{r} = x \hat{i} + y \hat{j} + z \hat{k}$$

surface defined by e.g. $z = f(x, y)$

so vector to surface

$$\underline{r}(x, y) = x \hat{i} + y \hat{j} + f(x, y) \hat{k}$$



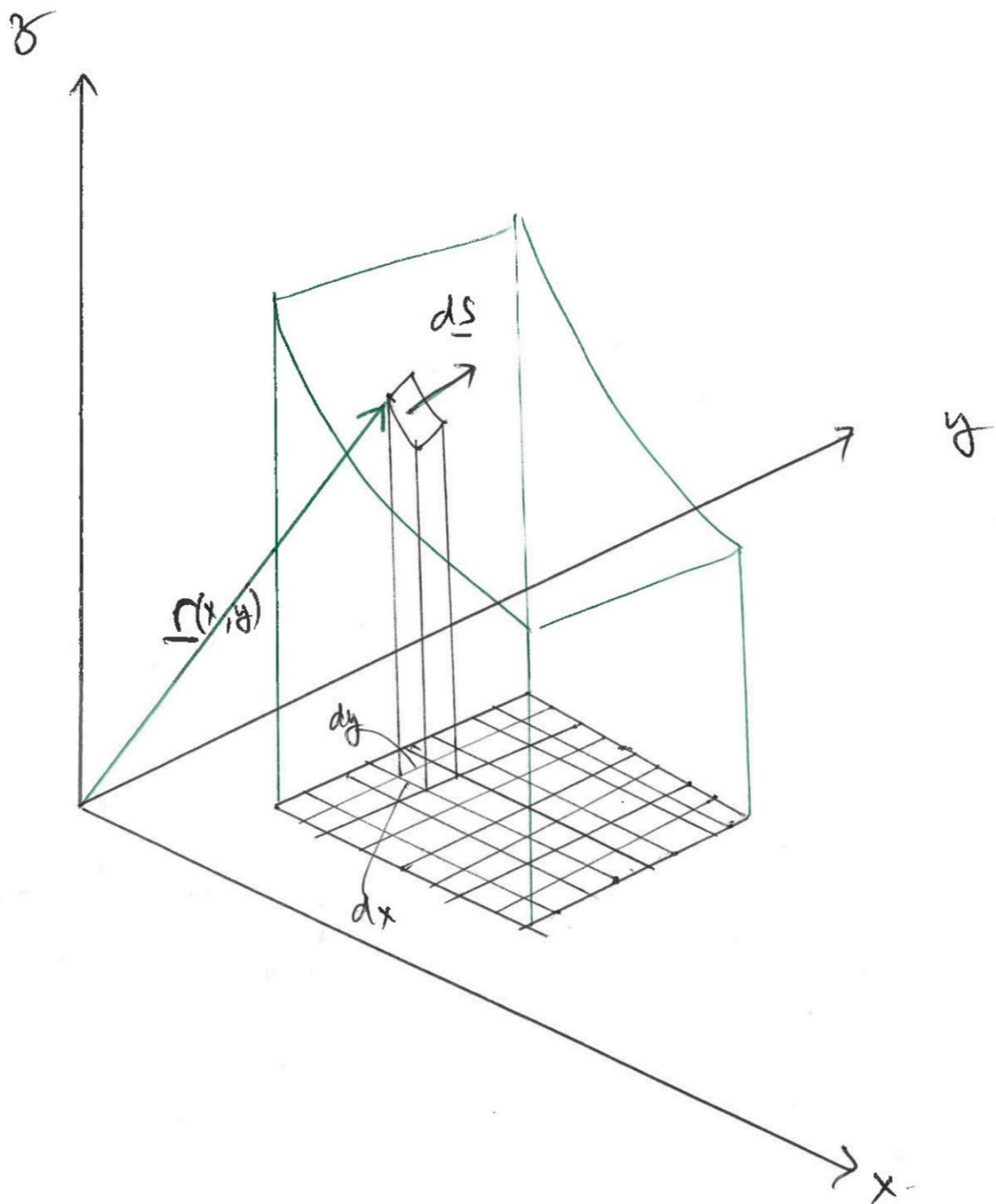
$$dr_x = \frac{\partial \underline{r}}{\partial x} dx$$

$$dr_y = \frac{\partial \underline{r}}{\partial y} dy$$

On Surface

$$ds = \left(\frac{\partial \underline{r}}{\partial x} \times \frac{\partial \underline{r}}{\partial y} \right) dx dy = N dx dy$$

(you may want $-ds$ depending on the question)



More generally we can express the vector
to the surface in terms of 2 variables u, v
then:

$$d\vec{S} = \left(\frac{\partial \vec{r}}{\partial u} \times \frac{\partial \vec{r}}{\partial v} \right) du dv$$

REMEMBER

e.g. x, y or y, z

or ρ, ϕ or θ, ϕ

close for convenience

e.g. in cylindrical polar coordinates

position vector $\vec{r} = \rho \hat{f}(\phi) + z \hat{k}$

surface e.g. $z = f(\rho, \phi)$

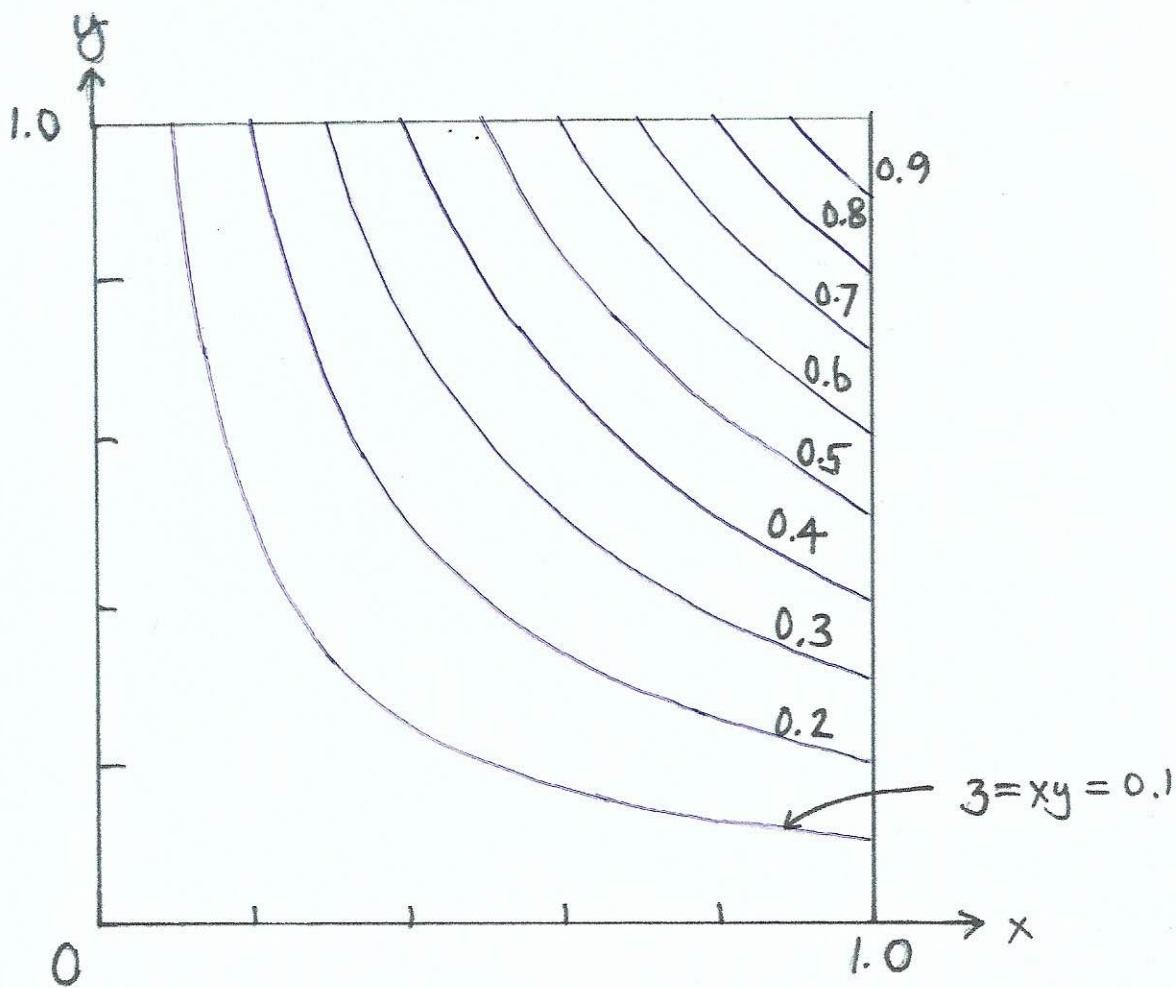
vector to surface $\vec{r}(\rho, \phi) = \rho \hat{f}(\phi) + f(\rho, \phi) \hat{k}$

$$d\vec{S} = \left(\frac{\partial \vec{r}}{\partial \rho} \times \frac{\partial \vec{r}}{\partial \phi} \right) d\rho d\phi$$

or express $\vec{r}(\rho, \phi) \approx \vec{r}(\phi, z)$

Examplesurface $z = f(x, y) = xy$ vector field $\mathbf{F} = x^2 \hat{i} + y^2 \hat{j}$ find the flux into the surface

$$\iint_S \mathbf{F} \cdot d\mathbf{S} \quad \text{over} \quad \begin{aligned} 0 < x < 1 \\ 0 < y < 1 \end{aligned}$$



Key step express \underline{S} to the surface in terms of
just two variables from x, y, z

$$\underline{S} = x \hat{i} + y \hat{j} + xy \hat{k} \quad x \text{ and } y \\ x = u \quad y = v$$

[or $\underline{r} = x \hat{i} + \frac{z}{x} \hat{j} + z \hat{k} \quad x \text{ and } z$]

$$\frac{\partial \underline{r}}{\partial x} = \hat{i} + 0 \hat{j} + y \hat{k}$$

$$\frac{\partial \underline{r}}{\partial y} = 0 \hat{i} + \hat{j} + x \hat{k}$$

$$\underline{N} = \frac{\partial \underline{r}}{\partial x} \times \frac{\partial \underline{r}}{\partial y} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ 1 & 0 & y \\ 0 & 1 & x \end{vmatrix} = -y \hat{i} - x \hat{j} + \hat{k}$$

$$d\underline{S} = \underline{N} dx dy = (-y \hat{i} - x \hat{j} + \hat{k}) dx dy$$

check the sign : to get flux into the surface

we want $-\underline{E} \cdot d\underline{S}$

$$-\underline{E} \cdot d\underline{S} = (x^2 \hat{i} + y^2 \hat{j} + 0 \hat{k}) \cdot (y \hat{i} + x \hat{j} - \hat{k}) dx dy$$

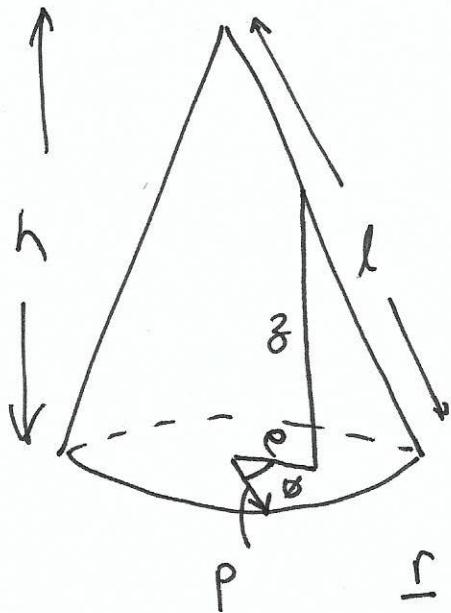
$$-\underline{E} \cdot d\underline{S} = (x^2 y + y^2 x) dx dy$$

$$\text{total flux} = \iint_{\substack{y=0 \\ x=0}}^{ } (x^2 y + y^2 x) dx dy = I$$

..... you check ... $I = \frac{1}{3}$

Example 2 Surface area (sloping part)
of a cone - the hard way!

$$[\text{we know } A = \pi p \sqrt{h^2 + p^2} = \pi p l]$$



$$\text{on surface: } p = r \left(1 - \frac{\phi}{\pi}\right)$$

$$z = \left(1 - \frac{\phi}{\pi}\right)^h$$

express Σ to surface in
terms of p, ϕ, z only

$$\Sigma(p, \phi, z) = p \hat{f}(\phi) + z \hat{k}$$

$$\Sigma(p, \phi) = p \hat{f}(\phi) + \left(1 - \frac{\phi}{\pi}\right)^h \hat{k}$$

$$\frac{\partial \Sigma}{\partial p} = \hat{f} - \frac{h}{p} \hat{k}$$

$$\frac{\partial \Sigma}{\partial \phi} = p \hat{\phi} \quad \left(\frac{\partial \hat{f}}{\partial \phi} = \hat{\phi} \right)$$

$$\frac{\partial \Sigma}{\partial p} \times \frac{\partial \Sigma}{\partial \phi} = \begin{vmatrix} \hat{f} & \hat{\phi} & \hat{k} \\ 1 & 0 & -\frac{h}{p} \\ 0 & p & 0 \end{vmatrix} = \frac{h}{p} p \hat{f} + p \hat{k} = N$$

$$d\Sigma = \left(\frac{h}{p} \hat{f} + p \hat{k} \right) dp d\phi$$

$$|d\Sigma| = p \cdot \left(1 + \frac{h^2}{p^2}\right)^{\frac{1}{2}} dp d\phi$$

$$= \boxed{\frac{l}{p}}$$

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$$A = \iint_S |dS| = \int_0^P \int_0^{2\pi} \frac{\rho l}{P} d\phi d\rho$$

$$A = 2\pi \frac{l}{P} \left[\frac{\rho^2}{2} \right]_0^P = \pi Pl \quad \text{as expected}$$

Section 4 Line integral

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Integral along a path, a curve C , in space.

Different forms, e.g.:

$$\int_C r \, d\Gamma \quad \int_C \underline{F} \cdot d\Gamma \quad \int_C \underline{F} \times d\Gamma$$

↑
curve
scalar

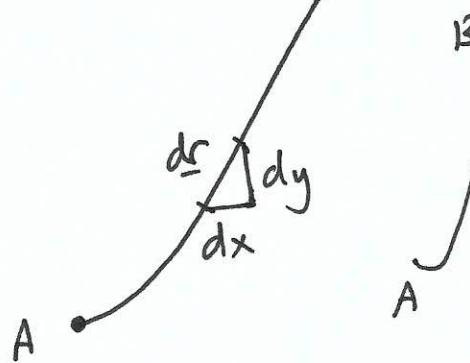
we are particularly interested in this one

e.g. $\underline{F} \cdot d\Gamma = W$ work done

4.1 How to calculate (2D)

We have a curve $y = y(x)$, or equivalently $x = x(y)$
 and a vector field $\underline{F}(x, y) = F_x(x, y) \hat{i} + F_y(x, y) \hat{j}$

$$d\Gamma = dx \hat{i} + dy \hat{j}$$



$$\int_C \underline{F} \cdot d\Gamma = \sum_i F_{x_i}(x_i, y_i) dx_i + F_{y_i}(x_i, y_i) dy_i \quad (1) \quad (2)$$

* Using the curve we can write each term entirely using only x or only y i.e. integrate w.r.t. x or y

(Same is true in 3D because a point on a line is defined by only one coordinate)

e.g. $z = x + y \quad y = x^2$ defines a line in 3D
 $\therefore z = x + x^2 = y^{1/2} + y$

e.g. ② may be expressed

$$\int_{y_A}^{y_B} F_y(x(y), y) dy \quad \text{or} \quad \int_{x_A}^{x_B} F_y(x, y(x)) \frac{dy}{dx} (x \cancel{y(x)}) dx$$

① may be expressed

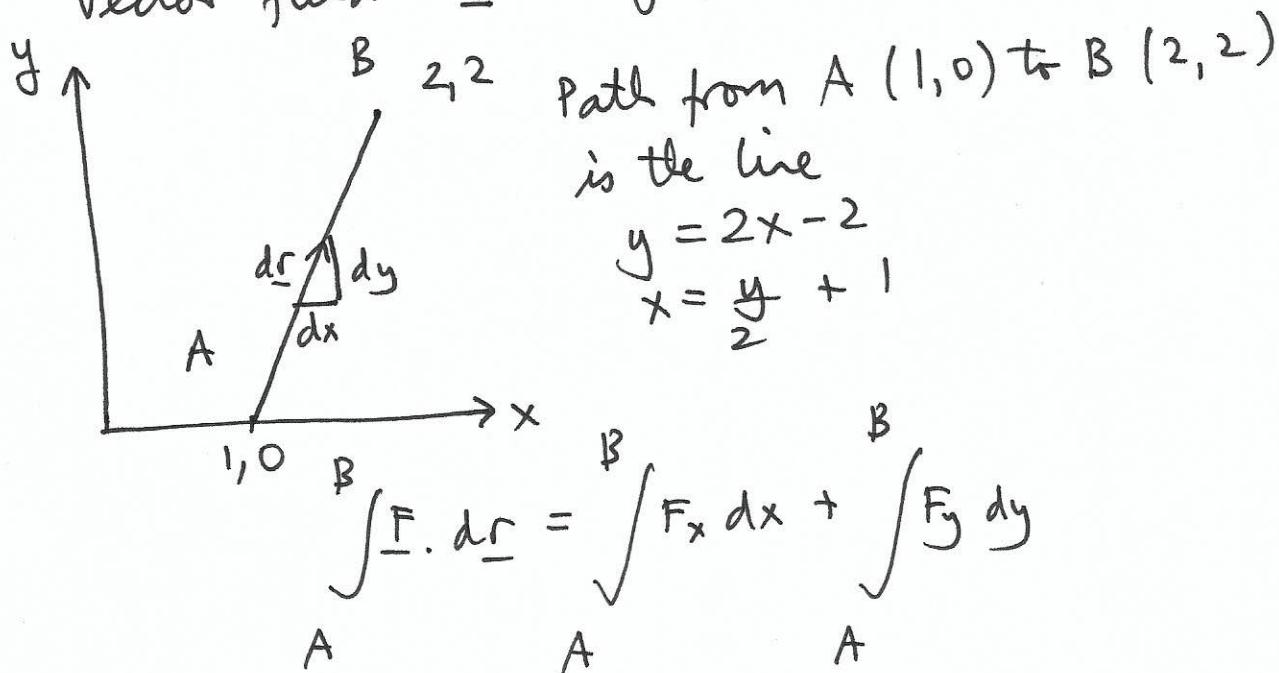
$$\int_{x_A}^{x_B} F_x(x, y(x)) dx \quad \text{or} \quad \int_{y_A}^{y_B} F_x(x(y), y) dx (\cancel{x(y)} dy)$$

4.2 Four examples

Recipe: express each integral with one parameter using the curve, and set the limits for that parameter.

Example 1

Vector field $\mathbf{F} = 2xy \hat{i} + x^2 \hat{j}$



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$$\begin{aligned}
 I &= \int_C F \cdot d\vec{r} = \int_C 2xy \, dx + \int_C x^2 \, dy = I_1 + I_2 \\
 &\quad \text{or} \quad y = y(x) \quad dy = \frac{dy}{dx} dx = 2dx \\
 &= \int_1^2 2x(2x-2) \, dx + \int_0^2 \left(\frac{y}{2} + 1\right)^2 \, dy \quad \text{or} \quad \int_1^2 x^2 \, 2dx \\
 &\quad \uparrow \quad \uparrow \quad \uparrow \quad \text{alternative } I_2 \\
 &= \left[\frac{4x^3}{3} - 2x^2 \right]_1^2 + \left[\frac{y^3}{12} + \frac{y^2}{2} + y \right]_0^2 \quad \text{or} \quad \left[\frac{2}{3}x^3 \right]_1^2
 \end{aligned}$$

$$\begin{aligned}
 I &= \frac{10}{3} + \frac{14}{3} \quad \text{or} \quad \frac{14}{3} \quad \checkmark \\
 I_1 & \quad \quad I_2
 \end{aligned}$$

$$I = \frac{24}{3} = 8$$

Example 2. The line may be expressed

parametrically (where we cannot write $y = f(x)$)

e.g. $\begin{cases} x(t) = 2t + 1 \\ y(t) = 4t \end{cases}$ from $t=0$ to $t=\frac{1}{2}$

This is actually the line $y = 2x - 2$, from A to B, before!

need $dx = \frac{dx}{dt} dt = 2dt$ $dy = \frac{dy}{dt} dt = 4dt$

$$\begin{aligned} I &= \int E \, dx = \int_c^{\frac{1}{2}} 2xy \, dx + \int_c^{\frac{1}{2}} x^2 \, dy \\ &= \int_0^{\frac{1}{2}} 2(2t+1)4t \, 2dt + \int_0^{\frac{1}{2}} (2t+1)^2 4 \, dt \end{aligned}$$

you do algebra

$$= 16 \left[\frac{2t^3}{3} + \frac{t^2}{2} \right]_0^{\frac{1}{2}} + 4 \left[\frac{4}{3}t^3 + 2t^2 + t \right]_0^{\frac{1}{2}}$$

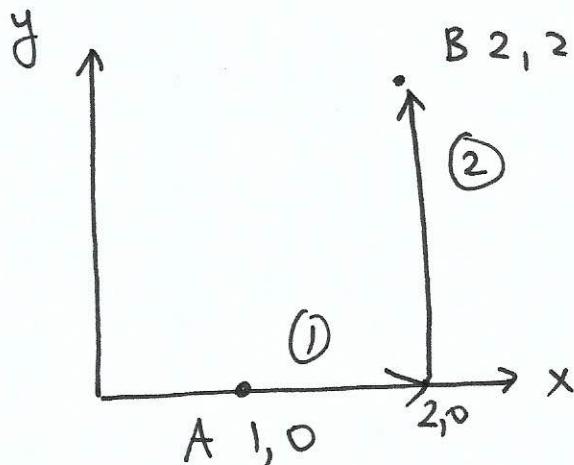
$$= \frac{10}{3} + \frac{14}{3}$$

I, ✓

I₂ ✓

Same as before

Example 3 Same \mathbf{F} , same end points A, B,
different path



path is along ①, then ②

$$\text{Along } ① \int_{\mathcal{C}} \mathbf{F} \cdot d\mathbf{r} = \int_{\mathcal{C}} 2xy \, dx + \int_{\mathcal{C}} x^2 \, dy$$

$I_1 = 0$ because
 $y = 0$

$I_2 = 0$ because
 $dy = 0$

$$\text{Along } ② \int_{\mathcal{C}} \mathbf{F} \cdot d\mathbf{r} = \int_{\mathcal{C}} 2xy \, dx + \int_{\mathcal{C}} x^2 \, dy$$

$I_1 = 0$ because
 $dx = 0$

For I_2 , sub $x = 2$

$$I_2 = \int_{y=0}^2 4 \, dy = [4y]_0^2 = 8$$

$$I = I_1 + I_2 = \underbrace{0 + 0}_{I_1} + \underbrace{0 + 8}_{I_2} = 8 \text{ same as before}$$

Example 4 Plane polar coords. Same end

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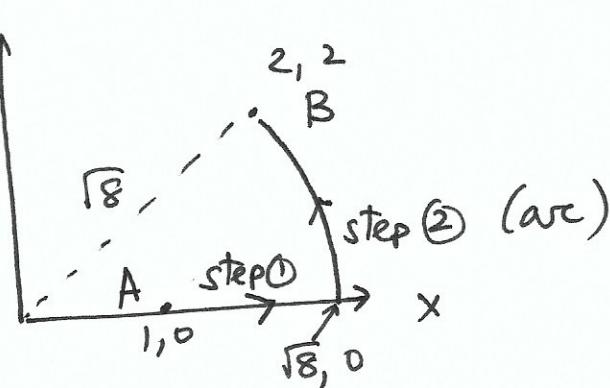
points, different path.
[Messy, ^{awkward} coords for this ^{vector field} problem, just to show it can be done]

Step 1 $\phi = 0, 1 \leq \rho \leq \sqrt{8}$

Step 2 $\rho = \sqrt{8}, 0 \leq \phi \leq \frac{\pi}{4}$

curve

limits



$$\text{we have } \underline{F} \cdot d\underline{r} = 2xy dx + x^2 dy$$

$$x = \rho \cos \phi \quad y = \rho \sin \phi$$

$$\text{e.g. } dx = \frac{\partial x}{\partial \rho} d\rho + \frac{\partial x}{\partial \phi} d\phi$$

change variable, messy, done for you

$$\rightarrow \int_C \underline{F} \cdot d\underline{r} = \int_1^{\sqrt{8}} 3 \cos^2 \phi \sin \phi \rho^2 d\rho + \int_0^{\frac{\pi}{4}} \cos \phi (1 - 3 \sin^2 \phi) \rho^3 d\phi$$

$$= I_1 + I_2$$

$$\begin{aligned} \text{Step 1} \quad \phi = 0, \sin \phi = 0 & \quad \therefore I_1 = 0 \\ d\phi = 0 & \quad \therefore I_2 = 0 \end{aligned}$$

$$\text{Step 2} \quad d\rho = 0 \quad \therefore I_1 = 0$$

$$I = I_2 = \int_0^{\frac{\pi}{4}} \rho^3 (\cos \phi - 3 \cos \phi \sin^2 \phi) d\phi \quad \rho = \sqrt{8} \text{ const}$$

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$$I = 8\sqrt{8} [\sin \phi - \sin^3 \phi]_0^{\pi/4}$$

$$= 8\sqrt{8} \left[\frac{1}{\sqrt{2}} - \frac{1}{2\sqrt{2}} \right]$$

$$= 8\sqrt{8} \left[\frac{2}{\sqrt{8}} - \frac{1}{\sqrt{8}} \right] = 8$$

independent of path

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4.2 Line integrals $\int \underline{F} \cdot d\underline{r}$, between the same end points, that are independent of the path

Summary of previous calcs:

$$\underline{F}_1 = 2xy \hat{i} + x^2 \hat{j}$$

$$\boxed{\underline{F}_1 \cdot d\underline{r} = 2xy dx + x^2 dy} \quad \text{Eqn ①}$$

start A = (1, 0) end B = (2, 2)

$$\int_C \underline{F}_1 \cdot d\underline{r} = \int_C 2xy dx + \int_C x^2 dy = I_1 + I_2$$

Path 1 $y = 2x - 2$

$$I = I_1 + I_2 = \frac{10}{3} + \frac{14}{3} = 8$$

Path 2 $y = 0 \quad 1 \leq x \leq 2$, then $x=2 \quad 0 \leq y \leq 2$

$$I = I_1 + I_2 = 0 + 8 = 8$$

I is independent of the path

Now consider:

$$\underline{F}_2 = 2xy \hat{i} - x^2 \hat{j}$$

$$\boxed{\underline{F}_2 \cdot d\underline{r} = 2xy dx - x^2 dy} \quad \text{Eqn ②}$$

Path 1 $I = I_1 + I_2 = \frac{10}{3} - \frac{14}{3} = -\frac{4}{3}$

Path 2 $I = I_1 + I_2 = 0 - 8 = -8$

I depends on the path

The big idea:

Eqn ① is an exact differential
check mixed second partial derivatives

$$\frac{\partial}{\partial y} (2xy) = 2x \quad \frac{\partial}{\partial x} (x^2) = 2x \quad \checkmark$$

There is a parent function $\underline{r}(x,y)$

$$\int_{\underline{F}_1} \underline{d\underline{r}} = \int_c^{2xy} dx + \int_c^{x^2} dy = \int d\underline{r}(x,y) = \underline{r}_B(x,y) - \underline{r}_A(x,y)$$

The path does not matter, only the end points

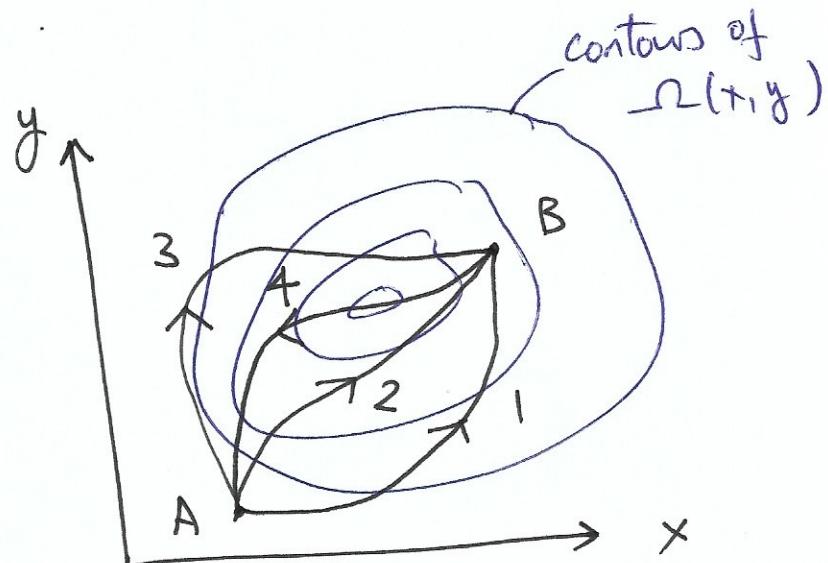
$$\underline{r} = x^2y + c \quad (\text{Lecture 1})$$

$$\text{check: } d\underline{r} = \frac{\partial \underline{r}}{\partial x} dx + \frac{\partial \underline{r}}{\partial y} dy = 2xy dx + x^2 dy$$

$$\begin{aligned} \underline{r}_B - \underline{r}_A &= [x^2y + c]_{B=(2,2)} - [x^2y + c]_{A=(1,0)} \\ &= 8 + c - 0 - c = 8 \quad \checkmark \end{aligned}$$

the line integral
calculates the
"change in height"

$$\int_A^B d\underline{r} = \underline{r}_B - \underline{r}_A$$



Eqn 2 is not an exact differential.

$$\int_{\text{path 1}} \underline{F}_1 \cdot d\underline{r} = \underline{r}_B - \underline{r}_A$$

$$\int_{\text{path 4}} \underline{F}_1 \cdot d\underline{r} = \underline{r}_A - \underline{r}_B$$

$$\int_{\text{path 1}} \underline{F}_1 \cdot d\underline{r} + \int_{\text{path 4}} \underline{F}_1 \cdot d\underline{r} = 0 = \oint_C \underline{F}_1 \cdot d\underline{r} = 0$$

closed path or loop

The integral of an exact differential around a closed path is 0.

We call \underline{F}_1 "conservative" - no work done around loop

Summary of 4.2 All statements equivalent - if one is true, all are true

- (1) $\underline{F} \cdot d\underline{r}$ is an exact differential
- (2) $\underline{F} = \frac{\partial \underline{r}}{\partial x} \hat{i} + \frac{\partial \underline{r}}{\partial y} \hat{j} + \frac{\partial \underline{r}}{\partial z} \hat{k}$ for some \underline{r}
- (3) $\int \underline{F} \cdot d\underline{r}$ from A to B does not depend on path
- (4) $\oint_C \underline{F} \cdot d\underline{r} = 0$
- (5) \underline{F} is conservative

5. Gradient $\text{grad } \Omega$ or $\nabla \Omega$

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5.1 Definition

From a scalar field $\Omega(x, y, z)$, the vector field

$$\underline{F} = \frac{\partial \Omega}{\partial x} \hat{i} + \frac{\partial \Omega}{\partial y} \hat{j} + \frac{\partial \Omega}{\partial z} \hat{k} = \text{grad } \Omega = \nabla \Omega$$

is conservative i.e. $\oint \underline{F} \cdot d\underline{r} = 0$.

The symbol ∇ "del" (or "nabla") is an operator,

$$\nabla = \hat{i} \frac{\partial}{\partial x} + \hat{j} \frac{\partial}{\partial y} + \hat{k} \frac{\partial}{\partial z}$$

Operating on a ~~scalar~~^{field}, it produces a vector field.

Here Ω (often Φ in physics) is the potential associated with the vector field \underline{F} .

[N.B. Take care over sign e.g. the gravitational field $\underline{g} = -\nabla \Phi$. But force doing work $\underline{F} = -m\underline{g}$]

S.2 Directional derivative

Using ∇r we can calculate the derivative of r in any direction.

We can write

$$dr = \frac{\partial r}{\partial x} dx + \frac{\partial r}{\partial y} dy + \frac{\partial r}{\partial z} dz = \nabla r \cdot d\underline{r}$$

What is derivative in particular direction \hat{a} ?

If we move distance dS , then

$$dr = \nabla r \cdot \hat{a} dS$$

Rate of change

$$\frac{dr}{dS} = \nabla r \cdot \hat{a} = \text{directional derivative}$$

e.g. choose $\hat{a} = \hat{k}$

$$\frac{dr}{dS} = \left(\hat{i} \frac{\partial r}{\partial x} + \hat{j} \frac{\partial r}{\partial y} + \hat{k} \frac{\partial r}{\partial z} \right) \cdot \hat{k} = \frac{\partial r}{\partial z}$$

as expected

At a particular point x_1, y_1, z_1

What direction \hat{a}_{\max} is $\frac{dr}{dS}$ maximum? (steepest gradient)

evidently

$$\hat{a}_{\max} = \frac{\nabla r}{|\nabla r|}$$

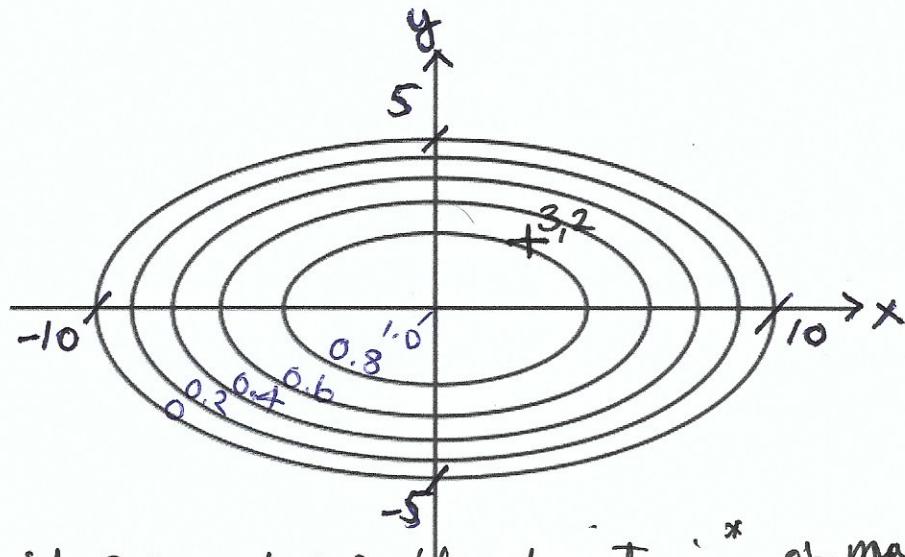
Steepest gradient is $|\nabla r|$

Example (2D)

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$$z = g(x, y) = 1 - \frac{x^2}{100} - \frac{y^2}{25}$$

an elliptical hill (!) units are km



- ① At the point $3, 2$ what is the direction* of max. gradient, and the value of the gradient?

* a unit vector

$$\nabla z = \hat{i} \frac{\partial z}{\partial x} + \hat{j} \frac{\partial z}{\partial y} = -\frac{x}{50} \hat{i} - \frac{2y}{25} \hat{j} \quad \text{N.B. it's a 2D vector}$$

$$x = 3, y = 2$$

$$\nabla z(3, 2) = -\frac{3}{50} \hat{i} - \frac{4}{25} \hat{j} = -0.06 \hat{i} - 0.16 \hat{j}$$

$$\text{magnitude} = \sqrt{(0.06^2 + 0.16^2)} = 0.17$$

$$\text{direction } \hat{a} = \frac{-0.06}{0.17} \hat{i} - \frac{0.16}{0.17} \hat{j}$$

- ② At $3, 2$, in the direction of $\hat{i} + \hat{j}$, what is the derivative?

$$\hat{a} = \frac{\hat{i}}{\sqrt{2}} + \frac{\hat{j}}{\sqrt{2}} \text{ unit vector}$$

$$\nabla z \cdot \hat{a} = (-0.06 \hat{i} - 0.16 \hat{j}) \cdot \left(\frac{\hat{i}}{\sqrt{2}} + \frac{\hat{j}}{\sqrt{2}}\right)$$

$$= -\frac{0.06}{\sqrt{2}} - \frac{0.16}{\sqrt{2}} = -0.155 \quad (\text{it's downhill})$$

5.3

 $\nabla \cdot \underline{r}$ in other coordinate systems

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generally $d\underline{r} = \nabla \cdot \underline{r} \cdot d\underline{r}$

Derive $\nabla \cdot \underline{r}$ in cylindrical polar

$$d\underline{r} = \frac{\partial \underline{r}}{\partial p} dp + \frac{\partial \underline{r}}{\partial \phi} d\phi + \frac{\partial \underline{r}}{\partial z} dz$$

$$d\underline{r} = dp \hat{f} + p d\phi \hat{\phi} + dz \hat{k}$$

$$\therefore \nabla \cdot (\underline{r}, \phi, z) = \frac{\partial}{\partial p} \hat{f} + \frac{1}{p} \frac{\partial}{\partial \phi} \hat{\phi} + \frac{\partial}{\partial z} \hat{k}$$

spherical polar

prove to yourself that

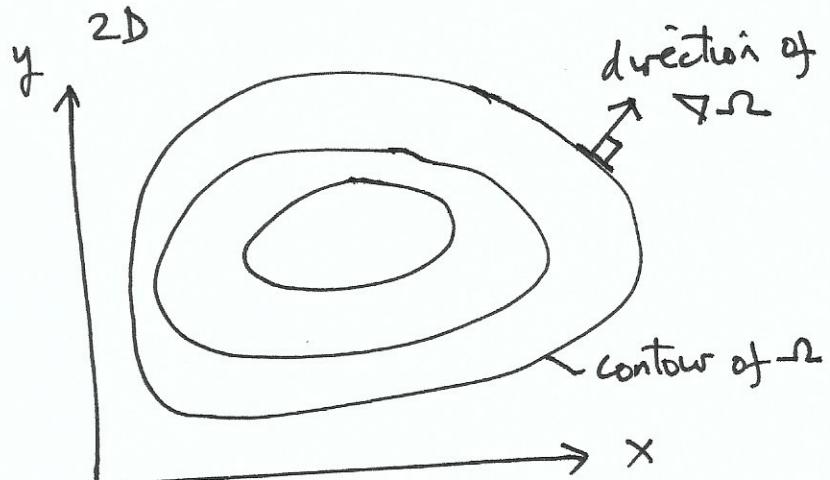
$$\nabla \cdot (\underline{r}, \theta, \phi) = \frac{\partial}{\partial r} \hat{r} + \frac{1}{r} \frac{\partial}{\partial \theta} \hat{\theta} + \frac{1}{r \sin \theta} \frac{\partial}{\partial \phi} \hat{\phi}$$

5.4 $\nabla \varphi$ and the normal to a surface

$$\text{In 2D } \frac{d\varphi}{ds} = \nabla \varphi \cdot \hat{\mathbf{a}}$$

$$\text{along a contour } \frac{d\varphi}{ds} = 0$$

$\therefore \nabla \varphi$ is \perp to line of constant φ



In 3D $\varphi(x, y, z)$, $\nabla \varphi$ is \perp to surface of constant φ .

$$\text{E.g. } \varphi = x^2 + y^2 + z^2, \quad \nabla \varphi = 2x \hat{i} + 2y \hat{j} + 2z \hat{k} = 2r \hat{s}$$

Now consider a 3D surface defined by $z = f(x, y)$. Suppose we want to find the direction normal to a point on the surface.

Key step: define $\varphi(x, y, z) = f(x, y) - z$

Then the surface is the surface $\varphi = 0 = \text{constant}$

\therefore A vector normal to the surface at point x, y, z is

$$\underline{n} = \nabla \varphi(x, y, z)$$

$$\text{unit vector } \hat{\underline{n}} = \frac{\underline{n}}{|\nabla \varphi|}$$

Example Section 3.5. For $z = xy$ we derived $\underline{N} = -y \hat{i} - x \hat{j} + \hat{k}$
so $\hat{\underline{n}} = \frac{\underline{N}}{|\underline{N}|}$ is unit vector \perp to surface

Use grad: define $\varphi = f(x, y) - z = xy - z$

$$\nabla \varphi = y \hat{i} + x \hat{j} - \hat{k} \quad \text{same as } \underline{N}$$

except for ambiguity of sign.

6. Divergence $\text{div } \underline{B}$ or $\nabla \cdot \underline{B}$

6.1 Definition

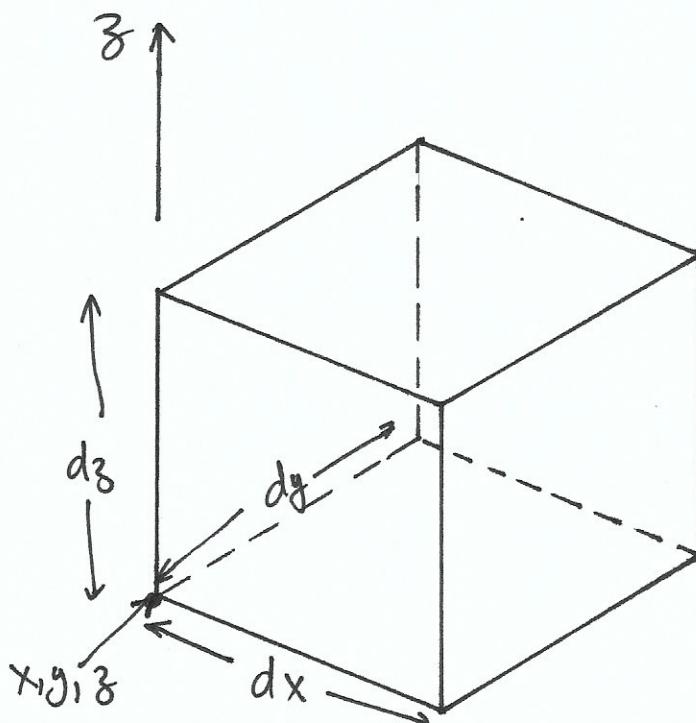
$$\nabla \cdot \underline{B} = \lim_{V \rightarrow 0} \left(\frac{1}{V} \oint_S \underline{B} \cdot d\underline{S} \right)$$

Closed surface, $d\underline{S}$ is out

so divergence is a "flux density"

Derive geometrically using Cartesian coordinates

$$\underline{B}(x, y, z) = B_x \hat{i} + B_y \hat{j} + B_z \hat{k}$$



Face	$d\underline{S}$
① $\Delta x = 0$	$-\hat{i} dy dz$
② $\Delta x = dx$	$\hat{i} dy dz$
③ $\Delta y = 0$	$-\hat{j} dx dz$
④ $\Delta y = dy$	$\hat{j} dx dz$
⑤ $\Delta z = 0$	$-\hat{k} dx dy$
⑥ $\Delta z = dz$	$\hat{k} dx dy$

We want $\sum_{i=1}^6 F_i$ where F_i is flux out over face i .

We will compute F_i using tangent-plane approximation to \underline{B} over each face. Then F_i arbitrarily accurate as $dx, dy, dz \rightarrow 0$

On ① \hat{i} component of field varies as

$$B_x + \frac{\partial B_x}{\partial y} dy + \frac{\partial B_x}{\partial z} dz$$

Because planar, average value over face is value at centre

$$\therefore F_1 = - \left(B_x + \frac{\partial B_x}{\partial y} \frac{dy}{2} + \frac{\partial B_x}{\partial z} \frac{dz}{2} \right) dy dz = - \bar{B}_x dy dz$$

$$F_2 = \left(\bar{B}_{x1} + \frac{\partial \bar{B}_{x1}}{\partial x} dx \right) dx dy dz$$

$$F_1 + F_2 = \frac{\partial}{\partial x} \left(B_x + \frac{\partial B_x}{\partial y} \frac{dy}{2} + \frac{\partial B_x}{\partial z} \frac{dz}{2} \right) dx dy dz$$

There are analogous terms for $F_3 + F_4, F_5 + F_6$

$$\text{Now } \nabla \cdot \underline{B} = \lim_{dx, dy, dz \rightarrow 0} \frac{\sum_{i=1}^6 F_i}{dx dy dz}$$

$$= \lim_{dx, dy, dz \rightarrow 0} \left[\frac{\partial}{\partial x} \left(B_x + \frac{\partial B_x}{\partial y} \frac{dy}{2} + \frac{\partial B_x}{\partial z} \frac{dz}{2} \right) \right. \\ \left. + \frac{\partial}{\partial y} \left(B_y + \frac{\partial B_y}{\partial x} \frac{dx}{2} + \frac{\partial B_y}{\partial z} \frac{dz}{2} \right) \right. \\ \left. + \frac{\partial}{\partial z} \left(B_z + \frac{\partial B_z}{\partial x} \frac{dx}{2} + \frac{\partial B_z}{\partial y} \frac{dy}{2} \right) \right]$$

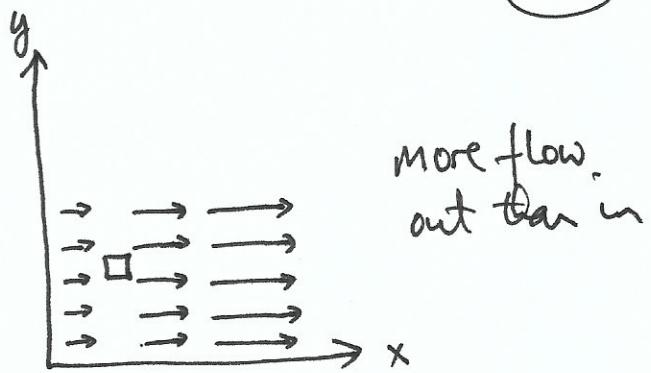
$$\nabla \cdot \underline{B} = \frac{\partial B_x}{\partial x} + \frac{\partial B_y}{\partial y} + \frac{\partial B_z}{\partial z} \quad (\text{rigorous})$$

[Note: terms varying across face not important,
only variations between faces]

Example ①

$$\underline{B} = \hat{i} ax$$

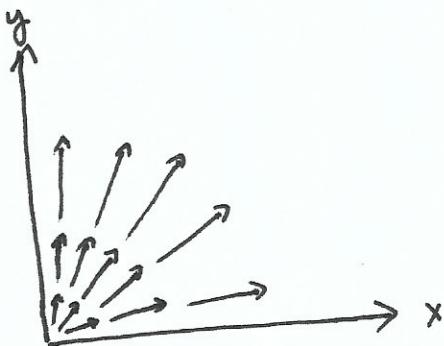
$$\nabla \cdot \underline{B} = \frac{\partial (ax)}{\partial x} + \frac{\partial (0)}{\partial y} + \frac{\partial (0)}{\partial z} = a \quad \text{everywhere}$$



Ex ②

$$\underline{B} = x \hat{i} + y \hat{j} + z \hat{k} = r \hat{r}$$

$$\nabla \cdot \underline{B} = 1 + 1 + 1 = 3 \quad \text{everywhere}$$



Ex ③ $\underline{B} = \hat{i} + \hat{j} + \hat{k}$ same everywhere

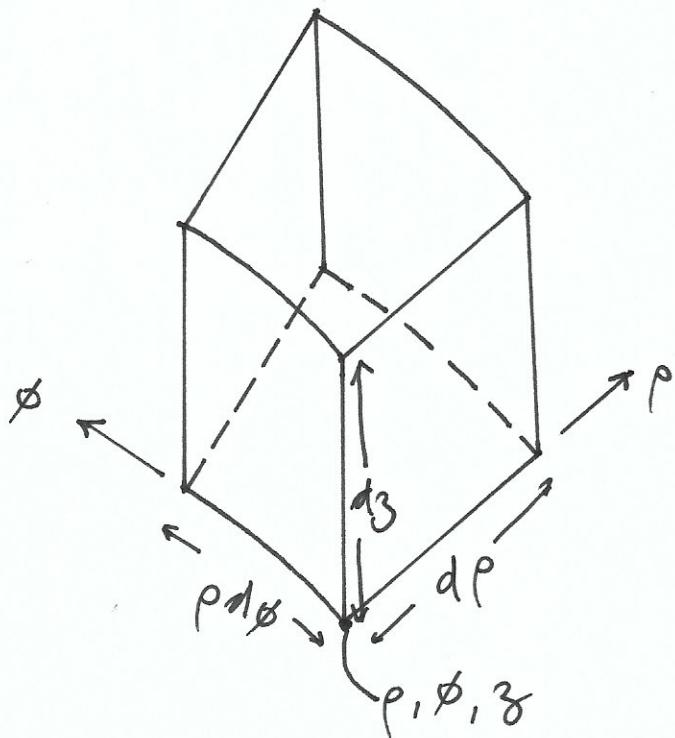
$$\nabla \cdot \underline{B} = 0 \quad \text{everywhere}$$

6.2 $\nabla \cdot \underline{B}$ in other coordinate systems

(61)

cylindrical coordinates - geometric derivation

$$\underline{B} = B_\rho \hat{\rho} + B_\phi \hat{\phi} + B_z \hat{z}$$



Face

- | | $d \underline{\Sigma}$ |
|-------------------------|---|
| ① $\Delta \rho = 0$ | $- \rho d\phi dz \hat{\rho}$ |
| ② $\Delta \rho = 1\rho$ | $(\rho + d\rho) d\phi dz \hat{\rho}$ |
| ③ $\Delta \phi = 0$ | $-1\rho dz \hat{\phi}$ |
| ④ $\Delta \phi = 1\phi$ | $1\rho dz \hat{\phi}$ |
| ⑤ $\Delta z = 0$ | $-\hat{z} \frac{1}{2}\phi [(\rho + d\rho)^2 - \rho^2] = -\rho d\phi d\rho \left[1 + \frac{d\rho}{2\rho}\right] \hat{z}$ |
| ⑥ $\Delta z = dz$ | $\rho d\phi d\rho \left[1 + \frac{d\rho}{2\rho}\right] \hat{z}$ |

From before, ignore variation over face e.g. $\frac{\partial B_p}{\partial \phi} \frac{d\phi}{2}$ on ① (62)

$$F_1 = -B_p \rho d\phi dz \quad F_2 = (B_p + \frac{\partial B_p}{\partial p} dp)(\rho + dp) d\phi dz$$

$$F_1 + F_2 = \left[\frac{B_p}{\rho} + \frac{\partial B_p}{\partial p} + \frac{\partial B_p}{\partial p} \frac{dp}{\rho} \right] \rho dp d\phi dz$$

$$F_3 = -B_\phi \rho dp dz \quad F_4 = \left[B_\phi + \frac{\partial B_\phi}{\partial \phi} d\phi \right] dp dz$$

$$F_3 + F_4 = \pm \frac{\partial B_\phi}{\partial \phi} \rho dp d\phi dz$$

$$F_5 = -B_3 \rho d\phi dp \left[1 + \frac{dp}{2\rho} \right]$$

$$F_6 = \left[B_3 + \frac{\partial B_3}{\partial z} dz \right] \rho d\phi dp \left[1 + \frac{dp}{2\rho} \right]$$

$$F_5 + F_6 = \frac{\partial B_3}{\partial z} \left[1 + \frac{dp}{2\rho} \right] \rho dp d\phi dz$$

$$\nabla \cdot \underline{B} = \lim_{\substack{dp dz d\phi \\ \rightarrow 0}} \frac{\sum F_i}{\sqrt{\rho dp d\phi dz}} = \frac{B_p}{\rho} + \frac{\partial B_p}{\partial p} + \frac{1}{\rho} \frac{\partial B_\phi}{\partial \phi} + \frac{\partial B_3}{\partial z}$$

$$\nabla \cdot \underline{B} = \frac{1}{\rho} \frac{\partial (\rho B_p)}{\partial p} + \frac{1}{\rho} \frac{\partial B_\phi}{\partial \phi} + \frac{\partial B_3}{\partial z}$$

Challenge: try the same in spherical polar:

$$\nabla \cdot \underline{B} = \frac{1}{r^2} \frac{\partial (r^2 B_r)}{\partial r} + \frac{1}{r \sin \theta} \frac{\partial (\sin \theta B_\theta)}{\partial \theta} + \frac{1}{r \sin \theta} \frac{\partial B_\phi}{\partial \phi}$$

What does $\nabla \cdot \underline{B}$ mean?

Cartesian

$$\nabla = \hat{i} \frac{\partial}{\partial x} + \hat{j} \frac{\partial}{\partial y} + \hat{k} \frac{\partial}{\partial z} \quad (\text{not a vector})$$

$$\underline{B} = \hat{i} B_x + \hat{j} B_y + \hat{k} B_z$$

$$\nabla \cdot \underline{B} = \frac{\partial B_x}{\partial x} + \frac{\partial B_y}{\partial y} + \frac{\partial B_z}{\partial z}$$

looks like dot product of 2 vectors

The bad news

Cylindrical

$$\nabla = \hat{r} \frac{\partial}{\partial r} + \frac{1}{r} \hat{\phi} \frac{\partial}{\partial \phi} + \hat{z} \frac{\partial}{\partial z}$$

$$\underline{B} = \hat{r} B_r + \hat{\phi} B_\phi + \hat{z} B_z$$

$$\nabla \cdot \underline{B} = \frac{B_r}{r} + \frac{\partial B_r}{\partial r} + \frac{1}{r} \frac{\partial B_\phi}{\partial \phi} + \frac{\partial B_z}{\partial z}$$

extra term?!

$\nabla \cdot \underline{B}$ not a dot product of two vectors

"abuse of notation"

- it's just shorthand for divergence

The good news . . .

Think of $\nabla \cdot \underline{B}$ as "differentiate first,
dot product second"

Cartesian

$$\nabla \cdot \underline{B} = \hat{i} \cdot \frac{\partial \underline{B}}{\partial x} + \hat{j} \cdot \frac{\partial \underline{B}}{\partial y} + \hat{k} \cdot \frac{\partial \underline{B}}{\partial z}$$

looks like grad

$$\nabla \phi = \hat{i} \frac{\partial \phi}{\partial x} + \hat{j} \frac{\partial \phi}{\partial y} + \hat{k} \frac{\partial \phi}{\partial z}$$

check e.g. first term

$$\frac{\partial \underline{B}}{\partial x} = \hat{i} \frac{\partial B_x}{\partial x} + \hat{j} \frac{\partial B_y}{\partial x} + \hat{k} \frac{\partial B_z}{\partial x}$$

$$\hat{i} \cdot \frac{\partial \underline{B}}{\partial x} = \frac{\partial B_x}{\partial x} \quad \checkmark$$

This idea works for cylindrical, spherical
div, curl

curl is "differentiate first, cross product second"

Analytic derivation of $\nabla \cdot \underline{B}$ is
cylindrical coordinates

$$\nabla = \hat{r} \frac{\partial}{\partial r} + \frac{1}{r} \hat{\phi} \frac{\partial}{\partial \phi} + \hat{z} \frac{\partial}{\partial z}$$

$$\underline{B} = \hat{r} B_r + \hat{\phi} B_\phi + \hat{z} B_z$$

"differentiate first, dot product second"

$$\nabla \cdot \underline{B} = \hat{r} \cdot \frac{\partial \underline{B}}{\partial r} + \frac{1}{r} \hat{\phi} \cdot \frac{\partial \underline{B}}{\partial \phi} + \hat{z} \cdot \frac{\partial \underline{B}}{\partial z}$$

recall $\hat{r}(\phi)$, $\hat{\phi}(\phi)$, $\frac{\partial \hat{r}}{\partial \phi} = \hat{\phi}$, $\frac{\partial \hat{\phi}}{\partial \phi} = -\hat{r}$, $B_r(r, \phi, z)$
 $B_\phi(r, \phi, z)$
 $B_z(r, \phi, z)$

let

$$\frac{\partial \underline{B}}{\partial r} = \hat{r} \frac{\partial B_r}{\partial r} + \hat{\phi} \frac{\partial B_\phi}{\partial r} + \hat{z} \frac{\partial B_z}{\partial r}$$

$$\hat{r} \cdot \frac{\partial \underline{B}}{\partial r} = \frac{\partial B_r}{\partial r} \quad (1)$$

2nd

$$\frac{\partial \underline{B}}{\partial \phi} = \hat{\phi} B_r + \hat{r} \frac{\partial B_r}{\partial \phi} - \hat{r} B_\phi + \frac{1}{r} \frac{\partial B_\phi}{\partial \phi} + \hat{z} \frac{\partial B_z}{\partial \phi}$$

$$\frac{1}{r} \hat{\phi} \cdot \frac{\partial \underline{B}}{\partial \phi} = \left(\frac{B_r}{r} \right) + \frac{1}{r} \frac{\partial B_\phi}{\partial \phi} \quad (2) \quad \text{the extra term!}$$

3rd

$$\frac{\partial \underline{B}}{\partial z} = \hat{z} \frac{\partial B_r}{\partial z} + \hat{\phi} \frac{\partial B_\phi}{\partial z} + \hat{r} \frac{\partial B_z}{\partial z}$$

$$\hat{r} \cdot \frac{\partial \underline{B}}{\partial z} = \frac{\partial B_z}{\partial z} \quad (3)$$

summing

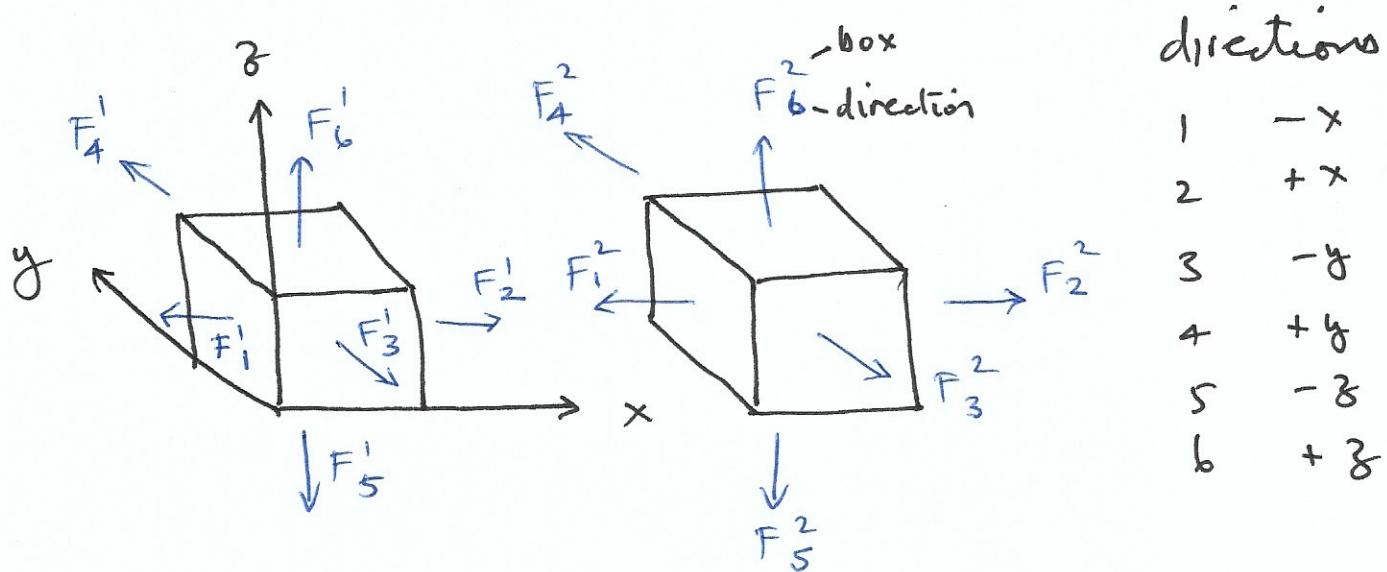
$$\nabla \cdot \underline{B} = \frac{\partial B_r}{\partial r} + \frac{B_r}{r} + \frac{1}{r} \frac{\partial B_\phi}{\partial \phi} + \frac{\partial B_z}{\partial z}$$

$$\nabla \cdot \underline{B} = \frac{1}{r} \frac{\partial}{\partial r} (r B_r) + \frac{1}{r} \frac{\partial B_\phi}{\partial \phi} + \frac{\partial B_z}{\partial z} \quad \text{as before}$$

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6.3 Divergence theorem (sometimes called Gauss' theorem, but not Gauss' law)

Consider 2 infinitesimal boxes, adjacent along x axis



on each face $\underline{F} = \underline{B} \cdot d\underline{S}$

$$\text{Box 1 } \sum_{i=1}^6 F_i^1 = \nabla \cdot \underline{B}_1 dV$$

$$\text{Box 2 } \sum_{i=1}^6 F_i^2 = \nabla \cdot \underline{B}_2 dV$$

note that $F_2^1 = -F_1^2$

Now push the two boxes together and sum $\underline{B} \cdot d\underline{S}$ over the surface

$$\sum F = \sum_{i=1}^6 F_i^1 + \sum_{i=1}^6 F_i^2 - F_2^1 - F_1^2 = \nabla \cdot \underline{B}_1 dV + \nabla \cdot \underline{B}_2 dV = 0$$

$$\therefore \sum \underline{B} \cdot d\underline{S} = \sum_{j=1}^2 \nabla \cdot \underline{B}_j dV$$

add more boxes to create a macroscopic volume

$$\iint_S \underline{B} \cdot d\underline{S} = \iiint \nabla \cdot \underline{B} dV \quad \text{the divergence theorem}$$

closed surface

(an integral theorem)

Example (sketch)

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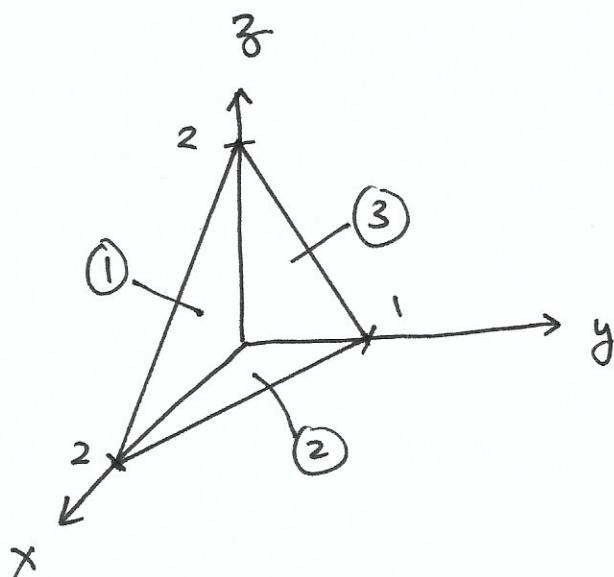
(Sometimes one integral is hard, so evaluate it by doing the other integral)

here we can do both

$$B = x^1 + y^2 + z^3$$

tetrahedron bound by

- (3) $x = 0$
 - (1) $y = 0$
 - (2) $z = 0$
 - (4) $z = 2 - x - 2y$ sloping surface



$$\oint_S \underline{B} \cdot d\underline{S} = \iiint_V \nabla \cdot \underline{B} \cdot dV$$

S closed surface RHS

sketch of answer

LHS $\stackrel{0_n}{\text{① ② ③}}$ easy to show $\underline{\underline{B}} \cdot d\underline{\underline{S}} = 0$

e.g. on ① $d \perp$ points in $-\hat{j}$ direction but $B_y = y \cancel{\perp} = 0$
 $\therefore B \cdot d \perp = 0$

on (4) find $dS = (\hat{L} + 2\hat{J} + \hat{K}) dx dy$
by standard method

$$\text{Then } \underline{B} \cdot d\underline{S} = (x+2y+z) dx dy = 2 dx dy$$

$$\textcircled{4} \quad \oint B \cdot dS = 2 \times \text{area of } \textcircled{2} = 2 = \text{LHS}$$

RHS

$$\nabla \cdot \underline{B} = \frac{\partial B_x}{\partial x} + \frac{\partial B_y}{\partial y} + \frac{\partial B_z}{\partial z} = 1 + 1 + 1 = 3$$

$$\therefore \iiint \nabla \cdot \underline{B} \cdot dV = 3 \times \text{vol. of tetrahedron}$$

$$V = \frac{1}{3} \text{base} \times \text{height} = \frac{1}{3} \times 1 \times 2$$

$$3 \times \text{vol} = 2 = \text{RHS}$$

$$\therefore \text{LHS} = \text{RHS} \text{ as expected}$$

Homework: check all the steps in this argument

6.4 Laplacian

$$\nabla \cdot \underline{r} = \hat{i} \frac{\partial r}{\partial x} + \hat{j} \frac{\partial r}{\partial y} + \hat{k} \frac{\partial r}{\partial z}$$

$$\nabla \cdot (\nabla \cdot \underline{r}) = \frac{\partial^2 r}{\partial x^2} + \frac{\partial^2 r}{\partial y^2} + \frac{\partial^2 r}{\partial z^2} = \nabla^2 r$$

∇^2 or "del squared" is called the Laplacian

seen e.g. in Laplace's equation $\nabla^2 u = 0$

and the wave equation $\nabla^2 u = \frac{1}{c^2} \frac{\partial^2 u}{\partial t^2}$

(if you like, derive Laplacian in cylindrical coords)

7. Curl $\nabla \times \underline{B}$

(69)

7.1 Green's theorem in the plane

$$\oint p(x, y) dx + Q(x, y) dy = \iint_R \frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} dx dy$$

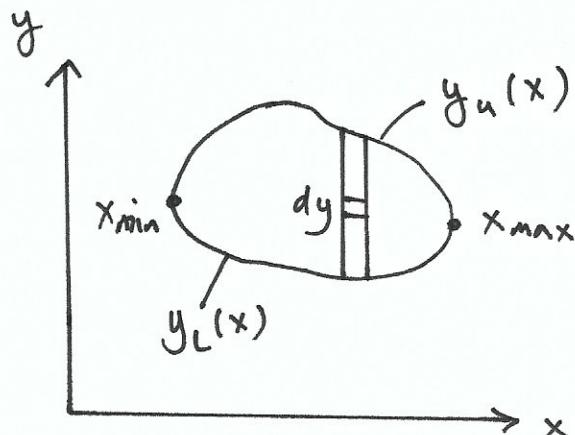
line integral, anticlockwise
looking down on plane x, y

double integral
over region enclosed

Proof Consider $I_1 = \iint \frac{\partial P}{\partial y} dy dx$

first step $- \int \frac{\partial P}{\partial y}(x, y) dy$
 $y = g_L(x)$

$$= -P(x, y_u) + P(x, y_L)$$



now add up slices

$$I_1 = - \int_{x_{\min}}^{x_{\max}} P(x, y_u) dx + \int_{x_{\min}}^{x_{\max}} P(x, y_L) dx$$

$$= + \int_{x_{\max}}^{x_{\min}} P(x, y_u) dx + \int_{x_{\min}}^{x_{\max}} P(x, y_L) dx = + \oint P dx$$

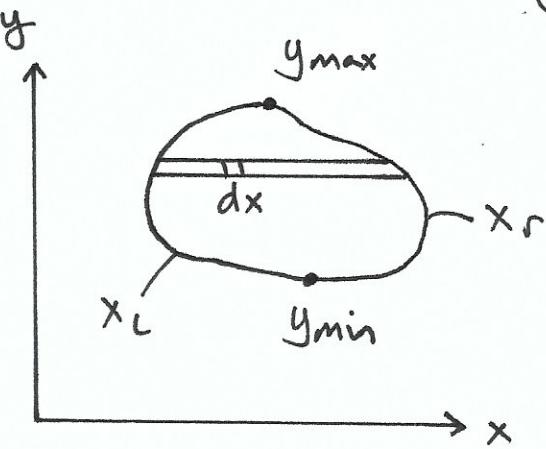
$$\therefore \oint P dx = - \iint \frac{\partial P}{\partial y} dy dx$$

similarly for $I_2 = \iint_R \frac{\partial Q}{\partial x} dx dy$

first step $\int \frac{\partial Q(x, y)}{\partial x} dx$
 $x = x_l(y)$

$$= Q(x_r, y) - Q(x_l, y)$$

$$I_2 = \int_{y=y_{\min}}^{y_{\max}} Q(x_r, y) dy + \int_{y=y_{\min}}^{y_{\max}} Q(x_l, y) dy = \oint Q dy$$



combining

$$\oint P dx + Q dy = \iint_R \frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} dx dy$$

P and Q can be any (continuous) function.

Very general!

Particular examples are of special interest to ~~vector calculus~~ electromagnetism.

4 ExamplesExample 1

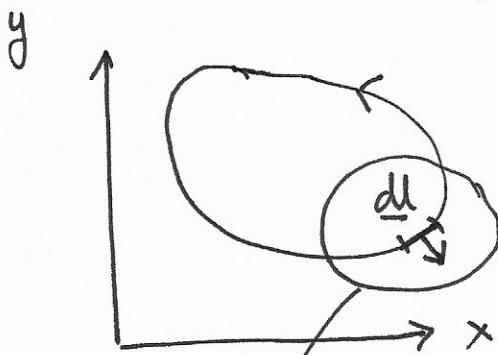
$Pdx + Qdy$ is an exact differential

$$\text{Then } \frac{\partial P}{\partial y} = \frac{\partial Q}{\partial x}$$

$$\therefore \oint Pdx + Qdy = \iint \frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} dx dy = 0$$

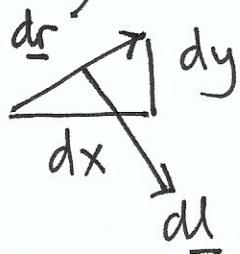
as expected!

Example 2 Consider 'flux' out of a closed loop in 2D
(2D equiv of $\oint_S \mathbf{B} \cdot d\mathbf{l}$)



vector field \underline{B}

we want $\oint \underline{B} \cdot d\underline{l}$



$d\underline{l} = dy \hat{i} - dx \hat{j}$ defines outward* vector of correct length

* for anticlockwise loop

$$\text{Then } \underline{B} \cdot d\underline{l} = (B_x \hat{i} + B_y \hat{j}) \cdot (dy \hat{i} - dx \hat{j})$$

$$\oint \underline{B} \cdot d\underline{l} = \oint -B_y dx + B_x dy$$

$$\oint \underline{B} \cdot d\underline{l} = \iint \frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \, dx \, dy = \iint \frac{\partial B_x}{\partial x} + \frac{\partial B_y}{\partial y} \, dx \, dy$$

the divergence theorem in 2 dimensions

Example 3

More generally, 'work done' line integral

$$\oint \underline{F} \cdot d\underline{r} = \oint F_x dx + F_y dy$$

$$= \iint \frac{\partial F_y}{\partial x} - \frac{\partial F_x}{\partial y} \, dx \, dy$$

= Stokes' theorem (L17) in 2D

Example 4 can replace a line integral
with a 2D integral (and vice versa)

Recall line integral in Section 4.2

$$\underline{F}_2 = 2xy \hat{i} - x^2 \hat{j}$$

We computed $\int_C \underline{F} \cdot d\underline{r}$ along :

$$\text{path (1)} \int_A^B \underline{F} \cdot d\underline{r} = -\frac{4}{3}$$

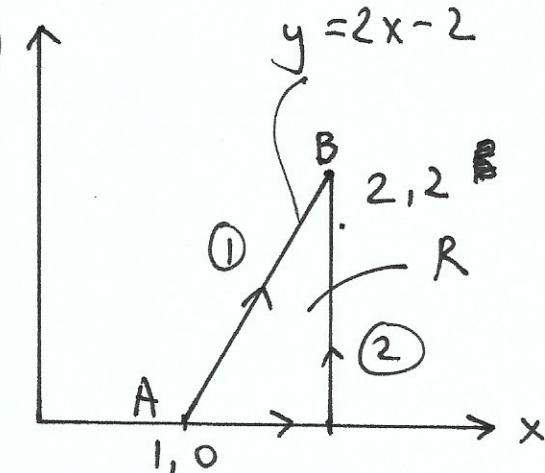
$$\therefore \int_B^A \underline{F} \cdot d\underline{r} = \frac{4}{3}$$

$$\text{path (2)} \int_A^B \underline{F} \cdot d\underline{r} = -8$$

$$\therefore \oint \underline{F} \cdot d\underline{r} = -\frac{20}{3} = \oint_P^Q 2xy dx - x^2 dy$$

Green's theorem

$$\oint \underline{F} \cdot d\underline{r} = \iint_R \frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} dx dy = -\iint_R 4x dx dy$$



(74)

$$I = - \iint_{x=1, y=0}^{2x-2} 4x \, dy \, dx = - \int_1^2 [4xy]_0^{2x-2} \, dx$$

$$I = - \int_1^2 (8x^2 - 8x) \, dx = \left[-\frac{8}{3}x^3 + 4x^2 \right]_1^2 = -\frac{20}{3}$$

as expected

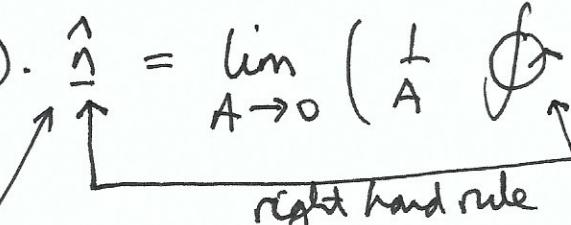
7.2 Curl definition $\nabla \times \underline{B}$

(75)

Curl is a vector that quantifies the "circulation surface density"

$$(\nabla \times \underline{B}) \cdot \hat{\underline{n}} = \lim_{A \rightarrow 0} \left(\frac{1}{A} \oint \underline{B} \cdot d\underline{s} \right)$$

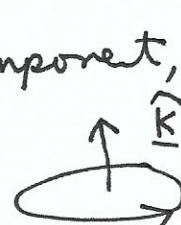
right hand rule

Curl 

unit vector $\hat{\underline{n}}$
to area



In Cartesian coords to derive e.g. $\hat{\underline{k}}$ component, consider loop of finite size and shrink.



$$\begin{aligned} \frac{1}{A} \oint \underline{B} \cdot d\underline{s} &= \frac{1}{A} \oint B_x dx + B_y dy \\ &= \frac{1}{A} \iint_R \frac{\partial B_y}{\partial x} - \frac{\partial B_x}{\partial y} dx dy \quad (\text{Green's theorem}) \end{aligned}$$

Now shrink:

$$\nabla \times \underline{B} \cdot \hat{\underline{k}} = \lim_{\substack{\delta x, \delta y \rightarrow 0 \\ A \rightarrow 0}} \frac{\iint_R \frac{\partial B_y}{\partial x} - \frac{\partial B_x}{\partial y} dx dy}{\iint dx dy} = \frac{\partial B_y}{\partial x} - \frac{\partial B_x}{\partial y}$$

Similarly

$$\nabla \times \underline{B} \cdot \hat{\underline{i}} = \frac{\partial B_z}{\partial y} - \frac{\partial B_y}{\partial z}$$

$$\nabla \times \underline{B} \cdot \hat{\underline{j}} = \frac{\partial B_x}{\partial z} - \frac{\partial B_z}{\partial x}$$

Nice summary:

$$\nabla \times \underline{B} = \begin{vmatrix} \hat{\underline{i}} & \hat{\underline{j}} & \hat{\underline{k}} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ B_x & B_y & B_z \end{vmatrix}$$

$$\text{Now } \nabla = \hat{i} \frac{\partial}{\partial x} + \hat{j} \frac{\partial}{\partial y} + \hat{k} \frac{\partial}{\partial z}$$

$$\underline{B} = \hat{i} B_x + \hat{j} B_y + \hat{k} B_z$$

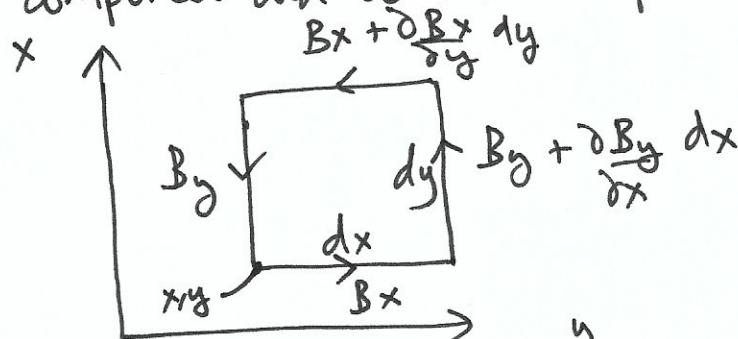
so $\nabla \times \underline{B}$ looks like cross product between 2 vectors.

More coherent to write it as

$$\nabla \times \underline{B} = \hat{i} \times \frac{\partial \underline{B}}{\partial x} + \hat{j} \times \frac{\partial \underline{B}}{\partial y} + \hat{k} \times \frac{\partial \underline{B}}{\partial z}$$

home work : check this

To understand "circulation surface density" look again at \hat{k} component and consider infinitesimal area $dxdy$



$$\oint \frac{\underline{B} \cdot d\underline{r}}{A} = \frac{B_x dx + (By + \frac{\partial B_x}{\partial y} dy) dy - (B_x + \frac{\partial B_y}{\partial y} dy) dx - By dy}{dx dy}$$

$$= \frac{\partial B_y}{\partial x} - \frac{\partial B_x}{\partial y}$$

causes rotation ↗ *causes rotation* ↘

(explains minus sign)

A conservative field has zero curl!

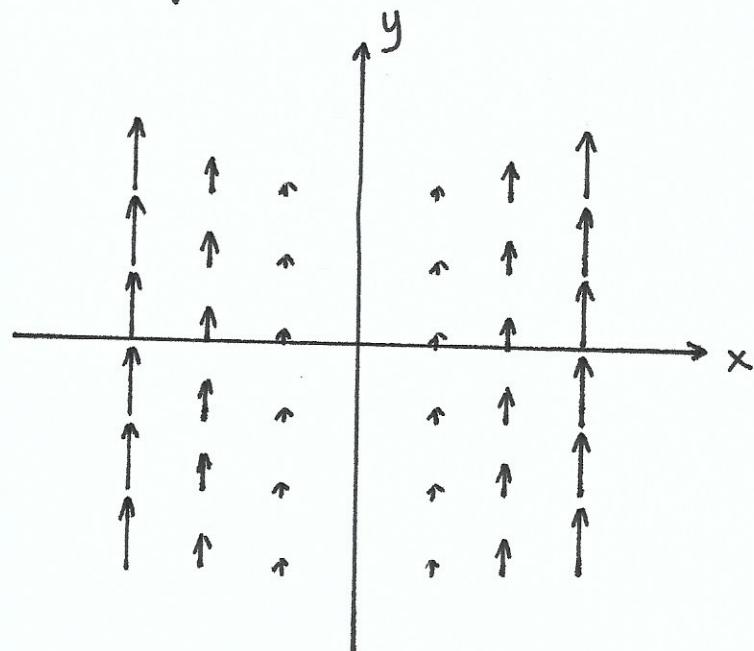
$$\nabla \times \nabla \phi = \left| \begin{array}{ccc} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ \frac{\partial \phi}{\partial x} & \frac{\partial \phi}{\partial y} & \frac{\partial \phi}{\partial z} \end{array} \right| = \hat{i} \left(\frac{\partial^2 \phi}{\partial y \partial z} - \frac{\partial^2 \phi}{\partial z \partial y} \right) + \hat{j} \dots + \hat{k} \dots$$

$\nabla \times \underline{B} = 0$ implies \underline{B} is a conservative field, or "irrotational" field

Example ① $\underline{B} = 0 \hat{i} + x^2 \hat{j} + 0 \hat{k}$

$$\nabla \times \underline{B} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ 0 & x^2 & 0 \end{vmatrix}$$

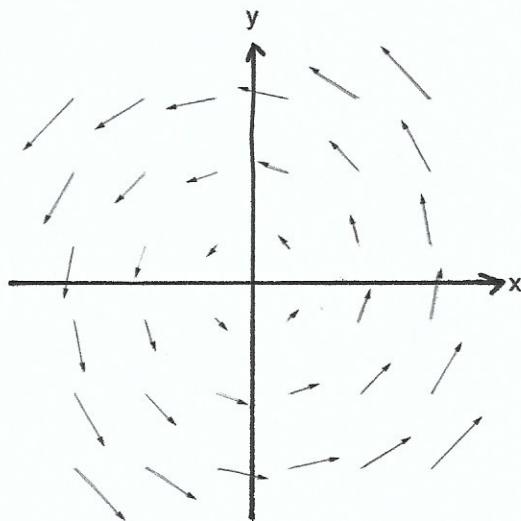
$$\nabla \cdot \underline{B} = 2x$$



Example ② $\underline{B} = -y \hat{i} + x \hat{j} + 0 \hat{k}$

$$\nabla \times \underline{B} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ -y & x & 0 \end{vmatrix}$$

$$\nabla \cdot \underline{B} = 2$$



7.3 Other coordinate systems

cylindrical polar

$$\nabla = \hat{r} \frac{\partial}{\partial r} + \frac{1}{r} \hat{\theta} \frac{\partial}{\partial \theta} + \hat{z} \frac{\partial}{\partial z}$$

$$\underline{B} = \hat{r} B_r + \hat{\theta} B_\theta + \hat{z} B_z$$

can get from "differentiate first, cross product second"

$$\nabla \times \underline{B} = \hat{r} \times \frac{\partial \underline{B}}{\partial r} + \frac{1}{r} \hat{\theta} \times \frac{\partial \underline{B}}{\partial \theta} + \hat{z} \times \frac{\partial \underline{B}}{\partial z}$$

you check ...

$$\nabla \times \underline{B} = \frac{1}{r} \begin{vmatrix} \hat{r} & \hat{\theta} & \hat{z} \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial z} \\ B_r & r B_\theta & B_z \end{vmatrix}$$

spherical polar

same procedure

$$\nabla \times \underline{B} = \frac{1}{r^2 \sin \theta} \begin{vmatrix} \hat{r} & \hat{\theta} & \hat{\phi} \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial \phi} \\ B_r & r B_\theta & r \sin \theta B_\phi \end{vmatrix}$$

Vector calculus Lecture 17 (final)

7.4 Stokes theorem

7.5 Vector identities

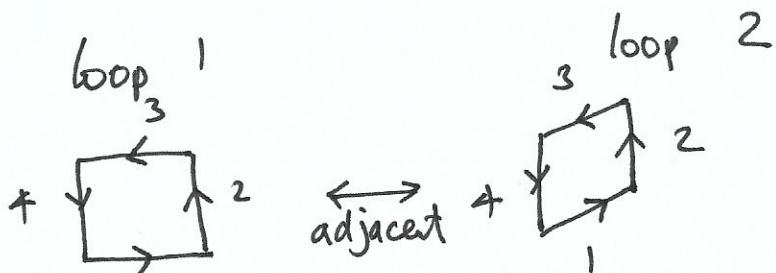
7.4 Stokes' theorem (see additional notes on Blackboard)

(79)

Consider two adjacent infinitesimal square loops, not necessarily in the same plane

$$\text{Recall } \nabla \times \underline{B} \cdot \hat{\underline{n}} = \lim_{A \rightarrow 0} \frac{\oint \underline{B} \cdot d\underline{r}}{A}$$

$$\therefore \nabla \times \underline{B} \cdot d\underline{S} = \oint \underline{B} \cdot d\underline{r} \text{ for infinitesimal loop}$$



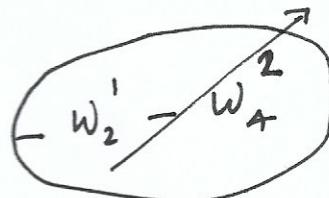
$$\text{loop 1} \quad \sum_{l=1}^4 \underline{B} \cdot d\underline{r} = \sum_{l=1}^4 w_i^1 = \nabla \times \underline{B}_1 \cdot d\underline{S}_1$$

$$\text{loop 2} \quad \sum_{l=1}^4 \underline{B} \cdot d\underline{r} = \sum_{l=1}^4 w_i^2 = \nabla \times \underline{B}_2 \cdot d\underline{S}_2$$

join the two loops together

$$\sum_{1+2}^4 \underline{B} \cdot d\underline{r} = \sum_{l=1}^4 w_i^1 + \sum_{l=1}^4 w_i^2$$

$$\text{But } w_2^1 = -w_4^2$$



$$\therefore \sum_{1+2}^4 \underline{B} \cdot d\underline{r} = \nabla \times \underline{B}_1 \cdot d\underline{S}_1 + \nabla \times \underline{B}_2 \cdot d\underline{S}_2 = \sum_{j=1}^2 \nabla \times \underline{B}_j \cdot d\underline{S}_j$$

add more loops to create a macroscopic surface attached to a large loop



$$\oint \underline{B} \cdot d\underline{r} = \iint_S \nabla \times \underline{B} \cdot d\underline{S}$$

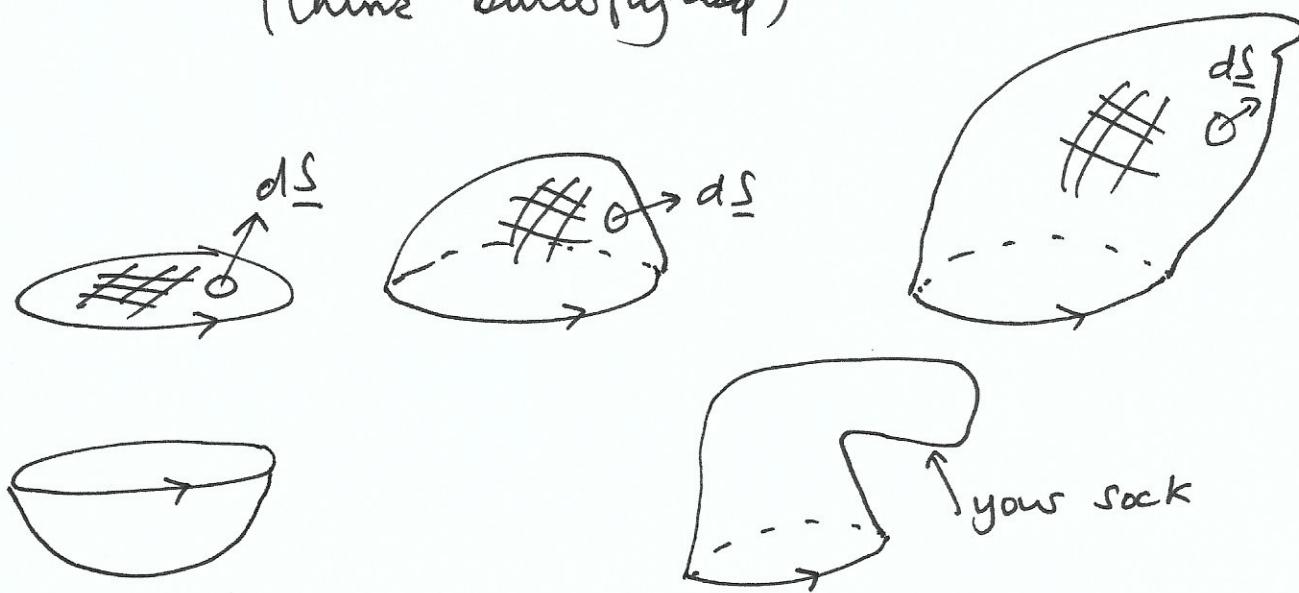
RH rule

closed

open !!!

any surface attached to the loop
 (think butterfly ^{net} loop)

(80)



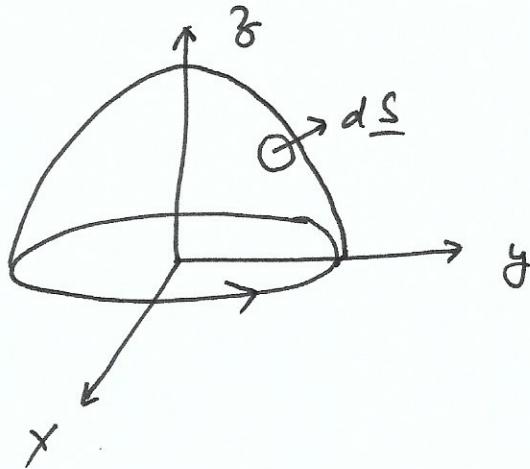
to be clear σ^{\wedge}
 orientation of $d\vec{S}$, "collapse" surface to the loop

sometimes we want a surface integral
 $\oint \mathbf{P} \times \underline{\mathbf{B}} \cdot d\vec{S}$ but line integral is easier
 \int_s or vice versa,
 or you can choose a different surface
 attached to the same loop!

(81)

Example

Hemisphere of radius a
at $z > 0$



vector field

$$\underline{B} = z \hat{i} - y \hat{j} + x \hat{k}$$

$$d\underline{S} = a^2 \sin\theta \, d\theta \, d\phi \hat{i}$$

we want to evaluate

$$\oint_C \underline{B} \cdot d\underline{r} = \iint_S \nabla \times \underline{B} \cdot d\underline{S} \quad (1) \quad (2)$$

$$\nabla \times \underline{B} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ z & -y & -x \end{vmatrix} = 2 \hat{j}$$

① in the x, y plane

$$x = a \cos\phi \quad dx = -a \sin\phi \, d\phi$$

$$y = a \sin\phi \quad dy = a \cos\phi \, d\phi$$

$$\underline{B} \cdot d\underline{r} = B_x dx + B_y dy + B_z dz = z dx - y dy = -a^2 \sin\phi \cos\phi d\phi$$

$$\oint_C \underline{B} \cdot d\underline{r} = -a^2 \int_0^{2\pi} \sin\phi \cos\phi d\phi = -\frac{a^2}{2} [\sin^2\phi]_0^{2\pi} = 0$$

(2) On the hemisphere

$$d\bar{S} = a^2 \sin \theta d\theta d\phi \hat{r}$$

$$\nabla \times \underline{B} = 2 \hat{f}$$

$$\hat{f} \cdot \hat{r} = \sin \theta \sin \phi$$

$$\iint \nabla \times \underline{B} \cdot d\bar{S} = 2a^2 \iint_{\theta=0}^{2\pi} \int_{\phi=0}^{\pi/2} \sin^2 \theta \sin \phi d\phi d\theta = 0$$

(agrees)

quicker:

choose surface in x, y plane

$$d\bar{S} = dS \hat{k}$$

$$\nabla \times \underline{B} \cdot d\bar{S} = 2 dS \hat{f} \cdot \hat{k} = 0$$

7.5 Vector identities

(83)

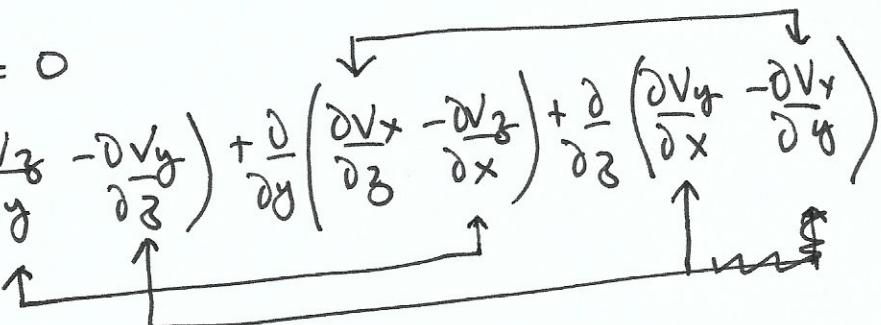
There are many.

3 are particularly important

$$\textcircled{1} \quad \nabla \times (\nabla \cdot \underline{\mathbf{B}}) = 0 \quad (\text{section 7.2})$$

i.e. if $\underline{\mathbf{B}} = \nabla \cdot \underline{\mathbf{v}}$ $\underline{\mathbf{v}}$ = "potent function"
 i.e. if ~~$\underline{\mathbf{B}} = \nabla \times \underline{\mathbf{v}}$~~ $\underline{\mathbf{B}}$ is "conservative"
 or "irrotational"

$$\textcircled{2} \quad \nabla \cdot (\nabla \times \underline{\mathbf{v}}) = 0$$

$$= \frac{\partial}{\partial x} \left(\frac{\partial v_z}{\partial y} - \frac{\partial v_y}{\partial z} \right) + \frac{\partial}{\partial y} \left(\frac{\partial v_x}{\partial z} - \frac{\partial v_z}{\partial x} \right) + \frac{\partial}{\partial z} \left(\frac{\partial v_y}{\partial x} - \frac{\partial v_x}{\partial y} \right)$$


$$= 0$$

i.e. if $\underline{\mathbf{B}} = \nabla \times \underline{\mathbf{v}}$ $\underline{\mathbf{v}}$ = "potent function"
 $\underline{\mathbf{B}}$ is "solenoidal"
 $\underline{\mathbf{v}}$ is called the vector potential

(1) + (2) read more on Helmholtz theorem to appreciate

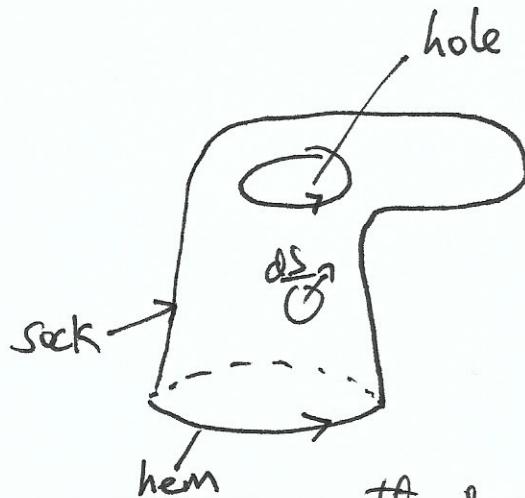
$$\textcircled{3} \quad \nabla \times (\nabla \times \underline{\mathbf{B}}) = \nabla (\nabla \cdot \underline{\mathbf{B}}) - \nabla^2 \underline{\mathbf{B}}$$

you check
 used in EM to derive wave equation

$$\nabla^2 \underline{\mathbf{B}} \equiv \hat{i} \nabla^2 B_x + \hat{j} \nabla^2 B_y + \hat{k} \nabla^2 B_z$$

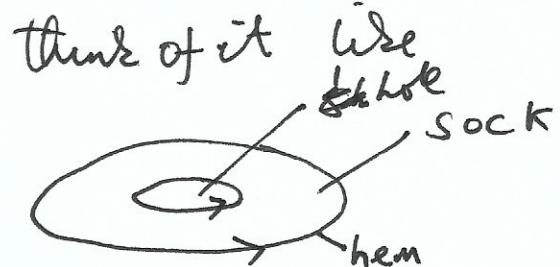
final point

8+



what is

$$\iint_{\text{SOCK} \text{ (only)}} \nabla \times \underline{B} \cdot d\underline{S}$$



now

$$\oint_{\text{hem}} \underline{B} \cdot d\underline{r} = \iint_{\text{SOCK}} \nabla \times \underline{B} \cdot d\underline{S} + \iint_{\text{hole}} \nabla \times \underline{B} \cdot d\underline{S}$$

$$\oint_{\text{hole}} \underline{B} \cdot d\underline{r} = \iint_{\text{hole}} \nabla \times \underline{B} \cdot d\underline{S}$$

$$\iint_{\text{SOCK}} \nabla \times \underline{B} \cdot d\underline{S} = \oint_{\text{hem}} \underline{B} \cdot d\underline{r} - \oint_{\text{hole}} \underline{B} \cdot d\underline{r}$$

[see 2020 exam]